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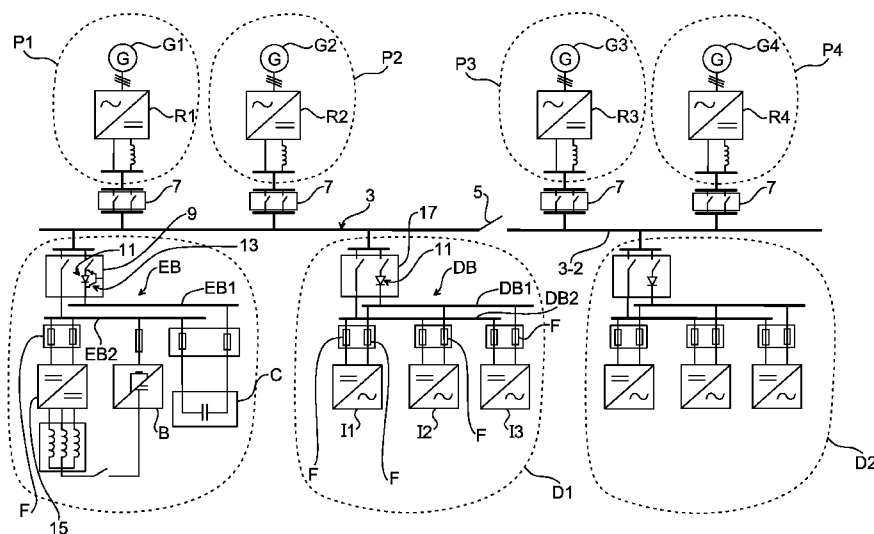


Fig. 1

(57) Abstract: It is presented a DC-power system (1) comprising a main DC bus(3), a power generating unit (P1, P2, P3, P4) arranged to feed the main DC bus(3), an isolator switch arranged (7) between the main DC bus (3) and the power generating unit (P1, P2, P3, P4) for isolating the power generating unit (P1, P2, P3, P4) from the main DC bus (3) in case of a main DC bus fault, a drive unit (D1, D2) arranged to be fed by the main DC bus, wherein the drive unit (D1, D2) comprises a drive unit bus system(DB), converter units (I1, I2, I3) connected to the drive unit bus system(DB), and fuses (F) arranged between the drive unit bus system (DB) and the converter units (I1, I2, I3) for protecting the converter units (I1, I2, I3) in case of a drive unit fault.

## **A DC-POWER SYSTEM WITH SYSTEM PROTECTION CAPABILITIES**

### **TECHNICAL FIELD**

- 5 The present disclosure generally relates to power systems and in particular to a DC-power system with protection capabilities.

### **BACKGROUND**

- Power systems typically comprise a plurality of components, such as one or more power generation source, drives and energy storage modules. These  
10 components are typically interconnected by means of a busbar system in which currents can flow for providing power to one or more loads connected to the power system.

- At some point a fault, such as a short circuit will inevitably occur in the power system, either in the busbar system, in one of the components of the system,  
15 or in a load. In case of a fault, it is important to isolate the fault from the healthy part of the system such that normal power provision can be continued by means of the healthy part, and for protecting the healthy parts from being damaged. For this purpose, a protection system is typically included in the power system.

- 20 A protection system arranged to handle faults in a power system typically comprise monitoring equipment arranged to monitor electrical parameters such as currents in the power system, and circuit breakers controlled by the monitoring equipment. The circuit breakers are arranged in such a way in the power system that selective fault isolation can be obtained in case of a fault.

- 25 Existing protection systems can however in some applications be both very expensive and space consuming.

## SUMMARY

Direct current (DC) circuit breakers are particularly large, because on the contrary to alternating current circuit (AC) breakers, they cannot depend on zero crossings. Therefore, larger air gaps are needed for DC circuit breakers  
5 to ensure proper protection. As a result, DC circuit breakers typically consume large amounts of space, and they are expensive to manufacture.

In view of the above considerations, a general object of the present disclosure is to provide a DC-power system that has protective capabilities that requires less space than the prior art.

10 Another object is to provide a DC-power system that is affordable.

Hence, there is provided a DC-power system comprising: a main DC bus, a power generating unit arranged to feed the main DC bus, an isolator switch arranged between the main DC bus and the power generating unit for isolating the power generating unit from the main DC bus in case of a main  
15 DC bus fault, and a drive unit arranged to be fed by the main DC bus, wherein the drive unit comprises a drive unit bus system, converter units connected to the drive unit bus system, and fuses arranged between the drive unit bus system and the converter units for protecting the converter units in case of a drive unit fault.

20 Thereby, the various units in the DC-power system can selectively be protected in case of faults in any of the units or on the main DC bus, without the use of large, space consuming and expensive circuit breakers.

According to one embodiment, the drive unit comprises a first type of input unit arranged between the main DC bus and the drive unit bus system, and  
25 wherein the first type of input unit comprises an isolator switch for disconnecting the drive unit from the main DC bus in case of a drive unit fault. Hence, the drive unit can be disconnected from the remaining DC-power system in case of a fault in the drive unit without the utilisation of circuit breakers.

According to one embodiment, the first type of input unit comprises a current blocking device arranged to block currents in a direction from the drive unit bus system to the main DC bus and to allow current to flow from the main DC bus to the drive unit. Thereby, fault currents that would be provided to a fault  
5 on the main DC bus or in another unit connected to the main DC bus from the capacitor banks of the converter units in the drive unit can be reduced or eliminated, as the current blocking device acts essentially as an open circuit in the direction from the drive unit bus system to the main DC bus.

