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(71) Applicant(s)
Pulmatrix, Inc.

(72) Inventor(s)
Brande, Matthew Frederick;Clarke, Robert William;Edwards, David A.;Dehaan, Wesley Hugh;Man, Jonathan Chun-Wah;Gabrielson, Mark J.

(74) Agent / Attorney
Davies Collison Cave, Level 14 255 Elizabeth Street, Sydney, NSW, 2000

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(71) Applicant (for all designated States except US): PULMATRIX, INC. [US/US]; 12 Emily Street, Cambridge, Massachusetts 02139 (US).

(72) Inventors; and

(75) Inventors/Applicants (for US only): EDWARDS, David, A. [US/US]; 171 Commonwealth Avenue, Boston, Massachusetts 02116 (US). GABRIELSON, Mark, J. [US/US];

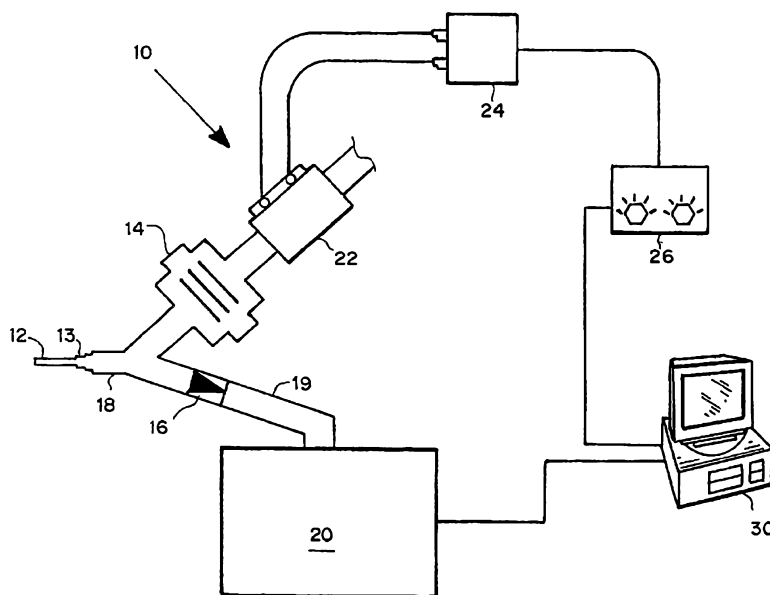
165 Lounsbury Road, Ridgefield, Connecticut 06877 (US). CLARKE, Robert, William [US/US]; 60 Kings Road, Canton, Massachusetts 02021 (US). DEHAAN, Wesley, Hugh [CA/US]; 20 Jackson Road, Belmont, Massachusetts 02478 (US). BRANDE, Matthew, Frederick [US/US]; 317 Perkins Street, Bristol, Connecticut 06010 (US). MAN, Jonathan, Chun-Wah [US/US]; 10 Rollins Court, Cambridge, Massachusetts 02139 (US).

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(54) Title: METHOD AND DEVICE FOR DECREASING CONTAMINATION



(57) Abstract: Methods and devices to determine rate of particle production and the size range for the particles produced for an individual are described herein. The device (10) contains a mouthpiece (12), a filter (14), a low resistance one-way valve (16), a particle counter (20) and a computer (30). Optionally, the device also contains a gas flow meter (22). The data obtained using the device can be used to determine if a formulation for reducing particle exhalation should be administered to an individual. This device is particularly useful prior to and/or following entry in a cleanroom to ensure that the cleanroom standards are maintained.

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METHOD AND DEVICE FOR DECREASING CONTAMINATION

Cross-Reference to Related Applications

This application claims priority to U.S.S.N. 60/642,643, filed 10
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Field of the Invention

The present invention is in the field of methods, formulations and
devices to decrease particle exhalation and contamination in various
environments, and is particularly useful in cleanrooms.

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Background of the Invention

A cleanroom is a controlled environment where products are
manufactured. It is a room in which the concentration of airborne particles is
controlled to specified limits. Eliminating sub-micron airborne
contamination is really a process of control. These contaminants are
15 generated by people, process, facilities and equipment. They must be
continually removed from the air. The level to which these particles need to
be removed depends upon the standards required. The most frequently used
standard is the Federal Standard 209E. The 209E is a document that
establishes standard classes of air cleanliness for airborne particulate levels
20 in cleanrooms and clean zones. Strict rules and procedures are followed to
prevent contamination of the product.

The following table shows the latest cleanroom classifications. Note
that ISO Class 2 is equivalent to 209 Class 10.

Table 1: Airborne Particulate Cleanliness Classes

Classification numbers (N)	Maximum concentration limits (particles/m ³ of air) for particles equal to and larger than the sizes listed below									
	0.1micron	0.2micron	0.3micron	0.5micron	1micron	5micron				
ISO 1	10	2								
ISO 2	100	24	10	4						
ISO 3	1,000	237	102	35	8					
ISO 4	10,000	2,370	1,020	352	83					
ISO 5	100,000	23,700	10,200	3,520	832	29				
ISO 6	1,000,000	237,000	102,000	35,200	8,320	293				
ISO 7				352,000	83,200	2,930				
ISO 8				3,520,000	832,000	29,300				
ISO 9				35,200,000	8,320,000	293,000				

The only way to control contamination is to control the total environment. Air flow rates and direction, pressurization, temperature, humidity and specialized filtration all need to be tightly controlled. The sources of these particles also need to be controlled or eliminated whenever possible. Cleanrooms are planned and manufactured using strict protocol and methods. They are frequently found in electronics, pharmaceutical, biopharmaceutical, medical device industries and other critical manufacturing environments.

It only takes a quick monitor of the air in a cleanroom compared to a typical office building to see the difference. Typical office building air contains from 500,000 to 1,000,000 particles (0.5 microns or larger) per cubic foot of air. A Class 100 cleanroom is designed to never allow more than 100 particles (0.5 microns or larger) per cubic foot of air. Class 1000 and Class 10,000 cleanrooms are designed to limit particles to 1000 and 10,000 respectively.

A human hair is about 75-100 microns in diameter. A particle 200 times smaller (0.5 micron) than the human hair can cause major disaster in a cleanroom. Contamination can lead to expensive downtime and increased production costs. Once a cleanroom is built, it must be maintained and cleaned to the same high standards.

Contamination is a process or act that causes materials or surfaces to be soiled with contaminating substances. There are two broad categories of surface contaminants: film type and particulates. These contaminants can produce a "killer defect" in a miniature circuit. Film contaminants of only 10 nm (nanometers) can drastically reduce coating adhesion on a wafer or chip. It is widely accepted that particles of 0.5 microns or larger are the target. However, some industries are now targeting smaller particles.

A partial list of contaminants is provided below. Any of these can be the source for killing a circuit. Preventing these contaminants from entering the cleanroom environment is a major objective. It has been found that many of these contaminants are generated from five basic sources: facilities, people, tools, fluids and the product being manufactured.

1. **Facilities:** Walls, floors and ceilings; Paint and coatings; Construction material (sheet rock, saw dust etc.); Air conditioning debris; Room air and vapors; Spills and leaks
 2. **People:** Skin flakes and oil; Cosmetics and perfume; Spit; 5 Clothing debris (lint, fibers etc.); Hair
 3. **Tool Generated:** Friction and wear particles; Lubricants and emissions; Vibrations; Brooms, mops and dusters
 4. **Fluids:** Particulates floating in air; Bacteria, organics and moisture; Floor finishes or coatings; Cleaning chemicals; Plasticizers 10 (outgasses); Deionized water
 5. **Product generated:** Silicon chips; Quartz flakes; Cleanroom debris; Aluminum particles
- Current methods and devices used to decrease contamination include HEPA (High Efficiency Particulate Air) filters. These filters are extremely 15 important for maintaining contamination control. They filter particles as small as 0.3 microns with a 99.97% minimum particle-collective efficiency. Cleanrooms are designed to achieve and maintain an airflow in which essentially the entire body of air within a confined area moves with uniform velocity along parallel flow lines. This air flow is called laminar flow. The 20 more restriction of air flow the more turbulence. Turbulence can cause particle movement. In addition to the HEPA filters commonly used in cleanrooms, there are a number of other filtration mechanisms used to remove particles from gases and liquids. These filters are essential for providing effective contamination control. Cleaning is also an essential 25 element of contamination control. The requirements for cleanroom garments will vary from location to location. Gloves, face masks and head covers are standard in nearly every cleanroom environment. Smocks are being used more and more. Jump suits are required in very clean environments. Care must be taken when selecting and using commodity items in cleanrooms. 30 Wipers, cleanroom paper and pencils and other supplies that service the cleanroom should be carefully screened and selected. Review of the local cleanroom requirements for approving and taking these items into the

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cleanroom is essential. In fact, many cleanroom managers will have approval lists of these types of items.

There are both physical and psychological concerns when humans are present in cleanrooms. Physical behavior like fast motion and horseplay can increase contamination. Psychological concerns like room temperature, humidity, claustrophobia, odors and workplace attitude are important. Ways people produce contamination include body regenerative processes resulting in skin flakes, oils, perspiration and hair; behavior including the rate of movement, sneezing and coughing; attitude in the work habits and communication between workers. People are a major source of contamination in the cleanroom, as demonstrated below in table 2. Table 2 lists a person's typical activities and the corresponding rate or particle production (number of particles produced per minute). The particles are 0.3 microns and larger.

Table 2: Typical activities and rate of particle production

People Activity	Rate of Particle (0.3 microns and larger) Production (particles/minute)
Motionless (Standing or Seated)	100,000
Walking about 2 mph	5,000,000
Walking about 3.5 mph	7,000,000
Walking about 5 mph	10,000,000
Horseplay	100,000,000

15 The present invention seeks to provide a device and methods for use in decreasing contamination in environments such as cleanrooms.

The present invention also seeks to provide a method for decreasing or limiting the airborne transmission of viruses and bacteria in environments such as cleanrooms.

The present invention also seeks to facilitate the manufacture of a device for the measurement of exhaled particle number and particle size to determine if a formulation for decreasing particle exhalation is needed.

Summary of the Invention

5 Methods and devices to determine rate of particle production and the size range for the particles produced for an individual are described herein. The device (10) contains a mouthpiece (12), a filter (14), a low resistance one-way valve (16), a particle counter (20) and a computer (30). Optionally, the device also contains a gas flow meter (22). The data
10 obtained using the device can be used to determine if a formulation for reducing particle exhalation is needed. This device is particularly useful prior to and/or following entry in a cleanroom to ensure that the cleanroom standards are maintained. The device can also be used to identify animals and humans who have an enhanced propensity to exhale aerosols (referred to herein as "over producers", "super-producers", or "superspreaders").

 Formulations to reduce particle production are also described herein. The
15 formulation is administered in an amount sufficient to alter biophysical properties in the mucosal linings of the body. When applied to mucosal lining fluids, the formulation alters the physical properties such as the gel characteristics at the air/liquid interface, surface elasticity, surface viscosity, surface tension and bulk viscoelasticity of the mucosal lining. The formulation is administered in an effective amount to minimize ambient contamination
20 due to particle formation during breathing, coughing, sneezing, or talking, which is particularly important in the cleanroom applications. In one embodiment, the formulation for administration is a non-surfactant solution. In one embodiment, the formulations are conductive formulations containing conductive agents, such as salts, ionic surfactants, or other substances that are in an ionized state or easily ionized in an aqueous or organic
25 solvent environment. One or more active agents, such as antivirals, antimicrobials, antiinflammatories, proteins or peptides, may be included with the formulation.

Brief Description of the Drawings

Figure 1 is a schematic of a diagnostic instrument for the measurement of particles produced and exhaled by a person.

Figure 2 is a schematic of a diagnostic instrument for the measurement of particles produced and exhaled by a person with associated breathing rate.

Figures 3A, 3B and 3C illustrate particle concentration following three coughs measured over time for plain mucus simulant and following saline delivery at $t=0$ (Figure 3A), $t=30$ (Figure 3B) and $t=60$ minutes (Figure 3C).

Figure 4A is a chart of baseline particle count (greater than 150nm) expired by individuals ($n=11$) while inhaling particle free air; and Figure 4B is a graph of particle count (greater than 150nm) expired by individuals ($n=11$) after saline (approximately 1g) had been administered to the lungs in the form of an aerosol over time (minutes).

