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DESCRIPTION

[0001] The present invention relates to an actuator unit for moving a rigid, preferably optical, element, e.g. a mirror. It especially relates to an actuator for moving a micro mirror with a stroke of more than 9 μ m at 20V formed out of a silicon-on-insulator wafer with integrated piezoelectric actuators is presented. The primary application is a Fabry-Perot Interferometer for infrared gas spectroscopy.

[0002] In adjustable Fabry-Perot interferometers and other devices it is a challenge to provide sufficiently large and reliable displacement of a rigid optical element such as a mirror in micromechanical devices. Piezoelectric actuators have been tried but as they are limited to movements in one direction the available movements have not been sufficient. Piezoelectric thin-films integrated with MEMS allow long-stroke actuation at low voltages [1]. An additional advantage is that piezoelectric films generate large forces, thus the actuators can be made stiffer and more robust than what is possible with commonly used electrostatic actuators. The use of such elements have been discussed in WO2006/110908, and JP2007-206480, both showing the use of piezoelectric actuators moving a rigid element. Both, however, rely of the us a bendable beams for controlling the position and orientation of the element, which is at the cost of production complexity and long term reliability of the unit.

[0003] US-B1-7359124 and US-B1-7369723 disclose tunable MEMS type microlenses comprising bendable membranes and piezoelectric actuators.

[0004] US-B1-6178033 discloses a MEMS tilt mirror device comprising a bendable membrane and electrostatic actuators.

[0005] US-A1-2004/0027671 discloses a MEMS type Fabry-Perot etalon comprising electrostatic deformable membrane actuators.

[0006] EP-A1-1684406 discloses a MEMS type mechanism for in-plane motion comprising extendable piezoelectric beams.

[0007] EP-B1-1148561 discloses an acceleration sensor comprising a rigid body supported by a flexible membrane comprising a piezoelectric electro-restrictive layer.

[0008] Thus it is an object of the present invention to provide a compact actuator unit being inexpensive in production using MEMS technology and providing a robust and reliably unit being controllably within the accuracy necessary for optical use such as interferometers.

[0009] The object of this invention is obtained by providing an actuator unit according to claim 1, a reflecting device according to claim 9 and an interferometer according to claim 10.

[0010] According to the invention a novel micromirror is presented which is vertically deflected

by using a double ring push-pull actuator. The micromirror has a wide range of applications in optics and microoptics, but the primary purpose is a Fabry-Perot Interferometer for infrared gas spectroscopy [2, 3].

[0011] The actuator unit is compatible with standard MEMS production and provides a robust means for moving micromirrors or similar rigid devices with sufficient accuracy.

[0012] The invention is described below with reference to the accompanying drawings illustrating the invention by way of examples, wherein

Figure 1a,b

illustrates a moveable micro mirror according to the invention.

Figure 2a,b

illustrates a preferred embodiment of the embodiment illustrated in figure 1a,b.

Figure 3

illustrates a preferred embodiment of the invention used in a Fabry-Perot interferometer.

Figure 4

shows the obtained deflection of an embodiment as illustrated in figure 2a,b.

Figure 5a-c

illustrates alternative embodiments of the invention based on essentially circular membrane and piezoelectric actuators.

Figure 6a-c

illustrates alternative embodiments of the invention.

Figure 7a-g

illustrates the process of producing the embodiment illustrated in figure 6a,b,c.

[0013] Figure 1a and b illustrates a 3D-model of a rigid element 1, e.g. a micro mirror, formed out of an SOI wafer comprising a thin silicon device layer 2, a buried oxide layer 6 and thick silicon handle layer 7. The device is provided with a ring-shaped piezoelectric actuator 3 positioned on membrane defining the coupling area 2a between the frame 4 and the rigid element 1. The actuator 3 deflects the disc with an open aperture in the center (Figure 1a). The rigid element disc 1 has the full thickness of the handle silicon wafer 7 and is held in place by the thin device silicon layer 2 constituting the membrane 2a around the edge of the disc 1. The membrane 2a is shown as a continuous membrane surrounding the rigid element, but may have openings in suitable positions, e.g. for pressure equalization between the cavity beneath the element and the environment. The optical element 1 is rigid so as to maintain essentially the same shape when moved by the actuator element 3 and the actuator element 3 is preferably positioned close to either the frame 4 or the rigid element 1, so that when the piezoelectric material contracts the part of the actuator positioned on the membrane is bent upward thus pulling the membrane in that direction.