One embodiment comprises an energy storage unit arranged to feed the main  
10 DC bus, wherein the energy storage unit comprises an energy storage unit bus system, power provision units, and fuses arranged between the energy storage unit bus system and the power provision units for protection of the power provision units in case of an energy storage unit fault. Thus, if a backup power component for e.g. redundancy purposes is added to the  
15 system, also this component can be protected from internal faults without the utilisation of circuit breakers.

According to one embodiment, the energy storage unit comprises a second type of input unit arranged between the energy storage unit bus system and the main DC bus, wherein the second type of input unit comprises an isolator  
20 switch for disconnecting the energy storage unit from the main DC bus in case of an energy storage unit fault. Thus, the energy storage unit can be disconnected from the main DC bus without the utilisation of circuit breakers.

According to one embodiment, the second type of input unit comprises a  
25 current blocking device arranged to block currents in a direction from the energy storage unit bus system to the main DC bus and to allow current to flow from the main DC bus to the energy storage unit, and a semiconductor switching unit for selectively allowing current to bypass the current blocking device and flow to the main DC bus. Hence, current can be allowed to flow  
30 into the main DC bus in case of additional power is needed from the energy storage unit by setting the semiconductor switching unit in its on-state.

Alternatively, fault currents from the energy storage unit to a fault on the main DC bus or in another part of the DC-power system can be minimized in case the semiconductor switching unit is set in its off-state.

According to one embodiment, the current blocking device and the  
5 semiconductor switching unit are connected in anti-parallel.

According to one embodiment, the power generating unit comprises a generator and a rectifier, wherein the rectifier includes a plurality of fuses arranged to protect the rectifier in case of a rectifier fault. Thereby, internal rectifier faults can be handled by means of the fuses without utilising local  
10 circuit breakers in the power generating unit.

According to one embodiment, the plurality of fuses included in the rectifier are dimensioned such that they do not blow when subjected to fault currents as a result of faults downstream of the rectifier. Hence, fuses are only blown by currents caused by internal faults in the rectifier. Fault currents provided  
15 to faults outside the power generating unit should thus not trigger the fuse to blow. The current rating of the fuses in the rectifier should hence be selected to be at a threshold current level that is only reached or exceeded by fault currents created by rectifier faults in that particular power generating unit.

According to one embodiment, each converter unit has terminals connected  
20 to the drive unit bus, wherein each terminal of a converter unit is connected to a fuse.

According to one embodiment, the current blocking device is a diode.

According to one embodiment, the first input unit comprises a semiconductor switching unit connected in anti-parallel with the current  
25 blocking device for selectively allowing current to bypass the current blocking device and flow to the main DC bus.

By combining fuses and isolator switches as disclosed herein, a hybrid protection system is obtained where local faults, i.e. faults in a specific unit, are handled by fuses, and where global faults, i.e. faults on the main DC bus,

are handled by interruption of current at the source such that an appropriate isolator switches can isolate the affected part of the DC-power system.

Thereby fuse sizes can be kept smaller, ensuring that the magnitude of the local fault currents will be able to blow the fuse in case of a local fault, thus  
5 ensuring dependable DC-power system protection both locally and globally.

If necessary, additional capacitor banks can be installed to provide extra fault current to ensure that fuses have enough fault current available to clear a fault.

Generally, all terms used in the claims are to be interpreted according to their  
10 ordinary meaning in the technical field, unless explicitly defined otherwise herein. All references to "a/an/the element, apparatus, component, means, etc. are to be interpreted openly as referring to at least one instance of the element, apparatus, component, means, etc., unless explicitly stated otherwise.

## 15 **BRIEF DESCRIPTION OF THE DRAWINGS**

The specific embodiments of the inventive concept will now be described, by way of example, with reference to the accompanying drawings, in which:

Fig. 1 is a schematic diagram of a DC-power system;

Fig. 2 is a schematic diagram of a power generating unit in the DC-power  
20 system in Fig. 1;

Fig. 3a depicts an example of a fault in the DC-power system in Fig. 1; and

Fig. 3b depicts another example of a fault in the DC-power system in Fig. 1.

## **DETAILED DESCRIPTION**

The inventive concept will now be described more fully hereinafter with  
25 reference to the accompanying drawings, in which exemplifying embodiments are shown. The inventive concept may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather, these embodiments are provided by

way of example so that this disclosure will be thorough and complete, and will fully convey the scope of the inventive concept to those skilled in the art. Like numbers refer to like elements throughout the description.

Fig. 1 depicts a schematic diagram of one example of a DC-power system 1.

5 The DC-power system 1 comprises a main DC bus 3 having a first busbar 3-1 and a second busbar 3-2 separable by means of a bustie breaker 5, a first power generating unit P1, a second power generating unit P2, a third power generating unit P3, a fourth power generating unit P4, an energy storage unit E, a first drive D1 and a second drive D2.

10 The first drive unit D1 and the second drive unit D2 are arranged to power electrical motors or similar equipment. Examples of such drive units are single drives, multi drives and static frequency converters intended to supply normal AC consumers with 50 Hz or 60 Hz AC power.

The DC-power system 1 further comprises isolator switches 7, i.e.  
15 disconnectors, associated with a respective power generating unit P1, P2, P3, P4 for being able to disconnect the power generating units P1, P2, P3, P4 from the main DC bus 3. Thereby each power generating unit can be isolated from a fault on e.g. the main DC bus 3, or they can be isolated for maintenance purposes.