Figure 5A is a graph of particle count (greater than 150 nm) exhaled by individuals ($n=2$) who, prior to treatment have a baseline exhalation of greater than 1000 particles/liter (while inhaling particle free air), after isotonic saline solution (approximately 1g solution) had been administered to the lungs in the form of an aerosol over time (minutes); and Figure 5B is a graph of particle count (greater than 150 nm) exhaled by individuals ($n=2$) who, prior to treatment have a baseline exhalation of greater than 1000 particles/liter (while inhaling particle free air), after isotonic saline solution containing phospholipids (approximately 1g solution) had been administered to the lungs in the form of an aerosol over time (minutes).

Figure 6A is a graph of total particles exhaled (greater than 0.3 microns) over time (minutes) showing data obtained from sham treated animals. Figure 6B is a graph of mean percent (%) baseline particle counts over time (minutes) showing data obtained from animals treated with nebulized saline for 1.8 minutes (-■-), 6.0 minutes (-▲-), 12.0 minutes (-□-), and sham (-◆-).

Figure 7 is a graph of time following completion of administration of formulation for reduction of particle production (hours) versus average particle counts greater than 0.3 μm produced relative to baseline (% counts/liter).

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Detailed Description of the Invention

Lung mucociliary clearance is the primary mechanism by which the airways are kept clean from particles present in the liquid film that coats them. The conducting airways are lined with ciliated epithelium that beat to drive a layer of mucus towards the larynx, clearing the airways from the lowest ciliated region in 24 hours. The fluid coating consists of water, sugars, proteins, glycoproteins, and lipids. It is generated in the airway epithelium and the submucosal glands, and the thickness of the layer ranges from several microns in the trachea to approximately 1 micron in the distal airways in humans, rat, and guinea pig.

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A second important mechanism for keeping the lungs clean is via momentum transfer from the air flowing through the lungs to the mucus coating. Coughing increases this momentum transfer and is used by the body to aid the removal of excess mucus. It becomes important when mucus cannot be adequately removed by ciliary beating alone, as occurs in mucus hypersecretion associated with many disease states. Air speeds as high as 200 m/s can be generated during a forceful cough. The onset of unstable sinusoidal disturbances at the mucus layer has been observed at such air speeds. This disturbance results in enhanced momentum transfer from the air to the mucus and consequently accelerates the rate of mucus clearance from the lungs. Experiments have shown that this disturbance is initiated when the air speed exceeds some critical value that is a function of film thickness, surface tension, and viscosity (M. Gad-El-Hak, R.F. Blackwelder, J.J. Riley, *J. Fluid Mech.* (1984) 140:257-280). Theoretical predictions and experiments with mucus-like films suggest that the critical speed to initiate wave disturbances in the lungs is in the range of 5-30 m/s.

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It is clear from the discussion above relating to cleanrooms that it would be highly advantages to (1) determine that rate of particle production

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and size range of particles produced by individuals, (2) predict which people will produce the greatest level of contamination and (3) minimize contamination produced by breathing, coughing, moving, etc.

5 The first and second goals can be achieved using a device such as that described herein which measures the size and number of particles produced on an individual basis. Particle production can be measured at rest or during various activities. This allows for determination if a formulation for reducing particle exhalation should be administered to an individual and/or for selection of individuals with the minimal particle production for use in cleanroom environments.

10 The third goal can be achieved by administering a formulation for decreasing particle production, such as formulation containing a substances that are easily ionized in an aqueous or organic solvent environment (also referred to herein as "conductive agents"), as described herein. In one embodiment, the formulation is administered to one or more individuals using a device which provides an aerosol that sprays a fine mist of the
15 formulation into the pulmonary and/or nasal region of an individual, thereby decreasing the output of particles. Individuals may be treated prior to entering, and/or after entering, the cleanroom.

I. Diagnostic Device for Determining Particle Production (rate and size range)

20 Diagnosis of animals or humans to determine their rate of particle production and the size range of particles produced during exhalation. The analysis of this data can be used to determine if a formulation for reducing particle exhalation is needed. This device is particularly useful prior to entry in a cleanroom or while a user is working in a cleanroom to ensure that the cleanroom standards are maintained. The device can also be used to identify animals and humans who have an enhanced propensity to exhale aerosols (referred
25 to herein as "over producers", "super-producers", or "super spreaders"). This can be accomplished by screening for a number of factors including the measurement of expired air and inspired air, the assessment of exhaled particle numbers, the assessment of exhaled particle

size, the assessment of tidal volume and respiratory frequency during sampling, and the assessment of viral and bacterial infectivity. The assessment of exhaled particle numbers is done at a respiratory flow rate of about 10 to about 120 liters per minutes (LPM).

5 A diagnostic instrument (10) for the measurement of particles produced and exhaled by a person is illustrated in Figures 1 and 2. As shown in Figure 1, the device (10) contains a mouthpiece (12). The outlet (13) of the mouthpiece (12) is attached to a filter (14) and a low resistance one-way valve (16) via a branched connector (18), such as a wye or tee connector. 10 The one-way valve (16) is typically located inside a tube (19) which forms one half of the connector (18) or is attached directly to one end of the connector (18). At an end distal to the outlet (13) of the mouthpiece, the tube (19) is attached to a particle counter (20). The particle counter (20) is connected to the computer (30) in a manner that allows data to be provided 15 to the computer (30). The data from the particle counter (20) is sent to a computer (30), to allow a user to read, analyze and interpret the data. In one embodiment the device is portable and, optionally, operates on batteries.

Any suitable mouthpiece may be used. In one embodiment, illustrated in figures 1 and 2, the mouthpiece (12) is designed to allow the 20 user to place his lips around the outside of the mouthpiece and thereby form a seal between his lips and the mouthpiece. In another embodiment, the mouthpiece is in the form of a nasal prongs and a seal is formed between the user's nostrils and the prongs. In another embodiment, the mouthpiece is in the form of a mask, which covers the user's mouth and nose. In this 25 embodiment, a seal is formed between the user's face and the mask. In another embodiment, the mouthpiece is in the form of a mask which only covers the user's nose. Preferably the mouthpiece is disposable.

The filter (14) is typically a high efficiency (>99.97% at 0.3 μ m), low pressure drop (<2.5 cm H₂O at 60 L/min) filter, optionally the filter has a 30 bacterial/viral removal efficiency of >99.99%. The filter is selected to remove at least particles having sizes in the range to be measured by the particle counter (20), preferably the filter removes particles having a sizes

even smaller than the range to be measured by the particle counter. Preferably, the filter is designed to remove particles of greater than or equal to 0.1 micrometer in diameter. In one embodiment, a series of two or more filters (14) (not shown in figure) may be included between the mouthpiece
5 and the ambient air in order to prevent the contamination of the upstream system between users. In this embodiment, one or more of the filters may be replaced with a bank of filters in parallel in order to minimize flow resistance.

In a preferred embodiment, the mouthpiece (12), filter (14),
10 connector (18), and one-way valve (16) are all disposable. Optionally, the mouthpiece (12), filter (14), connector (18), and/or one-way valve (16) are formed from biodegradable materials.

The particle counter (20) must have sufficient sensitivity to accurately count sub-micron sized particles and may be designed and
15 assembled as described. The measurement of particle number and particle size can be done by electrical mobility analysis, impaction, electrostatic impaction, infrared spectroscopy, laser diffraction, or light scattering. Examples of currently available particle counters for the measurement of particle number and size include: Scanning Mobility Particle Sizer (SMPS)
20 (TSI, Shoreview MN), Andersen cascade impactor or Next generation pharmaceutical impactor (Copley Scientific, Nottingham UK), Electrical low pressure impactor (ELPI) (Dekati, Tampere Finland) and Helos (Sympatec, Clausthal, Germany). In a preferred embodiment, the particle counter is an optical particle counter, most preferably one which operated by light
25 scattering using a LASER or laser diode light source. In this preferred embodiment, the optical particle counter has a range of at least 0.3 to 5 μm and preferably from 0.1 to 25 μm . It differentiates its measurement range into at least 2 channels and preferably at least 4 channels. It operates at a steady sample flow rate of at least 0.1 cubic foot per minute and preferably
30 of at least 1 cubic foot per minute which may be generated and controlled as part of the particle counter or as separate vacuum pump and flow regulator components (not shown in figure). Currently available optical particle

counters that may be appropriate for this preferred embodiment include model CI-450, CI-500, CI-550 of Ultimate 100 (Climet Instruments, Redlands CA) and models Lasair II, Airnet 310 (Particle Measuring Systems, Boulder CO)

5 The particle counter (20) is connected to the computer (30) in a manner that allows data from the particle counter (20) to be sent to the computer (30). Optionally, the particle counter (20) is also connected to the computer (30) in a manner that allows control commands to be sent from the computer (30) to the particle counter (20). The computer may be a
10 microprocessor internal or external to the particle counter.

 In one embodiment, illustrated in Figure 2, the device (10) contains a gas flow meter (22). The gas flow meter (22) should have a low flow resistance so as not to influence the user's respiration rate such as a pneumotachometer or pneumotachograph of type Fleisch or Lilly.
15 Alternatively, the gas flow meter may measure flow by measuring the temperature change or heat transfer from an electrically heated wire (e.g. a hot wire anemometer), or by counting the number of revolutions per unit of time of a small turbine (e.g a turbine flow meter), or by measuring the differential pressure across or the bypass flow rate through a bypass around a
20 flow restriction, such as a laminar flow element. The volume displacement is then computed by integrating flow with respect to time.

 Pneumotachometers are commonly used to measure the flow rate of different gases during respiration. Air is passed through a short tube (e.g. a Fleisch tube) that contains a mesh which presents a small resistance to the air
25 flow (not shown in figure). The resulting pressure drop across the mesh is proportional to the flow rate. The pressure drop is very small, usually around a few mmH₂O. A differential pressure transducer (24) is normally used to measure the pressure drop across the flow meter (e.g. Fleisch tube), in order to enhance detection of such small drops in pressure. Preferably the
30 differential pressure transducer is connected to a signal conditioner (26) which amplifies the signal and sends it to data acquisition software in the computer (30). In a preferred embodiment, the differential pressure

transducer (24) is a Validyne DP45-14 differential pressure transducer. In a preferred embodiment, the signal conditioner (26) is a Validyne CD15 sine wave carrier demodulator. The pneumotachometer may be used in lung function analysis, or during artificial ventilation of the lungs.

5 In a preferred embodiment, the flow meter (22) is a low flow rate mass flow meter measuring the bypass flow around a flow restriction, such as a laminar flow element. In this embodiment, the laminar flow element (not shown in figure) consists of a series of parallel tubes sized such that the flow through the tubes is in the laminar flow regime for respirable flow rates,
10 preferably for flow rates between +130 and -70 L/min, where positive flow represents the flow direction during exhalation. In a preferred embodiment, the low flow meter provides digital output at a frequency greater than 5Hz. One example of this type of flow meter is the Sensirion model ASF1430.

 In another embodiment, the device (10) includes connections for
15 performing further exhaled breath analysis simultaneously or in series with particle size and count measurements. For example, exhaled breath condensate may be collected in standard devices such as R-tubes or exhaled air may be passed through culture media filters for further analysis via connections (not shown in figure) located along the tube (19) leading to the
20 optical particle counter (20).

II. Formulations for Decreasing Particle Production

Bioaerosol particles are formed by instabilities in the endogenous surfactant layer in the airways. The formulations described herein are effective to alter the biophysical properties of the mucosal lining. These
25 properties include, for example, increasing gelation at the mucus surface, the surface tension of the mucosal lining, the surface elasticity of the mucosal lining, and the bulk viscoelasticity of the mucosal lining. The formulations described herein are effective to decrease particle exhalation, by preventing or reducing exhaled particle formation from the oropharynx or nasal cavities.
30 The endogenous surfactant layer may be altered by simply diluting the endogenous surfactant pool via either delivery of isotonic saline (though not in such a large amount as to cause a subject to expectorate) or a hypertonic

saline solution that causes the cells lining the lung's airways to dilute further the endogenous surfactant layer via production of water.

It has been discovered that physical properties of the endogenous surfactant fluid in the lungs, can be altered by administration of a saline solution, as well as by administration of an aqueous saline solution containing other materials, such as osmotically active materials, conductive materials, and/or surfactants. Concentration ranges of the salt or other osmotically active material range from about 0.01% to about 10% by weight, preferably between 0.9% to about 10%. A preferred aerosol solution for altering physical properties of the mucosal lining is isotonic saline.