[0014] The device shown in figure 1a,b is formed out of a silicon-on-insulator (SOI) wafer as described above by etching away the device silicon 2 as well as the buried oxide 6 in the

central portion of the device, as seen in the top view of Figure 1a. The bottom side is shaped as seen in the bottom view of Figure 1b, where the handle silicon layer 7 of the SOI has been etched through to the buried oxide 6, leaving a rigid element, e.g. constituting a stiff disc-shaped mirror plate 1 which is held in place by the device silicon layer 2a constituting a membrane around circumference of the rigid element 1 on its top side. A ring-shaped (i.e. annulus) piezoelectric film 3 is structured on top of the thin device silicon holding the central disc, the piezoelectric film preferably being made from lead zirconate titanate (PZT). Upon actuation, the piezoelectric film contracts in the radial direction, causing the bending of the device silicon membrane 2a through a bimorph effect. Due to the circular symmetry of the structure, this bending causes an out-of-plane deflection of the disc 1. This way an actuator unit may according to a preferred embodiment of the invention be produced being constructed from one single SOI element with PZT actuator elements applied on the surface, thus being suitable for simple and cost efficient production.

[0015] The preferred design contains two ring shaped actuators 3a,3b , as shown in Figure 2a and 2b. This allows push-pull actuation of the central disc, as illustrated in Figure 2b as the membrane 2a is bent upward when outer actuator 3b is contracted while the membrane is bent downward when the inner actuator 3a is contracted. As both the frame and the rigid element are rigid the outer actuator (largest diameter) will pull the membrane and thus the optical upwards, while actuation of the inner disc (smallest diameter) will pull the membrane and thus the rigid element downwards. This solution extends the possible range of movement for the rigid element 1.

[0016] The primary application of the rigid element as a disc-shaped micromirror is as part of a Fabry-Perot Interferometer illustrated in Figure 3. In this application, the top surface of the disc 1 is coated with an antireflective (AR) layer 11 while it is the bottom surface which acts as a mirror for the light 13 passing through the unit, but other choices may be made depending e.g. on the required distance 15 between the mirrors 16,17 formed by the surfaces above and below the cavity. The mirrors 16,17 may either be provided with reflective coatings or the refractive index of the material itself, like silicon, may provide the necessary reflectivity. By bonding (on wafer scale) the mirror to a second un-structured silicon wafer 10 which is also AR-coated on one side 12, a cavity 15 is formed in which light can undergo multiple reflections. The AR coating 11,12 and possible reflecting coatings within the resonator cavity may be provided in any suitable way, e.g. using dielectric layers at suitable thicknesses or photonic crystals.

[0017] The height of the gap 15 determines which wavelength will interfere constructively and thus be fully transmitted through the interferometer. For the FP-interferometer to be applicable to infrared spectroscopy in the wavelength range 3-1 μ m, a stroke of several micrometers is desirable for sufficient tunability. The Fabry-Perot Interferometer is formed by the disc-shaped micromirror which is bonded to a second silicon wafer using adhesive bonding with a polymer such as BCB 9.

[0018] As is illustrated in figure 3 the Fabry-Perot may include leakage channels in the BCB

layer 9 for pressure equilibration as well as end stops 14. The end stops 14 may be used for calibration, as the rigid element may be positioned at the end stops and the position may be controlled relative to this. As will be discussed below different types of position measuring means may be used, such as using optical, capacitive or piezoresistive measuring means. An end stop for the upward movement may also be provided e.g. in a housing enclosing the interferometer.

[0019] The micromirrors were fabricated as part of a multi-project-wafer (MPW) process developed and standardized for industrial use as described in [1], being included here by way of reference and will not be described in detail here. In this process the piezoelectric elements are mounted on the membrane, and the piezoelectric film used to form the actuators is lead zirconate titanate (PZT) which is sandwiched between a bottom platinum electrode and a top electrode made by gold. For the fabrication of the micromirror, the wet-etch of the backside cavity was replaced by deep reactive ion etching (DRIE) for better dimensional control.

[0020] Other means for mounting the piezoelectric elements 3 on the membrane area 2a may also be contemplated depending on the available technology and intended use of the element.

[0021] The starting SOI wafer used according to the preferred embodiment of the invention has 380µm handle silicon 7, 300nm buried oxide 6, and a device silicon layer 2 of 8µm. For the fabrication of the micromirrors, the backside etch was carried out using deep reactive ion etching (DRIE).

