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(54) **Title:** OXIDATION OF HYDROGEN BROMIDE

(57) **Abstract:** This invention provides a process for forming elemental bromine. The process comprises bringing feeds of a gas comprising hydrogen bromide and a gas comprising molecular oxygen into contact with a catalyst comprising cerium oxide and/or cerium bromide on an inorganic oxide support. The process is characterized in that the catalyst contains cerium in an amount of about 25 wt% to about 75 wt%, expressed as cerium oxide, relative to the total weight of the catalyst, and that the feeds are at a temperature of about 200°C or below during process initiation, with the proviso that when the feeds are at a temperature of about 100°C or below, the feeds are anhydrous during process initiation.

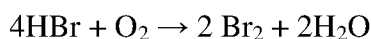
OXIDATION OF HYDROGEN BROMIDE

TECHNICAL FIELD

[0001] This invention relates to oxidation of hydrogen bromide to bromine in the presence of a catalyst.

BACKGROUND

[0002] Many industrial processes employ bromine, and produce gaseous hydrogen bromide as a by-product. One way to recover the bromine values is to oxidize hydrogen bromide to bromine. Several processes for oxidizing hydrogen bromide to bromine with oxygen are known, and many run at relatively high temperatures. The overall reaction for the oxidation can be represented as follows.



[0003] These oxidation processes often involve a catalyst. There are several disclosures of a cerium compound on a support, with a relatively high minimum reaction temperature. See U.S. Pat. Nos. 2,536,457 (700°C); 2,163,877 and 3,346,340 (300°C); 3,346,340 (225°C); and U.S. Pub. No. 2011/015458 (250°C). Various loadings of cerium on a support are taught; see U.S. Pat. Nos. 3,353,916 (0.75 to 25 wt% Ce); 3,273,964 (0.15 to 15 wt% Ce); and 5,366,949 (0.15 to 15 wt% Ce). Routes to recover bromine from hydrogen bromide that are economical and/or practical on large scales are desired.

SUMMARY OF THE INVENTION

[0004] This invention provides processes for oxidation of hydrogen bromide to elemental bromine by contact with a catalyst at relatively low temperatures. Advantageously, conversions greater than 98% have been achieved at these conditions. In addition, ambient temperatures are suitable when the process is conducted under anhydrous conditions.

[0005] An embodiment of this invention is a process for forming elemental bromine. The process comprises bringing feeds of a gas comprising hydrogen bromide and oxygen into contact with a catalyst comprising cerium oxide and cerium bromide on an inorganic oxide support, characterized in that the catalyst comprises cerium in an amount of about 25 wt% to about 75 wt%, expressed as cerium relative to the total weight of the catalyst, and that the feeds are at a temperature of

200°C or below during process initiation, with the proviso that when the feeds a temperature of about 100°C or below, the feeds are anhydrous during process initiation.

[0006] These and other embodiments and features of this invention will be still apparent from the ensuing description and appended claims.

FURTHER DETAILED DESCRIPTION OF THE INVENTION

[0007] As used throughout this document, the chemical formula "HBr" stands for hydrogen bromide; the term "bromine" refers to elemental bromine, Br₂, unless otherwise specified; and the term "molecular oxygen" refers to O₂.

[0008] Throughout this document, the phrase "HBr gas" is used interchangeably with "gas comprising hydrogen bromide", and the phrase "oxygen gas" is used interchangeably with "gas comprising molecular oxygen".

[0009] The term "process initiation", and the words "initiating" and "initiation" refer to the processes of this invention, as used throughout this document, referring to a period of time from the beginning of the feeds of the gas comprising hydrogen bromide and the gas comprising molecular oxygen into the reaction zone until an exotherm is observed in the reaction zone. The exotherm is a significant increase in temperature, typically an increase of about 50°C or more.

[0010] In the processes of this invention, hydrogen bromide is oxidized by molecular oxygen, O₂, to elemental bromine in the presence of a catalyst; water is a by-product of the reaction. The components of the process other than the catalyst are normally present preferably in the gas phase at least in the reaction zone.