A. Conductive formulations

Preferred formulations for altering the biophysical properties of the lung's lining fluid are formulations containing certain charge concentrations and mobility, and thus liquid conductivity. In one preferred embodiment, the formulations include aqueous solutions or suspensions that are conductive (also referred to herein as the "conductive formulation(s)"). Suitable conductive formulations typically have conductivity values of greater than 5,000 $\mu\text{S}/\text{cm}$, preferably greater than 10,000 $\mu\text{S}/\text{cm}$, and more preferably greater than 20,000 $\mu\text{S}/\text{cm}$. These formulations are particularly useful when administered to a patient to suppress particle exhalation. Solution conductivity is a product of the ionic strength, concentration, and mobility (the latter two contribute to the conductivity of the formulation as a whole). Any form of the ionic components (anionic, cationic, or zwitterionic) can be used. These conductive materials may alter the mucosal lining properties by acting, for example, as a cross-linking agent within the mucus. The ionic components in the formulations described herein may interact with the strongly linked anionic glycoproteins within normal tracheobronchial mucus. These interactions may influence the state of the air/liquid surface of the airway lining fluid and transiently the nature of the physical entanglements due to covalent and noncovalent interactions, including hydrogen bonding, hydrophobic, and electrostatic interactions (Dawson, M., Wirtz, D., Hanes, J.

(2003) *The Journal of Biological Chemistry*. Vol. 278, No. 50, pp. 50393-50401).

Optionally the formulation includes mucoactive or mucolytic agents, such as MUC5AC and MUC5B mucins, DNA, N-acetylcysteine (NAC), cysteine, nacystelyn, dornase alfa, gelsolin, heparin, heparin sulfate, P2Y2 agonists (e.g. UTP, INS365), and nedocromil sodium.

i. Conductive agents

The formulations contain substances that are easily ionized in an aqueous or organic solvent environment (also referred to herein as “conductive agents”), such as salts, ionic surfactants, charged amino acids, charged proteins or peptides, or charged materials (cationic, anionic, or zwitterionic). Suitable salts include any salt form of the elements sodium, potassium, magnesium, calcium, aluminum, silicon, scandium, titanium, vanadium, chromium, cobalt, nickel, copper, manganese, zinc, tin, and similar elements. Examples include sodium chloride, sodium acetate, sodium bicarbonate, sodium carbonate, sodium sulfate, sodium stearate, sodium ascorbate, sodium benzoate, sodium biphosphate, sodium phosphate, sodium bisulfite, sodium citrate, sodium borate, sodium gluconate, calcium chloride, calcium carbonate, calcium acetate, calcium phosphate, calcium alginite, calcium stearate, calcium sorbate, calcium sulfate, calcium gluconate, magnesium carbonate, magnesium sulfate, magnesium stearate, magnesium trisilicate, potassium bicarbonate, potassium chloride, potassium citrate, potassium borate, potassium bisulfite, potassium biphosphate, potassium alginate, potassium benzoate, magnesium chloride, cupric sulfate, chromium chloride, stannous chloride, and sodium metasilicate and similar salts. Suitable ionic surfactants include sodium dodecyl sulfate (SDS) (also known as sodium lauryl sulfate (SLS)), magnesium lauryl sulfate, Polysorbate 20, Polysorbate 80, and similar surfactants. Suitable charged amino acids include L-Lysine, L-Arginine, Histidine, Aspartate, Glutamate, Glycine, Cysteine, Tyrosine. Suitable charge proteins or peptides include proteins and peptides containing the charged amino acids, Calmodulin (CaM), and Troponin C. Charged phospholipids, such as 1,2-dioleoyl-sn-

glycero-3-ethylphosphocholine triflate (EDOPC) and alkyl phosphocholine trimesters, can be used.

The preferred formulations are formulations containing salts, such as saline (0.15 M NaCl or 0.9%) solution, CaCl₂ solution, CaCl₂ in saline
5 solution, or saline solution containing ionic surfactants, such as SDS or SLS. In the preferred embodiment, the formulation contains saline solution and CaCl₂. Suitable concentration ranges of the salt or other conductive/charged compounds can vary from about 0.01% to about 20% (weight of conductive or charged compound/total weight of formulation), preferably between 0.1%
10 to about 10% (weight of conductive or charged compound/total weight of formulation), most preferably between 0.1 to 7% (weight of conductive or charged compound/total weight of formulation).

Saline solutions have long been delivered chronically to the lungs with small amounts of therapeutically active agents, such as beta agonists,
15 corticosteroids, or antibiotics. For example, VENTOLIN[®] Inhalation Solution (GSK) is an albuterol sulfate solution used in the chronic treatment of asthma and exercise-induced bronchospasm symptoms. A VENTOLIN[®] solution for nebulization is prepared (by the patient) by mixing 1.25-2.5mg of albuterol sulfate (in 0.25-0.5mL of aqueous solution) into sterile normal
20 saline to achieve a total volume of 3mL. No adverse effects are thought to be associated with the delivery of saline to the lungs by VENTOLIN[®] nebulization, even though nebulization times can range from 5-15 minutes. Saline is also delivered in more significant amounts to induce expectoration. Often these saline solutions are hypertonic (sodium chloride concentrations
25 greater than 0.9%, often as high as 5%) and generally they are delivered for up to 20 minutes.

B. Osmotically Active Materials

Many materials may be osmotically active, including binary salts, such as sodium chloride, or any other kinds of salts, or sugars, such as
30 mannitol. Osmotically active materials, normally owing to their ionization and possibly size, do not easily permeate cell membranes and therefore exert an osmotic pressure on contiguous cells. Such osmotic pressure is essential

to the physical environment of cellular material, and regulation of this pressure occurs by cell pumping of water into or out of the cell. Solutions delivered to the lungs that are isotonic normally do not create an imbalance in osmotic pressure in the lung fluid and therefore simply dilute the natural
5 endogenous lung fluid with water and salt. Solutions of high osmotic content (i.e. hypertonic solutions) create an imbalance of osmotic pressure, with greater pressure in the lung fluid, causing cells to pump water into the lung fluid and therefore further dilute lung surfactant composition.

C. Active Ingredients

10 The formulations disclosed herein can be used by any route for delivery of a variety of organic or inorganic molecules, especially small molecule drugs, such as antivirals and antibacterial drugs including antibiotics, antihistamines, bronchodilators, cough suppressants, anti-inflammatory, vaccines, adjuvants and expectorants. Examples of
15 macromolecules include proteins and large peptides, polysaccharides and oligosaccharides, and DNA and RNA nucleic acid molecules and their analogs having therapeutic, prophylactic or diagnostic activities. Nucleic acid molecules include genes, antisense molecules that bind to complementary DNA to inhibit transcription, and ribozymes. Preferred
20 agents are antiviral, steroid, bronchodilators, antibiotics, mucus production inhibitors and vaccines.

In the preferred embodiment, the concentration of the active agent ranges from about 0.01% to about 20% by weight. In a more preferred embodiment, the concentration of active agent ranges from between 0.9% to
25 about 10%.

D. Carriers and Aerosols for Administration

The formulation may be delivered in a solution, a suspension, a spray, a mist, a foam, a gel, a vapor, droplets, particles, or a dry powder form (for example, using a metered dose inhaler including HFA propellant, a
30 metered dose inhaler with non-HFA propellant, a nebulizer, a pressurized can, or a continuous sprayer). Carriers can be divided into those for

administration via solutions or suspensions (liquid formulations) and those for administration via particles (dry powder formulations).

1. Dosage forms for Administration to different mucosal surfaces

5 For administration to mucosal surfaces in the respiratory tract, the formulation is typically in the form of solution, suspension or dry powder. Preferably, the formulation is aerosolized. The formulation can be generated via any aerosol generators, such as dry powder inhaler (DPI), nebulizers or pressurized metered dose inhalers (pMDI). The term "aerosol" as used herein
10 refers to any preparation of a fine mist of particles, typically less than 10 microns in diameter. The preferred mean diameter for aqueous formulation aerosol particles is about 5 microns, for example between 0.1 and 30 microns, more preferably between 0.5 and 20 microns and most preferably between 0.5 and 10 microns.

15 For administration to the oral mucosa, including buccal mucosa, the formulation may be administered as a solid that dissolves following administration to the mouth and/or adheres to the mucosal surface, or a liquid.

A preferred aerosol solution for altering physical properties of the
20 lung's lining fluid is isotonic saline. The aerosol can consist just of a solution, such as an aqueous solution, most preferably a saline solution. Alternatively, the aerosol may consist of an aqueous suspension or dry particles.

2. Liquid Formulations

25 Aerosols for the delivery of therapeutic agents to the respiratory tract have been developed. See, for example, Adjei, A. and Garren, *J. Pharm. Res.*, 7: 565-569 (1990); and Zanen, P. and Lamm, J.-W. *J. Int. J. Pharm.*, 114: 111-115 (1995). These are typically formed by atomizing a liquid formulation, such as a solution or suspension, under pressure through a
30 nebulizer or through the use of a metered dose inhaler ("MDI"). In the preferred embodiment, the liquid formulations are aqueous solutions or suspensions.

3. Dry Powder Formulations

The geometry of the airways is a major barrier for drug dispersal within the lungs. The lungs are designed to entrap particles of foreign matter that are breathed in, such as dust. There are three basic mechanisms of deposition: impaction, sedimentation, and Brownian motion (J.M. Padfield. 1987. In: D. Ganderton & T. Jones eds. Drug Delivery to the Respiratory Tract, Ellis Harwood, Chichester, U.K.). Impaction occurs when particles are unable to stay within the air stream, particularly at airway branches. They are adsorbed onto the mucus layer covering bronchial walls and cleaned out by mucocilliary action. Impaction mostly occurs with particles over 5 μm in diameter. Smaller particles ($<5 \mu\text{m}$) can stay within the air stream and be transported deep into the lungs. Sedimentation often occurs in the lower respiratory system where airflow is slower. Very small particles ($<0.6 \mu\text{m}$) can deposit by Brownian motion. This regime is undesirable because deposition cannot be targeted to the alveoli (N. Worakul & J.R. Robinson. 2002. In: Polymeric Biomaterials, 2nd ed. S. Dumitriu ed. Marcel Dekker. New York).

The preferred mean diameter for aerodynamically light particles for inhalation is at least about 5 microns, for example between about 5 and 30 microns, most preferably between 3 and 7 microns in diameter. The particles may be fabricated with the appropriate material, surface roughness, diameter and tap density for localized delivery to selected regions of the respiratory tract such as the deep lung or upper airways. For example, higher density or larger particles may be used for upper airway delivery. Similarly, a mixture of different sized particles, provided with the same or different therapeutic agent may be administered to target different regions of the lung in one administration.

As used herein, the phrase "aerodynamically light particles" refers to particles having a mean or tap density less than about 0.4 g/cm^3 . The tap density of particles of a dry powder may be obtained by the standard USP tap density measurement. Tap density is a standard measure of the envelope mass density. The envelope mass density of an isotropic particle is defined

as the mass of the particle divided by the minimum sphere envelope volume in which it can be enclosed. Features contributing to low tap density include irregular surface texture and porous structure.

Dry powder formulations ("DPFs") with large particle size have
5 improved flowability characteristics, such as less aggregation (Visser, J.,
Powder Technology 58: 1-10 (1989)), easier aerosolization, and potentially
less phagocytosis. Rudt, S. and R. H. Muller, *J. Controlled Release*, 22: 263-
272 (1992); Tabata, Y., and Y. Ikada, *J. Biomed. Mater. Res.*, 22: 837-858
(1988). Dry powder aerosols for inhalation therapy are generally produced
10 with mean diameters primarily in the range of less than 5 microns, although a
preferred range is between one and ten microns in aerodynamic diameter.
Ganderton, D., *J. Biopharmaceutical Sciences*, 3:101-105 (1992); Gonda, I.
"Physico-Chemical Principles in Aerosol Delivery," in Topics in
Pharmaceutical Sciences 1991, Crommelin, D. J. and K. K. Midha, Eds.,
15 Medpharm Scientific Publishers, Stuttgart, pp. 95-115 (1992). Large
"carrier" particles (containing no drug) have been co-delivered with
therapeutic aerosols to aid in achieving efficient aerosolization among other
possible benefits. French, D. L., Edwards, D. A. and Niven, R. W., *J.*
Aerosol Sci., 27: 769-783 (1996). Particles with degradation and release
20 times ranging from seconds to months can be designed and fabricated by
established methods in the art.