[0022] Note that the micromirror is designed so that the part of the device silicon layer holding the central mirror disc is not structured in the region where it bridges the backside gap etched into the handle silicon, but forms a continuous membrane. This increases the robustness of the structure significantly and keeps the monocrystalline silicon free from any defect which could easily form cracks if strained in the fabrication process.

[0023] After dicing, the piezoelectric actuators of the finished devices were poled by applying 20V at a temperature of 150°C for 10 minutes.

[0024] Measurements have been performed using a finished micromirror of the type shown in Figure 2. where the region in the middle is the clear aperture, which for the device shown has a diameter of 3 mm and the double ring actuators 3a,3b have top electrodes 3c,3d of gold.

[0025] The actuation characteristic of the mirror was measured with a ZYGO white light interferometer. The mirror was pushed downwards by applying 20V to the inner actuator, and upward with a voltage of 20V is applied to the outer ring. Note that the mirror disc remains perfectly flat in both cases. This is due to the high stiffness of the silicon disc which has the full thickness of the handle silicon wafer.

[0026] The high stiffness of the mirror disc also allows the fabrication of much larger diameter mirrors than the 3 mm presented here. The structures formed were found to be incredibly

robust, thus apertures of 5-10 mm should be feasible.

[0027] The complete characteristic for the micromirror with the two actuators is shown in Figure 4. A total stroke of $9.3\mu\text{m}$ for the mirror plate is achieved when applying an actuation voltage of 20V to each of the two actuators in sequence. The hysteresis is a typical feature of PZT-based actuators. Feedback is needed for accurate positioning. This can be done optically by using a reference laser. In future designs, however, piezoresistors will be added to the device silicon which is part of the actuators to allow closed-loop operation and highly accurate positioning of the mirror. The actuation characteristic of the micromirror thus provides an actuator in which voltage sweep going from 0 to 20 V applied to the outer actuator ring generates the upper curve, while applying the same sweep to the inner ring generates the lower curve. The total stroke is $9\mu\text{m}$.

[0028] Thus a micromirror was presented, which achieves a stroke of $9\mu\text{m}$ at 20V by using a dual ring, push-pull actuator. The mirror is formed out of the handle silicon of an SOI wafer. The high stiffness ensures a high planarity upon actuation. Large mirrors with apertures of more than 3mm were successfully fabricated. The mirror is highly suited for its primary application which is a Fabry-Perot Interferometer for gas spectroscopy.

[0029] Figures 5a-5c illustrates embodiments of the invention based on the ring shaped membrane 2a providing the coupling means between the rigid element 1 and the frame 4. In figure 5a piezoresistors 5 are positioned beneath the piezoelectric actuator 3, thus measuring the bend in the membrane at the same position that the bend is provided.

[0030] Figure 5b illustrates that the rigid element, while being rigid at the edges, may have a rigid frame enclosing a hole or hollow area having a thin central membrane.

[0031] Figure 5c illustrates another ring shaped membrane 2a but wherein the actuator is split along the circumference into four sections $3a_1, 3a_2, 3a_3, 3a_4$. According to the preferred embodiment of the invention corresponding inner actuator parts will be provided. In figure 5c the position measuring means being provided as piezoresistors 5 are positioned in the gaps between the actuator sections. An advantage with the split actuator sections is that they may provide a tilt movement in addition to the translational movement and thus some adjustments or calibrations in the position and orientation of the rigid element.

[0032] Figures 6a, and 6b illustrates an alternative embodiment of the invention, wherein rigid element 1 has a central opening and an optical element 17a made from a glass or quartz is fastened to it, as is seen in the cross section of the unit shown in figure 6b. Thus the rigid element 1 may comprise an element 17a having a suitable transmission spectrum suitable for the relevant wavelengths if used in an optical measurement such as a Fabry-Perot filter. This way the unit may be used in the visible, near infrared or ultra violet ranges, depending on the chosen material, while a rigid element 1 made from silicon will be suitable for wavelengths above approximately 1100nm.

[0033] Figures 7a-7g describes the production process for making the unit shown in figure 6b, where the drawings show cross sections of the unit in different stages of the production.

[0034] As can be seen in figures 7a and 7b this unit shares the same starting point as the other embodiments discussed above, starting with an SOI structure with a piezoelectric actuator ring as discussed with reference to figures 1a,3 and 5a, and wherein the device layer is etched from the area to be used as rigid element 1.