[0011] Hydrogen bromide from various sources can be subjected to the processes of this invention, and the HBr gas does not need to be pure. Preferably, the HBr gas contains about 20 mol% or more HBr, more preferably about 50 mol% or more HBr. In some embodiments, preferably, the HBr gas contains about 20 mol% to about 100 mol%, more preferably about 50 mol% to about 100 mol% HBr. In some embodiments, it is preferable to include other substances from their admixture with HBr when they are present in large amounts. As long as the impurities present in the HBr gas do not adversely affect the catalytic activity (e.g., hydrocarbons), the HBr gas can be subjected to the processes of this invention. Some impurities, such as sulfur-containing compounds, if present in the HBr gas, may affect the catalyst, and should be minimized in, or absent from, the HBr gas. Although the HBr gas does not need to be anhydrous, in some embodiments, anhydrous HBr gas is preferred.

[0012] The oxidant is molecular oxygen. The molecular oxygen can be in a carrier gas or in a mixture of carrier gases. Suitable carrier gases include helium, argon, nitrogen, carbon dioxide, and mixtures thereof; air is an example of a mixture of carrier gases containing molecular oxygen. Molecular oxygen without a carrier is preferred.

[0013] Suitable catalysts in the practice of this invention include cerium oxide, cerium bromide, and mixtures thereof, on an inorganic oxide support; cerium oxide is preferred. Inorganic oxide supports include zirconia, hafnia, alumina, titania, yttria, silica, thorium oxide, and the like, and mixtures thereof. Preferred supports comprise zirconia; more preferably, zirconia is the only support material. The amount of cerium oxide and/or cerium bromide on the support is preferably about 25 to about 75 wt% as cerium oxide relative to the total weight of the catalyst, preferably about 30 wt% to about 70 wt% as cerium oxide, and especially about 40 to about 70 wt% cerium oxide, and especially with about 60 to about 70 wt% as cerium oxide, relative to the total weight of the catalyst. In some preferred embodiments, the catalyst is cerium oxide on zirconia, with about 25 to about 75 wt% cerium oxide, preferably about 30 to about 70 wt%, more preferably about 40 to about 70 wt% cerium oxide, and especially about 60 to 70 wt% cerium oxide relative to the total weight of the catalyst.

[0014] As used throughout this document, the phrase "as cerium oxide" refers to the amount of cerium on the support, where the numerical value is for cerium oxide. For example, cerium bromide may be used, but the amount of cerium in the catalyst is as the value for cerium oxide.

[0015] The reaction zone is defined as the area where the HBr gas and the oxygen gas come into contact with the catalyst. Both HBr and Br₂ are known to corrode steel in the presence of water, so it is recommended and preferred that the reaction zone is composed of other materials, such as quartz or ceramic; glass-lined reactors may also be used.

[0016] The HBr gas and the oxygen gas can be fed in any desired manner. The HBr gas and the oxygen gas can be combined at a time before being fed into the reaction zone, or the mixture is kept at a relatively low temperature (*e.g.*, about 100°C or lower). Preferably, the HBr gas and the oxygen gas are fed to the reaction zone separately. Another preferred feeding method, the HBr gas and the oxygen gas are mixed immediately prior to being fed into the reaction zone.

[0017] It is recommended and preferred to feed the HBr gas and the oxygen proportions such that at least the stoichiometric amount of molecular oxygen is present in the reaction zone. When the amount of oxygen gas supplied is less than the stoichiometric amount of molecular oxygen, a decreased conversion of HBr to elemental bromine is observed. Preferably, the oxygen gas is fed in an amount such that an excess of about 2 mol% to about 20 mol%, more preferably about 2 mol% to about 10 mol%, still more preferably about 5 mol% to about 10 mol%, of molecular oxygen over the stoichiometric amount is present in the reaction zone.

[0018] Feed temperatures refer to both the HBr gas and the oxygen gas. When fed separately, the HBr gas and the oxygen gas are in the desired feed temperature range. The HBr gas and the oxygen gas may be at different temperatures, and are preferably at the same or similar temperatures (*e.g.*, preferably a difference of about 25°C or less, still more preferably a difference of about 10°C or less). When the HBr gas and the oxygen gas are fed as a mixture, it is understood that the feed temperature is for the mixture, which is in the desired feed temperature range.

[0019] At least during process initiation, one or both of the HBr gas and the oxygen gas are preferably at one or more temperatures of about 200°C or below during their feed into the reaction zone, with the proviso that the gas comprising hydrogen bromide and the gas comprising molecular oxygen are anhydrous when the feed temperature is about 100°C or below. In some embodiments, the processes of this invention are initiated with feeds of HBr gas and the oxygen gas at feed temperatures in the range of about 100°C to about 200°C, preferably about 100°C to about 175°C, more preferably at about 100°C to about 150°C, still more preferably at about 100°C to about 125°C, at atmospheric pressure. Anhydrous conditions are not necessary when feeding the HBr gas and the oxygen gas at about 200°C or above.