Particles can contain conductive agent(s), alone, or in combination
with drug, antiviral, antibacterial, antimicrobial, surfactant, proteins,
peptides, polymer, or combinations thereof. Representative surfactants
25 include L- α -phosphatidylcholine dipalmitoyl ("DPPC"), diphosphatidyl
glycerol (DPPG), 1,2-Dipalmitoyl-sn-glycero-3-phospho-L-serine (DPPS),
1,2-Dipalmitoyl-sn-glycero-3-phosphocholine (DSPC), 1,2-Distearoyl-sn-
glycero-3-phosphoethanolamine (DSPE), 1-palmitoyl-2-
oleoylphosphatidylcholine (POPC), fatty alcohols, polyoxyethylene-9-lauryl
30 ether, surface active fatty acids, sorbitan trioleate (Span 85), glycocholate,
surfactin, poloxomers, sorbitan fatty acid esters, tyloxapol, phospholipids,
and alkylated sugars. Polymers may be tailored to optimize particle

characteristics including: i) interactions between the agent to be delivered and the polymer to provide stabilization of the agent and retention of activity upon delivery; ii) rate of polymer degradation and thus drug release profile; iii) surface characteristics and targeting capabilities via chemical
5 modification; and iv) particle porosity. Polymeric particles may be prepared using single and double emulsion, solvent evaporation, spray drying, solvent extraction, phase separation, simple and complex coacervation, interfacial polymerization, and other methods well known to those of ordinary skill in the art. Particles may be made using methods for making microspheres or
10 microcapsules known in the art. The preferred methods of manufacture are by spray drying and freeze drying, which entails using a solution containing the conductive/charged materials, spraying the solution onto a substrate to form droplets of the desired size, and removing the solvent.

III. Administration of Formulations to the Respiratory Tract

15 A. Administration of Conductive formulations to reduce amount of exhaled particles

In a preferred embodiment, the conductive formulation contains a suitable conductivity for increasing the viscoelasticity of the mucosal membrane at the site of administration of the formulation to suppress or
20 reduce the formation of bioaerosol particles formation during breathing, coughing, sneezing, and/or talking. Preferably, the formulation is administered to one or more individuals in an effective amount to reduce particle production. Preferably the formulation is administered to a person prior to entry in a cleanroom or while a person is working in a cleanroom to
25 ensure that the cleanroom standards are maintained. If animals or humans have been identified as having an enhanced propensity to exhale aerosols (i.e. are “over producers”, “super-producers”, or “superspreaders”), the formulation may be administered to reduce particle production, to prevent or reduce spread of infections, or to prevent or reduce uptake of pathogens by
30 the human or animal.

B. Administration to the Respiratory Tract

The respiratory tract is the structure involved in the exchange of gases between the atmosphere and the blood stream. The lungs are branching structures ultimately ending with the alveoli where the exchange of gases occurs. The alveolar surface area is the largest in the respiratory system and is where drug absorption occurs. The alveoli are covered by a thin epithelium without cilia or a mucus blanket and secrete surfactant phospholipids. J.S. Patton & R.M. Platz. 1992. *Adv. Drug Del. Rev.* 8:179-196

The respiratory tract encompasses the upper airways, including the oropharynx and larynx, followed by the lower airways, which include the trachea followed by bifurcations into the bronchi and bronchioli. The upper and lower airways are called the conducting airways. The terminal bronchioli then divide into respiratory bronchioli which lead to the ultimate respiratory zone, the alveoli or deep lung. The deep lung, or alveoli, is the primary target of inhaled therapeutic aerosols for systemic drug delivery.

The formulations are typically administered to an individual to deliver an effective amount to alter physical properties such as surface tension and viscosity of endogenous fluid in the upper airways, thereby enhancing delivery to the lungs and/or suppressing coughing and/or improving clearance from the lungs. Effectiveness can be measured using a diagnostic device as described herein. For example, saline can be administered in a volume of 1 gram to a normal adult. Exhalation of particles is then measured. Delivery is then optimized to minimize dose and particle number.

Formulations can be administered using a metered dose inhaler ("MDI"), a nebulizer, an aerosolizer, or using a dry powder inhaler. Suitable devices are commercially available and described in the literature.

Aerosol dosage, formulations and delivery systems may be selected for a particular therapeutic application, as described, for example, in Gonda, I. "Aerosols for delivery of therapeutic and diagnostic agents to the respiratory tract," in *Critical Reviews in Therapeutic Drug Carrier Systems*,

6:273-313, 1990; and in Moren, "Aerosol dosage forms and formulations,"
in: *Aerosols in Medicine, Principles, Diagnosis and Therapy*, Moren, et al.,
Eds. Eisevier, Amsterdam, 1985.

5 Delivery is achieved by one of several methods, for example, using a
metered dose inhaler including HFA propellant, a metered dose inhaler with
non-HFA propellant, a nebulizer, a pressurized can, or a continuous sprayer.
For example, the patient can mix a dried powder of pre-suspended
therapeutic with solvent and then nebulize it. It may be more appropriate to
10 use a pre-nebulized solution, regulating the dosage administered and
avoiding possible loss of suspension. After nebulization, it may be possible
to pressurize the aerosol and have it administered through a metered dose
inhaler (MDI). Nebulizers create a fine mist from a solution or suspension,
which is inhaled by the patient. The devices described in U.S. Patent No.
5,709,202 to Lloyd, et al., can be used. An MDI typically includes a
15 pressurized canister having a meter valve, wherein the canister is filled with
the solution or suspension and a propellant. The solvent itself may function
as the propellant, or the composition may be combined with a propellant,
such as FREON® (E. I. Du Pont De Nemours and Co. Corp.). The
composition is a fine mist when released from the canister due to the release
20 in pressure. The propellant and solvent may wholly or partially evaporate
due to the decrease in pressure.

In an alternative embodiment, the formulation is in the form of salt or
osmotically active material particles which are dispersed on or in an inert
substrate, which is placed over the nose and/or mouth and the formulation
25 particles inhaled. The inert substrate is preferably a biodegradable or
disposable woven or non-woven fabric and more preferably the fabric is
formed of a cellulosic-type material. An example is tissues currently sold
which contain lotion to minimize irritation following frequent use. These
formulations can be packaged and sold individually or in packages similar to
30 tissue or baby wipe packages, which are easily adapted for use with a liquid
solution or suspension.

In one embodiment, the formulation is administered to one or more individuals using a device which provides an aerosol that sprays a fine mist of the formulation into the pulmonary and/or nasal region of an individual, thereby decreasing the output of particles. The formulation may be administered to humans or animals by creating an aqueous environment in which the humans and animals move or remain for sufficient periods of time to sufficiently hydrate the lungs. This atmosphere might be created by use of a nebulizer or even a humidifier. Preferably the nebulizer or humidifier administers a conductive formulation. Individuals may be treated prior to entering, and/or after entering, a cleanroom.

IV. Methods of using the Diagnostic Device

When using the device illustrated in Figures 1 and 2, the user places his lips around the mouthpiece (12). The user seals his airways off from the ambient air preferably via a nose clip and by sealing his lips to a mouthpiece. If a mask is used as the mouthpiece, the user places the mask over his mouth and/or nose. If nose prongs are used as the mouthpiece, the user places the nose prongs in his nose. If the mouthpiece is in the form of a mask, the user places the mask over his nose and/or mouth, and thereby seals off his airways from the ambient air. Then the user inhales. Inspired air enters the system through the filter (14) which removes particles in the predetermined measured range. Exhaled air passes through the low resistance one-way valve (16) and into the particle counter (20). The one-way valve (16) helps to prevent the transmission of exhaled pathogens from one user to the next.

The expired air travels to the particle counter (20), which measures the number of particles and size of particles. The particle counter (20) samples at a fixed flow rate preferably greater than the peak exhaled flow rate so that at all points in time the mean flow direction through the filter (14) is into the system, preventing the loss of exhaled particles into the filter (14). Preferably the particle counter samples at flow rates greater than 28 L/min. The particle counter (20) then provides the data from the particle counter (20) to the computer (30). In one embodiment, the user is provided with a visual feedback of his breathing pattern and cues to maintain a

prescribed breathing pattern, for example tidal breathing. The particle counter (20) can be controlled either remotely from a PC or locally such as from a touch screen interface with data measurement and analysis performed locally at the optical particle counter or remotely at a personal computer. A
5 controller (not shown in figure) for the generation and control of the sample flow rate may be internal or external to the optical particle counter. The inhalation, exhalation, and measurement steps may be repeated multiple times. Then the computer calculates the mean particle size, the average particle distribution, and mean rate of particle production. If it is necessary
10 to decrease the number and size of particles exhaled by the user, a formulation for decreasing particle exhalation as described herein, is administered to the user.

Optionally, the diagnostic instrument (10) is designed to measure particles produced and exhaled by a person with associated breathing rate. In
15 this embodiment, illustrated in Figure 2, the inspired air enters the system through a low flow resistance flow meter (22) which characterizes the breathing pattern of the user and the particle counter flow rate together. Air then enters the filter (14) which removes particles in the measured range. Exhaled air passes through a low resistance one way valve (16), through the
20 tube (18) and into the particle counter (20), as described above. The data from the flow meter, differential pressure transducer, and or signal conditioner is sent to the computer for calculation and analysis.

Depending on the rate of particle production and size of particles produced, as determined by the data obtained using the diagnostic device, a
25 formulation may be administered to the user in an effective amount to reduce particle production. The formulation may be administered prior to entry or following entry into a cleanroom.

The present invention will be further understood by reference to the following non-limiting examples.

30 **Examples**

Example 1: *In Vitro* Simulation

A simulated cough machine system was designed similar to that described by King *Am. J. Respir. Crit. Care Med.* 156(1):173-7 (1997). An air-tight 6.25-liter Plexiglas tank equipped with a digital pressure gauge and pressure relief valve was constructed to serve as the capacitance function of the lungs. To pressurize the tank, a compressed air cylinder with regulator and air filter was connected to the inlet. At the outlet of the tank, an Asco two-way normally-closed solenoid valve (8210G94) with a sufficient Cv flow factor was connected for gas release. The solenoid valve was wired using a typical 120V, 60Hz light switch. Connected to the outflow of the solenoid valve was a Fleisch no. 4 pneumotachograph, which created a Poiseuille flow needed to examine the “cough” profile. The outlet of the Fleisch tube was connected to a ¼” NPT entrance to the model trachea. A Validyne DP45-14 differential pressure transducer measured the pressure drop through the Fleisch tube. A Validyne CD15 sine wave carrier demodulator was used to amplify this signal to the data acquisition software. Weak polymeric gels with rheological properties similar to tracheobronchial mucus were prepared as described by King et al *Nurs Res.* 31(6):324-9 (1982). Locust bean gum (LBG) (Fluka BioChemika) solutions were crosslinked with sodium tetraborate ($\text{Na}_2\text{B}_4\text{O}_7$) (J.T.Baker). LBG at 2% wt/vol was dissolved in boiling Milli-Q distilled water. A concentrated sodium tetraborate solution was prepared in Milli-Q distilled water. After the LBG solution cooled to room temperature, small amounts of sodium tetraborate solution were added and the mixture was slowly rotated for 1 minute. The still watery mucus simulant was then pipetted onto the model trachea creating simulant depth based on simple trough geometry. Mucus simulant layers were allowed 30 minutes to crosslink prior to initiation of “cough” experiments. At this point, $t=0$ min, time points were measured, followed by $t=30$ min and $t=60$ min. Final concentrations of sodium tetraborate ranged from 1-3 mM. An acrylic model trachea was designed 30 cm long with interior width and height of 1.6 cm. The model trachea formed a rectangular shaped tube with a separate top to fit, allowing for easy access to the mucus simulant layer. A gasket and C-clamps were used to create an

air-tight seal. A rectangular cross-section was chosen to enable uniform mucus simulant height and to avoid problems associated with round tubes and gravity drainage. The cross-sectional area of the model trachea was also physiologically relevant. The end of the model trachea remained open to the atmosphere. Nebulized solutions were delivered to the mucus simulant via a PARI LC Jet nebulizer and Proneb Ultra compressor. Formulations included normal isotonic 0.9% saline (VWR) and 100 mg/mL of synthetic phospholipids 1,2-Dipalmitoyl-sn-glycero-3-phosphocholine/1-Palmitoyl-2-oleoyl-sn-glycero-3-phosphoglycerol (DPPC/POPG) (Genzyme) 7/3 wt% suspended in isotonic saline. 3 mL of the chosen formulation was pipetted into the nebulizer and aerosolized until nebulizer sputter through the open-ended but clamped model trachea trough on the layer of mucus simulant. The model trachea was then attached to the outlet of the Fleisch tube prior to $t=0$ min experiments. As well, $t=30$ min and $t=60$ min (post-dose) experiments were performed.