[0035] The top of the unit carrying the piezoelectric actuator is then bonded temporarily to a carrying wafer 20 as shown in figure 7c. This may be performed using a polymer 21 such as WaferBOND from Brewer Science. The central area as well as the membrane area is then etched away as shown in figure 7d leaving an opening in the central area where the device layer was removed and a membrane where the device layer was intact.

[0036] A glass or quartz layer is then bonded to the unit from below, e.g. using BCB bonding, as illustrated in figure 7e. The bonding has to be strong enough to keep the wafer and glass connected permanently, and BCB bonding is suitable due to the combination of relatively low temperature and high strength.

[0037] The active part 17a of the optical element constituting a part of the rigid element is then separated from the rest of the glass or quartz layer by in example powder blasting, leaving the structure illustrated in figure 7f.

[0038] After removing the temporary carrying wafer the unit is finished and may be mounted in an optical unit similar to the unit illustrated in figure 3, but where the unstructured silicon layer 10 may be a glass or quartz layer being transparent in the same wavelength ranges as the transparent part 17a of the rigid element 1. Suitable anti reflection and reflective layers may be applied to the surfaces in any well known suitable manner.

[0039] To summarize the invention thus relates to an actuator for moving a rigid element, e.g. an optical element such as a lens, a mirror or an at least partially transparent and partially reflective window, where the element is mechanically coupled to a frame with a bendable membrane providing a coupling. Actuator elements are mounted on said coupling membrane between the frame and element, the membrane and actuator elements being adapted to provide a movement to the element when subject to signal from a signal generator. Preferable the actuator elements are constituted by at least piezoelectric element mounted on said coupling membrane being adapted to bend said coupling at the application of a voltage, as the piezoelectric element is adapted to contract in the direction of the coupling between the frame and the rigid element.

[0040] In an especially preferred embodiment each actuator element is constituted by two PZT elements, the first being mounted on the coupling close to the frame, the second being mounted on the coupling close to the rigid element, and coupled to the signal generator in such a way as to be operated independently of each other or preferably in an alternative

fashion so that one of them moves the rigid element in a first direction and the other moves the rigid element in the direction opposite of the first.

[0041] In one embodiment of the invention the coupling is constituted by a thin, circular section of the frame, said at least one piezoelectric element extending along the coupling. In a preferred version two piezoelectric elements are used as described above to increase the length of movement.

[0042] The actuator may be provided with position measuring means to provide feedback on the position of the rigid element relative to the frame, and in the embodiment using piezoelectric elements 3 the position measuring means is preferably also a piezoresistive element 5 provided on the coupling to monitor the bend of the coupling. The piezoresistive elements 5 may be positioned beneath the piezoelectric actuators 3 or in other positions where the coupling is bent.

[0043] The piezoresistors can be made in the silicon on insulator layer by ion implantation and subsequent annealing. With this doping procedure a pn-junction can be produced, which defines the geometry of the resistors. The resistor can be contacted with additional, higher doped areas which are connected with a metallization layer on the surface in later process steps. The process steps to fabricate the piezoresistors can be performed before depositing the bottom electrode for the piezoelectric layer. Such doped piezoresistors are used as stress sensors and normally assembled in a Wheatstone bridge configuration with four bendable resistors. Other configurations e.g. a half bridge are also possible depended on the available space in the mechanical structure and process tolerances. Instead of piezoresistors optical or capacitive solutions may be used to measure the position of the rigid element.

[0044] As illustrated in figure 3 the invention also relates to an interferometer according to claim 10. The rigid element has an at least partially reflective surface, the frame being mounted in a housing comprising a second reflective surface, at least one of the reflective surfaces being provided on an at least partially transparent body and the two reflective surfaces being positioned at a distance from each other constituting a Fabry-Perot element, the distance being adjusted by the movements induced by said actuator elements.

[0045] There is also disclosed a reflecting device including an actuator, where the rigid element constitutes a mirror or is at least partially transparent within a chosen wavelength range and the piezoelectric actuators are divided into individually controlled circle segments being capable of tilting the rigid element so as to adjust for misalignment or direct the light in a chosen direction.

