

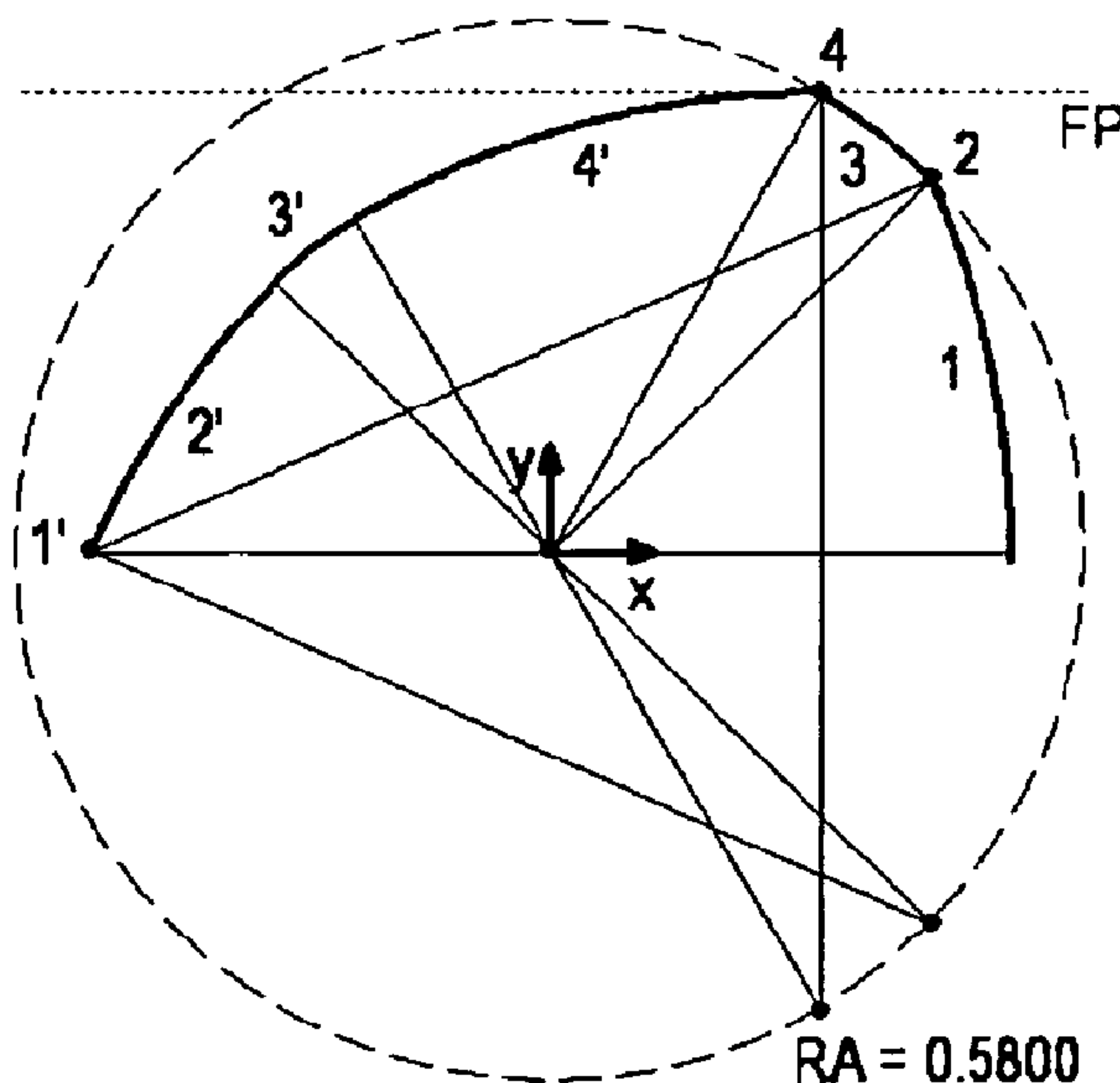


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(54) Titre : PROCEDE POUR LA CONSTRUCTION DE CORPS COROTATIFS ENTRANT EN CONTACT LES UNS
AVEC LES AUTRES, PROGICIEL POUR LA MISE EN OEUVRE DE CE PROCEDE ET ELEMENTS DE VIS SANS
FIN AINSI REALI SES

(54) Title: METHOD FOR CONSTRUCTING CO-ROTATING CONTIGUOUS BODIES AND COMPUTER PROGRAM
PRODUCT FOR CARRYING OUT SAID METHOD AND SCREW ELEMENTS PRODUCED ACCORDINGLY



Figur 17d

1)	$R = 0.9999$	$M_x = -0.4998$
	$\alpha = 0.4187$	$M_y = 0.0000$
2)	$R = 0.0000$	$M_x = 0.4137$
	$\alpha = 0.3580$	$M_y = 0.4065$
3)	$R = 0.5800$	$M_x = 0.0000$
	$\alpha = 0.2627$	$M_y = 0.0000$
4)	$R = 0.0000$	$M_x = 0.2939$
	$\alpha = 0.5315$	$M_y = 0.5000$
4')	$R = 1.0000$	$M_x = 0.2939$
	$\alpha = 0.5315$	$M_y = -0.5000$
3')	$R = 0.4200$	$M_x = 0.0000$
	$\alpha = 0.2627$	$M_y = 0.0000$
2')	$R = 1.0000$	$M_x = 0.4137$
	$\alpha = 0.3580$	$M_y = -0.4065$
1')	$R = 0.0001$	$M_x = -0.4998$
	$\alpha = 0.4187$	$M_y = 0.0000$

(57) Abrégé/Abstract:

The invention relates to a method for producing closely intermeshing, self-cleaning, co-rotating screw profiles, to the use of screw profiles in screw and transition elements, to novel screw profiles that are produced by the method and to a computer program product for carrying out the method on a computer system.

Abstract

The present invention relates to a method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles, the use of the screw profiles in screw and transition elements,
5 novel screw profiles which have been generated by the method and a computer program product for executing the method in a computer system.

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METHOD FOR CONSTRUCTING CO-ROTATING CONTIGUOUS BODIES AND COMPUTER PROGRAM PRODUCT FOR CARRYING OUT SAID METHOD AND SCREW ELEMENTS PRODUCED ACCORDINGLY

The present invention relates to a method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles, a computer program product for carrying out the method in a computer system, novel screw profiles generated by the method and the use of the screw profiles obtained in screw and transition elements.

Those skilled in the art are familiar with co-rotating twin- and multiscrew extruders from the patent and technical literature. The following publication [1] can be mentioned as an example: K. Kohlgrüber: "*Der gleichläufige Doppelschneckenextruder*", ("The co-rotating twin-screw extruder"), Publishers: Hanser Verlag, 2007. This publication explains in detail the design, function and operation of twin- and multiscrew extruders. An entire chapter (pages 227 - 248) is devoted to the subject of screw elements and their mode of action. A detailed explanation is provided of the design and the function of conveying, kneading and mixing elements. In order to provide a transition between screw elements with different numbers of flights (or screw channels), washers are frequently used as spacers. In special cases, so-called transition elements are used which provide a continuous transition between two screw profiles with different numbers of flights, a self-cleaning pair of screw profiles being present at each transition point. When mentioned and described in the following, the terms screw elements and screw profiles are also understood to include transition elements and their profiles. The profiles of the transition elements are also referred to as transition profiles.

As is well-known to those skilled in the art and as is explained, for example, on pages 96 to 98 of [1], the known self-cleaning Erdmenger screw profile is clearly defined by the following three parameters: the number of flights z ¹⁾, the outer screw radius ra and the centre distance a . The number of flights z is an integer greater than or equal to 1. An additional important parameter of screw profiles is their inner radius ri . Another important parameter of screw profiles is their flight depth h .

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1) For the sake of clarity, in the description all abbreviations, symbols and indices used are written in italics and in the figures all abbreviations, symbols and indices used are written in normal script.

As is well-known to those skilled in the art and as is explained, for example, on pages 96 to 98 of [1], the known self-cleaning Erdmenger screw profile consists of arcs of circles. The size of an arc is defined by its central angle and its radius. In the following, the "central angle of an arc" is abbreviated to the "angle of an arc". The position of an arc is defined by the position of its central point and that of its starting or end point. The position of the starting point and the end point of an arc is, however, not predefined, since an arc can begin or end either in a clockwise or an anti-clockwise direction. The starting and end points are therefore interchangeable.

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The methods so far known for producing tightly intermeshing, self-cleaning, co-rotating screw profiles have the disadvantage that they are mathematically complicated and always associated with specific screw profiles, such as, for example, the Erdmenger screw profile. Known processes for producing Erdmenger screw profiles are described for example in [1] or in the publication by Booy [2]: *"Geometry of fully wiped twin-screw equipment"*, Polymer Engineering and Science 18 (1978) 12, pages 973 – 984. In the aforementioned publications screw profiles are generated by making use of the kinematic peculiarity that the same sense rotation (= co-rotation) of two screws about their stationary axes is kinematically identical to the "movement without rotation" of one screw about another, in this case stationary, screw. This phenomenon can be used for the stepwise generation of screw profiles. The first screw (the "generated" screw) remains stationary using such a method and the second screw (the "generating" screw) is moved translationally around the first screw on an arc. It is then possible to predefine part of the profile in the second screw and examine which profile is thereby generated in the first screw. The generated screw is "carved" by the generating screw. [1] does not, however, describe how the predefined part of the second screw is actually to be generated. [2] describes a possible method of generating the starting profile section from which the remaining profile is generated. This method is, however, mathematically very complicated and above all not universally applicable, i.e. it is not possible to generate any desired type of profile for screw and transition elements using this method.

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Based on the prior art, the problem therefore arises of providing a method for generating screw profiles in which screw profiles can be generated without any predefined existing

profiles and/or profile sections. The problem also arises of providing a method of generating any desired profiles for tightly intermeshing screw and transition elements. The problem also arises of providing a simple method of generating profiles for tightly intermeshing screw and transition elements. This method must be capable of being carried
5 out by the mere use of a pair of compasses and an angle ruler without the need for complicated computations.

Surprisingly it has been found that the above problem can be solved by a method in which the profiles of screw elements can be formed completely of arcs which merge tangentially
10 into each other, it being possible for an arc also to have a radius of zero.

The present invention therefore relates to a method of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with a selectable centre distance a between the rotating axes of a generating and a generated screw profile, characterized in
15 that the generating screw profile consists of n arcs and the generated screw profile consists of n' arcs.

The method according to the invention is not limited to screw elements with a modular design of the type commonly used today with a screw consisting of screw elements and
20 central shafts, but can also be used for screws designed in one piece. Screw elements therefore also refer to screws designed as integrated wholes.

The method according to the invention provides its user with certain degrees of freedom, which are characterized in that specific parameters can be freely selected. Certain
25 requirements do, however, have to be fulfilled for obtaining valid screw profiles. Thus certain parameters have to have a specific value or have to lie within a certain range of values. Valid screw profiles are understood to be screw profiles which have the required properties, i.e. which are planar, tightly intermeshing, self-cleaning and rotate in the same direction. Such screw profiles can be used for producing screw and transition elements in
30 multiscrew extruders.

The method V0 according to the invention is characterized in that

- the generating screw profile and the generated screw profile lie in the same plane,

- the axis of rotation of the generating screw profile and the axis of rotation of the generated screw profile each lie vertically on said plane of the screw profiles, the point of intersection between the rotational axis of the generating screw profile and said plane being referred to as the point of rotation of the generating screw profile and the point of intersection between the rotational axis of the generated screw profile and said plane being referred to as the point of rotation of the generated screw profile,
- the number of arcs n of the generating screw profile is selected such that n is an integer greater or equal to 1,
- the outer radius ra of the generating screw profile is selected such that ra is greater than 0 ($ra > 0$) and smaller than or equal to the distance between the axes (the centre distance) ($ra \leq a$),
- the inner radius ri of the generating screw profile is selected such that ri is greater than or equal to 0 ($ri \geq 0$) and smaller than or equal to ra ($ri \leq ra$),
- the arcs of the generating screw profile are arranged clockwise or anti-clockwise about the rotational axis of the generating screw profile in such a manner according to the following configuration rules that:
 - o all of the arcs of the generating screw profile merge into each other tangentially such that a closed, convex screw profile is obtained, wherein an arc whose radius is 0 is treated as an arc whose radius is eps , which is a very small positive real number which tends towards 0 ($eps < 1$, $eps \rightarrow 0$),
 - o each of the arcs of the generating screw profile is located within and/or on the boundaries of an annulus which has an outer radius ra and an inner radius ri and whose centre point lies on the point of rotation of the generating screw profile,
 - o at least one of the arcs of the generating screw profile touches the outer radius ra of the generating screw profile,
 - o at least one of the arcs of the generating screw profile touches the inner radius ri of the generating screw profile,
- the size of a first arc of the generating screw profile which is defined by an angle α_1 and a radius r_1 is selected such that angle α_1 is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π , wherein π is understood to be pi ($\pi \approx 3.14159$), and radius r_1 is greater than or equal to 0 and

- smaller than or equal to the centre distance a , and the position of this first arc of the generating screw profile, which is obtained by positioning two different points of this first arc, is defined according to the above configuration rules, wherein the first point of this first arc to be positioned is preferably the starting point of this first arc and wherein the second point of this first arc to be positioned is preferably the centre point of this first arc,
- the sizes of additional $n-2$ arcs of the generating screw profile, which are defined by angles $\alpha_2, \dots, \alpha_{(n-1)}$ and radii $r_2, \dots, r_{(n-1)}$ are selected such that angles $\alpha_2, \dots, \alpha_{(n-1)}$ are, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π and radii $r_2, \dots, r_{(n-1)}$ are greater than or equal to 0 and smaller than or equal to the centre distance a and the positions of these additional $n-2$ arcs of the generating screw profile are defined according to the above configuration rules,
 - the size of the last arc of the generating screw profile, which is defined by angle α_n and radius r_n , is such that the sum of the n angles of the n arcs of the generating screw profile is, in terms of radian measurement, 2π , wherein angle α_n is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π , and radius r_n completes the generating screw profile, wherein radius r_n is greater than or equal to 0 and smaller than or equal to the centre distance a and the position of this last arc of the generating screw profile is defined according to the above configuration rules,
 - the n' arcs of the generated screw profile are based on the n arcs of the generating screw profile such that
 - the number of arcs n' of the generated screw profile is identical to the number of arcs n of the generating screw profile, wherein n' is an integer,
 - the outer radius ra' of the generated screw profile is equal to the centre distance minus the inner radius ri of the generating screw profile ($ra' = a - ri$),
 - the inner radius ri' of the generated screw profile is equal to the centre distance minus the outer radius ra of the generating screw profile ($ri' = a - ra$),
 - angle α_i' of the i' th arc of the generated screw profile is the same as angle α_i of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and

i' is an index which represents all integers in the range from 1 to the number of arcs n' ($\alpha_{1'} = \alpha_1, \dots, \alpha_{n'} = \alpha_n$),

- the sum of radius $r_{i'}$ of the i' th arc of the generated screw profile and radius r_i of the i th arc of the generating screw profile is equal to the centre distance a , wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($r_{1'} + r_1 = a, \dots, r_{n'} + r_n = a$),
- the distance between the centre point of the i' th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is the same as the centre distance a and the distance between the centre point of the i' th arc of the generated screw profile and the point of rotation of the generated screw profile is the same as the distance between the centre point of the i th arc of the generating screw profile and the point of rotation of the generating screw profile, and the connecting line between the centre point of the i' th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is a line parallel to the connecting line between the point of rotation of the generated screw profile and the point of rotation of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ,
- the starting point of the i' th arc of the generated screw profile lies in an opposite direction, in relation to the centre point of the i' th arc of the generated screw profile, to that of the starting point of the i th arc of the generating screw profile, in relation to the centre point of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' .

The method V0 according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles produces the following features in the generated screw profile:

- the generated screw profile is closed,
- the generated screw profile is convex,
- each of the arcs of the generated screw profile merges tangentially into the next arc of the generated screw profile, wherein an arc with a radius of 0 is treated as an arc with a radius of eps , which is a very small positive real number which tends towards 0 ($eps \ll 1$, $eps \rightarrow 0$),
- each of the arcs of the generated screw profile is located within and/or on the boundaries of an annulus which has an outer radius ra' and an inner radius ri' and whose centre point is located on the point of rotation of the generated screw profile,
- at least one of the arcs of the generated screw profile touches the outer radius ra' of the generated screw profile,
- at least one of the arcs of the generated screw profile touches the inner radius ri' of the generated screw profile.

15 A further result of the method V0 of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles is that only if the inner radius ri of the generating screw profile equals the centre distance a minus the outer radius ra of the generating screw profile ($ri = a - ra$) the outer radius ra' of the generated screw profile is equal to the outer radius ra of the generating screw profile and the inner radius ri' of the generated screw profile is equal to
20 the inner radius ri of the generating screw profile.

If the generating screw profile has an arc with a radius $r_i = 0$, the screw profile has, at the point of this arc, a bend whose size is characterized by an angle α_i . If the generated screw profile has an arc with a radius $r_i' = 0$, the screw profile has, at the point of this arc, a bend
25 whose size is characterized by an angle α_i' .

The method V0 of generating planar, tightly intermeshing, co-rotating screw profiles is also characterized in that it can be carried out merely by using an angle ruler and a pair of compasses. Thus the tangential transition between the i th and the $(i+1)$ th arc of the
30 generating screw profile is constructed by forming a circle with a radius r_{i+1} around the end point of the i th arc and that point of intersection between this circle and a straight line through the centre point and the end point of the i th arc which is located nearer the point of rotation of the generating screw profile is the centre point of the $(i+1)$ th arc. In practice,

instead of an angle ruler and a pair of compasses, a computer program is used for constructing these screw profiles.

The method V0 according to the invention can be used for generating screw profiles which
5 are independent from a number of flights z .

The generated screw profile can be different from the generating screw profile. As is readily understandable to anyone of ordinary skill in the art, this method V0 is particularly suitable for generating transition elements between screw elements having different
10 numbers of flights. Based on a screw profile with z flights it is possible to change the generating and the generated screw profile gradually in such a manner that finally a screw profile with a number of flights z' which is not equal to z is obtained. It is possible to reduce or increase the number of arcs during this transition.

15 Typical screw profiles used in practice are characterized in that the generating and the generated screw profiles are identical for an odd number of flights and, for an even number of flights, the generated screw profile is identically superimposable on the generating screw profile after the generating or generated screw profile has rotated through an angle π/z . Such screw profiles known according to the prior art and having z flights are characterized
20 in that they have precisely z planes of symmetry which are vertical to the plane of the generating screw profile and pass through the axis of rotation of the generating screw profile. The same applies to the generated screw profile. The screw profiles each consist of $2z$ sections which have a section angle of π/z based on the respective point of rotation of the corresponding screw profile and can be made to coincide with each other by rotation or
25 mirroring about their planes of symmetry. Such screw profiles are referred to as symmetrical. In a special embodiment of the method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles – hereinafter referred to as VA1 – a flight number z applies, which subdivides the screw profiles into $2z$ sections. Using the special embodiment VA1 of the method according to
30 the invention it is however possible to generate not only symmetrical screw profiles in which the $2z$ sections can be made to coincide with each other by rotation and/or mirroring about their planes of symmetry but also asymmetrical screw profiles.

This special embodiment VA1 of the method according to the invention is characterized in that:

- the number of flights z is selected such that z is an integer greater than or equal to 1,
- 5 - the number of arcs n of the generating screw profile is selected such that it is an integer multiple p of $4z$,
- the generating screw profile is subdivided into $2z$ sections, which are characterized in that
 - each section is bounded by two straight lines which form an angle to each other, in terms of radian measurement, of π/z and which intersect each other at the point of rotation of the generating screw profile, wherein these two straight lines are referred to as section boundaries, wherein π is pi ($\pi \approx 3.14159$),
 - each of these $2z$ sections is subdivided into a first and a second part,
 - 15 ○ the first part of a section is composed of p arcs which are numbered in ascending or descending order,
 - the angles $\alpha_1, \dots, \alpha_p$ belonging to the p arcs are selected such that the sum of these angles is $\pi/(2z)$, wherein angles $\alpha_1, \dots, \alpha_p$ are, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to
 - 20 $\pi/(2z)$,
 - the second part of a section is composed of p' arcs, which are numbered in reverse order to the arcs of the first part of a section, wherein p' is an integer which is the same as p ,
 - angles $\alpha_{p'}, \dots, \alpha_{1'}$ of the p' arcs are defined such that the angle $\alpha_{j'}$ of the
 - 25 j' th arc of the second part of a section is the same as the angle α_j of the j th arc of the first part of a section, wherein j is an index which represents all integers in the range from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p' ($\alpha_{1'} = \alpha_1, \dots, \alpha_{p'} = \alpha_p$),
 - 30 ○ the sum of the radius $r_{j'}$ of the j' th arc of the second part of a section and the radius r_j of the j th arc of the first part of a section is equal to the centre distance a , wherein j is an index which represents all integers in the

range from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p' ($r_{1'} + r_1 = a, \dots, r_{p'} + r_p = a$),

- the centre point and the starting point of the arc with which the screw profile begins in the first part of a section are positioned on one of the section boundaries of this section, the selected section boundary depending on whether the arcs are arranged in a clockwise or an anticlockwise direction,
- the end point of the arc with which the screw profile ends in the first part of a section touches a straight line FP at one point, the straight line FP being vertical to the angle bisector of the two boundary limits of this section and at such a distance from the point of rotation of the generating screw profile in the direction of this section which is equal to half the centre distance, the angle bisector passing, in the same way as the section boundaries, through the point of rotation of the generating screw profile.

The method VA1 of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights produces a generated screw profile in which each of the sections of the generated screw profile is designed such that the radii of the arcs of the generated screw profile are, in reverse order, the same as the radii of the arcs of the generating screw profile.

Screw profiles which are generated according to the above method VA1 consist of $2z$ sections which can be different from each other. If the sections are different from each other, asymmetrical screw profiles are obtained.

In the case of axially symmetrical screw profiles all $2z$ sections can be identically superimposed by being rotated and/or by being mirrored about the section boundaries. The section boundaries are then located on the lines of intersection between the planes of symmetry of the respective profile and the plane in which the profile lies. A special embodiment VA2 of the method according to the invention exists for generating planar, axially symmetrical, tightly intermeshing, self-cleaning, co-rotating screw profiles with z

flights. This special embodiment VA2 of the method according to the invention is characterized in that

- only a first section of the generating screw profile is predefined and
- the remaining sections are generated by successive mirroring about the section boundaries.

Using the method according to the invention it is also possible to generate screw profiles which are dot-symmetrical about the point of rotation (VA3). In this case the profile of one section is predefined, whereas the section on the opposite side of the profile is obtained by dot mirroring of the predefined section about the point of rotation. In this manner dot-symmetrical screw profiles can be generated section by section, although the abovementioned configuration rules must be followed in order to obtain a closed, convex profile.

All the abovementioned methods are characterized in that they can be carried out merely by using an angle ruler and a pair of compasses. Thus the tangential transition between the j th and the $(j+1)$ th arc of the first part of a section of the generating screw profile is constructed by forming a circle with a radius $r_{(j+1)}$ around the end point of the j th arc and that point of intersection of this circle with a straight line through the centre point and the end point of the j th arc which is located nearer the point of rotation of the generating screw profile is the centre point of the $(j+1)$ th arc. In addition, where the arcs are numbered in ascending order, the p th arc of the first part of a section of the generating screw profile is constructed in such a manner that a tangent is placed on the $(p-1)$ th arc at the end point of the $(p-1)$ th arc, the point of intersection of the tangent with the straight line FP being the centre point of a circle whose radius is equal to the length of the distance between the end point of the $(p-1)$ th arc and the point of intersection of the tangent with the straight line FP , and the point of intersection of the circle with the straight line FP , which is located in the direction of the selected clock direction, is the required point of contact between the end point of the p th arc and the straight line FP . In practice, instead of an angle ruler and a pair of compasses, a computer program is used for constructing the screw profiles.

As is readily understandable to a person of ordinary skill in the art from the information provided, the methods described are particularly suitable for generating transition elements

between screw elements with an identical number of flights. Based on a screw profile with z flights it is possible to obtain a different z -flight screw profile, by gradually changing the screw profile in the transition. It is permissible to decrease or increase the number of arcs during the transition.

5

In practice a screw profile is appropriately placed in a coordinate system in order to be able to define it distinctly and in an appropriate form for further use by specifying the coordinates of characteristic parameters. It is recommendable to use dimensionless parameters (written in capital letters in the following, e.g. RA , A , RI etc.) in order to
10 simplify the process of applying the method to different extruder sizes. The centre distance a is a useful reference value for geometrical dimensions such as, for example, lengths or radii, since this value cannot be changed in an extruder. The dimensionless centre distance is $A=a/a=1$. The dimensionless outer screw radius of a screw profile is $RA=ra/a$. The dimensionless inner radius of a screw profile is $RI=ri/a$. The dimensionless flight depth of
15 a screw profile is $H=h/a=RA-RI$.

It is appropriate to position the point of rotation of a generating screw profile at the origin of a Cartesian coordinate system ($x=0$, $y=0$) and to position the point of rotation of the generated screw profile at point $x=A=1$, $y=0$.

20

One concrete embodiment VK1 of the method according to the invention is obtained by using dimensionless parameters and a Cartesian coordinate system where the point of rotation of the generating screw profile lies at the origin ($x=0$, $y=0$) and the point of rotation of the generated screw profile lies at the coordinate point $x=A=1$, $y=0$. This concrete
25 embodiment VK1 is characterized as follows:

- the generating screw profile is formed from 1, 2, ..., $(i-1)$, i , $(i+1)$, ..., $(n-1)$, n arcs which are arranged in a clockwise or anticlockwise manner, wherein n is an integer greater than or equal to 1 and i is an integer which is greater than or equal to 1 and smaller than or equal to n ,
- 30 - the outer radius RA is selected to be greater than 0 ($RA>0$) and smaller than or equal to the centre distance ($RA\leq 1$),

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- the inner radius RI is selected to be greater than or equal to 0 ($RI \geq 0$) and smaller than or equal to RA ($RI \leq RA$),
- the sum of the angles $\alpha_1, \dots, \alpha_n$ of arcs 1, ..., n of the generating screw profile is 2π , wherein π is pi ($\pi \approx 3.14159$),
- 5 - the radii $R_1, \dots, R_n$ of arcs 1, ..., n of the generating screw profile are greater than or equal to 0 and smaller than or equal to 1,
- the starting and centre points of a first arc of the generating screw profile are positioned on the x -axis, the starting point being positioned in the region from $x=RI$ to $x=RA$ and the x -coordinate of the centre point being smaller than or equal to the x -coordinate of the starting point,
- 10 - where $i < n$, the end point of the i th arc of the generating screw profile is at the same time the starting point of the $(i+1)$ th arc of the generating screw profile,
- where $i = n$, the end point of the i th arc of the generating screw profile is at the same time the starting point of the first arc of the generating screw profile,
- 15 - each arc of the generating screw profile merges tangentially into the next arc, wherein an arc with $R_i = 0$ is treated in the same way as an arc with $R_i = \epsilon$, wherein ϵ is a very small positive real number which tends towards 0 ($\epsilon \ll 1, \epsilon \rightarrow 0$),
- 20 - at no point of the generating screw profile is the distance from the point of rotation greater than the outer radius RA ,
- at at least one point of the generating screw profile the distance from the point of rotation is equal to the outer radius RA ,
- 25 - at no point of the generating profile is the distance from the point of rotation smaller than the inner radius RI ,
- at at least one point of the generating screw profile the distance from the point of rotation is equal to the inner radius RI ,
- the generating screw profile is convex,

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- the generated screw profile consists of $1', 2', \dots, (i-1)', i', (i+1)', \dots, (n-1)', n'$ arcs which are arranged in the same clock direction as the arcs of the generating screw profile, wherein the number of arcs n' of the generated screw profile is equal to the number of arcs n of the generating screw profile and wherein i' is an integer which is greater than or equal to 1 and smaller than or equal to n' ,
- the angle $\alpha_{i'}$ of the i' 'th arc of the generated screw profile is the same as the angle α_i of the i 'th arc of the generating screw profile,
- the sum of the radius $R_{i'}$ of the i' 'th arc of the generated screw profile and the radius R_i of the i 'th arc of the generating screw profile is 1,
- the starting point of the first arc of the generated screw profile is at the same time the starting point of the first arc of the generating screw profile and the centre point of the first arc of the generated screw profile is located on the x -axis, the x -coordinate of the centre point being greater than or equal to the x -coordinate of the starting point,
- where $i' < n'$, the end point of the i' 'th arc of the generated screw profile is at the same time the starting point of the $(i+1)'$ 'th arc of the generated screw profile,
- where $i' = n'$, the end point of the i' 'th arc of the generated screw profile is at the same time the starting point of the $1'$ 'th arc of the generated screw profile,
- each of the arcs of the generated screw profile merges tangentially into the next arc, wherein an arc with $R_{i'} = 0$ is treated in the same way as an arc with $R_{i'} = \text{eps}$, wherein eps is a very small positive real number which tends towards 0 ($\text{eps} \ll 1, \text{eps} \rightarrow 0$) and
- the generated screw profile is convex.

Some screw profiles generated using this concrete embodiment VK1 have a special feature: They contain adjacent profile-generating arcs which have the same radius and the same centre point and which can be united to form an arc with a larger angle (see for example Figures 62a and 62b and the corresponding description of these figures).

One concrete embodiment VK2 of the method according to the invention for screw profiles with z flights is characterized in that

- the flight number z is selected such that z is an integer greater than or equal to 1,
- 5 - the number of arcs n of the generating screw profile is selected such that it is an integer multiple p of $4z$,
- the generating screw profile, preferably beginning with the first arc of the generating screw profile, is divided into $2z$ parts which are characterized in that each of these $2z$ parts of the generating screw profile is composed of $1, \dots, j, \dots,$
10 $p, p', \dots, j', \dots, 1'$ arcs, wherein p' is an integer which is the same as p , and wherein j and j' are to be understood to be integers which are greater than or equal to 1 and smaller than or equal to p or p' ,
- the angles $\beta_1, \dots, \beta_p$ of arcs $1, \dots, p$ of the first part of the generating screw profile are selected such that their sum is equal to $\pi/(2z)$, wherein π is pi ($\pi \approx$
15 3.14159),
- the angle $\beta_{j'}$ of the j' th arc of the first part of the generating screw profile is the same as the angle β_j of the j th arc of the first part of the generating screw profile ($\beta_{1'} = \beta_1, \dots, \beta_{p'} = \beta_p$),
- the radii $R_1, \dots, R_p$ of arcs $1, \dots, p$ of the first part of the generating screw profile are selected such that they are greater than or equal to 0 and smaller than
20 or equal to 1,
- the sum of the radius $R_{j'}$ of the j' th arc of the first part of the generating screw profile and the radius R_j of the j th arc of the first part of the generating screw profile is 1 ($R_{1'} + R_1 = 1, \dots, R_{p'} + R_p = 1$),
- 25 - the starting and centre points of the first arc of the first part of the generating screw profile are positioned on the x -axis, the starting point being positioned in the region from $x=RI$ to $x=RA$ and the x -coordinate of the centre point being smaller than or equal to x -coordinate of the starting point,
- the arcs are arranged in a counter-clockwise direction,
- 30 - the end point of the p th arc of the first part of the generating screw profile touches a straight line FP at one point, wherein the straight line FP is at a

distance from the point of rotation which corresponds to half the centre distance and has a slope which is 0 where $z=1$ and $-1/\tan(\pi/(2z))$ where $z>1$,

- in the case of axially symmetrical screw profiles, the remaining parts of the generating screw profile are characterized in that
 - the angles of the arcs of the first part of the generating screw profile are reproduced in the same order when forming the angles of the arcs of the remaining parts of the generating screw profile,
 - the radii of the arcs of the first part of the generating screw profile are reproduced in reverse order when forming the radii of the arcs of the second part of the generating screw profile,
 - the radii of the arcs of the first and the second part of the generating screw profile are reproduced in the same order when forming the radii of the arcs of the remaining parts of the generating screw profile,
- in the case of dot-symmetrical screw profiles, the remaining parts of the generating screw profile are characterized in that
 - a second part is generated opposite the first part by dot mirroring about the point of rotation,
 - the remaining parts of the generating screw profile are generated analogously to the method used for the first part of the generating screw profile and their opposing parts are generated by dot mirroring about the point of rotation,
- in the case of asymmetrical screw profiles, the remaining parts of the generating screw profile are generated independently of each other and analogously to the method used for the first part of the generating screw profile.

Some screw profiles generated using this concrete embodiment VK2 have a special feature: They contain adjacent profile-generating arcs which have the same radius and the same centre point and which can be united to form an arc with a larger angle (see for example Figures 62a and 62b and the corresponding description of these figures).

The present invention also relates to profiles for screw and transition elements which have been produced by means of the method according to the invention. Surprisingly, completely new types of profiles for screw and transition elements have been obtained by

the method according to the invention. Profiles according to the invention for screw and transition elements are specified in more detail in the examples.

The screw profiles which are obtained by the method according to the invention for
5 generating tightly intermeshing, self-cleaning, co-rotating screw profiles can be used in screw and transition elements. In particular, such screw profiles can be used in conveying, kneading and mixing elements. The present invention thus also relates to conveying, kneading and mixing elements with a profile according to the invention or a profile which has been generated by the method according to the invention, as well as to methods for
10 their production.

As is known (see, for example pages 227 - 248 of [1]), a conveying element is characterized in that the screw profile continuously rotates and progresses in an axial direction in a screw-like fashion. The conveying element can be right- or left-handed. The
15 pitch of the conveying element, i.e. the axial length required for the complete rotation of the screw profile, is preferably in the range from 0.1 to 10 times the centre distance and the axial length of a conveying element is preferably in the range from 0.1 to 10 times the centre distance.

20 As is known (see, for example pages 227 - 248 of [1]), a kneading element is characterized in that the screw profile progresses stepwise in an axial direction in the form of kneading discs. The kneading discs can be arranged in a right-handed, left-handed or neutral fashion. The axial length of the kneading discs is preferably in the range from 0.05 to 10 times the centre distance. The axial distance between two adjacent kneading discs is
25 preferably in the range from 0.002 to 0.1 times the centre distance.

As is known (see, for example, pages 227 - 248 of [1]), mixing elements are formed by designing conveying elements with openings in the screw tips. The mixing elements can be right-handed or left-handed. Their pitch is preferably in the range from 0.1 to 10 times
30 the centre distance and the axial length of the elements is preferably in the range from 0.1 to 10 times the centre distance. The openings are preferably designed in the form of a u- or v-shaped groove and they are preferably arranged either in a back-conveying manner or parallel to the axis.

Transition elements can be right- or left-handed. Their pitch is preferably in the range from 0.1 to 10 times the centre distance and their axial length is preferably in the range from 0.1 to 10 times the centre distance.

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The present invention also relates to a co-rotating multi-screw extruder with at least one screw element whose profile has been generated by the method according to the invention, wherein the multiscrew extruder has two or more screws.

- 10 The present invention also relates to a computer program product for carrying out the method for generating tightly intermeshing, self-cleaning, co-rotating screw profiles in a computer system.

The execution of the method according to the invention in a computer system is
15 advantageous since the coordinates and the dimensions of the profiles are in such a form that they can be processed further by a computer. In particular, flow simulation processes are simple to carry out in a computer. The profile generated by the method according to the invention is developed further in an axial direction in order to generate a three-dimensional computer model of a screw or transition element. A model of a conveying element is for
20 example generated in such a manner that the profile is rotated in a screw-like fashion in an axial direction. A model of a kneading element is for example generated by continuing to develop the profile in an axial direction section by section, the sections being staggered in relation to each other, thus resulting in staggered discs. A so-called computational grid is used for modelling a screw or transition element in a computer. Such a grid consisting of
25 polyhedrons, such as for example tetrahedrons or hexahedrons, is applied to the volume between the inner surface of the barrel and the surfaces of a screw or transition element. The computational grid, the physical properties of the viscous fluid and the operating conditions of the screw machine in which the screw elements and the viscous fluid are used are entered into a flow simulation program and the flow conditions are calculated. Then
30 the computed flow fields are analyzed for determining, inter alia, the quality of the screw profile with regard to its characteristic properties such as, for example, the mixing behaviour or the power consumption in relation to the physical properties and the operating conditions used.

The computer program product according to the invention is characterized in that the method according to the invention is stored in the form of program codes on a data carrier. The data carrier is computer-readable to enable the method according to the invention to be carried out using a computer when the computer program product is executed in a computer. A suitable data carrier is, for example, a disc, an optical data carrier such as for example a CD, DVD, or Blu-ray disc, a hard disc, a flash memory or a memory stick, etc. Preferably the computer program product, if executed in a computer, has a graphical user interface (GUI) which provides users with a simple means of entering the freely selectable parameters for generating screw profiles with the aid of input devices such as, for example a mouse and/or a keyboard. In addition, the computer program product preferably has a graphical output, by means of which the computed screw profiles can be visualized in a graphical output device, such as for example a screen and/or printer. Preferably the computer program product allows computed screw profiles to be exported, i.e. in the form of storable data sets, which include the geometrical dimensions of the computed screws, or, for further types of use, to be stored on a data carrier or to be transferred to a connected device. In particular, the computer program product is designed in such a manner that, when executed in a computer, it can compute not only screw profiles but also screw and transition elements generated from the screw profiles and can deliver the computed geometries in a format that can be used by a machine for producing screw and transition elements, for example by a milling machine for producing actual screw elements. Such formats are known to those of ordinary skill in the art.

The present invention allows the generation of screw profiles, screw elements and transition elements *ab initio*. In contrast to the prior art, the method according to the invention is not based on existing screw profiles but allows the generation of any desired profiles by selecting the values for characteristic parameters such as for example the centre distance and the number of arcs for developing the required screw profiles and generating the screw profiles step by step by observing simple rules. The method according to the invention is simple to use and can also even be carried out using a pair of compasses and an angle ruler, without the need for complicated calculations. The method according to the invention is universally applicable, i.e. it is for example not restricted to a concrete number of flights, but it is even possible by varying the values concerned to generate profiles which

merge from one flight number into another. In addition, the invention allows the generation of symmetrical and asymmetrical screw profiles, screw elements and transition elements. It is also possible to generate screw profiles in which the generating and the generated profile are different, i.e. are not identically superimposable on each other.

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The invention is explained in more detail below with reference to the figures, without however being limited thereto. All of the figures were generated with the aid of a computer program.

- 10 It is recommendable to use dimensionless parameters in order to simplify the application of the method to varying extruder sizes. A useful reference value for geometrical dimensions, such as for example lengths or radii, is the centre distance a , since this value cannot be changed in an extruder. The dimensionless centre distance A is $a/a=1$. The dimensionless outer screw radius RA of a screw profile is ra/a . The dimensionless inner radius RI of a
- 15 screw profile is ri/a . The dimensionless flight depth H of a screw profile is $h/a=RA-RI$.

In the figures all of the geometrical values are used in their dimensionless form. All of the angles are stated in terms of radian measurement.

- 20 The method of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles is explained in more detail in relation to Figure 61, without the method being however limited to this figure.

- Figures 61a to 61f show the transition from a pair of two-flight screw profiles to a pair of
- 25 one-flight screw profiles. All of these figures have the same structure, which is described in detail in the following. The generating screw profile is depicted by the screw profile on the left. The generated screw profile is depicted by the screw profile on the right. Both screw profiles consist of 16 arcs. The arcs of the generating and the generated screw profile are characterized by thick, unbroken lines labelled with the respective numbers of
- 30 the arcs. Due to the plurality of arcs and the generation of the figures by means of a computer program it is possible for the numbers of individual arcs to overlap each other and therefore to be difficult to read - see, for example, arcs 3', 4' and arcs 5', 6' and 7' in Figure 61a. Despite the somewhat poor readability of individual numbers, the structure of

the profiles is nevertheless clear from the figures in combination with the present description.

The centre points of the arcs are depicted by small circles. The centre points of the arcs are connected by thin unbroken lines both to the starting point and to the end point of the
5 corresponding arc. The outer screw radius is almost identical in size both for the generating and the generated screw profile. In the region of the screw barrel, the outer screw radius is characterized by a thin, broken line, and, in the intermeshing zone, by a thin dotted line.

10 Figure 61a shows a pair of two-flight screw profiles at the start of the transition section. The generating and the generated screw profile are symmetrical to each other. Arcs 1 and 9 of the generating screw profile touch the outer screw radius over their entire length. Arcs 4, 5 and 12 and 13 of the generating screw profile touch the inner radius over their entire
15 length. Arcs 4', 5' and 12' and 13' of the generated screw profile touch the outer screw radius over their entire length. Arcs 1' and 9' of the generated screw profile touch the inner radius over their entire length.

Figure 61f shows a pair of one-flight screw profiles at the end of the transition section. The generating and the generated screw profile are symmetrical to each other. Arcs 1 and
20 12 of the generating screw profile touch the outer screw radius over their entire length. Arcs 4 and 9 of the generating screw profile touch the inner radius over their entire length. Arcs 4' and 9' of the generated screw profile touch the outer screw radius over their entire length. Arcs 1' and 12' of the generated screw profile touch the inner radius over their entire length.

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Figure 61b shows a pair of transition profiles in which the transition from the two-flight screw profiles to the one-flight screw profiles has been completed to an extent of 20%. Figure 61c shows a pair of transition profiles in which the transition has been completed to an extent of 40%. Figure 61d shows a pair of transition profiles in which the transition has
30 been completed to an extent of 60%. Figure 61e shows a pair of transition profiles in which the transition has been completed to an extent of 80%.

The transition takes place in such a manner that in all cases arc 1 of the generating screw profile touches the dimensionless outer screw radius RA over its entire length, as a result of which the corresponding arc 1' of the generated screw profile touches the dimensionless inner radius RI' over its entire length. The transition takes place in such a manner that in all cases arc 4' of the generated screw profile touches the dimensionless outer screw radius RA' , as a result of which the corresponding arc 4 of the generating screw profile touches the dimensionless inner radius RI . Since in all cases one arc of the generating and one arc of the generated screw profile rests on or touches the outer screw radius the wiping of the inner barrel surface is guaranteed during the entire transition. In addition, it is clear from Figures 61b to 61e that the generating and the generated screw profiles are asymmetrical. A pair of transition elements consists in all cases of a first transition element which is based on the generating transition profiles and a second transition element which is based on the generated transition profiles.

Figure 61 shows transition profiles in which the dimensionless outer screw radius of the generating screw profile and the dimensionless outer screw radius of the generated screw profile are in the range from $RA=RA'=0.6146$ to $RA=RA'=0.6288$. The method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles is not limited to this range of the dimensionless outer screw radius. Using the method according to the invention, screw profiles with a dimensionless outer screw radius of the generating screw profile of between RA greater than 0 and RA smaller than or equal to 1, and preferably in the range from $RA=0.52$ to $RA=0.707$, can be generated. Using the method according to the invention, screw profiles with a dimensionless outer screw radius of the generated screw profile between RA' greater than 0 and RA' smaller than or equal to 1, and preferably in the range from $RA'=0.52$ to $RA'=0.707$, can be generated.

The method according to the invention for generating planar, tightly intermeshing, self-cleaning and co-rotating screw profiles is explained in the following using the example of the pair of screw profiles in Figure 61d.

According to the invention, the generating and generated screw profiles are located in one plane. For the sake of simplicity this plane is placed in the xy plane of a Cartesian coordinate system. Also for the sake of simplicity the point of rotation of the generating

screw profile is placed at the origin of the Cartesian coordinate system ($x=0$, $y=0$). The dimensionless centre distance between the two points of rotation of the generating and the generated screw profile is $A=1$. For the sake of simplicity the point of rotation of the generated screw profile is placed at coordinate $x=A=1$, $y=0$.

5

According to the invention the number of arcs n of the generating screw profile is selected such that n is greater than or equal to 1. In the present example the number of arcs is selected to be $n=16$. According to the invention, the dimensionless outer screw radius RA of the generating screw profile is selected such that it is greater than 0 and smaller than or equal to the dimensionless centre distance A . In the present example the dimensionless outer screw radius of the generating screw profile is selected to be $RA=0.6203$. According to the invention, the dimensionless inner radius RI of the generating screw profile is selected such that it is greater than or equal to 0 and smaller than or equal to the dimensionless outer screw radius RA . In the present example the dimensionless inner radius of the generating screw profile is selected to be $RI=0.3798$.

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The arcs of the generating screw profile can be arranged in a clockwise or anticlockwise direction around the axis of rotation of the generating screw profile. In the present example the arcs are arranged anti-clockwise around the axis of rotation of the generating screw profile.

20

According to the invention, angle α_1 of arc 1 of the generating screw profile is selected such that it is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π . In the present example the angle of arc 1 is selected to be $\alpha_1=0.2744$. According to the invention, the dimensionless radius R_1 of arc 1 of the generating screw profile is selected such that it is greater than or equal to 0 and smaller than or equal to the dimensionless centre distance A . In the present example the dimensionless radius of arc 1 is selected to $R_1=RA=0.6203$. According to the invention, the position of arc 1 of the generating screw profile is selected such that arc 1 is located within and/or on the boundaries of an annulus having a dimensionless outer radius RA and a dimensionless inner radius RI , whose centre point is located on the point of rotation of the generating screw profile. The position of arc 1 is preferably predefined by the positions of the starting point and the centre point of arc 1. In the present example the starting point of arc 1 is

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placed at coordinate $x=RA=0.6203$, $y=0.0000$ and the centre point of arc 1 at coordinate $Mx_1=0.0000$, $My_1=0.0000$. Thus, arc 1 is located on the outer screw radius RA and the configuration rule that at least one arc touches the outer screw radius RA is fulfilled.

- 5 According to the invention, the angles $\alpha_2, \dots, \alpha_{(n-1)}$ of $n-2$ additional arcs, i.e. 14 additional arcs of the generating screw profile are selected such that they are, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π . In the present example, the angles of these 14 additional arcs are selected to be $\alpha_2=0.6330$, $\alpha_3=0.6330$, $\alpha_4=0.2208$, $\alpha_5=0.1864$, $\alpha_6=0.4003$, $\alpha_7=0.4003$, $\alpha_8=0.3934$,
 10 $\alpha_9=0.2744$, $\alpha_{10}=0.6330$, $\alpha_{11}=0.6330$, $\alpha_{12}=0.2208$, $\alpha_{13}=0.1864$, $\alpha_{14}=0.4143$ and $\alpha_{15}=0.4143$. According to the invention, the dimensionless radii $R_2, \dots, R_{(n-1)}$ of these 14 additional arcs of the generating screw profile are selected such that they are greater than or equal to 0 and smaller than or equal to the dimensionless centre distance A . In the present example the dimensionless radii of these additional 14 arcs are selected to be
 15 $R_2=0.0000$, $R_3=1.0000$, $R_4=0.3797$, $R_5=0.7485$, $R_6=0.4726$, $R_7=0.4726$, $R_8=0.1977$, $R_9=0.4827$, $R_{10}=0.6000$, $R_{11}=0.4000$, $R_{12}=0.5173$, $R_{13}=0.1485$, $R_{14}=0.8887$ and $R_{15}=0.8887$. According to the configuration rules the arcs are arranged in such a manner that they merge tangentially into each other in such a manner that a closed, convex screw profile is obtained, wherein an arc whose dimensionless radius is 0 is
 20 treated in the same way as an arc whose dimensionless radius is ϵ , which is a very small positive real number which tends towards 0 ($\epsilon \ll 1$, $\epsilon \rightarrow 0$). Based on this configuration rule the end point of an arc is at the same time the starting point of the next arc. The required tangential transition between a first arc and a second subsequent arc is such that the centre point of this second subsequent arc is positioned in such a manner on the straight
 25 line through the end point and the centre point of the first arc that the distance between the centre point of the second subsequent arc and the end point of the first arc is equal to the radius of the second subsequent arc and the screw profile is convex. An arc with a radius of 0 is treated in the same way as an arc with a very small radius ϵ , which tends towards 0, so that the tangential transition can continue to be constructed. Alternatively an arc with
 30 a radius of 0 can be treated in such a manner that the screw profile has a bend at the position of this arc, the size of the bend being determined by the angle of this arc. In the present example, the abovementioned configuration rule results in the following positions of the centre points of the 14 additional arcs: $Mx_2=0.5971$, $My_2=0.1681$, $Mx_3=-$

0.0187, $My_3=-0.6198$, $Mx_4=0.0001$, $My_4=0.0002$, $Mx_5=0.0699$, $My_5=-0.3619$,
 $Mx_6=-0.0316$, $My_6=-0.1054$, $Mx_7=-0.0316$, $My_7=-0.1054$, $Mx_8=-0.2855$,
 $My_8=0.0000$, $Mx_9=-0.0005$, $My_9=0.0000$, $Mx_{10}=0.1124$, $My_{10}=0.0318$, $Mx_{11}=-$
0.0107, $My_{11}=-0.1258$, $Mx_{12}=-0.0072$, $My_{12}=-0.0086$, $Mx_{13}=0.0626$, $My_{13}=-$
5 0.3707, $Mx_{14}=-0.2097$, $My_{14}=0.3176$ and $Mx_{15}=-0.2097$, $My_{15}=0.3176$. The end
point of arc 4 and the starting point of arc 5 are located on the dimensionless inner radius
 RI of the generating screw profile, thus fulfilling the configuration rule that at least one arc
touches the dimensionless inner radius RI .

10 According to the invention, angle α_{16} of the last arc of the generating screw profile is
such that the sum of the angles of the 16 arcs of the generating screw profile is, in terms of
radian measurement, 2π , wherein angle α_{16} is, in terms of radian measurement, greater
than or equal to 0 and smaller than or equal to 2π . In the present example, the angle of the
last arc α_{16} is 0.3654. According to the invention, the dimensionless radius R_{16} of the
15 last arc of the generating screw profile is such that this last arc closes the generating screw
profile. Since the end point of arc 15 is at the same time the starting point of the first arc,
the radius of arc 16, R_{16} , is 0.0000. The centre point of arc 16 is thus located at
coordinate $Mx_{16}=0.6203$, $My_{16}=0.0000$.

20 In the present example, the configuration rule that all arcs of the generating screw profile
are located within and/or on the boundaries of an annulus with a dimensionless outer radius
 RA and a dimensionless inner radius RI with a centre point at the point of rotation of the
generating screw profile is also fulfilled by the angles and radii selected for the 16 arcs and
their positions.

25

The generated screw profile is based on the generating screw profile. According to the
invention, the number of arcs n' of the generated screw profile is the same as the number of
arcs n of the generating screw profile. In the present example, the number of arcs of the
generated screw profile n' is 16. According to the invention, the dimensionless outer screw
30 radius RA' of the generated screw profile is equal to the dimensionless centre distance A
minus the dimensionless inner radius RI of the generating screw profile. In the present
example the dimensionless outer screw radius of the generated screw profile RA' is $A-$
 $RI=0.6202$. According to the invention, the dimensionless inner radius RI' of the generated

screw profile is equal to the dimensionless centre distance A minus the dimensionless outer screw radius RA of the generating screw profile. In the present example, the dimensionless inner radius R_I' of the generated screw profile is $A-RA=0.3797$.

- 5 According to the invention, the angle $\alpha_{i'}$ of the i' th arc of the generated screw profile is the same as the angle α_i of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' . In the present example, the angles of the 16 arcs of the generated screw profile are:
- 10 $\alpha_1'=\alpha_1=0.2744$, $\alpha_2'=\alpha_2=0.6330$, $\alpha_3'=\alpha_3=0.6330$, $\alpha_4'=\alpha_4=0.2208$,
 $\alpha_5'=\alpha_5=0.1864$, $\alpha_6'=\alpha_6=0.4003$, $\alpha_7'=\alpha_7=0.4003$, $\alpha_8'=\alpha_8=0.3934$,
 $\alpha_9'=\alpha_9=0.2744$, $\alpha_{10}'=\alpha_{10}=0.6330$, $\alpha_{11}'=\alpha_{11}=0.6330$, $\alpha_{12}'=\alpha_{12}=0.2208$,
 $\alpha_{13}'=\alpha_{13}=0.1864$, $\alpha_{14}'=\alpha_{14}=0.4143$, $\alpha_{15}'=\alpha_{15}=0.4143$ and $\alpha_{16}'=\alpha_{16}=0.3654$.
- 15 According to the invention, the sum of the dimensionless radius $R_{i'}$ of the i' th arc of the generated screw profile and the dimensionless radius R_i of the i th arc of the generating screw profile is equal to the dimensionless centre distance A , wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($R_1'+R_1=A=1$, ..., $R_{n'}'+R_n=A=1$). In the present example the radii of the 16 arcs of the generated screw profile are: $R_1'=A-R_1=1-0.6203=0.3797$, $R_2'=A-R_2=1-0.0000=1.0000$, $R_3'=A-$
 $R_3=1-1.0000=0.0000$, $R_4'=A-R_4=1-0.3797=0.6203$, $R_5'=A-R_5=1-0.7485=0.2515$,
 $R_6'=A-R_6=1-0.4726=0.5274$, $R_7'=A-R_7=1-0.4726=0.5274$, $R_8'=A-R_8=1-$
 $0.1977=0.8023$, $R_9'=A-R_9=1-0.4827=0.5173$, $R_{10}'=A-R_{10}=1-0.6000=0.4000$,
25 $R_{11}'=A-R_{11}=1-0.4000=0.6000$, $R_{12}'=A-R_{12}=1-0.5173=0.4827$, $R_{13}'=A-R_{13}=1-$
 $0.1485=0.8515$, $R_{14}'=A-R_{14}=1-0.8887=0.1113$ $R_{15}'=A-R_{15}=1-0.8887=0.1113$ and
 $R_{16}'=A-R_{16}=1-0.0000=1.0000$.

- 30 According to the invention, the distance between the centre point of the i' th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is equal to the dimensionless centre distance A and, according to the invention, the distance between the centre point of the i' th arc of the generated screw profile and the point of rotation of the generated screw profile is equal to the distance between the centre point of

the i th arc of the generating screw profile and the point of rotation of the generating screw profile and, according to the invention, the connecting line between the centre point of the i 'th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is a line parallel to a connecting line between the point of rotation of the generated screw profile and the point of rotation of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($i'=i$). By positioning the point of rotation of the generating screw profile at point $x=0, y=0$ and the point of rotation of the generated screw profile at point $x=A=1, y=0$, the x coordinate of the centre of the circle $Mx_{i'}$ of the generated screw profile can be calculated by adding the dimensionless centre distance A to the x coordinate of the centre of the circle Mx_i of the generating screw profile, and the y coordinate of the centre of the circle $My_{i'}$ of the generated screw profile is the same as the y coordinate of the centre of the circle My_i of the generating screw profile. In the present example the positions of the centre points of the 16 arcs of the generated screw profile are: $Mx_1'=1.0000, My_1'=0.0000, Mx_2'=1.5971, My_2'=0.1681, Mx_3'=0.9813, My_3'=-0.6198, Mx_4'=1.0001, My_4'=0.0002, Mx_5'=1.0699, My_5'=-0.3619, Mx_6'=0.9684, My_6'=-0.1054, Mx_7'=0.9684, My_7'=-0.1054, Mx_8'=0.7145, My_8'=0.0000, Mx_9'=0.9995, My_9'=0.0000, Mx_{10}'=1.1124, My_{10}'=0.0318, Mx_{11}'=0.9893, My_{11}'=-0.1258, Mx_{12}'=0.9928, My_{12}'=-0.0086, Mx_{13}'=1.0626, My_{13}'=-0.3707, Mx_{14}'=0.7903, My_{14}'=0.3176, Mx_{15}'=0.7903, My_{15}'=0.3176$ and $Mx_{16}'=1.6203, My_{16}'=0.0000$.

According to the invention, the starting point of the i 'th arc of the generated screw profile is located in an opposite direction, in relation to the centre point of the i 'th arc of the generated screw profile, to that of the starting point of the i th arc of the generating screw profile in relation to the centre point of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($i'=i$). In the present example the starting point of arc 1 of the generated screw profile is, for example, located at coordinate $x=0.6203, y=0$.

In the present example, the method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles produces a screw profile in which all

16 arcs merge tangentially into each other and form a closed, convex screw profile. Also, all 16 arcs of the generated screw profile are located within and/or on the boundaries of an annulus with a dimensionless outer radius RA' and a dimensionless inner radius RI' , whose centre point is located on the point of rotation of the generated screw profile. In addition, arc 1 of the generated screw profile is located on the dimensionless inner radius RI' and the configuration rule that at least one arc touches the dimensionless inner radius RI' is thereby fulfilled. In addition, the end point of arc 4, which is also the starting point of arc 5, of the generated screw profile, is located on the dimensionless outer screw radius RA' of the generated screw profile and the configuration rule that at least one arc touches the dimensionless outer screw radius RA' is thereby fulfilled.

The method of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights produces a screw profile in which each of the sections of the generated screw profile is designed in such a manner that the radii of the arcs of the generated screw profile are, in reverse order, identical to the radii of the arcs of the generating screw profile. As will be clear to any person of ordinary skill in the art, the profile sections of the generating screw profile and the generated screw profile are identically superimposable by rotation and mirroring. In the description of the figures hereinbelow, which relate to sections of screw profiles with different numbers of flights, frequently no distinction is therefore made between the generating and the generated screw profile, reference merely being made to screw profiles.

Figures 1 to 24 depict screw profiles with one flight obtained by the method according to the invention. Figures 1 to 20 all depict one half and thus one section of a screw profile with 1 flight. All of these figures have the same type of structure, which is described in detail in the following. The xy coordinate system, at whose origin the point of rotation of the screw profile is located, is in the middle of the figures. The arcs of the screw profile are shown by thick, unbroken lines which are labelled with the respective arc numbers. The centre points of the arcs are depicted in the form of small circles. The centre points of the arcs are connected by thin, unbroken lines both to the starting point and the end point of the corresponding arc. The straight line FP is depicted by a thin dotted line. The outer screw radius RA is characterized by a thin, broken line and its numerical value is given to four significant digits on the bottom righthand side of each figure. On the righthand side of

the figures the radius R , the angle α and the x and y coordinates of the centre point Mx and My of each arc are given to four significant digits. The screw profile is clearly defined by these values.

- 5 Figures 1 to 24 show screw profiles and screw elements in which the dimensionless outer screw radius RA has the values 0.54, 0.56, 0.57, 0.58 and 0.63. The method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights is not limited to these discrete values of the dimensionless outer screw radius. Using the method according to the invention, one-flight screw profiles with a
10 dimensionless outer screw radius between RA greater than 0.5 and RA smaller than or equal to 1, and preferably in the range from $RA=0.52$ to $RA=0.707$, can be generated.

Screw profiles in which a screw profile section consists of a total of 2 arcs are referred to hereinafter as 2-circle screw profiles. Screw profiles in which a screw profile section
15 consists of a total of 4 arcs are referred to hereinafter as 4-circle screw profiles. Screw profiles in which a screw profile section consists of a total of 6 arcs are referred to hereinafter as 6-circle screw profiles. Screw profiles in which a screw profile section consists of a total of 8 arcs are referred to hereinafter as 8-circle screw profiles.

- 20 **Figure 1:** Figures 1a and 1b depict preferred 2-circle screw profiles. Figures 1a and 1b differ in their outer screw radius RA . In Figure 1a the outer screw radius RA is 0.58. In Figure 1b the outer screw radius RA is 0.63. In Figures 1a and 1b arc 1 has a radius $R_1=A/2=0.5$. In Figures 1a and 1b arc 1 has an angle $\alpha_1=\pi/2$.

Figure 2: Figures 2a and 2b depict preferred 4-circle screw profiles. Figures 2a and 2b
25 differ in their outer screw radius RA . In Figure 2a the outer screw radius RA is 0.58. In Figure 2b the outer screw radius RA is 0.63. In Figures 2a and 2b arc 1 has a radius $R_1=RA$. In Figures 2a und 2b arc 2 has a radius $R_2=0$. In Figures 2a and 2b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 2a and 2b angle α_2 of arc 2 is dependent on the outer screw radius RA .

- 30 **Figure 3:** Figures 3a and 3b depict additional preferred 4-circle screw profiles. Figures 3a and 3b differ in their outer screw radius RA . In Figure 3a the outer screw radius RA is 0.58. In Figure 3b the outer screw radius RA is 0.63. In Figures 3a and 3b arc 1 has a radius

$R_1=0$. In Figures 3a and 3b arc 2 has a radius $R_2=A=1$. In Figures 3a and 3b arc 1 has an angle $\alpha_1=\pi/6$. In Figures 3a and 3b arc 2 has an angle $\alpha_2=\pi/3$.

Figure 4: Figures 4a to 4d depict additional preferred 4-circle screw profiles. Figures 4a to 4d depict a preferred transition between Figure 3b and Figure 1b. In Figures 4a to 4d the
5 outer screw radius RA is 0.63. In Figures 4a to 4d arc 1 has a radius $R_1=0$. In Figures 4a to 4d angle α_1 of arc 1 is gradually decreased.

Figure 5: Figures 5a to 5d depict additional preferred 4-circle screw profiles. Figures 5a to 5d depict an additional preferred transition between Figure 3b and Figure 1b. In Figures 5a to 5d the outer screw radius RA is 0.63. In Figures 5a to 5d arc 1 has an angle $\alpha_1=\pi/6$.
10 In Figures 5a to 5d radius R_1 of arc 1 is gradually increased.

Figure 6: Figures 6a to 6d depict additional preferred 4-circle screw profiles. Figures 6a to 6d depict an additional preferred transition between Figure 3b and Figure 1b. In Figures 6a to 6d the outer screw radius RA is 0.63. In Figures 6a to 6d arc 2 has a radius $R_2=A=1$. In Figures 6a to 6d radius R_1 of arc 1 is gradually increased.

15 **Figure 7:** Figures 7a to 7d depict additional preferred 4-circle screw profiles. Figures 7a to 7d depict a preferred transition between Figure 2b and Figure 1b. In Figures 7a to 7d the outer screw radius RA is 0.63. In Figures 7a to 7d arc 1 has a radius $R_1=RA$. In Figures 7a to 7d angle α_1 of arc 1 is gradually decreased.

Figure 8: Figures 8a to 8d depict additional preferred 4-circle screw profiles. Figures 8a to 8d depict an additional preferred transition between Figure 2b and Figure 1b. In Figures 8a to 8d the outer screw radius RA is 0.63. In Figures 8a to 8d arc 2 has a radius $R_2=0$. In Figures 8a to 8d radius R_1 of arc 1 is gradually decreased and angle α_1 of arc 1 is gradually increased.
20

25 A direct transition between Figure 2b and Figure 3b is not possible via a 4-circle screw profile. In such a case the transition takes place via Figure 1b.

Figure 9: Figures 9a to 9d depict preferred 6-circle screw profiles. Figures 9a to 9d depict a preferred transition between Figure 2a and Figure 3a. In Figures 9a to 9d the outer screw
30 radius RA is 0.58. In Figures 9a to 9d arc 1 has a radius $R_1=RA$. In Figures 9a to 9d arc 2 has a radius $R_2=0$. In Figures 9a to 9d arc 3 has a radius $R_3=A=1$. In Figures 9a to 9d angle α_1 of arc 1 is gradually decreased.

Figure 10: Figures 10a to 10d depict additional preferred 6-circle screw profiles. Figures 10a to 10d depict an additional preferred transition between Figure 2a and a figure which is similar to Figure 4b. In Figures 10a to 10d the outer screw radius RA is 0.58. In Figures 10a to 10d arc 1 has a radius $R_1=RA$. In Figures 10a to 10d arc 2 has a radius $R_2=0$. In
 5 Figures 10a to 10d arc 3 has a radius $R_3=0.75$. In Figures 10a to 10d angle α_1 of arc 1 is gradually decreased.

Figure 11: Figures 11a to 11d depict additional preferred 6-circle screw profiles. Figures 11a to 11d depict an additional preferred transition between Figure 2a and Figure 1a. In Figures 11a to 11d the outer screw radius RA is 0.58. In Figures 11a to 11d arc 1 has a
 10 radius $R_1=RA$. In Figures 11a to 11d arc 2 has a radius $R_2=0$. In Figures 11a to 11d arc 3 has a radius $R_3=0.5$. In Figures 11a to 11d angle α_1 of arc 1 is gradually decreased.

In addition to the abovementioned transitions between the screw profiles in the individual figures, transitions from one figure to another are also possible. Thus, the screw profiles of
 15 Figures 9a, 10a and 11a or Figures 9b, 10b and 11b can, for example, merge gradually into each other.

Figure 12: Figures 12a to 12d depict additional preferred 6-circle screw profiles. Figures 12a to 12d depict a further preferred transition based on Figure 2a. In Figures 12a to 12d
 20 the outer screw radius RA is 0.58. In Figures 12a to 12d arc 1 has a radius $R_1=RA$. In Figures 12a to 12d arc 2 has a radius $R_2=0.125$. In Figures 12a to 12d arc 3 has a radius $R_3=A=1$. In Figures 12a to 12d angle α_1 of arc 1 is gradually decreased.

Figure 13: Figures 13a to 13d depict additional preferred 6-circle screw profiles. Figures 13a to 13d depict an additional preferred transition based on Figure 2a. In Figures 13a to
 25 13d the outer screw radius RA is 0.58. In Figures 13a to 13d arc 1 has a radius $R_1=RA$. In Figures 13a to 13d arc 2 has a radius $R_2=0.125$. In Figures 13a to 13d arc 3 has a radius $R_3=0.75$. In Figures 13a to 13d angle α_1 of arc 1 is gradually decreased.

In addition to the abovementioned transitions between the individual screw profiles in each
 30 figure, transitions from one figure to another are also possible. Thus, the screw profiles of Figures 12a and 13a or Figures 12b and 13b can, for example, merge gradually into each other.

Figure 14: Figures 14a to 14d depict additional preferred 6-circle screw profiles. Figures 14a to 14d depict an additional preferred transition based on Figure 2a. In Figures 14a to 14d the outer screw radius RA is 0.58. In Figures 14a to 14d arc 1 has a radius $R_1=RA$. In Figures 14a to 14d arc 2 has a radius $R_2=0.25$. In Figures 14a to 14d arc 3 has a radius $R_3=A=1$. In Figures 14a to 14d angle α_1 of arc 1 is gradually decreased.

Figure 15: Figures 15a to 15d depict additional preferred 6-circle screw profiles. Figures 15a to 15d depict an additional preferred transition based on Figure 2a. In Figures 15a to 15d the outer screw radius RA is 0.58. In Figures 15a to 15d arc 1 has a radius $R_1=RA$. In Figures 15a to 15d arc 2 has a radius $R_2=0.25$. In Figures 15a to 15d arc 3 has a radius $R_3=0.75$. In Figures 15a to 15d angle α_1 of arc 1 is gradually decreased.

In addition to the abovementioned transitions between the individual screw profiles in each figure, transitions from one figure to another are also possible. Thus, the screw profiles of Figures 14a and 15a or Figures 9a, 12a and 14a or Figures 10a, 13a and 15a can, for example, merge gradually into each other.

In the above figures relating to one-flight screw profiles the screw profile always starts at point $x=RA, y=0$. Figures 16 to 19 depict a selection of 8-circle screw profiles which start at point $x<RA, y=0$ and in which only arc 3 is positioned on the outer screw radius.

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Figure 16: Figures 16a to 16d depict preferred 8-circle screw profiles. Figures 16a to 16d depict a preferred transition based on Figure 2a. In Figures 16a to 16d the outer screw radius RA is 0.58. In Figures 16a to 16d radius R_1 of arc 1 is gradually increased. In Figures 16a to 16d arc 2 has a radius $R_2=0$. In Figures 16a to 16d arc 3 has a radius $R_3=RA$ and is positioned on the outer screw radius. In Figures 16a to 16d arc 4 has a radius $R_4=0$. In Figures 16a to 16d angle α_1 of arc 1 is gradually decreased and angle α_2 of arc 2 is gradually increased. In Figures 16a to 16d arc 3 has an angle $\alpha_3=0.4285$. In Figures 16a to 16d arc 4 has an angle $\alpha_4=0.5315$.

Figure 17: Figures 17a to 17d depict additional preferred 8-circle screw profiles. Figures 17a to 17d depict an additional preferred transition based on Figure 2a. In Figures 17a to 17d the outer screw radius RA is 0.58. In Figures 17a to 17d radius R_1 of arc 1 is gradually increased. In Figures 17a to 17d arc 2 has a radius $R_2=0$. In Figures 17a to 17d arc 3 has a radius $R_3=RA$ and is positioned on the outer screw radius. In Figures 17a to

30

- 17d angle α_1 of arc 1 is gradually decreased and angle α_2 of arc 2 is gradually increased. In Figures 17a to 17d arc 3 has an angle $\alpha_3=0.2627$. In Figures 17a to 17d arc 4 has an angle $\alpha_4=0.5315$. In Figures 17a to 17d arc 4 has a radius $R_4=0$, i.e. at this point there is a bend in the profile. The centre point of arc 4 coincides with the bend. The "size of the bend" is determined by angle α_4 , i.e. the transition from arc 3 to arc 4' takes place by rotation about angle α_4 . Or in other words: A tangent on arc 3 at the centre point of arc 4 intersects a tangent on arc 4' at the centre point of arc 4 and at an angle α_4 . With the inclusion of arc 4 all of the adjacent arcs $3 \rightarrow 4$, $4 \rightarrow 4'$ merge tangentially into each other.
- 10 In addition to the abovementioned transitions between the individual screw profiles in each figure, transitions from one figure to another are also possible. Thus, the screw profiles of Figures 16a and 17a or Figures 16b and 17b can, for example, merge gradually into each other.
- 15 **Figure 18:** Figures 18a to 18d depict additional preferred 8-circle screw profiles. Figures 18a to 18d depict an additional preferred transition based on Figure 2a. In Figures 18a to 18d the outer screw radius RA is 0.58. In Figures 18a to 18d radius R_1 of arc 1 is gradually increased and radius R_2 of arc 2 is gradually decreased. In Figures 18a to 18d arc 3 has a radius $R_3=RA$ and is positioned on the outer screw radius. In Figures 18a to 18d arc 4 has a radius $R_4=0$. In Figures 18a to 18d angle α_1 of arc 1 is gradually decreased and angle α_2 of arc 2 is gradually increased. In Figures 18a to 18d arc 3 has an angle $\alpha_3=0.2278$. In Figures 18a to 18d arc 4 has an angle $\alpha_4=0.5315$.
- 20 **Figure 19:** Figures 19a to 19d depict additional preferred 8-circle screw profiles. Figures 19a to 19d depict a preferred transition based on Figure 18d. In Figures 19a to 19d the outer screw radius RA is 0.58. In Figures 19a to 19d arc 1 has a radius $R_1=0.9061$. In Figures 19a to 19d arc 2 has a radius $R_2=0.1385$. In Figures 19a to 19d arc 3 has a radius $R_3=RA$ and is located on the outer screw radius. In Figures 19a to 19d radius R_4 of arc 4 is gradually increased. In Figures 19a to 19d arc 1 has an angle $\alpha_1=0.4304$. In Figures 19a to 19d arc 2 has an angle $\alpha_2=0.3812$. In Figures 19a to 19d angle α_3 of arc 3 is gradually decreased and angle α_4 of arc 4 is gradually increased.
- 30

The method according to the invention for generating planar, tightly intermeshing, self-cleaning and co-rotating screw profiles with z flights is illustrated in the following by means of the section of a screw profile shown in Figure 19b.