A Sympatec HELOS/KF laser diffraction particle sizer was used to size the created mucus simulant bioaerosols. The Fraunhofer method for sizing diffracted particles was used. The HELOS was equipped with an R2 submicron window module enabling a measuring range of 0.25-87.5 μm . Prior to "cough" experiments, the end of the model trachea was adjusted to be no more than 3 cms from the laser beam. As well, the bottom of the model trachea was aligned with the 2.2 mm laser beam using support jacks and levels. Dispersed bioaerosols were collected after passing through the diffraction beam using a vacuum connected to an inertial cyclone followed by a HEPA filter. Before each run, the laser was referenced for 5 s to ambient conditions. Measurement began after a specified trigger condition of optical concentration ($C_{\text{opt}} \geq 0.2\%$) and stopped 2 s after $C_{\text{opt}} \leq 0.2\%$. Sympatec WINDOX software was used to create cumulative and density distribution graphs versus log particle size by volume.

A typical cough profile, consisting of a biphasic burst of air, was passed over the 1.5 mm layer of mucus simulant. The initial flow of air

possessed a flow rate of about 12 L/s for 30-50 ms. The second phase lasted 200-500 ms and then rapidly decayed.

Bioaerosol particle concentration following three coughs was measured over time (Figures 3A, 3B and 3C) in the case of an undisturbed
5 mucus simulant, and in the cases of saline delivery (Figures 3A, 3B and 3C) and surfactant delivery (not shown). In the undisturbed case, bioaerosol particle size remains constant over time with a median size of about 400 nanometers. Following the addition of saline, bioaerosol particle size increases from 1 micron (t=0) (Figure 3A) to about 60 microns (t=30 min)
10 (Figure 3B) and then diminishes to 30 microns (t=60 min) (Figure 3C).

These *in vitro* results show that saline delivered to a mucus layer causes a substantial increase in particle size on breakup, possibly owing to an increase in surface tension. As indicated by the *in vivo* results, the larger size droplets are less capable of exiting the mouth. Therefore, delivery of the
15 solution serves to significantly lower the number of expired particles.

Example 2: Reduction of Exhaled Aerosol Particles in Human Study

A proof of concept study of exhaled aerosol particle production was performed using 12 healthy subjects. The objectives of the study were (1) to determine the nature of exhaled bioaerosol particles (size distribution and
20 number); (2) to validate the utility of a device that is sensitive enough to accurately count the exhaled particles; (3) to assess the baseline count of particles exhaled from the healthy lung; and (4) to measure the effect of two exogenously administered treatment aerosols on exhaled particle count suppression. Experiments were performed with different particle detectors to
25 determine average particles per liter and average particle size for healthy human subjects. Following the inspiration of particle-free air, healthy subjects breathe out as little as 1-5 particles per liter, with an average size of 200-400 nm in diameter. Significant variations occur in numbers of particles from subject to subject, so that some subjects exhale as many as 30,000
30 particles per liter, again predominantly of submicron particle size. A device with sufficient sensitivity to accurately count sub-micron sized particles was designed and assembled. The LASER component of the device was

calibrated in accordance with manufacturer procedures (Climet Instruments Company, Redlands, CA). This device accurately measured particles in the range of 150-500 nm with a sensitivity of 1 particle/liter. A series of filters eliminated all background particle noise.

5 Following protocol IRB approval, 12 healthy subjects were enrolled in the study. Inclusion criteria were good health, age 18 – 65 years, normal lung function (FEV_1 predicted > 80%), informed consent and capability to perform the measurements. Exclusion criteria were presence or a history of significant pulmonary disease (e.g. asthma, COPD, cystic fibrosis),
10 cardiovascular disease, acute or chronic infection of the respiratory tract, and pregnant or lactating females. One individual was not able to complete the entire dosing regimen and therefore was excluded from the data analysis.

 Following a complete physical exam, the subjects were randomized into two groups: those to initially receive prototype formulation 1 and those
15 to receive prototype formulation 2. Baseline exhaled particle production was measured after a two minute “wash out” period on the device. The assessment was made over a two minute period with the per-minute count derived from the average of the two minutes. Following the baseline measurement, the prototype formulation was administered over a six minute
20 period using a commercial aqueous nebulizer (Pari Respiratory Equipment, Starnberg, Germany). Formulation 1 consisted of an isotonic saline solution. Formulation 2 consisted of a combination of phospholipids suspended in an isotonic saline vehicle. Following administration, exhaled particle counts were assessed 5 minutes, 30 minutes, one hour, two hours, and three hours
25 after the single administration.

 As shown in Figure 4A, substantial inter-subject variability was found in baseline particle counts. The data shown are measurements made prior to administration of one of the test aerosols. This baseline expired particle result points to the existence of “super producers” of exhaled
30 aerosols. In this study “super-producers” were defined as subjects exhaling more than 1,000 particles/liter at baseline measurement. Figure 4B shows the individual particle counts for subjects receiving Formulation 1. The data

indicate that a simple formulation of exogenously applied aerosol can suppress exhaled particle counts.

Figure 5A shows the effect of prototype formulation 1 on the two “super-producers” found at baseline in this group. These data indicate that
5 the prototype formulation may exert a more pronounced effect on super-producers.

Similar results were found on delivery of formulation 2. Figure 5B summarizes the percent change (versus baseline) of the cumulative exhaled particle counts for the “super-producers” identified in the two treatment
10 groups.

Results from this study demonstrate that exhaled particles can be accurately measured using a laser-detection system, that these particles are predominantly less than 1 micron in diameter, and that the number of these particles varies substantially from subject to subject. “Super-producing”
15 subjects respond most markedly to delivery of an aerosol that modifies the physical properties of the surface of the lining fluid of the lungs. Such super-producers might bear significant responsibility for pathogen shedding and transmission in a population of infected patients. These data also demonstrate that suppressing aerosol exhalation is practical with relatively
20 simple and safe exogenously administered aerosol formulations.

Example 3: Large Animal Study

Seven (7) Holstein bull calves were anesthetized, intubated, and screened for baseline particle exhalation by optical laser counting. Animals were subsequently untreated (sham) or treated with a nebulized aerosol of
25 saline at one of three doses (1.8 minutes, 6.0 minutes or 12.0 minutes). During the sham dosage, the animals were handled in the same manner as they were when the dosages of the isotonic saline solution were administered. One animal was dosed per day and nebulizer doses were randomized throughout the exposure period (see Table 3 for dosing
30 schedule). Each animal was slated to receive all doses during the duration of the study. Following the administration of each dose, exhaled particle counts

were monitored at discrete timepoints (0, 15, 30, 45, 60, 90, 120) through 180 minutes.

The exposure matrix for the animals included in the study is found in Table 3. The dosing occurred over a 57 day period, with at least a 7 day
5 interval between dosages. Each animal (n=7) received each dose at least once during the duration of dosing, with the exception of the omission of one 6.0 minute dose (see animal no. 1736) and one 12.0 minute dose (see animal no. 1735). These two were excluded due to unexpected problems with the ventilator and/or anesthesia equipment.

10

Table 3: Dosing Regime for Large Animals

Dosage				
Animal No.	Sham	1.8 min.	6.0 min.	12.0 min.
1731	Day 17	Day 3	Day 10	Day 25
1732	Day 7	Day 21	Day 1	Day 14
1735	Day 18	Day 11	Day 4	N/A
1736	Day 23	Day 2	N/A	Day 9
1738	Day 8	Day 15	Day 36	Day 25
1739	Day 20	Day 38	Day 30	Day 45
1741	Day 50	Day 35	Day 57	Day42

Results

Figure 6A show the particle count over time for each animal after it received a sham dosage. Each timepoint typically represents the mean of at least three particle count determinations. The data in Figure 6A shows that
15 certain individual animals inherently produce more particles than others (“superspreaders”). Additionally, the data show that throughout the assessment period, quiescently breathing anesthetized animals maintain a relatively stable exhaled particle output (see e.g. Animal nos. 1731, 1735, 1738, 1739, and 1741).

20

Figure 6B represents the mean percent change in exhaled particle counts over time following each treatment. Each data point represents the mean of six to seven measurements from the treatment group. All animals had returned to baseline by 180 minutes post treatment. The data suggest

that the 6.0 minute treatment period provides an adequate dose to prevent the exhalation of particles for at least 150 minutes post-treatment. The other treatments appear to be either too short or too long to provide an effective, lasting suppression of aerosol exhalation.

5 **Example 4: Reduction of Exhaled Aerosol Particles in Human Study**

In a study of 4 healthy adults, particle counts were measured using a device similar to that illustrated in Figure 2 prior and subsequent to treatment with a formulation for reducing the number of exhaled particles. Treatment involved a six minute inhalation from a Pari LC+ jet nebulizer of a
10 formulation containing 1.29% CaCl₂ by weight in 0.9% NaCl solution. Exhaled particles were measured prior to treatment and at timepoints 10 minutes, 1, 2, 4, and 6 hours after treatment completion. Total count rate of particles greater than 0.3µm in diameter during a 3 minute test immediately following a 2 minute washout of ambient particles from the lungs was
15 measured using a device similar to that illustrated in figure 2. The device contained a Climet CI-500B optical particle counter. This device accurately measured particles in the range of 300-2500 nm. A series of filters eliminated all background particle noise.

Figure 7 shows the effect of the inhaled treatment on the count rate of
20 particles greater than 0.3µm particles produced. The mean count rate was seen to decrease from the baseline count rate prior to treatment for all timepoints up to 6 hours after treatment.

Example 5: Characterization of Exhaled Aerosol Particles in Human Study

25 In two separate studies, particle size distribution and number of particles produced during tidal breathing were measured in 580 adults and in 97 children using a measurement system similar to that illustrated in Figure 2.

For both studies, the measurement system included a Fleisch
30 pneumotachometer (model no. 1, Phipps and Bird, Richmond VA) for measuring the patient flow rate during the test and an optical particle counter (Climet Model CI-500B, Climet Instruments Company, Redlands, CA) for

measuring particle counts and size distribution over the range of 0.3-25 μm . Following a 2 minute washout period of breathing particle free air, the particle count rate was measured during a 3 minute test interval.

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5 Similar to the smaller study from Example 2, large intersubject variability was seen in the number of particles exhaled for both of the studies. In the adult study, 26% of the population was classified as "super producers", producing greater than 10,000 particles per minute and accounting for 94% of the particles measured in the study. The number of counts per minute ranged over nearly 5 orders of magnitude.

10 In the study of exhaled particle production in children, 12% of the population was classified as "super producers" by the same criteria and accounted for 86% of the total particles produced. Particle counts per minute again ranged over nearly 5 orders of magnitude.

15 The reference in this specification to any prior publication (or information derived from it), or to any matter which is known, is not, and should not be taken as, an acknowledgement or admission or any form of suggestion that prior publication (or information derived from it) or known matter forms part of the common general knowledge in the field of endeavour to which this specification relates.

20 Throughout this specification and the claims which follow, unless the context requires otherwise, the word "comprise", and variations such as "comprises" or "comprising", will be understood to imply the inclusion of a stated integer or step or group of integers or steps but not the exclusion of any other integer or step or group of integers or steps.

The claims defining the present invention are as follows:

1. A diagnostic device for measuring particle exhalation in an individual, including
a mouthpiece,
5 a two-way filter,
a branched connector,
a low resistance one-way valve,
a particle counter,
a gas flow meter, and
10 a computer,
wherein the outlet of the mouthpiece is connected to the filter and to the one-way
valve via the branched connector,
wherein the gas flow meter is exposed to the ambient environment at one end and
connected to the filter at the other end,
15 wherein the particle counter is coupled to the one-way valve,
wherein the particle counter operates at a steady sample gas rate; and
wherein the particle counter is connected to the computer in a manner that allows
data from the particle counter to be sent to the computer.
- 20 2. The device of claim 1, wherein the filter is capable of removing particles having a
size greater than or equal to 0.1 microns in diameter.
3. The device of claim 1, wherein the mouthpiece is selected from the group
consisting of mouthpieces that are designed for a user to place his lips around the
25 mouthpiece, nasal prongs, masks that are capable of covering a user's mouth and nose, and
masks that are capable of covering a user's nose.
4. The device of claim 1, wherein the filter is a combination of two or more filters.
- 30 5. The device of claim 1, wherein the mouthpiece, filter, tube, and one-way valve are
disposable.

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6. The device of claim 1, wherein the particle counter is selected from the group consisting of electrical mobility particle counters, impaction particle counters, electrostatic impaction particle counters, infrared spectroscopy particle counters, laser diffraction
5 particle counters, and light scattering particle counters.

7. The device of claim 1, wherein the particle counter is an optical particle counter.

8. The device of claim 1, wherein the particle counter is connected to the computer in
10 a manner that allows control commands to be sent from the computer to the particle counter.