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[0046]

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- **NORBERT NEUMANNMARTIN EBERMANNSTEFFEN KURTHKARLA HILLER**Tunable infrared detector with integrated micromachined Fabry-Perot filterJ. Micro/Nanolith. MEMS MOEMS, 2008, vol. 7, 021004- [0046]

PATENTKRAV

1. Aktuatorenhed af en MEMS-type til bevægelse af et stift element (1) f.eks. et optisk element, aktuatorenheden omfatter en ramme (4) og en bøjelig membran (2a), der omslutter elementet, periferien af det stive element (1) er mekanisk koblet til nævnte ramme (4) gennem nævnte bøjelige membran (2a), hvor nævnte aktuatorenhed omfatter mindst et aktuatorelement (3), der er monteret på nævnte bøjelige membran (2a) mellem rammen (4) og det stive element (1), hvilket definerer et koblingsområde, **kendetegnet ved**, at den bøjelige membran (2a) og aktuatorelementet er indrettet til tilvejebringe en bevægelse i en retning ud af membranplanet mod det stive element (1), når det udsættes for et signal fra en signalgenerator ved at bøje nævnte bøjelige membran (2a), hvor nævnte mindst ene aktuatorelement (3) udgøres af to piezoelektriske elementer (3a, 3b) monteret på den bøjelige membran (2a) beregnet til at bøje nævnte membran ved påføring af et signal, og hvor en første af nævnte piezoelektriske elementer (3b) er monteret i koblingsområdet, der vender imod det stive element (1) således, at det er i stand til at trække det stive element både op og ned.
2. Aktuator ifølge krav 1, hvor den bøjelige membran (2a) består af et tyndt, cirkulært udsnit af membranen, nævnte piezoelektriske elementer (3a, 3b) er ringformede elementer, der forløber langs med membranen omkring det stive element (1).
3. Aktuator ifølge krav 2, hvor det ringformede piezoelektriske element er opdelt i et antal individuelt styrede sektioner.
4. Aktuator ifølge krav 1, hvor aktuatoren er opdelt i fire sektioner (3a1, 3a2, 3a3, 3a4) fordelt langs den bøjelige membran (2a), der omslutter det stive element (1).
5. Aktuator ifølge krav 1 omfattende et positionsmåleorgan, der overvåger positionen af det stive element (1) i forhold til rammen (4).
6. Aktuator ifølge krav 5, hvor positionsmåleorganet inkluderer en piezomodstand (5) påført i en position på koblingen for at indikere bøjning af koblingen og dermed positionen af det optiske element i forhold til rammen.

7. Aktuator ifølge krav 5, hvor positionsmåleorganet inkluderer en kapacitiv eller optisk føler beregnet til at måle positionen af det optiske element i forhold til rammen.
8. Aktuator ifølge krav 1, hvor nævnte mindst ene piezoelektriske aktuator er en bly zirkonat titanat (PZT) aktuator.
9. Reflekteringsindretning inkluderende en aktuator ifølge krav 1, hvor det stive element (1) omfatter et spejl.
10. Interferometer inkluderende en aktuatorenhed ifølge krav 1, hvor det optiske element har en i det mindste delvist reflekterende overflade (16), idet rammen (4) er monteret i et hus omfattende en anden reflekterende overflade (17), hvor mindst en af de reflekterende overflader er tilvejebragt på et mindst delvist transparent legeme og de to reflekterende overflader (16, 17) er placeret i en afstand fra hinanden og udgør et Fabry-Perot-element, hvor afstanden justeres af bevægelserne forårsaget af nævnte aktuatorelementer (3).
11. Interferometer ifølge krav 10, hvor den bøjelige membran (2a) består af et tyndt, cirkulært udsnit af rammen, idet nævnte mindst ene ringformede piezoelektriske element forløber langs den bøjelige membran (2a) rundt om det stive element.
12. Interferometer ifølge krav 11, hvor det ringformede piezoelektriske element er opdelt i et antal individuelt styrede sektioner.
13. Interferometer ifølge krav 10, hvor aktuatoren er opdelt i fire sektioner (3a1, 3a2, 3a3, 3a4) fordelt langs den bøjelige membran (2a), der omslutter det stive element (1).
14. Interferometer ifølge krav 10 omfattende et positionsmåleorgan, der overvåger positionen af det stive element (1) i forhold til rammen (4).
15. Interferometer ifølge krav 14, hvor positionsmåleorganet inkluderer en piezomodstand (5) påført i en position på koblingen for at indikere bøjning af koblingen og dermed positionen af det optiske element i forhold til rammen.