[0020] When operating with the HBr gas and the oxygen gas feeds under anhydrous conditions, the process can be initiated or conducted with the HBr gas and the oxygen gas feeds at temperatures of about 100°C or below, and the HBr gas and the oxygen gas feeds can be at temperatures as low as ambient temperatures (*e.g.*, about 18°C). Preferred feed temperatures when the process is initiated with the HBr gas and the oxygen gas under anhydrous conditions are in the range of about 18°C to about 150°C, preferably about 50°C to about 110°C, and still more preferably about 50°C to about 100°C.

[0021] Anhydrous conditions mean the absence of water, but it is understood that adventitious amounts of water may be present. In some preferred embodiments, processes of this invention are initiated under anhydrous conditions. Initiating a process under anhydrous conditions generally means that the HBr gas and the oxygen gas are introduced into the reaction zone under anhydrous conditions during process initiation.

[0022] While the feed temperatures for the HBr gas and the oxygen gas refer to the period of time before an exotherm occurs in the reaction zone, the HBr gas and the oxygen gas can be fed at their feed temperatures after the exotherm occurs, if desired.

[0023] The reaction zone or at least a portion thereof can be preheated, although not necessary, because of the exothermicity of the reaction that occurs during the process. Preheating is preferred when operating on smaller scales, *e.g.*, laboratory scales. In initiating the feeds of the HBr gas and the oxygen gas, it is recommended and preferred to flush an inert gas (*e.g.*, helium, neon, argon, nitrogen, carbon dioxide, or mixtures of two or more of these, preferably nitrogen) through the reaction zone during the preheating period.

[0024] Typically, the preheating is for a period of time at a temperature of about 100°C or more, preferably about 125°C to about 250°C, more preferably about 125°C to about 200°C, to remove water from the reaction zone before starting the feeds of HBr gas and the oxygen gas into the reaction zone.

[0025] Heating of the reaction zone is generally not required during the processes of this invention because the oxidation reaction that occurs in these processes is very exothermic. The magnitude of the exotherm is large enough that heat transfer from the reaction zone is normally needed to keep the reaction zone at the desired temperature, even when the feeds of HBr gas and the oxygen gas are at ambient temperature.

[0026] All of the components in the reaction zone other than the catalyst are normally and preferably in the vapor phase. This means that the reactants, HBr and O₂, as well as the products, Br₂ and water, are in the vapor phase while in the reaction zone. At a minimum, water should be in the vapor phase to prevent condensation of water on the catalyst. Normally, the heat of reaction is sufficient or more than enough to maintain the temperature in the reaction zone high enough that all or nearly all of the non-catalyst components remain in the vapor phase.

[0027] Residence times in the reaction zone may be quite short (on the order of seconds) because the oxidation reaction that occurs during the process appears to be instantaneous or nearly instantaneous.

[0028] In some more preferred embodiments of this invention, the inorganic support is zirconia, the cerium is about 30 wt% to about 70 wt%, preferably about 40 to about 70 wt%, more preferably about 60 wt% to about 70 wt%, expressed as oxide, relative to the total weight of the catalyst, and the feeds are at a temperature range of about 100°C to about 175°C during process initiation.

[0029] In other more preferred embodiments of this invention, the inorganic support is zirconia, the cerium is about 30 wt% to about 70 wt%, preferably about 40 to about 70 wt%, more preferably about 60 wt% to about 70 wt%, expressed as oxide, relative to the total weight of the catalyst, and the feeds are at a temperature about 100°C or below during process initiation.

[0030] As mentioned above, the processes of this invention produce elemental bromine and water. The water can be separated from bromine by any convenient means. A preferred method is distillation. Another method is to condense the product into a flask to allow it to separate into layers, and draw off the layers separately; the water layer contains some residual elemental bromine, which can be recovered if desired.

[0031] Elemental bromine produced in the processes of this invention can be recycled to the process from which the HBr emanated, if applicable. Alternatively, the elemental bromine can be used in a different process, or stored for later use.