9. The device of claim 1, wherein the computer is a microprocessor internal or external to the particle counter.
15

10. The device of claim 1, wherein the gas flow meter is a Fleisch-type pneumotachometer or a Lilly-type pneumotachometer.

11. The device of claim 1, wherein the gas flow meter operates by measuring the
20 differential pressure across or the bypass flow rate through a bypass around a laminar flow element.

12. The device of claim 1, further including a differential pressure transducer, wherein the differential pressure transducer is capable of measuring the pressure drop across the
25 flow meter, and a signal conditioner, wherein the signal conditioner is connected to the differential pressure transducer and is capable of amplifying the signal and sending the signal to the computer.

13. A method for using a diagnostic device to measure the rate and size of particle
30 exhalation in an individual, wherein the device includes
a mouthpiece,

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- 5 a two-way filter,
a branched connector,
a low resistance one-way valve,
a particle counter,
a gas flow meter, and
a computer,
wherein the outlet of the mouthpiece is connected to the filter and to the one-way
valve via the branched connector,
wherein the gas flow meter is exposed to the ambient environment at one end and
10 connected to the filter at the other end,
wherein the particle counter is coupled to the one-way valve,
wherein the particle counter operates at a steady sample gas rate, and
wherein the particle counter is connected to the computer, including
(i) placing the mouthpiece in or over the individual's mouth or nose,
15 (ii) inhaling through air through the mouthpiece, wherein the air is pulled
through the filter prior to inhalation,
(iii) exhaling through the mouthpiece and into the one-way valve,
(iv) measuring the number of particles and size of particles using the
particle counter, and
20 (v) providing the data from the particle counter to the computer.

14. The method of claim 13, wherein the device further includes a differential pressure
transducer, wherein the differential pressure transducer is capable of measuring the
pressure drop across the flow meter, and a signal conditioner, wherein the signal
25 conditioner is connected to the differential pressure transducer and is capable of
amplifying the signal and sending the signal to the computer.

15. The method of claim 13, wherein during step (ii) the air is pulled through the gas
flow meter prior to being pulled through the filter.
30

16. The method of claim 14, further including prior to step (iii), providing data from

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the signal conditioner to the computer.

17. The method of claim 13, wherein steps (ii) - (v) are repeated multiple times.

5 18. The method of claim 17, further including (vi) calculating the mean particle size, the average particle distribution, and mean rate of particle production.

19. The method of claim 18, further including (vii) inhaling a formulation that when administered to the mucosal lining of a human or other animal alters the surface
10 viscoelastic properties of the mucosal lining, surface tension of the mucosal lining, or bulk viscosity of the mucosal lining, and then repeating steps (i) - (vi).

20. The method of claim 19, wherein the formulation includes a charged compound.

15 21. The method of claim 20, wherein the charged compound is selected from the group consisting of salts, ionic surfactants, charged amino acids, charged proteins or peptides, and combinations thereof.

22. The method of claim 19, wherein the formulation is an aqueous, non-surfactant
20 formulation.

23. The method of claim 19, wherein the formulation is in the form of an aerosol.

24. The method of claim 23, wherein the formulation is saline.

25

25. The method of any one of claims 13 to 24, wherein steps (i) - (v) occur prior to entering a clean room.

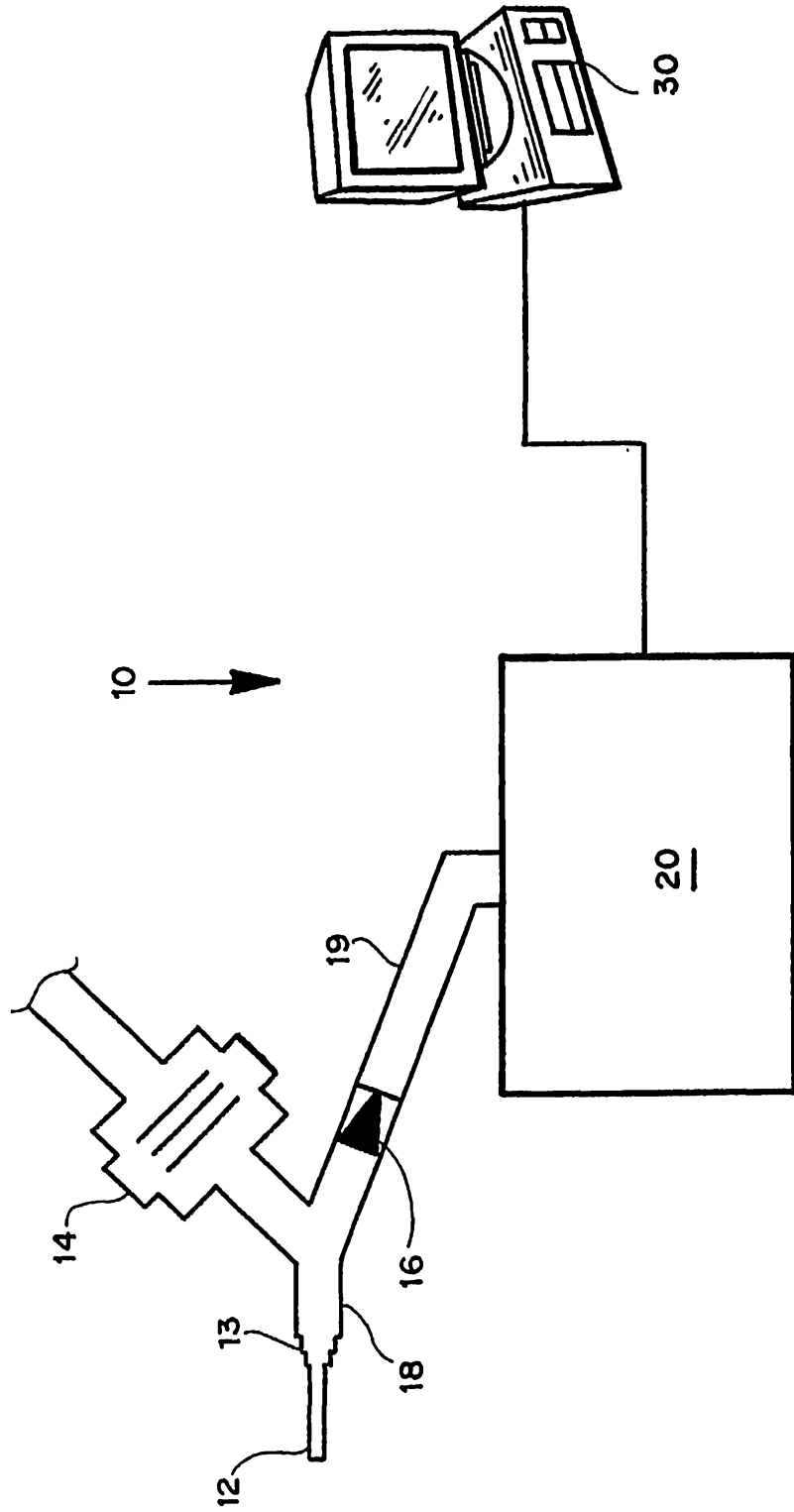
26. The method of any one of claims 13 to 24, wherein prior to step (i), the user enters
30 a cleanroom.

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27. A diagnostic device for measuring particle exhalation in an individual, substantially as herein described with reference to the accompanying drawings.
28. A method for using a diagnostic device to measure the rate and size of particle
5 exhalation in an individual, substantially as herein described.

FIG. 1



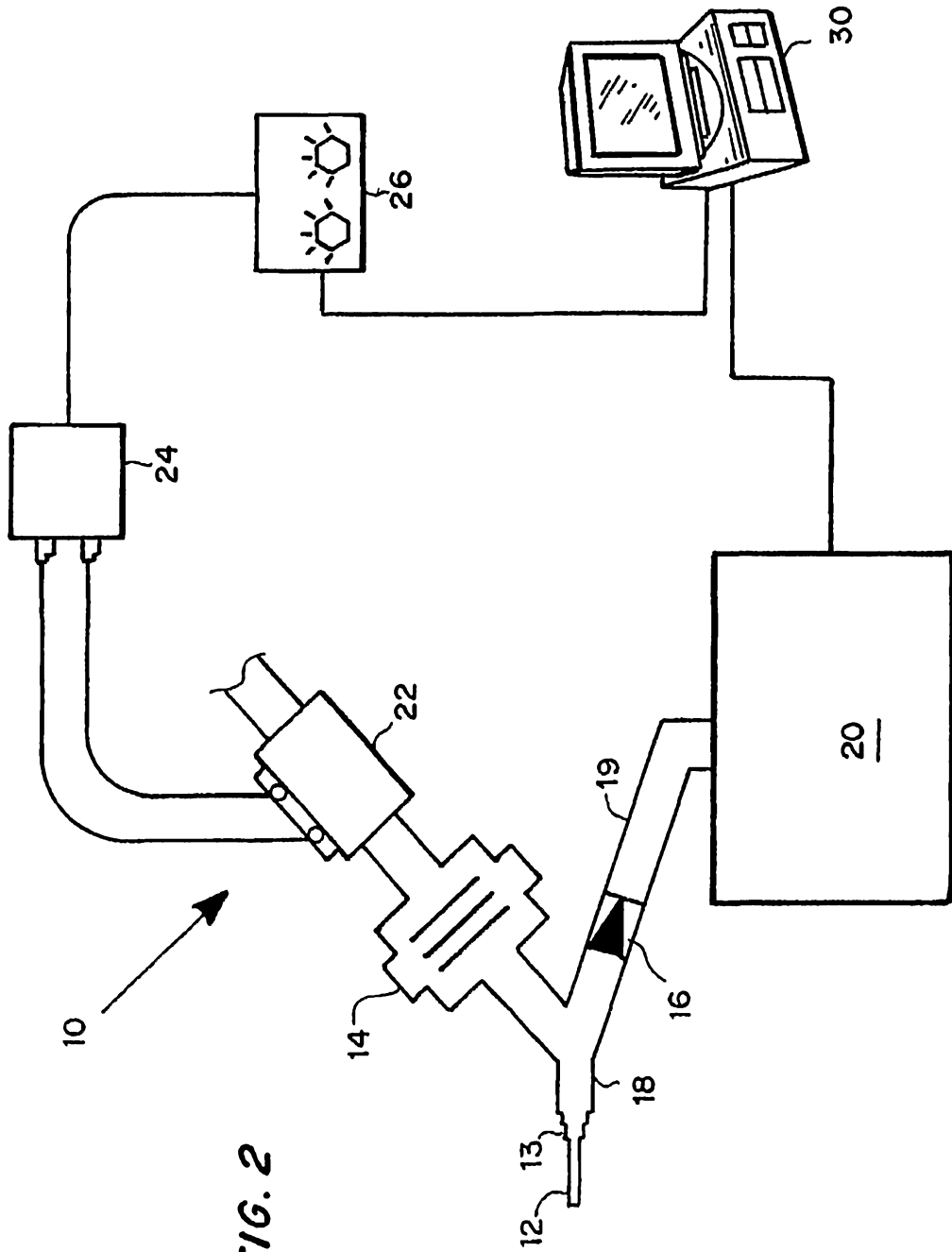
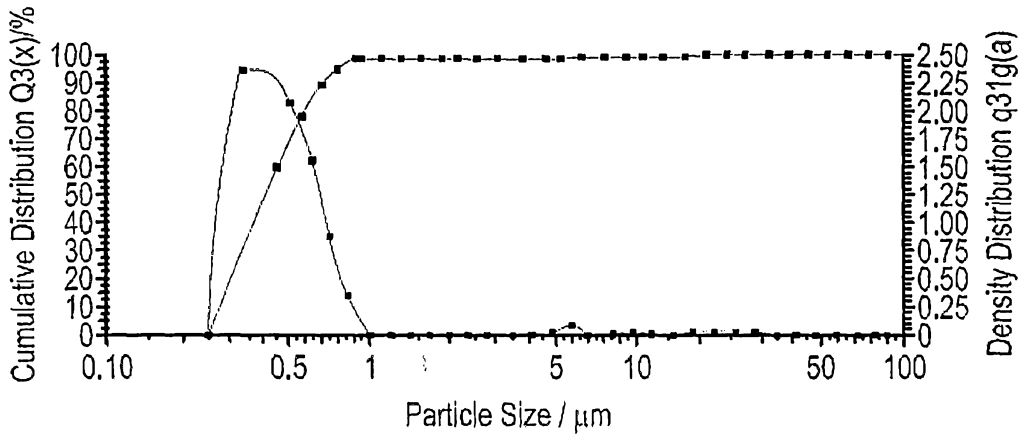