- 5 According to the invention, the screw profile and the screw profile section are both located in one plane. For the sake of simplicity this plane is placed on the xy plane of a Cartesian coordinate system. For the sake of simplicity the point of rotation of the screw profile is placed at the origin of the Cartesian coordinate system ($x=0, y=0$).
- 10 According to the invention, the flight number z is selected such that z is greater than or equal to 1. In the present example the flight number is selected to be $z=1$. According to the invention, the number of arcs n of the screw profile is selected such that n is an integer multiple p of $4z$. In the present example the number of arcs is selected to be $n=16$, resulting in $p=4$. According to the invention, the dimensionless outer screw radius RA of
- 15 the screw profile is selected such that it is greater than 0 and smaller than or equal to the dimensionless centre distance A . In the present example the dimensionless outer screw radius of the screw profile is selected to be $RA=0.58$. According to the invention, the dimensionless inner radius RI of the screw profile is selected such that it is greater than or equal to 0 and smaller than or equal to the dimensionless outer screw radius RA . In the
- 20 present example the dimensionless inner radius of the screw profile is selected to be $RI=A-RA=0.42$.

The arcs of the screw profile can be arranged in a clockwise or anti-clockwise direction about the axis of rotation of the screw profile. In the present example, the arcs are arranged

25 in an anti-clockwise direction about the axis of rotation of the screw profile.

The screw profile is subdivided into $2z$ sections which are characterized in that each section is enclosed between two straight lines which are at an angle to each other of π/z in terms of radian measurement and which meet at the point of rotation of the screw profile,

30 these two straight lines being referred to as section boundaries. In the present example the screw profile is subdivided into two sections. For the sake of simplicity, both section boundaries are located on the x axis of the coordinate system. In relation to the present

example, only that screw profile section is explained hereinbelow which is positioned in the positive y direction.

The screw profile section is subdivided into a first and a second part, the first part
 5 consisting of p arcs and the second part consisting of p' arcs, wherein $p'=p$. In the present example it follows that $p'=4$. The arcs of the first part of the screw profile section can be numbered in ascending or descending order. The arcs of the second part of the screw profile section are numbered in reverse order to the arcs of the first part of the screw profile section. In the present example the arcs of the first part of the screw profile section are
 10 numbered in ascending order and the arcs of the second part of the screw profile section are accordingly numbered in descending order.

According to the invention, angle α_1 of arc 1 of the first part of the screw profile section is selected such that it is, in terms of radian measurement, greater than or equal to 0 and
 15 smaller than or equal to $\pi/(2z)$. In the present example the angle of arc 1 is selected to be $\alpha_1=0.4304$. According to the invention, the dimensionless radius R_1 of arc 1 of the first part of the screw profile section is selected such that it is greater than or equal to 0 and smaller than or equal to the centre distance A . In the present example the dimensionless radius of arc 1 is selected to be $R_1=0.9061$. According to the invention, the position of
 20 arc 1 of the first part of the screw profile section is selected such that arc 1 is located within and/or on the boundaries of an annulus with a dimensionless outer screw radius RA and a dimensionless inner radius RI , whose centre point is located on the point of rotation of the screw profile. Its position is preferably determined by the position of the starting point and the centre point of arc 1. In the method according to the invention the starting point and
 25 the centre point of arc 1 are located on one of the section boundaries, the starting point resulting from the position of the centre point and the dimensionless radius R_1 . In the present example the centre point of arc 1 is located at coordinate $Mx_1=-0.3937$, $My_1=0.0000$ and the starting point is thus located at coordinate $x=0.5124$, $y=0.0000$.

30 According to the invention, the angles $\alpha_2, \dots, \alpha_{(p-1)}$ of $p-2$ additional arcs, i.e. 2 additional arcs of the first part of the screw profile section are selected such that they are, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to $\pi/(2z)$. In the present example the angles of the 2 additional arcs are selected to be $\alpha_2=0.3812$ and

$\alpha_3=0.1580$. According to the invention, the dimensionless radii $R_2, \dots, R_{(p-1)}$ of the 2 additional arcs of the first part of the screw profile section are selected such that they are greater than or equal to 0 and smaller than or equal to the dimensionless centre distance A . In the present example the dimensionless radii of the 2 additional arcs are selected to be
 5 $R_2=0.1385$ and $R_3=0.5800$. According to the configuration rules the arcs are arranged so that they merge into each other tangentially in such a manner that a closed, convex screw profile is obtained, an arc with a dimensionless radius of 0 being treated in the same manner as an arc with a dimensionless radius of ϵ , which is a very small positive real number which tends towards 0 ($\epsilon \ll 1, \epsilon \rightarrow 0$). This configuration rule means that the
 10 end point of an arc is at the same time the starting point of the next arc. The required tangential transition between a first arc and a second successive arc is obtained by the centre point of the second successive arc being placed in such a manner on a straight line through the end point and the centre point of the first arc that the distance between the centre point of the second successive arc and the end point of the first arc is equal to the
 15 radius of the second successive arc and the screw profile is convex. An arc with a radius of 0 is treated in the same way as an arc with a very small radius ϵ , which tends towards 0, so as to allow the tangential transition pattern to be continued. Alternatively, an arc with a radius of 0 can be treated in such a manner that the screw profile has a bend at the position of this arc, the size of the bend being determined by the angle of this arc. In the present
 20 example the abovementioned configuration rule results in the following positions of the centre points of the two additional arcs: $Mx_2=0.3039, My_2=0.3202$ and $Mx_3=0.0000, My_3=0.0000$. Arc 3 is positioned on the dimensionless outer screw radius RA and the configuration rule that at least one arc touches the dimensionless outer screw radius RA is thereby fulfilled.

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According to the invention, angle α_4 of the last arc of the first part of the screw profile section is such that the sum of the angles of the 4 arcs of the first part of the screw profile section is, in terms of radian measurement, $\pi/(2z)$, wherein angle α_4 is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to $\pi/(2z)$. In the present
 30 example, the angle of this last arc, α_4 , is 0.6013. According to the invention, the dimensionless radius R_4 of the last arc of the first part of the screw profile section is such that the end point of this last arc touches a straight line FP at one point, this straight line FP being vertical to the angle bisector of the two section boundaries of this section and at

such a distance from the point of rotation of the screw profile in the direction of this section which is equal to half the centre distance, the angle bisector and the section boundaries passing through the point of rotation of the screw profile. In Figure 19b, straight line FP is shown in the form of a dotted line. Arc 4 of the first part of the screw profile section is constructed in such a manner that a tangent is placed on arc 3 at the end point of arc 3, the point of intersection between the tangent and the straight line FP being the centre point of a circle whose radius is equal to the length of the distance between the end point of arc 3 and the point of intersection between the tangent and the straight line FP and the point of intersection in the direction of the selected clock direction between the circle and the straight line FP is the required point of contact between the end point of arc 4 and straight line FP . At the end point of arc 4 a perpendicular to the straight line FP is formed. The point of intersection between this perpendicular and the straight line through the end point and the centre point of arc 3 is the centre point of arc 4. In the present example the position of the centre point of arc 4 is $Mx_4=0.2580$, $My_4=0.3761$ and the dimensionless radius of arc 4, R_4 , is 0.1239.

Angles $\alpha_{p'}$, ..., $\alpha_{1'}$ of the second part of the screw profile section are defined in such a manner that angle $\alpha_{j'}$ of the j' th arc of the second part of the section is the same as angle α_j of the j th arc of the first part of the section, wherein j is an index which represents all integers in the range from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p' ($\alpha_{1'}=\alpha_1$, ..., $\alpha_{p'}=\alpha_p$). In the present example the angles of the second part of the section are $\alpha_{1'}=\alpha_1=0.4304$, $\alpha_{2'}=\alpha_2=0.3812$, $\alpha_{3'}=\alpha_3=0.1580$ and $\alpha_{4'}=\alpha_4=0.6013$.

The dimensionless radii $R_{p'}$, ..., $R_{1'}$ of the second part of the screw profile section are defined in such a manner that the sum of the dimensionless radius $R_{j'}$ of the j' th arc of the second part of a section and the dimensionless radius R_j of the j th arc of the first part of a section is equal to the dimensionless centre distance A , wherein j is an index which represents all integers in the range from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p' ($R_{1'}+R_1=A=1$, ..., $R_{p'}+R_p=A=1$). In the present example the dimensionless radii of the second part of the section are $R_{1'}=A-R_1=0.0939$, $R_{2'}=A-R_2=0.8615$, $R_{3'}=A-R_3=0.4200$ and $R_{4'}=A-R_4=0.8761$.

According to the invention, the position of the arcs of the second part of the screw profile section is such that the arcs merge tangentially into each other and the screw profile is convex. In the present example the following coordinates apply to the centre points of the

5 4 arcs of the second part of the screw profile section: $Mx_1' = -0.3937$, $My_1' = 0.0000$, $Mx_2' = 0.3039$, $My_2' = -0.3202$, $Mx_3' = 0.0000$, $My_3' = 0.0000$ and $Mx_4' = 0.2580$, $My_4' = -0.3761$. Arc 3 of the second part of the screw profile section is positioned on the dimensionless inner radius RI and the configuration rule that at least one arc touches the dimensionless inner radius RI is thereby fulfilled.

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Figure 20: All one-flight screw profiles can be shifted to a certain extent along the x -axis in a positive or negative x direction without forfeiting their self-cleaning properties, since, due to the shift along the x -axis, the condition of touching the straight line FP at one point continues to be met. The maximum shift in a positive or negative x direction is reached

15 when the screw profile has a distance at one point from the point of rotation which is greater than the outer radius RA . The maximum degree of shift depends on the screw profile to be shifted and is smaller than or equal to the difference between the outer radius RA and the inner radius RI . If the shift is smaller than the maximum admissible shift, the maximum distance between the screw profile and the point of rotation is smaller than the

20 originally required outer radius RA . Figures 20a to 20d illustrate the stepwise shift of a screw profile corresponding to Figure 2a. It can be seen that the radii and the angles of the individual arcs are not changed by the shift.

Figures 21 to 23 show the generating and the generated screw profile inside a figure8-

25 shaped screw barrel. Numerical values are provided inside the two screw profiles for the following screw parameters:

- RG : radius of the two barrel bores
- RV : virtual barrel radius which is smaller than or equal to the barrel radius RG
- RA : outer screw radius of the tightly intermeshing self-cleaning screw profiles
- 30 - RF : outer screw radius of the screw profiles to be fabricated
- S : clearance between the two screw profiles to be fabricated
- D : clearance between the screw profiles to be fabricated and the barrel
- T : pitch of a conveying, mixing or transition element

- *VPR*: size of the shift of the tightly intermeshing, self-cleaning screw profiles if the latter are arranged eccentrically
- *VPW*: angle of the shift (in terms of direction) of the tightly intermeshing, self-cleaning screw profiles, if they are arranged eccentrically
- 5 - *VLR* : size of the shift within the clearances of the screw profile to be fabricated for the lefthand screw
- *VLW* : angle of the shift within the clearances of the screw profile to be fabricated for the righthand screw
- *VRR* : size of the shift within the clearances of the screw profile to be fabricated for the
- 10 righthand screw
- *VRW* : angle of the shift within the clearances of the screw profile to be fabricated for the righthand screw

The screw barrel consisting of two overlapping bores each with a radius RG and a spacing $A=1$ is depicted by a thin, broken line. In the overlapping area between the two barrel

15 bores the two bores are depicted by thin, dotted lines. The centre points of the two barrel bores are identical to the two points of rotation of the screw profiles and are each characterized by a small circle. The theoretical tightly intermeshing, self-cleaning screw profiles are characterized by a thick unbroken line. The screw profiles actually fabricated are depicted by a thin unbroken line.

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It is well-known to those skilled in the art that the equation $RA=RV-D+S/2$ applies to the relationship between the outer screw radius RA of the tightly intermeshing, self-cleaning screw profile, the virtual barrel radius RV , the clearance S between the two screw profiles to be fabricated and the clearance D between the screw profiles to be fabricated and the

25 screw barrel.

It is also well-known to those skilled in the art that the equation $RF=RV-D$ applies to the relationship between the outer screw radius RF of the screw profile to be fabricated, the virtual barrel radius RV and the clearance D between the screw profiles to be fabricated and

30 the screw barrel.

Typically, the virtual barrel radius RV is equal to the actual barrel radius RG . If the virtual barrel radius RV is smaller than the barrel radius RG additional clearance exists between

the screw profiles and the barrel. This clearance can be used for shifting the generating and the generated screw profile eccentrically while maintaining self-cleaning. This eccentricity is clearly characterized by the size of the shift VPR and the direction of the shift in the form of angle VPW .

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Figure 21: Figures 21a to 21d depict preferred variants of eccentrically positioned one-flight screw profiles. The depicted tightly intermeshing, self-cleaning screw profiles are based on Figure 2, although the outer screw radius RA is 0.54 in Figures 21a to 21d. The virtual barrel radius is $RV=0.54$ and is smaller than the barrel radius RG ($RG=0.63$). The remaining geometrical parameters can be found in the individual figures. Eccentrically positioned, one-flight, tightly intermeshing, self-cleaning screw profiles are characterized in that the distance between the screw profiles and the barrel is always identical for both screw profiles, regardless of the direction of the shift. The screw profiles in Figures 21a to 21d have in each case been shifted to such an extent that precisely one point of the screw profiles touches the barrel. The size of the shift required for this purpose depends on the direction of the shift. It is also possible for the screw profiles to be in eccentric positions in which no point of the screw profiles touches the barrel.

Figure 22: As is well-known to those skilled in the art, all screw elements require a certain amount of clearance in practice, not only between each other but also between them and the barrel. Figures 22a to 22d depict various clearance strategies. The depicted tightly intermeshing, self-cleaning screw profiles are based on Figure 2a. The remaining geometrical parameters can be found in the individual figures. Figure 22a depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is the same as that between the screw profiles to be fabricated and the barrel. Figure 22b depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is smaller than that between the screw profiles to be fabricated and the barrel. Figure 22c depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is greater than the clearance between the screw profiles to be fabricated and the barrel. Figure 22d depicts a further variant according to Figure 22c with particularly large clearances. Typical clearances occurring in practice for the clearance between the screw profiles to be fabricated are in the range from 0.002 to 0.1. Typical clearances occurring in practice for the clearance between the screw profiles to be fabricated and the barrel are in

the range from 0.002 to 0.1. Typical clearances occurring in practice are constant around the periphery of the screw profile. It is however possible to vary around the periphery of the screw profiles not only the clearance between the screw profiles to be fabricated but also the clearance between the screw profiles to be fabricated and the barrel.

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Figure 23: It is also possible to shift the screw profiles to be fabricated within the clearances. Figures 23a to 23d depict a selection of possible shifts. The tightly intermeshing, self-cleaning screw profiles depicted are based on Figure 2a. The depicted screw profiles to be fabricated are based on Figure 22d. The remaining geometrical parameters can be found in the individual figures. In Figures 23a to 23d the size of the shift for both screw profiles to be fabricated is $VLR = VRR = 0.02$. In Figures 23a to 23d the direction of the shift for each two screw profiles to be fabricated is varied gradually between $VLW = VRW = 0$ and $VLW = VRW = \pi$. It is possible to shift the two screw profiles to be fabricated independently of each other in various directions and to different degrees.

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One-flight screw profiles generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention can be used for fabricating screw elements. In particular, such screw profiles can be used for fabricating conveying, mixing, kneading and transition elements.

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Figure 24a depicts, as an example, a pair of one-flight conveying elements based on the screw profile of Figure 2a. The barrel radius RG is 0.58. The clearance S between the two conveying elements is 0.02. The clearance D between the two conveying elements and the barrel is 0.01. The pitch T of the conveying elements is 1.2. The length of the conveying elements is 1.2, which corresponds to the rotation of the screw profiles by an angle 2π . The barrel is depicted by thin, unbroken lines on the left and right of the two conveying elements. A possible computational grid is also depicted on the surfaces of the two conveying elements. This grid can be used for computing the flow through twin and multiple screw extruders.

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Figure 24b depicts, as an example, a pair of one-flight kneading elements based on the screw profile of Figure 2a. The barrel radius RG is 0.58. The clearance S between the kneading discs of the two kneading elements is 0.02. The clearance D between the

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kneading discs of the two kneading elements and the barrel is 0.01. The kneading element consists of 7 kneading discs each staggered clockwise in relation to each other by an angle $\pi/3$. The first and the last kneading disc have a length of 0.09. The kneading discs in the middle have a length of 0.18. The groove between the kneading discs has a length of 0.02.

5 The barrel is depicted by thin unbroken lines on the right and left of the two kneading elements. A possible computational grid is also depicted on the surfaces of the two kneading elements. This grid can be used for computing the flow in twin and multiple screw extruders.

10 Figures 25 to 46 show screw profiles with 2 flights, which are generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention. Figures 25 to 42 in each case depict a quarter of a screw profile with 2 flights. All of these figures have an analogous design to that of Figures 1 to 20, which has already been described in detail for these figures.

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Figures 25 to 46 depict screw profiles and screw elements in which the dimensionless outer screw radius RA is 0.54, 0.56, 0.57, 0.58 and 0.63. The method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights is not limited to these discrete values for the dimensionless outer screw radius.

20 Using the method according to the invention, two-flight screw profiles with a dimensionless outer screw radius between RA greater than 0.5 and RA smaller than or equal to 0.707, and preferably in the range from $RA=0.52$ to $RA=0.69$, can be generated.

Figure 25: Figures 25a and 25b depict preferred 2-circle screw profiles. Figures 25a and 25b differ in the outer screw radius RA . In Figure 25a the outer screw radius RA is 0.58. In Figure 25b the outer screw radius RA is 0.63. In Figures 25a and 25b radius R_1 of arc 1 is dependent on the outer screw radius RA . In Figures 25a and 25b arc 1 has an angle $\alpha_1=\pi/4$.

Figure 26: Figures 26a and 26b depict preferred 4-circle screw profiles. Figures 26a and 26b differ in the outer screw radius RA . In Figure 26a the outer screw radius RA is 0.58. In Figure 26b the outer screw radius RA is 0.63. In Figures 26a and 26b arc 1 has a radius $R_1=RA$. In Figures 26a and 26b arc 2 has a radius $R_2=0$. In Figures 26a and 26b angle

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α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 26a and 26b angle α_2 of arc 2 is dependent on the outer screw radius RA .

Figure 27: Figures 27a and 27b depict additional preferred 4-circle screw profiles. Figures 27a and 27b differ in the outer screw radius RA . In Figure 27a the outer screw radius is RA is 0.58. In Figure 27b the outer screw radius RA is 0.63. In Figures 27a and 27b arc 1 has a radius $R_1=0$. In Figures 27a and 27b arc 2 has a radius $R_2=A=1$. In Figures 27a and 27b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 27a and 27b angle α_2 of arc 2 is dependent on the outer screw radius RA .

Figure 28: Figures 28a to 28d depict additional preferred 4-circle screw profiles. Figures 28a to 28d depict a preferred transition between Figure 27b and Figure 25b. In Figures 28a to 28d the outer screw radius RA is 0.63. In Figures 28a to 28d arc 1 has a radius $R_1=0$. In Figures 28a to 28d angle α_1 of arc 1 is gradually decreased.

Figure 29: Figures 29a to 29d depict additional preferred 4-circle screw profiles. Figures 29a to 29d depict another preferred transition between Figure 27b and Figure 25b. In Figures 29a to 29d the outer screw radius RA is 0.63. In Figures 29a to 29d arc 1 has an angle $\alpha_1=0.4537$. In Figures 29a to 29d radius R_1 of arc 1 is gradually increased.

Figure 30: Figures 30a to 30d depict additional preferred 4-circle screw profiles. Figures 30a to 30d depict an additional preferred transition between Figure 27b and Figure 25b. In Figures 30a to 30d the outer screw radius RA is 0.63. In Figures 30a to 30d arc 2 has a radius $R_2=A=1$. In Figures 30a to 30d radius R_1 of arc 1 is gradually increased.

Figure 31: Figures 31a to 31d depict additional preferred 4-circle screw profiles. Figures 31a to 31d depict a preferred transition between Figure 26b and Figure 25b. In Figures 31a to 31d the outer screw radius RA is 0.63. In Figures 31a to 31d arc 1 has a radius $R_1=RA$. In Figures 31a to 31d angle α_1 of arc 1 is gradually decreased.

Figure 32: Figures 32a to 32d depict additional preferred 4-circle screw profiles. Figures 32a to 32d depict an additional preferred transition between Figure 26b and Figure 25b. In Figures 32a to 32d the outer screw radius RA is 0.63. In Figures 32a to 32d arc 2 has a radius $R_2=0$. In Figures 32a to 32d radius R_1 of arc 1 is gradually decreased and angle α_1 of arc 1 is gradually increased.

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A direct transition between Figure 26b and Figure 27b by means of a 4-circle screw profile is not possible. In such a case the transition takes place via Figure 25b.

Figure 33: Figures 33a to 33d depict preferred 6-circle screw profiles. Figures 33a to 33d depict a preferred transition between Figure 26a and Figure 27a. In Figures 33a to 33d the outer screw radius RA is 0.58. In Figures 33a to 33d arc 1 has a radius $R_1=RA$. In Figures 33a to 33d arc 2 has a radius $R_2=0$. In Figures 33a to 33d arc 3 has a radius $R_3=A=1$. In
 5 Figures 33a to 33d angle α_1 of arc 1 is gradually decreased.

Figure 34: Figures 34a to 34d depict additional preferred 6-circle screw profiles. Figures 34a to 34d depict a preferred transition between Figure 26a and a figure which is similar to Figure 28a. In Figures 34a to 34d the outer screw radius RA is 0.58. In Figures 34a to 34d arc 1 has a radius $R_1=RA$. In Figures 34a to 34d arc 2 has a radius $R_2=0$. In Figures 34a
 10 to 34d arc 3 has a radius $R_3=0.75$. In Figures 34a to 34d angle α_1 of arc 1 is gradually decreased.

Figure 35: Figures 35a to 35d depict additional preferred 6-circle screw profiles. Figures 35a to 35d depict a preferred transition between Figure 26a and a figure which is similar to Figures 28a and 28b. In Figures 35a to 35d the outer screw radius RA is 0.58. In Figures
 15 35a to 35d arc 1 has a radius $R_1=RA$. In Figures 35a to 35d arc 2 has a radius $R_2=0$. In Figures 35a to 35d arc 3 has a radius $R_3=0.5$. In Figures 35a to 35d angle α_1 of arc 1 is gradually decreased.

Figure 36: Figures 36a to 36d depict additional preferred 6-circle screw profiles. Figures 36a to 36d depict a preferred transition between Figure 26a and Figure 25a. In Figures 36a
 20 to 36d the outer screw radius RA is 0.58. In Figures 36a to 36d arc 1 has a radius $R_1=RA$. In Figures 36a to 36d arc 2 has a radius $R_2=0$. In Figures 36a to 36d arc 3 has a radius $R_3=0.3069$. In Figures 36a to 36d angle α_1 of arc 1 is gradually decreased.

In addition to the abovementioned transitions between the individual screw profiles in each
 25 figure, transitions from one figure to another are also possible. Thus, the screw profiles of Figures 33a, 34a, 35a, 36a or Figures 33b, 34b, 35b, 36b can, for example, merge gradually into each other.

Figure 37: Figures 37a to 37d depict additional preferred 6-circle screw profiles. Figures
 30 37a to 37d depict a preferred transition based on Figure 26a. In Figures 37a to 37d the outer screw radius RA is 0.58. In Figures 37a to 37d arc 1 has radius $R_1=RA$. In Figures 37a to 37d radius R_2 of arc 2 is gradually increased. In Figures 37a to 37d arc 3 has a radius $R_3=A=1$. In Figures 37a to 37d angle α_1 of arc 1 is gradually decreased.

Figure 38: Figures 38a to 38d depict additional preferred 6-circle screw profiles. Figures 38a to 38d depict a preferred transition based on Figure 26a. In Figures 38a to 38d the outer screw radius RA is 0.58. In Figures 38a to 38d arc 1 has a radius $R_1=RA$. In Figures 38a to 38d radius R_2 of arc 2 is gradually increased. In Figures 38a to 38d arc 3 has a radius $R_3=0.75$. In Figures 38a to 38d angle α_1 of arc 1 is gradually decreased.

Figure 39: Figures 39a to 39d depict additional preferred 6-circle screw profiles. Figures 39a to 39d depict a preferred transition based on Figure 26a. In Figures 39a to 39d the outer screw radius RA is 0.58. In Figures 39a to 39d arc 1 has a radius $R_1=RA$. In Figures 39a to 39d radius R_2 of arc 2 is gradually increased. In Figures 39a to 39d arc 3 has a radius $R_3=0.5$. In Figures 39a to 39d angle α_1 of arc 1 is gradually decreased.

Figure 40: Figures 40a to 40d depict additional preferred 6-circle screw profiles. Figures 40a to 40d depict a preferred transition between Figure 26a and Figure 25a. In Figures 40a to 40d the outer screw radius RA is 0.58. In Figures 40a to 40d arc 1 has a radius $R_1=RA$. In Figures 40a to 40d the radius R_2 of arc 2 is gradually increased. In Figures 40a to 40d arc 3 has a radius $R_3=0.3069$. In Figures 40a to 40d angle α_1 of arc 1 is gradually decreased.

In addition to the abovementioned transitions between the individual screw profiles in each figure, transitions from one figure to another are also possible. The screw profiles of Figures 37a, 38a, 39a and 40a or of Figures 37b, 38b, 39b and 40b can, for example, merge gradually into each other.

In the above figures for two-flight screw profiles, the screw profile always begins at point $x=RA$ and $y=0$. Figures 41 and 42 depict a selection of 8-circle screw profiles which begin at point $x<RA$ and $y=0$ and in which only arc 3 is located on the outer screw radius.

Figure 41: Figures 41a to 41d depict preferred 8-circle screw profiles. Figures 41a to 41d depict a preferred transition based on an Erdmenger screw profile with an outer screw radius $RA=0.54$. In Figures 41a to 41d the outer screw radius RA is 0.54. In Figures 41a to 41d the radius R_1 of arc 1 is gradually increased. In Figures 41a to 41d arc 2 has a radius $R_2=0$. In Figures 41a to 41d arc 3 has a radius $R_3=RA$ and is located on the outer screw radius. In Figures 41a to 41d arc 4 has a radius $R_4=0$. In Figures 41a to 41d angle α_1 of

arc 1 is gradually decreased and angle α_2 of arc 2 is gradually increased. In Figures 41a to 41d arc 3 has an angle $\alpha_3=0.145$. In Figures 41a to 41d arc 4 has an angle $\alpha_4=0.3873$.

Figure 42: Figures 42a to 42d depict additional preferred 8-circle screw profiles. Figures 42a to 42d depict an additional preferred transition based on an Erdmenger screw profile with an outer screw radius $RA=0.54$. In Figures 42a to 42d the outer screw radius RA is 0.54. In Figures 42a to 42d radius R_1 of arc 1 is gradually increased. In Figures 42a to 42d arc 2 has a radius $R_2=0$. In Figures 42a to 42d arc 3 has a radius $R_3=RA$ and is located on the outer screw radius. In Figures 42a to 42d arc 4 has a radius $R_4=0$. In Figures 42a to 42d angle α_1 of arc 1 is gradually decreased and angle α_2 of arc 2 is gradually increased. In Figures 42a to 42d arc 3 has an angle $\alpha_3=0.0419$. In Figures 42a to 42d arc 4 has an angle $\alpha_4=0.3873$.

In addition to the abovementioned transitions between the individual screw profiles in each figure, transitions from one figure to another are also possible. The screw profiles of Figures 41a and 42a or Figures 41b and 42b can, for example, merge gradually into each other.

Figures 43 to 45 depict the generating and the generated screw profile inside a figure 8-shaped screw barrel. All of these figures have an analogous design to that of Figures 21 to 23, which has already been described in detail in relation to these figures. The numerical values inside the screw profiles have also already been described in connection with Figures 21 to 23.

Figure 43: Figures 43a to 43d depict preferred variants of eccentrically positioned two-flight screw profiles. The depicted tightly intermeshing self-cleaning screw profiles are based on Figure 26, although the outer screw radius RA is 0.54 in Figures 43a to 43d. The virtual barrel radius RV is 0.54 and is smaller than the barrel radius RG ($RG=0.63$). The remaining geometrical parameters can be found in the individual figures. Eccentrically positioned, two-flight, tightly intermeshing, self-cleaning screw profiles are characterized in that the distance between the screw profiles and the barrel varies. The screw profiles in Figures 43a to 43c have in each case been shifted to such an extent that precisely one point of the lefthand screw profile touches the barrel. The degree of the shift necessary for this contact depends on the direction of the shift. Figure 43d shows a special case in which the

screw profiles are shifted to such a degree and in such a direction that both screw profiles touch the barrel at precisely one point. This shift takes place at an angle of $\pi/4$. It is also possible for the screw profiles to be in eccentric positions in which no point of the screw profiles touches the barrel.

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Figure 44: As is well-known to those skilled in the art, all screw profiles require a certain degree of clearance in practice, both in relation to each other and to the barrel. Figures 44a to 44d depict various clearance strategies. The depicted tightly intermeshing, self-cleaning screw profiles are based on Figure 26a. The remaining geometrical parameters can be found in the individual figures. Figure 44a depicts a clearance strategy in which the clearance between the screw profiles to be fabricated and between the screw profiles to be fabricated and the barrel is identical. Figure 44b depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is smaller than the clearance between the screw profiles to be fabricated and the barrel. Figure 44c depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is larger than the clearance between the screw profiles to be fabricated and the barrel. Figure 44d depicts an additional embodiment according to Figure 44c with particularly large clearances. Typical clearances used in practice for the clearance between the screw profiles to be fabricated are in the range from 0.002 to 0.1. Typical clearances used in practice for the clearance between the screw profiles to be fabricated and the barrel are in the range from 0.002 to 0.1. Typical clearances used in practice are constant around the periphery of the screw profile. It is however possible to vary around the periphery of the screw profiles not only the clearance between the screw profiles to be fabricated but also the clearance between the screw profiles to be fabricated and the barrel.

Figure 45: It is also possible to shift the screw profiles to be fabricated within the clearances. Figures 45a to 45d depict a selection of possible shifts. The depicted tightly intermeshing, self-cleaning screw profiles are based on Figure 26a. The depicted screw profiles to be fabricated are based on Figure 44d. The remaining geometrical parameters can be found in the individual figures. In Figures 45a to 45d the degree of the shift for each of the two screw profiles to be fabricated is $VLR = VRR = 0.02$. In Figures 45a to 45d the direction of the shift for each of the two screw profiles to be fabricated is varied gradually between $VLW = VRW = 0$ and $VLW = VRW = \pi/2$. It is possible to shift the two

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screw profiles to be fabricated independently of each other in various directions and to different degrees.

Two-flight screw profiles generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention can be used for fabricating screw elements. In particular, such screw profiles can be used for fabricating conveying elements, mixing elements, kneading elements and transition elements.

Figure 46a depicts a pair of two-flight conveying elements based on the screw profile of Figure 26a. The barrel radius RG is 0.58. The clearance S between the two conveying elements is 0.02. The clearance D between the two conveying elements and the barrel is 0.01. The pitch T of the conveying elements is 1.2. The length of the conveying elements is 1.2, which corresponds to rotation of the screw profiles by an angle 2π . The barrel is depicted by thin unbroken lines on the left and the right of the two conveying elements. A possible computational grid is also depicted on the surfaces of the two conveying elements. This grid can be used for computing the flow in twin and multiple screw extruders.

Figure 46b depicts a pair of two-flight kneading elements based on the screw profile of Figure 26a. The barrel radius RG is 0.58. The clearance S between the kneading discs of the two kneading elements is 0.02. The clearance D between the kneading discs of the two kneading elements and the barrel is 0.01. The kneading element consists of 7 kneading discs which are each staggered in a clockwise direction in relation to each other by an angle $\pi/6$. The first and the last kneading disc each have a length of 0.09. The kneading discs in the middle each have a length of 0.18. The groove between the kneading discs has a length of 0.02. The barrel is depicted by thin, unbroken lines on the left and right of the two kneading elements. In addition, a possible computational grid is depicted on the surfaces of the two kneading elements. This grid can be used for computing the flow in twin and multiple screw extruders.

Figures 47 to 53 depict screw profiles with 3 flights which are generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention. Figures 47 to 49 each show a sixth of a screw profile with 3 flights. All of these

figures have an analogous design to that of Figures 1 to 20, which has already been described in detail for these figures.

Figures 47 to 53 depict screw profiles and screw elements in which the dimensionless outer screw radius RA has the values 0.5233, 0.53, 0.5333, 0.5433 and 0.5567. The method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights is not limited to these discrete values for the dimensionless outer screw radius. Using the method according to the invention it is possible to generate three-flight screw profiles with a dimensionless outer screw radius between RA greater than 0.5 and RA smaller than or equal to 0.577, and preferably in the range from $RA=0.51$ to $RA=0.57$.

Figure 47: Figures 47a and 47b depict preferred 2-circle screw profiles. Figures 47a and 47b differ in their outer screw radius RA . In Figure 47a the outer screw radius is $RA=0.5433$. In Figure 47b the outer screw radius RA is 0.5567. In Figures 47a and 47b the radius R_1 of arc 1 is dependent on the outer screw radius RA . In Figures 47a and 47b arc 1 has an angle $\alpha_1=\pi/6$.

Figure 48: Figures 48a and 48b depict preferred 4-circle screw profiles. Figures 48a and 48b differ in the outer screw radius RA . In Figure 48a the outer screw radius RA is 0.5433. In Figure 48b the outer screw radius RA is 0.5567. In each of Figures 48a and 48b arc 1 has a radius $R_1=RA$. In each of Figures 48a and 48b arc 2 has a radius $R_2=0$. In Figures 48a and 48b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 48a and 48b the angle α_2 of arc 2 is dependent on the outer screw radius RA .

Figure 49: Figures 49a and 49b depict additional preferred 4-circle screw profiles. Figures 49a and 49b differ in the outer screw radius RA . In Figure 49a the outer screw radius RA is 0.5433. In Figure 49b the outer screw radius RA is 0.5567. In Figures 49a and 49b arc 1 has a radius $R_1=0$. In Figures 49a and 49b arc 2 has a radius $R_2=A=1$. In Figures 49a and 49b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 49a and 49b angle α_2 of arc 2 is dependent on the outer screw radius RA .

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Figures 47 to 49 depict screw profiles which are designed similarly to Figures 1 to 3 for one-flight screw profiles. Figures 47 to 49 depict screw profiles which are designed analogously to Figures 25 to 27 for two-flight screw profiles. The single- and two-flight

screw profiles depicted in Figures 4 to 19 and in Figures 28 to 42 can be applied analogously to three-flight screw profiles. It is thus possible to adjust the size of the tip region in many ways, even in three-flight screw profiles. Depending on the type of transition used between the flank and tip regions of the screw profile the ratios between the
5 elongating and shear forces acting on the viscous fluid can be adjusted in the same way as in one-flight and two-flight screw profiles.

Figures 50 to 52 depict the generating and the generated screw profile inside a figure 8-shaped screw barrel. All of these figures have a design analogous to that of Figures 21 to
10 23, which has already been described in detail in relation to these figures. The numerical values inside the screw profiles have also already been explained in connection with Figures 21 to 23.

Figure 50: Figures 50a to 50d depict preferred variants of eccentrically positioned three-
15 flight screw profiles. The depicted tightly intermeshing, self-cleaning screw profiles are based on Figure 48, although the outer screw radius RA is 0.53 in Figures 50a to 50d. The virtual barrel radius RV is 0.53 and is smaller than the barrel radius RG ($RG=0.63$). The remaining geometrical parameters can be found in the individual figures. Eccentrically positioned, three-flight, tightly intermeshing, self-cleaning screw profiles are characterized
20 in that the distance between the screw profiles and the barrel is always identical for both screw profiles, independently of the direction of shift. In each of Figures 50a to 50d the screw profiles have been shifted to such an extent that precisely one point in the screw profiles touches the barrel. The degree of the shift required for this purpose depends on the direction of the shift. It is also possible for the screw profiles to be in eccentric positions in
25 which no point of the screw profiles touches the barrel.

Figure 51: As is well-known to those skilled in the art, all screw elements require a certain degree of clearance in practice, not only between each other but also in relation to the barrel. As is well-known to those skilled in the art and as can be read on pages 28 to 30
30 and pages 99 to 105 of book [1], clearances can be obtained, inter alia, by the methods of increasing the centre distance, by longitudinal equidistant clearance or three-dimensional equidistant clearance. Usually the clearance around the periphery of the screw profiles is constant. It is however also possible for the clearance to be varied around the periphery of

the screw profile. Figures 51a to 51d depict various clearance strategies. The depicted tightly intermeshing self-cleaning screw profiles are based on Figure 48a. The remaining geometrical parameters can be found in the individual figures. Figure 51a depicts a clearance strategy in which the clearance is identical between the screw profiles to be fabricated and between the screw profiles to be fabricated and the barrel. Figure 51b depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is smaller than the clearance between the screw profiles to be fabricated and the barrel. Figure 51c depicts a clearance strategy in which the clearance between the screw profiles to be fabricated is larger than the clearance between the screw profiles to be fabricated and the barrel. Figure 51d depicts an additional variant according to Figure 51c with particularly large clearances. Typical clearances occurring in practice for the clearance between the screw profiles to be fabricated are in the range from 0.002 to 0.1. Typical clearances occurring in practice for the clearance between the screw profiles to be fabricated and the barrel are in the range from 0.002 to 0.1. Typical clearances occurring in practice are constant around the periphery of the screw profile. It is however possible to vary around the periphery of the screw profiles not only the clearance between the screw profiles to be fabricated but also the clearance between the screw profiles to be fabricated and the barrel.

Figure 52: It is also possible to shift the screw profiles to be fabricated within the clearances. Figures 52a to 52d depict a selection of possible shifts. The depicted, tightly intermeshing, self-cleaning screw profiles are based on Figure 48a. The depicted screw profiles to be fabricated are based on Figure 51d. The remaining geometrical parameters can be found in the individual figures. In Figures 52a to 52d the degree of the shift for both screw profiles to be fabricated is $VLR = VRR = 0.02$. In Figures 52a to 52d the direction of the shift for both screw profiles to be fabricated is gradually varied between $VLW = VRW = 0$ and $VLW = VRW = \pi/3$. It is possible to shift the two screw profiles to be fabricated independently of each other in various directions and to different degrees.

Three-flight screw profiles generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention can be used for fabricating screw elements. In particular, such screw profiles can be used for fabricating conveying elements, mixing elements, kneading elements and transition elements.

Figure 53a depicts a pair of three-flight conveying elements based on the screw profile of Figure 48a. The barrel radius RG is 0.5433. The clearance S between the two conveying elements is 0.02. The clearance D between the two conveying elements and the barrel is 0.01. The pitch T of the conveying elements is 1.8. The length of the conveying elements is 1.2, which corresponds to rotation of the screw profiles by an angle of 1.3333π . The barrel is depicted by thin, unbroken lines on the left and the right of the two conveying elements. A possible computational grid is also depicted on the surfaces of the two conveying elements, which can be used for computing the flow in twin and multiple screw extruders.

Figure 53b depicts a pair of three-flight kneading elements based on the screw profile of Figure 48a. The barrel radius RG is 0.5433. The clearance S between the kneading discs of the two kneading elements is 0.02. The clearance D between the kneading discs of the two kneading elements and the barrel is 0.01. The kneading element consists of 7 kneading discs each staggered in a clockwise direction in relation to each other by an angle of $\pi/9$. The first and the last kneading discs have a length of 0.09. The kneading discs in the middle have a length of 0.18. The groove between the kneading discs has a length of 0.02. The barrel is depicted by thin, unbroken lines on the left and the right of the two kneading elements. In addition, a possible computational grid is depicted on the surfaces of the two kneading elements. This grid can be used for computing the flow in twin and multiple screw extruders.

Figures 54 to 60 describe screw profiles with 4 flights which are generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention. Figures 54 to 56 each depict an eighth of a screw profile with 4 flights. All of these figures have an analogous design to that of Figures 1 to 20, which has already been described in detail for these figures.

Figures 54 to 60 depict screw profiles and screw elements in which the dimensionless outer screw radius RA has the values 0.5083, 0.515, 0.5183, 0.5217 and 0.5283. The method according to the invention for generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with z flights is not limited to these discrete values for the

dimensionless outer screw radius. Using the method according to the invention, four-flight screw profiles can be generated with a dimensionless outer screw radius between RA greater than 0.5 and RA smaller than or equal to 0.541, and preferably in the range from $RA=0.505$ to $RA=0.536$.

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Figure 54: Figures 54a and 54b display preferred 2-circle screw profiles. Figures 54a and 54b differ in their outer screw radius RA . In Figure 54a the outer screw radius RA is 0.5217. In Figure 54b the outer screw radius RA is 0.5283. In Figures 54a and 54b radius R_1 of arc 1 is dependent on the outer screw radius RA . In each of Figures 54a and 54b arc 1 has an angle $\alpha_1=\pi/8$.

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Figure 55: Figures 55a and 55b depict preferred 4-circle screw profiles. Figures 55a and 55b differ in the outer screw radius RA . In Figure 55a the outer screw radius RA is 0.5217. In Figure 55b the outer screw radius RA is 0.5283. In each of Figures 55a and 55b arc 1 has a radius $R_1=RA$. In each of Figures 55a and 55b arc 2 has a radius $R_2=0$. In Figures 55a and 55b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 55a and 55b the angle α_2 of arc 2 is dependent on the outer screw radius RA .

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Figure 56: Figures 56a and 56b depict additional preferred 4-circle screw profiles. Figures 56a and 56b differ in their outer screw radius RA . In Figure 56a the outer screw radius RA is 0.5217. In Figure 56b the outer screw radius RA is 0.5283. In Figures 56a and 56b arc 1 has a radius $R_1=0$. In Figures 56a and 56b arc 2 has a radius $R_2=A=1$. In Figures 56a and 56b angle α_1 of arc 1 is dependent on the outer screw radius RA . In Figures 56a and 56b the angle α_2 of arc 2 is dependent on the outer screw radius RA .

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Figures 54 to 56 show screw profiles which are designed analogously to Figures 1 to 3 for one-flight screw profiles. Figures 54 to 56 show screw profiles which are designed analogously to Figures 25 to 27 for two-flight screw profiles. Figures 54 to 56 show screw profiles which are designed analogously to Figures 47 to 49 for three-flight screw profiles. The one- and two-flight screw profiles shown in Figures 4 to 19 and in Figures 28 to 42 can be applied analogously to four-flight screw profiles. Thus the size of the tip region can also be adjusted in many different ways for four-flight screw profiles. Depending on the type of transition between the flank and tip region of the screw profile, the ratio between

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the elongating and shear forces acting on the viscous fluid can be adjusted in the same way as in the one-flight, two-flight and three-flight screw profiles.

As is clear from Figures 1 to 20, Figures 25 to 42, Figures 47 to 49 and Figures 54 to 56 the
5 centre points of the arcs of the second part of a z -flight section of a screw profile can be obtained in a particularly simple manner by shifting the straight line FP to the origin of the coordinates and by mirroring the centre points of the arcs of the first part of this screw profile section on the opposite side of the shifted straight line FP . In said figures the slope of the straight line FP is 0 for a number of flights $z=1$ and $-1/\tan(\pi/(2z))$ for a number of
10 flights $z>1$, wherein π is pi.

Figures 57 to 59 show the generating and the generated screw profile inside a figure8-shaped screw barrel. All of these figures have an analogous design to that of Figures 21 to 23, which has already been described in detail for these figures. The numerical values
15 inside the screw profiles have also already been described in connection with Figures 21 to 23.

Figure 57: Figures 57a to 57d show preferred variants of eccentrically positioned four-flight screw profiles. The tightly intermeshing self-cleaning screw profiles depicted are
20 based on Figure 55, although the outer screw radius RA is 0.515 in Figures 57a to 57d. The virtual barrel radius RV is 0.515 and is smaller than the barrel radius RG ($RG=0.63$). The remaining geometrical parameters can be found in the individual figures. Eccentrically positioned, four-flight, tightly intermeshing, self-cleaning screw profiles are characterized in that the distance between the screw profiles and the barrel varies in size depending on
25 the direction of the shift. In Figures 57a to 57c the screw profiles have in each case been shifted to such an extent that precisely one point in the lefthand screw profile touches the barrel. The degree of the shift necessary for this purpose depends on the direction of the shift. Figure 57d shows a special case in which the screw profiles are shifted in such a manner in degree and direction that both screw profiles touch the barrel at precisely one
30 point. This shift takes place at an angle of $\pi/8$. It is also possible for the screw profiles to be in eccentric positions in which no point of the screw profiles touches the barrel.

Figure 58: As is well-known to a person skilled in the art, all screw elements require a certain degree of clearance in practice, not only between each other but also in relation to the barrel. Figures 58a to 58d show different clearance strategies. The tightly intermeshing self-cleaning screw profiles depicted are based on Figure 55b. The remaining geometrical parameters can be found in the individual figures. Figure 58a shows a clearance strategy in which the clearance between the screw profiles to be fabricated is the same as the clearance between the screw profiles to be fabricated and the barrel. Figure 58b shows a clearance strategy in which the clearance between the screw profiles to be fabricated is smaller than the clearance between the screw profiles to be fabricated and the barrel. Figure 58c shows a clearance strategy in which the clearance between the screw profiles to be fabricated is greater than the clearance between the screw profiles to be fabricated and the barrel. Figure 58d shows another variant according to Figure 58c with particularly large clearances. Typical clearances used in practice are in the range from 0.002 to 0.1 for the clearance between the screw profiles to be fabricated. Typical clearances used in practice for the clearances between the screw profiles to be fabricated and the barrel are in the range from 0.002 to 0.1. Typical clearances used in practice are constant around the periphery of the screw profile. It is however possible to vary around the periphery of the screw profiles both the clearance between the screw profiles to be fabricated and the clearance between the screw profiles to be fabricated and the barrel.

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Figure 59: It is also possible to shift the screw profiles to be fabricated within the clearances. Figures 59a to 59d show a selection of possible shifts. The tightly intermeshing, self-cleaning screw profiles depicted are based on Figure 55b. The depicted screw profiles to be fabricated are based on Figure 58d. The remaining geometrical parameters can be found in the individual figures. In each of Figures 59a to 59d the degree of shift of the two screw profiles to be fabricated is $VLR = VRR = 0.02$. In each of Figures 59a to 59d the direction of shift of the two screw profiles to be fabricated is varied gradually between $VLW = VRW = 0$ and $VLW = VRW = \pi/4$. It is possible to shift the two screw profiles to be fabricated independently of each other in various directions and to different degrees.

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Four-flight screw profiles generated by the method of generating tightly intermeshing, self-cleaning, co-rotating screw profiles according to the invention can be used for fabricating

screw elements. In particular, such screw profiles can be used for fabricating conveying elements, mixing elements, kneading elements and transition elements.

Figure 60a depicts a pair of four-flight conveying elements based on the screw profile according to Figure 55a. The barrel radius RG is 0.5217. The clearance S between the two conveying elements is 0.02. The clearance D between the two conveying elements and the barrel is 0.01. The pitch T of the conveying elements is 2.4. The length of the conveying elements is 1.2, which corresponds to a rotation of the screw profiles by an angle π . The barrel is depicted by thin unbroken lines on the right and left of the two conveying elements. A possible computational grid is also depicted on the surfaces of the two conveying elements which can be used for computing the flow in twin and multiple screw extruders.

Figure 60b depicts a pair of four-flight kneading elements based on the screw profile according to Figure 55a. The radius of the barrel RG is 0.5217. The clearance S between the kneading discs of the two kneading elements is 0.02. The clearance D between the kneading discs of the two kneading elements and the barrel is 0.01. The kneading element consists of 7 kneading discs each staggered in a clockwise direction in relation to each other at an angle of $\pi/12$. The first and the last kneading disc have a length of 0.09. The kneading discs in the middle have a length of 0.18. The groove between the kneading discs has a length of 0.02. The barrel is depicted by thin unbroken lines on the left and right of the two kneading elements. A possible computational grid is also depicted on the surfaces of the two kneading elements which can be used for computing the flow in twin and multiple screw extruders.

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Figures 62a and 62b illustrate a special feature of the concrete embodiment VK1 of the method according to the invention.

Figure 62a shows schematically the cross-sectional profiles of a pair of screw elements generated by the concrete embodiment VK1 of the method according to the invention. In this figure, the generating screw profile consists of the 5 arcs 1, 2, 3, 4 and 5, which are arranged counterclockwise around the centre of rotation (the origin of the x,y -coordinate system). The outer radius RA is selected to be $RA = 0.63$. The starting and centre points

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of the first arc 1 are positioned on the x -axis according to the concrete embodiment VK1 of the method according to the invention. The remaining arcs of the generating and the generated screw profiles are constructed on the basis of this first arc 1. Arc 5 closes the generating profile and, according to the invention, merges tangentially into arc 1. Arc 1 and arc 5 have the same centre point and the same radius. The corresponding arcs 1' and 5' of the generated screw profile which, according to the invention, can be constructed from arcs 1 and 5 of the generating screw profile, also have the same centre point and the same radius. Thus arcs 1 and 5 with angles α_1 and α_5 can be united to form an arc with an angle $\alpha_1 + \alpha_5$. The corresponding arcs 1' and 5' of the generated screw profile with angles $\alpha_{1'}$ and $\alpha_{5'}$ can also be united to form an arc with an angle $\alpha_{1'} + \alpha_{5'}$. The special feature that by using the embodiment VK1 screw profiles can be generated which can be subsequently "simplified" in the described manner is due to the fact that in VK1 the centre point and the starting point of the first arc is positioned on the x -axis. In the generation of the screw profiles according to the invention one point of contact between the generating and the generated screw profile is positioned on the x -axis. When the finished screw profiles (see Figure 62b) are rotated in the same direction about their respective centres of rotation the contact between them does however never occur at a point which is simultaneously located on the x -axis and is a starting or end point of a profile-generating arc. This is why, in the concrete embodiment VK1, an alternative solution is employed of dividing one arc into two arcs which, after being constructed, can be reunited to form one arc.

Figure 62b depicts the "simplified" construction of the cross-sectional profiles of Figure 62a, in which arcs 1 and 5 and 1' and 5' from Figure 62a are in each case united to form arcs 1 and 1' in Figure 62b.

The same applies to the concrete embodiment VK2.

In the figures depicted a maximum of 16 arcs are used for constructing a generating or a generated screw profile. The methods V0, VA1, VA2, VA3, VK1 and VK2 according to the invention are however by no means restricted to a maximum of 16 arcs. On the contrary, as many arcs as required can be used for producing screw profiles. It is thereby possible to design the profile of a screw from the outset in such a manner that it is optimally suitable for a specified task. The screw elements known from the prior art are in most cases not optimally designed for a concrete task. On the contrary, manufacturers

supply screw elements (conveying, kneading and mixing elements) from a fixed modular system independently of a concrete task. The present invention makes it possible for the first time to almost completely freely design the profiles of self-cleaning screw elements, thus optimizing the parameters of such profiles for the application concerned down to the most minute variation. In addition it is possible to approximate screw profiles which are not composed of arcs and are therefore not self-cleaning by means of a sufficiently high number of arcs with the required precision. The profile approximated by means of arcs is of course self-cleaning. It is possible to calculate the longitudinal profile of a (generating or generated) screw profile. Preferably each arc of a screw profile is used for calculating that part of the longitudinal cross-section which belongs to this arc by means of an explicit function.

In a first step the intersecting point (S_x, S_y) of a straight line g with an arc kb is determined. The straight line g is located in the plane of the screw profile and it leads through the point of rotation of the screw profile. The orientation of the straight line is given by the angle φ . Arc kb is characterized by its radius r and the position of its centre point

(M_x, M_y) . In a second step the distance of the point of intersection (S_x, S_y) from the point of rotation of the screw profile is calculated. The point of intersection of a straight line with an arc can be calculated by an explicit function. The same applies to the calculation of the distance. The distance is therefore $s=s(\varphi, r, M_x, M_y)$. Given a known pitch t of a screw element over $\varphi/2\pi \cdot t$, angle φ can be converted into an axial position z_{ax} , so that the distance is $s=s(z_{ax}, r, M_x, M_y)=s(\varphi/2\pi \cdot t, r, M_x, M_y)$. The function $s(z_{ax}, r, M_x, M_y)$ defines the longitudinal profile of an arc of the screw profile.

Claims

1. Method of generating planar, tightly intermeshing, self-cleaning, co-rotating screw profiles with a selectable centre distance a between the rotational axes of a generating and a generated screw profile, characterized in that the generating screw profile consists of n arcs and the generated screw profile consists of n' arcs, wherein
 - the generating screw profile and the generated screw profile lie in the same plane,
 - the axis of rotation of the generating screw profile and the axis of rotation of the generated screw profile are each vertical to said plane of the screw profiles, the point of intersection between the rotational axis of the generating screw profile and said plane being referred to as the point of rotation of the generating screw profile and the point of intersection of the rotational axis of the generated screw profile and said plane being referred to as the point of rotation of the generated screw profile,
 - the number of arcs n of the generating screw profile is selected such that n is an integer greater than or equal to 1,
 - the outer radius ra of the generating screw profile is selected such that ra is greater than 0 ($ra > 0$) and smaller than or equal to the centre distance ($ra \leq a$),
 - the inner radius ri of the generating screw profile is selected such that ri is greater than or equal to 0 ($ri \geq 0$) and smaller than or equal to ra ($ri \leq ra$),
 - the arcs of the generating screw profile are arranged according to the following configuration rules, such that:
 - o all of the arcs of the generating screw profile merge into each other tangentially in such a manner that a closed, convex screw profile is formed, an arc whose radius is 0 being treated in the same way as an arc whose radius is eps , which is a very small positive real number tending towards 0 ($eps < 1$, $eps \rightarrow 0$),
 - o each of the arcs of the generating screw profile is located within and/or on the boundaries of an annulus which has an outer radius ra and an inner radius ri and whose centre point is located on the point of rotation of the generating screw profile,
 - o at least one of the arcs of the generating screw profile touches the outer radius ra of the generating screw profile,
 - o at least one of the arcs of the generating screw profile touches the inner radius ri of the generating screw profile,

- the size of a first arc of the generating screw profile which is defined by an angle α_1 and a radius r_1 is selected such that angle α_1 is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π , wherein π is pi ($\pi \approx 3.14159$) and radius r_1 is greater than or equal to 0 and smaller than or equal to the centre distance a and the position of this first arc of the generating screw profile, which is obtained by positioning two different points of this first arc, is defined according to said configuration rules, wherein the first point of this first arc to be positioned is preferably the starting point of this first arc and wherein the second point of this first arc to be positioned is preferably the centre point of this first arc,
- the sizes of additional $n-2$ arcs of the generating screw profile, which are defined by angles $\alpha_2, \dots, \alpha_{(n-1)}$ and radii $r_2, \dots, r_{(n-1)}$ are selected such that angles $\alpha_2, \dots, \alpha_{(n-1)}$ are, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π and radii $r_2, \dots, r_{(n-1)}$ are greater than or equal to 0 and smaller than or equal to the centre distance a and the positions of these additional $n-2$ arcs of the generating screw profile are defined according to said configuration rules,
- the size of the last arc of the generating screw profile, which is defined by angle α_n and radius r_n , is such that the sum of the n angles of the n arcs of the generating screw profile is, in terms of radian measurement, 2π , wherein angle α_n is, in terms of radian measurement, greater than or equal to 0 and smaller than or equal to 2π , and radius r_n completes the generating screw profile, wherein radius r_n is greater than or equal to 0 and smaller than or equal to the centre distance a and the position of this last arc of the generating screw profile is defined according to said configuration rules,
- the n' arcs of the generated screw profile are based on the n arcs of the generating screw profile such that
 - the number of arcs n' of the generated screw profile is identical to the number of arcs n of the generating screw profile, wherein n' is an integer,
 - the outer radius ra' of the generated screw profile is equal to the centre distance minus the inner radius ri of the generating screw profile ($ra' = a - ri$),
 - the inner radius ri' of the generated screw profile is equal to the centre distance minus the outer radius ra of the generating screw profile ($ri' = a - ra$),

- angle $\alpha_{i'}$ of the i' th arc of the generated screw profile is the same as angle α_i of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($\alpha_1' = \alpha_1, \dots, \alpha_{n'}' = \alpha_n$),
- the sum of the radius $r_{i'}$ of the i' th arc of the generated screw profile and the radius r_i of the i th arc of the generating screw profile is equal to the centre distance a , wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ($r_1' + r_1 = a, \dots, r_{n'}' + r_n = a$),
- the distance between the centre point of the i' th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is the same as the centre distance a and the distance between the centre point of the i' th arc of the generated screw profile and the point of rotation of the generated screw profile is the same as the distance between the centre point of the i th arc of the generating screw profile and the point of rotation of the generating screw profile, and the connecting line between the centre point of the i' th arc of the generated screw profile and the centre point of the i th arc of the generating screw profile is a line parallel to the connecting line between the point of rotation of the generated screw profile and the point of rotation of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' ,
- the starting point of the i' th arc of the generated screw profile lies in relation to the centre point of the i' th arc of the generated screw profile in an opposite direction to that of the starting point of the i th arc of the generating screw profile in relation to the centre point of the i th arc of the generating screw profile, wherein i is an index which represents all integers in the range from 1 to the number of arcs n and i' is an index which represents all integers in the range from 1 to the number of arcs n' .

2. The method according to claim 1, characterized in that the outer screw radius ra of the generating screw profile is the same as the outer screw radius ra' of the generated screw profile and the inner radius ri of the generating screw profile is the same as the inner radius ri' of the generated screw profile.
- 5 3. The method according to claim 1, characterized in that
- the number of flights z is selected such that z is an integer greater than or equal to 1,
 - the number of arcs n of the generating screw profile is selected such that it is an integer multiple p of $4z$,
 - the generating screw profile is subdivided into $2z$ sections, which are characterized
- 10 in that
- each section is bounded by two straight lines which form an angle to each other, in terms of radian measurement, of π/z and intersect each other at the point of rotation of the generating screw profile, wherein these two straight lines are referred to as section boundaries, wherein π is pi ($\pi \approx 3.14159$),
 - 15 ○ each of these $2z$ sections is subdivided into a first and a second part,
 - the first part of a section is composed of p arcs which are numbered in ascending or descending order,
 - the angles $\alpha_1, \dots, \alpha_p$ belonging to the p arcs are selected such that the sum of these angles is $\pi/(2z)$, wherein angles $\alpha_1, \dots, \alpha_p$ are, in terms of
 - 20 radian measurement, greater than or equal to 0 and smaller than or equal to $\pi/(2z)$,
 - the second part of a section is composed of p' arcs which are numbered in reverse order to the arcs of the first part of a section, wherein p' is an integer which is the same as p ,
 - 25 ○ angles $\alpha_{p'}, \dots, \alpha_1'$ of the p' arcs are defined such that the angle $\alpha_{j'}$ of the j' th arc of the second part of a section is the same as the angle α_j of the j th arc of the first part of a section, wherein j is an index which represents all integers in the range from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p'
 - 30 $(\alpha_1' = \alpha_1, \dots, \alpha_{p'}' = \alpha_p)$,
 - the sum of the radius $r_{j'}$ of the j' th arc of the second part of a section and the radius r_j of the j th arc of the first part of a section is equal to the centre distance a , wherein j is an index which represents all integers in the range

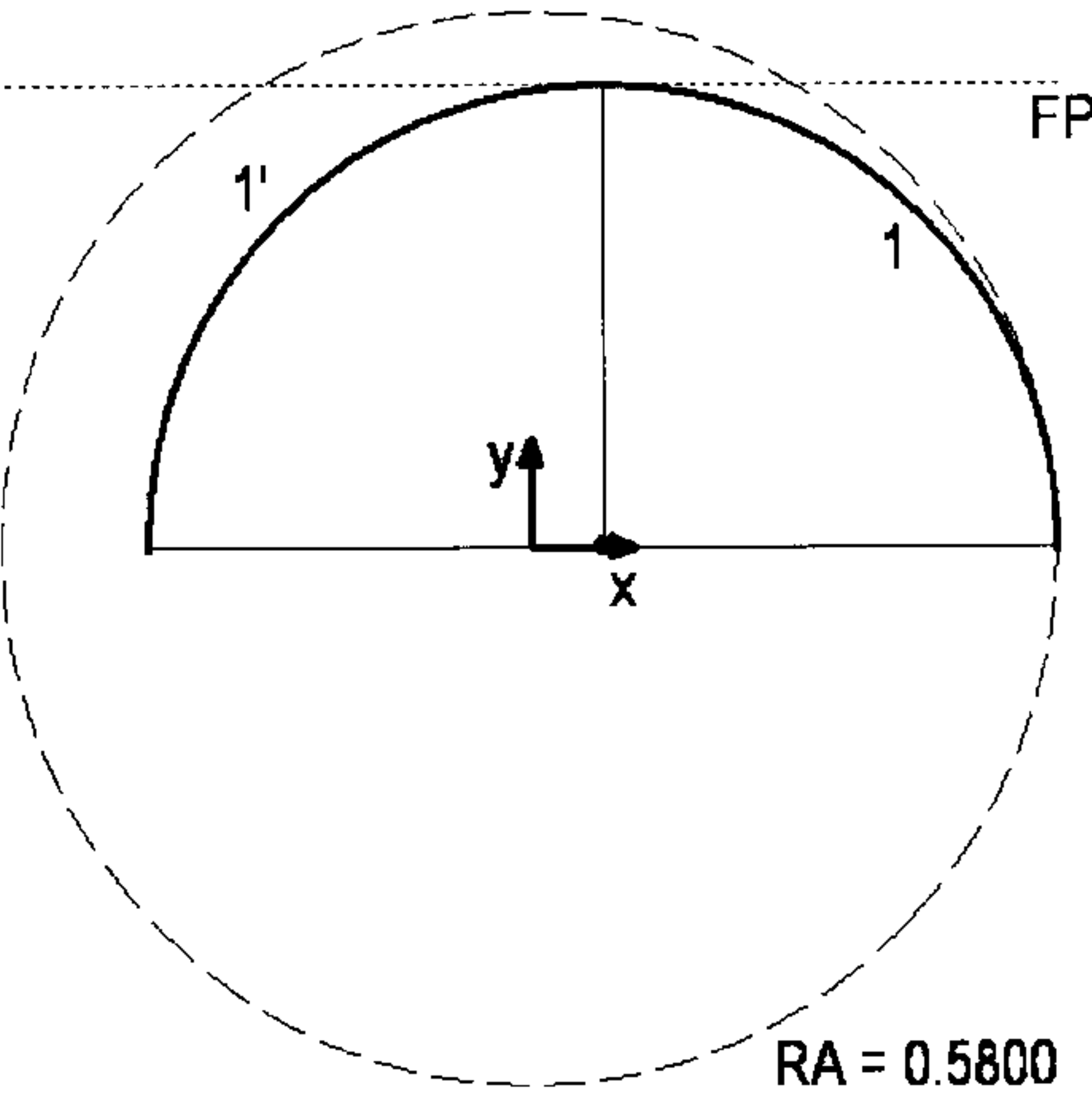
from 1 to the number of arcs p and j' is an index which represents all integers in the range from 1 to the number of arcs p' ($r_{1'}+r_1=a, \dots, r_{p'}+r_p=a$),

- 5 ○ the centre point and the starting point of the arc with which the screw profile begins in the first part of a section are positioned on one of the section boundaries of this section, the section boundary selected depending on whether the arcs are arranged in a clockwise or an anticlockwise direction,
- 10 ○ the end point of the arc with which the screw profile ends in the first part of a section touches a straight line FP at one point, the straight line FP being vertical to the angle bisector of the two section boundaries of this section and at a distance from the point of rotation of the generating screw profile in the direction of this section which is equal to half the centre distance, the angle bisector passing, in the same way as the section boundaries, through

15 the point of rotation of the generating screw profile.
- 4. The method according to claim 3, characterized in that one screw profile section is predefined in one of the $2z$ sections of the generating screw profile and the remaining screw profile sections are generated by successive mirroring of the predefined screw profile section about the section boundaries.
- 20 5. The method according to claims 2 to 4, characterized in that one-flight screw profiles are shifted along a section boundary.
- 6. The method according to claims 1 to 5, characterized in that the screw profiles are arranged eccentrically.
- 7. The method according to one of claims 1 to 6 for producing screw elements.
- 25 8. The method according to claim 7, wherein the screw elements are designed as mixing elements or conveying elements, characterized in that they rotate clockwise or anticlockwise and the pitch normalized in relation to the centre distance is in the range from 0.1 to 10 and the length of the elements normalized in relation to the centre distance is in the range from 0.1 to 10.
- 30 9. The method according to claim 7, wherein the screw elements are designed as kneading elements, characterized in that the kneading elements are arranged in a clockwise, anticlockwise or neutral manner and the length of the kneading discs normalized in relation to the centre distance is in the range from 0.05 to 10.

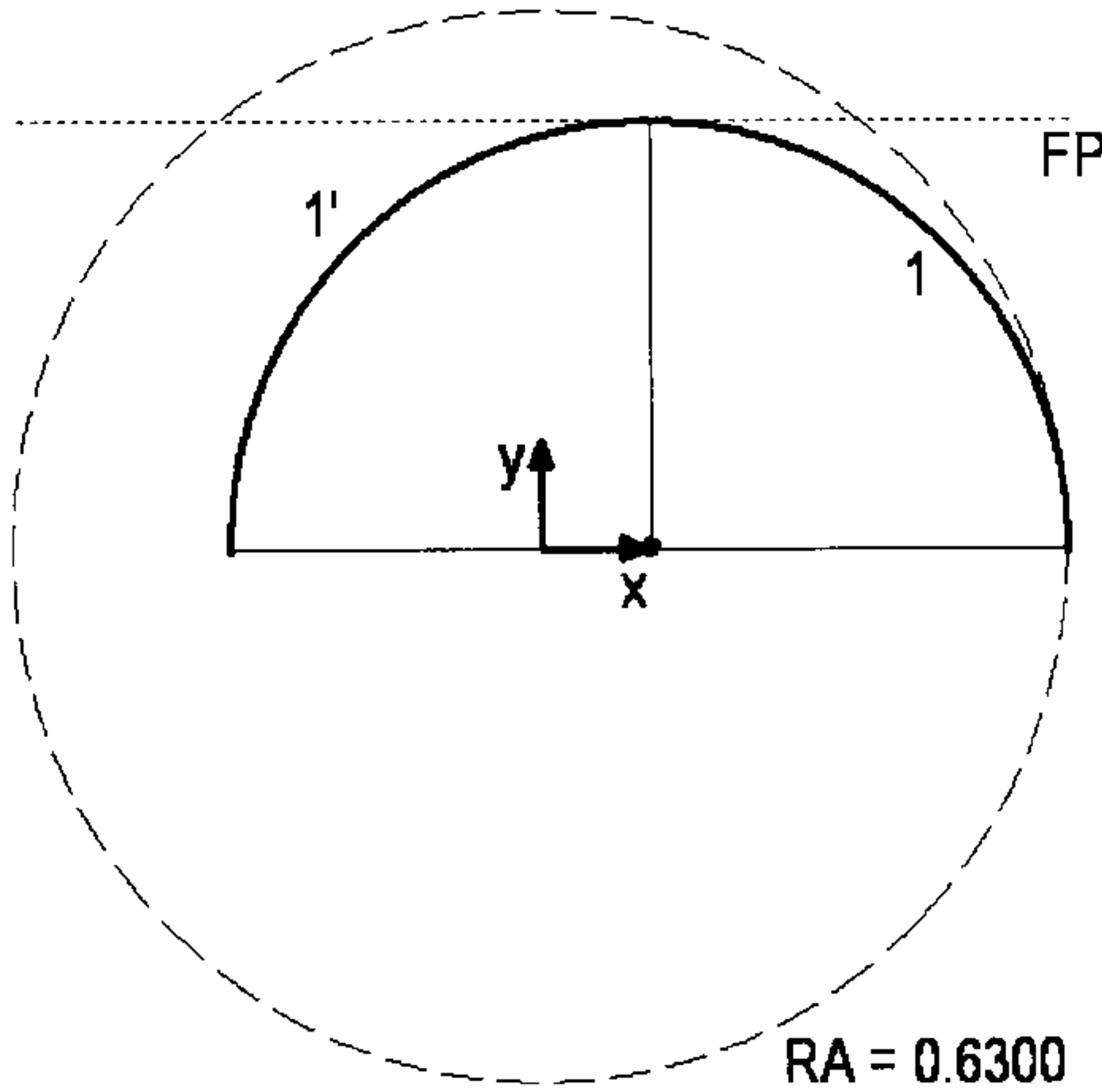
10. The method according to claim 7, characterized in that a transition element is generated in such a manner that the size and/or position of one or more arcs of a first generating screw profile or a first generated screw profile are gradually changed until they conform to the size and/or position of one or more arcs of a second generating screw profile or a second generated screw profile, characterized in that the transition element is clockwise or anticlockwise and the pitch normalized in relation to the centre distance is in the range from 0.1 to 10 and the length of the element normalized in relation to the centre distance is in the range from 0.1 to 10.
11. The method according to one of claims 7 to 10, characterized in that the screw elements have clearances, wherein the clearance between the screws is in the range from 0.002 to 0.1 times the centre distance and the clearance between the screw and the barrel is in the range from 0.002 to 0.1 times the centre distance.
12. The method according to claim 11, characterized in that the screw elements are shifted eccentrically within the clearances.
13. A computer program product with program code means which are stored in a computer-readable data carrier for executing the method according to one of claims 1 to 12 in a computer.
14. A computer program product according to claim 13, characterized in that the screw profiles are used for generating at least one computational grid on which the flow in twin and multiple screw extruders is computed, wherein the at least one computational grid depicts a conveying element, a mixing element, a kneading element or a transition element.
15. Screw elements which have been generated by a method according to one of claims 1 to 12.