[0032] The following examples are presented for purposes of illustration, and are not intended to impose limitations on the scope of this invention.

EXAMPLE 1

[0033] Two gas feed lines were connected to separate arms of a mixing "Y", which was then connected to a quartz tube reactor. Connected to and downstream from the reactor are two jacketed 1-L flasks that are cooled to 5°C, then a condensing column, followed by a caustic trap (NaOH, aq., 40%).

[0034] Cerium oxide on zirconia (20 g; 69.5 wt% cerium oxide; Actalys[®]; Rhodia) was placed in the quartz tube reactor. The HBr was supplied from a gas cylinder and molecular oxygen was supplied from a gas cylinder.

[0035] The quartz tube reactor was preheated at 150°C for 60 minutes with a stream of nitrogen flushing the quartz tube. Several runs of the reaction were carried out with the HBr and oxygen feeds at the same selected temperature (100°C, 150°C, or 200°C). HBr was fed into one gas feed line at a rate of 150 sccm (150 cm³/min.), and oxygen

fed into the other gas feed line at a rate of 50 sccm, and the mixture of HBr and oxygen was fed from the mixing "Y" into the quartz tube reactor. The HBr and oxygen were fed for 300 minutes. A visible red vapor was seen after only a few seconds of operation. During the reaction, an exotherm of approximately 50°C, measured at the outer wall of the reactor, was observed. Br₂ and water were collected in the two 1-L flasks, the condensation column, and the caustic trap. The amount of unreacted HBr was determined on samples from the caustic trap by acid-base titration. Results are summarized in Table 1.

TABLE 1

Run	Feed temp.	HBr conversion
1	200°C	98.8%
2	150°C	98.4%
3	150°C	97.2%
4	100°C	99.0%

EXAMPLE 2

[0036] Example 1 was repeated, using air instead of pure oxygen; the air was fed at a rate of 200 sccm. In this Example, the amount of bromine carried over to the caustic trap (~20% of the bromine produced) was greater than in Example 1 (3% of the bromine produced). Results are summarized in Table 2.

TABLE 2

Run	Feed temp.	HBr conversion
A	200°C	97.2%
B	175°C	93.7%

EXAMPLE 3

[0037] Another run was performed as described in Example 1, except that the was cooled to room temperature under a stream of nitrogen, and the reaction was run the HBr and oxygen feeds at room temperature (21°C). In this 30-second run, a red Br₂, was observed exiting the reactor. The HBr conversion was not determined.

[0038] These Examples show that the processes of this invention yield a high conversion of HBr to bromine and water, which are easily separated.

[0039] Components referred to by chemical name or formula anywhere in the specification or claims hereof, whether referred to in the singular or plural, are identified as they exist prior to coming into contact with another substance referred to by chemical name or chemical type (*e.g.*, another component, a solvent, or *etc.*). It matters not what chemical changes, transformations and/or reactions, if any, take place in the reaction mixture or solution as such changes, transformations, and/or reactions are the result of bringing the specified components together under the conditions called for pursuant to this disclosure. Thus the components are identified as ingredients brought together in connection with performing a desired operation or in forming a desired composition. Also, even though the claims hereinafter may refer to substances, components and/or ingredients in the present tense ("comprises", "is", *etc.*), the reference is to the substance, component or ingredient as it existed at the time just before it was contacted, blended or mixed with one or more other substances, components and/or ingredients in accordance with the present disclosure. The fact that a substance, component or ingredient may have lost its original identity through a chemical reaction or transformation during the course of contacting, blending or mixing operations conducted in accordance with this disclosure and with ordinary skill of a chemist, is of no practical concern.

[0040] The invention may comprise, consist, or consist essentially of the materials and/or procedures recited herein.

[0041] As used herein, the term "about" modifying the quantity of an ingredient in a composition of the invention or employed in the methods of the invention refers to a variation in the numerical quantity that can occur, for example, through typical measurement and liquid handling procedures used for making concentrates or use solutions in the real world; through inadvertent error in these procedures; through differences in manufacture, source, or purity of the ingredients employed to make the composition.

carry out the methods; and the like. The term about also encompasses amounts that are due to different equilibrium conditions for a composition resulting from a particular mixture. Whether or not modified by the term "about", the claims include equivalent quantities.