20 The first power generating unit P1 is arranged to feed the main DC bus 3, and is connectable to the main DC bus 3 via an isolator switch 7. According to the example in Fig. 1, the first power generating unit P1 is connectable to the first busbar 3-1.

The second power generating unit P2 is arranged to feed the main DC bus 3,  
25 and is connectable to the main DC bus 3 via an isolator switch 7. According to the example in Fig. 1, the second power generating unit P2 is connectable to the first busbar 3-1

The third power generating unit P3 is arranged to feed the main DC bus 3, and is connectable to the main DC bus 3 via an isolator switch 7. According to

the example in Fig. 1, the third power generating unit P3 is connectable to the second busbar 3-2.

The fourth power generating unit P4 is arranged to feed the main DC bus 3, and is connectable to the main DC bus 3 via an isolator switch 7. According to  
5 the example in Fig. 1, the fourth power generating unit P1 is connectable to the second busbar 3-2.

The first power generating unit P1 comprises a generator G1, such as a diesel engine driven generator, arranged to generate alternating current, and a rectifier R1 arranged to convert the alternating current to direct current to be  
10 fed into the main DC bus 3. The rectifier R1 may be provided with fuses dimensioned to blow in case of a fault in the rectifier R1.

The second power generating unit P2, the third power generating unit P3, and the fourth power generating unit P4 may have similar design as the first power generating unit P1. To this end, each of the second power generating  
15 unit P2, the third power generating unit P3, and the fourth power generating unit P4 can comprise a respective generator G2, G3, G4, and a respective rectifier R2, R3, R4 for providing DC signals to the main DC bus 3. It is however to be noted that a combination of different generators types is possible within the same system.

20 Each of the first drive unit D1 and the second drive unit D2 has a drive unit bus system DB comprising a first bus DB1 and a second bus DB2.  
Furthermore, each of the first drive unit D1 and the second drive unit D2 has a number of converter units, in the following exemplified by inverters I1, I2, I3, connected to their respective drive unit bus system DB, and fuses F  
25 arranged between the terminals of the inverters I1, I2, I3, and the drive unit bus system DB. An example of a suitable inverter is ABB's ACS800 inverter.

Each of the first drive unit D1 and the second drive unit D2 further has a first type of input unit 17 which at one end is arranged for connection with the main DC bus 3. At its other end the first type of input unit 17 is connected to  
30 the drive unit bus system DB. The first type of input unit 17 comprises an



isolator switch arranged to disconnect the drive unit D1, D2 from the main DC bus 3, and a current blocking device 11 that is able to block current flow in a direction from the drive unit bus system DB to the main DC bus 3, and to allow current to flow in a direction from the main DC bus 3 to the drive unit bus system DB. Such a current blocking device may be a semiconductor device such as a diode or several diodes, or an insulated gate bipolar transistor (IGBT), thyristor, or similar device.

It is to be noted that depending on the application, drive units can be designed with different number of inverters, from one inverter to a plurality of inverters. Moreover, the first type of drive unit may in one embodiment comprise a semiconductor switching unit connected in anti-parallel with the current blocking device, thereby allowing reverse power feeding during normal operation of the DC-power system. Such a semiconductor switching unit may for instance be an insulated gate bipolar transistor (IGBT).

The energy storage unit E has an energy storage unit bus system EB having a first bus EB1 and a second bus EB2. The energy storage unit E further comprises power provision units such as a battery unit B and a capacitor bank C connected to the energy storage unit bus system EB, a DC-DC converter 15 connected to the energy storage unit bus system EB, and fuses F. The fuses F are arranged between the terminals of the DC-DC converter 15 and the energy storage unit bus system EB, between the capacitor bank C and the energy storage unit bus system EB, and between the battery unit B and the energy storage unit bus system EB.

By means of the DC-DC converter 15 the voltage level output of the battery unit B can be controlled if power is to be provided to the main DC bus 3 from the energy storage unit E.

It is to be noted that the energy storage unit E is an example of a many possible configurations regarding the number of power provision units and converters. For instance, some variations of the energy storage unit E do not

have a capacitor bank. The general purpose of a capacitor bank in the energy storage unit is to assist in blowing fuses in the event of an internal fault.

The energy storage unit E further has a second type of input unit 9 which at one end is arranged for connection with the main DC bus 3. At its other end  
5 the second type of input unit 9 is connected to the energy storage unit bus system EB. The second type of input unit 9 comprises an isolator switch for disconnecting the energy storage unit E from the main DC bus 3, a semiconductor switching unit 13, and a current blocking device 11 that is able to block current flow in the direction from the energy storage unit bus system  
10 EB to the main DC bus 3, and to allow current to flow in a direction from the main DC bus 3 to the energy storage unit bus system EB. Such a current blocking device may be a semiconductor device such as a diode or several diodes, or an IGBT, thyristor, or similar device. The semiconductor switching unit 13 can for instance be an IGBT. The semiconductor switching unit 13 and  
15 the current blocking device 11 can be arranged in anti-parallel, thereby allowing current to flow in the direction from the energy storage unit bus system EB to the main DC bus 3 if the semiconductor switching device 13 is set in its saturated or open state by means of proper control signals. Hence, by means of the current blocking device 11 and the semiconductor switching  
20 unit 13, the current can selectively be allowed to bypass the current blocking device and flow to the main DC bus 3.