Figures



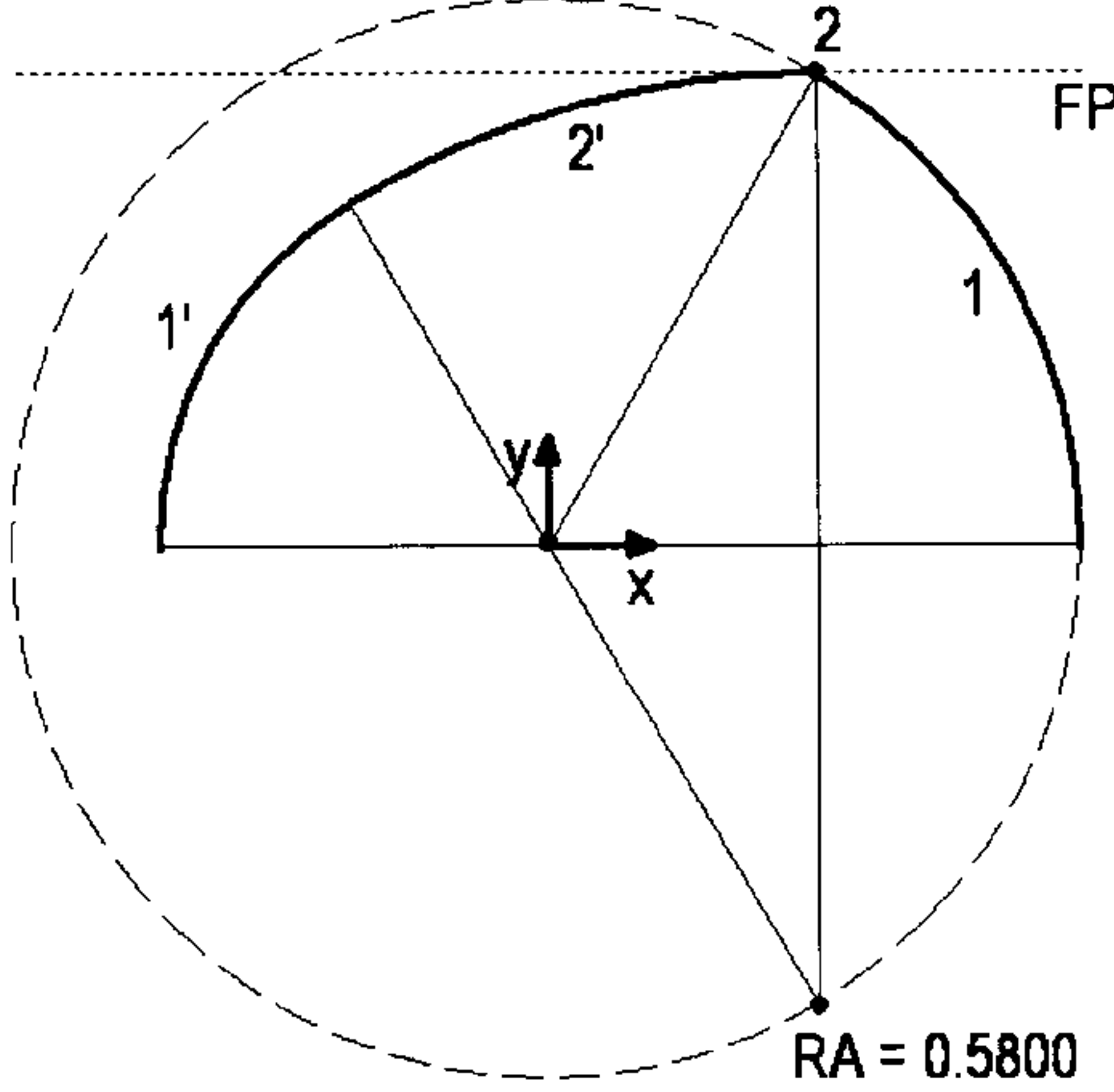
1) $R = 0.5000$ $M_x = 0.0800$
 $\alpha = 1.5708$ $M_y = 0.0000$
1') $R = 0.5000$ $M_x = 0.0800$
 $\alpha = 1.5708$ $M_y = -0.0000$

Figure 1a



1) $R = 0.5000$ $M_x = 0.1300$
 $\alpha = 1.5708$ $M_y = 0.0000$
1') $R = 0.5000$ $M_x = 0.1300$
 $\alpha = 1.5708$ $M_y = -0.0000$

Figure 1b



1) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 1.0393$ $M_y = 0.0000$
2) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
2') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
1') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 1.0393$ $M_y = 0.0000$

Figure 2a

- 2 -

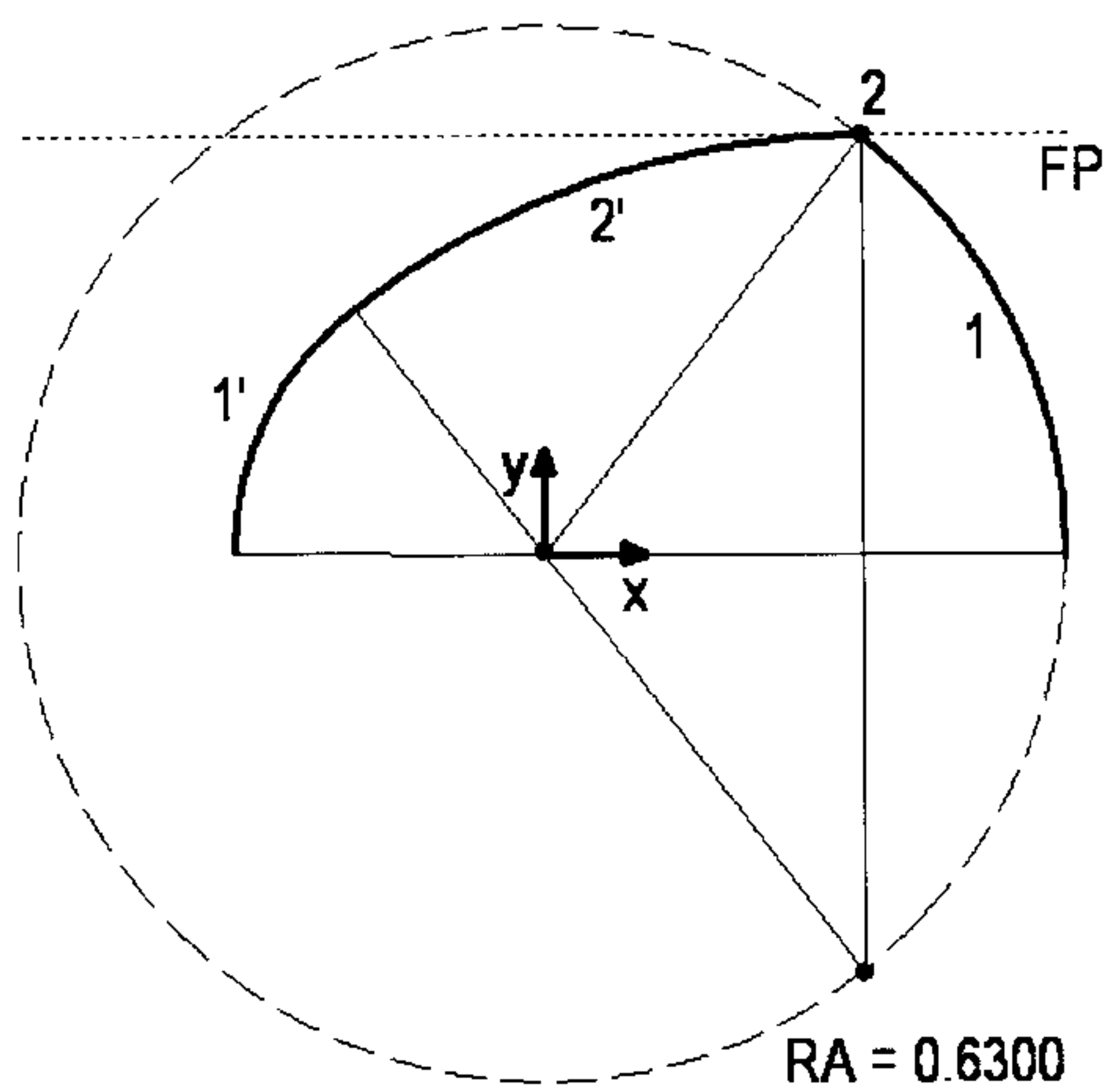


Figure 2b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.6300$ | $Mx = 0.0000$ |
| | $\alpha = 0.9168$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.3833$ |
| | $\alpha = 0.6540$ | $My = 0.5000$ |
| 2') | $R = 1.0000$ | $Mx = 0.3833$ |
| | $\alpha = 0.6540$ | $My = -0.5000$ |
| 1') | $R = 0.3700$ | $Mx = 0.0000$ |
| | $\alpha = 0.9168$ | $My = 0.0000$ |

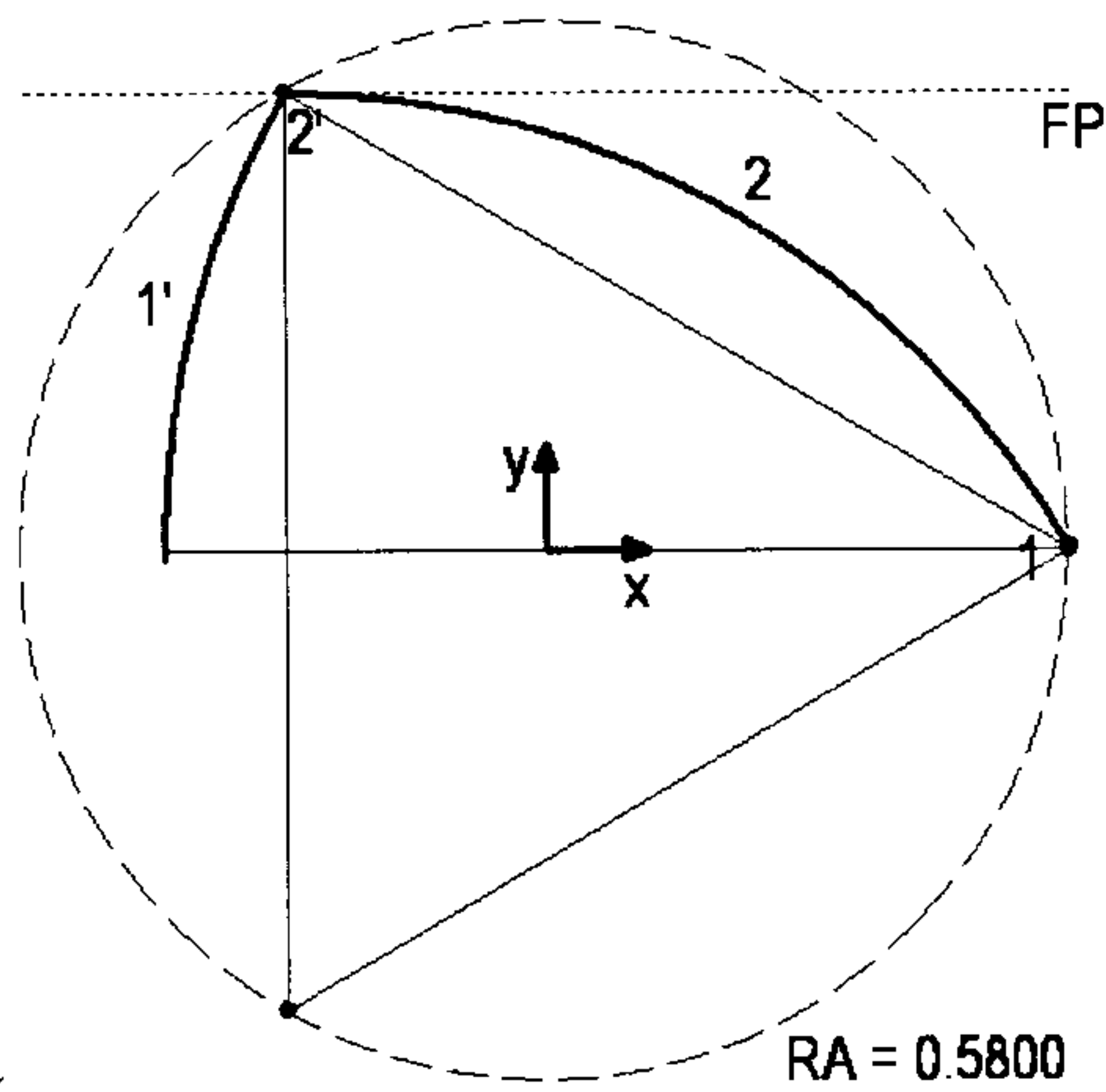


Figure 3a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.5800$ |
| | $\alpha = 0.5236$ | $My = 0.0000$ |
| 2) | $R = 1.0000$ | $Mx = -0.2860$ |
| | $\alpha = 1.0472$ | $My = -0.5000$ |
| 2') | $R = 0.0000$ | $Mx = -0.2860$ |
| | $\alpha = 1.0472$ | $My = 0.5000$ |
| 1') | $R = 1.0000$ | $Mx = 0.5800$ |
| | $\alpha = 0.5236$ | $My = -0.0000$ |

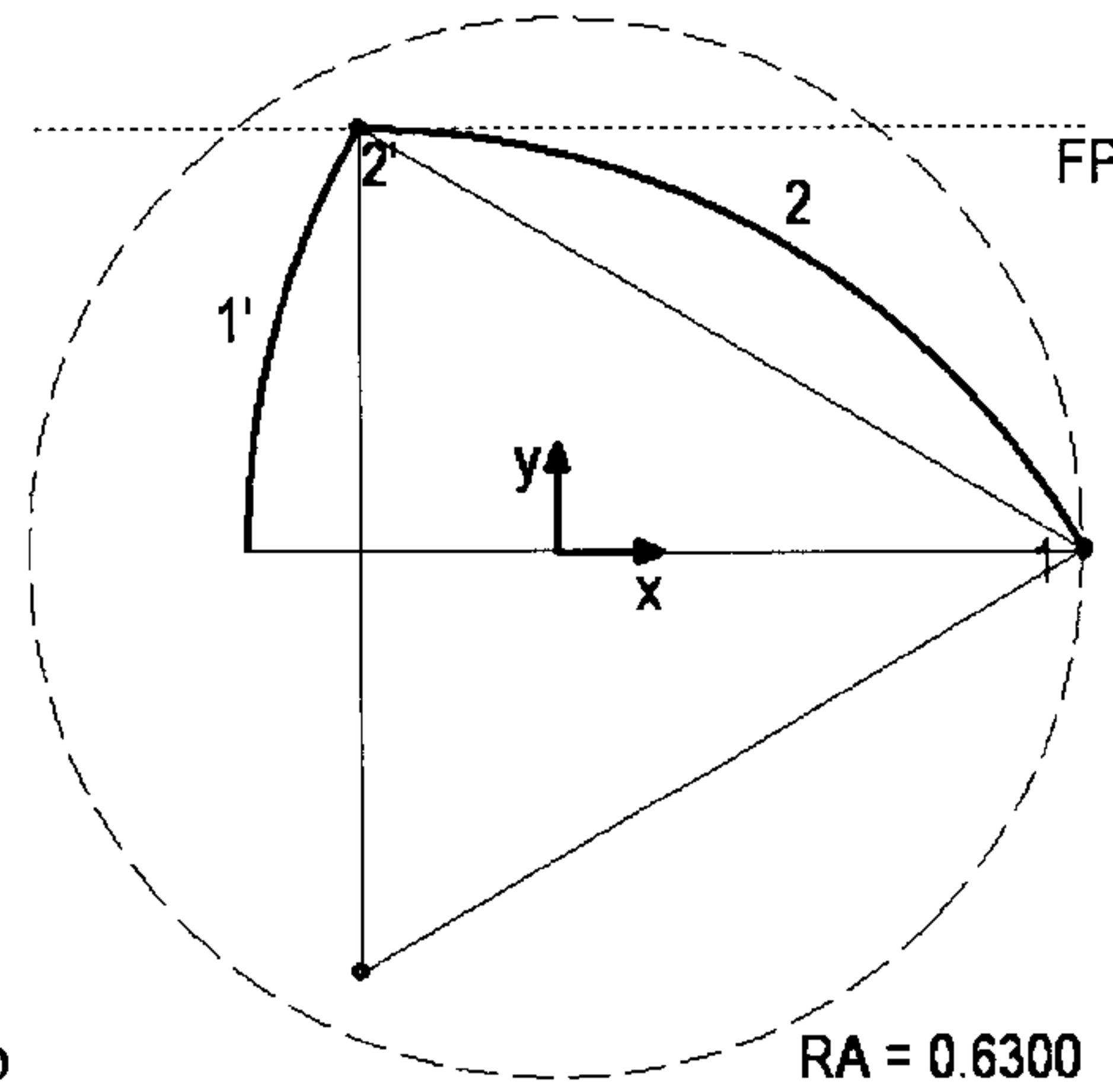


Figure 3b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.5236$ | $My = 0.0000$ |
| 2) | $R = 1.0000$ | $Mx = -0.2360$ |
| | $\alpha = 1.0472$ | $My = -0.5000$ |
| 2') | $R = 0.0000$ | $Mx = -0.2360$ |
| | $\alpha = 1.0472$ | $My = 0.5000$ |
| 1') | $R = 1.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.5236$ | $My = -0.0000$ |

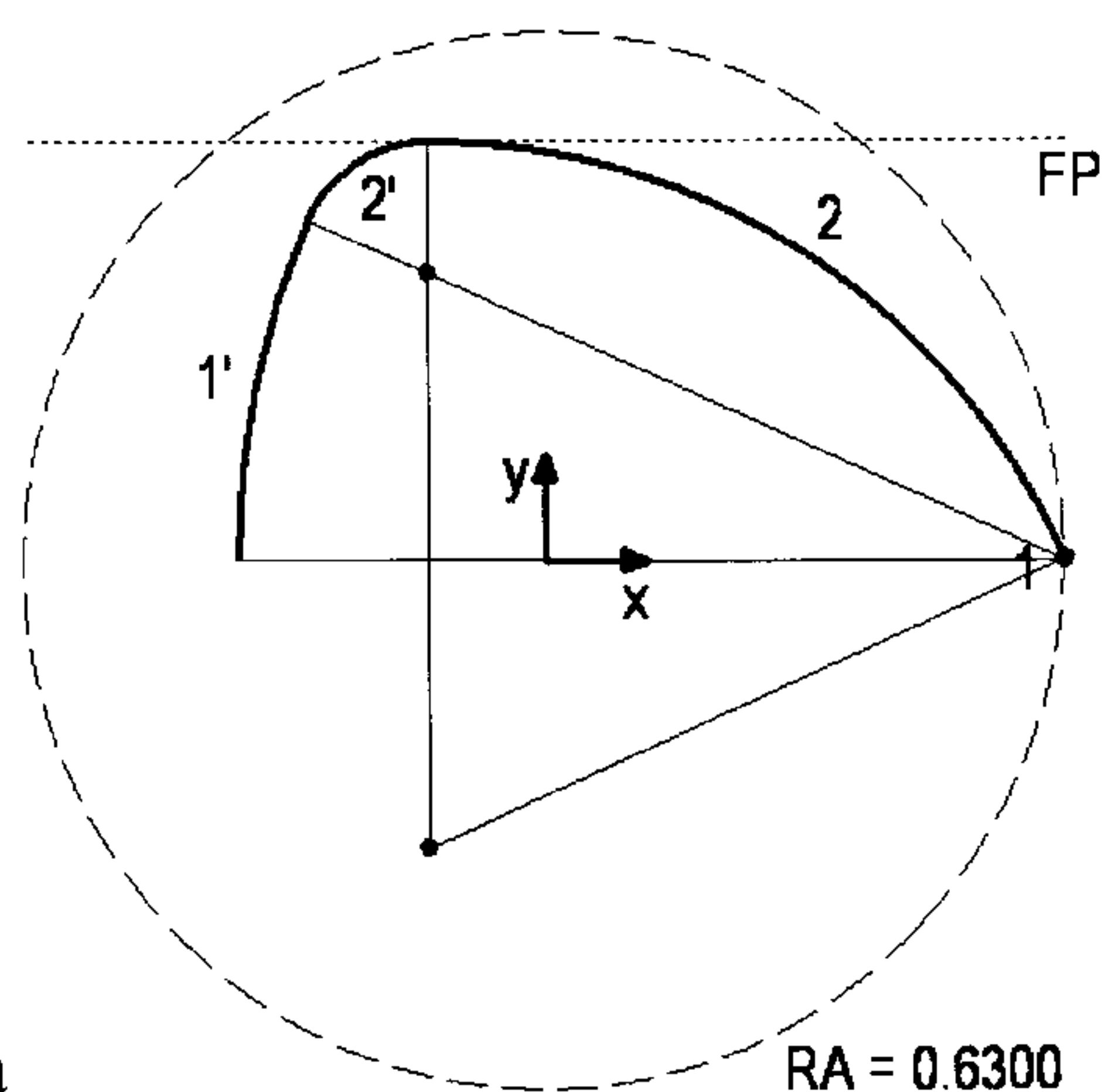


Figure 4a

- 1) $R = 0.0000$ $Mx = 0.6300$
 $\alpha = 0.4189$ $My = 0.0000$
- 2) $R = 0.8428$ $Mx = -0.1399$
 $\alpha = 1.1519$ $My = -0.3428$
- 2') $R = 0.1572$ $Mx = -0.1399$
 $\alpha = 1.1519$ $My = 0.3428$
- 1') $R = 1.0000$ $Mx = 0.6300$
 $\alpha = 0.4189$ $My = -0.0000$

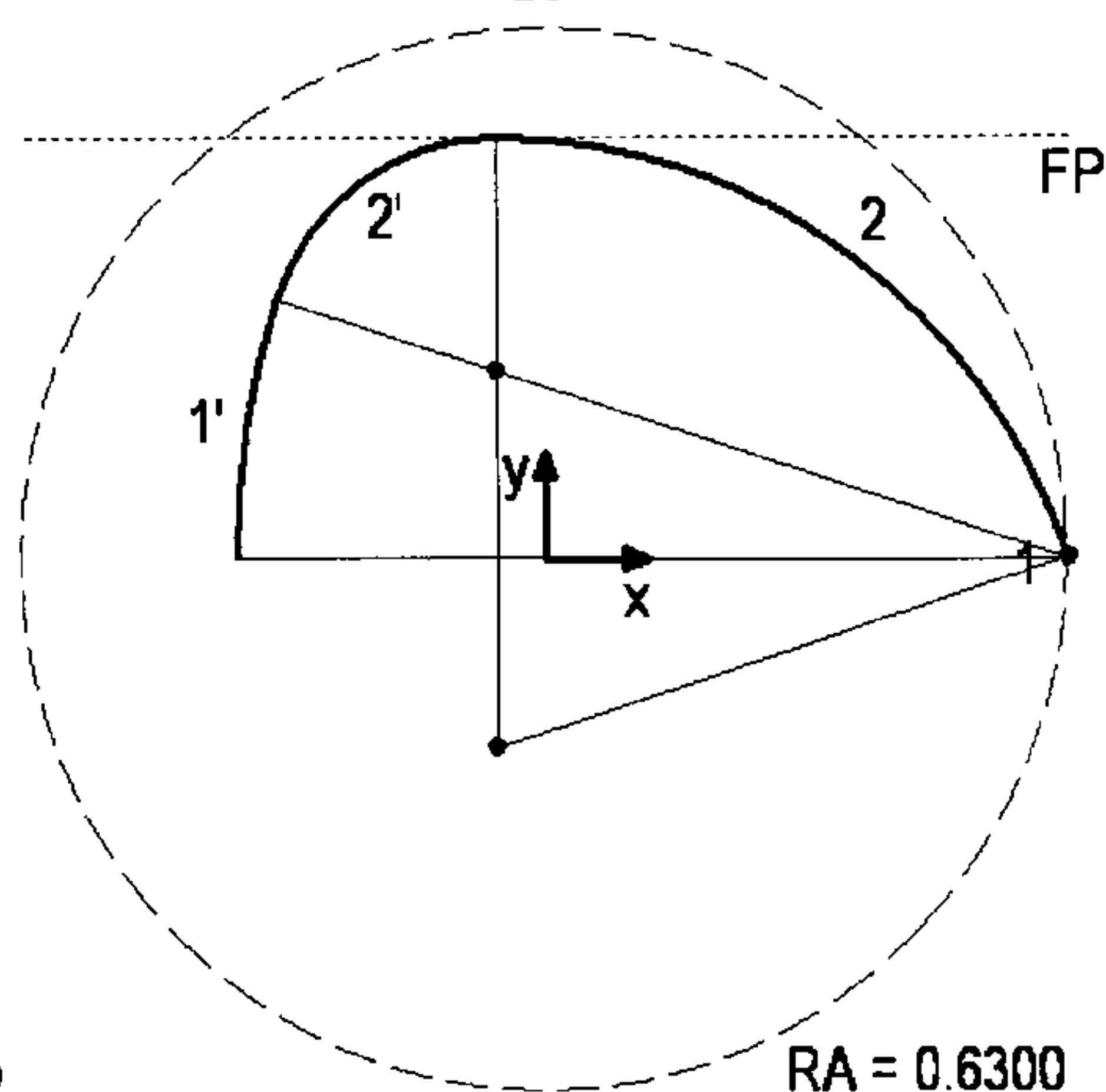


Figure 4b

- 1) $R = 0.0000$ $Mx = 0.6300$
 $\alpha = 0.3142$ $My = 0.0000$
- 2) $R = 0.7236$ $Mx = -0.0582$
 $\alpha = 1.2566$ $My = -0.2236$
- 2') $R = 0.2764$ $Mx = -0.0582$
 $\alpha = 1.2566$ $My = 0.2236$
- 1') $R = 1.0000$ $Mx = 0.6300$
 $\alpha = 0.3142$ $My = -0.0000$

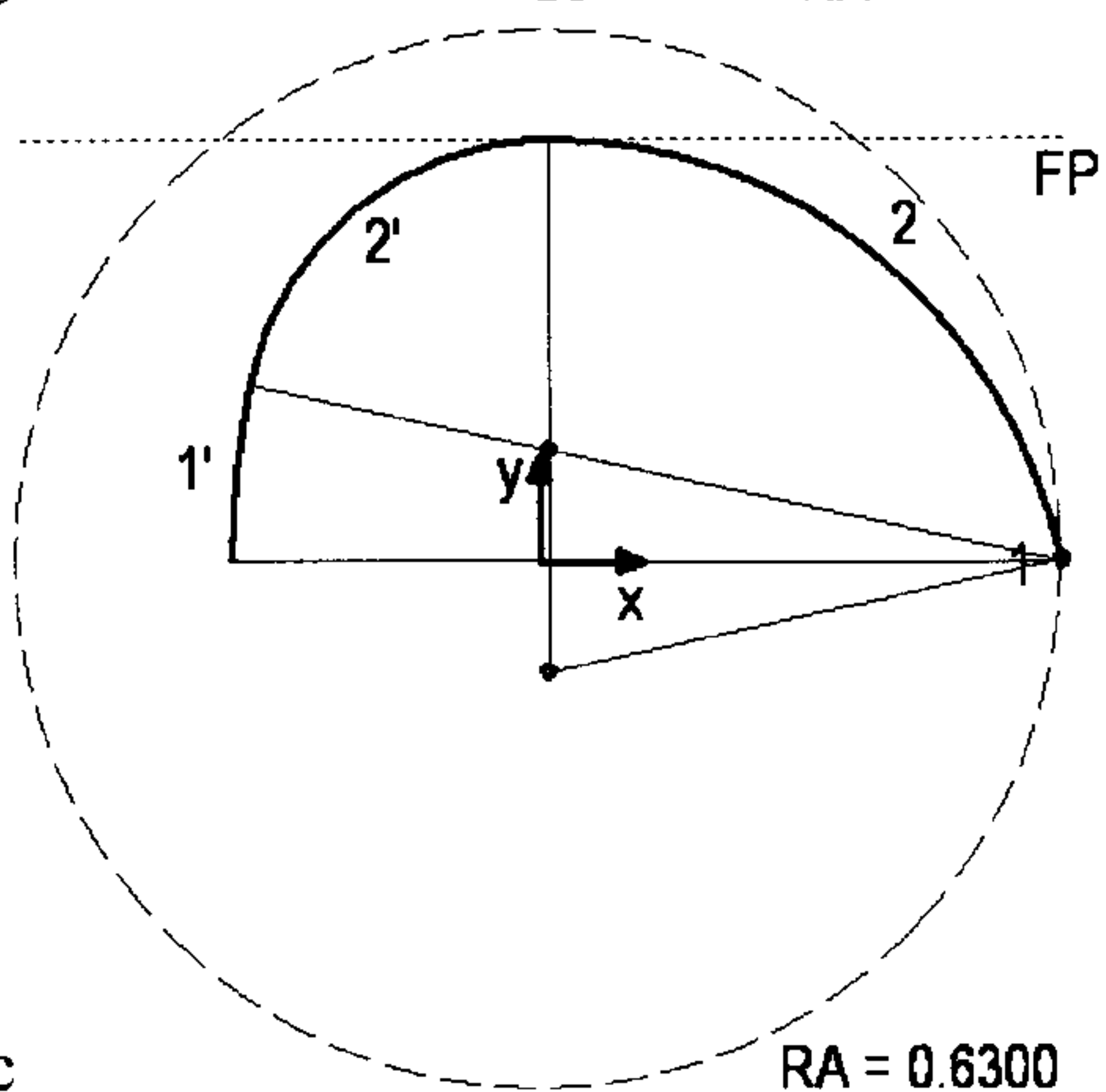


Figure 4c

- 1) $R = 0.0000$ $Mx = 0.6300$
 $\alpha = 0.2094$ $My = 0.0000$
- 2) $R = 0.6312$ $Mx = 0.0126$
 $\alpha = 1.3614$ $My = -0.1312$
- 2') $R = 0.3688$ $Mx = 0.0126$
 $\alpha = 1.3614$ $My = 0.1312$
- 1') $R = 1.0000$ $Mx = 0.6300$
 $\alpha = 0.2094$ $My = -0.0000$

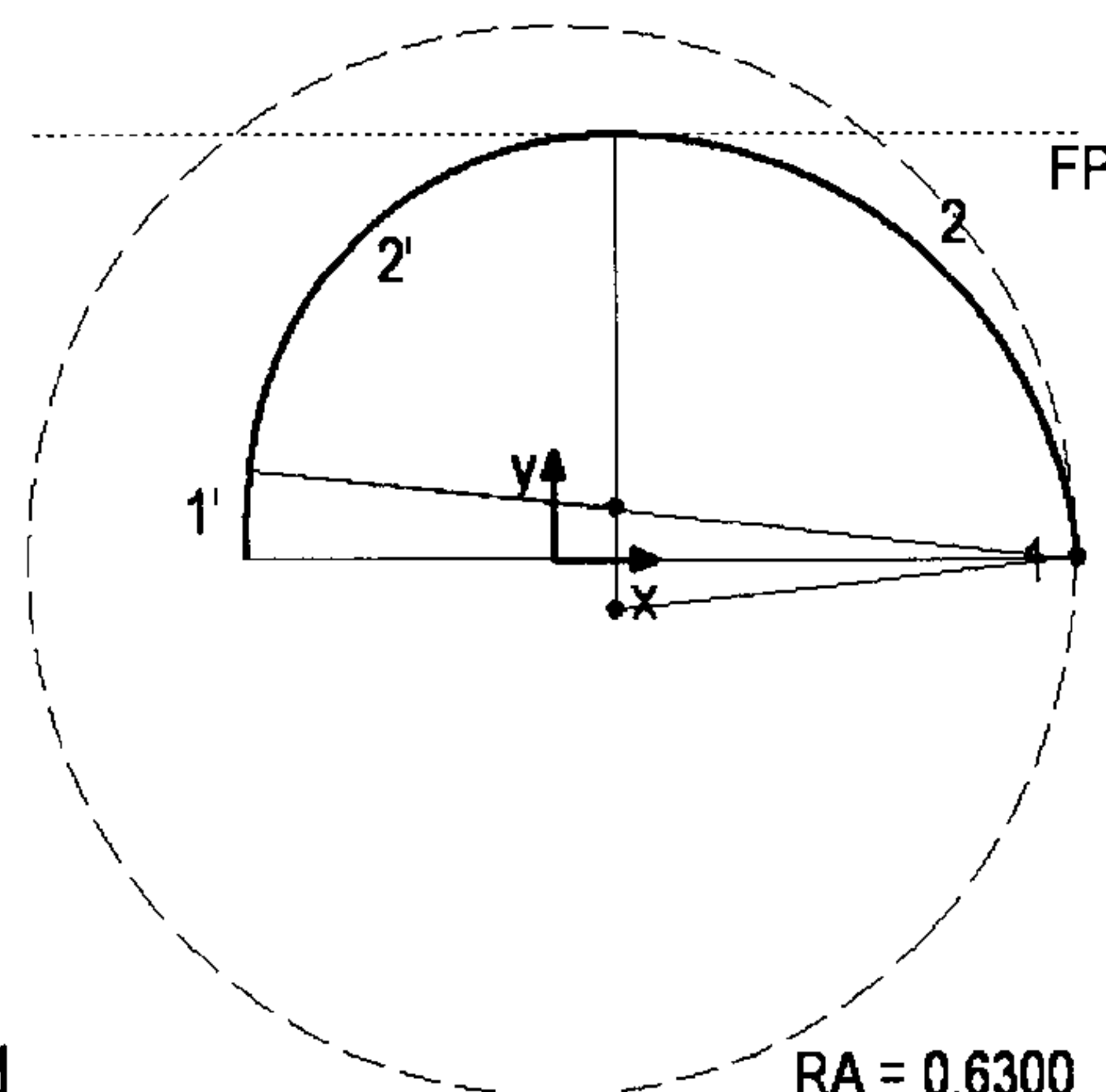


Figure 4d

- 1) $R = 0.0000$ $Mx = 0.6300$
 $\alpha = 0.1047$ $My = 0.0000$
- 2) $R = 0.5584$ $Mx = 0.0747$
 $\alpha = 1.4661$ $My = -0.0584$
- 2') $R = 0.4416$ $Mx = 0.0747$
 $\alpha = 1.4661$ $My = 0.0584$
- 1') $R = 1.0000$ $Mx = 0.6300$
 $\alpha = 0.1047$ $My = -0.0000$

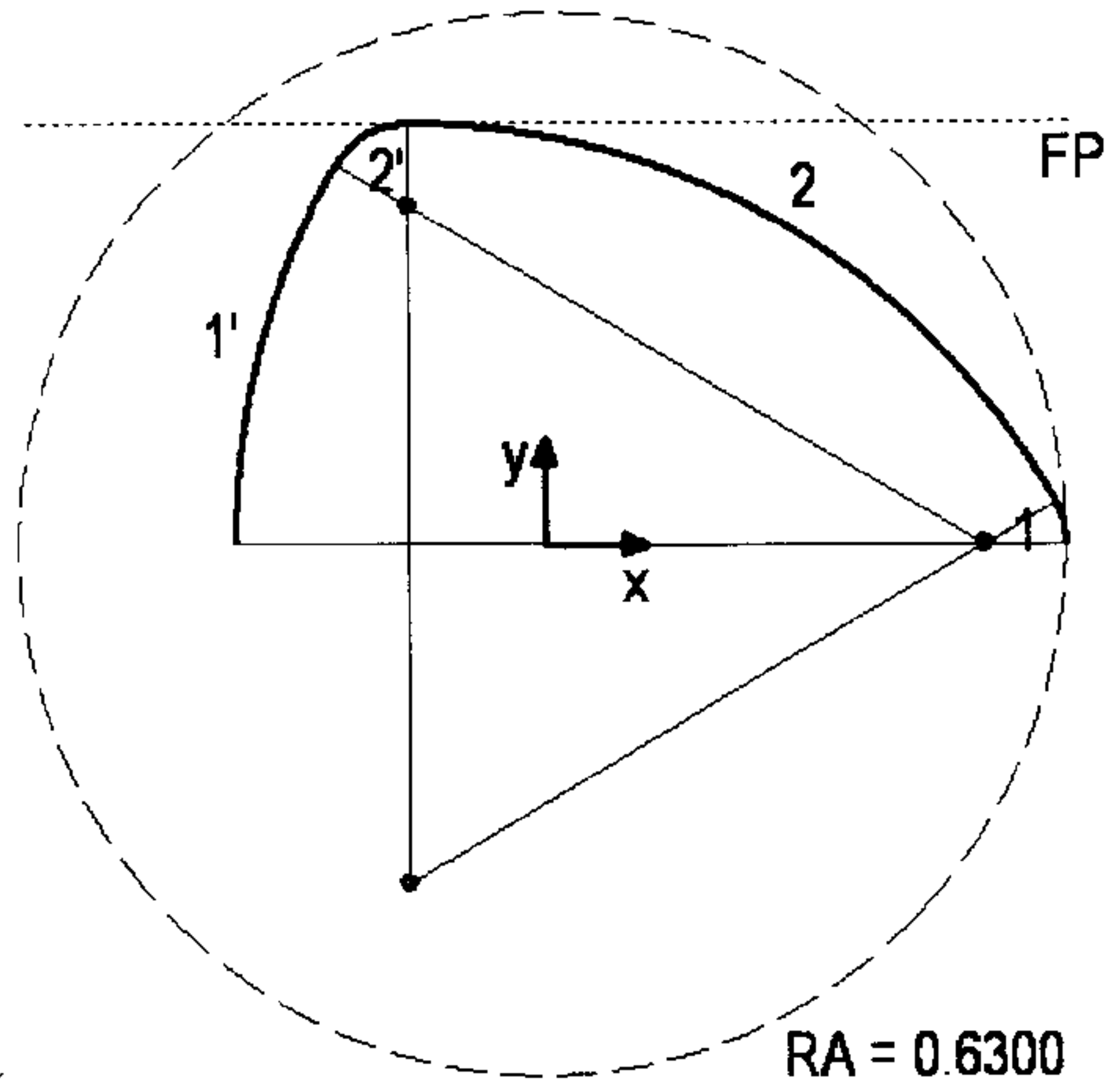


Figure 5a

- 1) $R = 0.1000$ $M_x = 0.5300$
 $\alpha = 0.5236$ $M_y = 0.0000$
 2) $R = 0.9000$ $M_x = -0.1628$
 $\alpha = 1.0472$ $M_y = -0.4000$
 2') $R = 0.1000$ $M_x = -0.1628$
 $\alpha = 1.0472$ $M_y = 0.4000$
 1') $R = 0.9000$ $M_x = 0.5300$
 $\alpha = 0.5236$ $M_y = -0.0000$

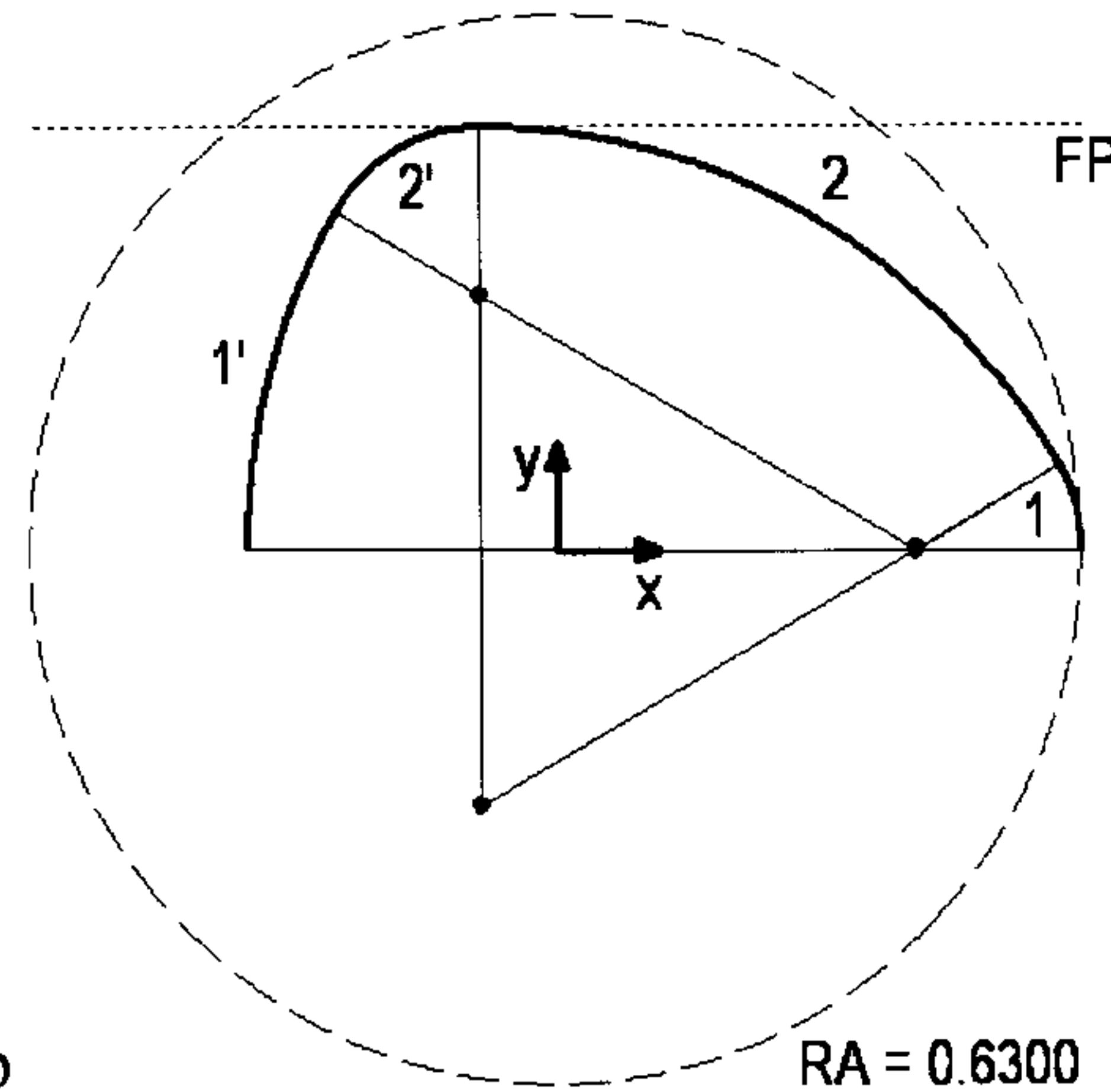


Figure 5b

- 1) $R = 0.2000$ $M_x = 0.4300$
 $\alpha = 0.5236$ $M_y = 0.0000$
 2) $R = 0.8000$ $M_x = -0.0896$
 $\alpha = 1.0472$ $M_y = -0.3000$
 2') $R = 0.2000$ $M_x = -0.0896$
 $\alpha = 1.0472$ $M_y = 0.3000$
 1') $R = 0.8000$ $M_x = 0.4300$
 $\alpha = 0.5236$ $M_y = -0.0000$

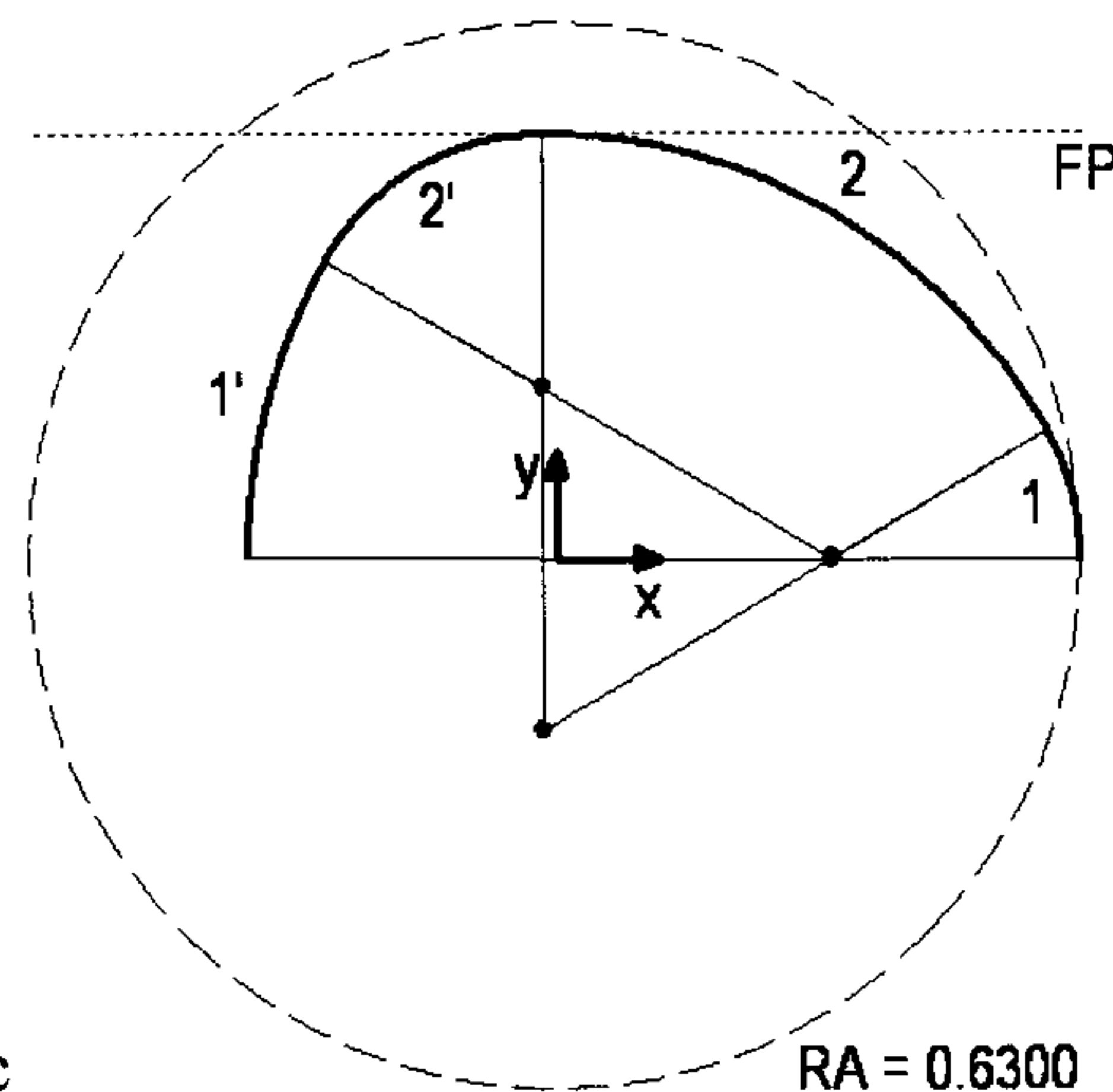


Figure 5c

- 1) $R = 0.3000$ $M_x = 0.3300$
 $\alpha = 0.5236$ $M_y = 0.0000$
 2) $R = 0.7000$ $M_x = -0.0164$
 $\alpha = 1.0472$ $M_y = -0.2000$
 2') $R = 0.3000$ $M_x = -0.0164$
 $\alpha = 1.0472$ $M_y = 0.2000$
 1') $R = 0.7000$ $M_x = 0.3300$
 $\alpha = 0.5236$ $M_y = -0.0000$

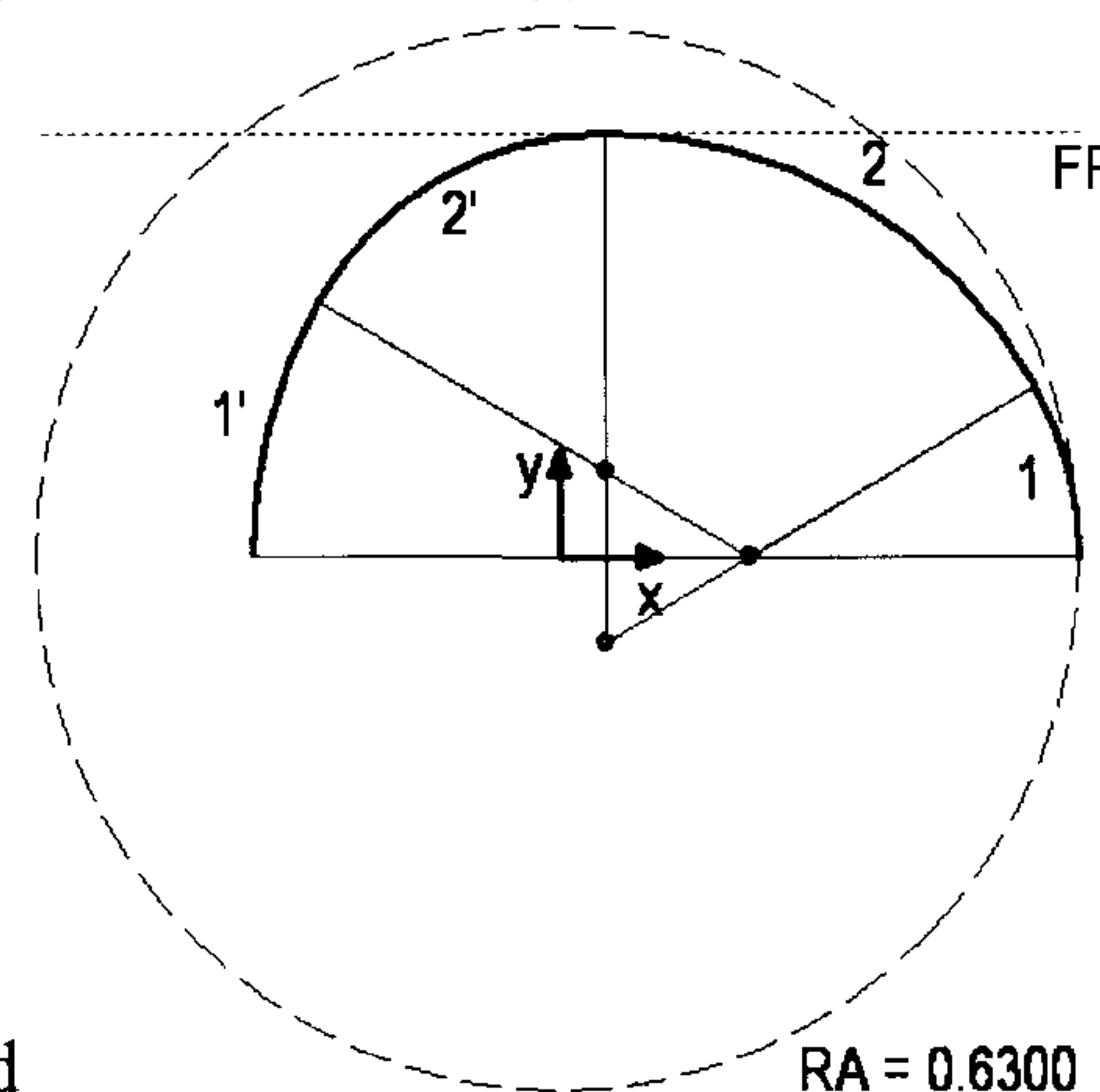


Figure 5d

- 1) $R = 0.4000$ $M_x = 0.2300$
 $\alpha = 0.5236$ $M_y = 0.0000$
 2) $R = 0.6000$ $M_x = 0.0568$
 $\alpha = 1.0472$ $M_y = -0.1000$
 2') $R = 0.4000$ $M_x = 0.0568$
 $\alpha = 1.0472$ $M_y = 0.1000$
 1') $R = 0.6000$ $M_x = 0.2300$
 $\alpha = 0.5236$ $M_y = -0.0000$

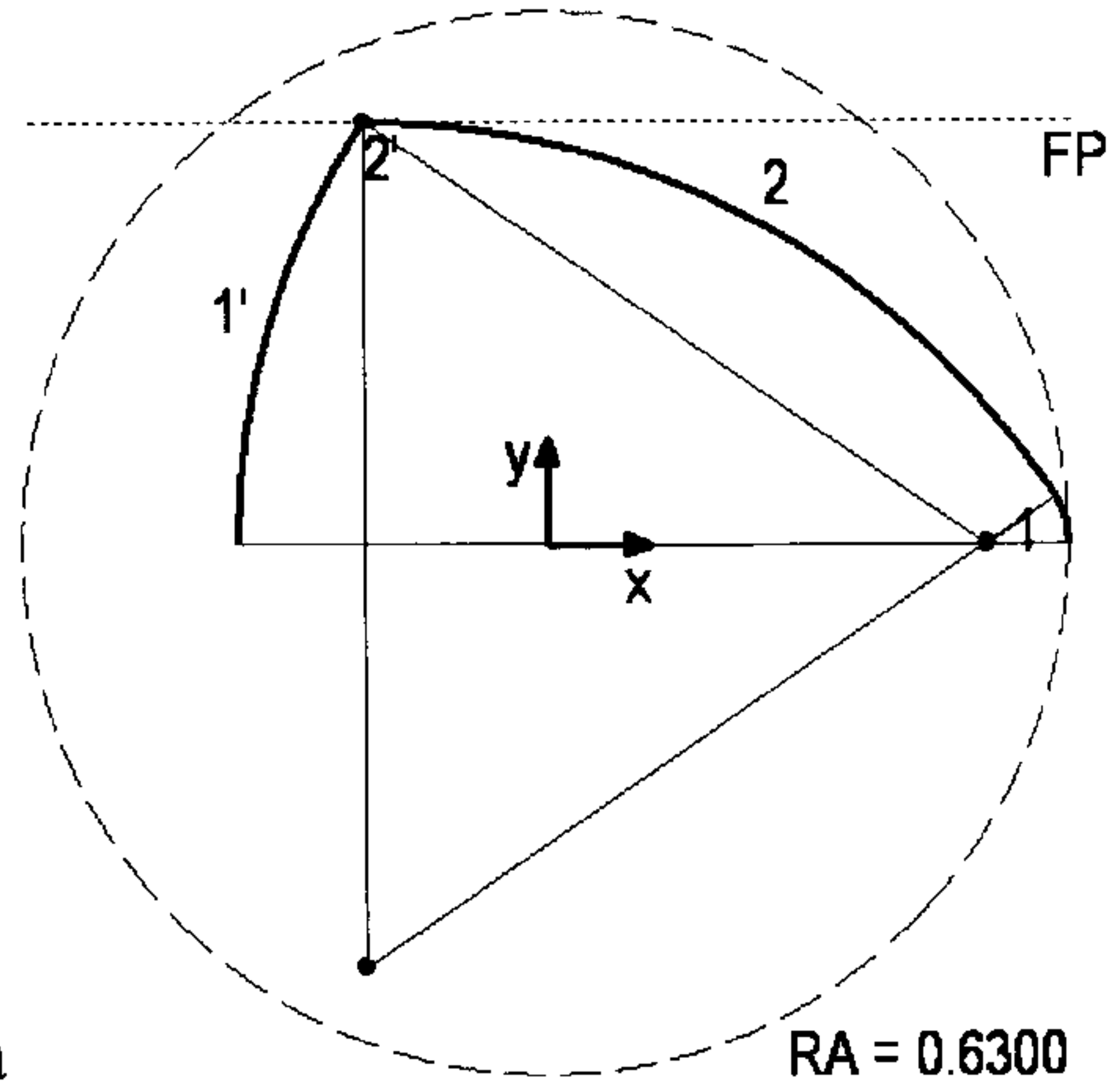


Figure 6a

- 1) $R = 0.1000$ $M_x = 0.5300$
 $\alpha = 0.5890$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.2183$
 $\alpha = 0.9818$ $M_y = -0.5000$
 2') $R = 0.0000$ $M_x = -0.2183$
 $\alpha = 0.9818$ $M_y = 0.5000$
 1') $R = 0.9000$ $M_x = 0.5300$
 $\alpha = 0.5890$ $M_y = -0.0000$

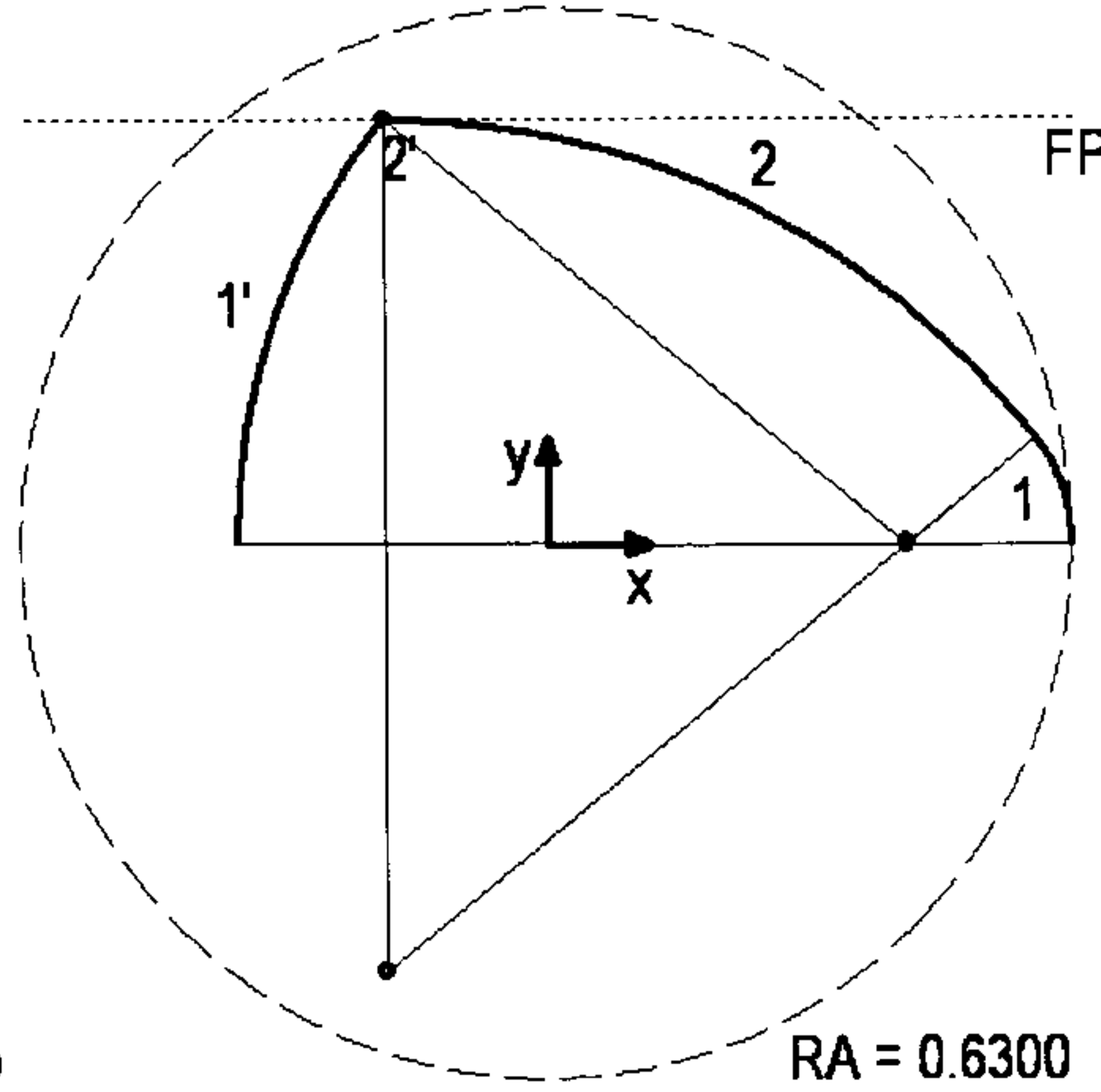


Figure 6b

- 1) $R = 0.2000$ $M_x = 0.4300$
 $\alpha = 0.6751$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.1945$
 $\alpha = 0.8957$ $M_y = -0.5000$
 2') $R = 0.0000$ $M_x = -0.1945$
 $\alpha = 0.8957$ $M_y = 0.5000$
 1') $R = 0.8000$ $M_x = 0.4300$
 $\alpha = 0.6751$ $M_y = -0.0000$

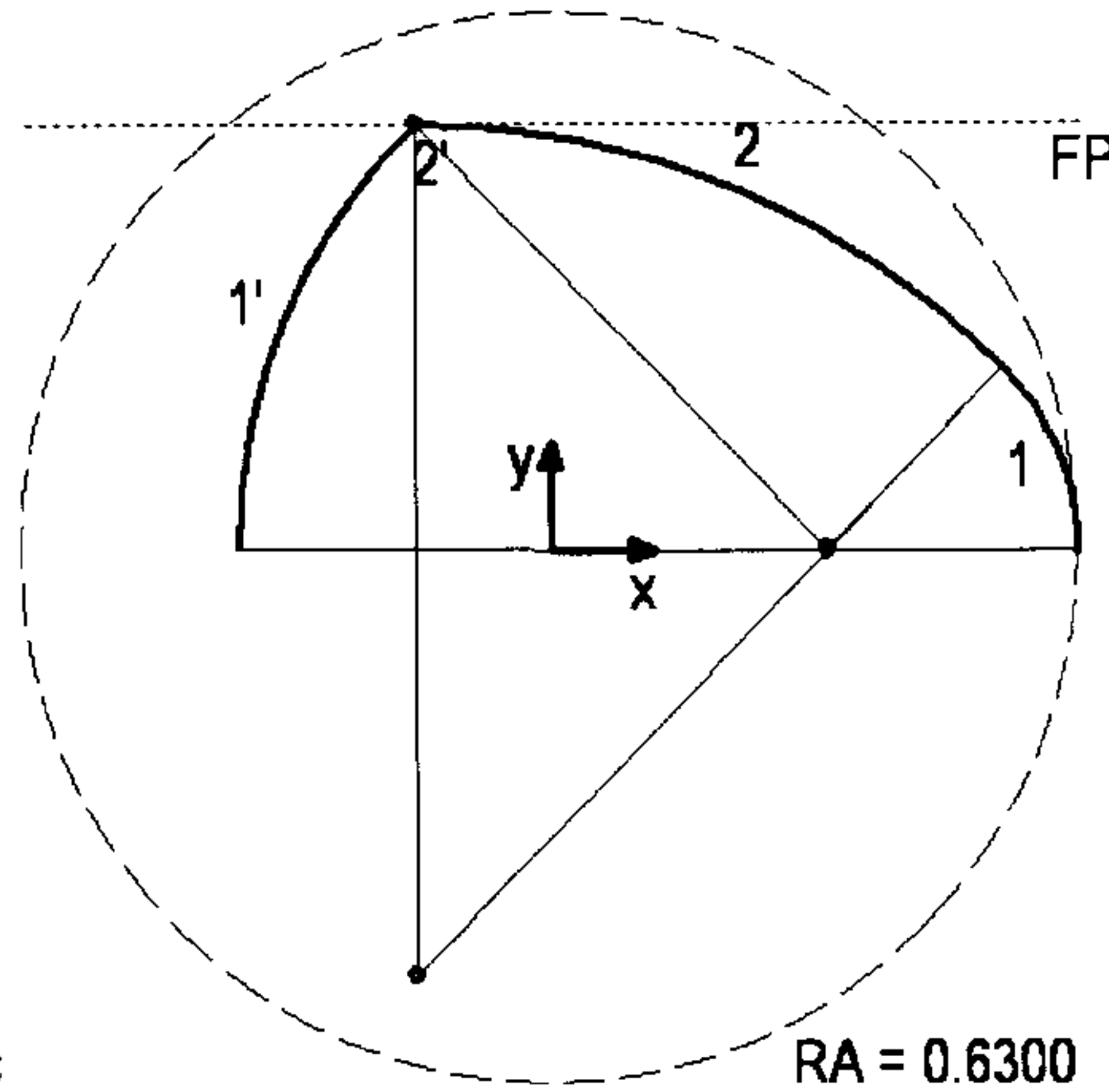


Figure 6c

- 1) $R = 0.3000$ $M_x = 0.3300$
 $\alpha = 0.7956$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.1599$
 $\alpha = 0.7752$ $M_y = -0.5000$
 2') $R = 0.0000$ $M_x = -0.1599$
 $\alpha = 0.7752$ $M_y = 0.5000$
 1') $R = 0.7000$ $M_x = 0.3300$
 $\alpha = 0.7956$ $M_y = -0.0000$

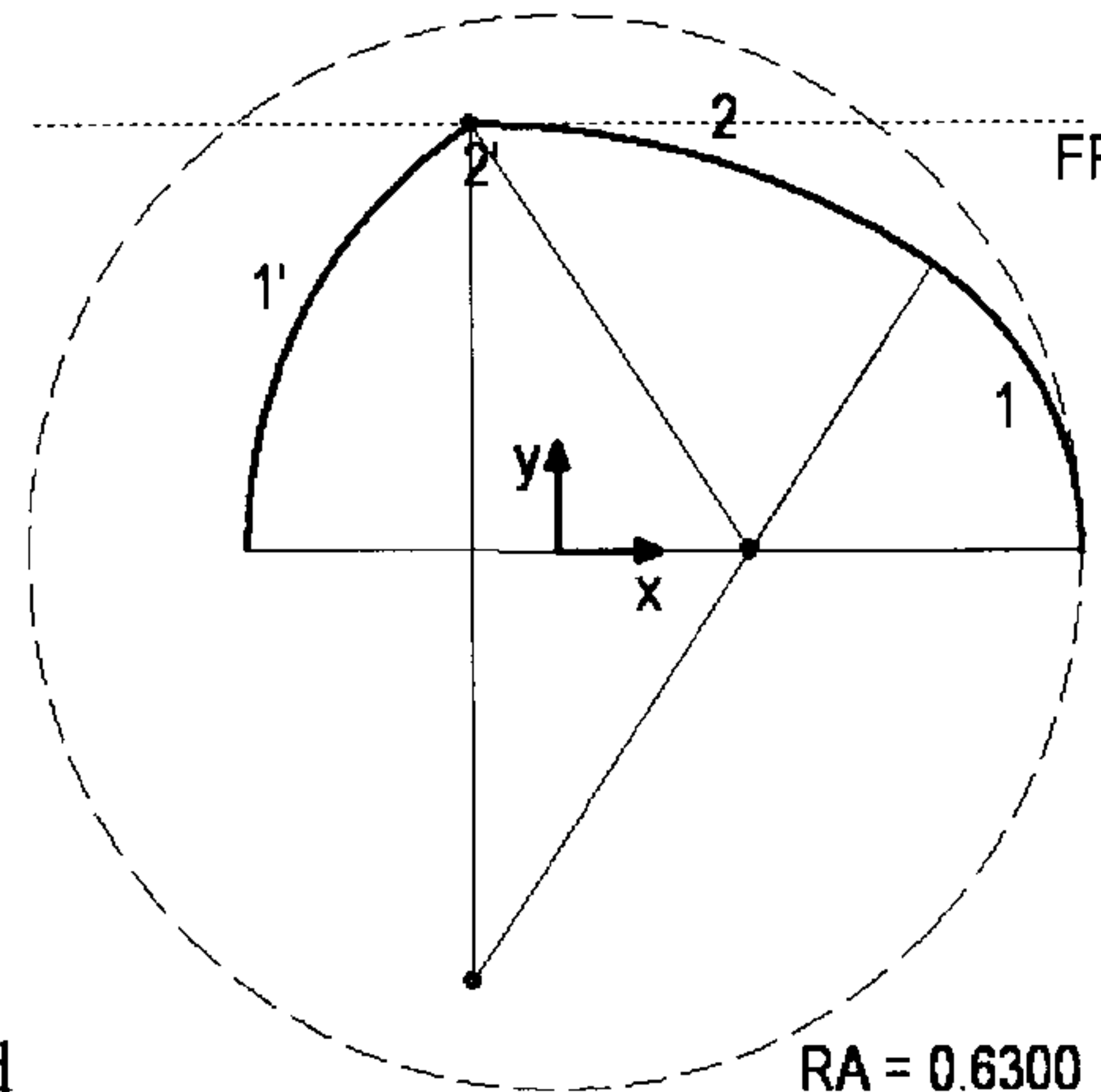


Figure 6d

- 1) $R = 0.4000$ $M_x = 0.2300$
 $\alpha = 0.9851$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.1017$
 $\alpha = 0.5857$ $M_y = -0.5000$
 2') $R = 0.0000$ $M_x = -0.1017$
 $\alpha = 0.5857$ $M_y = 0.5000$
 1') $R = 0.6000$ $M_x = 0.2300$
 $\alpha = 0.9851$ $M_y = -0.0000$