[0042] Except as may be expressly otherwise indicated, the article "a" or "an" if used herein is not intended to limit, and should not be construed as limiting a description or a claim to a single element to which the article refers. Rather, the article "a" or "an" if and as used herein is intended to cover one or more such elements, unless the text expressly indicates otherwise.

[0043] This invention is susceptible to considerable variation in its practice. The foregoing description is not intended to limit, and should not be construed as limiting the invention to the particular exemplifications presented hereinabove.

CLAIMS:

1. A process for forming elemental bromine, which process comprises bringing feeds of

(i) a gas comprising hydrogen bromide and

(ii) a gas comprising molecular oxygen

into contact with a catalyst comprising cerium oxide and/or cerium bromide on an inorganic oxide support, characterized in that the catalyst contains cerium in an amount of about 25 wt% to about 75 wt%, expressed as cerium oxide, relative to the total weight of the catalyst, and that the feeds are at a temperature of about 200°C or below at process initiation, with the proviso that when the feeds are at a temperature of about 200°C or below, the feeds are anhydrous during process initiation.

2. A process as in Claim 1 wherein the gas comprising hydrogen bromide contains about 20 mol% or more hydrogen bromide.

3. A process as in Claim 1 or 2 wherein the gas comprising molecular oxygen is pure oxygen.

4. A process as in Claim 1 or 2 wherein the gas comprising molecular oxygen is air.

5. A process as in any of Claims 1-4 wherein the inorganic oxide support is selected from the group consisting of zirconia, hafnia, alumina, titania, yttria, silica, and mixtures of any two or more thereof.

6. A process as in Claim 1 or 5 wherein the inorganic oxide support is zirconia.

7. A process as in any of Claims 1-6 wherein the cerium is about 30 wt% to about 70 wt%, expressed as cerium oxide, relative to the total weight of the catalyst.

8. A process as in any of Claims 1-7 wherein the molecular oxygen is in an excess of about 1 mol% to about 20 mol% relative to the hydrogen bromide.

9. A process as in any of Claims 1-8 wherein the feeds are at a temperature in the range of about 100°C to about 175°C during process initiation.

10. A process as in any of Claims 1-8 wherein the feeds are at a temperature of about 100°C or below during process initiation.

11. A process as in any of Claim 1-8 wherein the feeds are at a temperature in the range of about 18°C to about 150°C during process initiation.

12. A process as in any of Claim 1-8 wherein the feeds are at a temperature in the range of about 50°C to about 110°C during process initiation.

13. A process as in any of Claims 1-12 wherein the gas comprising hydrogen bromide is fed separately from the gas comprising molecular oxygen.

14. A process as in any of Claims 1-13 wherein the gas comprising hydrogen bromide and the gas comprising molecular oxygen are anhydrous.

15. A process as in Claim 1 wherein the inorganic oxide support is zirconia wherein the cerium is about 30 wt% to about 70 wt%, expressed as cerium oxide, relative to the total weight of the catalyst, and wherein the feeds are at a temperature in the range of about 100°C to about 175°C during process initiation.

16. A process as in Claim 1 wherein the inorganic oxide support is zirconia wherein the cerium is about 30 wt% to about 70 wt%, expressed as cerium oxide, relative to the total weight of the catalyst, and wherein the feeds are at a temperature of 100°C or below during process initiation.

17. A process as in Claim 15 or 16 wherein the cerium is about 40 wt% to about 70 wt%, expressed as cerium oxide, relative to the total weight of the catalyst.

18. A process as in Claim 15 or 16 wherein the cerium is about 60 wt% to about 70 wt%, expressed as cerium oxide, relative to the total weight of the catalyst.

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2016/012579

A. CLASSIFICATION OF SUBJECT MATTER
INV. C01B7/09
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
C01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 3 310 380 A (LESTER GEORGE R) 21 March 1967 (1967-03-21) claims 1,6; figure 1; examples I, IV -----	1-18
X	US 3 353 916 A (LESTER GEORGE R) 21 November 1967 (1967-11-21) claims 1,3 -----	1,4-7,9, 14-17
X	US 3 346 340 A (LOUVAR CECELIA J ET AL) 10 October 1967 (1967-10-10) examples I,III,IV,VI,IX -----	1-18
A	US 5 366 949 A (SCHUBERT PAUL F [US]) 22 November 1994 (1994-11-22) the whole document -----	1-18

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents :

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 3310380	A	21-03-1967	NONE

US 3353916	A	21-11-1967	NONE

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