Fig. 2 is a schematic diagram of power generating unit P1. The internal components of the rectifier R1 are shown. For each electrical phase, the AC signal generated by the generator G1 is provided to a respective leg of the  
25 rectifier R1. Switching devices T are provided at each leg, which switching devices T can be controlled in such a way that a DC signal can be output by the rectifier R1. In the example in Fig. 2 the switching devices are exemplified by thyristors, although other switch means are also possible e.g. IGBTs. Furthermore, the rectifier R1 comprises fuses F for protection of the rectifier  
30 R1 in case of a fault, i.e. a short circuit, in the rectifier R1. In that case, one or more of the fuses will blow in response to fault currents flowing to the fault and through the fuses F. In the example in Fig. 2, each switching device T is

associated with a fuse F. Thus, each leg, i.e. each phase, is associated with two fuses F. Other possible realisations of the power generating unit P1 include a crow bar design together with a diode on diode on the positive pole of the rectifier DC terminals. The general idea is that if an internal fault occurs, the  
5 rectifier with generator will isolate itself from the DC-power system to minimize the consequences for the wider system.

The fuses F in the rectifier are advantageously dimensioned such that they do not blow when subjected to fault currents as a result of faults downstream of the rectifier. The term downstream is to be understood in relation to a  
10 current flow direction in the DC-power system 1.

Fig. 3a is an example of a situation when a fault 19 has occurred in the DC-power system 1. In the example of Fig. 3a, the fault 19 is a short circuit and has occurred on the main DC bus 3. The fault 19 is hence a global fault. Several different fault-handling strategies are possible in this case.

15 In either case, due to the fault 19, fault currents 20-1, 20-2, 20-3, 20-4 flow to the location of the fault 19, which is on the first busbar 3-1 in this example. Generally, the fault 19 is detected by at least one of a plurality of sensors monitoring the DC-power system 1, e.g. current measuring sensors.

According to one strategy to handle the fault, the bustie breaker 5 is given the  
20 open command as the fault is detected. The healthy side, i.e. the second busbar 3-2 restarts automatically after the partitioning. Thus, once the DC-power system has been split the healthy side resumes operation. The faulty side, i.e. the first busbar 3-1, if aware of fault location, would not restart. If not aware of the location, due to lack of information, the faulty side would  
25 attempt a restart for detecting the fault.

In another version of the strategy, the rectifiers R1, R2, R3, R4 of the power generating units P1-P4 are controlled such that their current output tends towards zero, and any other energy source would also limit the current into the DC-power system whilst giving the open command to the bustie breaker  
30 5. Once the system is split, the healthy side detects that the fault is cleared,

whilst the faulty side will see the fault persist. This will cause the energy sources, e.g. the power generating units, on the faulty side to block current into fault.

In yet another version of the strategy the energy sources can limit their  
5 output voltage and currents to a level that would permit isolator switches to operate within their ratings, wherein the isolator switches 7 can disconnect power generating units from the main DC bus 3.

The first drive unit D1 and the second drive unit D2 do not contribute, or at least contribute minimally, to the fault current because of the current  
10 blocking feature of the current blocking devices 11. Furthermore, due to the isolator switches of the first type of input units 17, the first drive unit D1 and the second drive unit D2 can be disconnected from the main DC-bus 3. Thereby, each of the first drive unit D1 and the second drive unit D2 can be protected in case of a fault on the main DC bus 3.

15 The energy storage unit E is also protected during the fault 19 on the main DC bus 3. If the energy storage unit E was in the midst of providing power to the main DC bus 3 prior to the occurrence of the fault 19, the current output of the DC-DC converter 15 can be controlled, e.g. set to zero. Thereby, the energy storage unit E can be isolated from the main DC bus 3 by means of the  
20 isolator switch of the second type of input unit 9. Moreover, before the energy storage unit E is isolated from the main DC bus 3, the second type of input unit 9 can block current from flowing to the fault 19. This is obtained by means of the current blocking device 11 of the second type of input unit 9 and by setting the semiconductor switching unit 13 in its off-state.

25 By means of the current blocking properties of the first type of input device 17 and the second type of input device 9, the fault currents to the fault 19 can be reduced.

With reference to Fig. 3b, a situation where a fault 22 has occurred in the first drive unit D1 will now be described. This fault is hence a local fault in the first  
30 drive unit D1.

According to the example in Fig. 3b, a short circuit has occurred on the drive unit bus system DB. The first bus DB-1 and the second bus DB-2 may for instance be short circuited. When the fault 22 has occurred, currents 23-1, 23-2, 23-3, 23-4 and 23-5 flow to the fault 22. The currents 23-3, 23-4, 23-5 are provided by capacitor banks in the inverters I1, I2, I3. As the currents 23-3, 23-4, 23-5 provided by the capacitor banks flow through the fuses F arranged in the first drive unit D1, the fuses F will likely blow, thereby disconnecting the inverters I1, I2, I3 from the fault 22. The load connected to the inverters I1, I2, I3 is thereby disconnected from the drive unit bus system DB. As the current from the power generating units P1, P2, P3, P4 is reduced, e.g. by proper control of the rectifiers R1, R2, R3, R4, the isolator switch of the first type of input unit 17 of the first drive unit D1 can disconnect the first drive unit D1 from the main DC bus 3, and hence completely isolate the fault 22. When the fault 22 has been isolated, the remaining parts of the DC-power system 1 can resume normal operation.

Essentially no currents are provided to the fault 22 by capacitor banks of the second drive unit D2 because of the current blocking device 11 in the first type of input unit 17 of the second drive unit D2.

Furthermore, the second type of input unit 9 of the energy storage unit E can block current from flowing to the fault 22. This is obtained by means of the current blocking device 11 of the second type of input unit 9 and by setting the semiconductor switching unit 13 in its off-state.