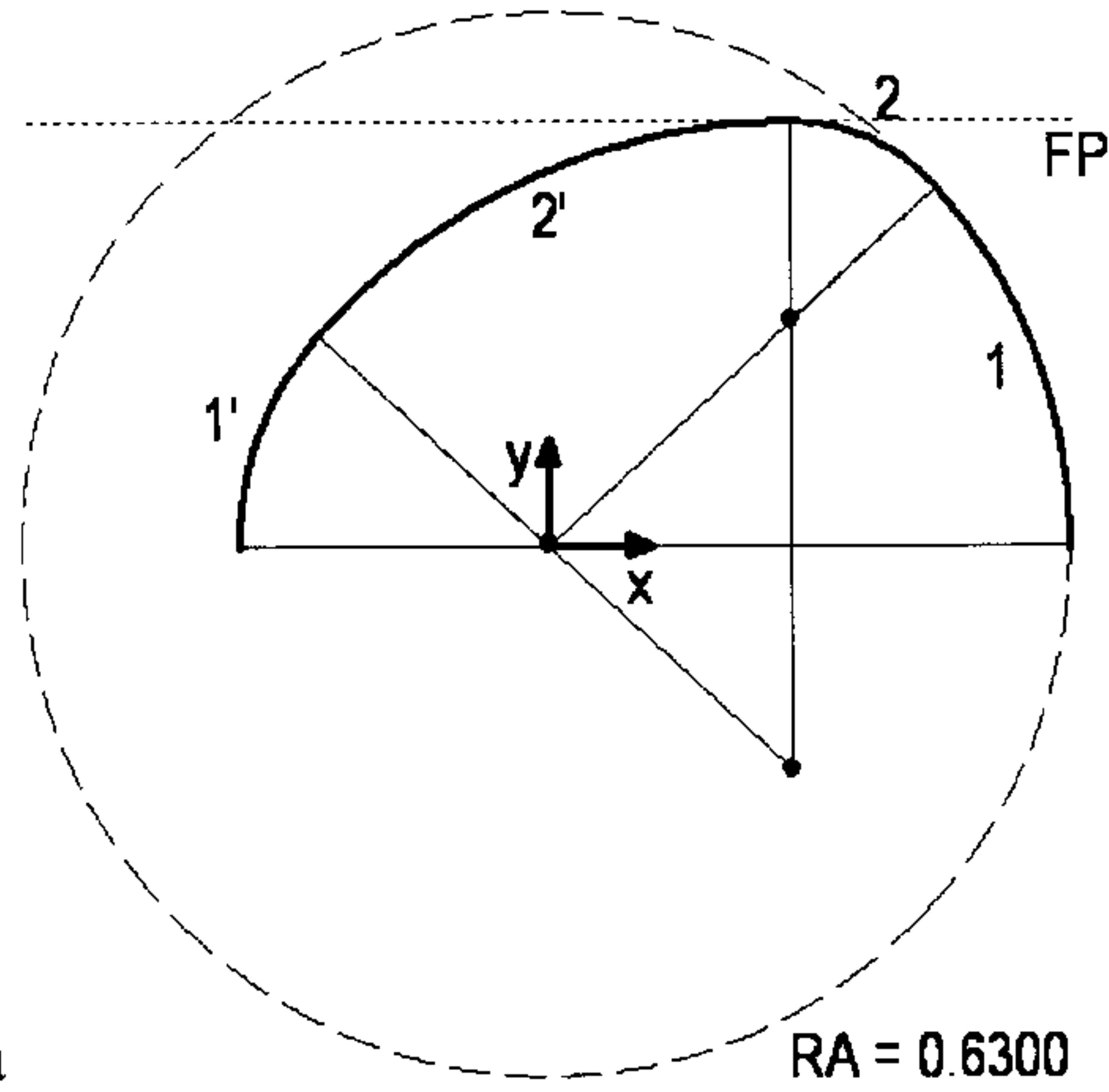


Figure 7a

- 1) $R = 0.6300$ $M_x = 0.0000$
 $\alpha = 0.7334$ $M_y = 0.0000$
 2) $R = 0.2368$ $M_x = 0.2921$
 $\alpha = 0.8374$ $M_y = 0.2632$
 2') $R = 0.7632$ $M_x = 0.2921$
 $\alpha = 0.8374$ $M_y = -0.2632$
 1') $R = 0.3700$ $M_x = 0.0000$
 $\alpha = 0.7334$ $M_y = 0.0000$

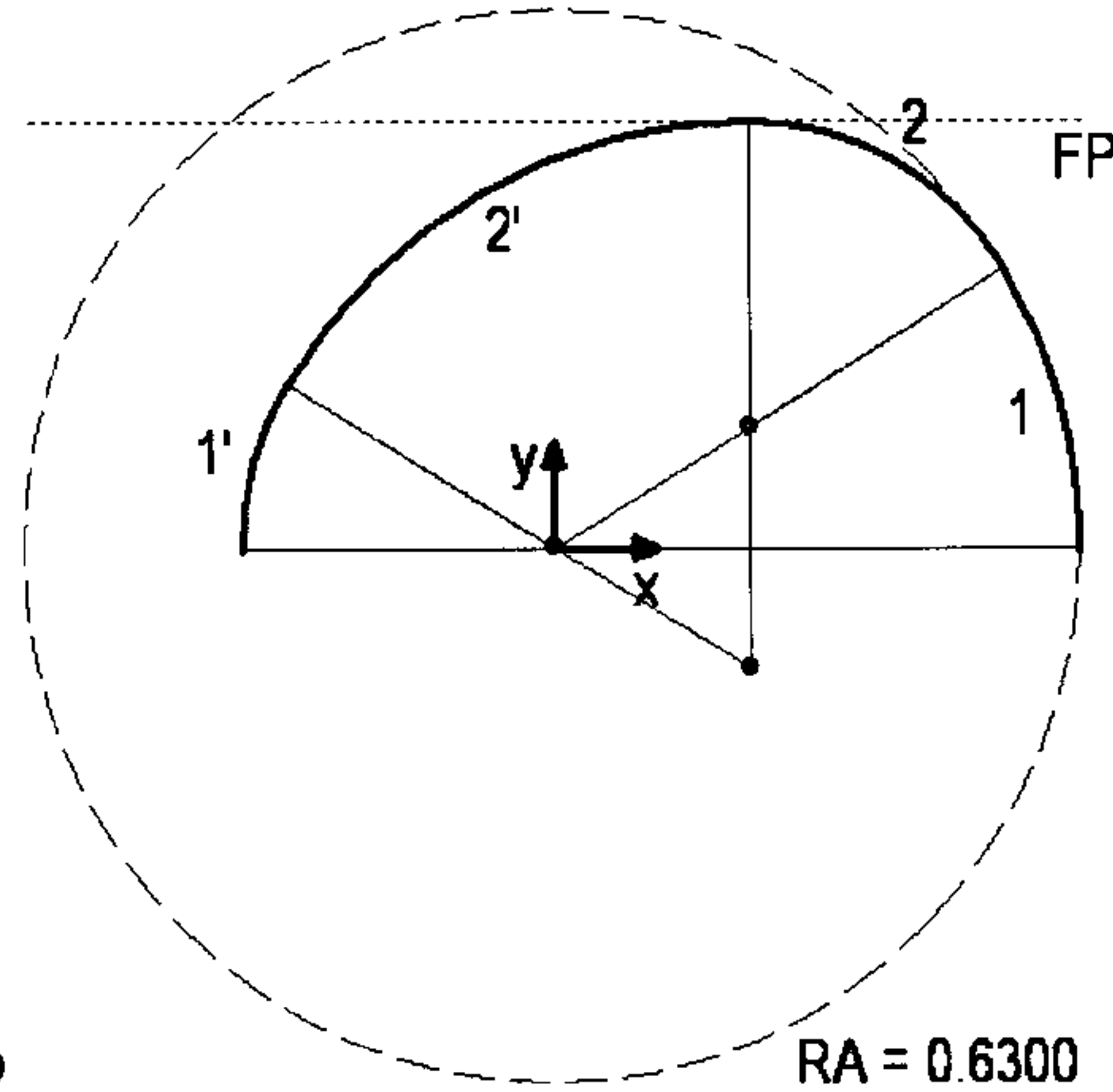


Figure 7b

- 1) $R = 0.6300$ $M_x = 0.0000$
 $\alpha = 0.5501$ $M_y = 0.0000$
 2) $R = 0.3576$ $M_x = 0.2322$
 $\alpha = 1.0207$ $M_y = 0.1424$
 2') $R = 0.6424$ $M_x = 0.2322$
 $\alpha = 1.0207$ $M_y = -0.1424$
 1') $R = 0.3700$ $M_x = 0.0000$
 $\alpha = 0.5501$ $M_y = 0.0000$

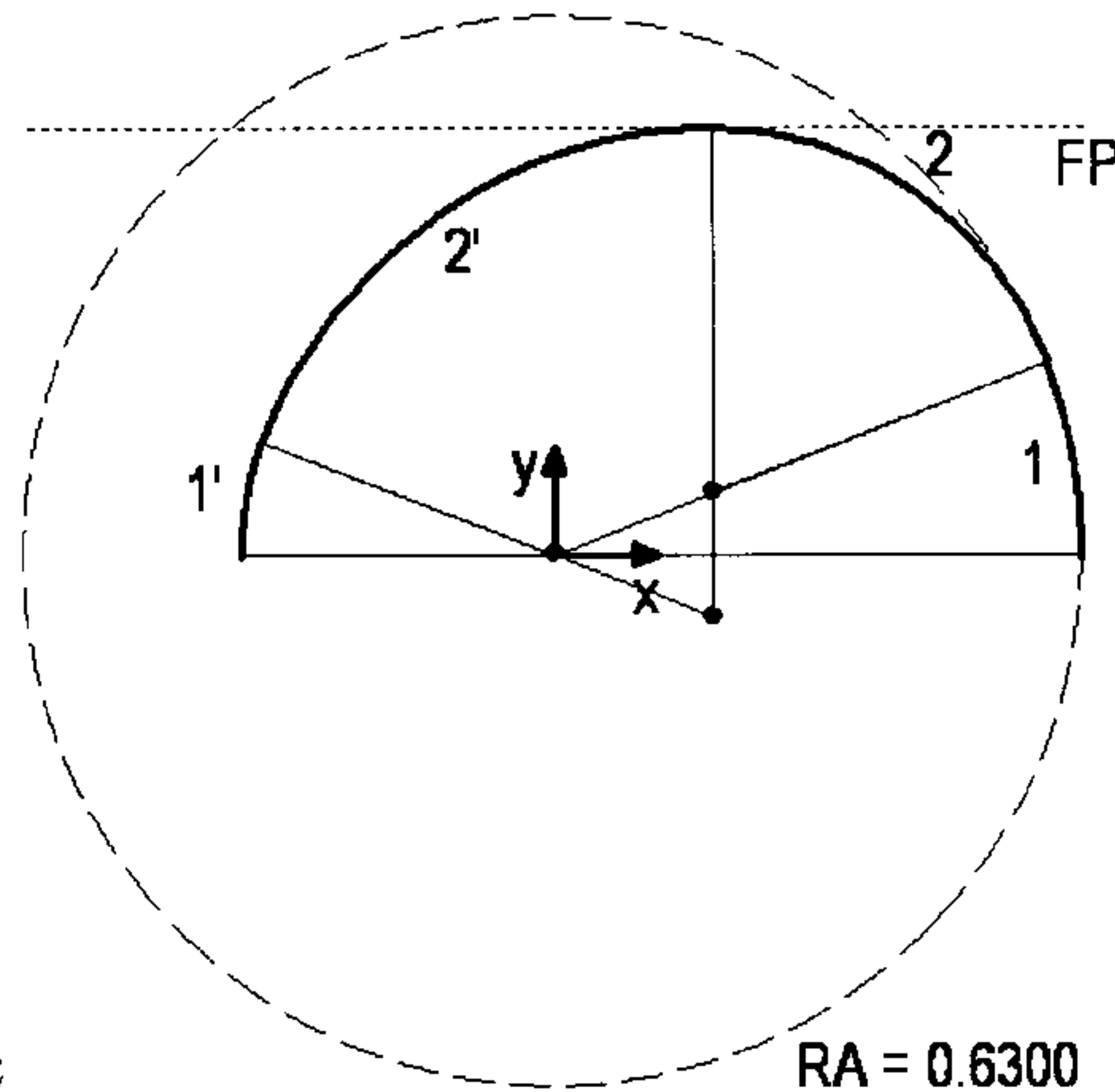


Figure 7c

- 1) $R = 0.6300$ $M_x = 0.0000$
 $\alpha = 0.3667$ $M_y = 0.0000$
 2) $R = 0.4273$ $M_x = 0.1892$
 $\alpha = 1.2041$ $M_y = 0.0727$
 2') $R = 0.5727$ $M_x = 0.1892$
 $\alpha = 1.2041$ $M_y = -0.0727$
 1') $R = 0.3700$ $M_x = 0.0000$
 $\alpha = 0.3667$ $M_y = 0.0000$

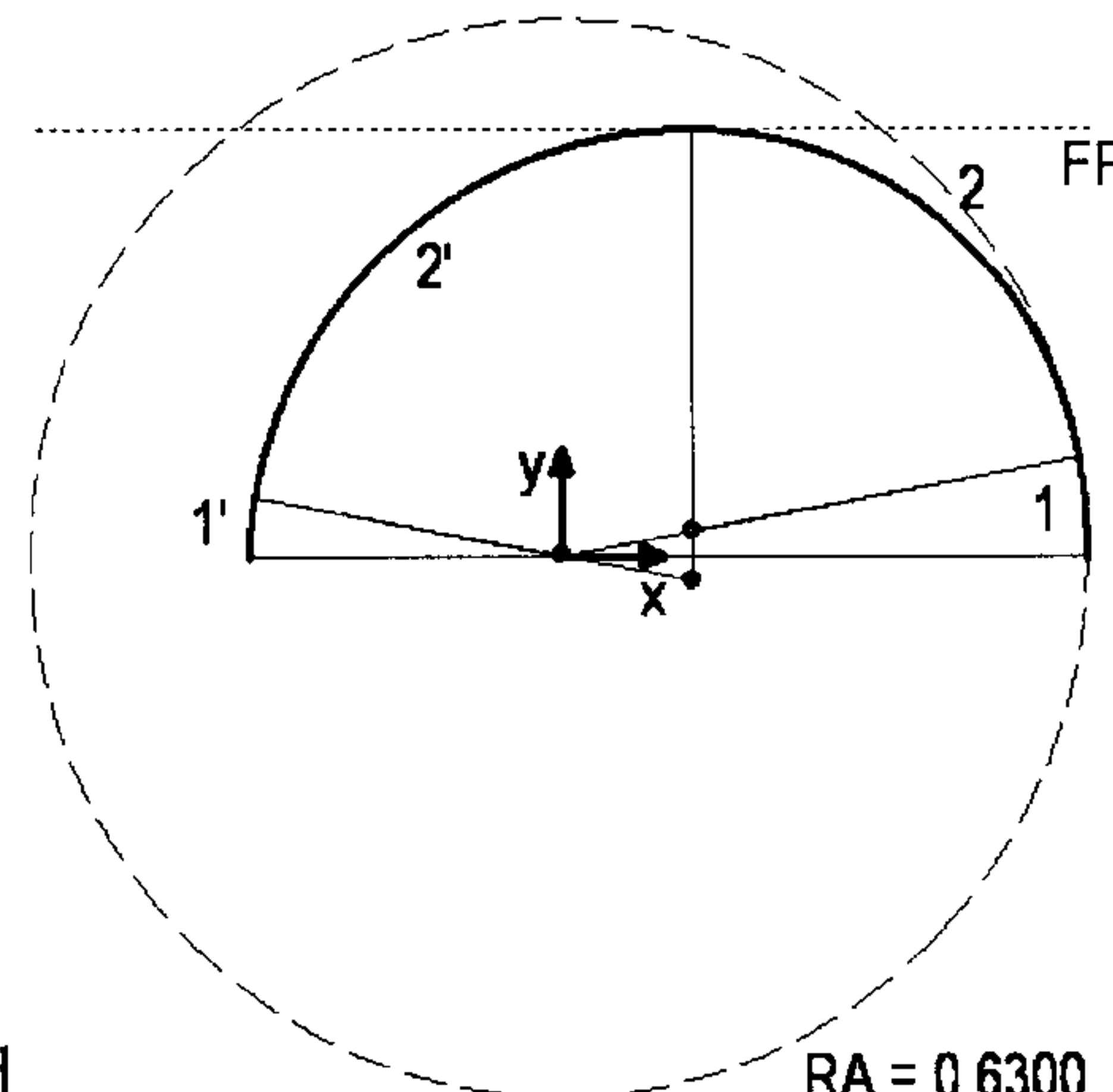


Figure 7d

- 1) $R = 0.6300$ $M_x = 0.0000$
 $\alpha = 0.1834$ $M_y = 0.0000$
 2) $R = 0.4710$ $M_x = 0.1563$
 $\alpha = 1.3874$ $M_y = 0.0290$
 2') $R = 0.5290$ $M_x = 0.1563$
 $\alpha = 1.3874$ $M_y = -0.0290$
 1') $R = 0.3700$ $M_x = 0.0000$
 $\alpha = 0.1834$ $M_y = 0.0000$

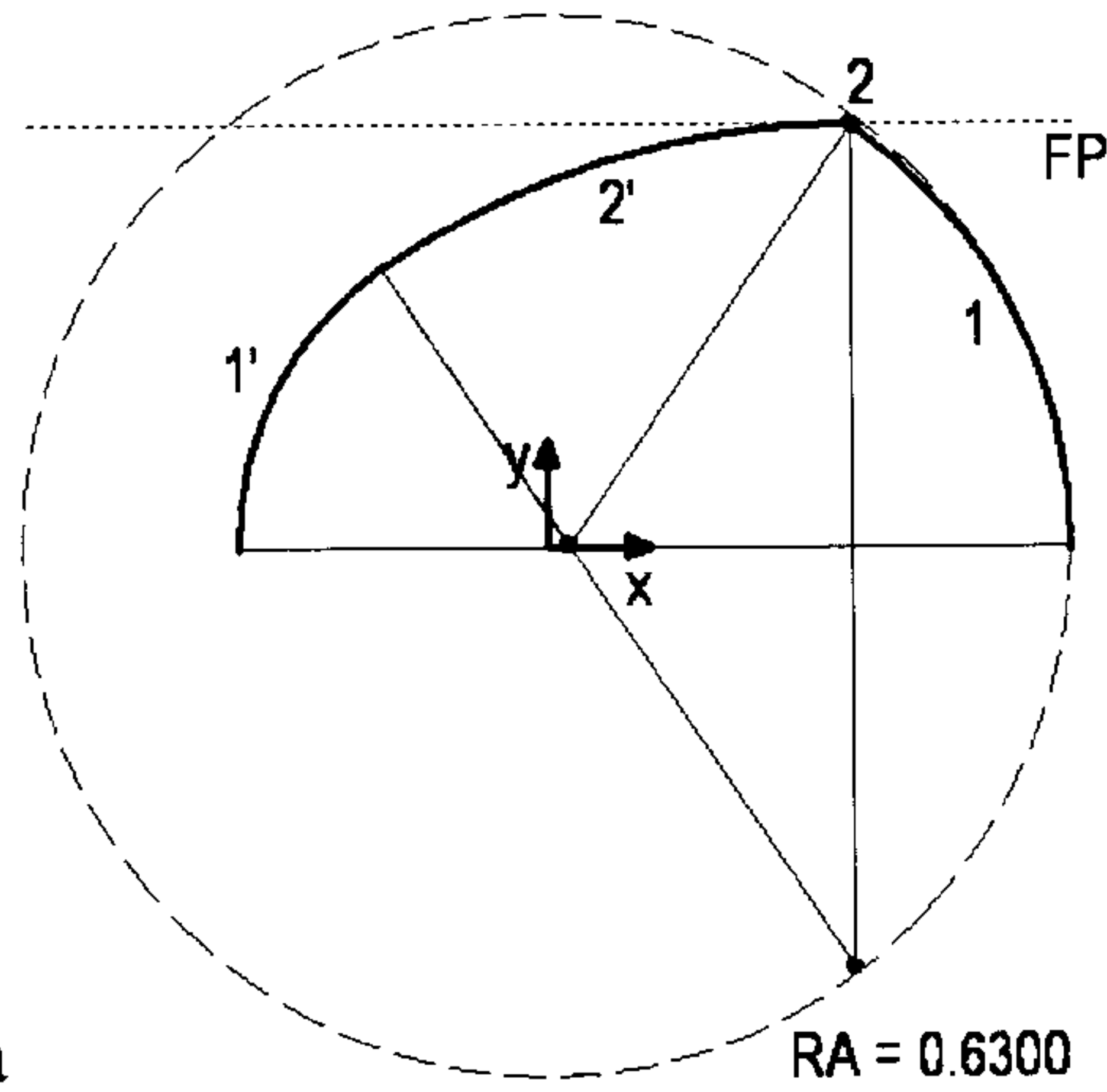


Figure 8a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.6040$ | $M_x = 0.0260$ |
| | $\alpha = 0.9752$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.3648$ |
| | $\alpha = 0.5956$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.3648$ |
| | $\alpha = 0.5956$ | $M_y = -0.5000$ |
| 1') | $R = 0.3960$ | $M_x = 0.0260$ |
| | $\alpha = 0.9752$ | $M_y = 0.0000$ |

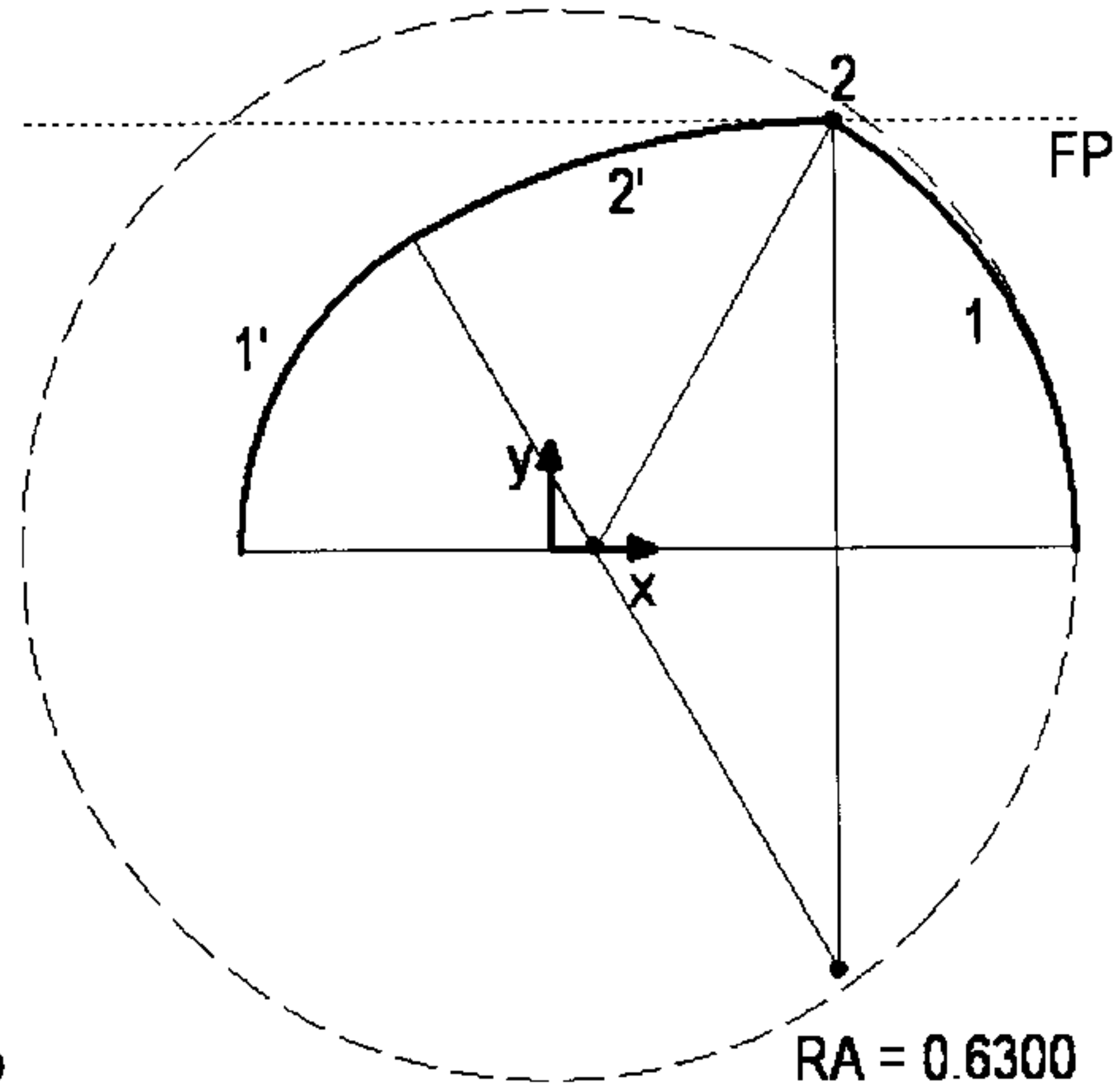


Figure 8b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5780$ | $M_x = 0.0520$ |
| | $\alpha = 1.0453$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.3420$ |
| | $\alpha = 0.5255$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.3420$ |
| | $\alpha = 0.5255$ | $M_y = -0.5000$ |
| 1') | $R = 0.4220$ | $M_x = 0.0520$ |
| | $\alpha = 1.0453$ | $M_y = 0.0000$ |

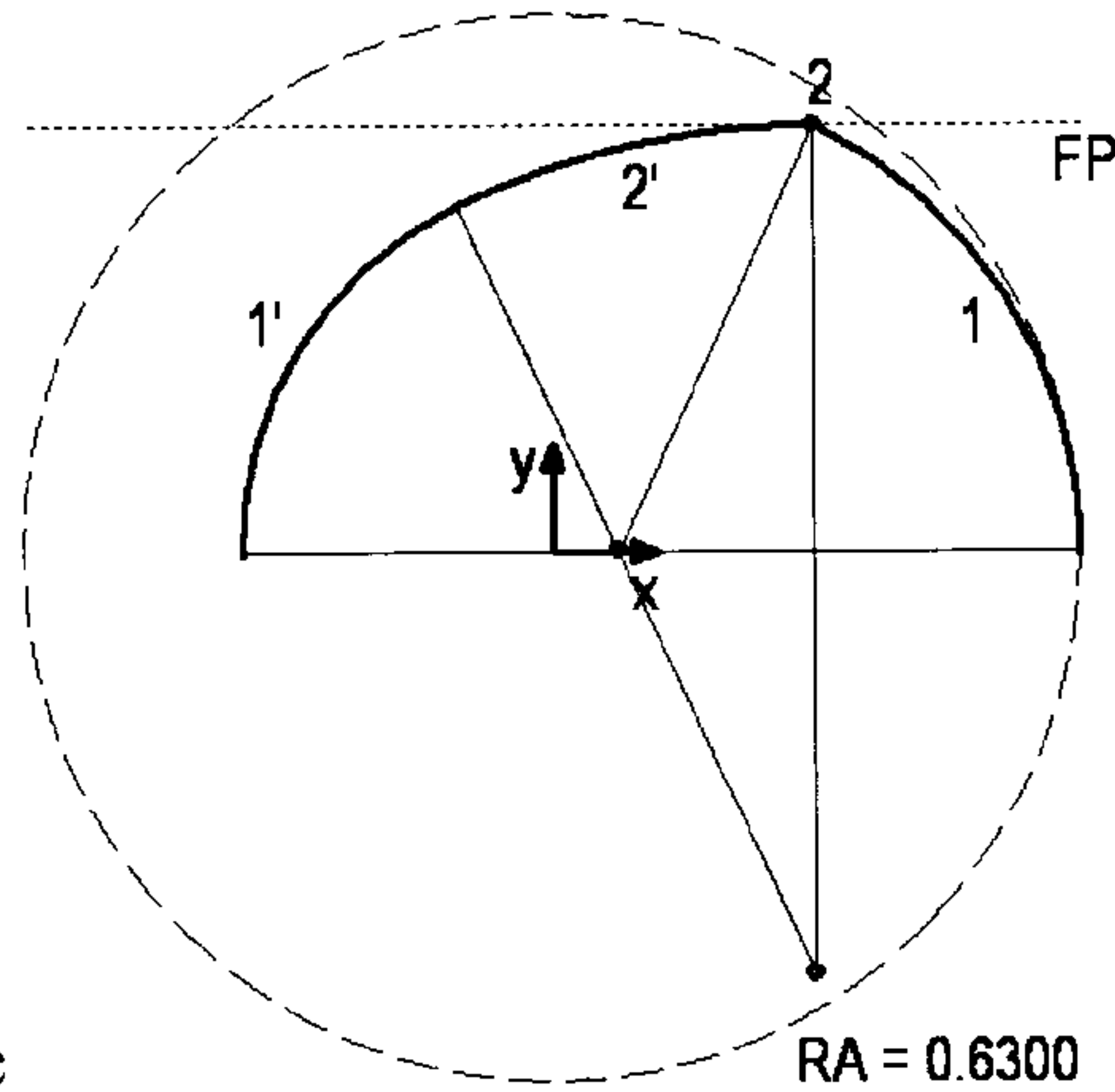


Figure 8c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5520$ | $M_x = 0.0780$ |
| | $\alpha = 1.1333$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.3119$ |
| | $\alpha = 0.4375$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.3119$ |
| | $\alpha = 0.4375$ | $M_y = -0.5000$ |
| 1') | $R = 0.4480$ | $M_x = 0.0780$ |
| | $\alpha = 1.1333$ | $M_y = 0.0000$ |

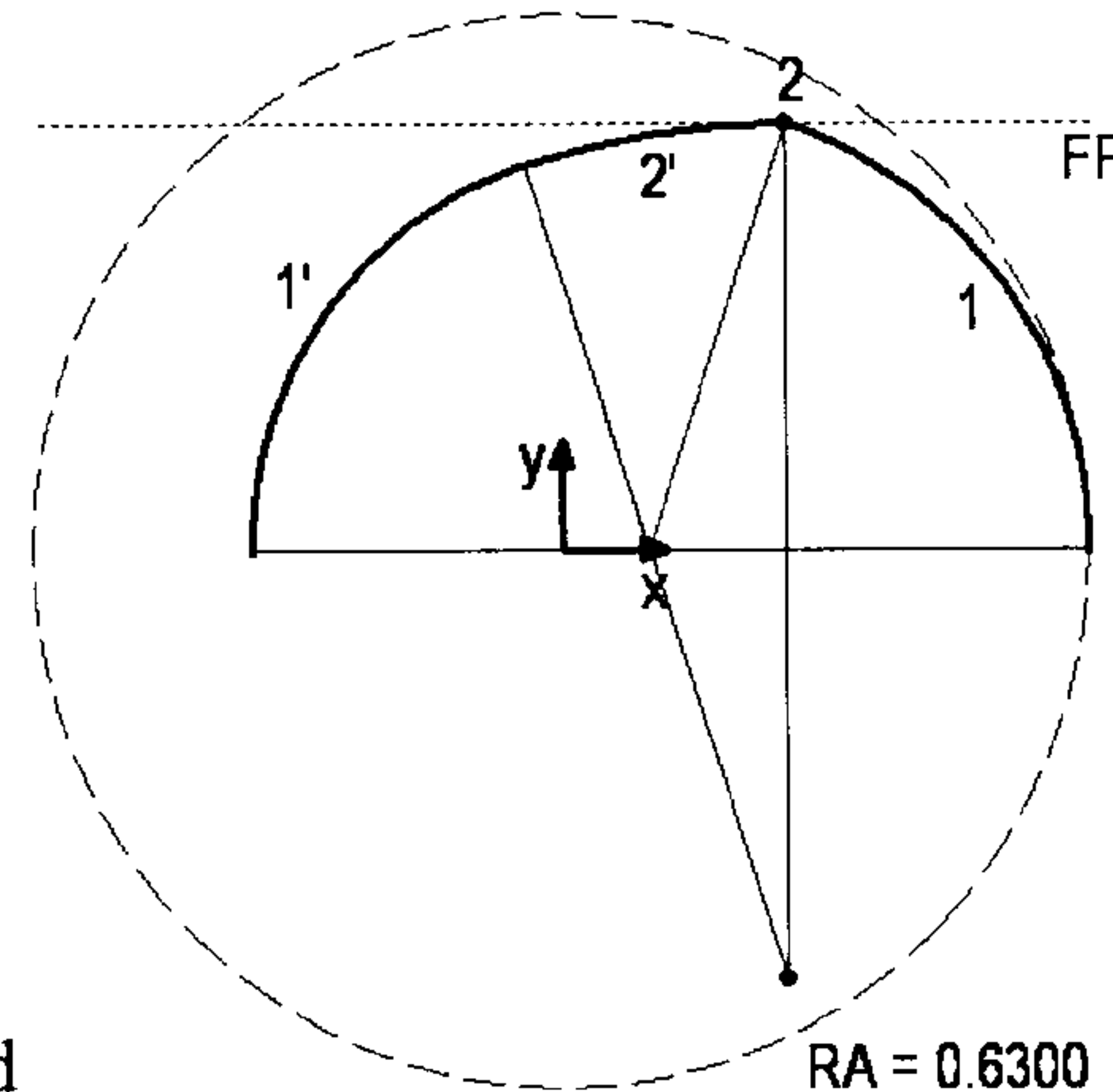


Figure 8d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5260$ | $M_x = 0.1040$ |
| | $\alpha = 1.2551$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.2673$ |
| | $\alpha = 0.3157$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.2673$ |
| | $\alpha = 0.3157$ | $M_y = -0.5000$ |
| 1') | $R = 0.4740$ | $M_x = 0.1040$ |
| | $\alpha = 1.2551$ | $M_y = 0.0000$ |

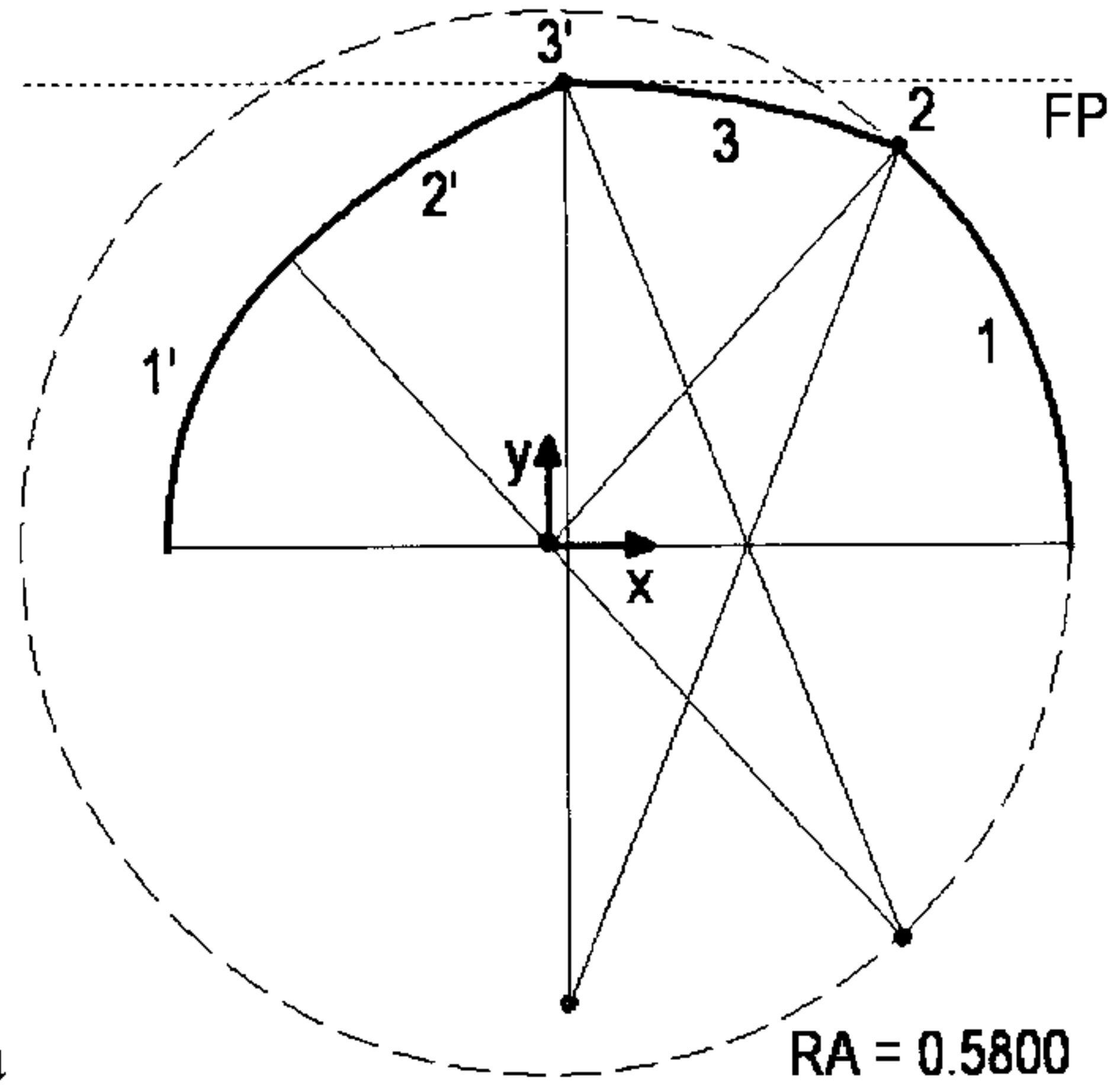


Figure 9a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.3908$ |
| | $\alpha = 0.3591$ | $M_y = 0.4286$ |
| 3) | $R = 1.0000$ | $M_x = 0.0197$ |
| | $\alpha = 0.3802$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = 0.0197$ |
| | $\alpha = 0.3802$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.3908$ |
| | $\alpha = 0.3591$ | $M_y = -0.4286$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |

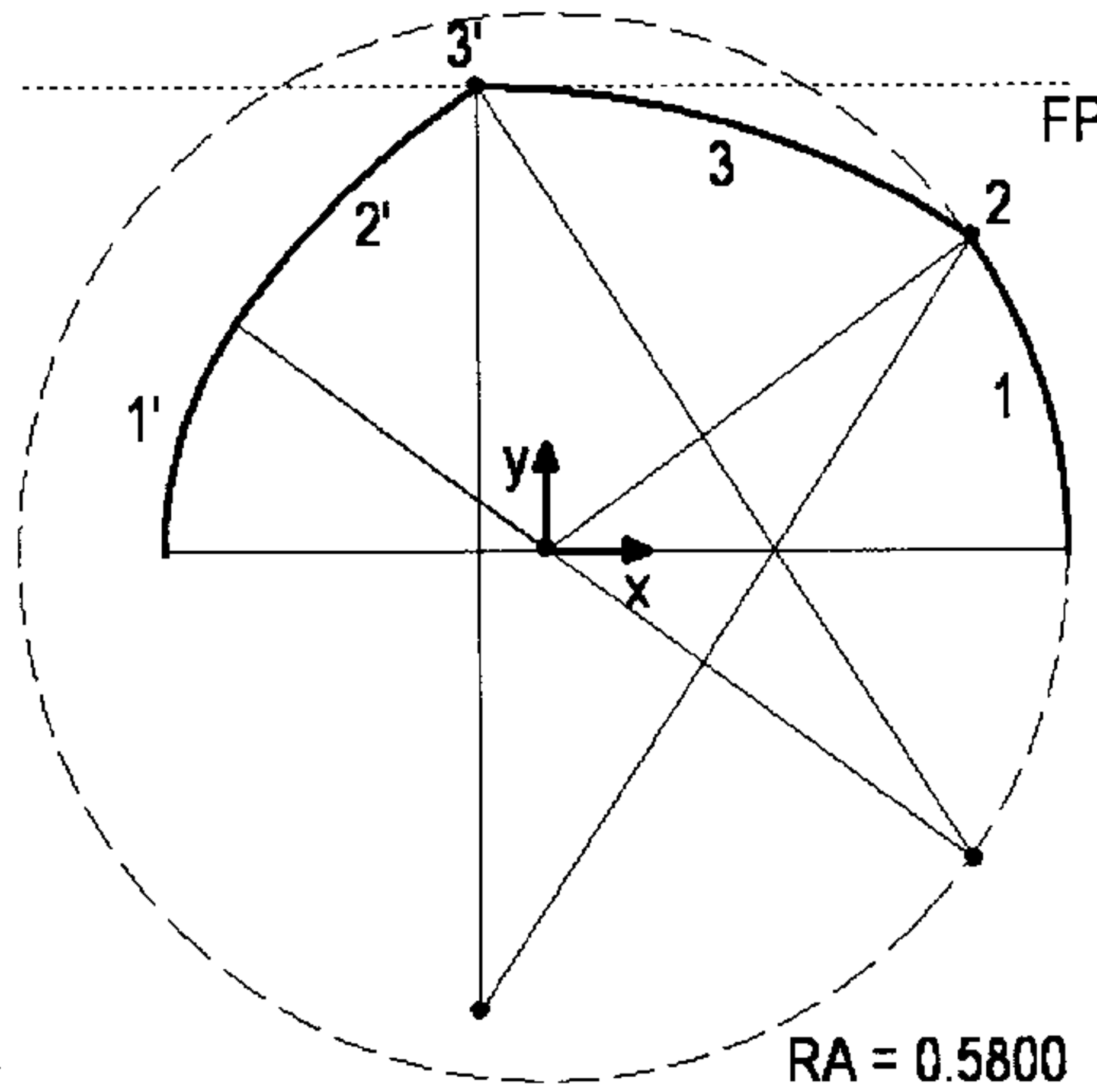


Figure 9b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.4708$ |
| | $\alpha = 0.3713$ | $M_y = 0.3387$ |
| 3) | $R = 1.0000$ | $M_x = -0.0738$ |
| | $\alpha = 0.5759$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.0738$ |
| | $\alpha = 0.5759$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.4708$ |
| | $\alpha = 0.3713$ | $M_y = -0.3387$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |

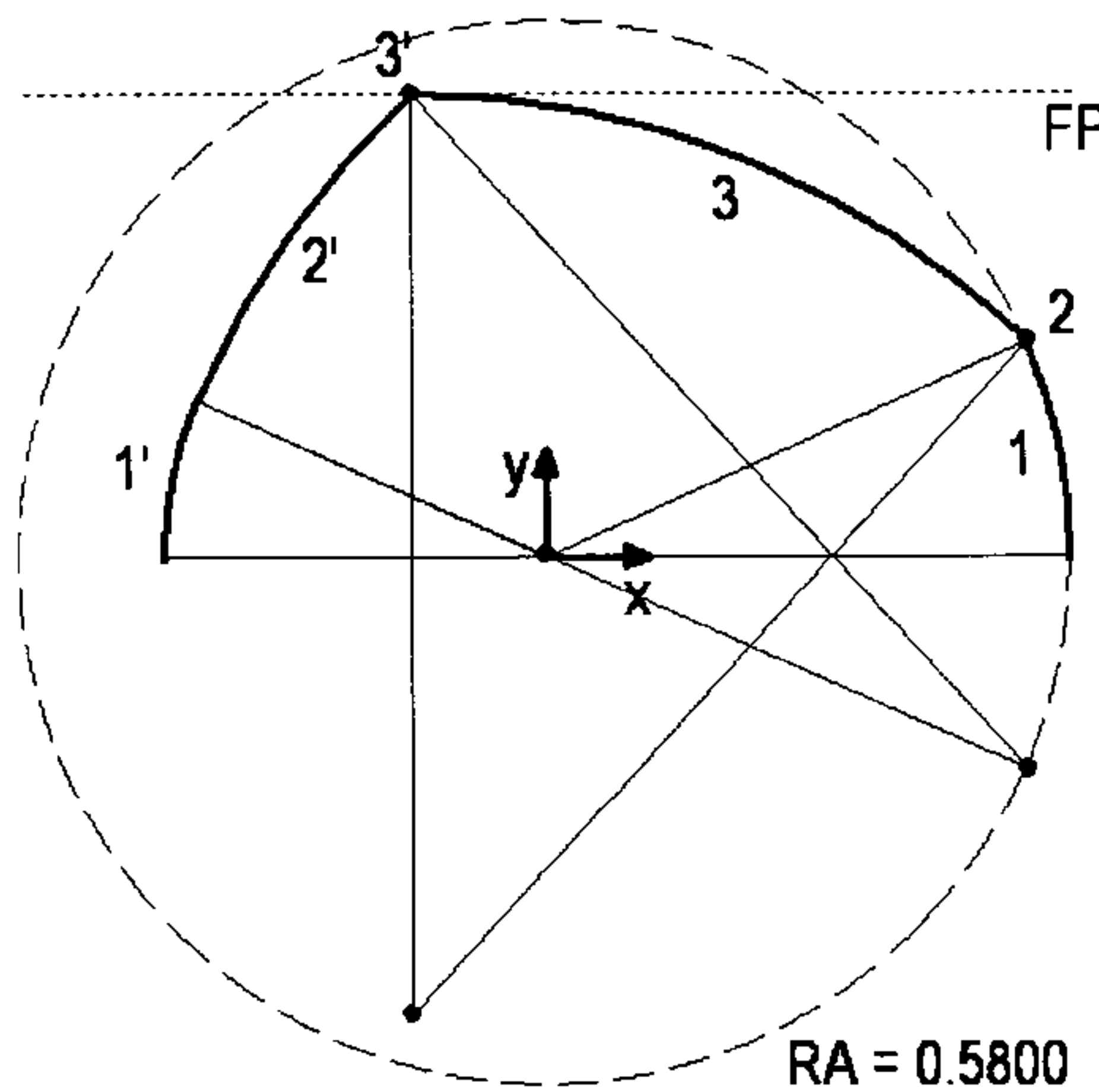


Figure 9c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.5306$ |
| | $\alpha = 0.4088$ | $M_y = 0.2342$ |
| 3) | $R = 1.0000$ | $M_x = -0.1483$ |
| | $\alpha = 0.7462$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.1483$ |
| | $\alpha = 0.7462$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.5306$ |
| | $\alpha = 0.4088$ | $M_y = -0.2342$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |

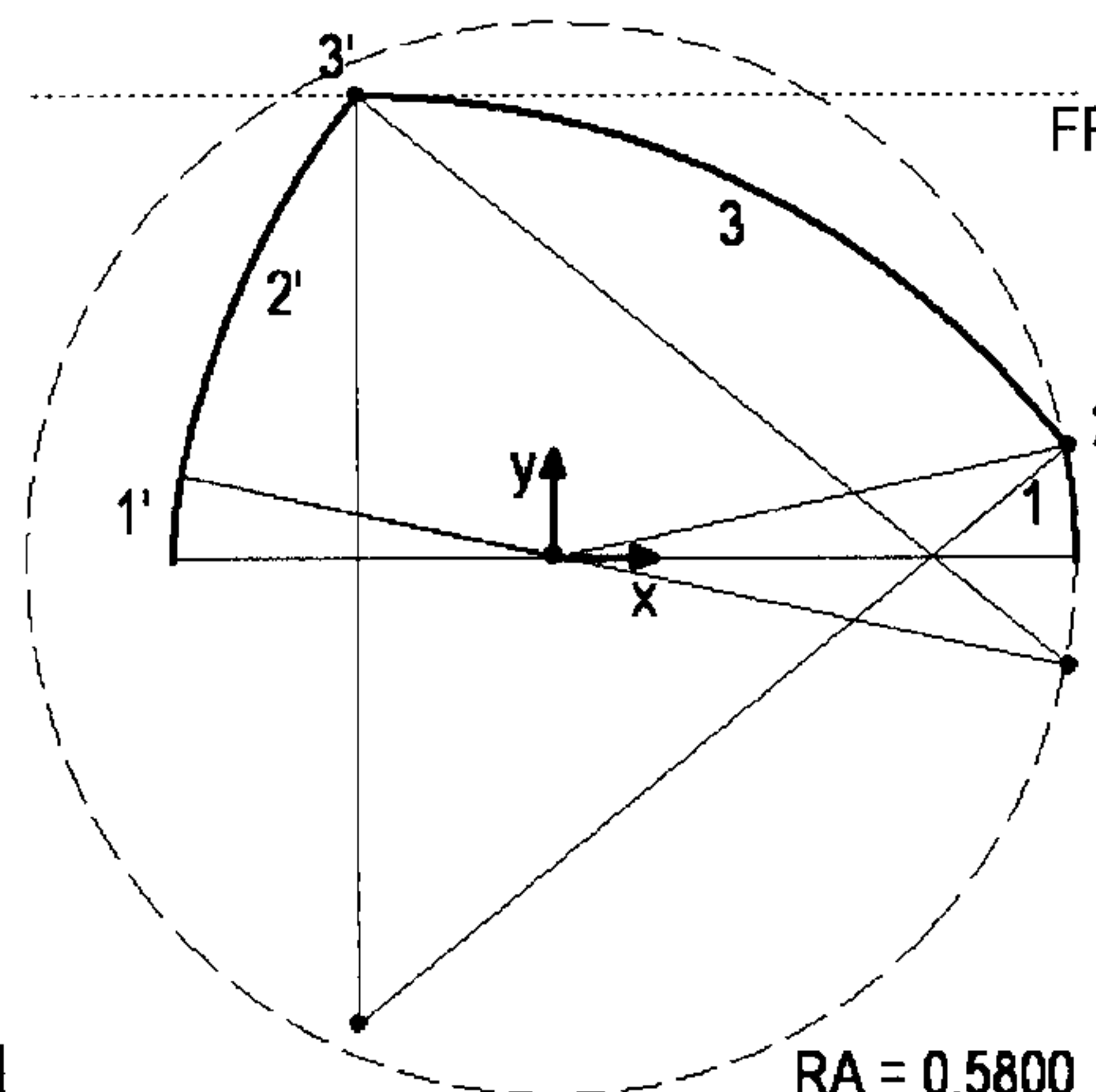


Figure 9d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.5675$ |
| | $\alpha = 0.4605$ | $M_y = 0.1197$ |
| 3) | $R = 1.0000$ | $M_x = -0.2173$ |
| | $\alpha = 0.9024$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.2173$ |
| | $\alpha = 0.9024$ | $M_y = 0.5000$ |
| 2') | $R = 1.0000$ | $M_x = 0.5675$ |
| | $\alpha = 0.4605$ | $M_y = -0.1197$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |

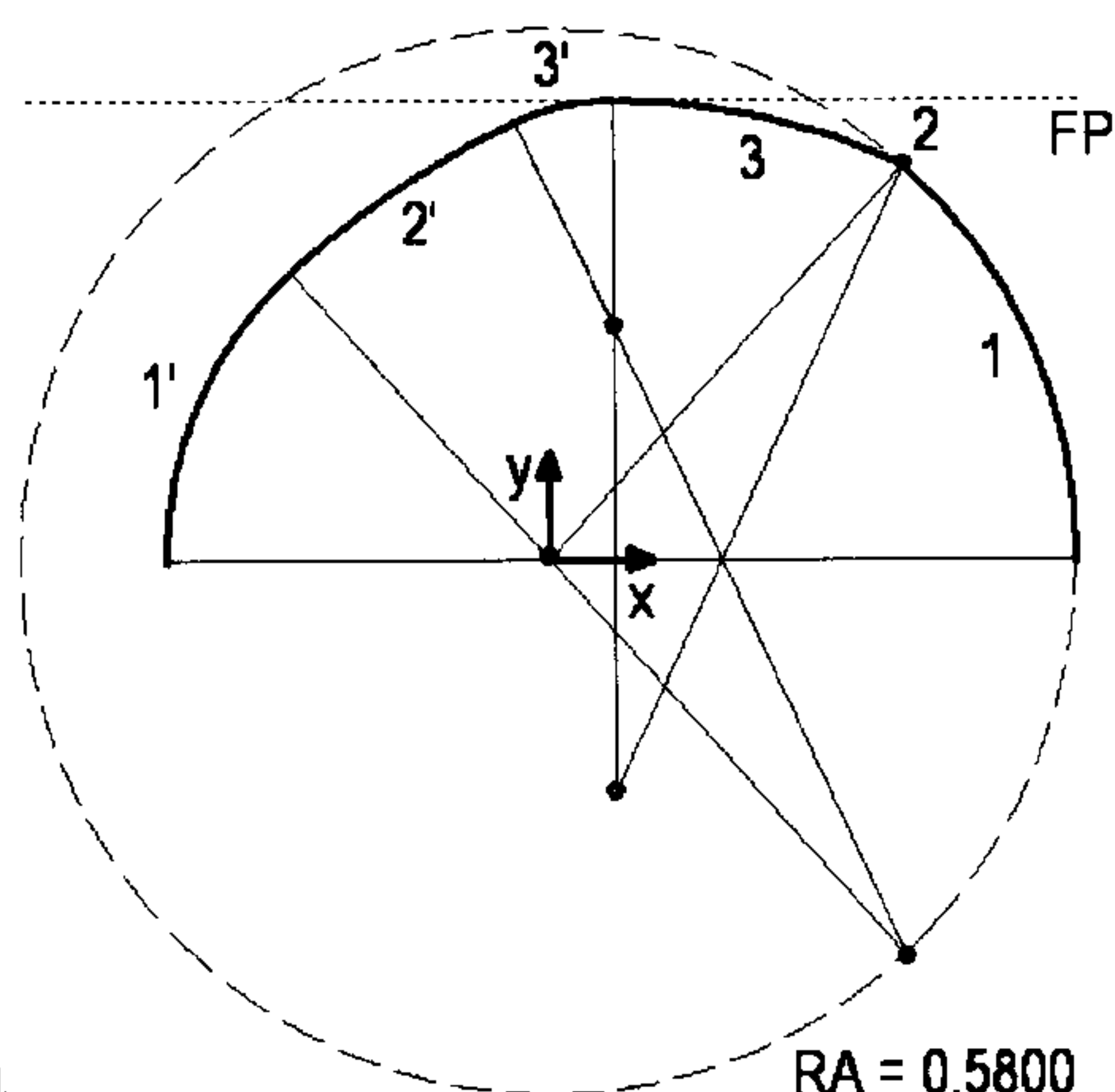


Figure 10a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.3908$ |
| | $\alpha = 0.2994$ | $M_y = 0.4286$ |
| 3) | $R = 0.7500$ | $M_x = 0.0714$ |
| | $\alpha = 0.4399$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = 0.0714$ |
| | $\alpha = 0.4399$ | $M_y = 0.2500$ |
| 2') | $R = 1.0000$ | $M_x = 0.3908$ |
| | $\alpha = 0.2994$ | $M_y = -0.4286$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |

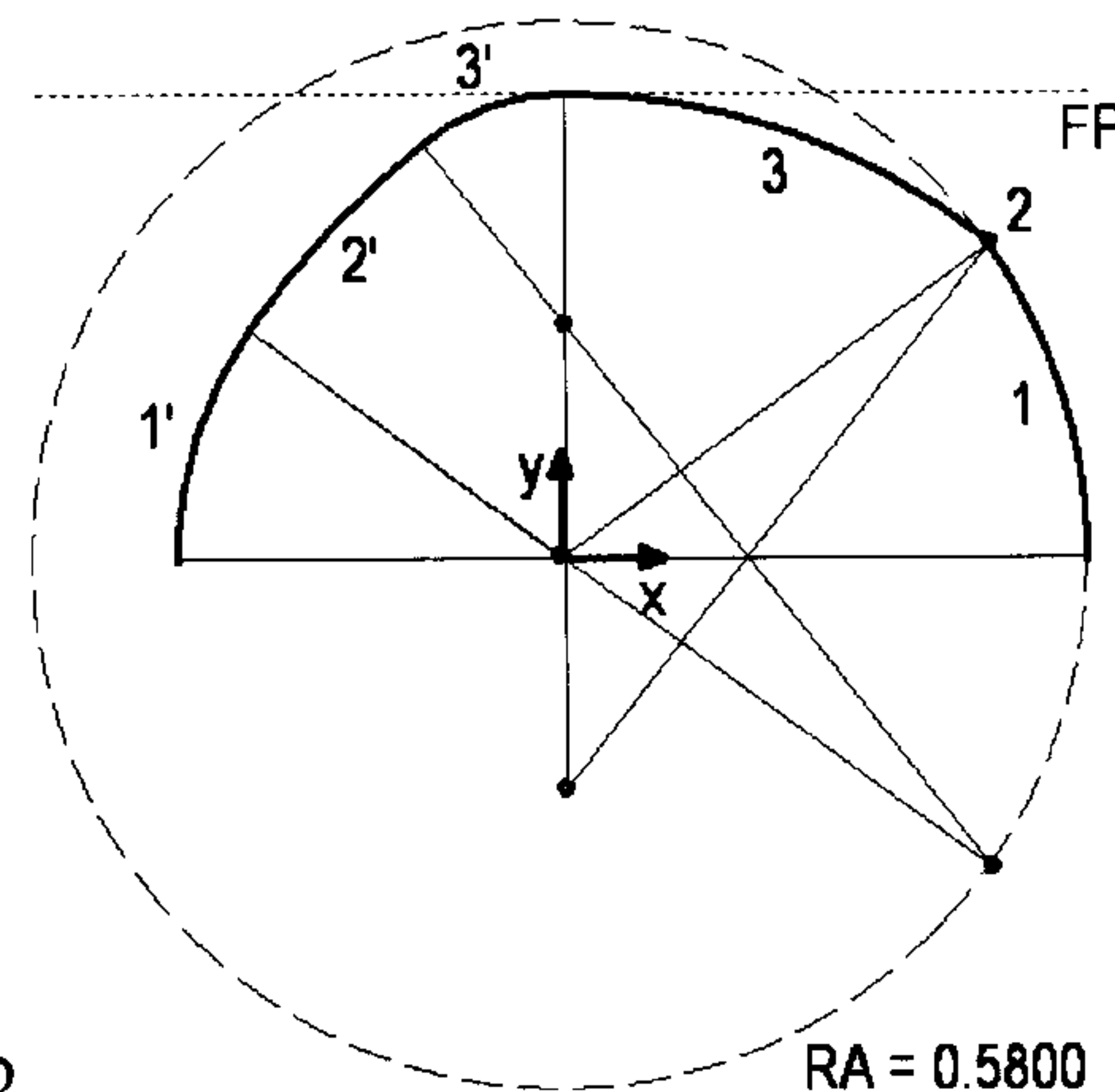


Figure 10b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.4708$ |
| | $\alpha = 0.2790$ | $M_y = 0.3387$ |
| 3) | $R = 0.7500$ | $M_x = 0.0061$ |
| | $\alpha = 0.6682$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = 0.0061$ |
| | $\alpha = 0.6682$ | $M_y = 0.2500$ |
| 2') | $R = 1.0000$ | $M_x = 0.4708$ |
| | $\alpha = 0.2790$ | $M_y = -0.3387$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |

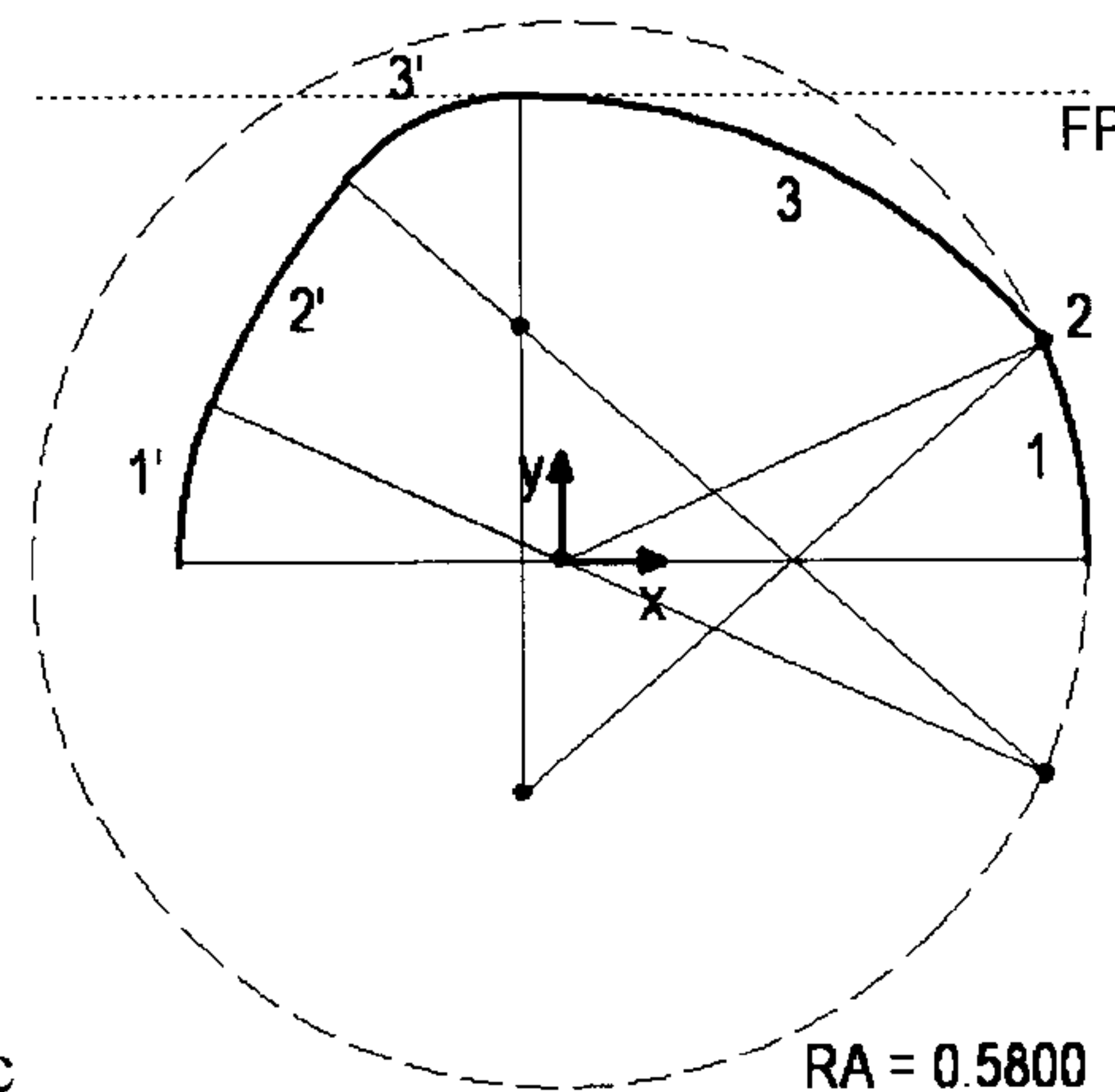


Figure 10c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.5306$ |
| | $\alpha = 0.2861$ | $M_y = 0.2342$ |
| 3) | $R = 0.7500$ | $M_x = -0.0421$ |
| | $\alpha = 0.8689$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = -0.0421$ |
| | $\alpha = 0.8689$ | $M_y = 0.2500$ |
| 2') | $R = 1.0000$ | $M_x = 0.5306$ |
| | $\alpha = 0.2861$ | $M_y = -0.2342$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |

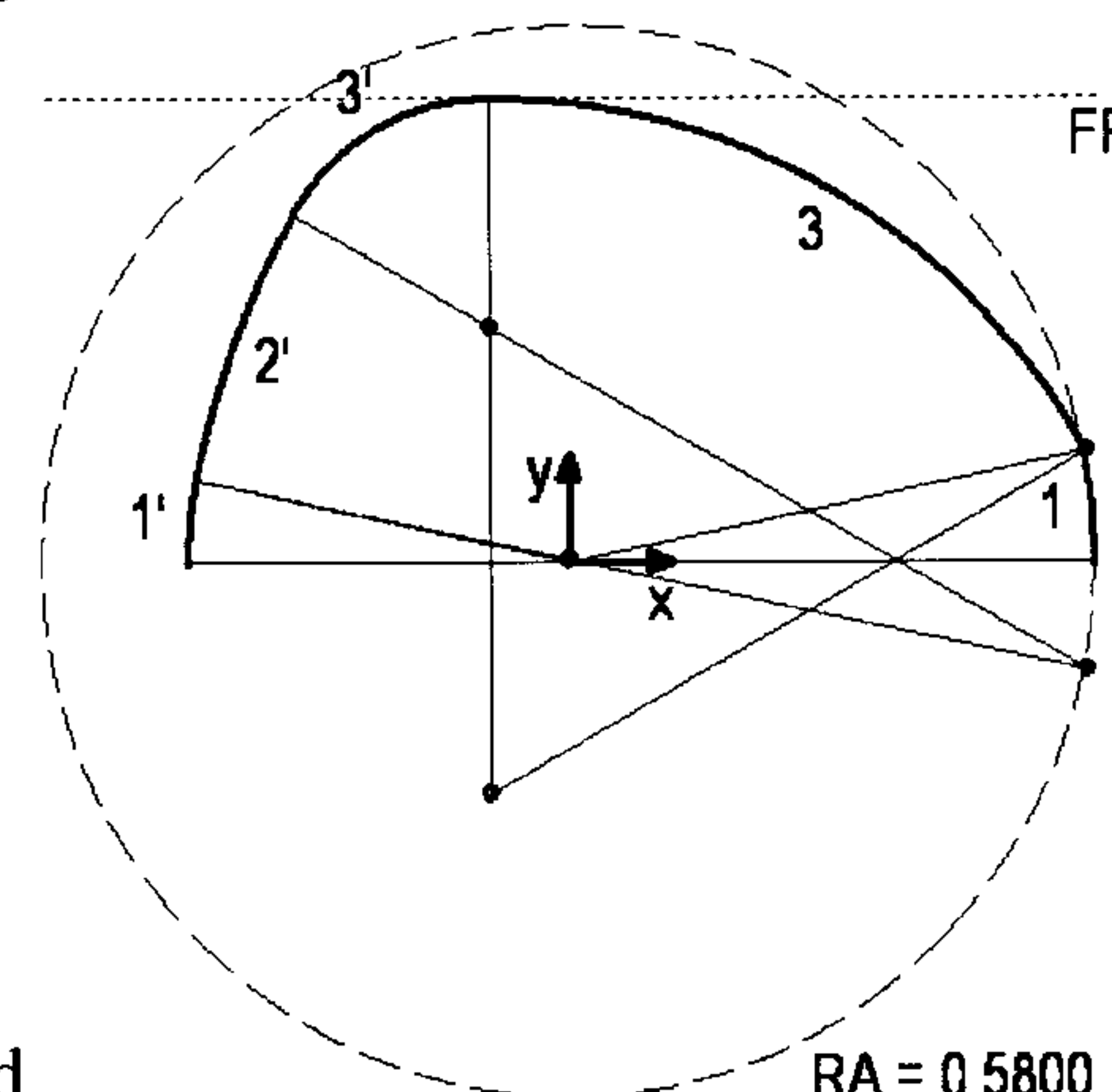


Figure 10d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |
| 2) | $R = 0.0000$ | $M_x = 0.5675$ |
| | $\alpha = 0.3076$ | $M_y = 0.1197$ |
| 3) | $R = 0.7500$ | $M_x = -0.0850$ |
| | $\alpha = 1.0553$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = -0.0850$ |
| | $\alpha = 1.0553$ | $M_y = 0.2500$ |
| 2') | $R = 1.0000$ | $M_x = 0.5675$ |
| | $\alpha = 0.3076$ | $M_y = -0.1197$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |

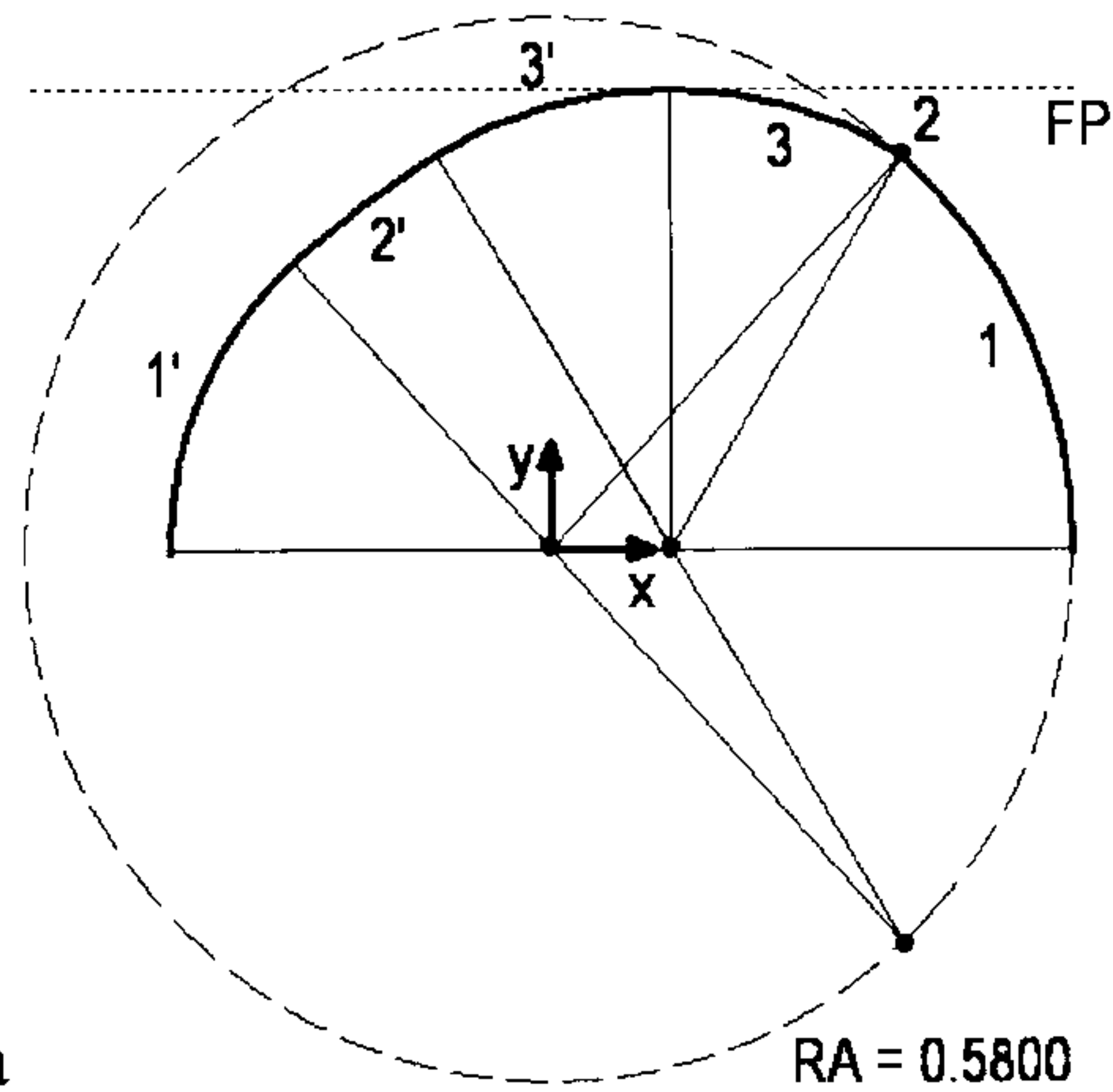


Figure 11a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.8315$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.3908$ |
| | $\alpha = 0.1983$ | $My = 0.4286$ |
| 3) | $R = 0.5000$ | $Mx = 0.1333$ |
| | $\alpha = 0.5411$ | $My = 0.0000$ |
| 3') | $R = 0.5000$ | $Mx = 0.1333$ |
| | $\alpha = 0.5411$ | $My = -0.0000$ |
| 2') | $R = 1.0000$ | $Mx = 0.3908$ |
| | $\alpha = 0.1983$ | $My = -0.4286$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.8315$ | $My = 0.0000$ |