FIG. 2

FIG. 3A

Cough Distribution at 0 Minutes

$x_{10} = 0.28 \mu\text{m}$ $x_{20} = 0.42 \mu\text{m}$ $x_{30} = 0.66 \mu\text{m}$



Cough Distribution at 0 Minutes (Post Dose)

$x_{10} = 0.51 \mu\text{m}$ $x_{20} = 1.00 \mu\text{m}$ $x_{30} = 1.67 \mu\text{m}$

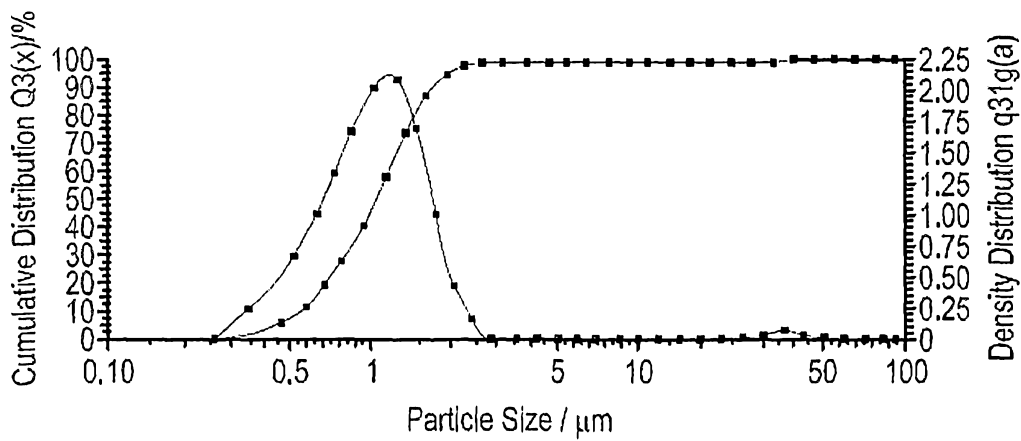
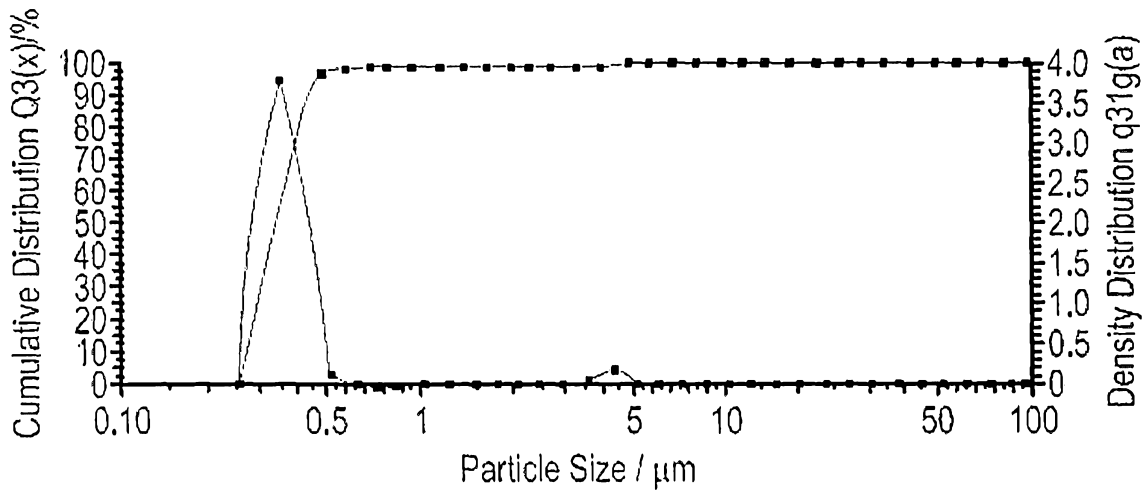


FIG. 3B

Cough Distribution at 30 Minutes

$x_{10} = 0.27 \mu\text{m}$ $x_{20} = 0.35 \mu\text{m}$ $x_{30} = 0.44 \mu\text{m}$



Cough Distribution at 30 Minutes (Post Dose)

$x_{10} = 47.89 \mu\text{m}$ $x_{20} = 61.94 \mu\text{m}$ $x_{30} = 71.19 \mu\text{m}$

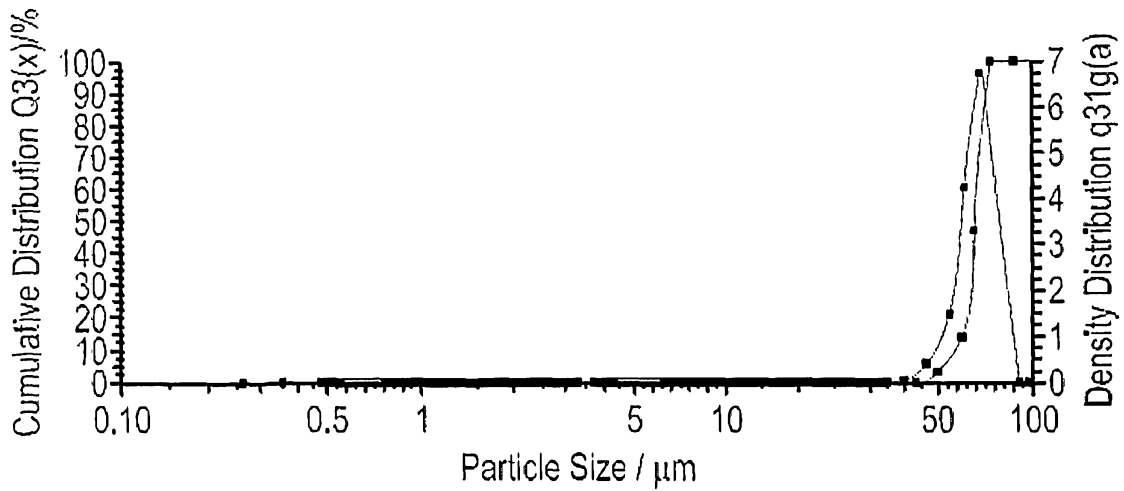
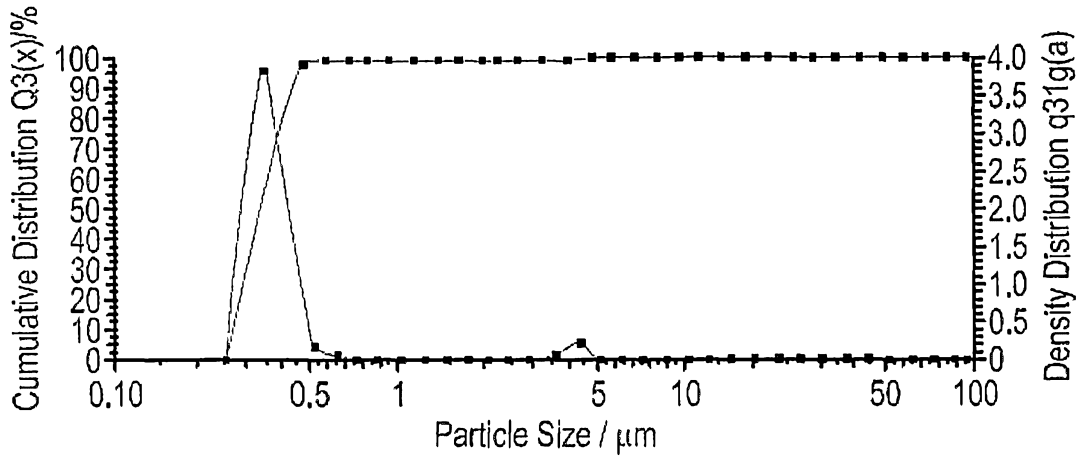


FIG. 3C

Cough Distribution at 60 Minutes

$x_{10} = 0.27 \mu\text{m}$ $x_{20} = 0.35 \mu\text{m}$ $x_{30} = 0.44 \mu\text{m}$



Cough Distribution at 60 Minutes (Post Dose)

$x_{10} = 25.58 \mu\text{m}$ $x_{20} = 31.71 \mu\text{m}$ $x_{30} = 36.90 \mu\text{m}$