Hence, by means of the current blocking properties of the first type of input device 17 and the second type of input device 9, the fault currents to the fault 22 can be reduced.

In situations when a fault occurs downstream of an inverter I1, I2, I3, such fault is typically handled by the fuses F of that inverter.

Generally, faults downstream of the fuses within a unit such as a power generating unit, energy storage unit or drive unit, is handled by the fuses of that unit.

The DC-power system described herein may advantageously be used as an on-board power system for powering a vessel, or as a power system in other confined spaces where large DC circuit breakers are undesirable. The present DC-power system is typically used in a low voltage environment, although  
5 higher voltage applications, e.g. medium voltage, are also envisaged.

The inventive concept has mainly been described above with reference to a few examples. However, as is readily appreciated by a person skilled in the art, other embodiments than the ones disclosed above are equally possible within the scope of the inventive concept, as defined by the appended claims.  
10 For instance, a DC-power system according to the present disclosure can include fewer or more power generating units than in the example described in Fig. 1. Moreover, the DC-power system does not have to include an energy storage unit or it can include additional energy storage units, and/or fewer or more drive units.

**CLAIMS**

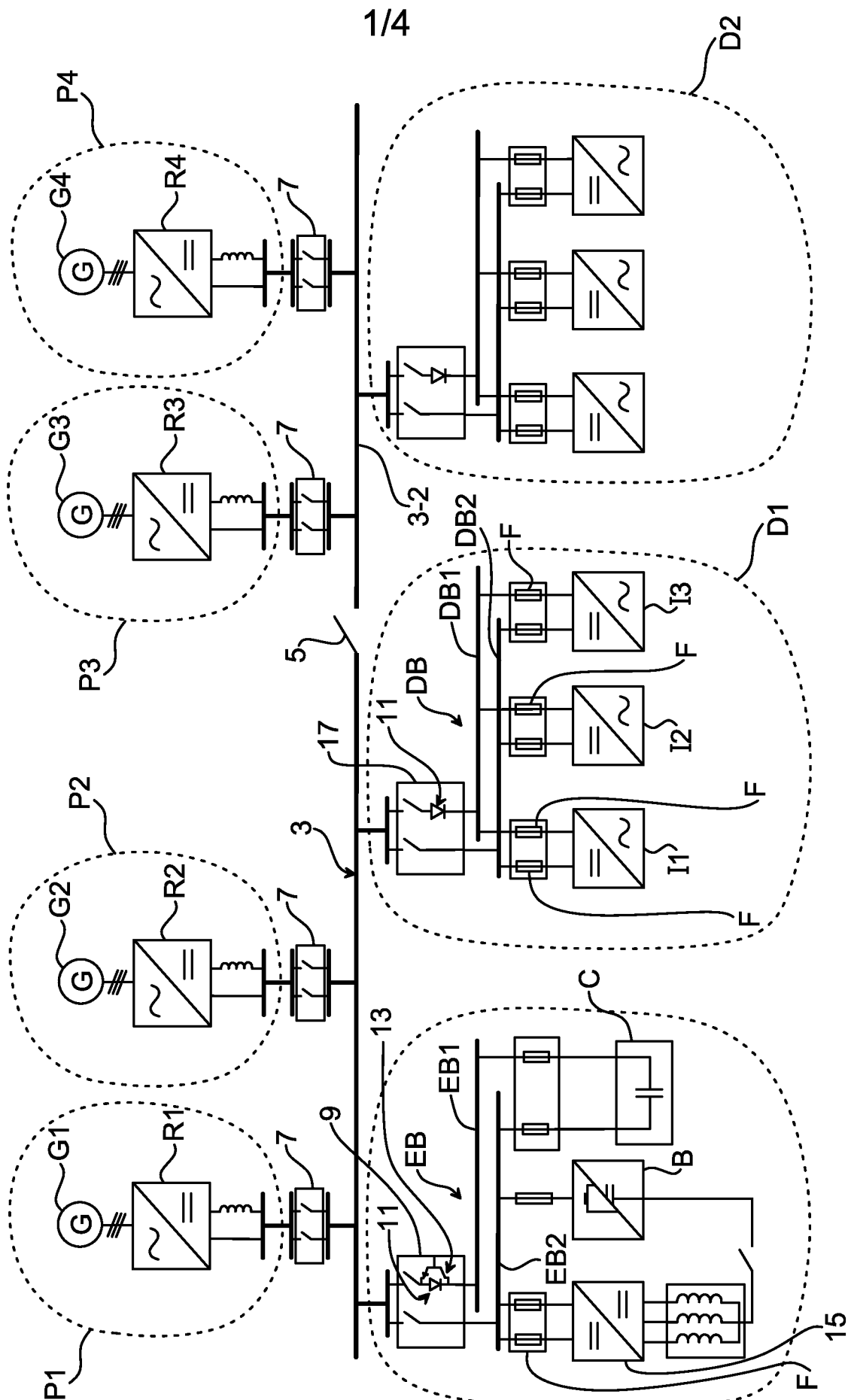
1. A DC-power system (1) comprising:
  - a main DC bus (3),
  - a power generating unit arranged (P1, P2, P3, P4) to feed the main DC bus
  - 5 (3),
  - an isolator switch (7) arranged between the main DC bus (3) and the power generating unit (P1, P2, P3, P4) for isolating the power generating unit (P1, P2, P3, P4) from the main DC bus (3) in case of a main DC bus fault, and
  - a drive unit (D1, D2) arranged to be fed by the main DC bus (3), wherein
  - 10 the drive unit (D1, D2) comprises a drive unit bus system (DB), converter units (I1, I2, I3) connected to the drive unit bus system (DB), and fuses (F) arranged between the drive unit bus system (DB) and the converter units (I1, I2, I3) for protecting the converter units (I1, I2, I3) in case of a drive unit fault.
- 15 2. The DC-power system (1) as claimed in claim 1, wherein the drive unit (D1, D2) comprises a first type of input unit (17) arranged between the main DC bus (3) and the drive unit bus system (DB), and wherein the first type of input unit (17) comprises an isolator switch for disconnecting the drive unit (D1, D2) from the main DC bus (3) in case of a drive unit fault.
- 20 3. The DC-power system (1) as claimed in claim 2, wherein the first type of input unit (17) comprises a current blocking device (11) arranged to block currents in a direction from the drive unit bus system (DB) to the main DC bus (3) and to allow current to flow from the main DC bus (3) to the drive unit (D1, D2).
- 25 4. The DC-power system (1) as claimed in any of the preceding claims, comprising an energy storage unit (E) arranged to feed the main DC bus (3), wherein the energy storage unit (E) comprises an energy storage unit bus system (EB), power provision units (B, C), and fuses (F) arranged between