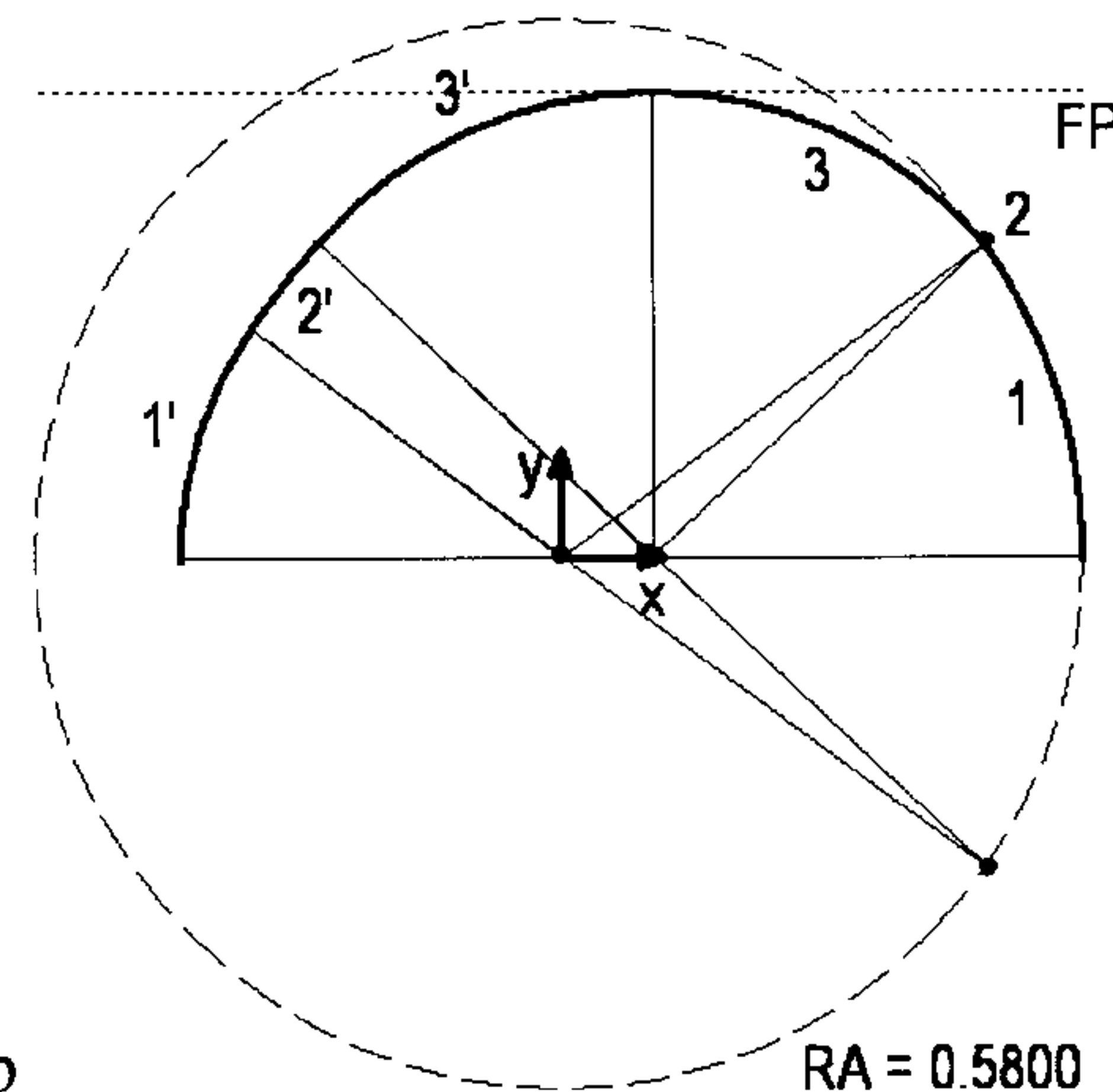


Figure 11b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.6236$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.4708$ |
| | $\alpha = 0.1206$ | $My = 0.3387$ |
| 3) | $R = 0.5000$ | $Mx = 0.1030$ |
| | $\alpha = 0.8266$ | $My = 0.0000$ |
| 3') | $R = 0.5000$ | $Mx = 0.1030$ |
| | $\alpha = 0.8266$ | $My = -0.0000$ |
| 2') | $R = 1.0000$ | $Mx = 0.4708$ |
| | $\alpha = 0.1206$ | $My = -0.3387$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.6236$ | $My = 0.0000$ |

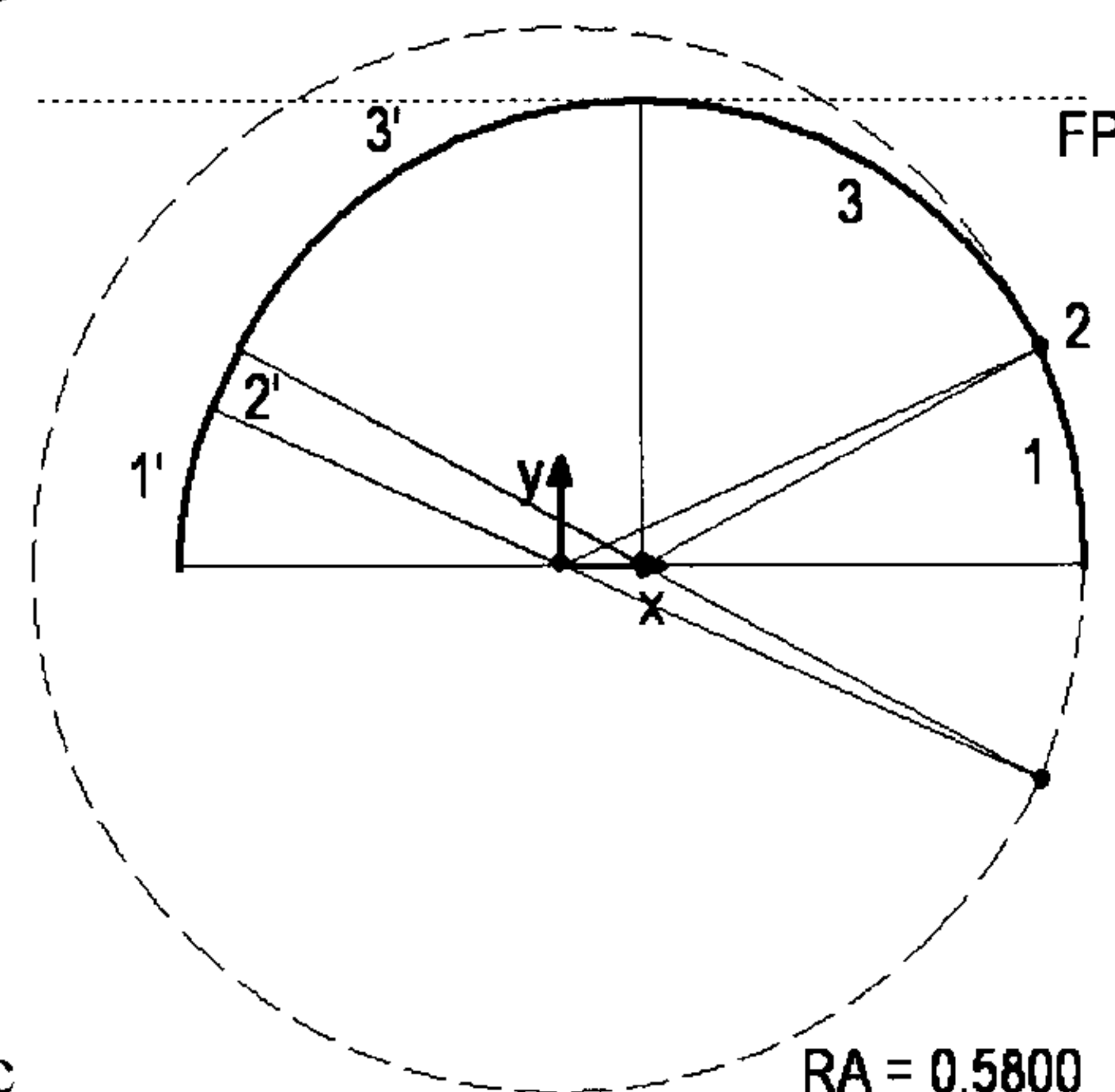


Figure 11c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.4157$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5306$ |
| | $\alpha = 0.0718$ | $My = 0.2342$ |
| 3) | $R = 0.5000$ | $Mx = 0.0889$ |
| | $\alpha = 1.0832$ | $My = -0.0000$ |
| 3') | $R = 0.5000$ | $Mx = 0.0889$ |
| | $\alpha = 1.0832$ | $My = 0.0000$ |
| 2') | $R = 1.0000$ | $Mx = 0.5306$ |
| | $\alpha = 0.0718$ | $My = -0.2342$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.4157$ | $My = 0.0000$ |

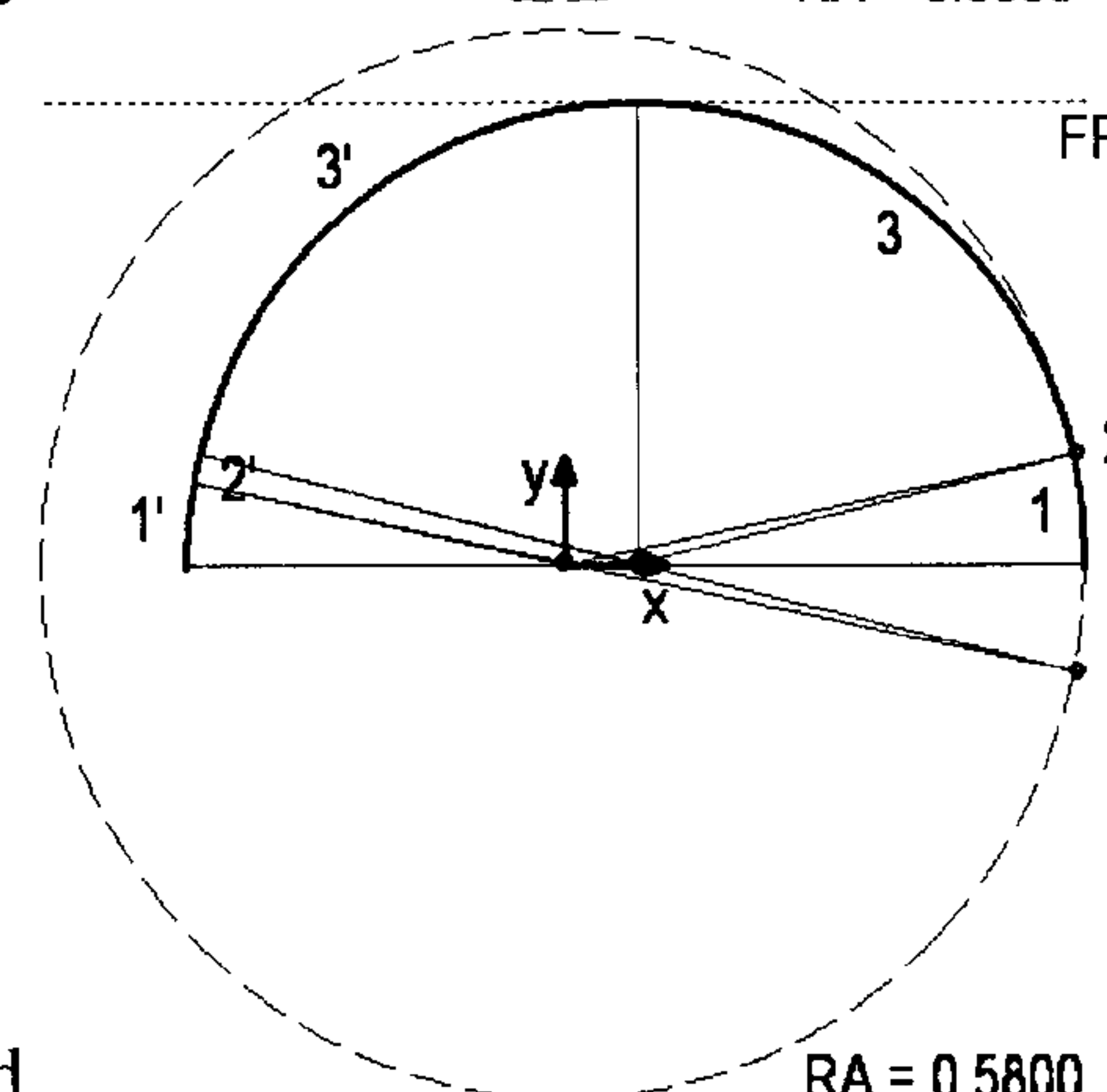


Figure 11d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2079$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5675$ |
| | $\alpha = 0.0339$ | $My = 0.1197$ |
| 3) | $R = 0.5000$ | $Mx = 0.0821$ |
| | $\alpha = 1.3291$ | $My = 0.0000$ |
| 3') | $R = 0.5000$ | $Mx = 0.0821$ |
| | $\alpha = 1.3291$ | $My = -0.0000$ |
| 2') | $R = 1.0000$ | $Mx = 0.5675$ |
| | $\alpha = 0.0339$ | $My = -0.1197$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2079$ | $My = 0.0000$ |

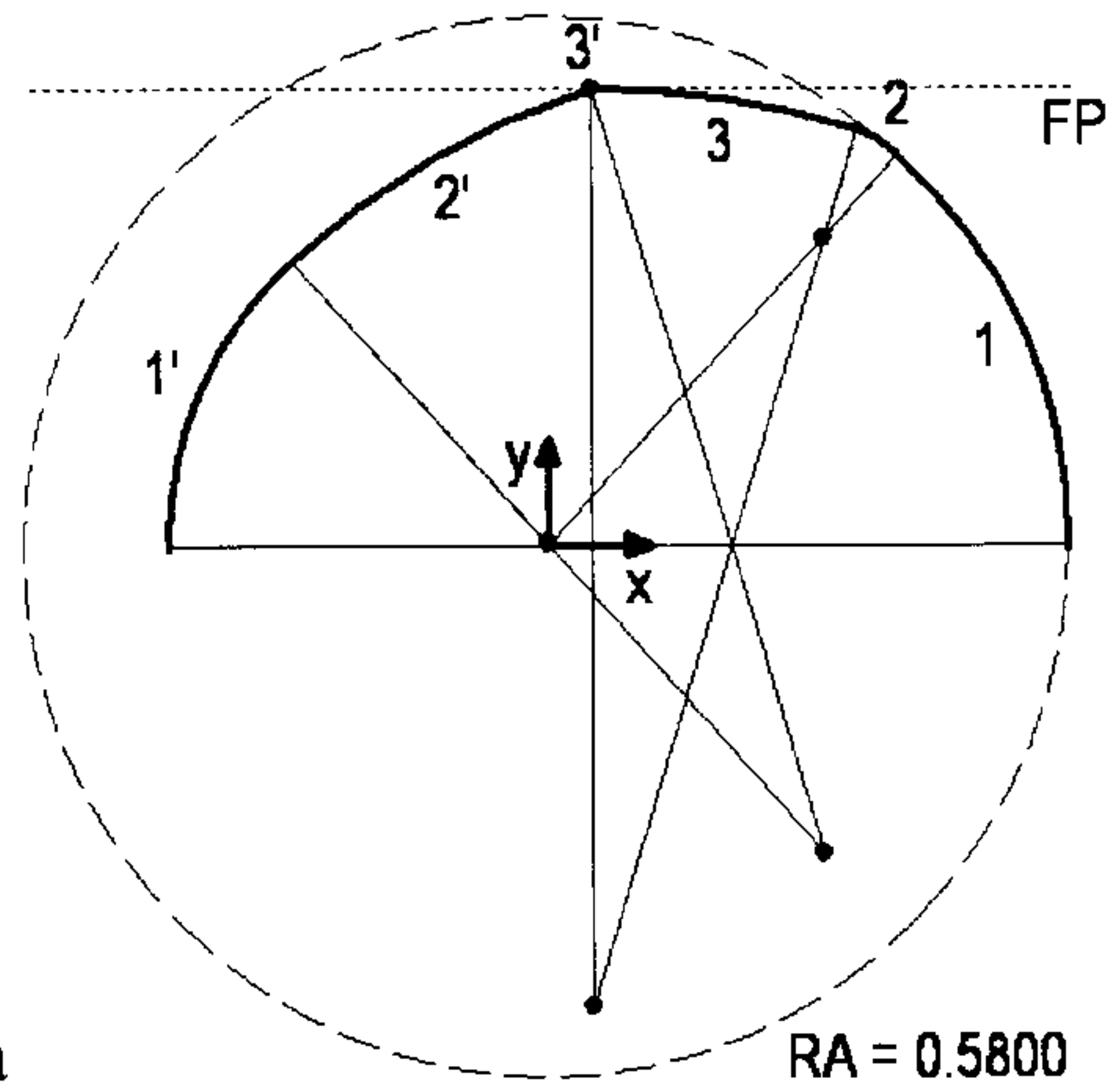


Figure 12a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.3066$ |
| | $\alpha = 0.4404$ | $M_y = 0.3362$ |
| 3) | $R = 1.0000$ | $M_x = 0.0489$ |
| | $\alpha = 0.2989$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = 0.0489$ |
| | $\alpha = 0.2989$ | $M_y = 0.5000$ |
| 2') | $R = 0.8750$ | $M_x = 0.3066$ |
| | $\alpha = 0.4404$ | $M_y = -0.3362$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |

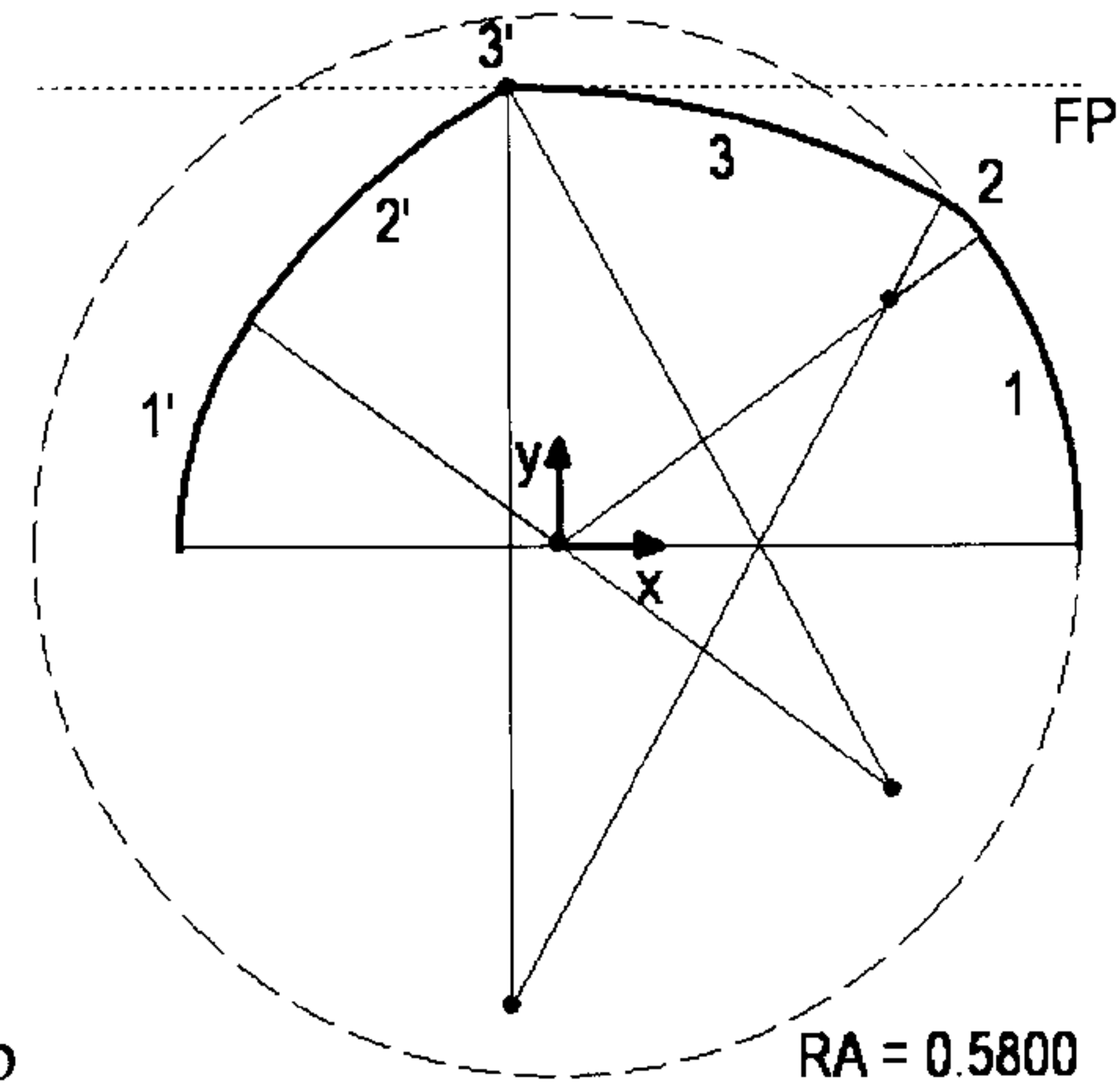


Figure 12b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.3694$ |
| | $\alpha = 0.4420$ | $M_y = 0.2657$ |
| 3) | $R = 1.0000$ | $M_x = -0.0541$ |
| | $\alpha = 0.5052$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.0541$ |
| | $\alpha = 0.5052$ | $M_y = 0.5000$ |
| 2') | $R = 0.8750$ | $M_x = 0.3694$ |
| | $\alpha = 0.4420$ | $M_y = -0.2657$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |

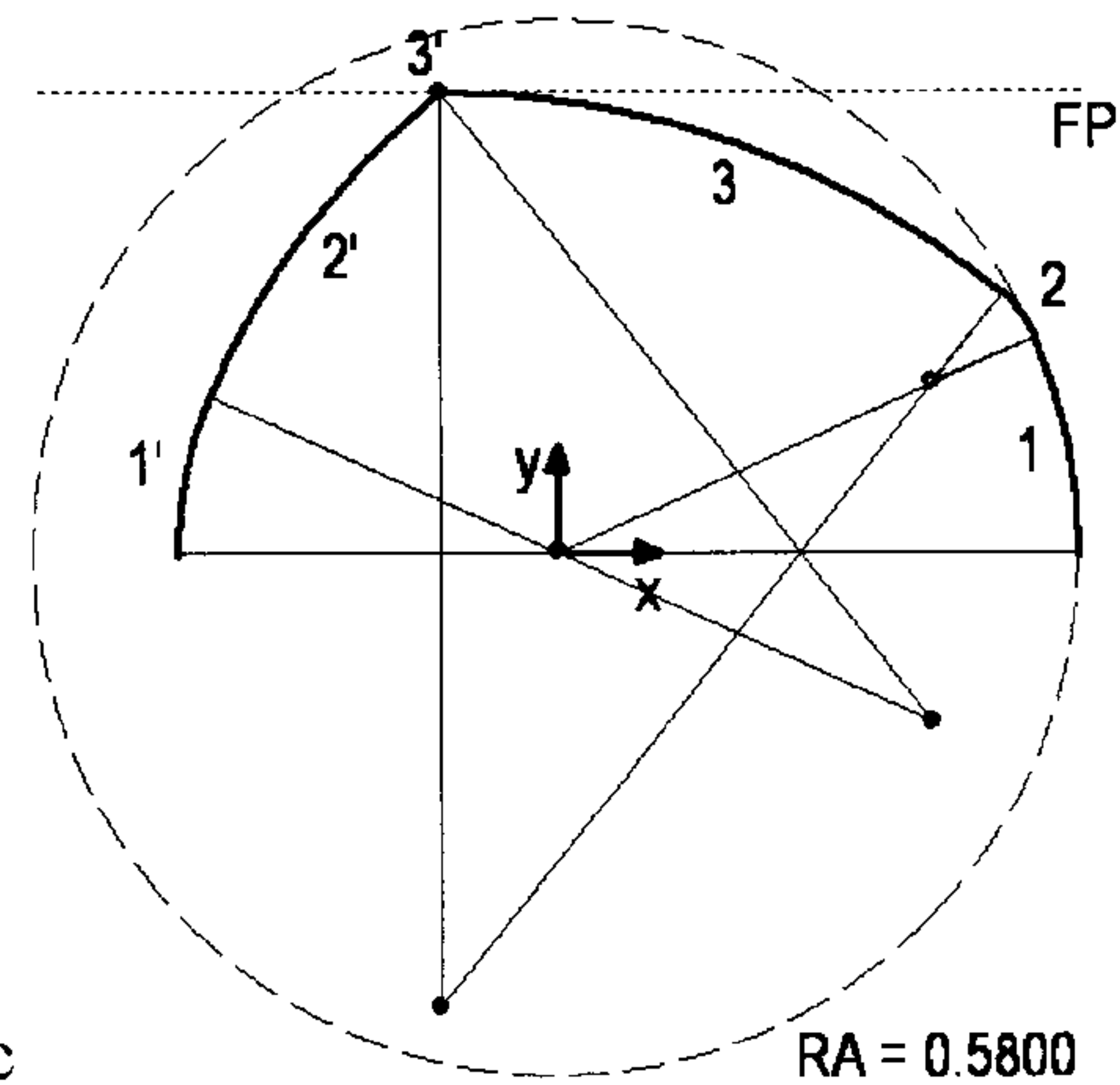


Figure 12c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.4162$ |
| | $\alpha = 0.4812$ | $M_y = 0.1838$ |
| 3) | $R = 1.0000$ | $M_x = -0.1297$ |
| | $\alpha = 0.6738$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.1297$ |
| | $\alpha = 0.6738$ | $M_y = 0.5000$ |
| 2') | $R = 0.8750$ | $M_x = 0.4162$ |
| | $\alpha = 0.4812$ | $M_y = -0.1838$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |

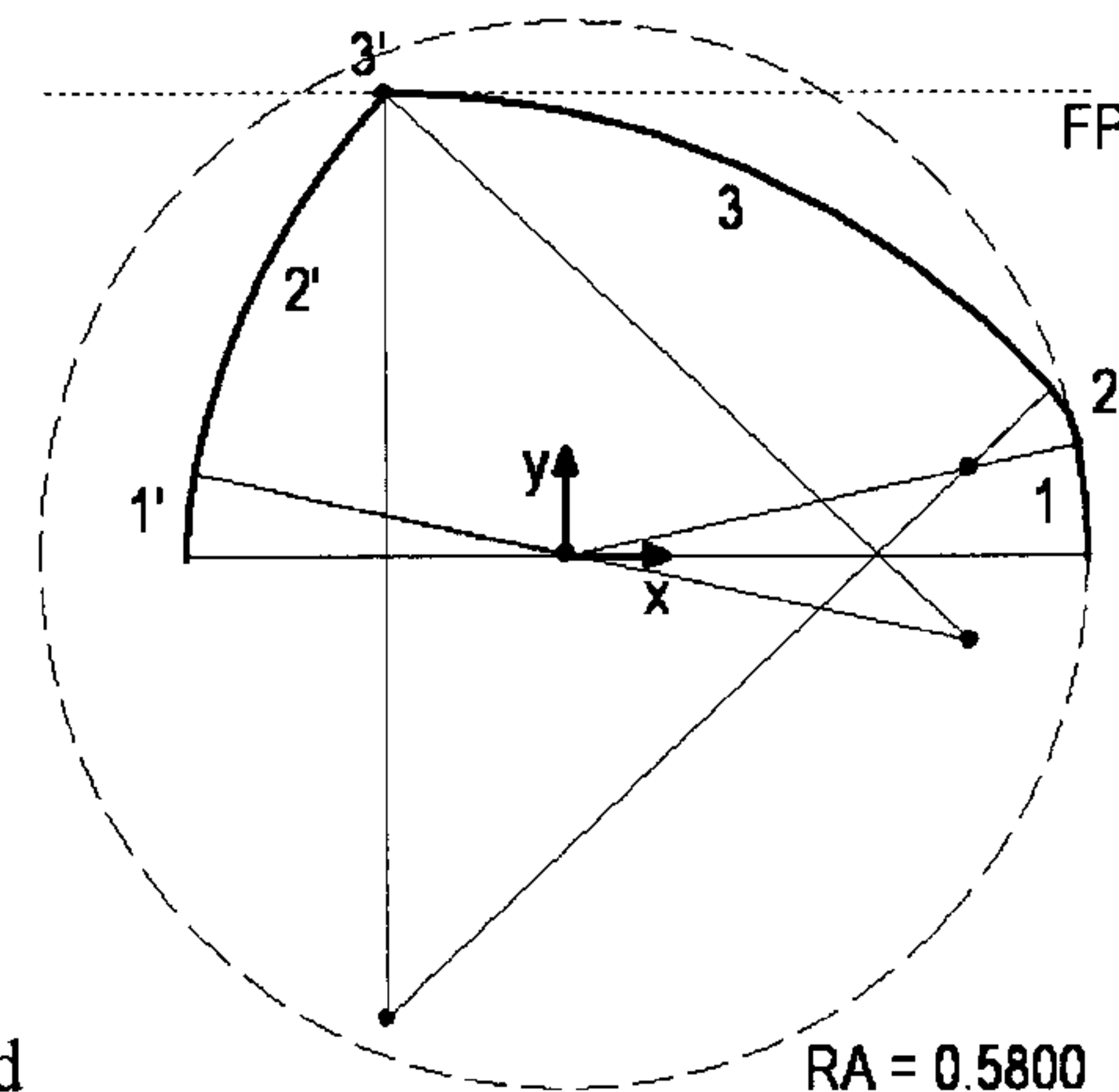


Figure 12d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.4452$ |
| | $\alpha = 0.5382$ | $M_y = 0.0939$ |
| 3) | $R = 1.0000$ | $M_x = -0.1974$ |
| | $\alpha = 0.8247$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.1974$ |
| | $\alpha = 0.8247$ | $M_y = 0.5000$ |
| 2') | $R = 0.8750$ | $M_x = 0.4452$ |
| | $\alpha = 0.5382$ | $M_y = -0.0939$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |

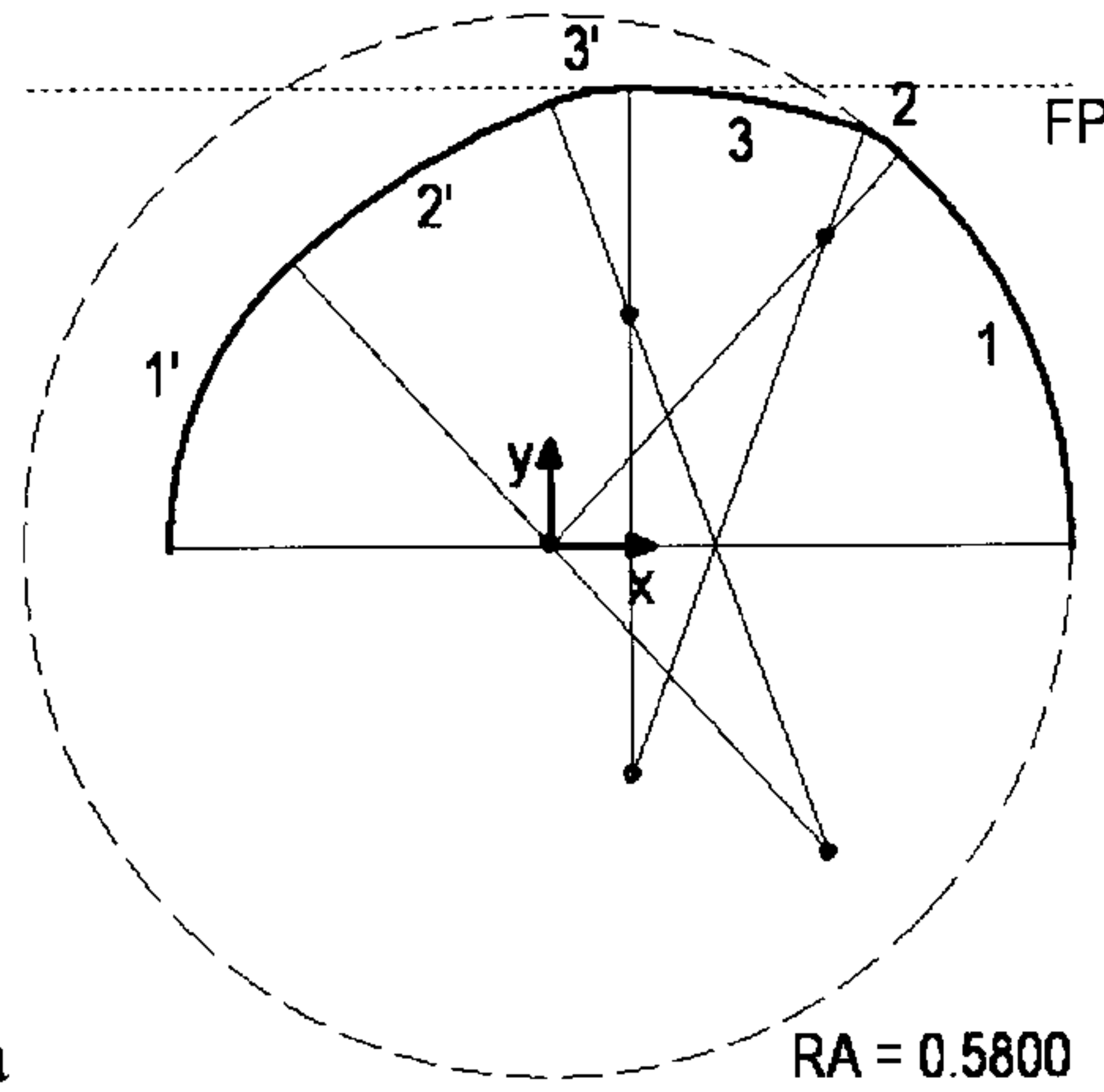


Figure 13a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.3066$ |
| | $\alpha = 0.3852$ | $M_y = 0.3362$ |
| 3) | $R = 0.7500$ | $M_x = 0.0898$ |
| | $\alpha = 0.3542$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = 0.0898$ |
| | $\alpha = 0.3542$ | $M_y = 0.2500$ |
| 2') | $R = 0.8750$ | $M_x = 0.3066$ |
| | $\alpha = 0.3852$ | $M_y = -0.3362$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |

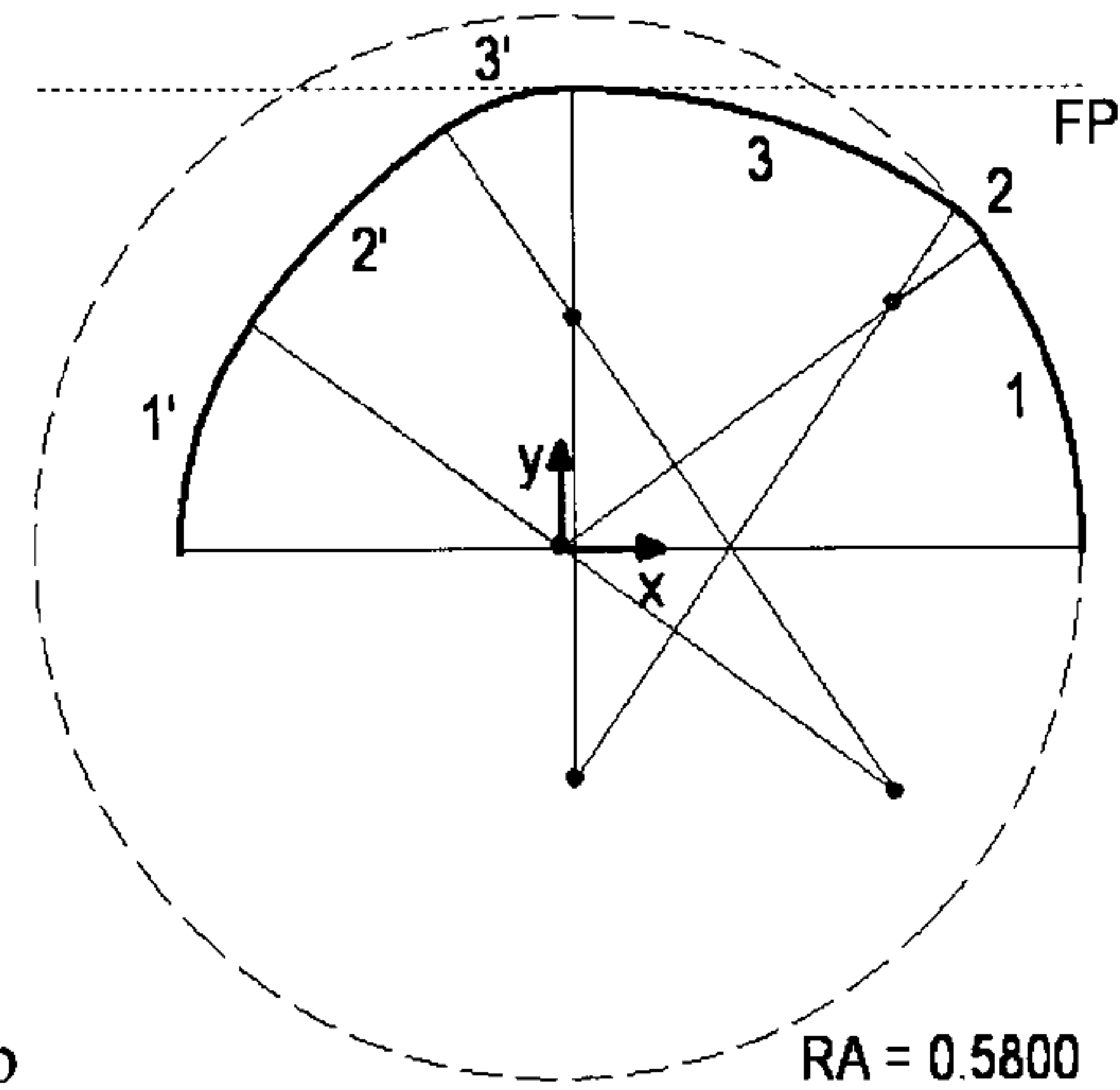


Figure 13b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.3694$ |
| | $\alpha = 0.3468$ | $M_y = 0.2657$ |
| 3) | $R = 0.7500$ | $M_x = 0.0163$ |
| | $\alpha = 0.6004$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = 0.0163$ |
| | $\alpha = 0.6004$ | $M_y = 0.2500$ |
| 2') | $R = 0.8750$ | $M_x = 0.3694$ |
| | $\alpha = 0.3468$ | $M_y = -0.2657$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |

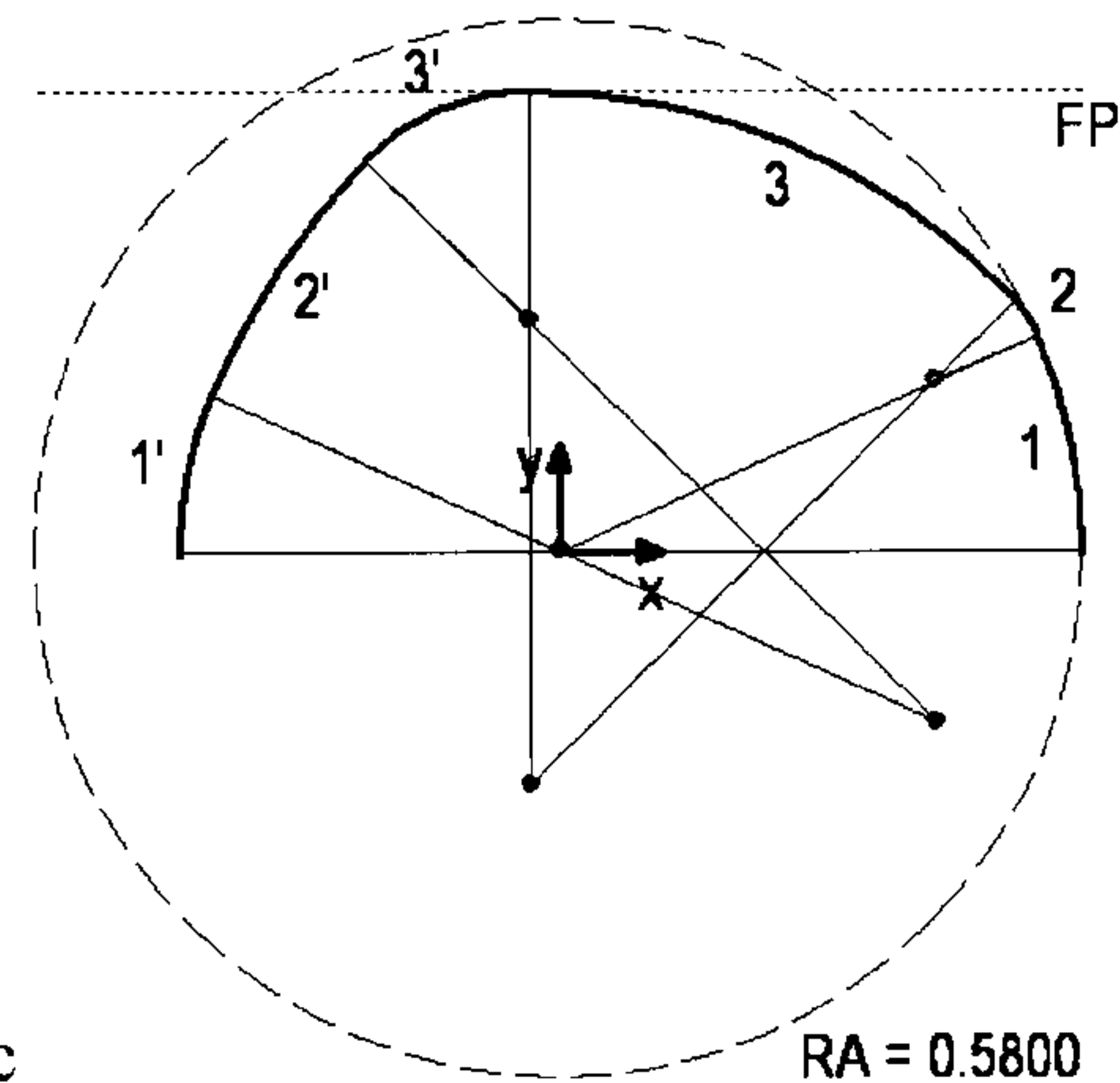


Figure 13c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.4162$ |
| | $\alpha = 0.3513$ | $M_y = 0.1838$ |
| 3) | $R = 0.7500$ | $M_x = -0.0337$ |
| | $\alpha = 0.8037$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = -0.0337$ |
| | $\alpha = 0.8037$ | $M_y = 0.2500$ |
| 2') | $R = 0.8750$ | $M_x = 0.4162$ |
| | $\alpha = 0.3513$ | $M_y = -0.1838$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |

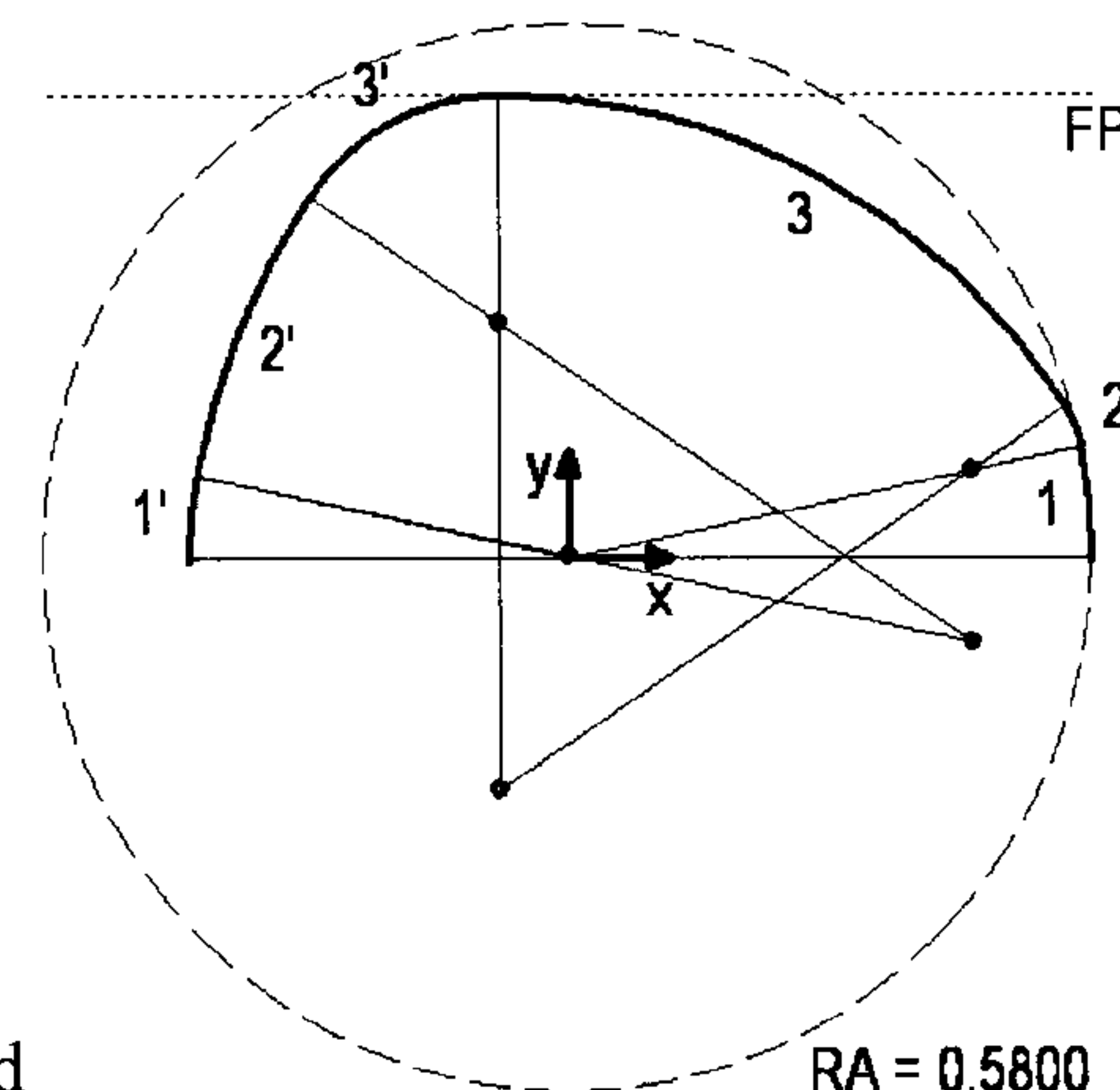


Figure 13d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |
| 2) | $R = 0.1250$ | $M_x = 0.4452$ |
| | $\alpha = 0.3748$ | $M_y = 0.0939$ |
| 3) | $R = 0.7500$ | $M_x = -0.0767$ |
| | $\alpha = 0.9881$ | $M_y = -0.2500$ |
| 3') | $R = 0.2500$ | $M_x = -0.0767$ |
| | $\alpha = 0.9881$ | $M_y = 0.2500$ |
| 2') | $R = 0.8750$ | $M_x = 0.4452$ |
| | $\alpha = 0.3748$ | $M_y = -0.0939$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |

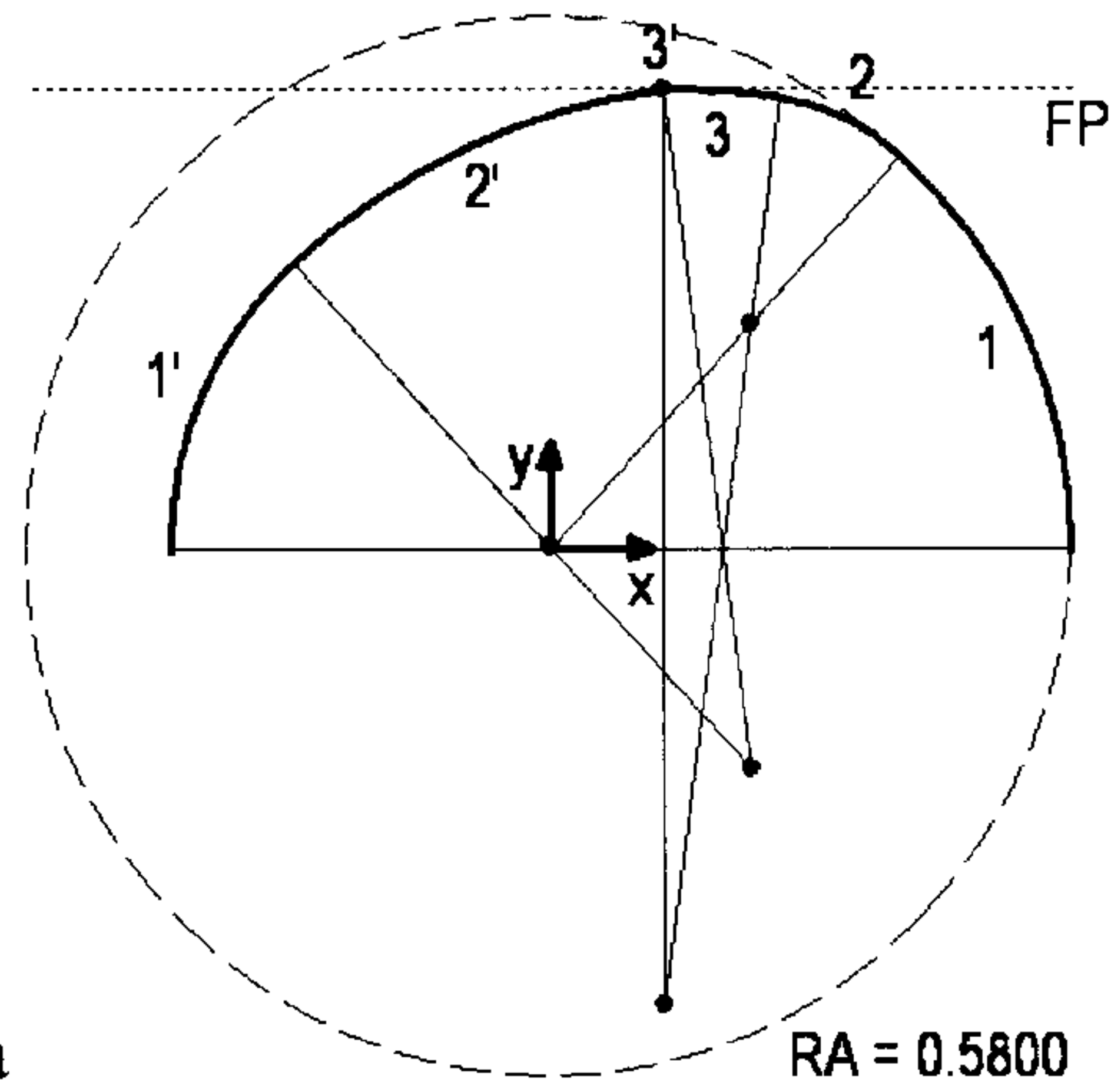


Figure 14a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |
| 2) | $R = 0.2500$ | $M_x = 0.2223$ |
| | $\alpha = 0.6111$ | $M_y = 0.2438$ |
| 3) | $R = 1.0000$ | $M_x = 0.1265$ |
| | $\alpha = 0.1282$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = 0.1265$ |
| | $\alpha = 0.1282$ | $M_y = 0.5000$ |
| 2') | $R = 0.7500$ | $M_x = 0.2223$ |
| | $\alpha = 0.6111$ | $M_y = -0.2438$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.8315$ | $M_y = 0.0000$ |

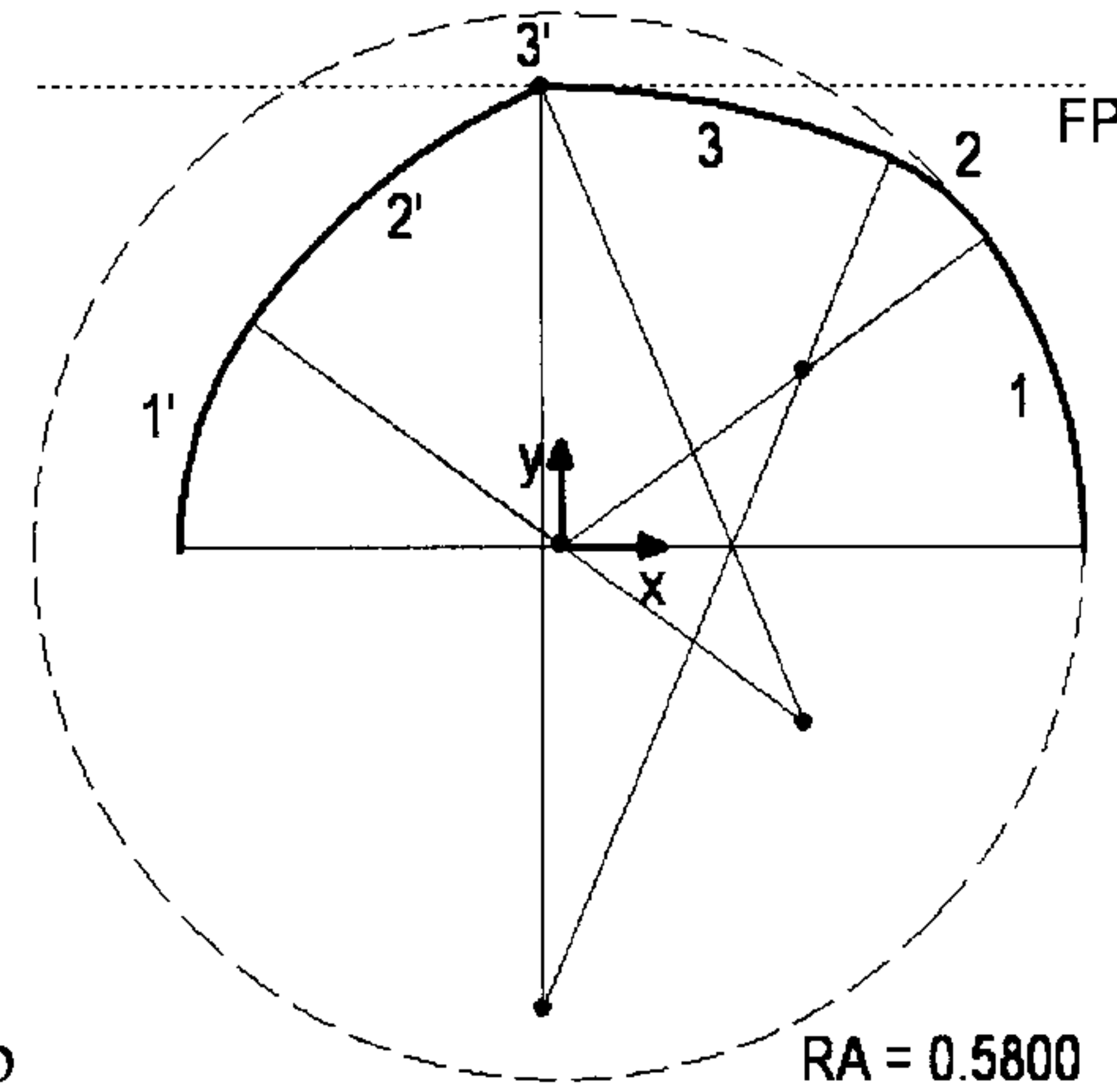


Figure 14b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |
| 2) | $R = 0.2500$ | $M_x = 0.2679$ |
| | $\alpha = 0.5538$ | $M_y = 0.1927$ |
| 3) | $R = 1.0000$ | $M_x = -0.0196$ |
| | $\alpha = 0.3934$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.0196$ |
| | $\alpha = 0.3934$ | $M_y = 0.5000$ |
| 2') | $R = 0.7500$ | $M_x = 0.2679$ |
| | $\alpha = 0.5538$ | $M_y = -0.1927$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.6236$ | $M_y = 0.0000$ |

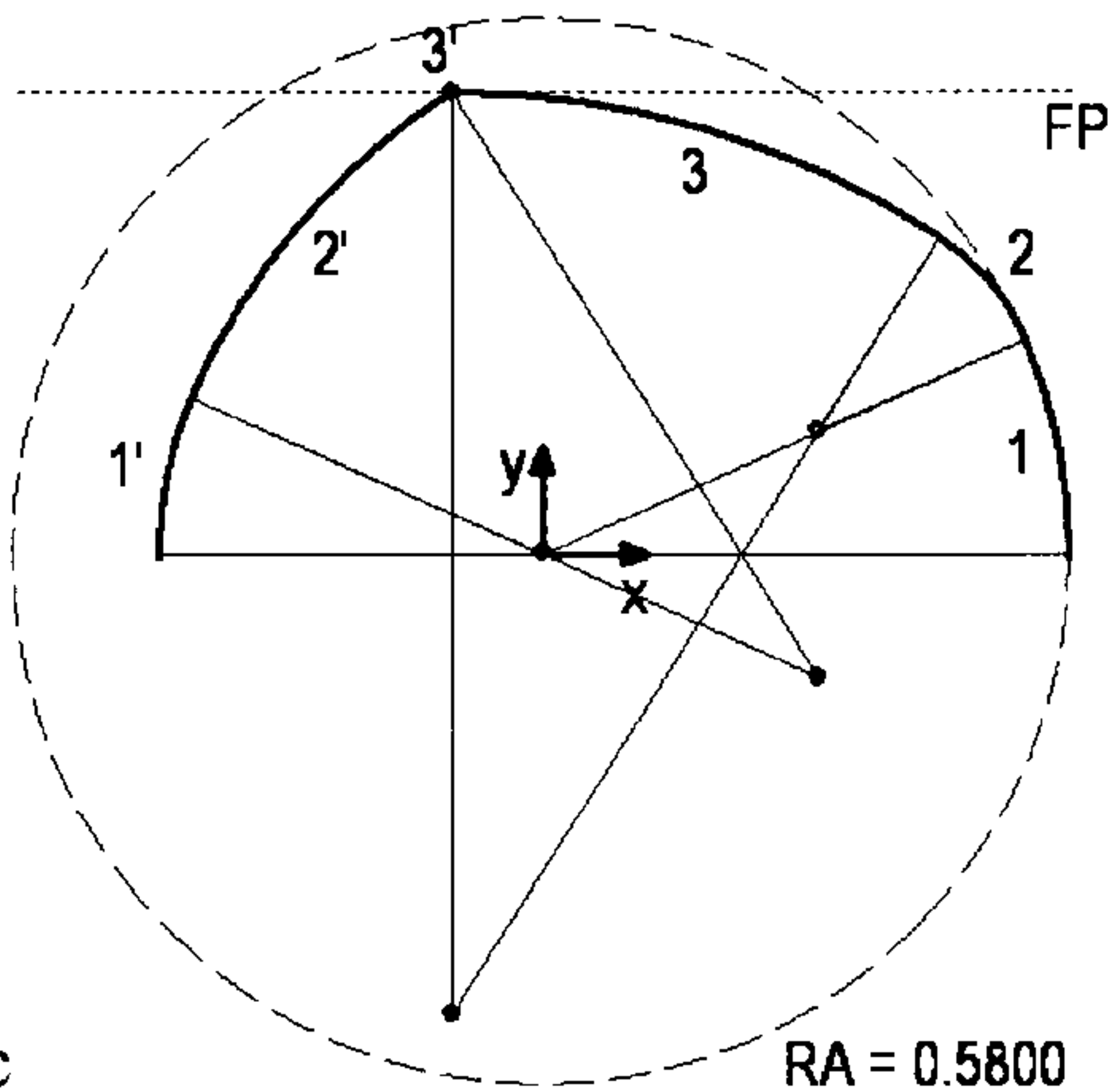


Figure 14c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |
| 2) | $R = 0.2500$ | $M_x = 0.3019$ |
| | $\alpha = 0.5896$ | $M_y = 0.1333$ |
| 3) | $R = 1.0000$ | $M_x = -0.0999$ |
| | $\alpha = 0.5654$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.0999$ |
| | $\alpha = 0.5654$ | $M_y = 0.5000$ |
| 2') | $R = 0.7500$ | $M_x = 0.3019$ |
| | $\alpha = 0.5896$ | $M_y = -0.1333$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.4157$ | $M_y = 0.0000$ |

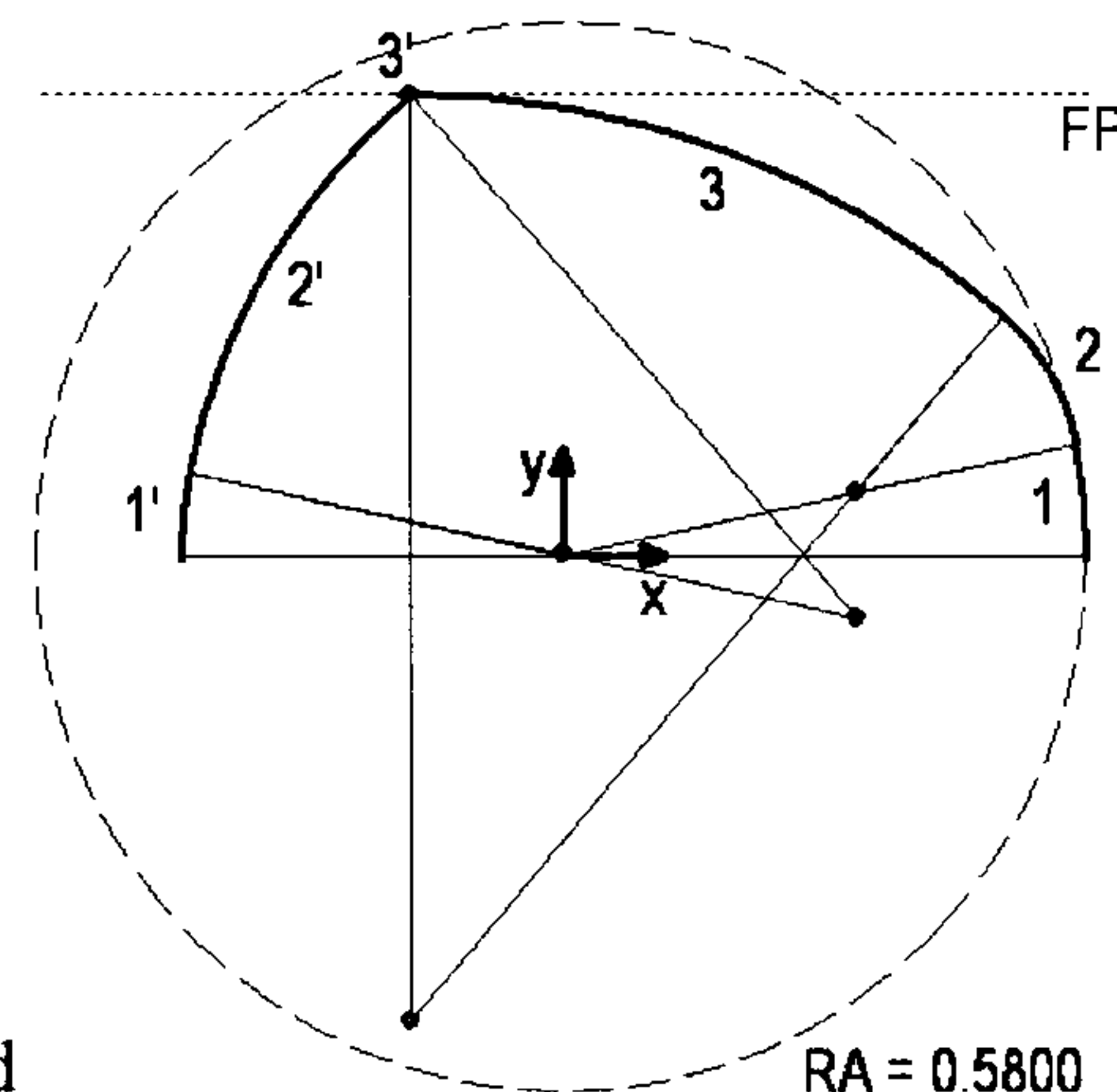


Figure 14d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |
| 2) | $R = 0.2500$ | $M_x = 0.3229$ |
| | $\alpha = 0.6516$ | $M_y = 0.0681$ |
| 3) | $R = 1.0000$ | $M_x = -0.1668$ |
| | $\alpha = 0.7114$ | $M_y = -0.5000$ |
| 3') | $R = 0.0000$ | $M_x = -0.1668$ |
| | $\alpha = 0.7114$ | $M_y = 0.5000$ |
| 2') | $R = 0.7500$ | $M_x = 0.3229$ |
| | $\alpha = 0.6516$ | $M_y = -0.0681$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2079$ | $M_y = 0.0000$ |

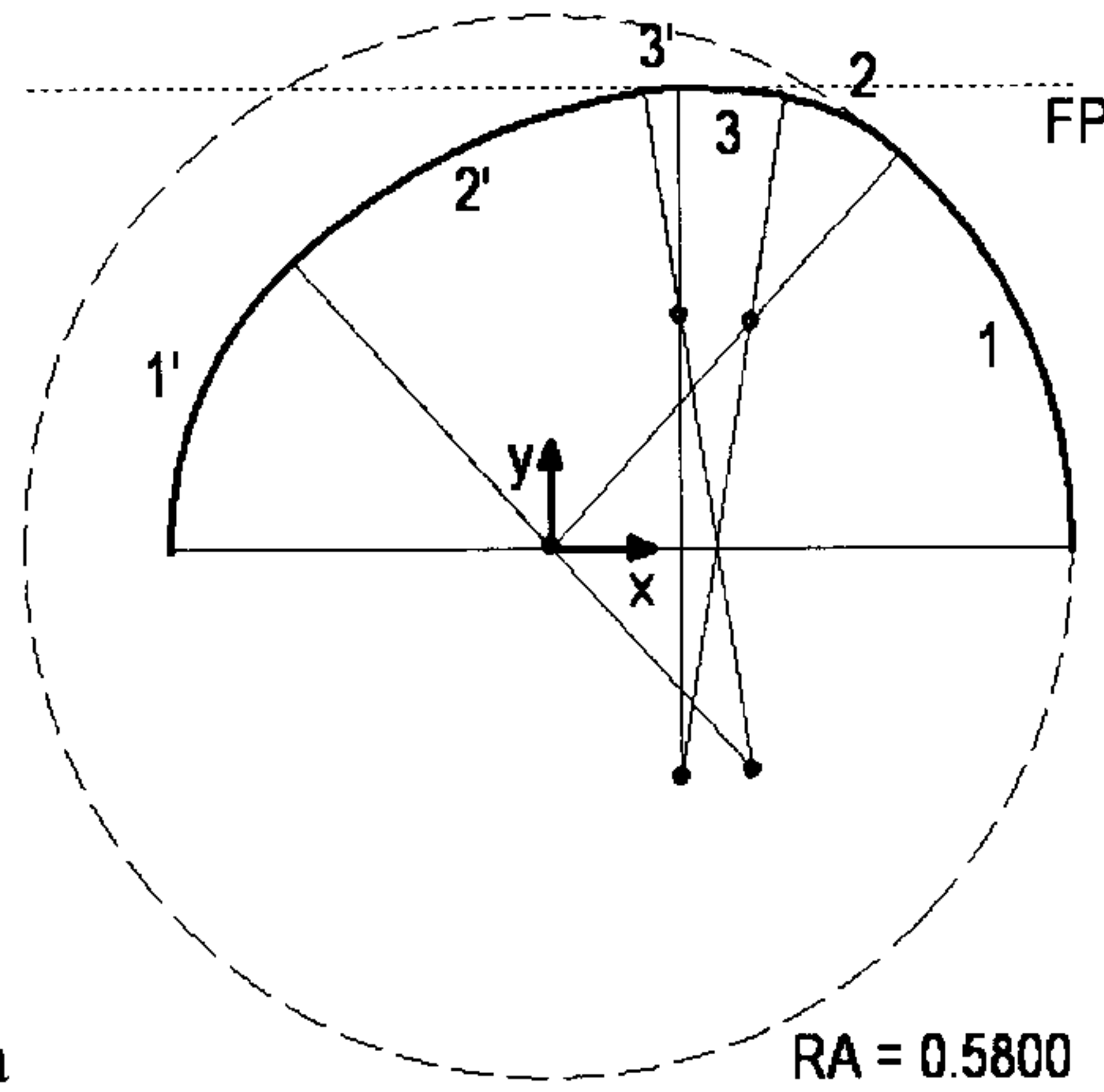


Figure 15a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.8315$ | $My = 0.0000$ |
| 2) | $R = 0.2500$ | $Mx = 0.2223$ |
| | $\alpha = 0.5823$ | $My = 0.2438$ |
| 3) | $R = 0.7500$ | $Mx = 0.1441$ |
| | $\alpha = 0.1571$ | $My = -0.2500$ |
| 3') | $R = 0.2500$ | $Mx = 0.1441$ |
| | $\alpha = 0.1571$ | $My = 0.2500$ |
| 2') | $R = 0.7500$ | $Mx = 0.2223$ |
| | $\alpha = 0.5823$ | $My = -0.2438$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.8315$ | $My = 0.0000$ |