16. Interferometer ifølge krav 14, hvor positionsmåleorganet inkluderer en kapacitiv eller optisk føler beregnet til at måle positionen af det optiske element i forhold til rammen.
- 5 17. Interferometer ifølge krav 10, hvor nævnte mindst ene piezoelektriske aktuator er en bly zirkonat titanat (PZT) aktuator.

DRAWINGS

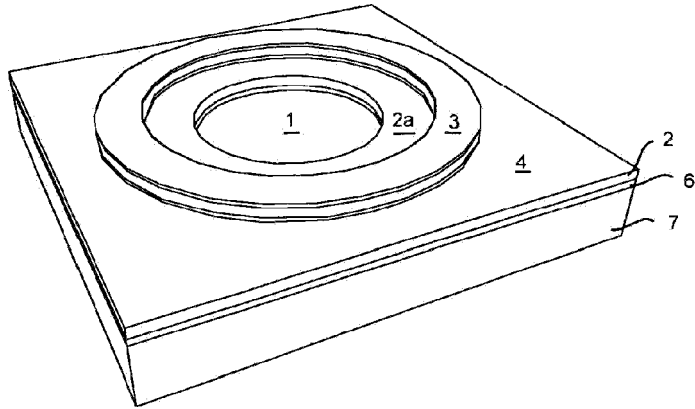


FIG. 1a

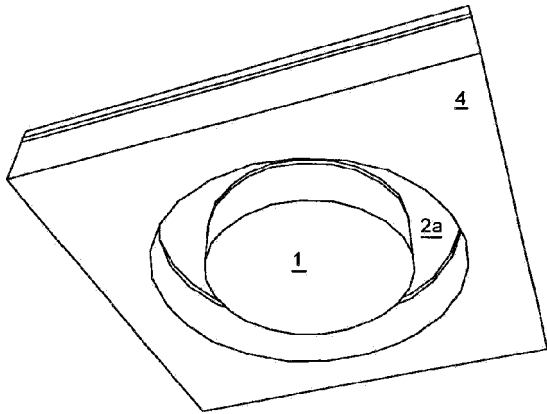