the energy storage unit bus system (EB) and the power provision units (B, C) for protection of the power provision units (B, C) in case of an energy storage unit fault.

- 5 5. The DC-power system (1) as claimed in claim 4, wherein the energy storage unit (E) comprises a second type of input unit (9) arranged between the energy storage unit bus system (EB) and the main DC bus (3), wherein the second type of input unit (9) comprises an isolator switch for disconnecting the energy storage unit (E) from the main DC bus (3) in case of an energy storage unit fault.
- 10 6. The DC-power system (1) as claimed in claim 5, wherein the second type of input unit (9) comprises a current blocking device (11) arranged to block currents in a direction from the energy storage unit bus system (EB) to the main DC bus (3) and to allow current to flow from the main DC bus (3) to the energy storage unit (E), and a semiconductor switching unit (13) for  
15 selectively allowing current to bypass the current blocking device (11) and flow to the main DC bus (3).
7. The DC-power system (1) as claimed in claim 6, wherein the current blocking device (11) and the semiconductor switching unit (13) are connected in anti-parallel.
- 20 8. The DC-power system (1) as claimed in any of the preceding claims, wherein the power generating unit (P1, P2, P3, P4) comprises a generator (G1, G2, G3, G4) and a rectifier (R1, R2, R3, R4), wherein the rectifier (R1, R2, R3, R4) includes a plurality of fuses (F) arranged to protect the rectifier (R1, R2, R3, R4) in case of a rectifier fault.
- 25 9. The DC-power system (1) as claimed in claim 8, wherein the plurality of fuses (F) included in the rectifier (R1, R2, R3, R4) are dimensioned such that they do not blow when subjected to fault currents as a result of faults downstream of the rectifier (R1, R2, R3, R4).



10. The DC-power system (1) as claimed in any of the preceding claims, wherein each converter unit (I1, I2, I3) has terminals connected to the drive unit bus (DB), wherein each terminal of a converter unit (I1, I2, I3) is connected to a fuse (F).
- 5 11. The DC-power system (1) as claimed in any of claims 3-10, wherein the current blocking device (11) is a diode.
12. The DC-power system (1) as claimed in any of claims 3-11, wherein the first input unit comprises a semiconductor switching unit connected in anti-parallel with the current blocking device for selectively allowing current to
- 10 bypass the current blocking device and flow to the main DC bus.