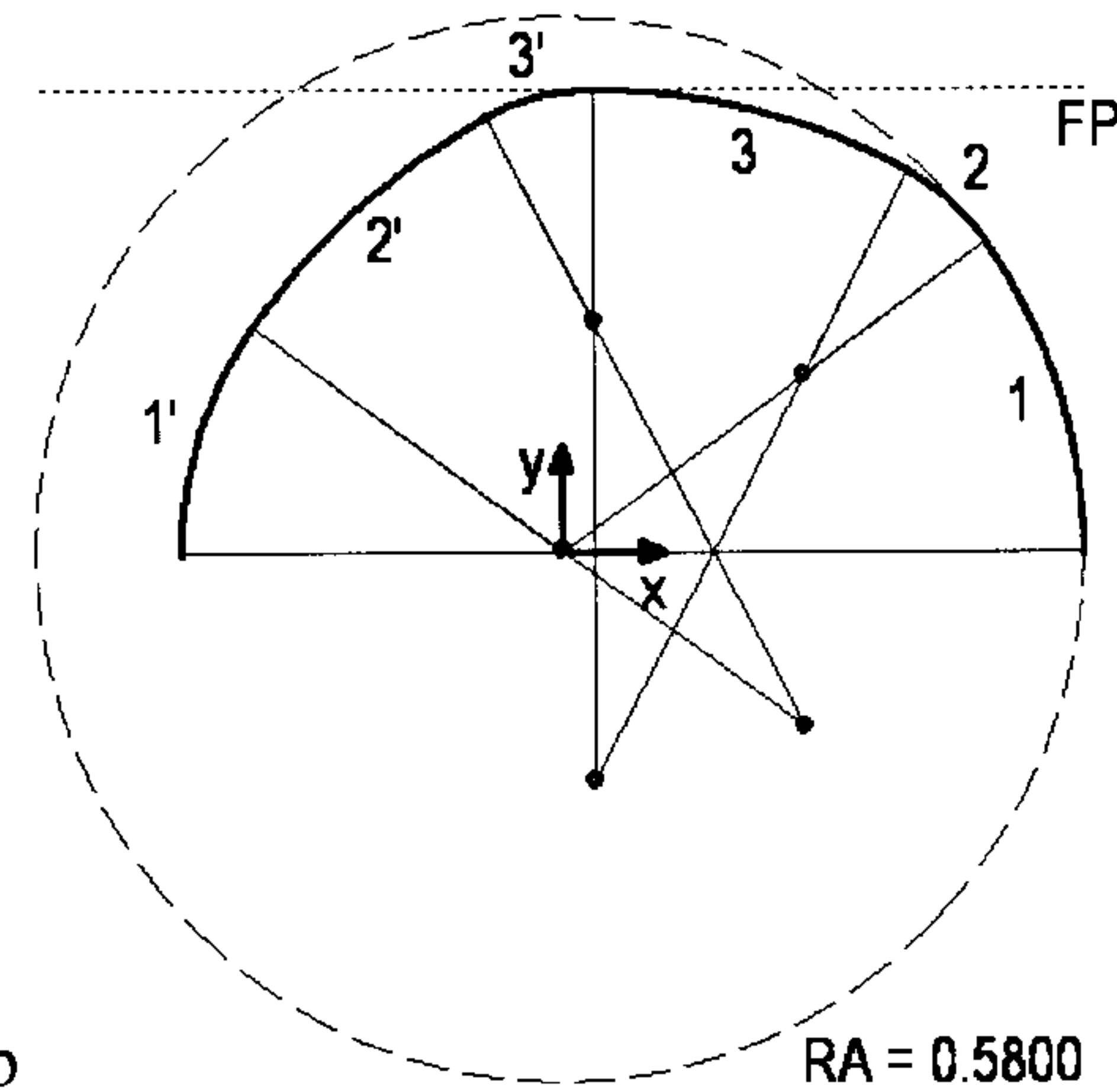


Figure 15b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.6236$ | $My = 0.0000$ |
| 2) | $R = 0.2500$ | $Mx = 0.2679$ |
| | $\alpha = 0.4638$ | $My = 0.1927$ |
| 3) | $R = 0.7500$ | $Mx = 0.0355$ |
| | $\alpha = 0.4834$ | $My = -0.2500$ |
| 3') | $R = 0.2500$ | $Mx = 0.0355$ |
| | $\alpha = 0.4834$ | $My = 0.2500$ |
| 2') | $R = 0.7500$ | $Mx = 0.2679$ |
| | $\alpha = 0.4638$ | $My = -0.1927$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.6236$ | $My = 0.0000$ |

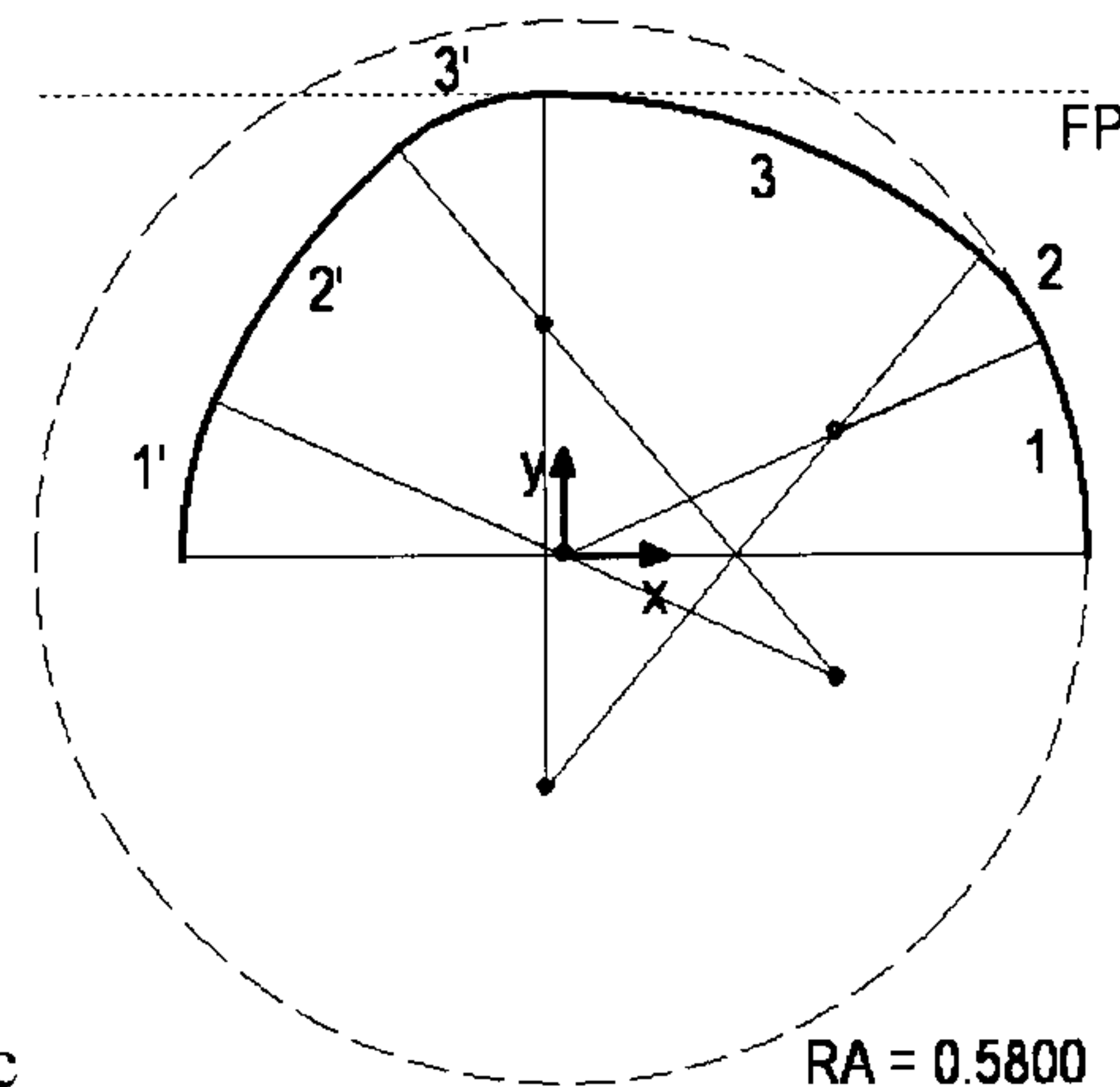


Figure 15c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.4157$ | $My = 0.0000$ |
| 2) | $R = 0.2500$ | $Mx = 0.3019$ |
| | $\alpha = 0.4577$ | $My = 0.1333$ |
| 3) | $R = 0.7500$ | $Mx = -0.0192$ |
| | $\alpha = 0.6973$ | $My = -0.2500$ |
| 3') | $R = 0.2500$ | $Mx = -0.0192$ |
| | $\alpha = 0.6973$ | $My = 0.2500$ |
| 2') | $R = 0.7500$ | $Mx = 0.3019$ |
| | $\alpha = 0.4577$ | $My = -0.1333$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.4157$ | $My = 0.0000$ |

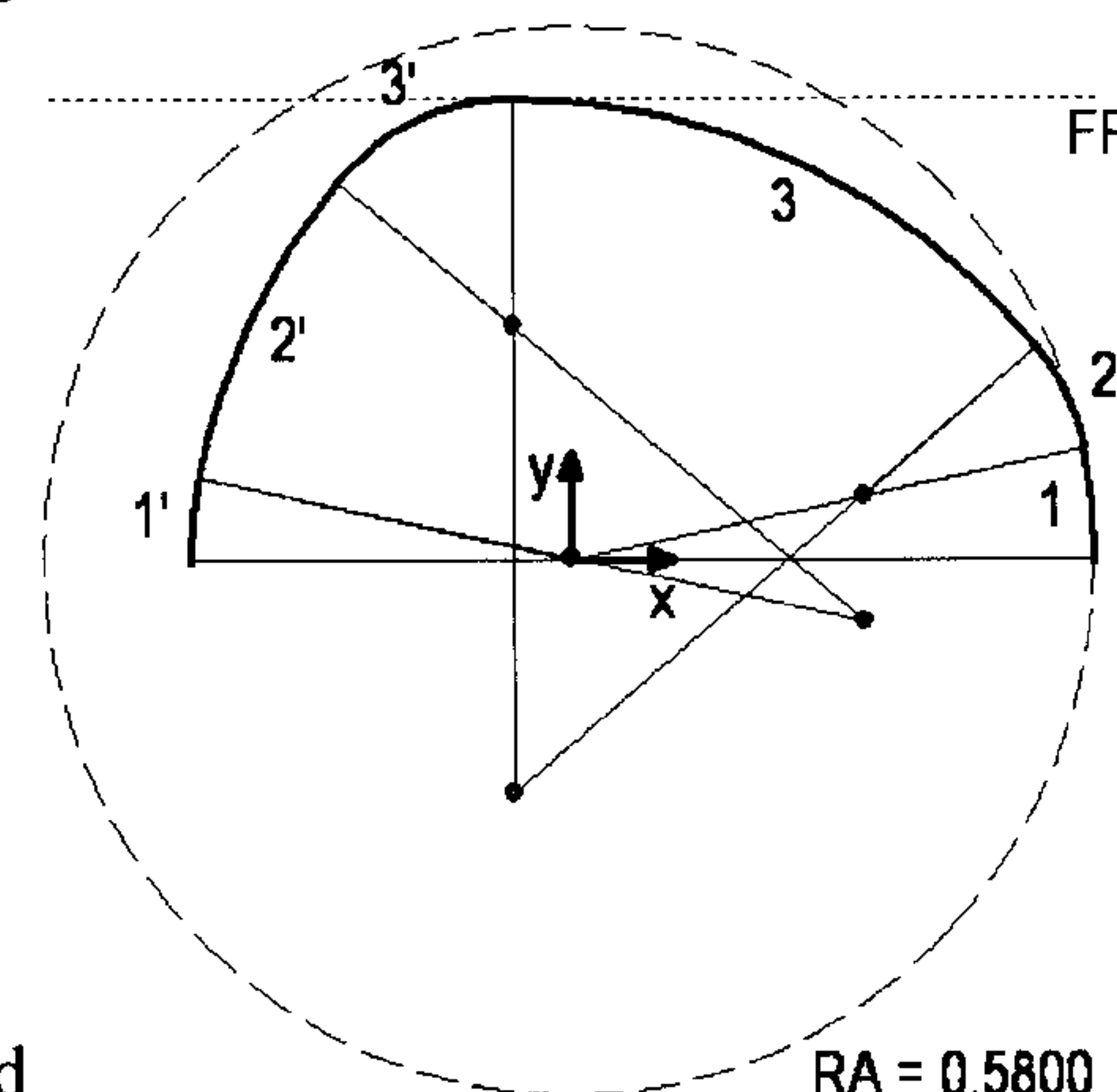


Figure 15d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2079$ | $My = 0.0000$ |
| 2) | $R = 0.2500$ | $Mx = 0.3229$ |
| | $\alpha = 0.4817$ | $My = 0.0681$ |
| 3) | $R = 0.7500$ | $Mx = -0.0629$ |
| | $\alpha = 0.8812$ | $My = -0.2500$ |
| 3') | $R = 0.2500$ | $Mx = -0.0629$ |
| | $\alpha = 0.8812$ | $My = 0.2500$ |
| 2') | $R = 0.7500$ | $Mx = 0.3229$ |
| | $\alpha = 0.4817$ | $My = -0.0681$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2079$ | $My = 0.0000$ |

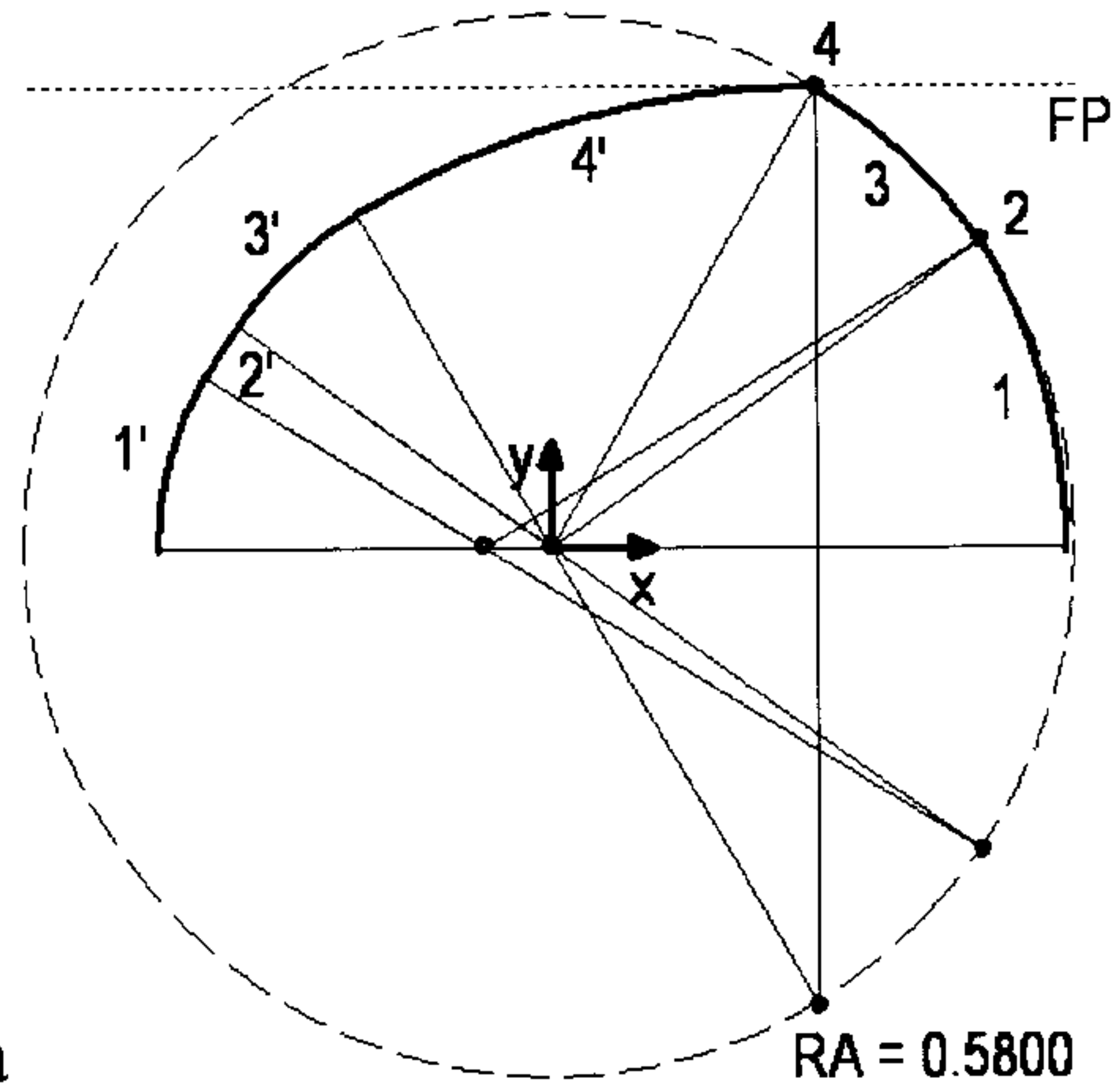


Figure 16a

- 1) $R = 0.6422$ $M_x = -0.0742$
 $\alpha = 0.5446$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.4751$
 $\alpha = 0.0663$ $M_y = 0.3327$
 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 2') $R = 1.0000$ $M_x = 0.4751$
 $\alpha = 0.0663$ $M_y = -0.3327$
 1') $R = 0.3578$ $M_x = -0.0742$
 $\alpha = 0.5446$ $M_y = 0.0000$

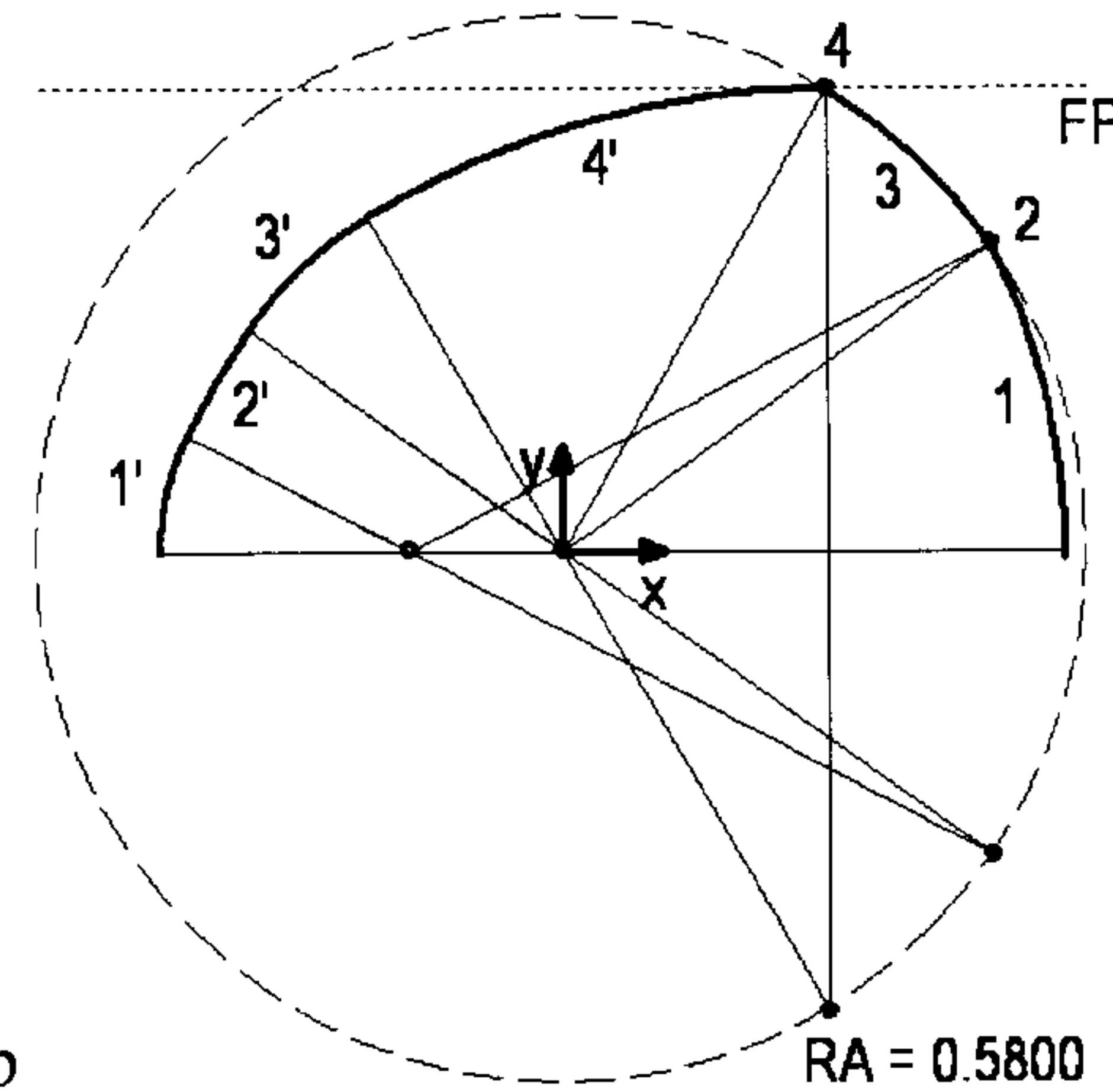


Figure 16b

- 1) $R = 0.7245$ $M_x = -0.1685$
 $\alpha = 0.4771$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.4751$
 $\alpha = 0.1338$ $M_y = 0.3327$
 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 2') $R = 1.0000$ $M_x = 0.4751$
 $\alpha = 0.1338$ $M_y = -0.3327$
 1') $R = 0.2755$ $M_x = -0.1685$
 $\alpha = 0.4771$ $M_y = 0.0000$

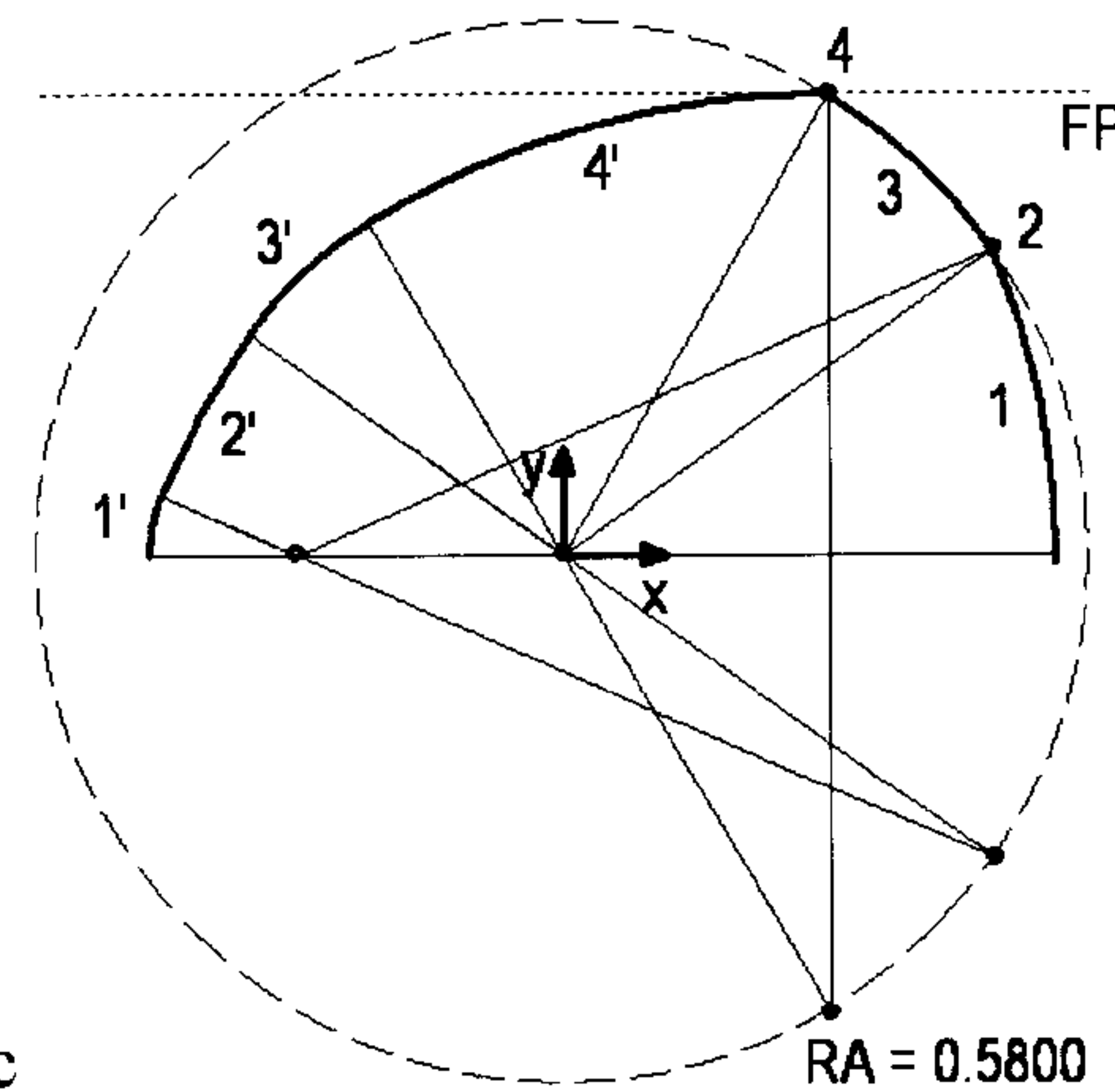


Figure 16c

- 1) $R = 0.8377$ $M_x = -0.2937$
 $\alpha = 0.4084$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.4751$
 $\alpha = 0.2025$ $M_y = 0.3327$
 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 2') $R = 1.0000$ $M_x = 0.4751$
 $\alpha = 0.2025$ $M_y = -0.3327$
 1') $R = 0.1623$ $M_x = -0.2937$
 $\alpha = 0.4084$ $M_y = 0.0000$

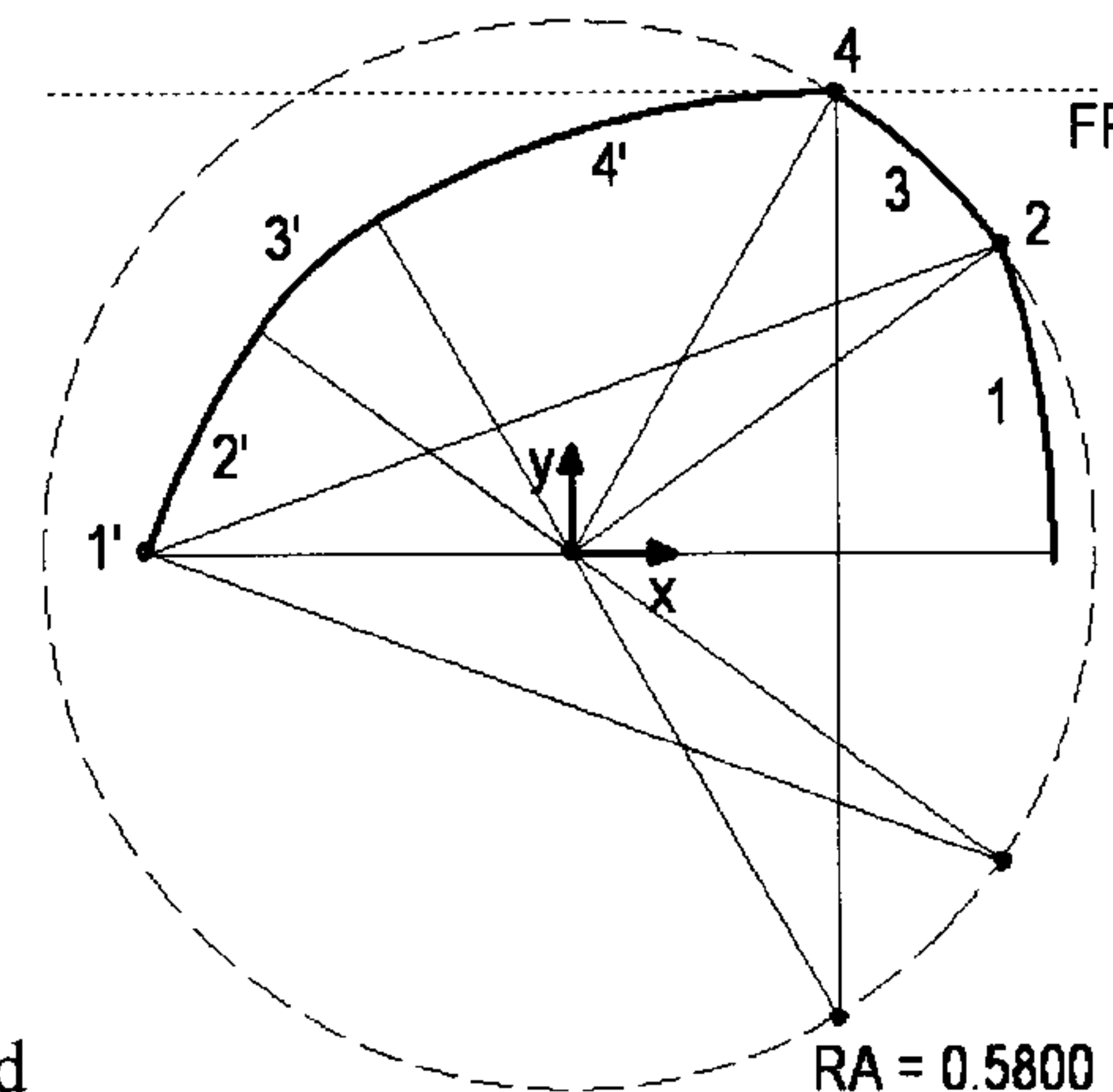


Figure 16d

- 1) $R = 0.9998$ $M_x = -0.4677$
 $\alpha = 0.3392$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.4751$
 $\alpha = 0.2716$ $M_y = 0.3327$
 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.4285$ $M_y = 0.0000$
 2') $R = 1.0000$ $M_x = 0.4751$
 $\alpha = 0.2716$ $M_y = -0.3327$
 1') $R = 0.0002$ $M_x = -0.4677$
 $\alpha = 0.3392$ $M_y = 0.0000$

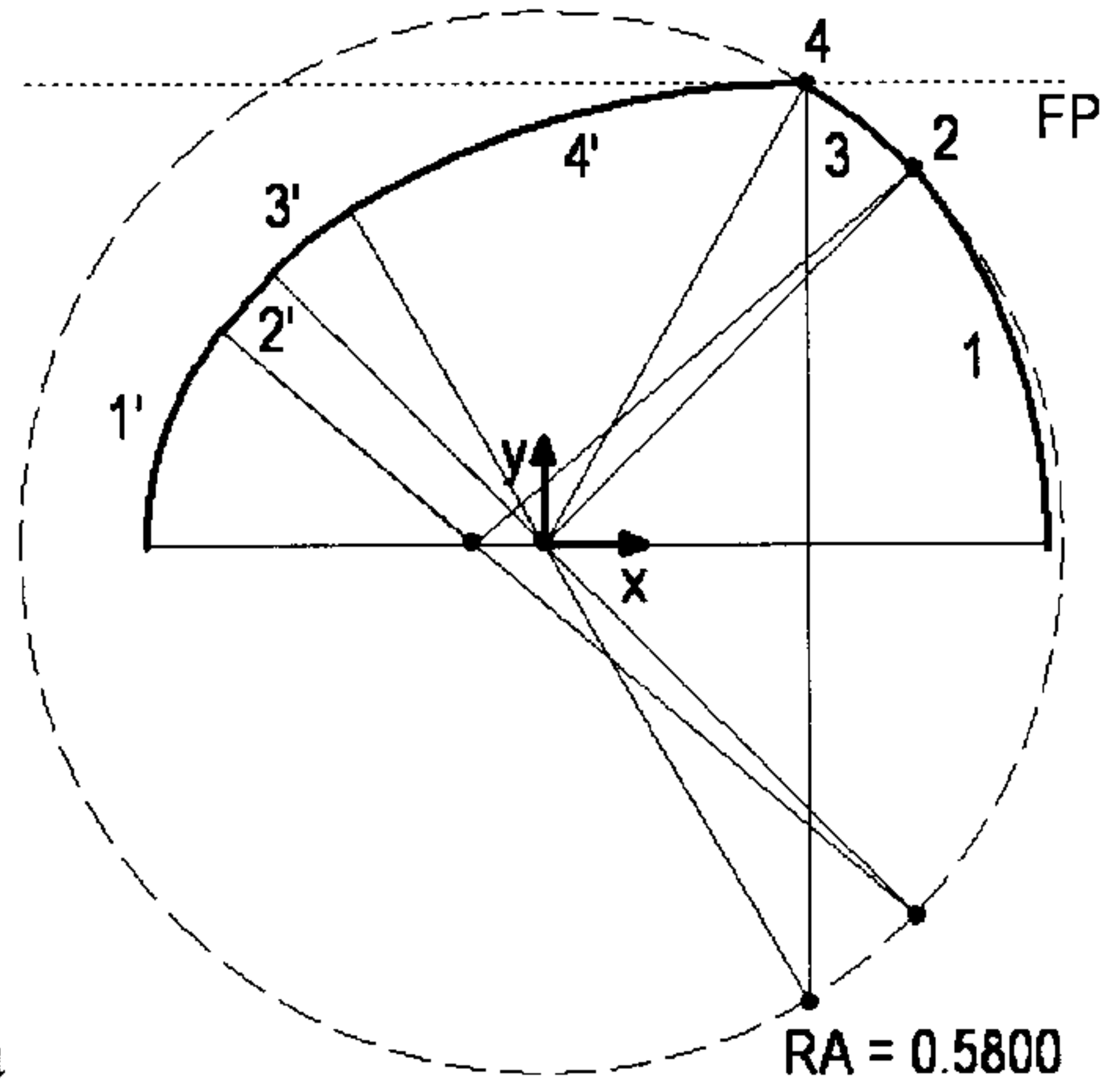


Figure 17a

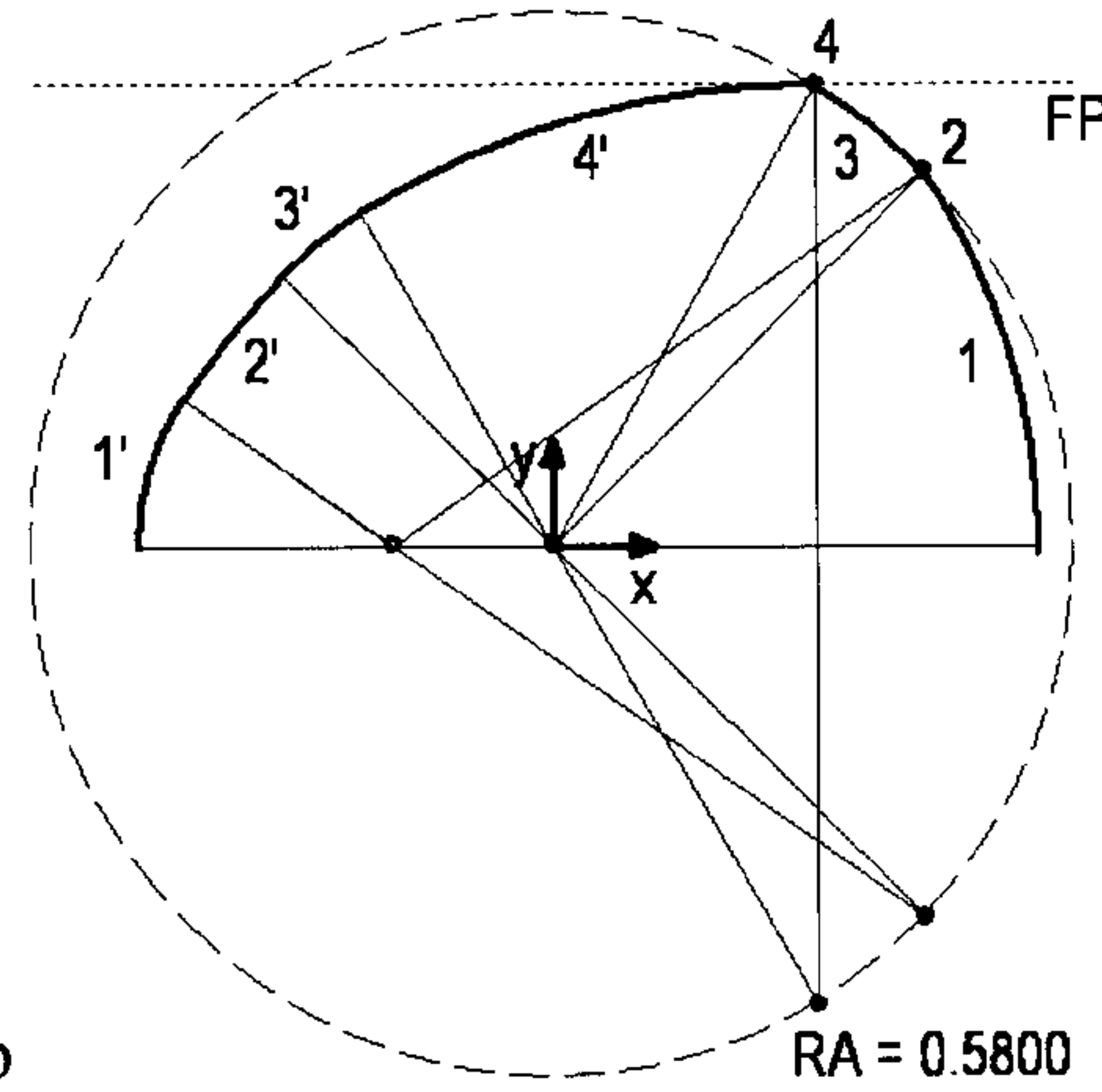


Figure 17b

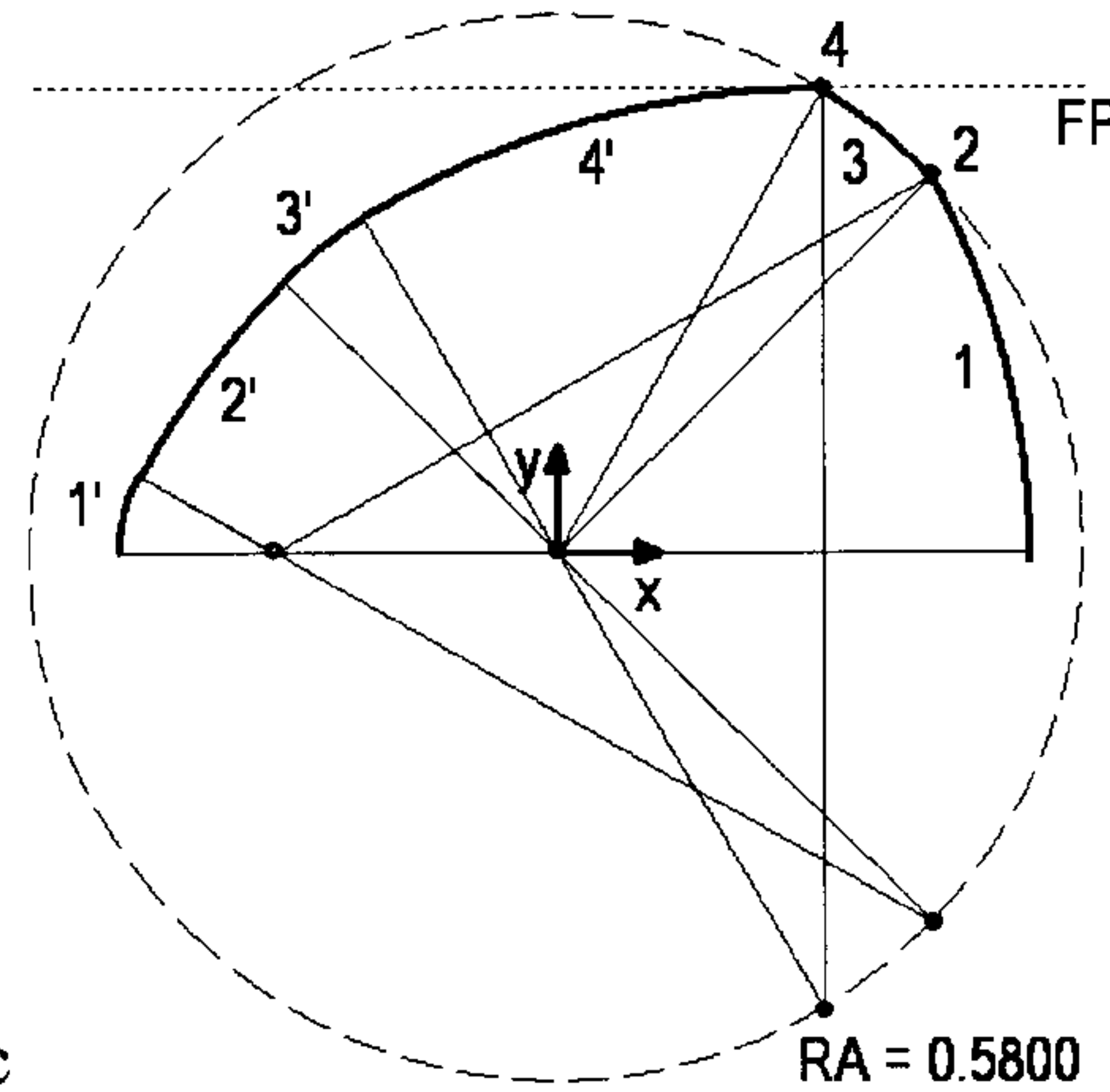


Figure 17c

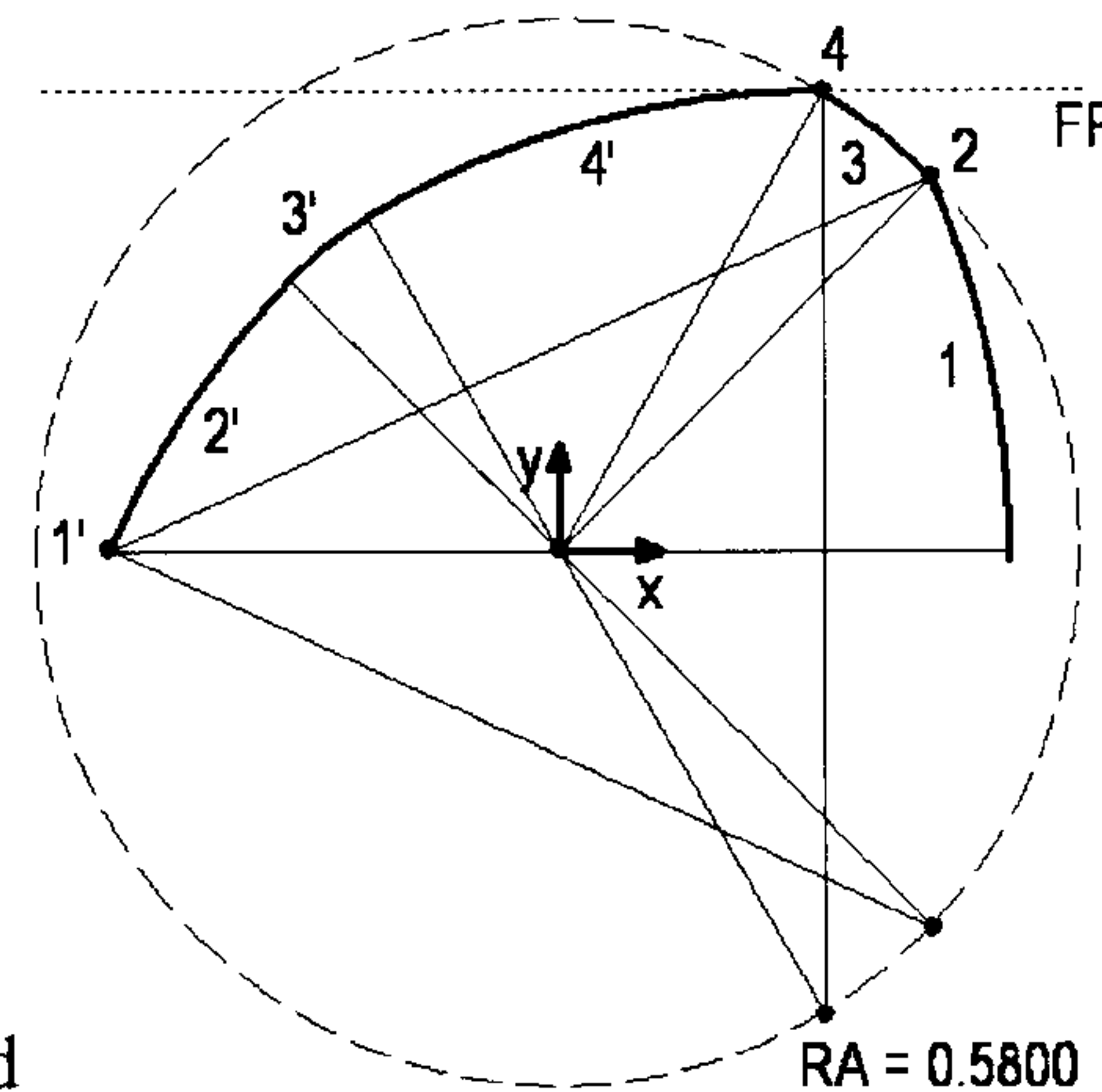


Figure 17d

- 1) $R = 0.6379$ $M_x = -0.0779$
 $\alpha = 0.6910$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.4137$
 $\alpha = 0.0857$ $M_y = 0.4065$
- 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 2') $R = 1.0000$ $M_x = 0.4137$
 $\alpha = 0.0857$ $M_y = -0.4065$
- 1') $R = 0.3621$ $M_x = -0.0779$
 $\alpha = 0.6910$ $M_y = 0.0000$

- 1) $R = 0.7173$ $M_x = -0.1773$
 $\alpha = 0.6025$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.4137$
 $\alpha = 0.1742$ $M_y = 0.4065$
- 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 2') $R = 1.0000$ $M_x = 0.4137$
 $\alpha = 0.1742$ $M_y = -0.4065$
- 1') $R = 0.2827$ $M_x = -0.1773$
 $\alpha = 0.6025$ $M_y = 0.0000$

- 1) $R = 0.8304$ $M_x = -0.3104$
 $\alpha = 0.5116$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.4137$
 $\alpha = 0.2651$ $M_y = 0.4065$
- 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 2') $R = 1.0000$ $M_x = 0.4137$
 $\alpha = 0.2651$ $M_y = -0.4065$
- 1') $R = 0.1696$ $M_x = -0.3104$
 $\alpha = 0.5116$ $M_y = 0.0000$

- 1) $R = 0.9999$ $M_x = -0.4998$
 $\alpha = 0.4187$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.4137$
 $\alpha = 0.3580$ $M_y = 0.4065$
- 3) $R = 0.5800$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 4) $R = 0.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 4') $R = 1.0000$ $M_x = 0.2939$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 3') $R = 0.4200$ $M_x = 0.0000$
 $\alpha = 0.2627$ $M_y = 0.0000$
- 2') $R = 1.0000$ $M_x = 0.4137$
 $\alpha = 0.3580$ $M_y = -0.4065$
- 1') $R = 0.0001$ $M_x = -0.4998$
 $\alpha = 0.4187$ $M_y = 0.0000$

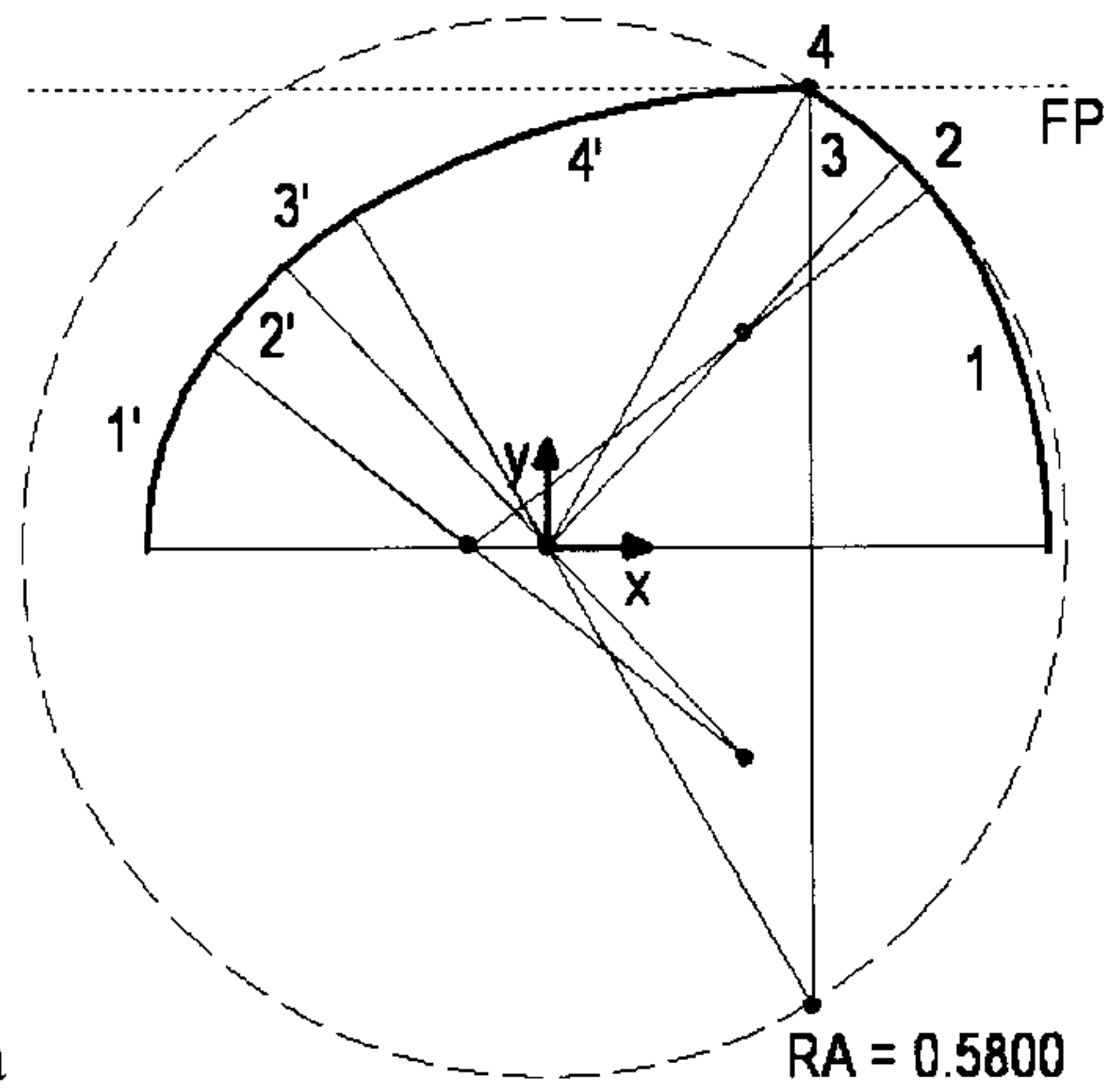


Figure 18a

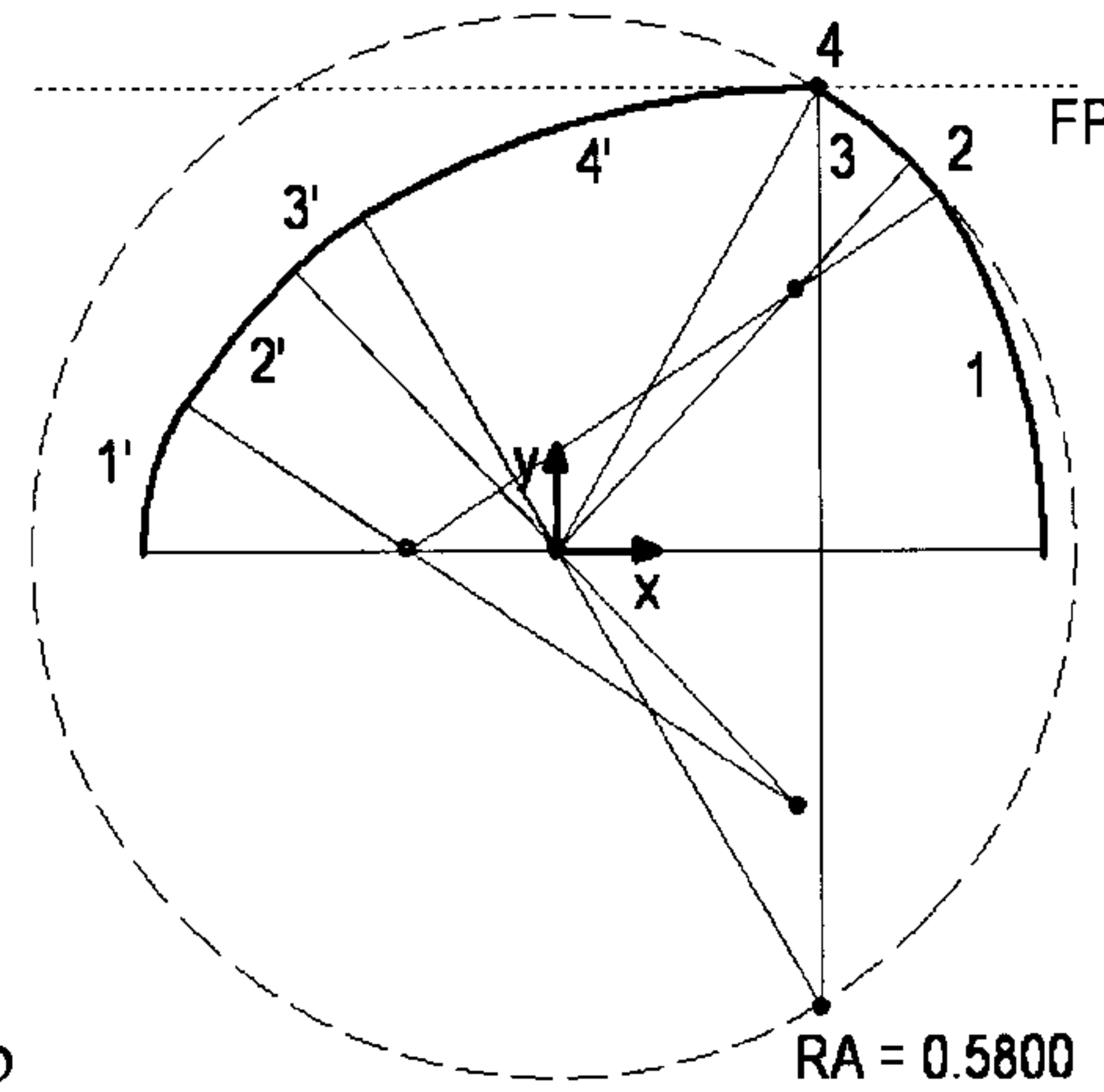


Figure 18b

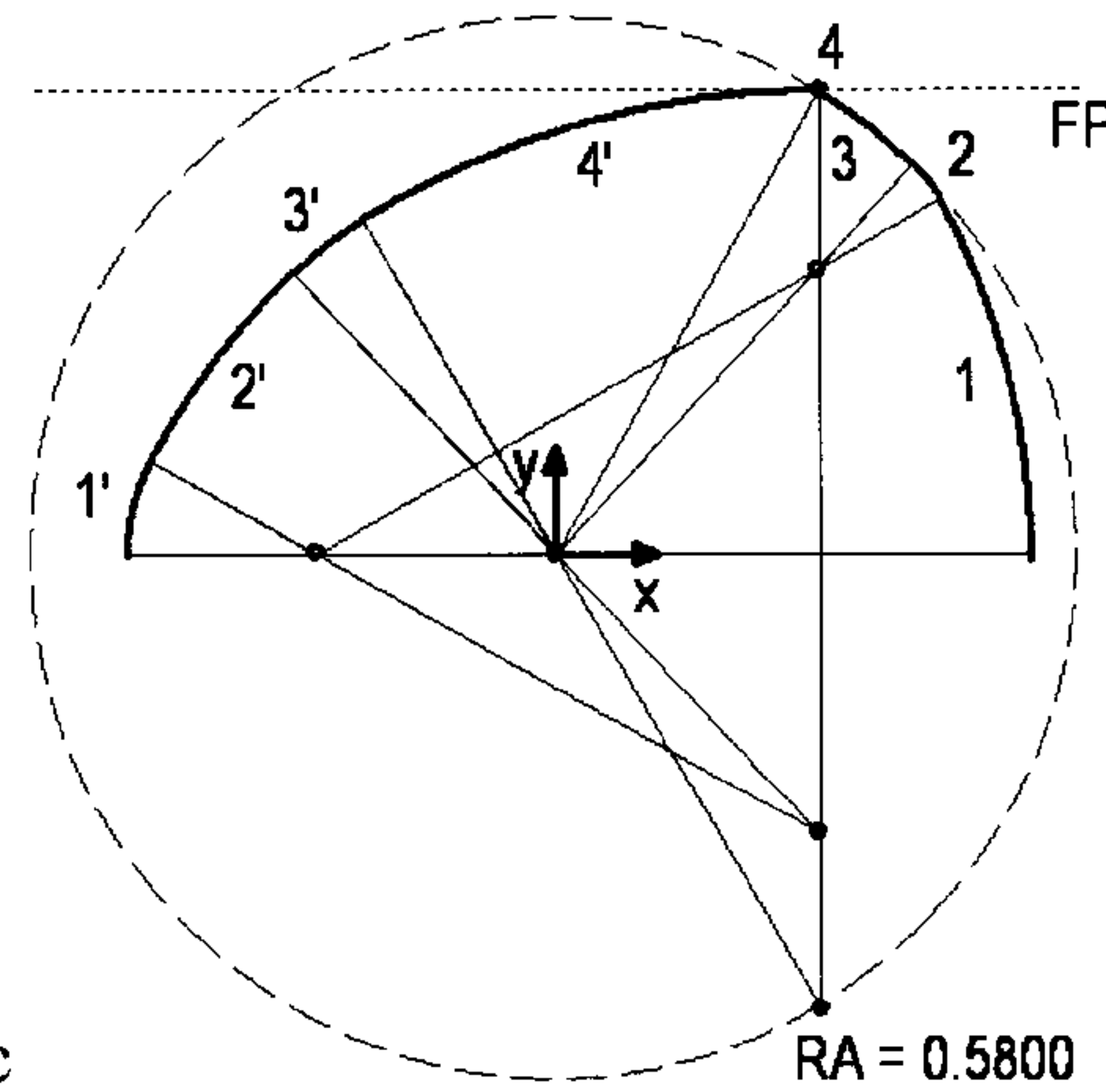


Figure 18c

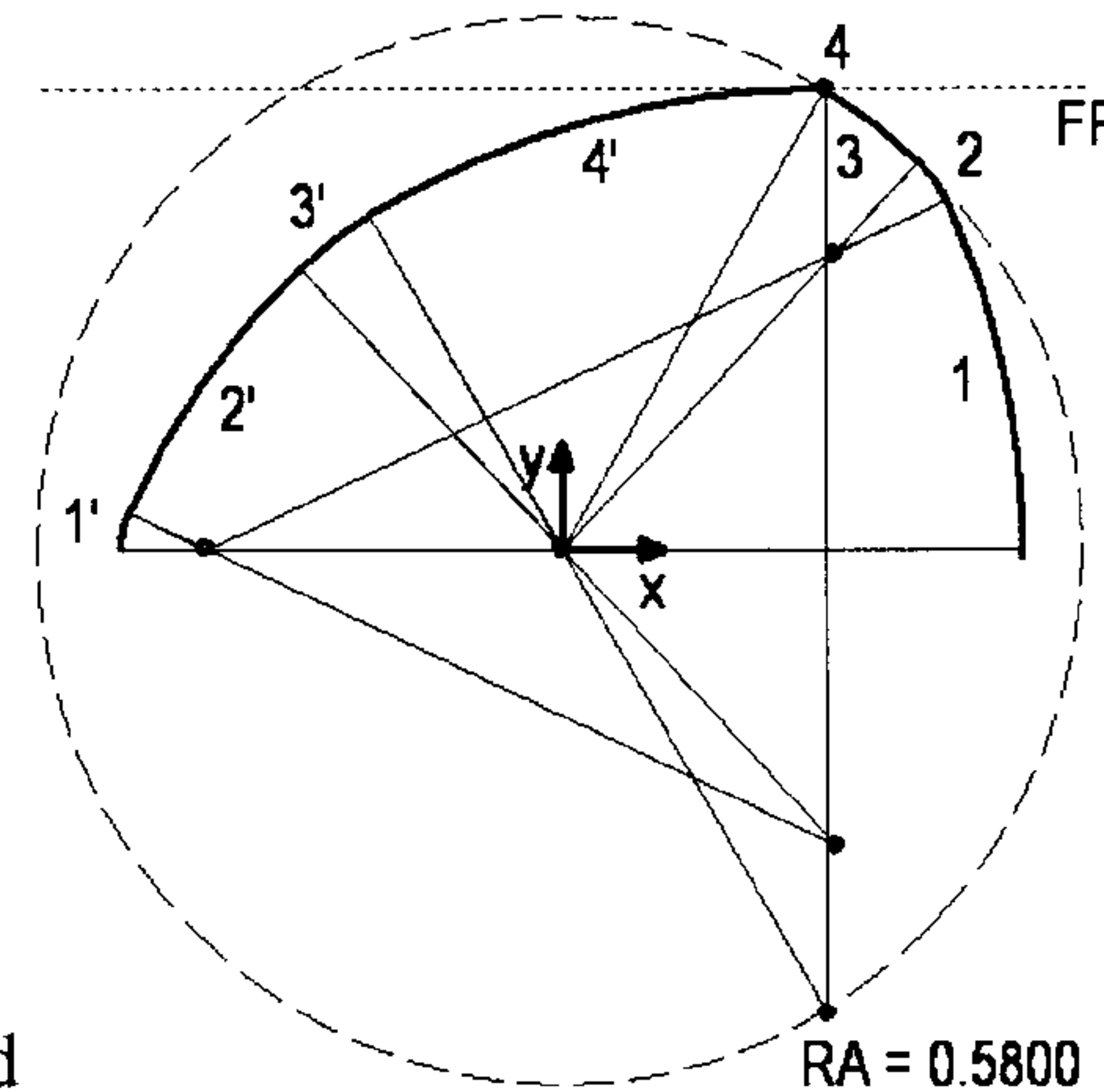


Figure 18d

$$1) R = 0.6447 \quad Mx = -0.0865 \\ \alpha = 0.6473 \quad My = 0.0000$$

$$2) R = 0.2608 \quad Mx = 0.2197 \\ \alpha = 0.1643 \quad My = 0.2315$$

$$3) R = 0.5800 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = -0.0000$$

$$4) R = 0.0000 \quad Mx = 0.2939 \\ \alpha = 0.5315 \quad My = 0.5000$$

$$4') R = 1.0000 \quad Mx = 0.2939 \\ \alpha = 0.5315 \quad My = -0.5000$$

$$3') R = 0.4200 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = 0.0000$$

$$2') R = 0.7392 \quad Mx = 0.2197 \\ \alpha = 0.1643 \quad My = -0.2315$$

$$1') R = 0.3553 \quad Mx = -0.0865 \\ \alpha = 0.6473 \quad My = 0.0000$$

$$1) R = 0.7081 \quad Mx = -0.1655 \\ \alpha = 0.5766 \quad My = 0.0000$$

$$2) R = 0.1924 \quad Mx = 0.2668 \\ \alpha = 0.2350 \quad My = 0.2812$$

$$3) R = 0.5800 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = -0.0000$$

$$4) R = 0.0000 \quad Mx = 0.2940 \\ \alpha = 0.5315 \quad My = 0.5000$$

$$4') R = 1.0000 \quad Mx = 0.2940 \\ \alpha = 0.5315 \quad My = -0.5000$$

$$3') R = 0.4200 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = 0.0000$$

$$2') R = 0.8076 \quad Mx = 0.2668 \\ \alpha = 0.2350 \quad My = -0.2812$$

$$1') R = 0.2919 \quad Mx = -0.1655 \\ \alpha = 0.5766 \quad My = 0.0000$$

$$1) R = 0.7919 \quad Mx = -0.2646 \\ \alpha = 0.5042 \quad My = 0.0000$$

$$2) R = 0.1575 \quad Mx = 0.2909 \\ \alpha = 0.3074 \quad My = 0.3065$$

$$3) R = 0.5800 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = -0.0000$$

$$4) R = 0.0000 \quad Mx = 0.2940 \\ \alpha = 0.5315 \quad My = 0.5000$$

$$4') R = 1.0000 \quad Mx = 0.2940 \\ \alpha = 0.5315 \quad My = -0.5000$$

$$3') R = 0.4200 \quad Mx = 0.0000 \\ \alpha = 0.2278 \quad My = 0.0000$$

$$2') R = 0.8425 \quad Mx = 0.2909 \\ \alpha = 0.3074 \quad My = -0.3065$$

$$1') R = 0.2081 \quad Mx = -0.2646 \\ \alpha = 0.5042 \quad My = 0.0000$$

$$1) R = 0.9061 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$2) R = 0.1385 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = 0.3202$$

$$3) R = 0.5800 \quad Mx = -0.0000 \\ \alpha = 0.2278 \quad My = -0.0000$$

$$4) R = 0.0000 \quad Mx = 0.2939 \\ \alpha = 0.5315 \quad My = 0.5000$$

$$4') R = 1.0000 \quad Mx = 0.2939 \\ \alpha = 0.5315 \quad My = -0.5000$$

$$3') R = 0.4200 \quad Mx = -0.0000 \\ \alpha = 0.2278 \quad My = 0.0000$$

$$2') R = 0.8615 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = -0.3202$$