FIG. 1b

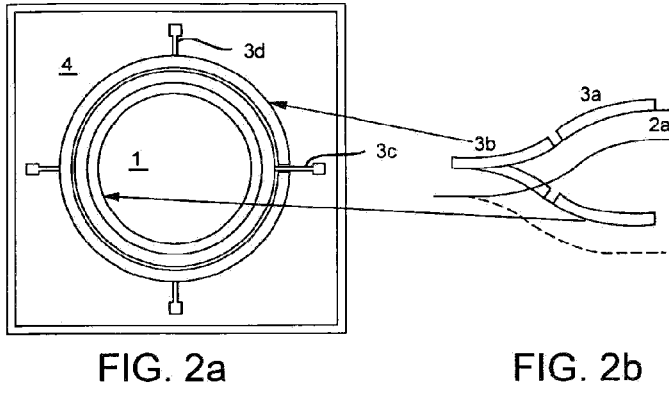


FIG. 2a

FIG. 2b

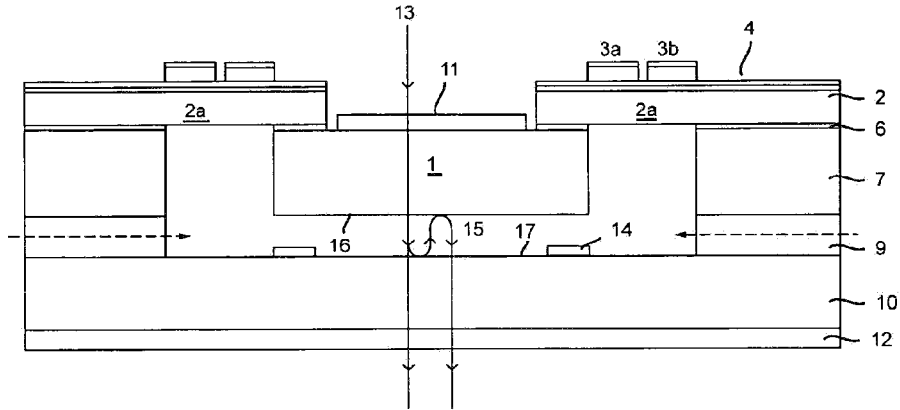


FIG. 3

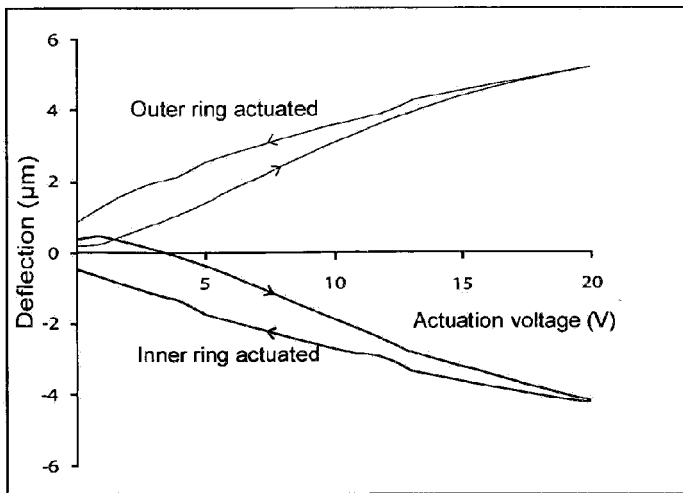


FIG. 4

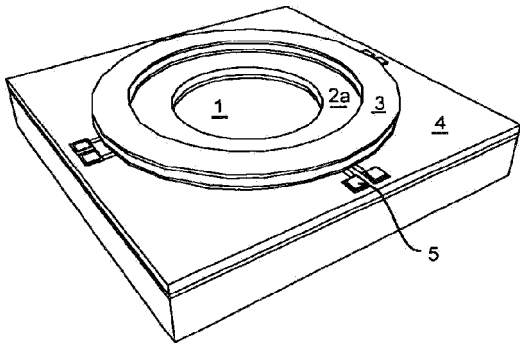


FIG. 5a

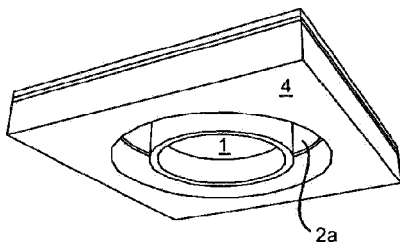


FIG. 5b

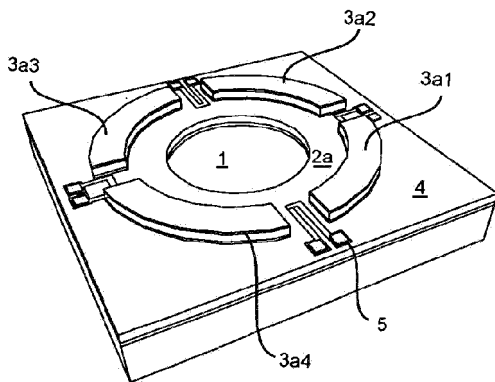


FIG. 5c

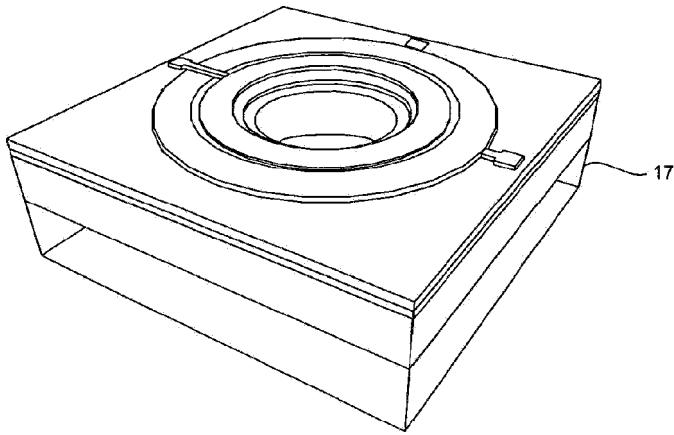


FIG. 6a