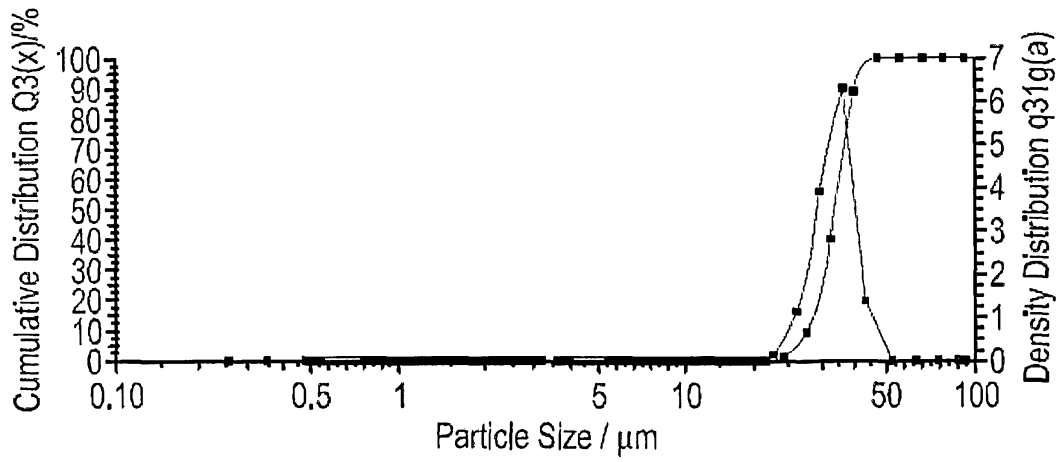


FIG. 4A

Baseline Particle Counts by Subject Pre-Dosing with Prototype Formulation 2

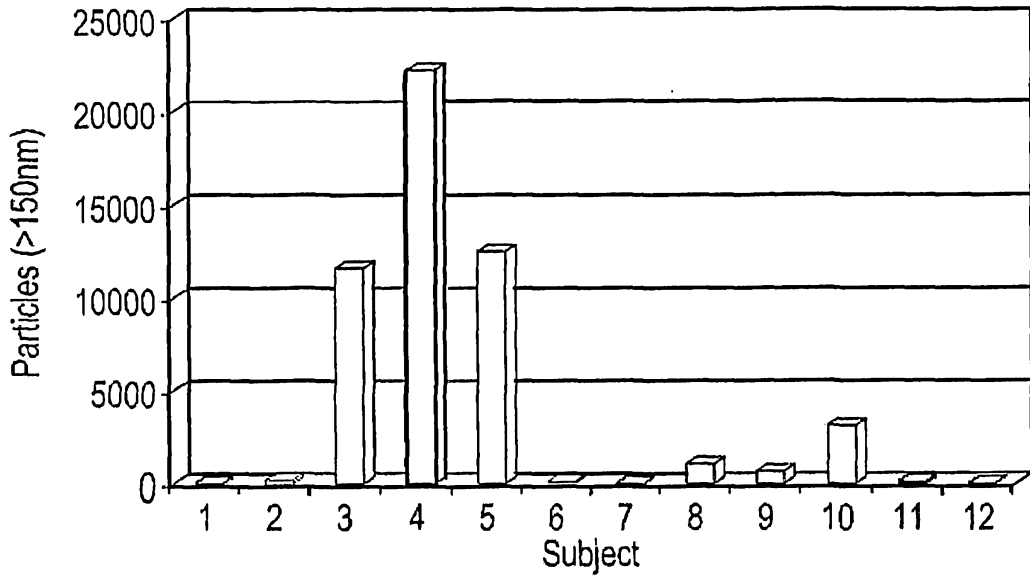


FIG. 4B

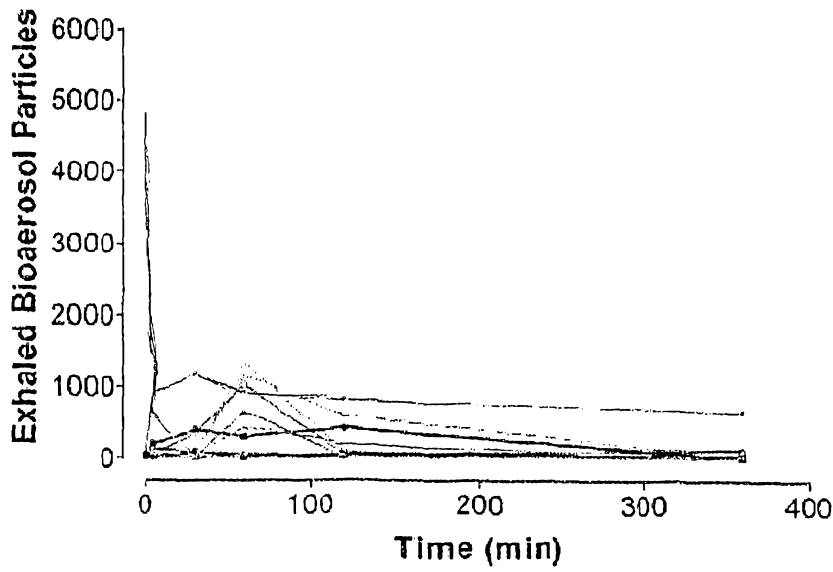


FIG. 5A

Patients w/Baseline >1,000 Particles/Liter
n=2

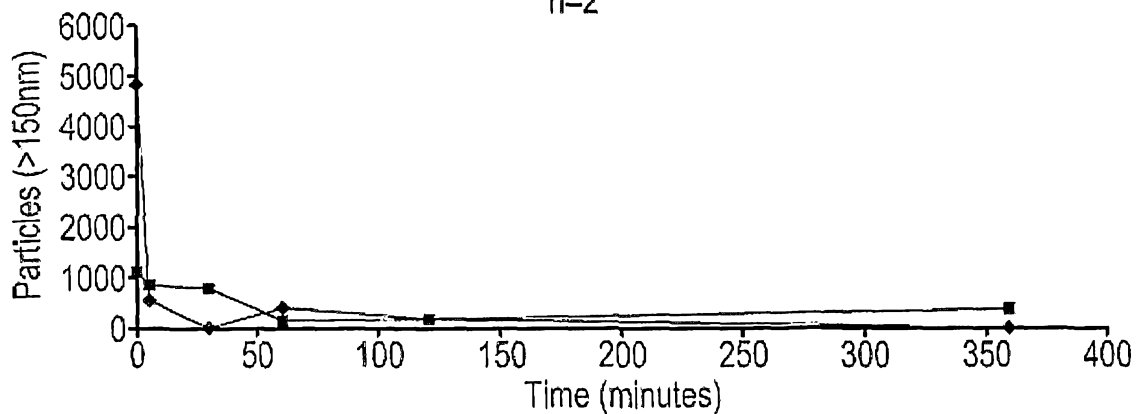


FIG. 5B

Patients w/Baseline >1,000 Particles/Liter
Formulation 1 (n=2); Formulation 2 (n=5)

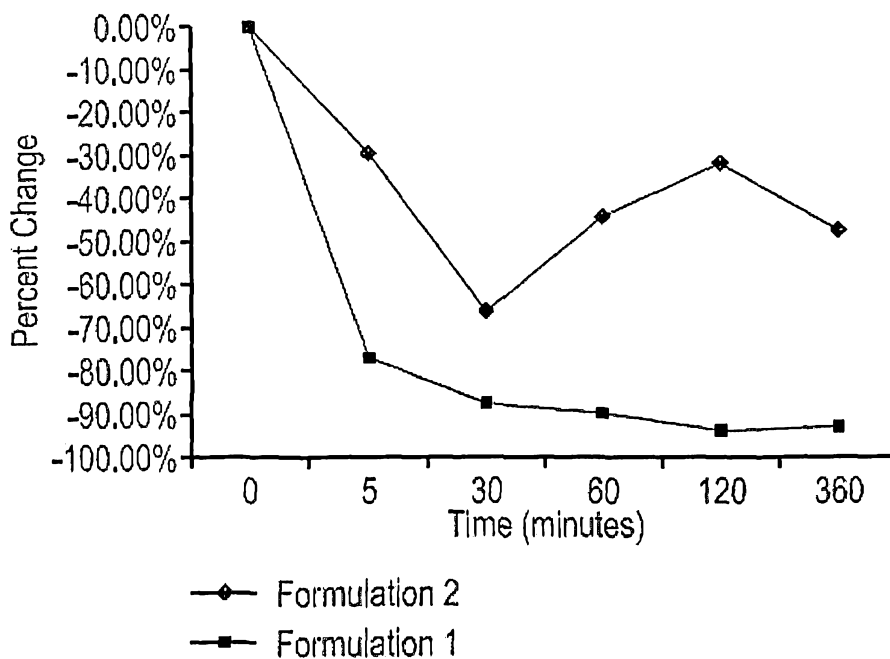


FIG. 6A

Sham Exposure Particle Counts (N=7)

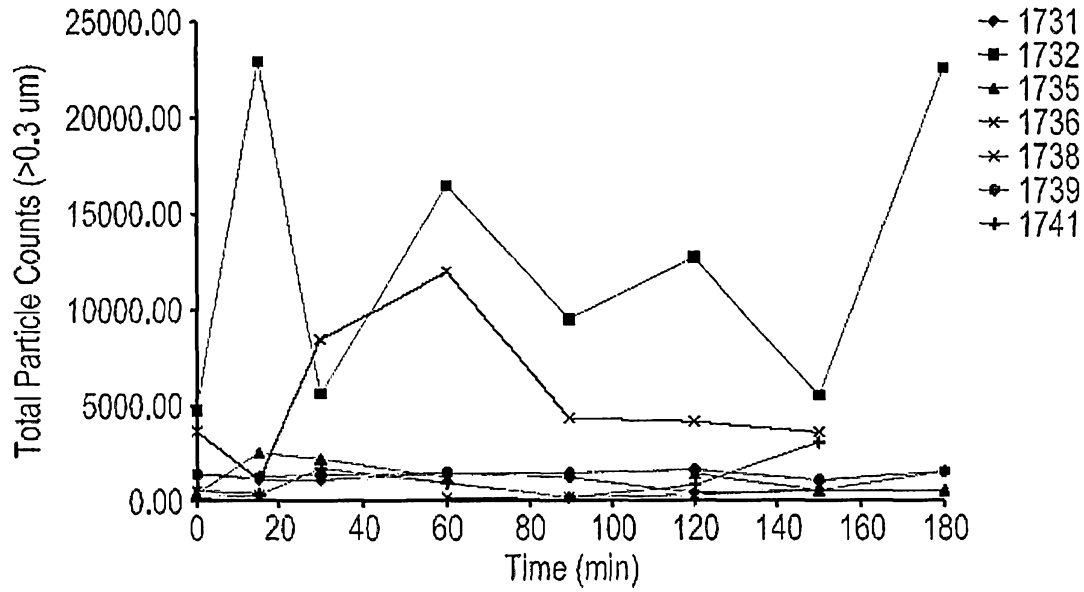
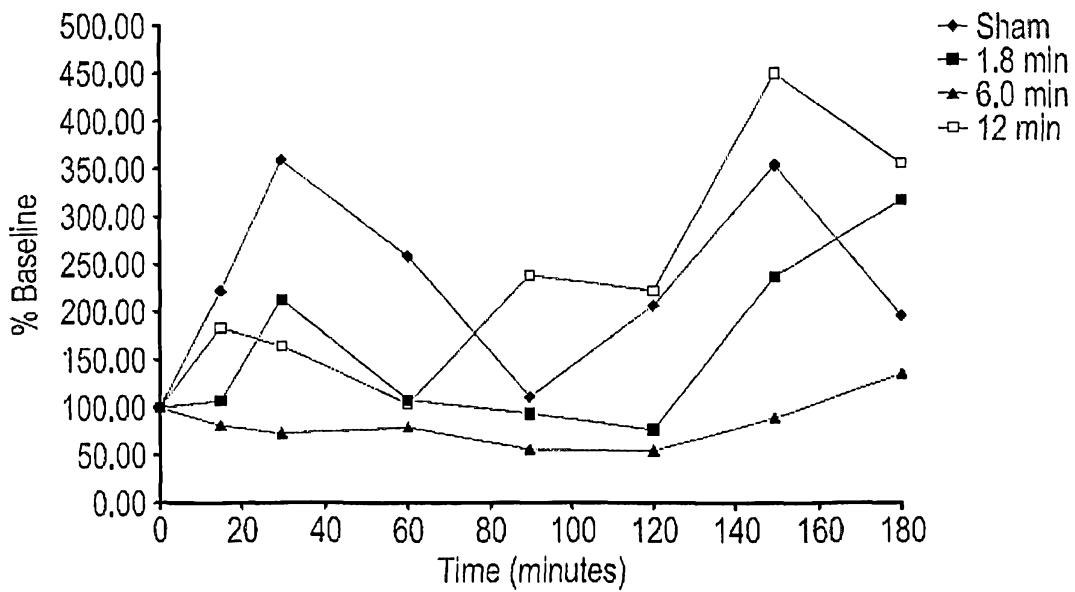


FIG. 6B

% Baseline Dose Data (n=6,7)



Effect of CaCl₂ administration on production of particles >0.3 μm, n=4, Tidal Breathing

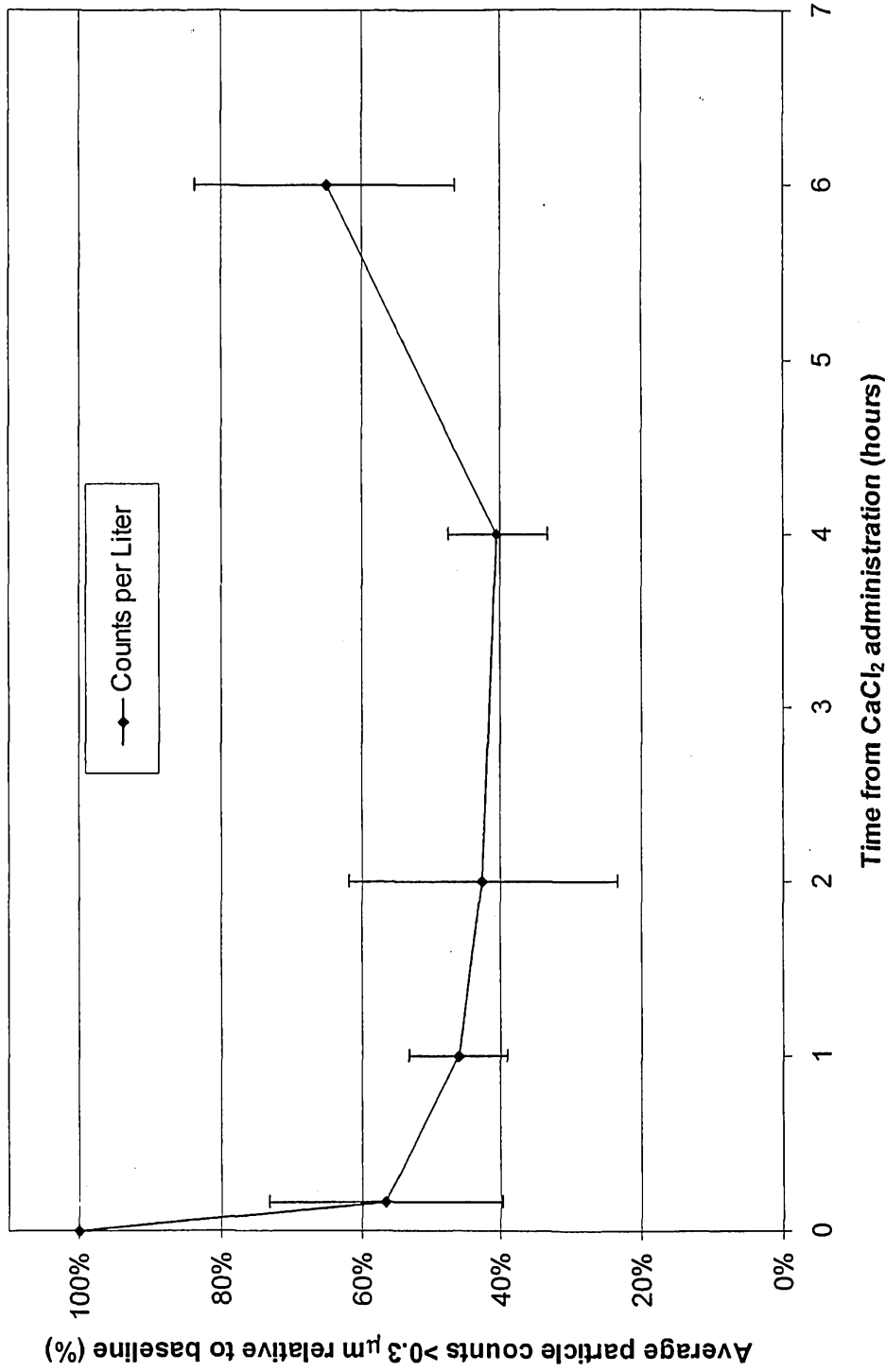


Figure 7