$$1') R = 0.0939 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

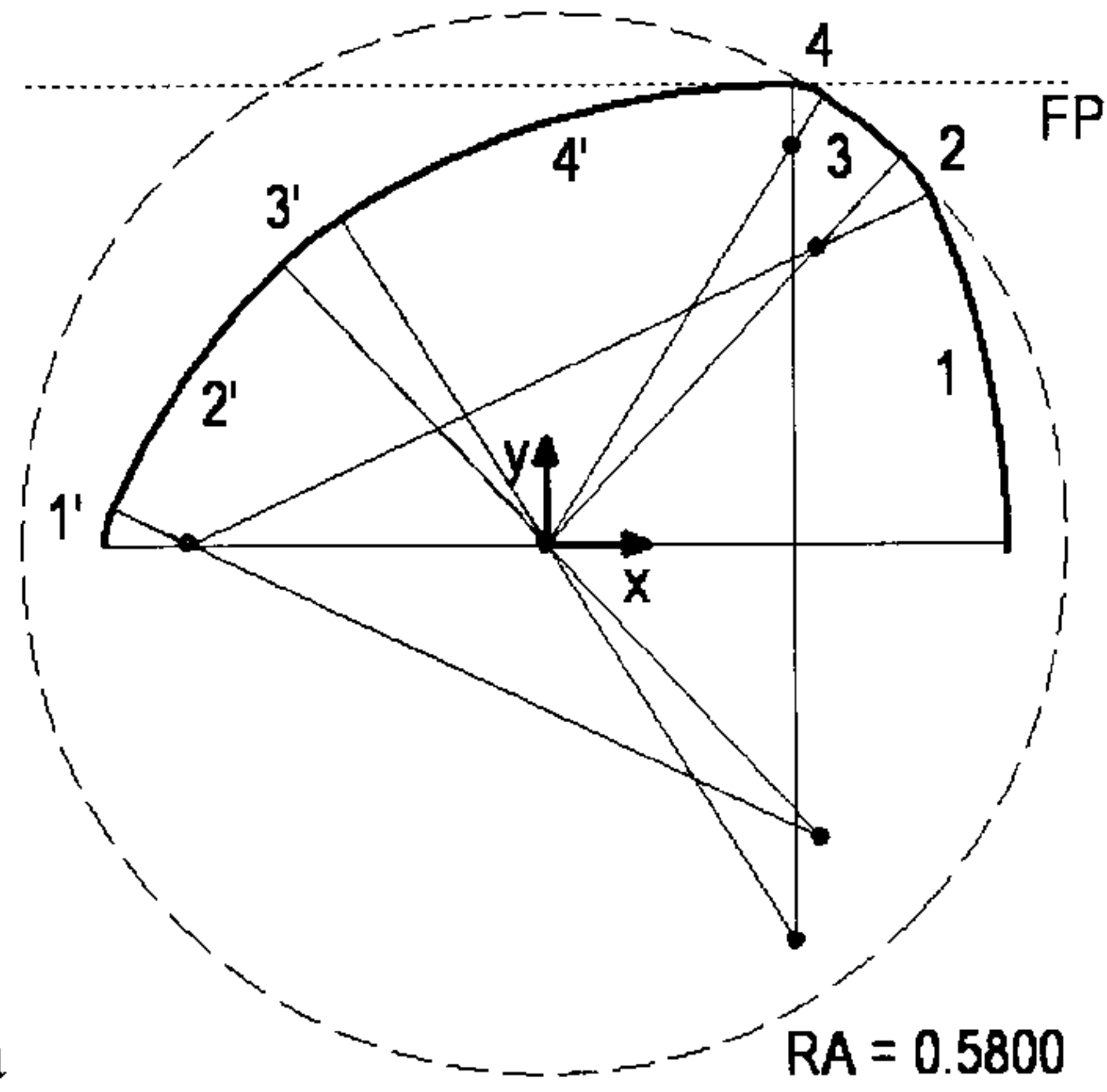


Figure 19a

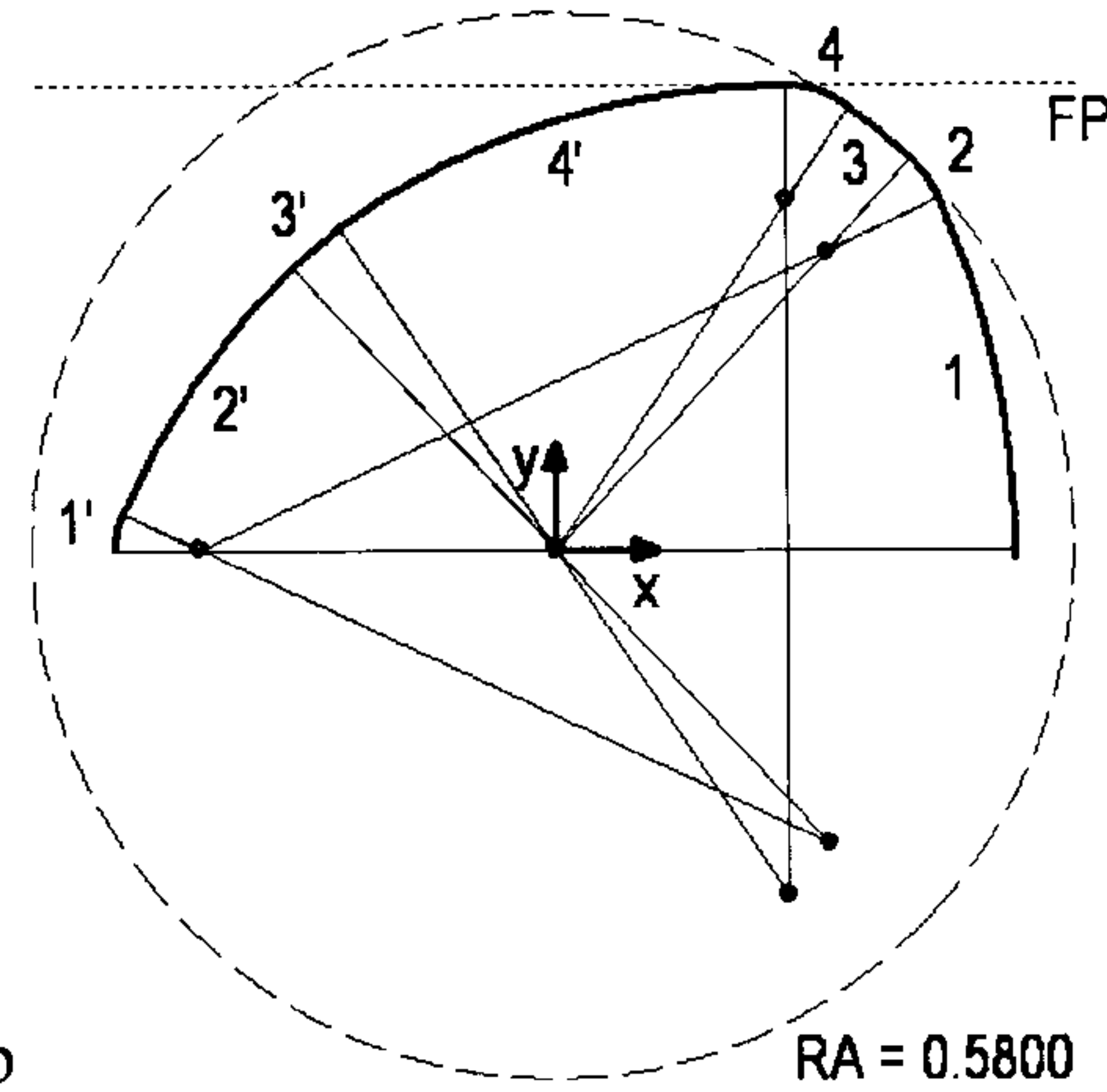


Figure 19b

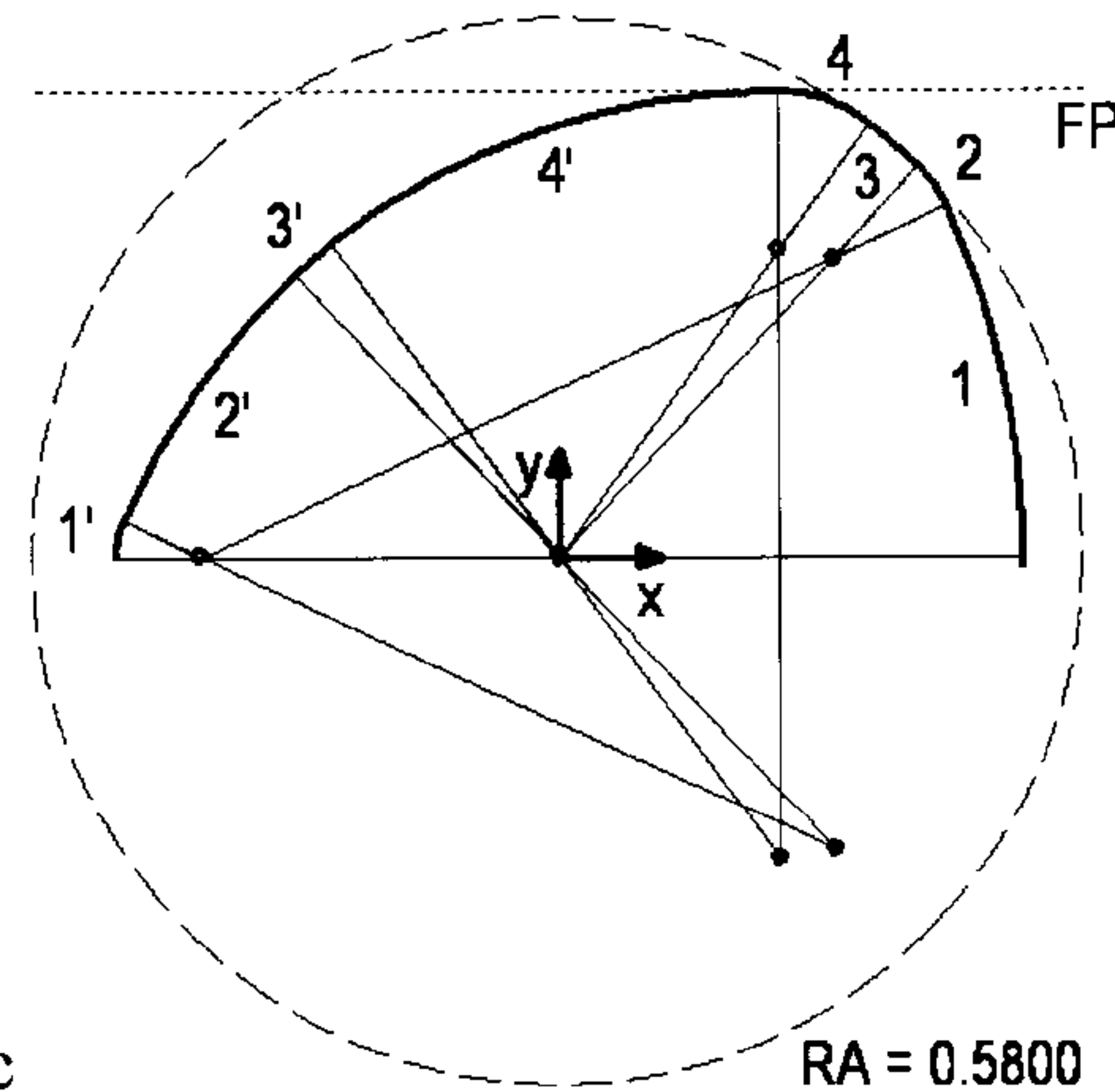


Figure 19c

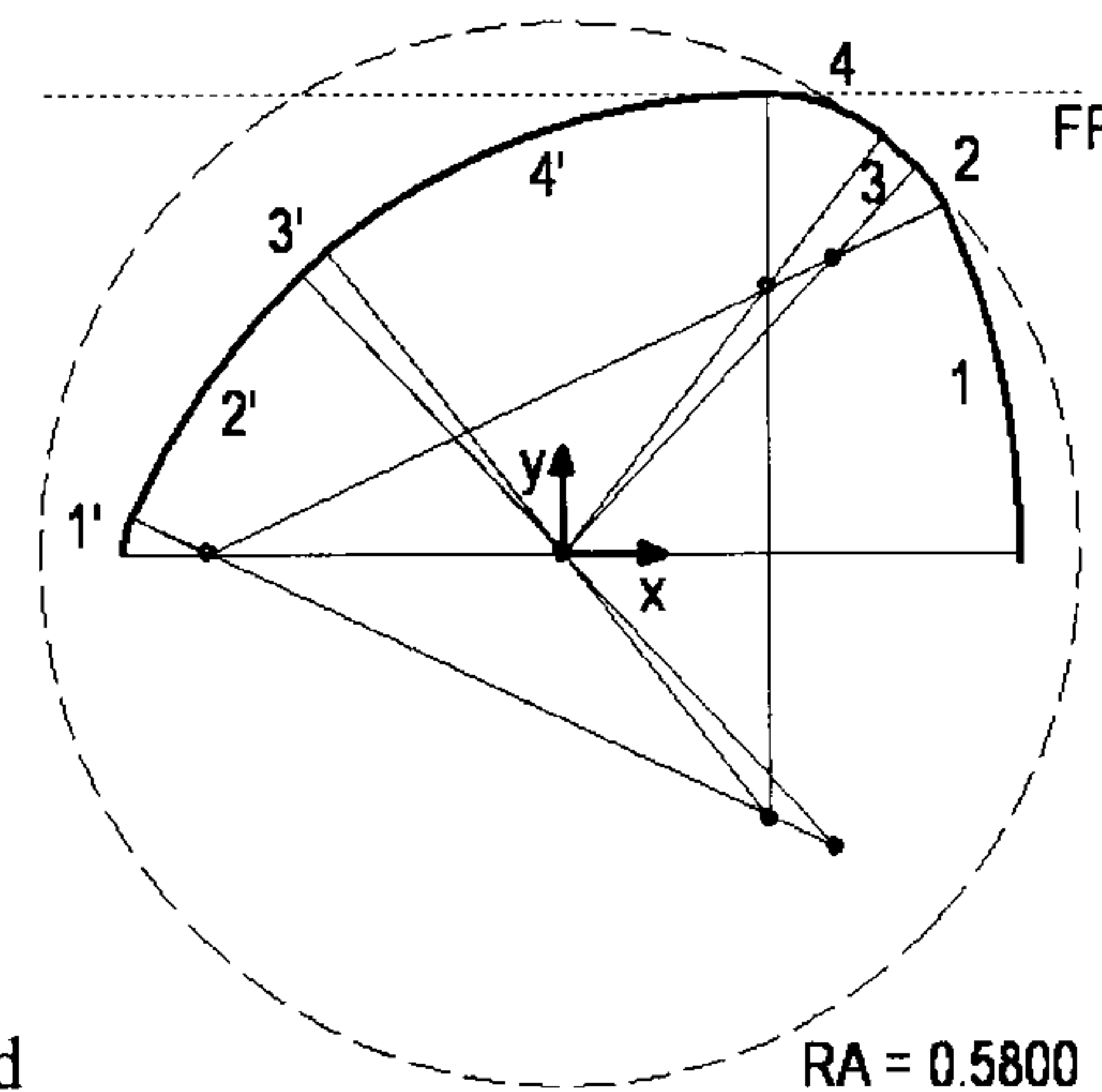


Figure 19d

$$1) R = 0.9061 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$2) R = 0.1385 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = 0.3202$$

$$3) R = 0.5800 \quad Mx = -0.0000 \\ \alpha = 0.1929 \quad My = -0.0000$$

$$4) R = 0.0677 \quad Mx = 0.2749 \\ \alpha = 0.5664 \quad My = 0.4323$$

$$4') R = 0.9323 \quad Mx = 0.2749 \\ \alpha = 0.5664 \quad My = -0.4323$$

$$3') R = 0.4200 \quad Mx = -0.0000 \\ \alpha = 0.1929 \quad My = 0.0000$$

$$2') R = 0.8615 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = -0.3202$$

$$1') R = 0.0939 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$1) R = 0.9061 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$2) R = 0.1385 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = 0.3202$$

$$3) R = 0.5800 \quad Mx = -0.0000 \\ \alpha = 0.1580 \quad My = -0.0000$$

$$4) R = 0.1239 \quad Mx = 0.2580 \\ \alpha = 0.6013 \quad My = 0.3761$$

$$4') R = 0.8761 \quad Mx = 0.2580 \\ \alpha = 0.6013 \quad My = -0.3761$$

$$3') R = 0.4200 \quad Mx = -0.0000 \\ \alpha = 0.1580 \quad My = 0.0000$$

$$2') R = 0.8615 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = -0.3202$$

$$1') R = 0.0939 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$1) R = 0.9061 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$2) R = 0.1385 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = 0.3202$$

$$3) R = 0.5800 \quad Mx = -0.0000 \\ \alpha = 0.1230 \quad My = -0.0000$$

$$4) R = 0.1711 \quad Mx = 0.2429 \\ \alpha = 0.6362 \quad My = 0.3289$$

$$4') R = 0.8289 \quad Mx = 0.2429 \\ \alpha = 0.6362 \quad My = -0.3289$$

$$3') R = 0.4200 \quad Mx = -0.0000 \\ \alpha = 0.1230 \quad My = 0.0000$$

$$2') R = 0.8615 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = -0.3202$$

$$1') R = 0.0939 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$1) R = 0.9061 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

$$2) R = 0.1385 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = 0.3202$$

$$3) R = 0.5800 \quad Mx = -0.0000 \\ \alpha = 0.0881 \quad My = -0.0000$$

$$4) R = 0.2111 \quad Mx = 0.2294 \\ \alpha = 0.6711 \quad My = 0.2889$$

$$4') R = 0.7889 \quad Mx = 0.2294 \\ \alpha = 0.6711 \quad My = -0.2889$$

$$3') R = 0.4200 \quad Mx = -0.0000 \\ \alpha = 0.0881 \quad My = 0.0000$$

$$2') R = 0.8615 \quad Mx = 0.3039 \\ \alpha = 0.3812 \quad My = -0.3202$$

$$1') R = 0.0939 \quad Mx = -0.3937 \\ \alpha = 0.4304 \quad My = 0.0000$$

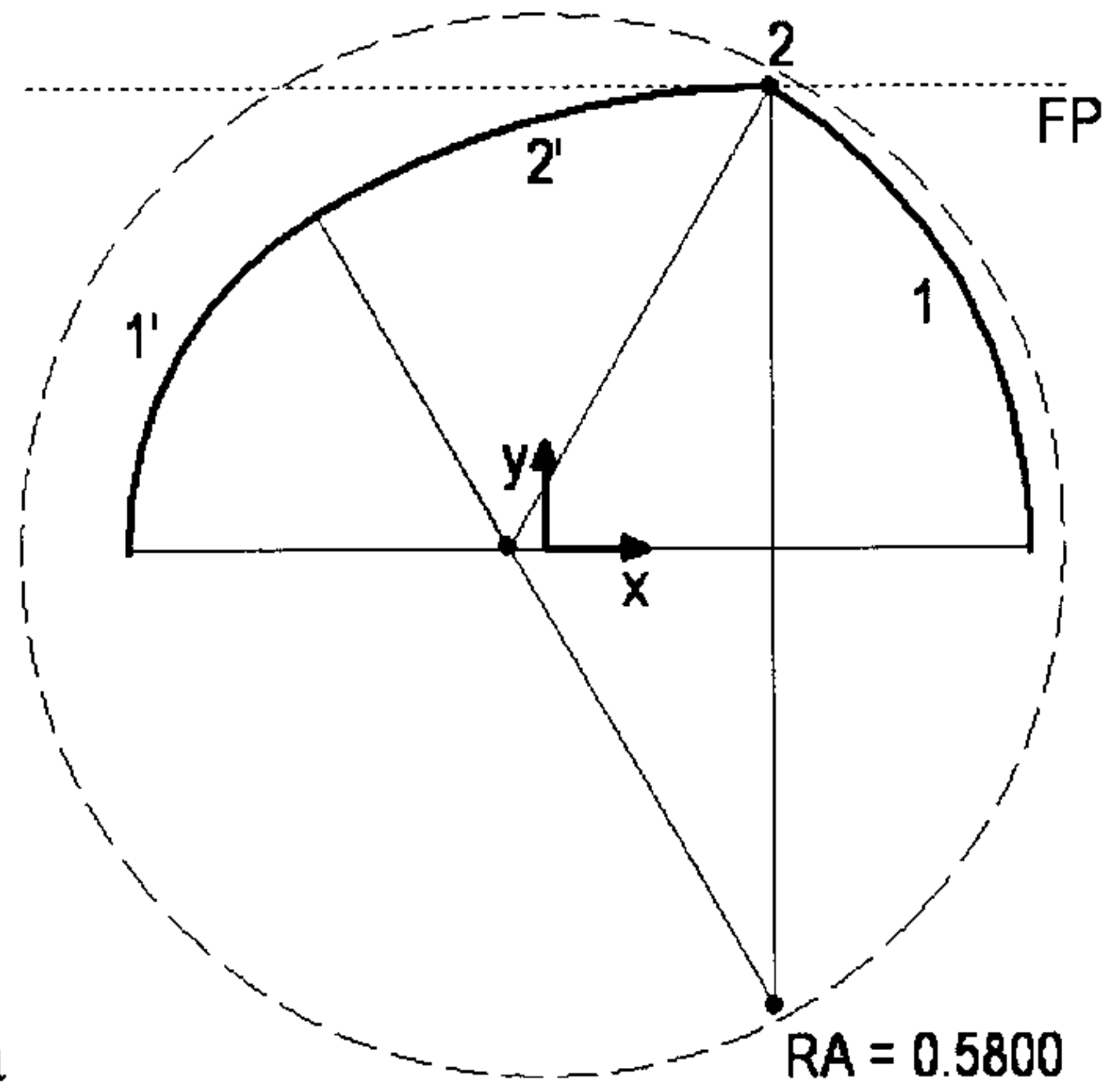


Figure 20a

- 1) $R = 0.5800$ $M_x = -0.0400$
 $\alpha = 1.0393$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.2539$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 2') $R = 1.0000$ $M_x = 0.2539$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 1') $R = 0.4200$ $M_x = -0.0400$
 $\alpha = 1.0393$ $M_y = 0.0000$

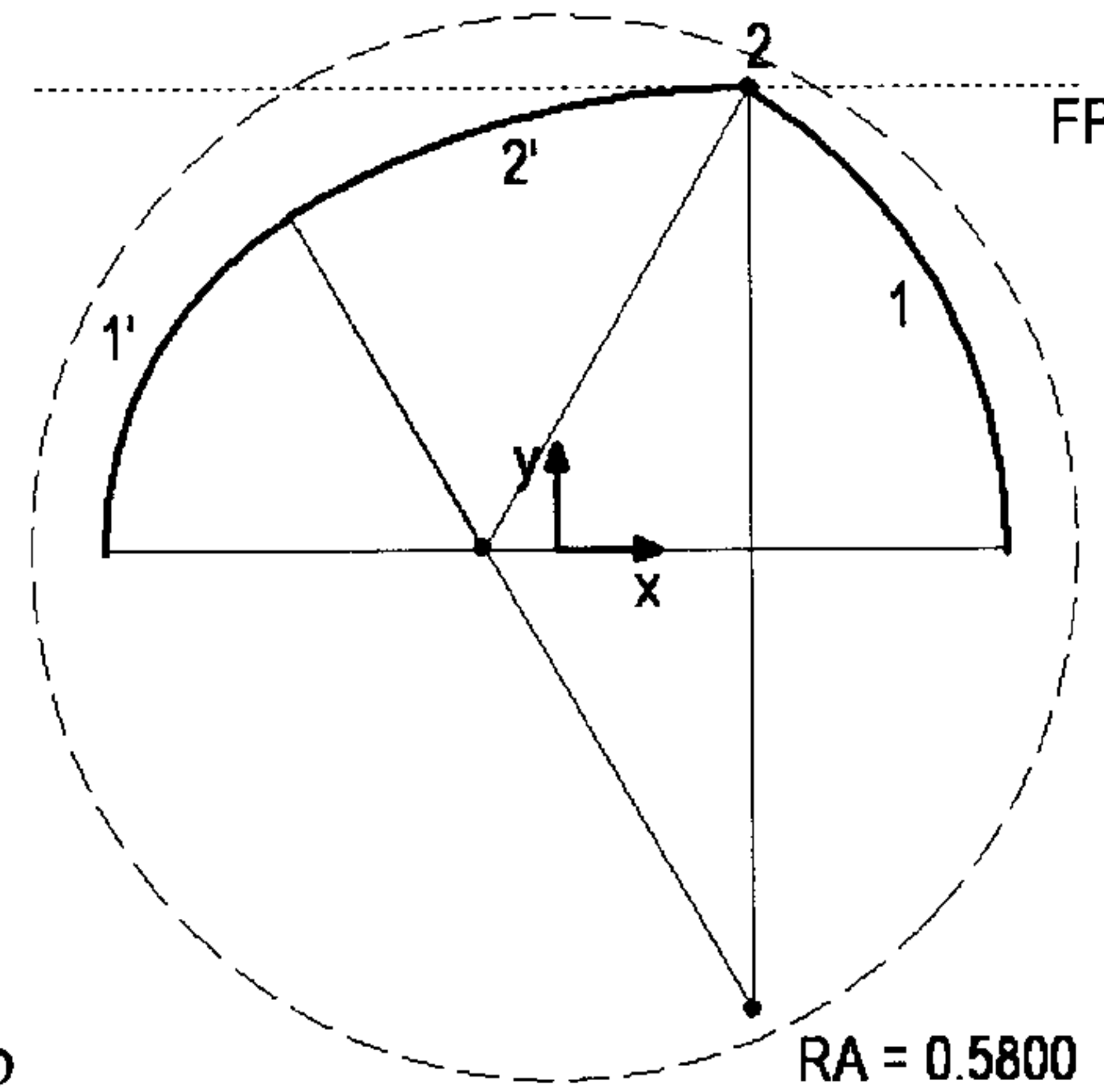


Figure 20b

- 1) $R = 0.5800$ $M_x = -0.0800$
 $\alpha = 1.0393$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.2139$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 2') $R = 1.0000$ $M_x = 0.2139$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 1') $R = 0.4200$ $M_x = -0.0800$
 $\alpha = 1.0393$ $M_y = 0.0000$

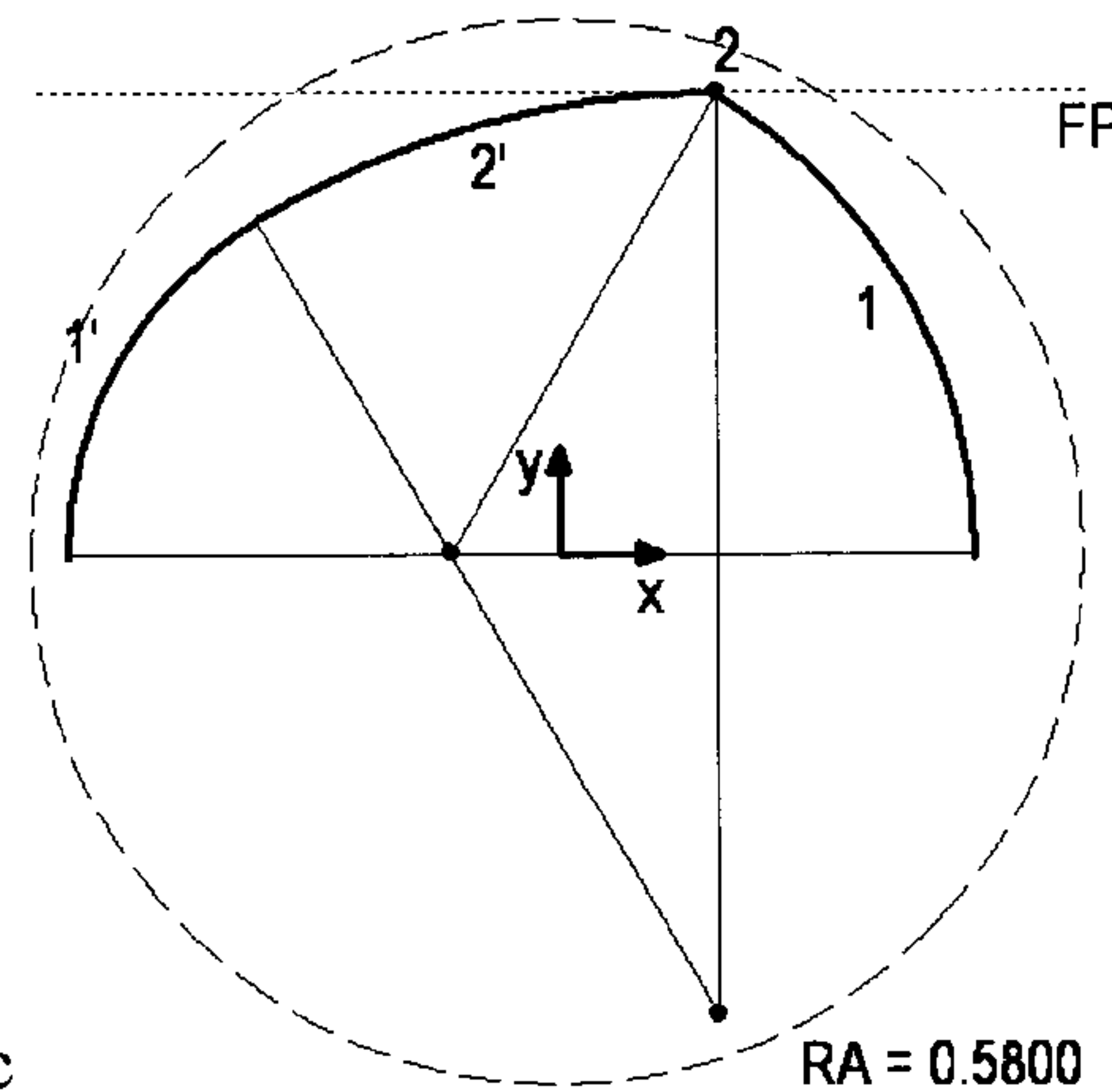


Figure 20c

- 1) $R = 0.5800$ $M_x = -0.1200$
 $\alpha = 1.0393$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.1739$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 2') $R = 1.0000$ $M_x = 0.1739$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 1') $R = 0.4200$ $M_x = -0.1200$
 $\alpha = 1.0393$ $M_y = 0.0000$

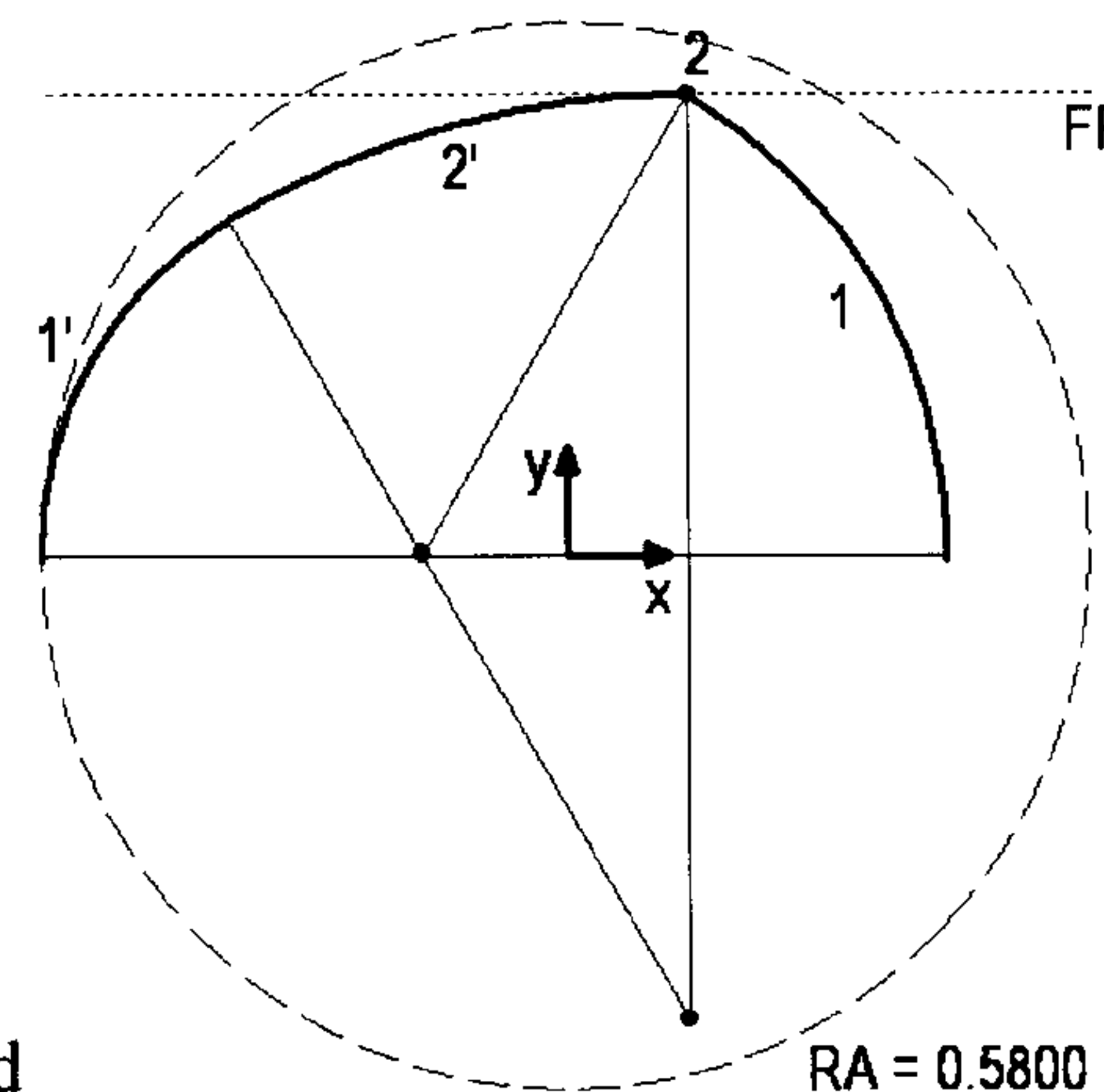


Figure 20d

- 1) $R = 0.5800$ $M_x = -0.1600$
 $\alpha = 1.0393$ $M_y = 0.0000$
- 2) $R = 0.0000$ $M_x = 0.1339$
 $\alpha = 0.5315$ $M_y = 0.5000$
- 2') $R = 1.0000$ $M_x = 0.1339$
 $\alpha = 0.5315$ $M_y = -0.5000$
- 1') $R = 0.4200$ $M_x = -0.1600$
 $\alpha = 1.0393$ $M_y = 0.0000$