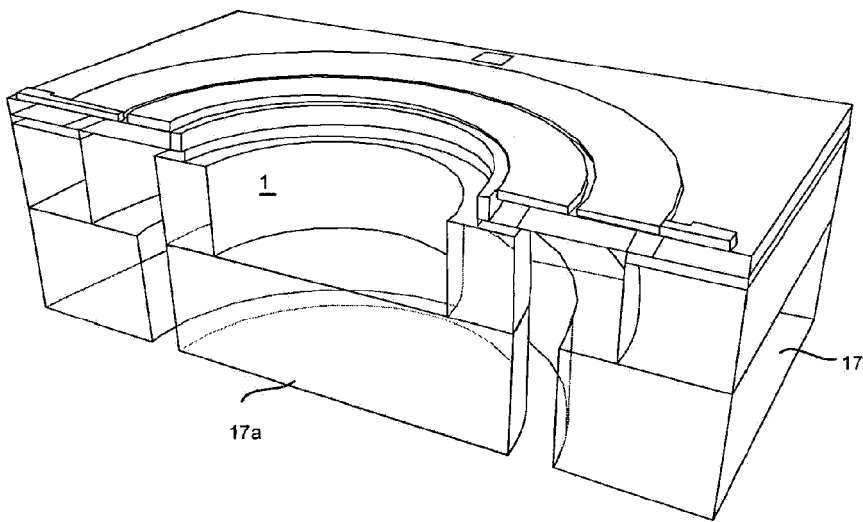


FIG. 6b

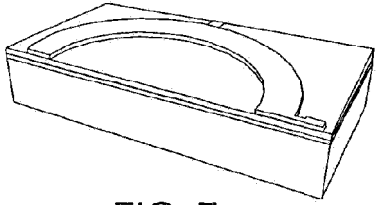


FIG. 7a

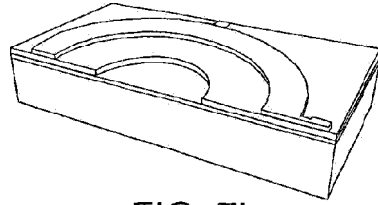


FIG. 7b

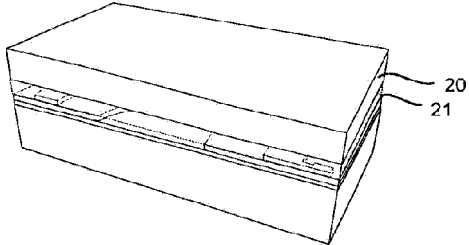


FIG. 7c

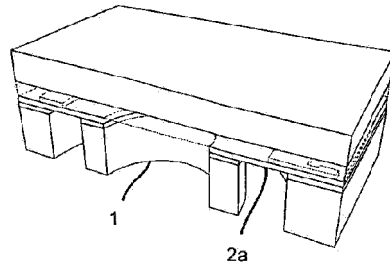


FIG. 7d

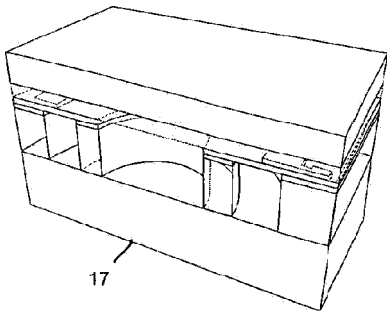


FIG. 7e

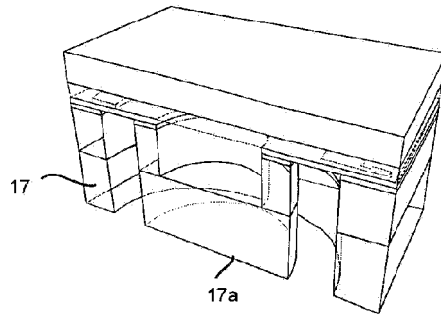


FIG. 7f

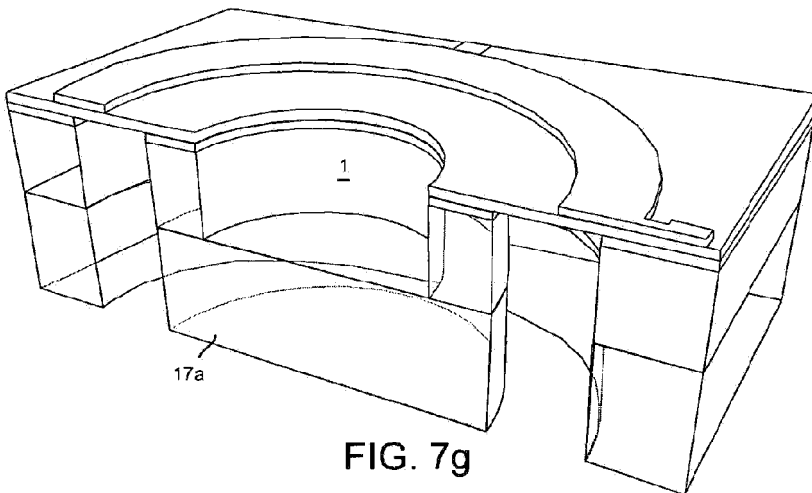


FIG. 7g