**Fig. 1**

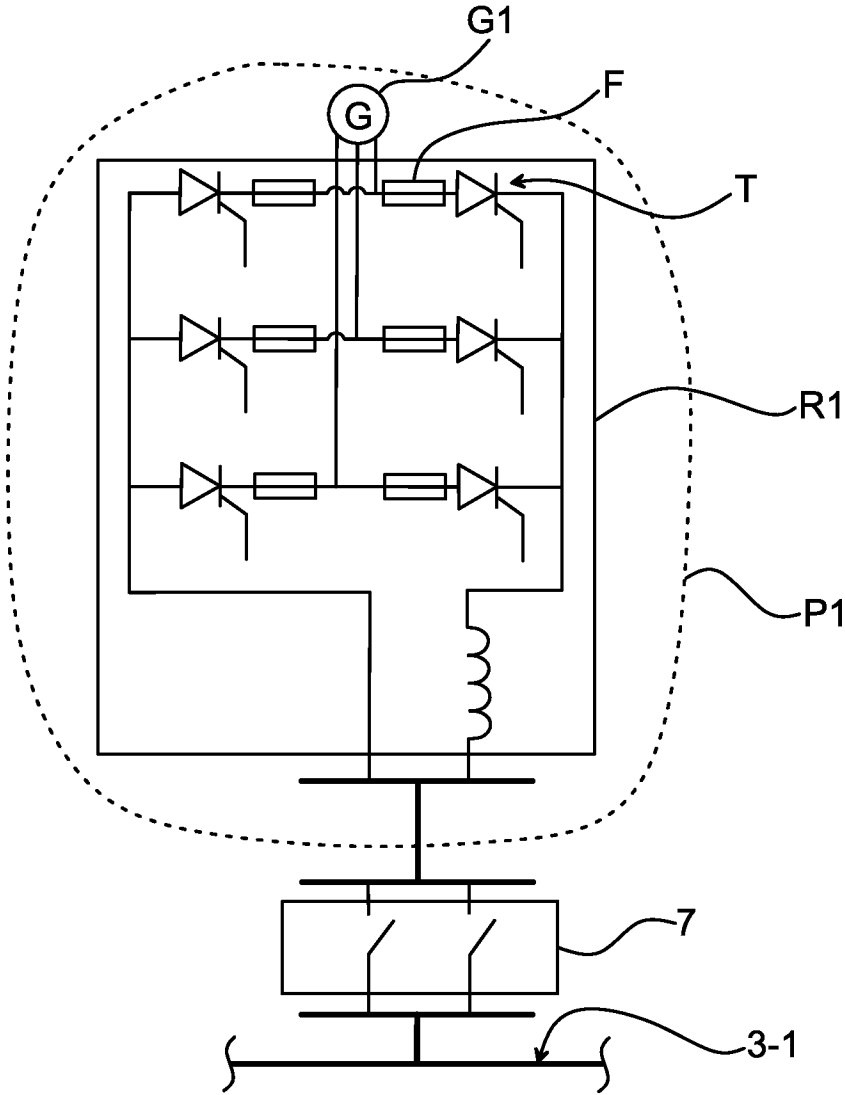


Fig. 2

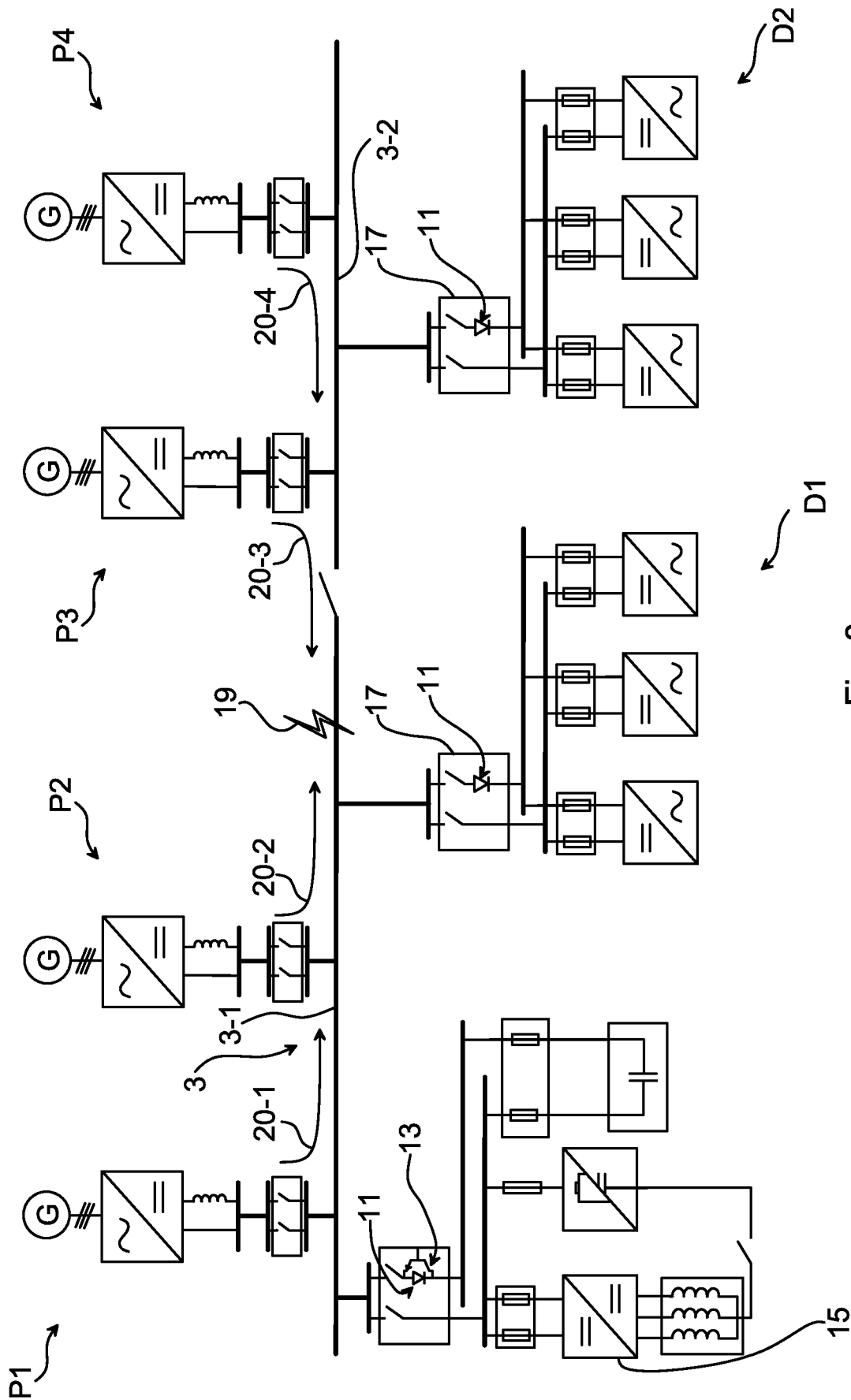


Fig. 3a

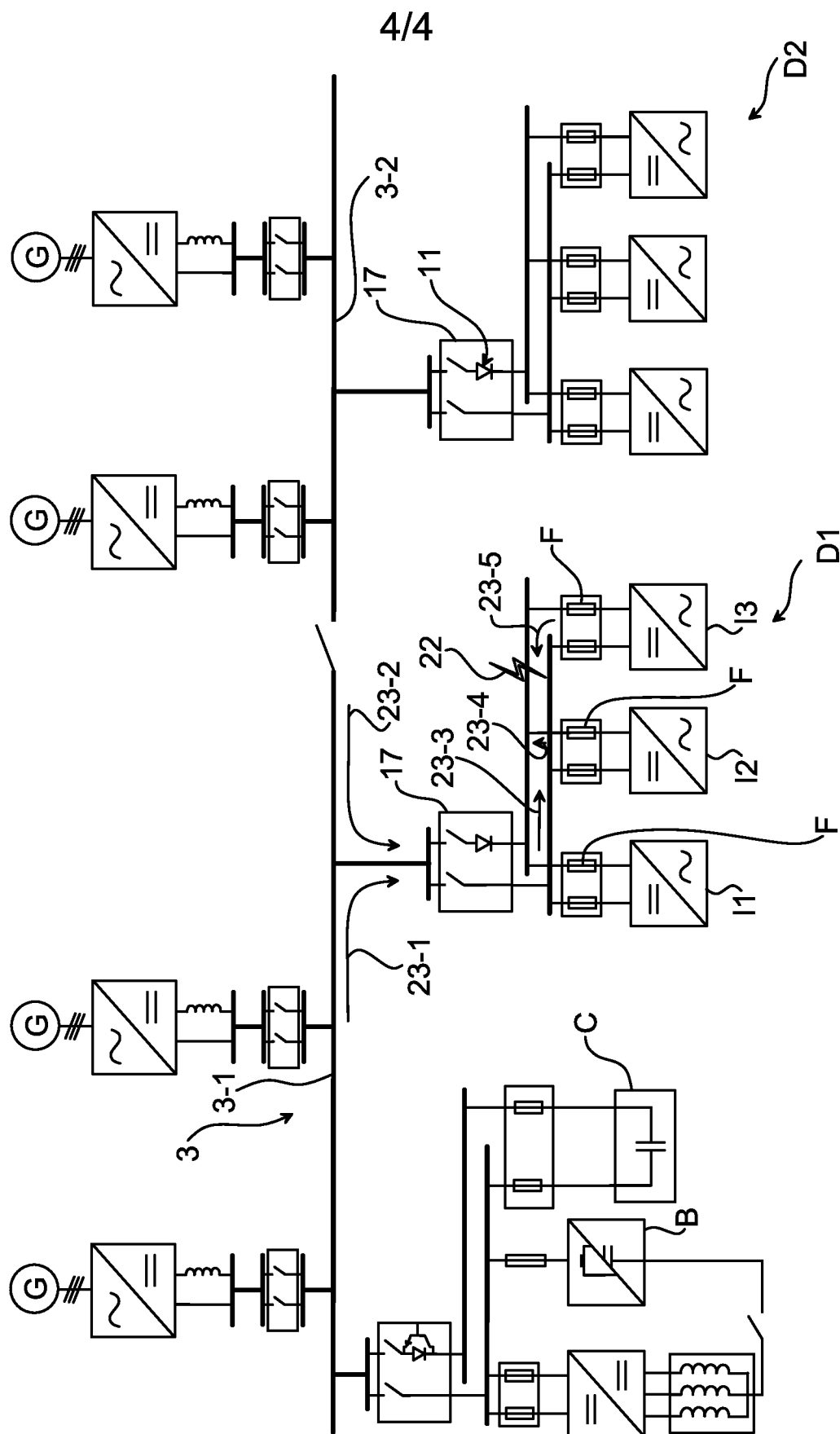


Fig. 3b

# INTERNATIONAL SEARCH REPORT

International application No  
PCT/EP2013/051314

<b>A. CLASSIFICATION OF SUBJECT MATTER</b> INV. H02H7/122      H02H7/06      H02H7/22 ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b> Minimum documentation searched (classification system followed by classification symbols) H02H		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EPO-Internal, WPI Data		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 2003/071633 A1 (FEDIRCHUK DAVID JAMES [CA] ET AL) 17 April 2003 (2003-04-17) paragraph [0074] - paragraph [0075] paragraph [0082] - paragraph [0084]; figure 1	1-12
Y	GB 1 151 457 A (BBC BROWN BOVERI & CIE [CH]) 7 May 1969 (1969-05-07) page 1, line 8 - line 21	1-12
Y	WO 2011/141052 A1 (ABB TECHNOLOGY AG [CH]; HAEFNER JURGEN [SE]; JACOBSON BJOERN [SE]) 17 November 2011 (2011-11-17) page 7, line 10 - line 30; figure 1	3,7,11,12
A	EP 1 843 443 A2 (ROLLS ROYCE PLC [GB]) 10 October 2007 (2007-10-10) figure 1	1
<div style="display: flex; justify-content: space-between; align-items: center;"> <div> <input type="checkbox"/> Further documents are listed in the continuation of Box C.         </div> <div> <input checked="" type="checkbox"/> See patent family annex.         </div> </div>		
<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>* Special categories of cited documents :</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&amp;" document member of the same patent family</p> </div> </div>		
Date of the actual completion of the international search  <div style="text-align: center; font-size: 1.2em;">8 March 2013</div>		Date of mailing of the international search report  <div style="text-align: center; font-size: 1.2em;">20/03/2013</div>
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016		Authorized officer  <div style="text-align: center; font-size: 1.2em;">Harms, Juergen</div>

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Information on patent family members

International application No

PCT/EP2013/051314

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