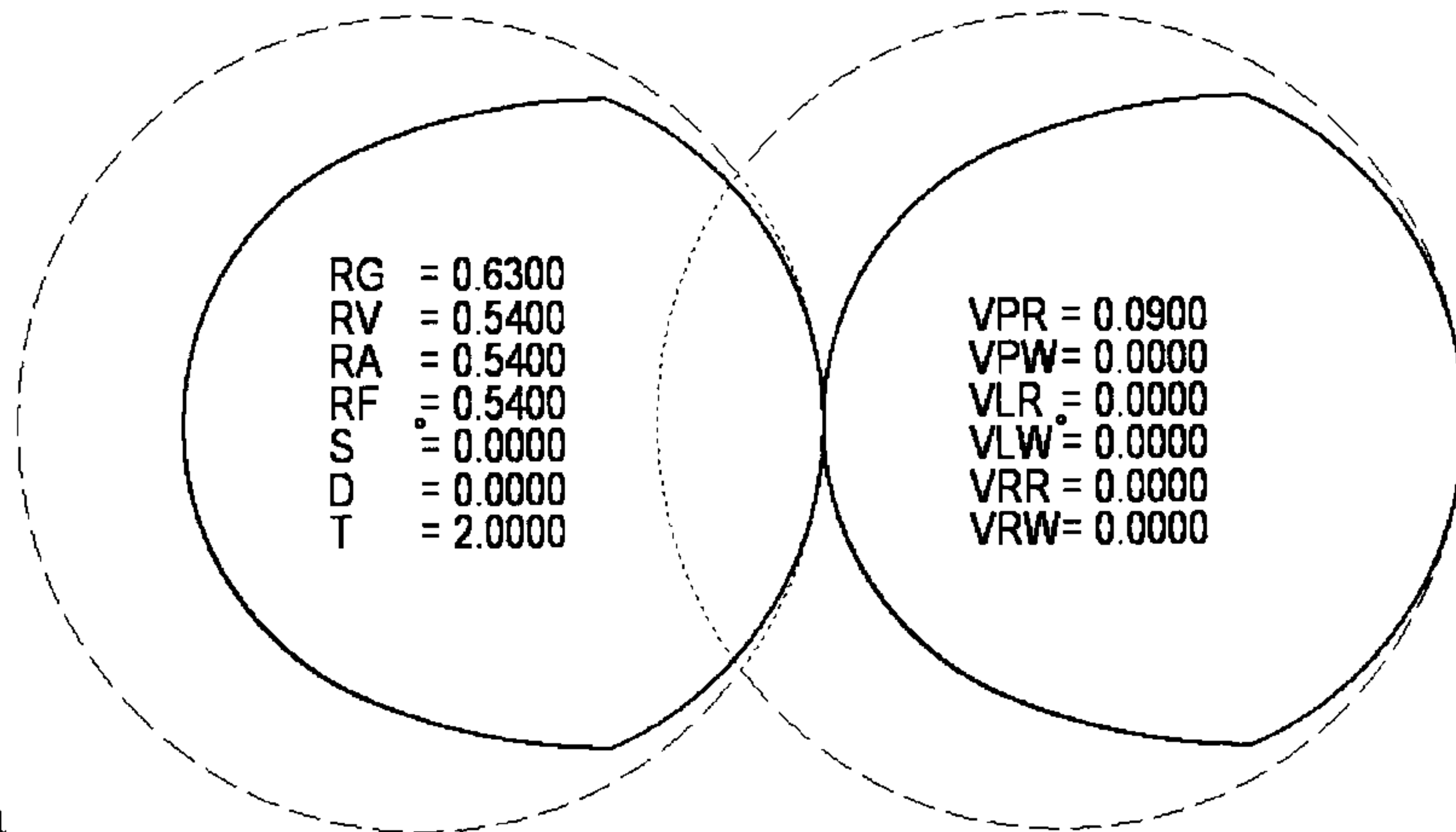


Figure 21a

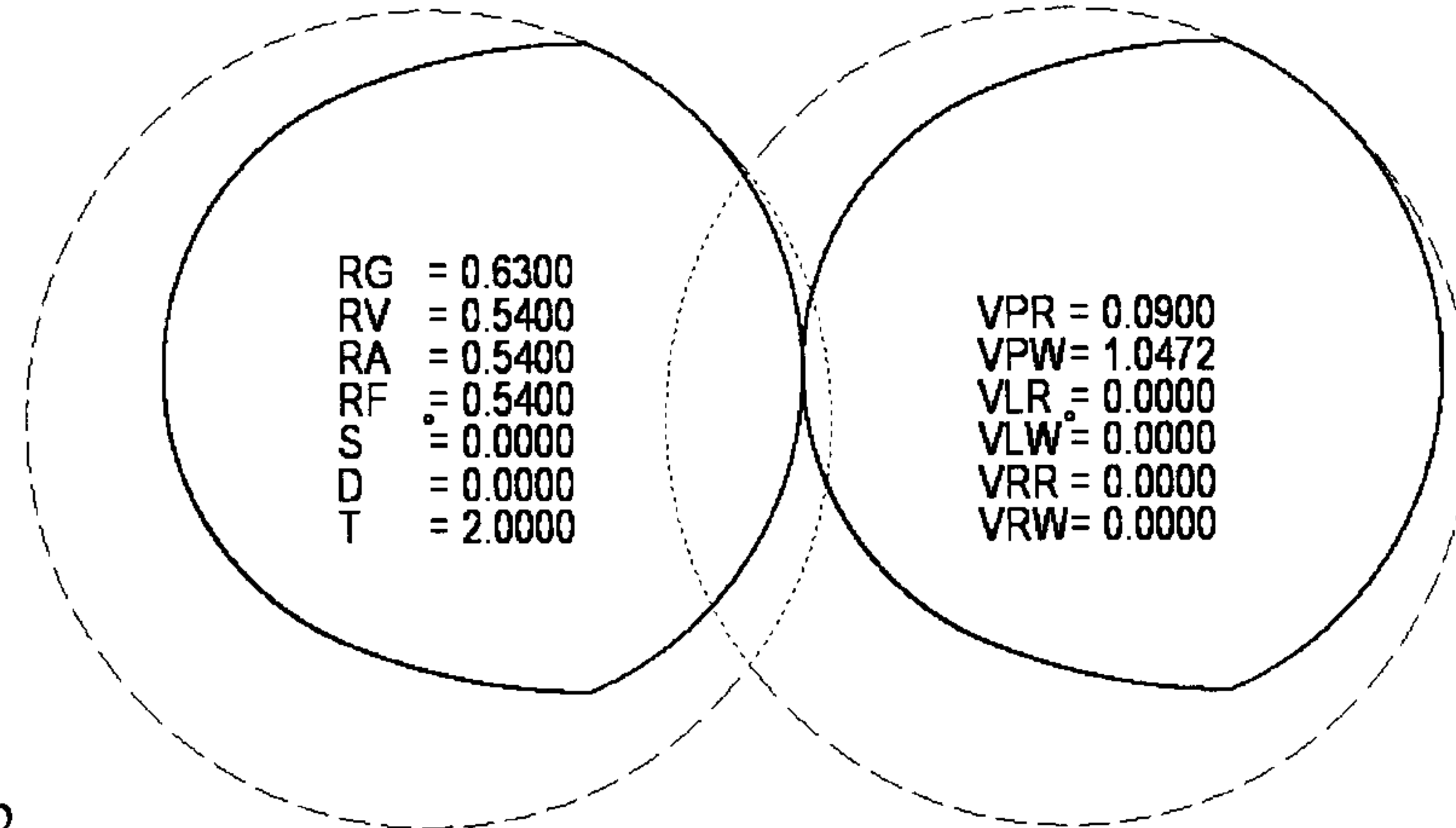


Figure 21b

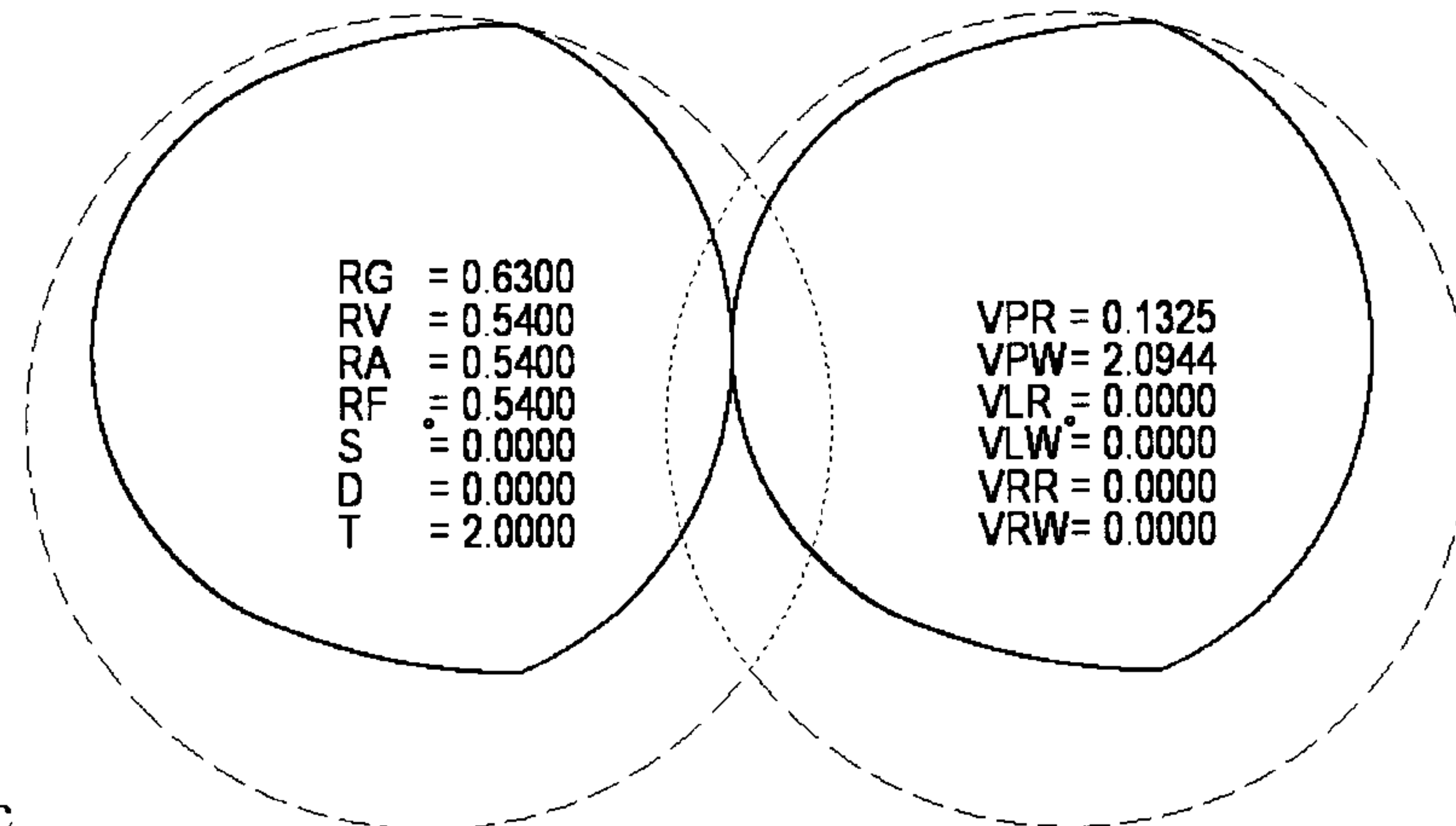


Figure 21c

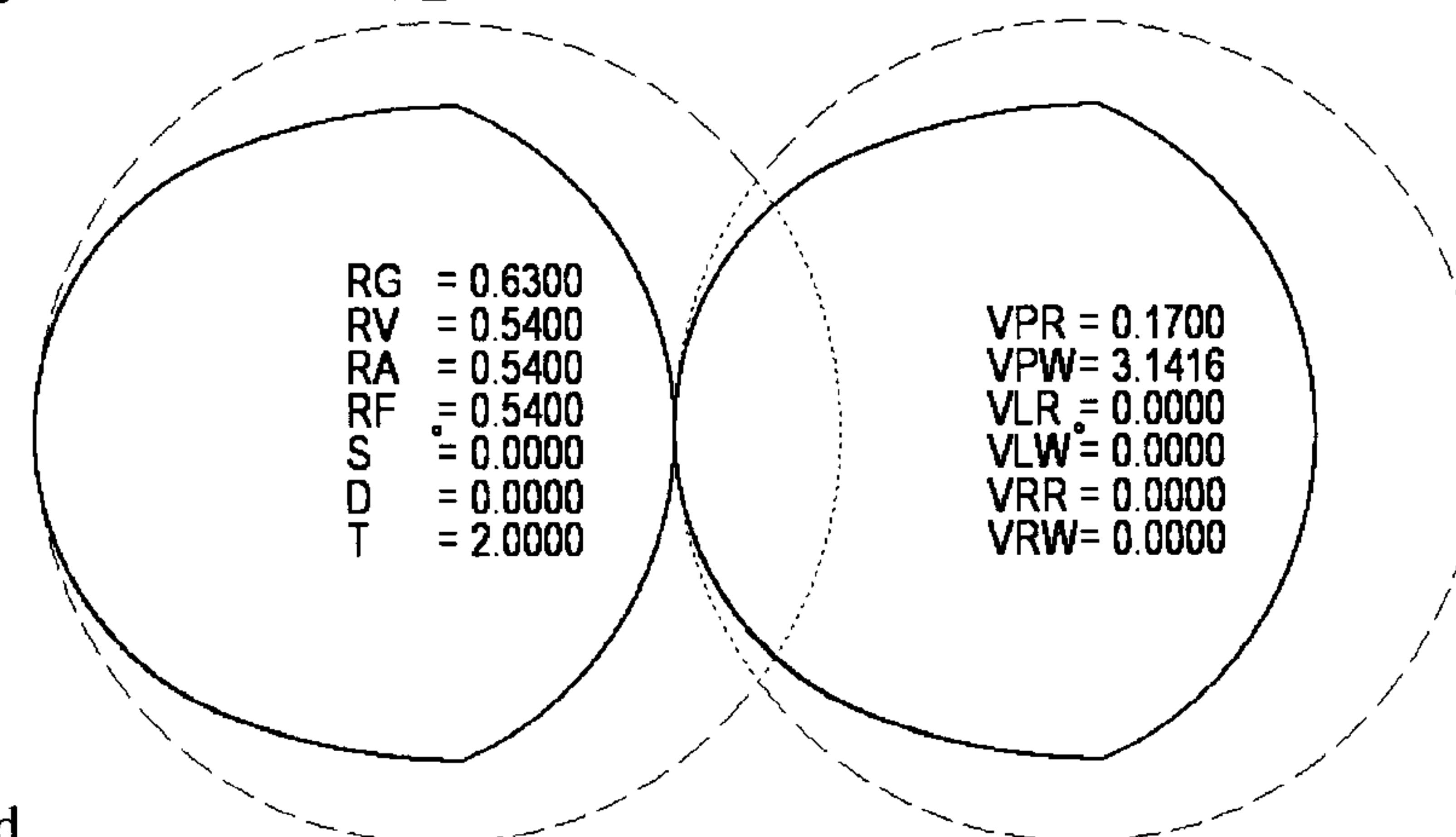


Figure 21d

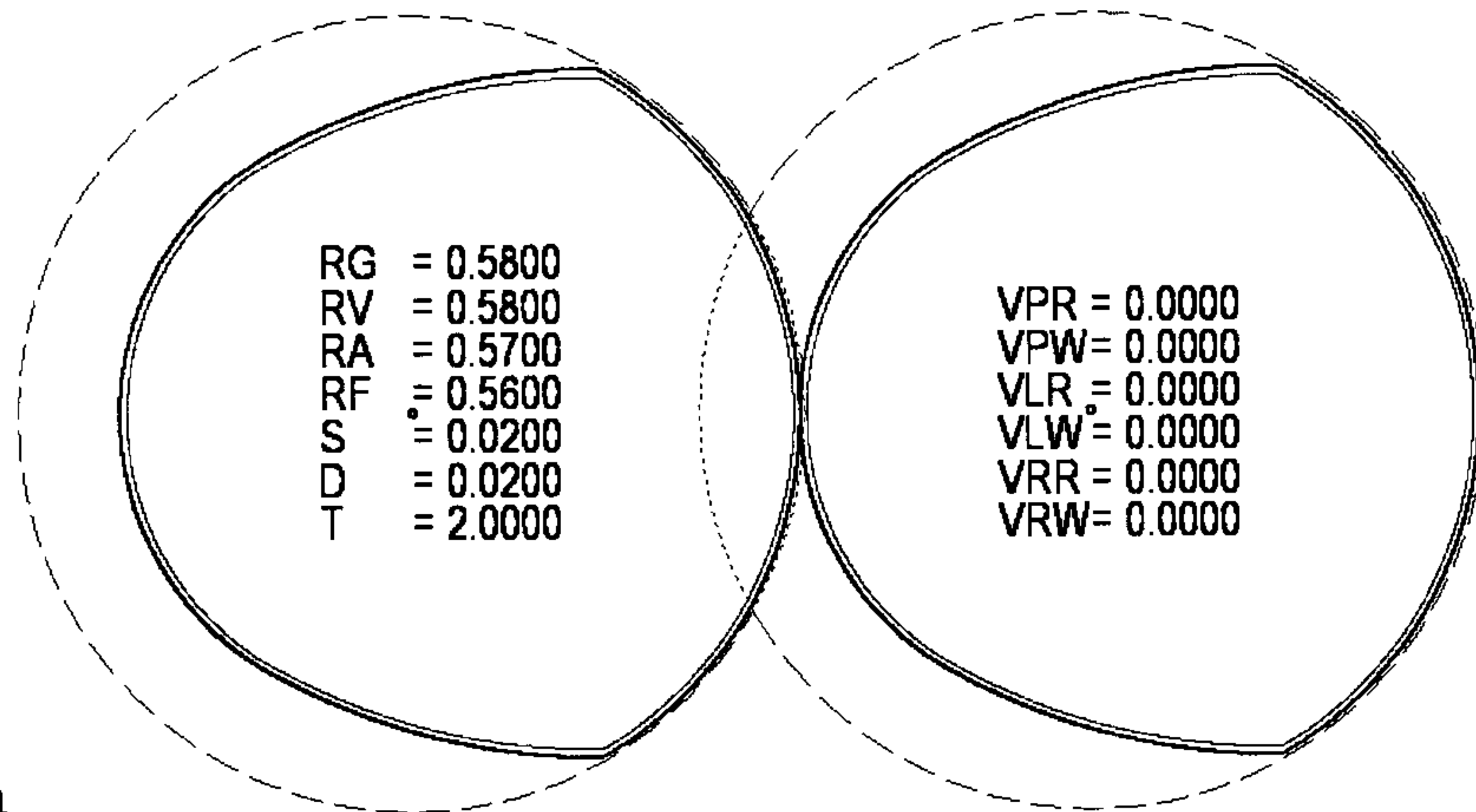


Figure 22a

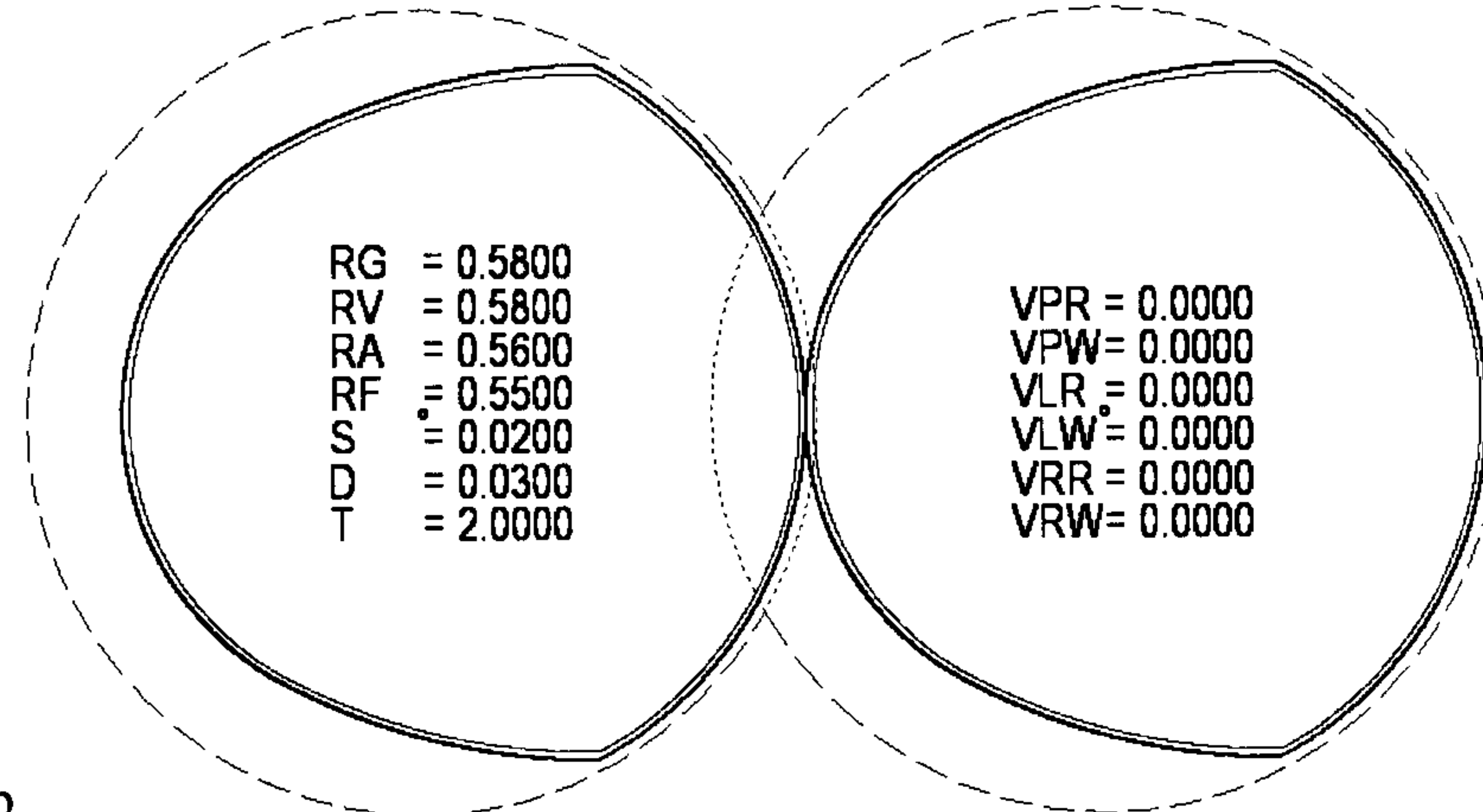


Figure 22b

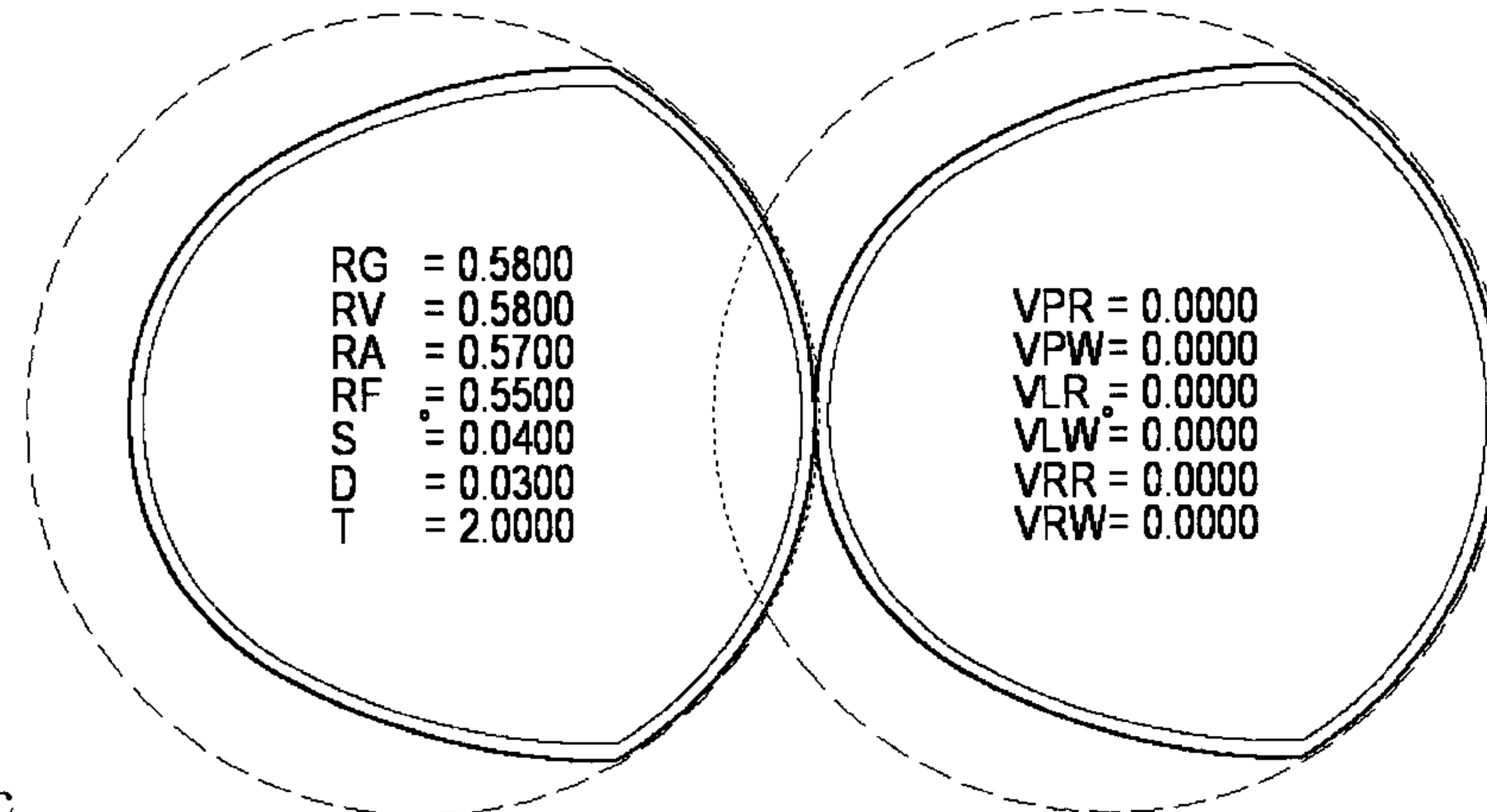


Figure 22c

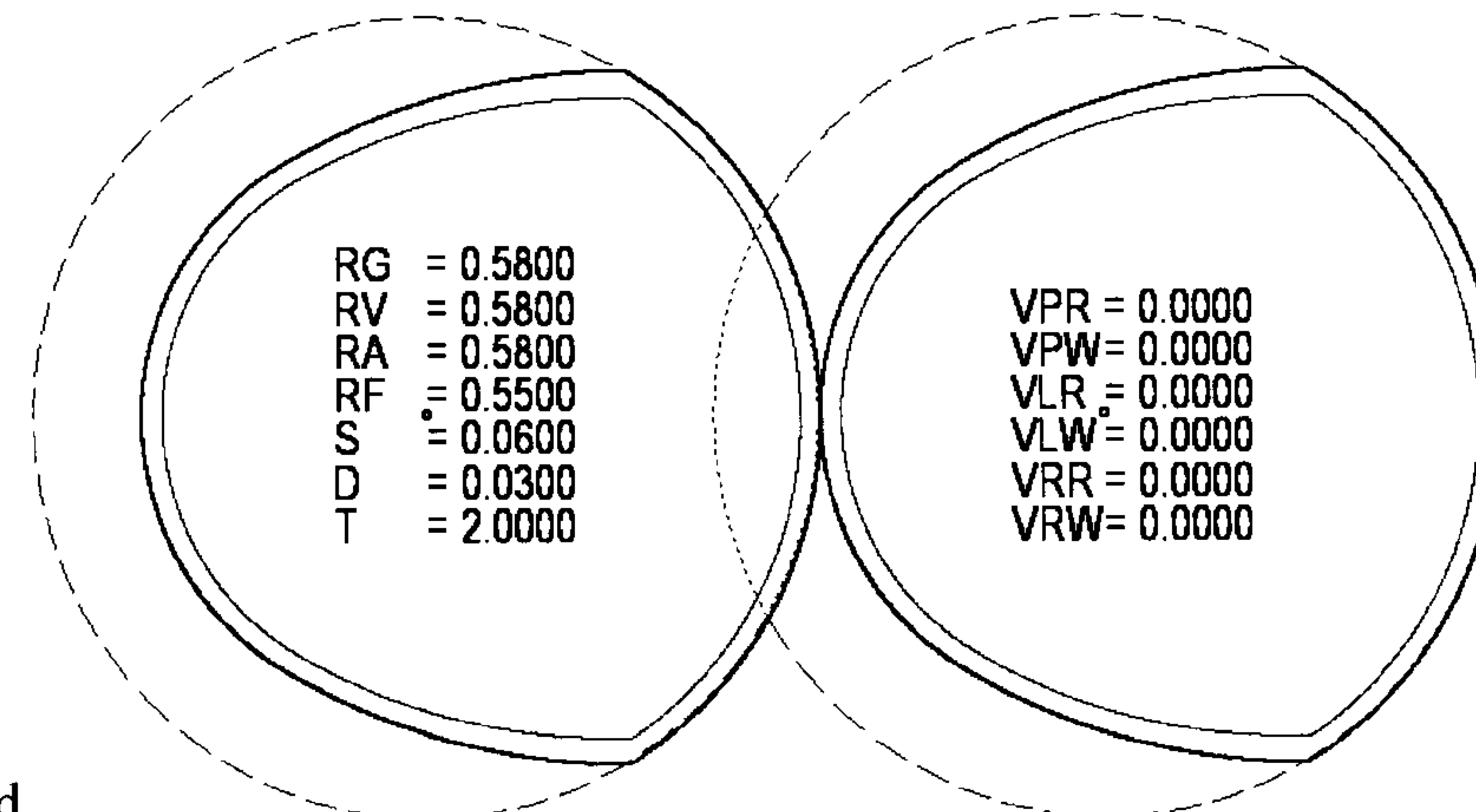


Figure 22d

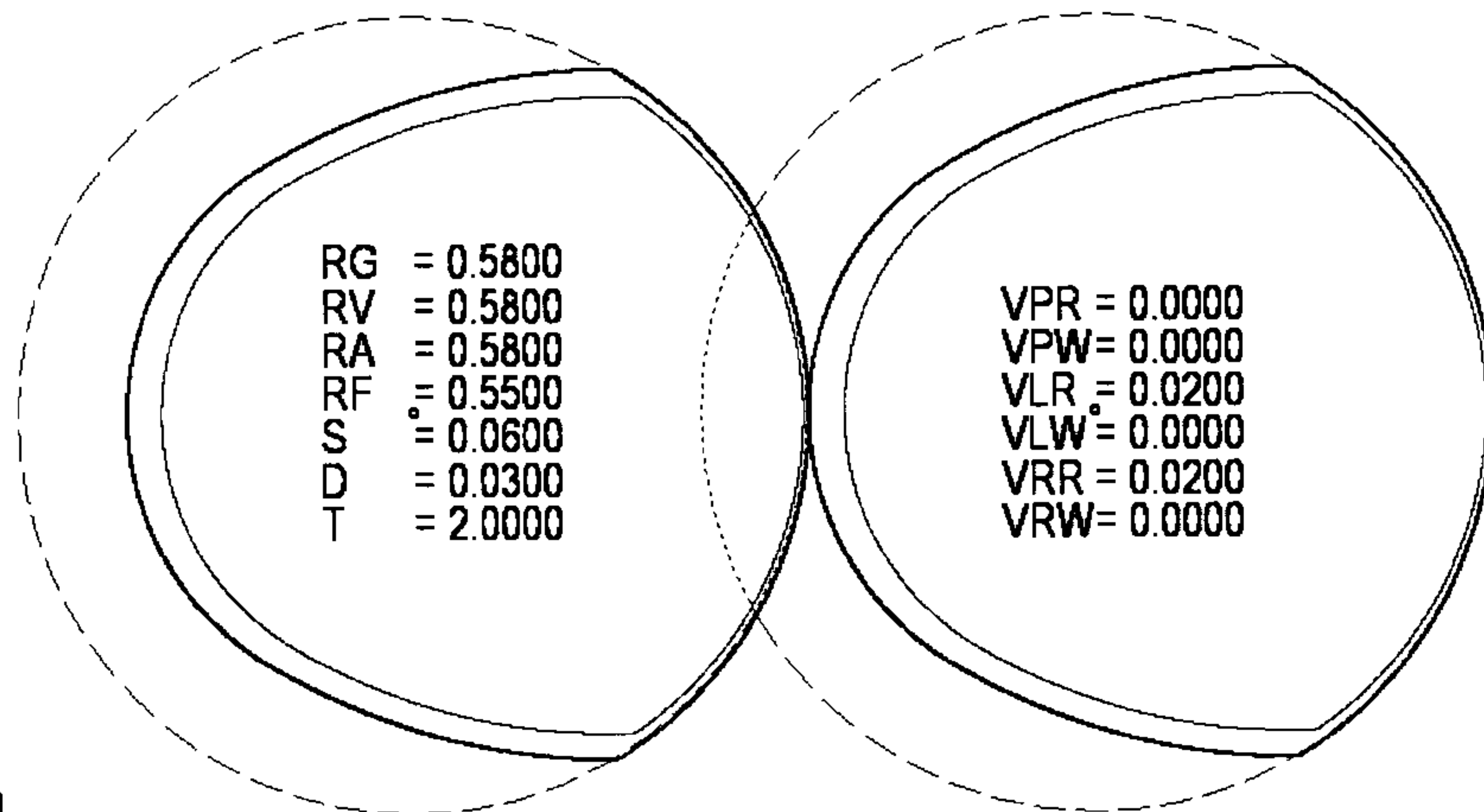


Figure 23a

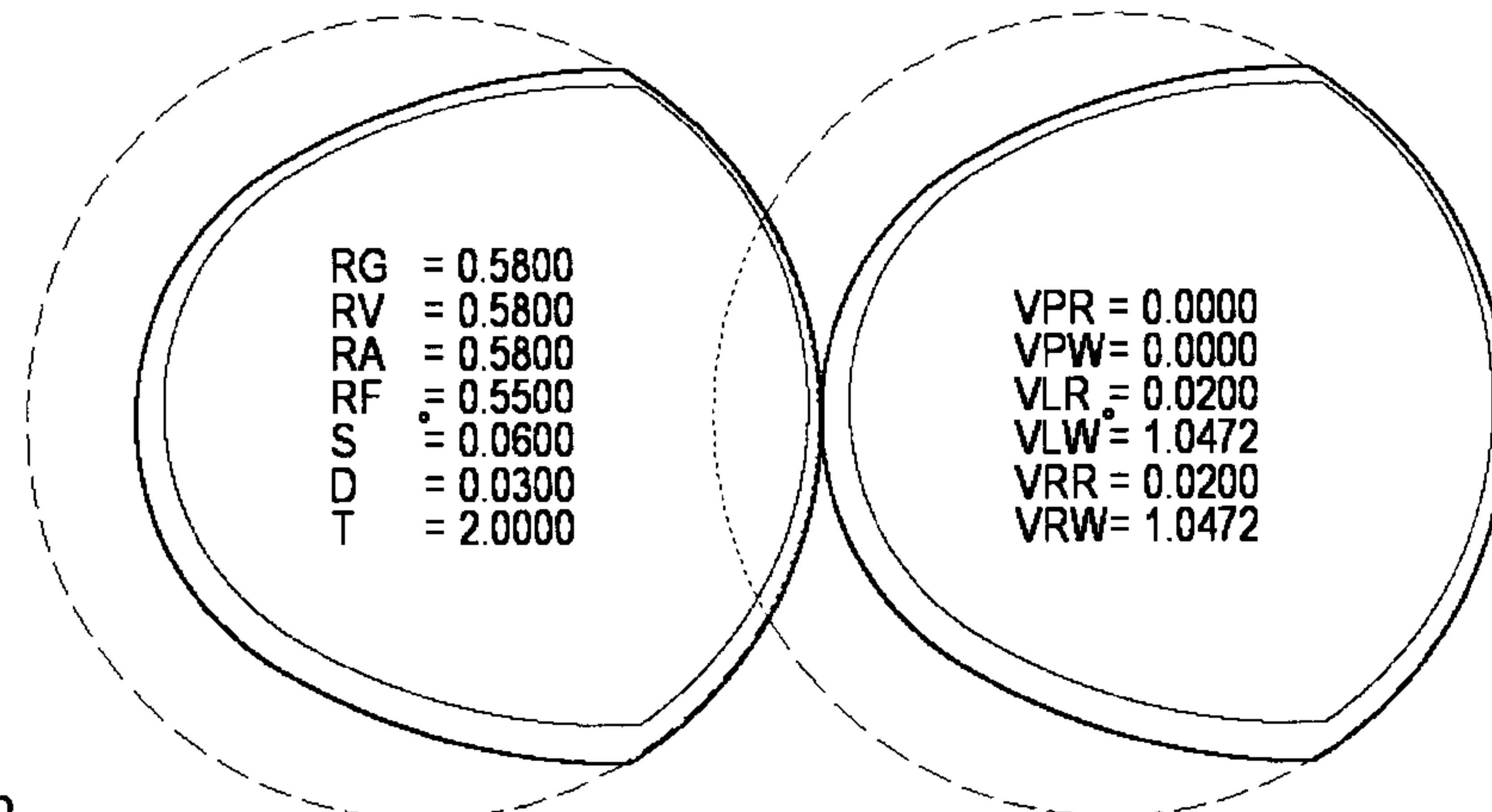


Figure 23b

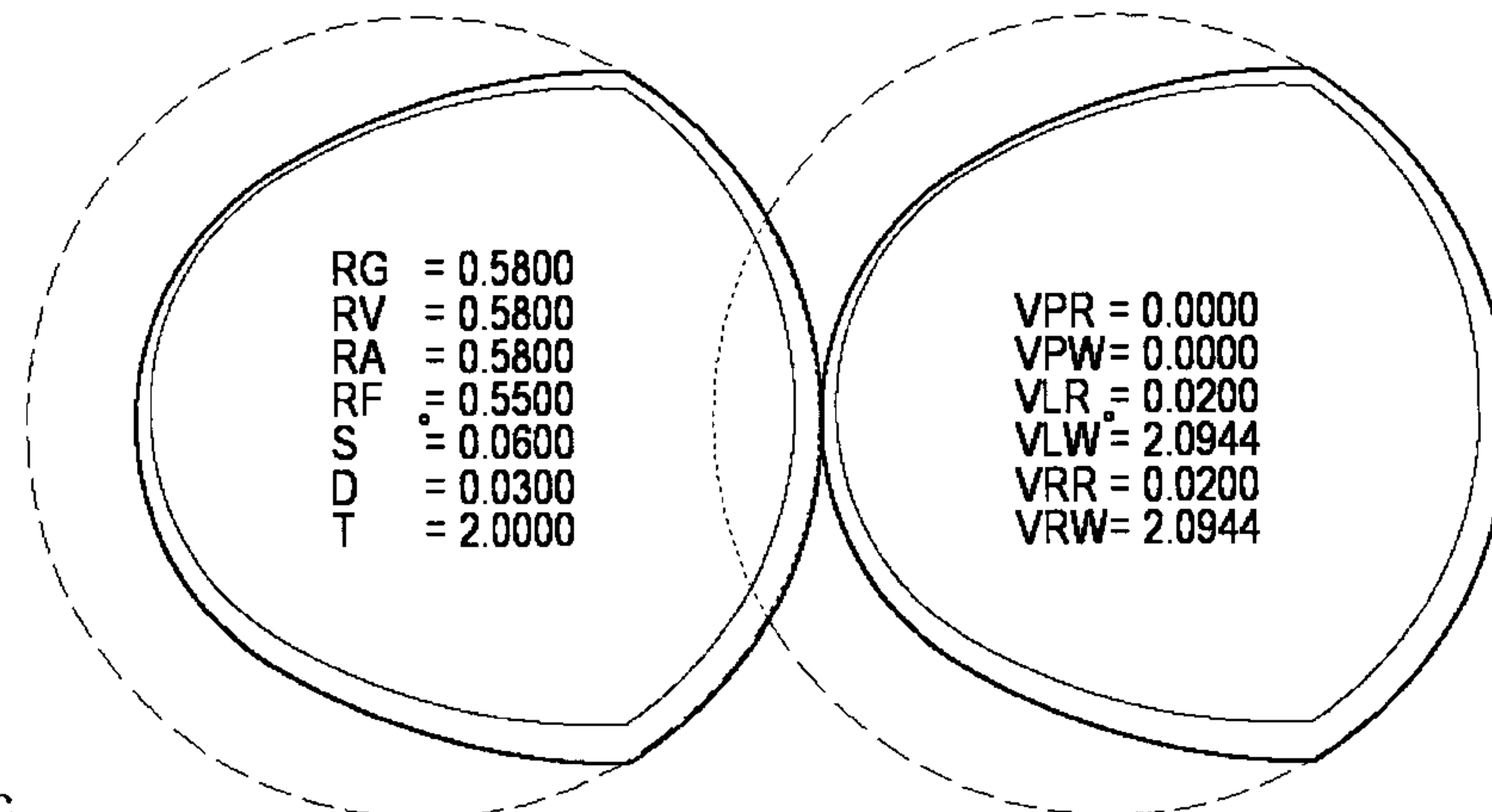


Figure 23c

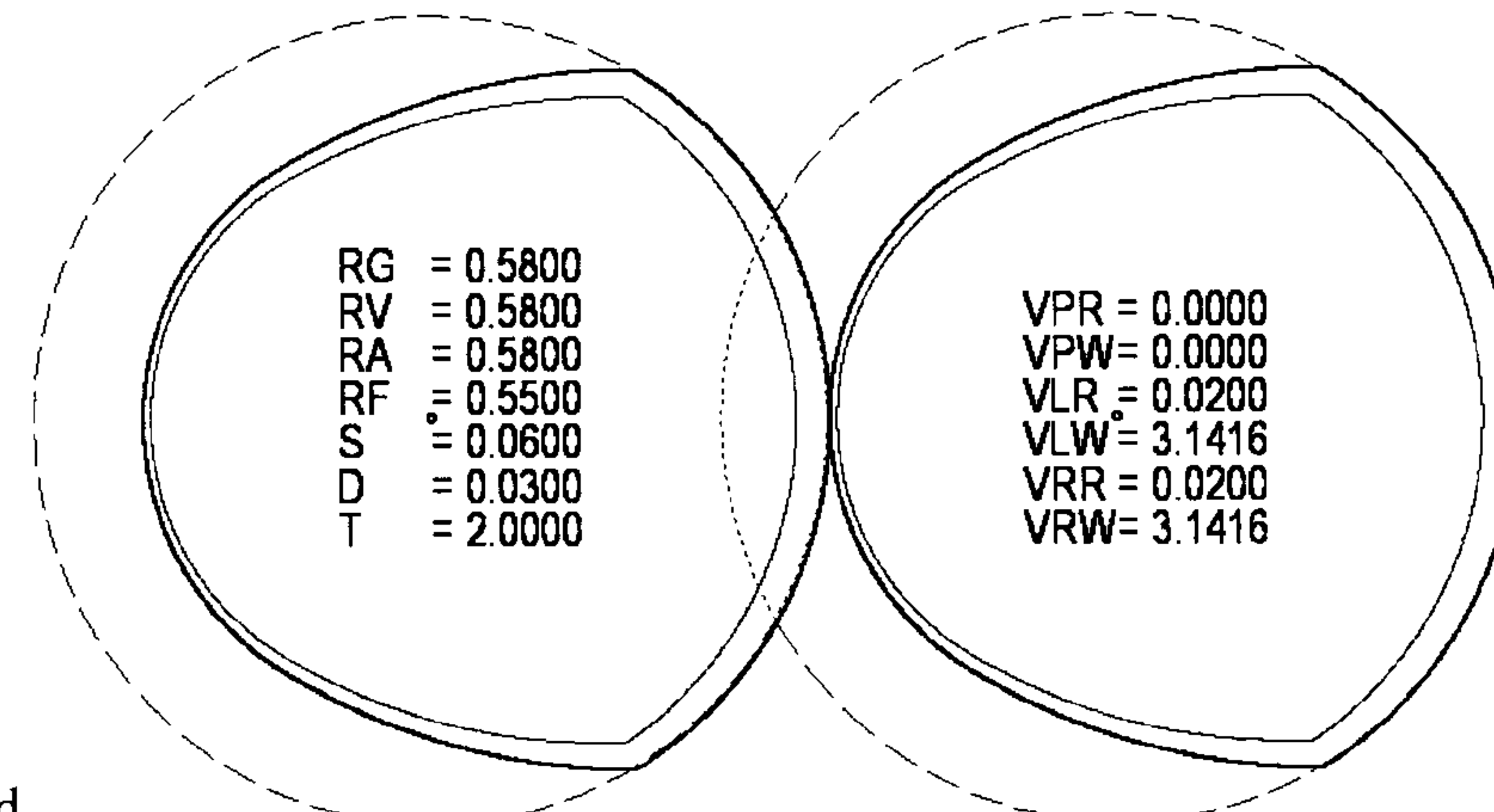


Figure 23d

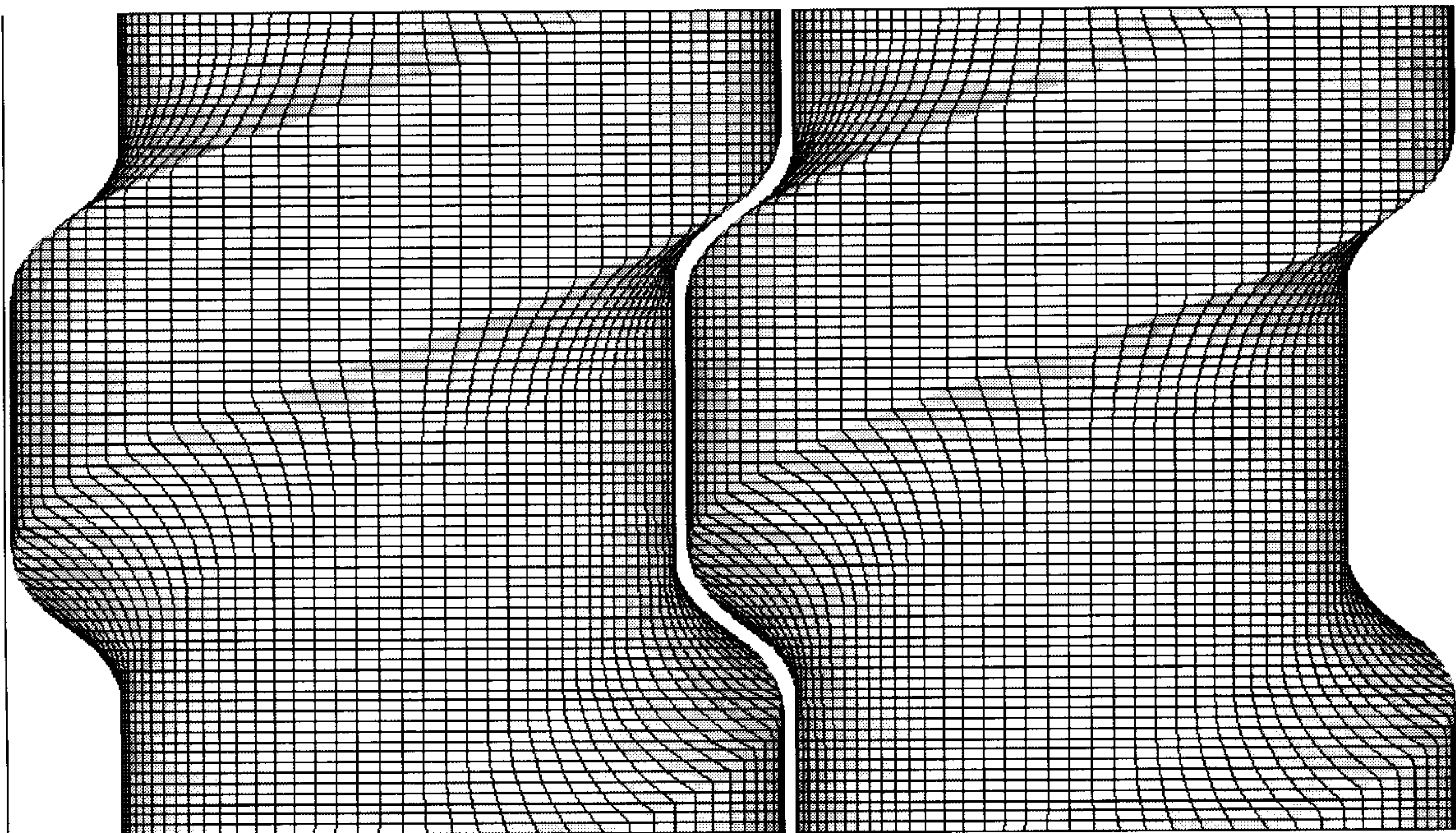
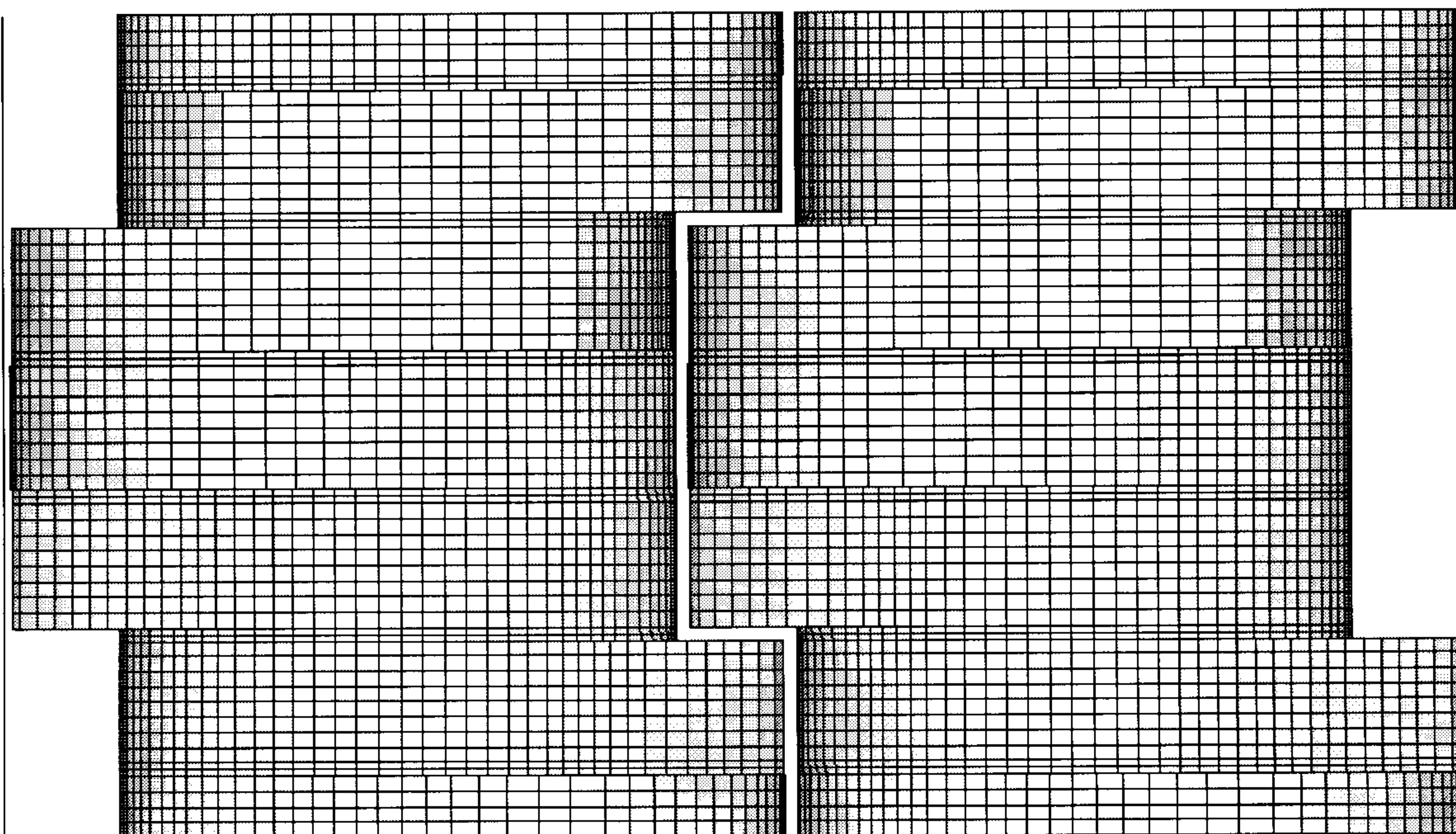
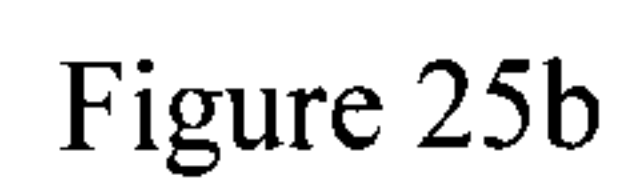
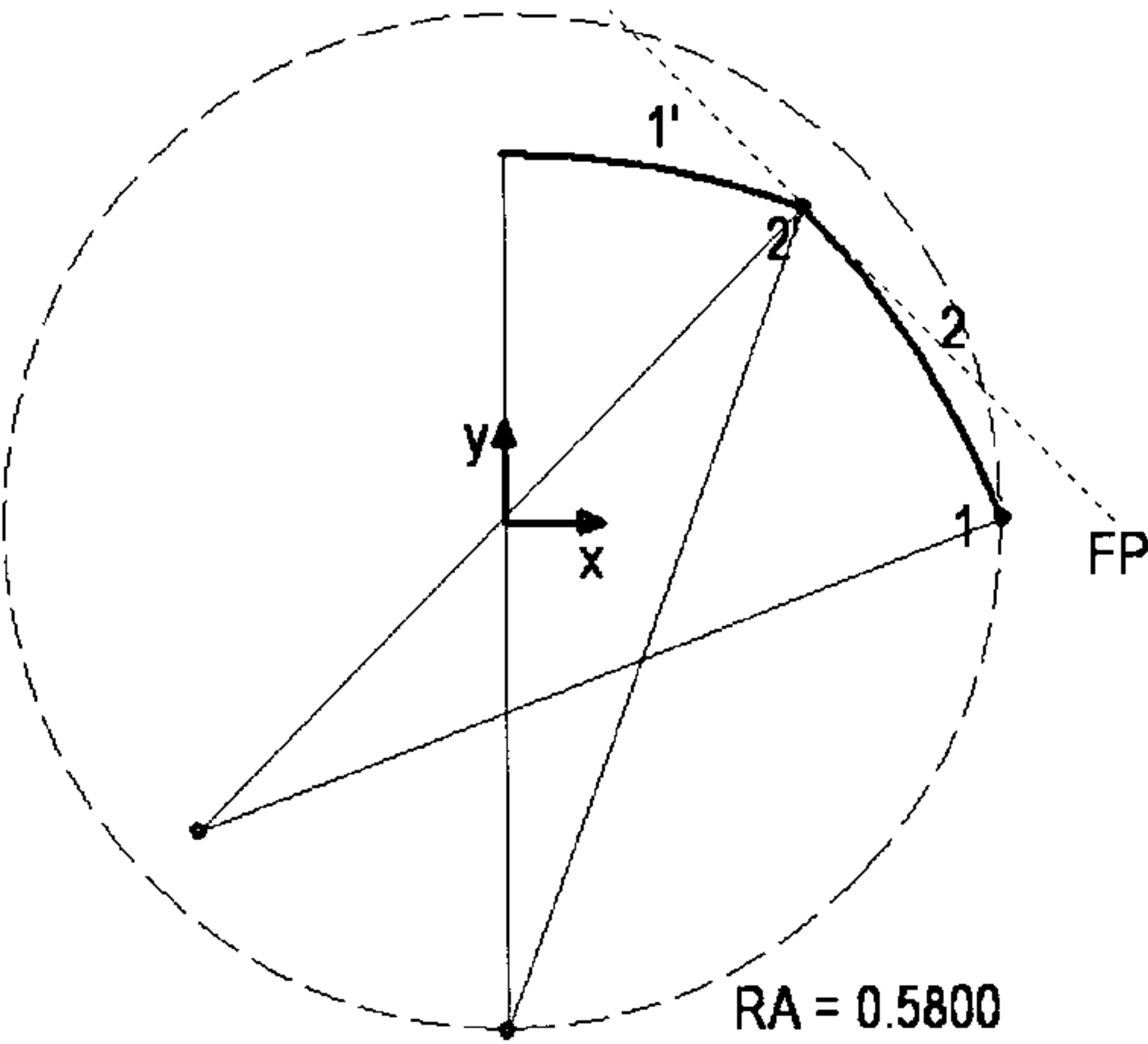


Figure 24a



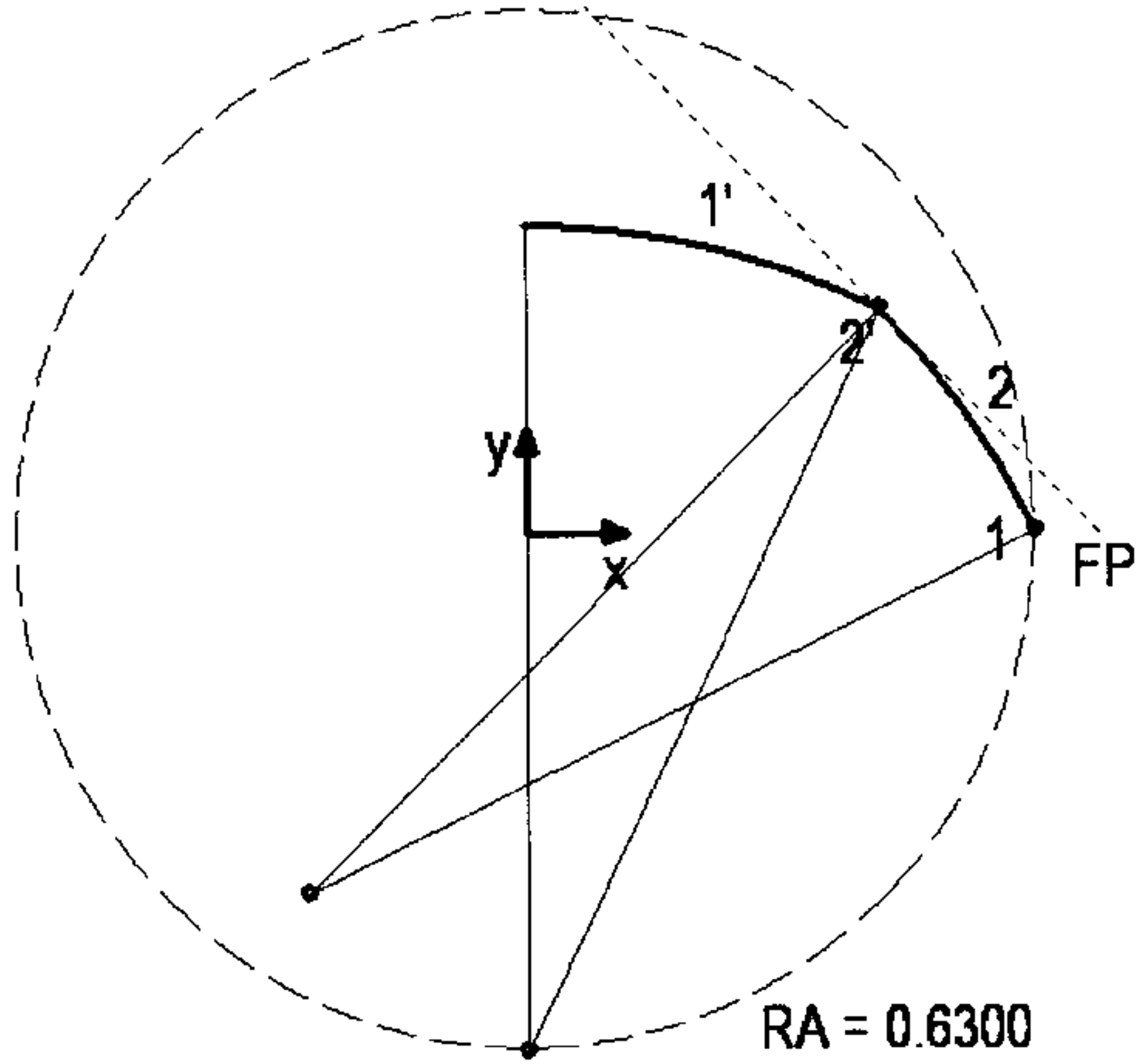
5 Figure 24b





- 1) $R = 0.0000$ $Mx = 0.5800$
 $\alpha = 0.3582$ $My = 0.0000$
- 2) $R = 1.0000$ $Mx = -0.3565$
 $\alpha = 0.4272$ $My = -0.3506$
- 2') $R = 0.0000$ $Mx = 0.3506$
 $\alpha = 0.4272$ $My = 0.3565$
- 1') $R = 1.0000$ $Mx = -0.0000$
 $\alpha = 0.3582$ $My = -0.5800$

Figure 27a



- 1) $R = 0.0000$ $Mx = 0.6300$
 $\alpha = 0.4537$ $My = 0.0000$
- 2) $R = 1.0000$ $Mx = -0.2688$
 $\alpha = 0.3317$ $My = -0.4383$
- 2') $R = 0.0000$ $Mx = 0.4383$
 $\alpha = 0.3317$ $My = 0.2688$
- 1') $R = 1.0000$ $Mx = -0.0000$
 $\alpha = 0.4537$ $My = -0.6300$

Figure 27b

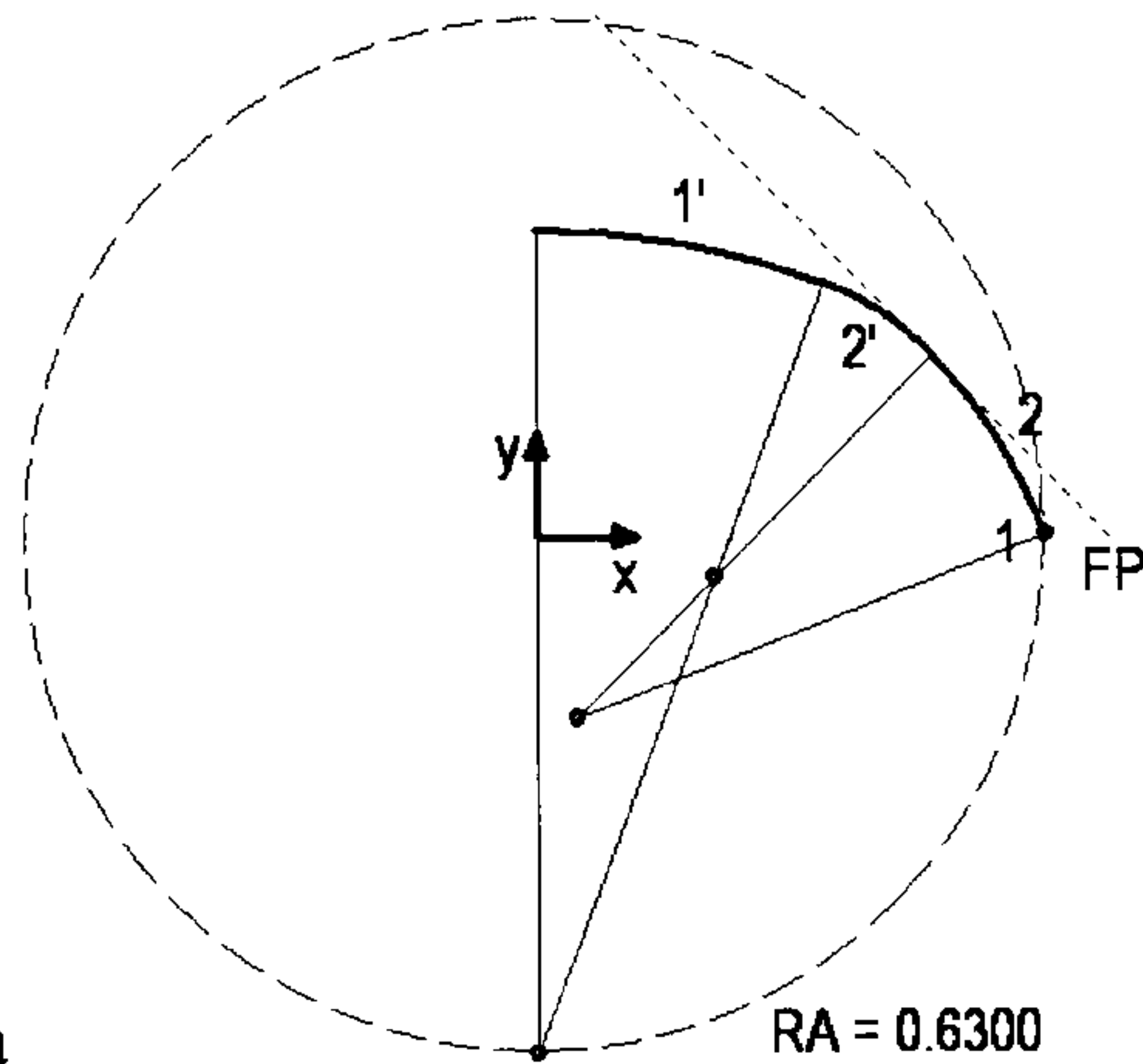


Figure 28a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.3629$ | $My = 0.0000$ |
| 2) | $R = 0.6201$ | $Mx = 0.0503$ |
| | $\alpha = 0.4225$ | $My = -0.2201$ |
| 2') | $R = 0.3799$ | $Mx = 0.2201$ |
| | $\alpha = 0.4225$ | $My = -0.0503$ |
| 1') | $R = 1.0000$ | $Mx = -0.0000$ |
| | $\alpha = 0.3629$ | $My = -0.6300$ |

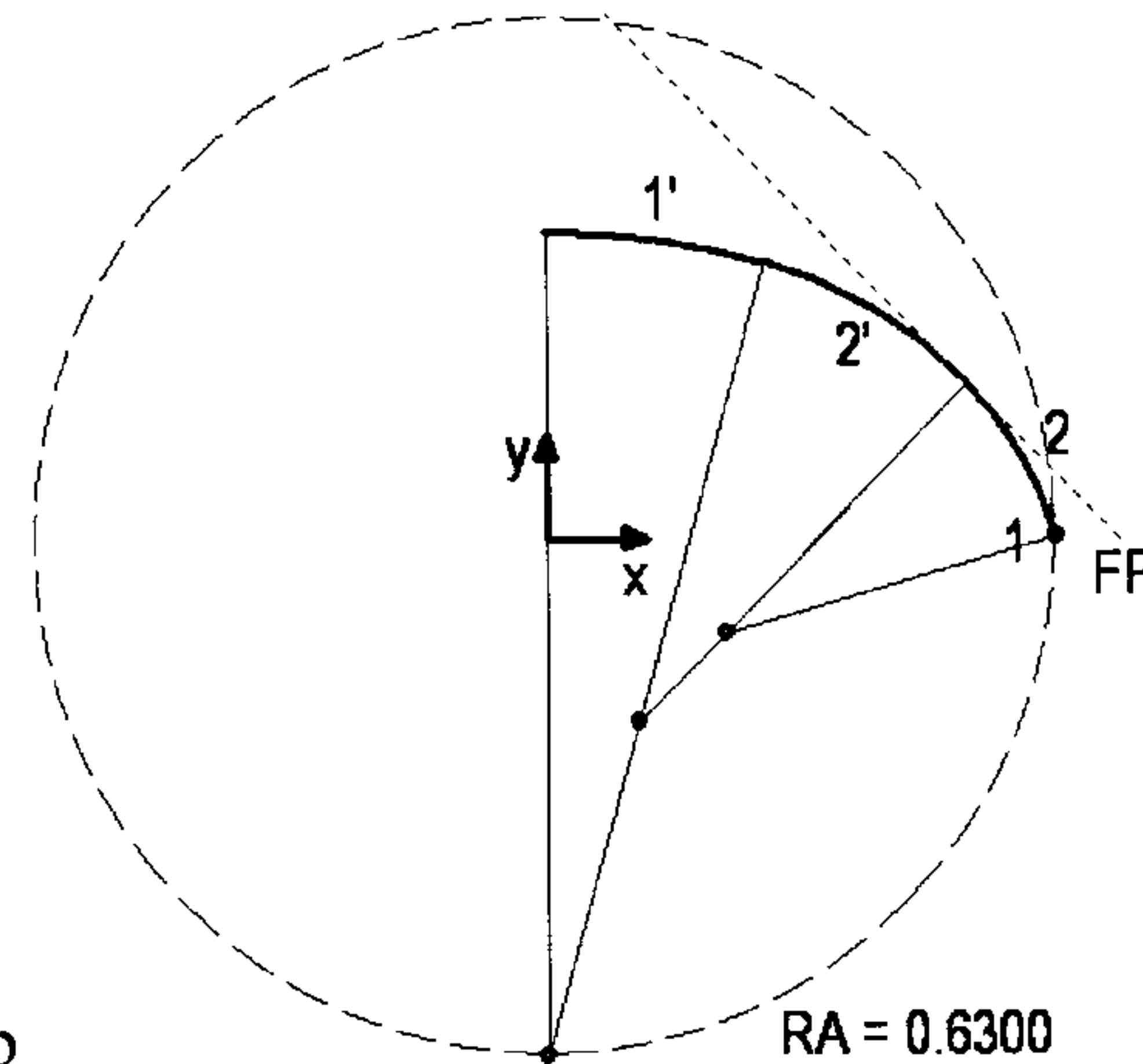


Figure 28b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.2722$ | $My = 0.0000$ |
| 2) | $R = 0.4232$ | $Mx = 0.2224$ |
| | $\alpha = 0.5132$ | $My = -0.1138$ |
| 2') | $R = 0.5768$ | $Mx = 0.1138$ |
| | $\alpha = 0.5132$ | $My = -0.2224$ |
| 1') | $R = 1.0000$ | $Mx = -0.0000$ |
| | $\alpha = 0.2722$ | $My = -0.6300$ |

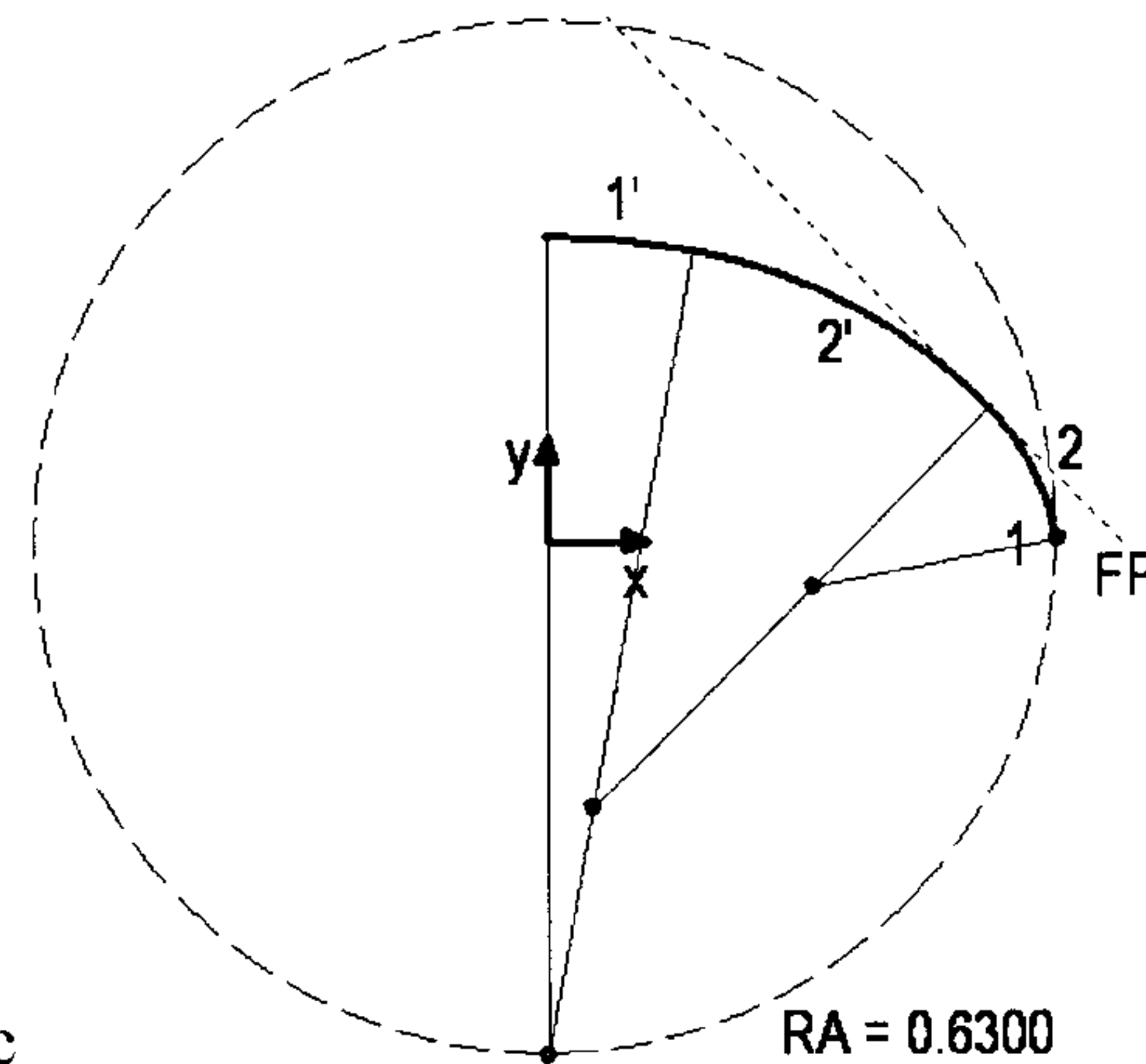


Figure 28c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.1815$ | $My = 0.0000$ |
| 2) | $R = 0.3082$ | $Mx = 0.3268$ |
| | $\alpha = 0.6039$ | $My = -0.0556$ |
| 2') | $R = 0.6918$ | $Mx = 0.0556$ |
| | $\alpha = 0.6039$ | $My = -0.3268$ |
| 1') | $R = 1.0000$ | $Mx = -0.0000$ |
| | $\alpha = 0.1815$ | $My = -0.6300$ |

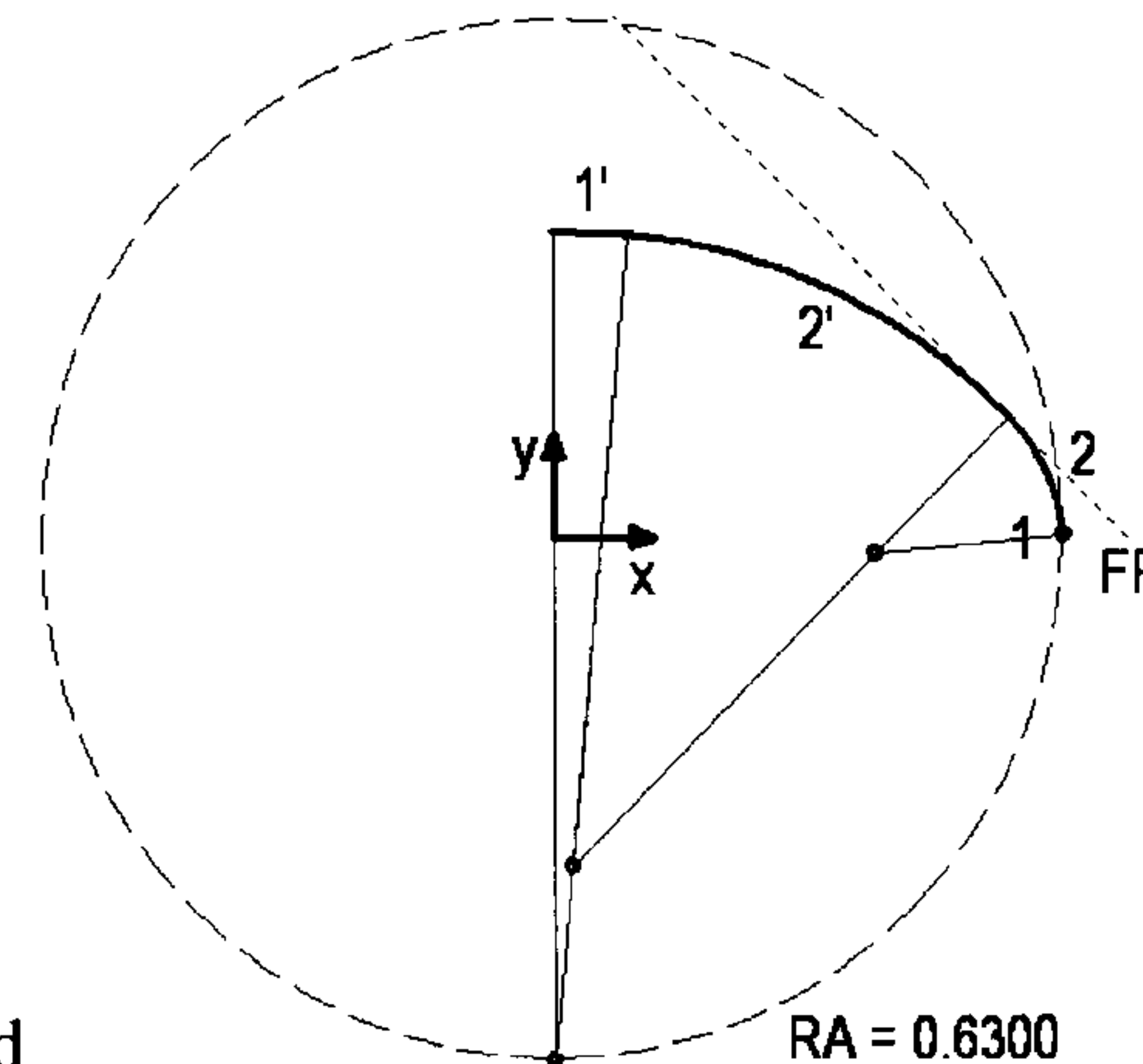


Figure 28d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.6300$ |
| | $\alpha = 0.0907$ | $My = 0.0000$ |
| 2) | $R = 0.2353$ | $Mx = 0.3957$ |
| | $\alpha = 0.6947$ | $My = -0.0213$ |
| 2') | $R = 0.7647$ | $Mx = 0.0213$ |
| | $\alpha = 0.6947$ | $My = -0.3957$ |
| 1') | $R = 1.0000$ | $Mx = -0.0000$ |
| | $\alpha = 0.0907$ | $My = -0.6300$ |

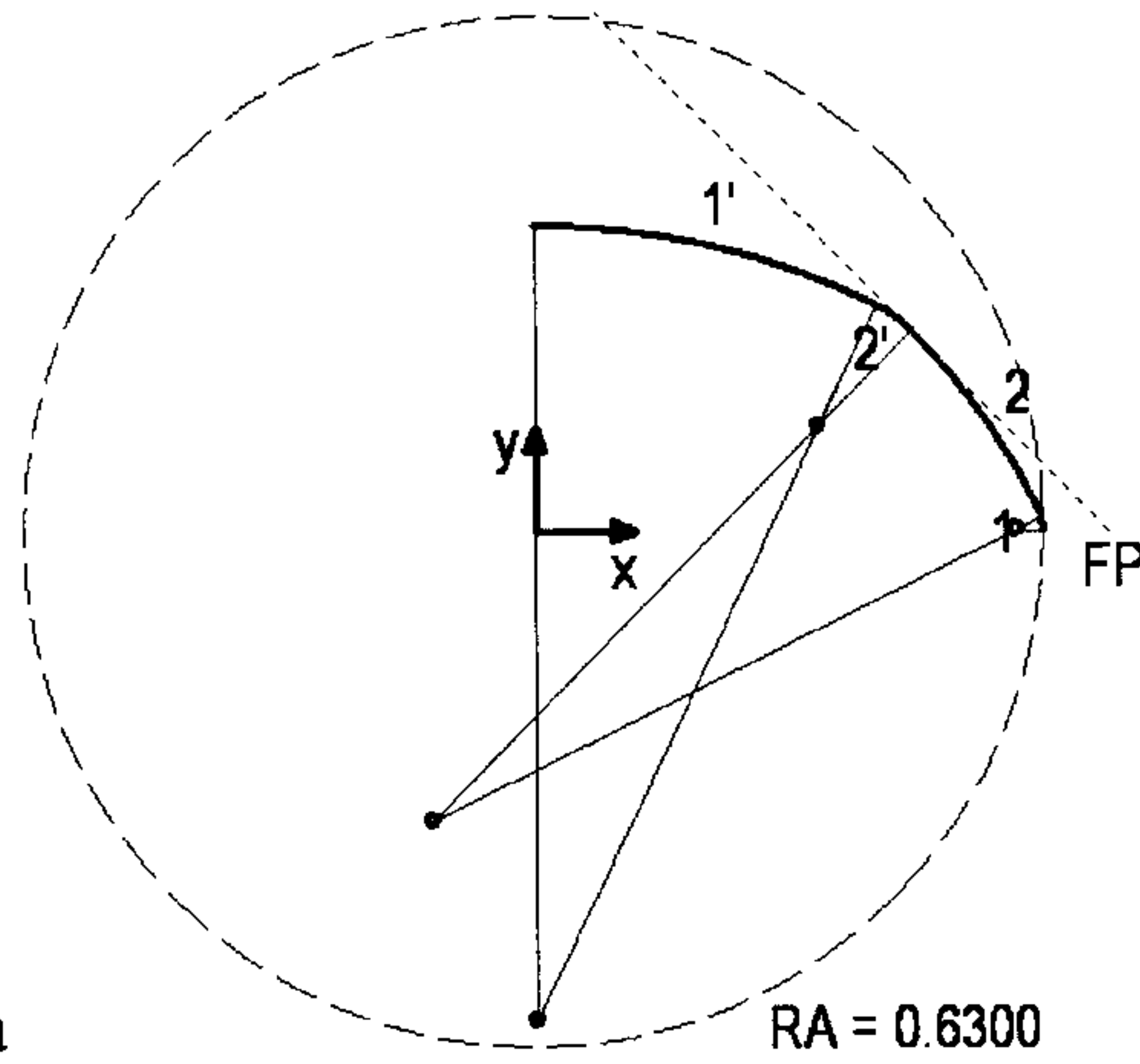


Figure 29a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.0372$ | $M_x = 0.5928$ |
| | $\alpha = 0.4537$ | $M_y = 0.0000$ |
| 2) | $R = 0.8372$ | $M_x = -0.1263$ |
| | $\alpha = 0.3317$ | $M_y = -0.3506$ |
| 2') | $R = 0.1628$ | $M_x = 0.3506$ |
| | $\alpha = 0.3317$ | $M_y = 0.1263$ |
| 1') | $R = 0.9628$ | $M_x = -0.0000$ |
| | $\alpha = 0.4537$ | $M_y = -0.5928$ |

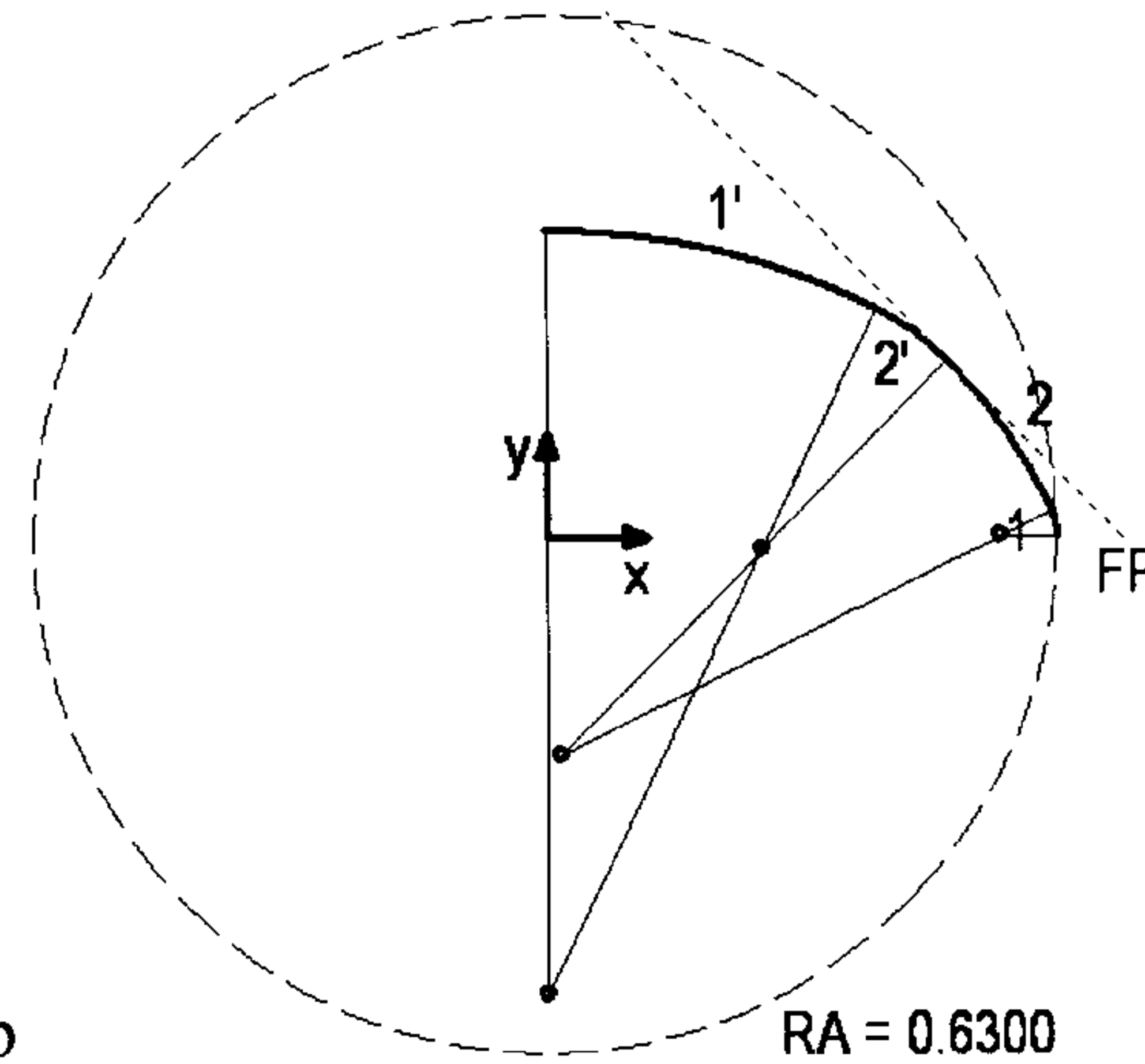


Figure 29b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.0745$ | $M_x = 0.5555$ |
| | $\alpha = 0.4537$ | $M_y = 0.0000$ |
| 2) | $R = 0.6745$ | $M_x = 0.0162$ |
| | $\alpha = 0.3317$ | $M_y = -0.2630$ |
| 2') | $R = 0.3255$ | $M_x = 0.2630$ |
| | $\alpha = 0.3317$ | $M_y = -0.0162$ |
| 1') | $R = 0.9255$ | $M_x = -0.0000$ |
| | $\alpha = 0.4537$ | $M_y = -0.5555$ |

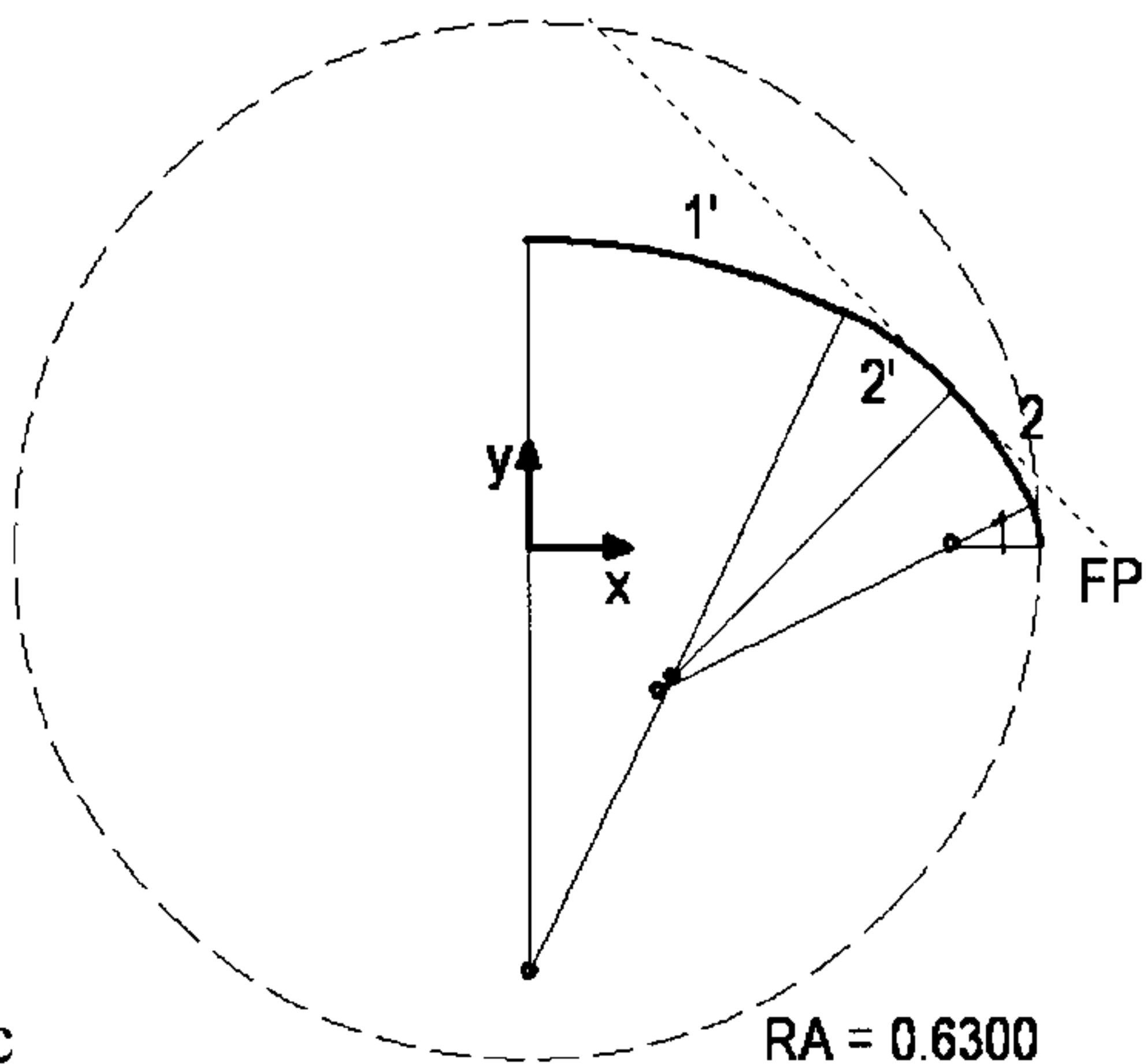


Figure 29c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.1117$ | $M_x = 0.5183$ |
| | $\alpha = 0.4537$ | $M_y = 0.0000$ |
| 2) | $R = 0.5117$ | $M_x = 0.1588$ |
| | $\alpha = 0.3317$ | $M_y = -0.1753$ |
| 2') | $R = 0.4883$ | $M_x = 0.1753$ |
| | $\alpha = 0.3317$ | $M_y = -0.1588$ |
| 1') | $R = 0.8883$ | $M_x = -0.0000$ |
| | $\alpha = 0.4537$ | $M_y = -0.5183$ |

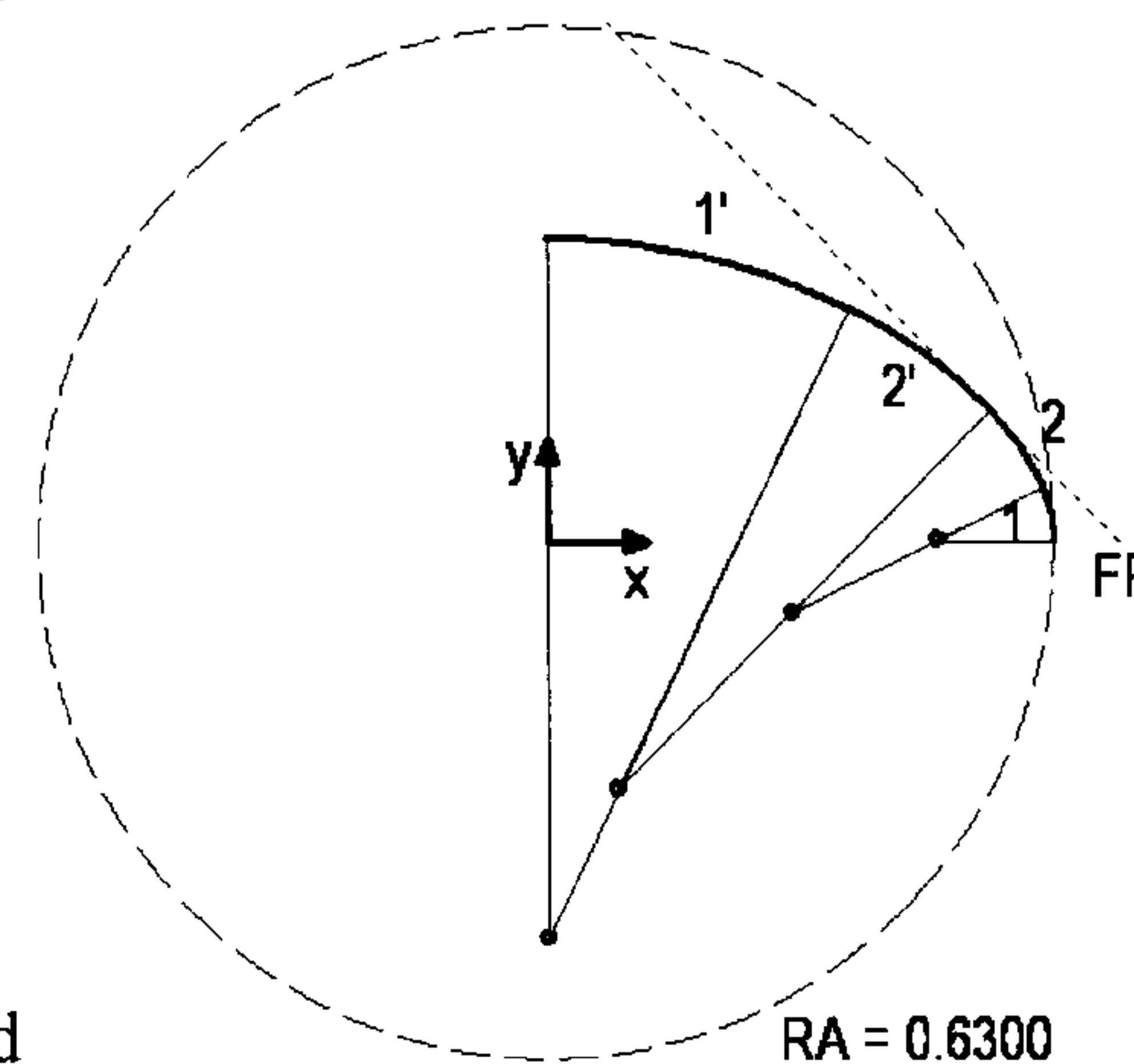


Figure 29d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.1489$ | $M_x = 0.4811$ |
| | $\alpha = 0.4537$ | $M_y = 0.0000$ |
| 2) | $R = 0.3489$ | $M_x = 0.3013$ |
| | $\alpha = 0.3317$ | $M_y = -0.0876$ |
| 2') | $R = 0.6511$ | $M_x = 0.0876$ |
| | $\alpha = 0.3317$ | $M_y = -0.3013$ |
| 1') | $R = 0.8511$ | $M_x = -0.0000$ |
| | $\alpha = 0.4537$ | $M_y = -0.4811$ |

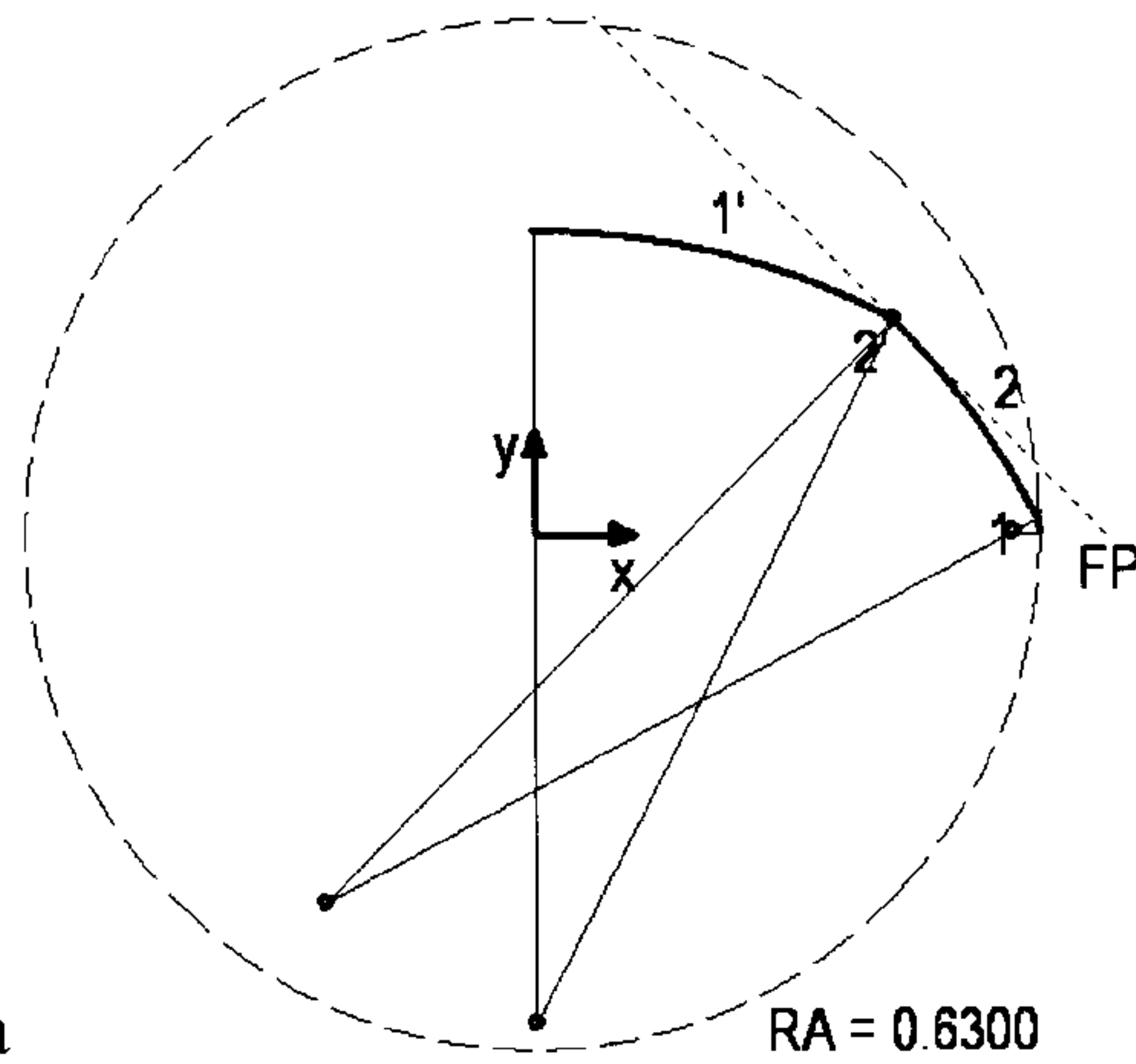


Figure 30a

- 1) $R = 0.0372$ $M_x = 0.5928$
 $\alpha = 0.4832$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.2598$
 $\alpha = 0.3022$ $M_y = -0.4474$
 2') $R = 0.0000$ $M_x = 0.4474$
 $\alpha = 0.3022$ $M_y = 0.2598$
 1') $R = 0.9628$ $M_x = 0.0000$
 $\alpha = 0.4832$ $M_y = -0.5928$

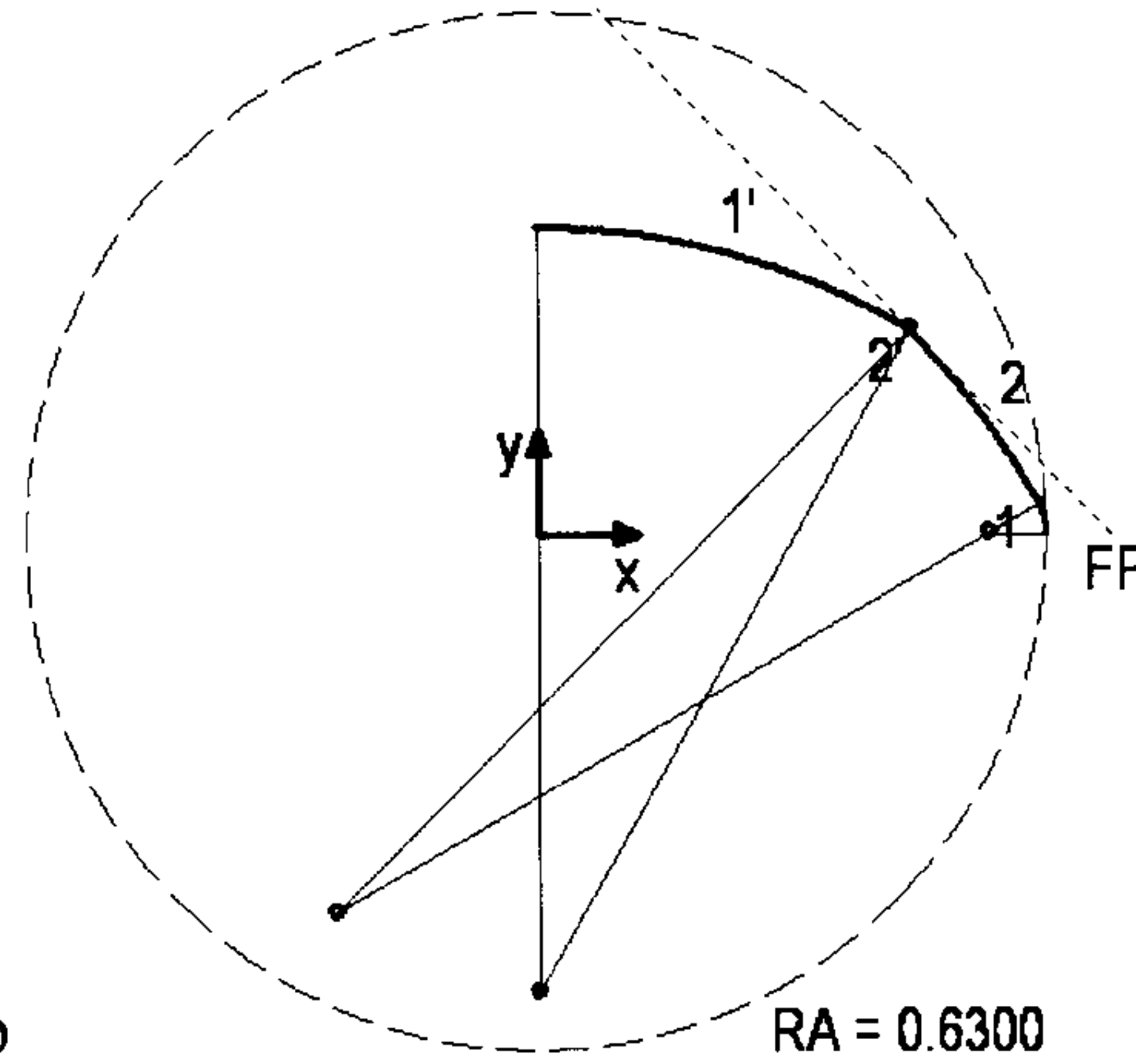


Figure 30b

- 1) $R = 0.0745$ $M_x = 0.5555$
 $\alpha = 0.5187$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.2482$
 $\alpha = 0.2667$ $M_y = -0.4589$
 2') $R = 0.0000$ $M_x = 0.4589$
 $\alpha = 0.2667$ $M_y = 0.2482$
 1') $R = 0.9255$ $M_x = -0.0000$
 $\alpha = 0.5187$ $M_y = -0.5555$

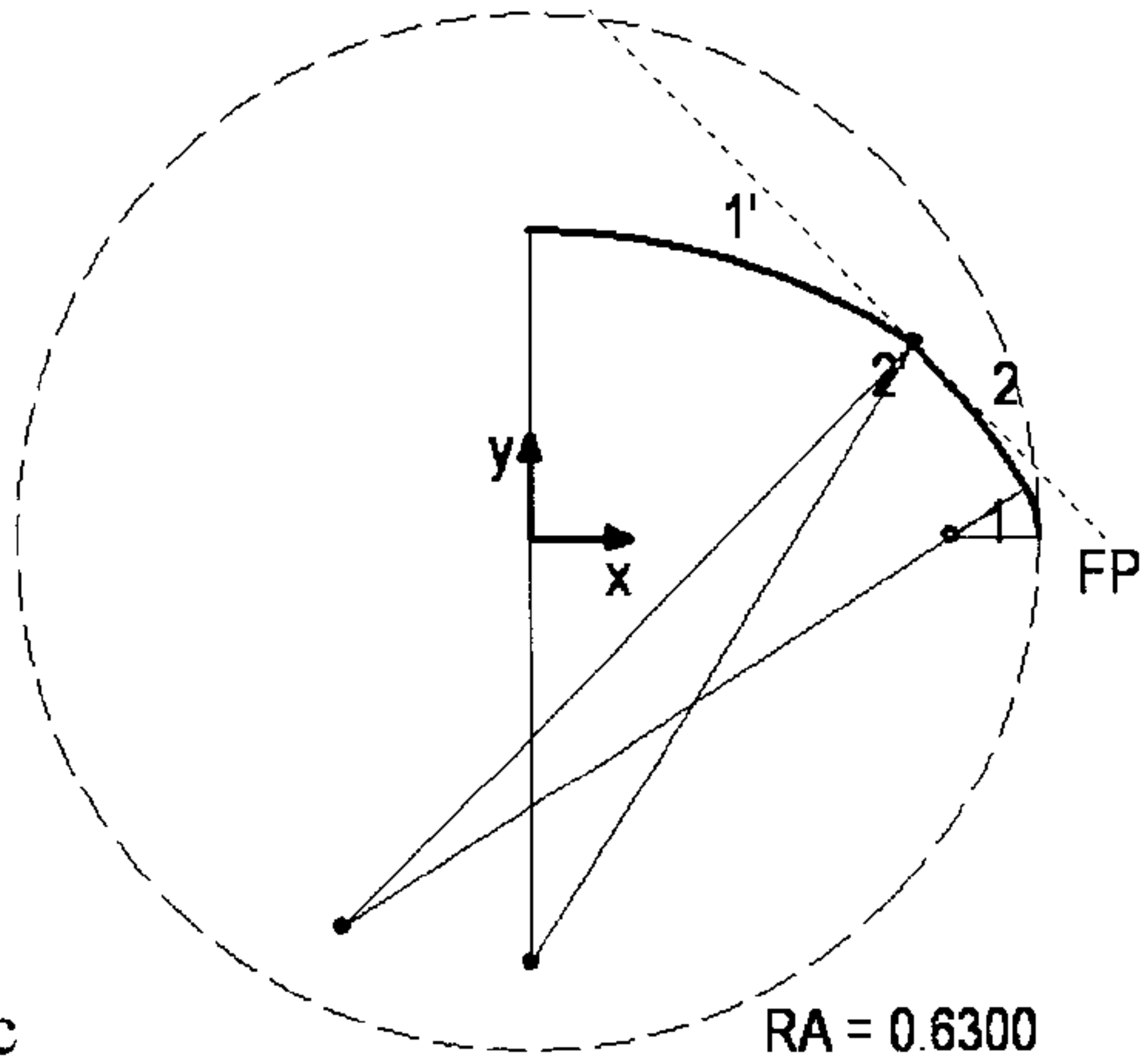


Figure 30c

- 1) $R = 0.1117$ $M_x = 0.5183$
 $\alpha = 0.5634$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.2327$
 $\alpha = 0.2220$ $M_y = -0.4744$
 2') $R = 0.0000$ $M_x = 0.4744$
 $\alpha = 0.2220$ $M_y = 0.2327$
 1') $R = 0.8883$ $M_x = -0.0000$
 $\alpha = 0.5634$ $M_y = -0.5183$

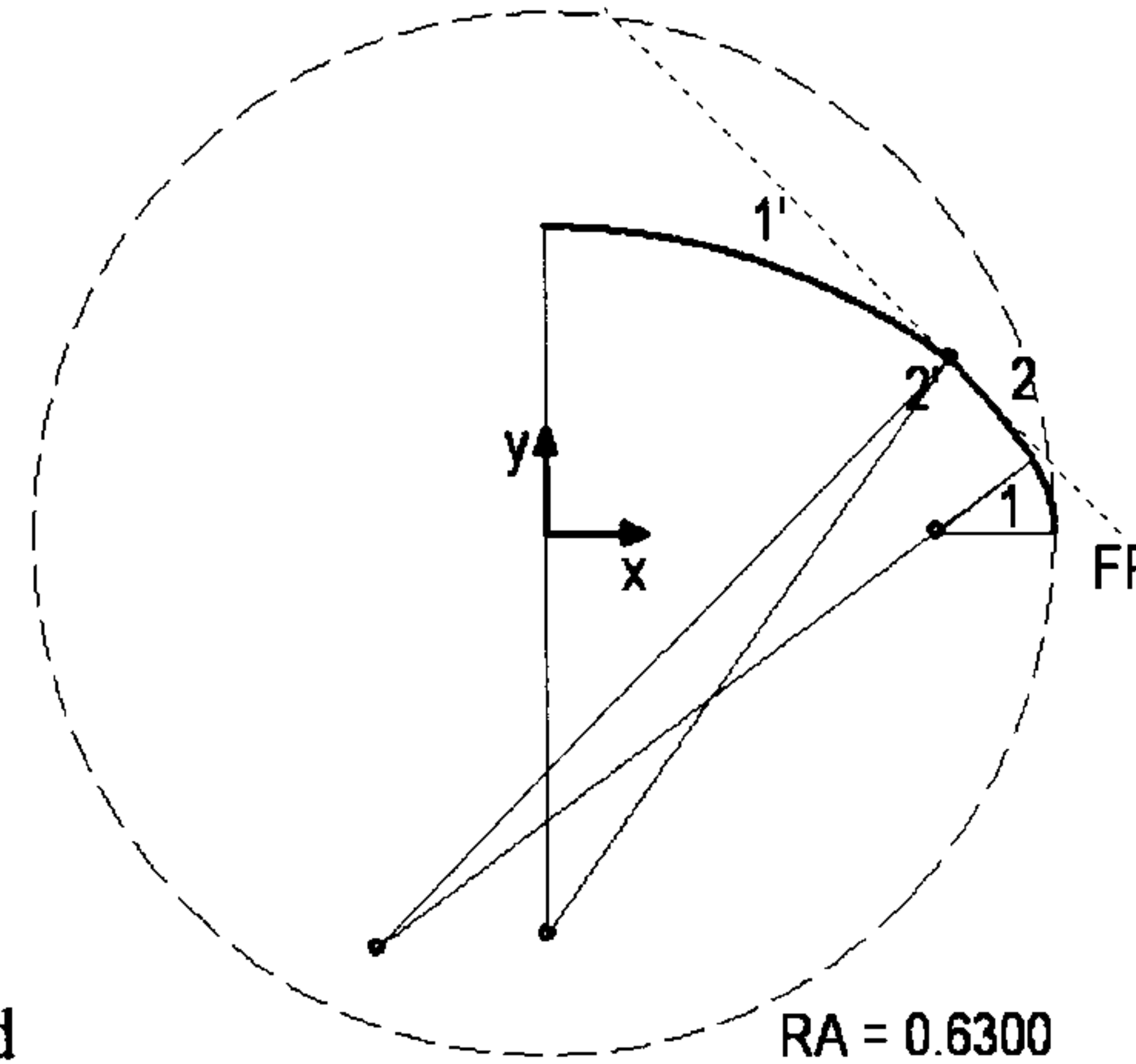


Figure 30d

- 1) $R = 0.1489$ $M_x = 0.4811$
 $\alpha = 0.6251$ $M_y = 0.0000$
 2) $R = 1.0000$ $M_x = -0.2090$
 $\alpha = 0.1603$ $M_y = -0.4981$
 2') $R = 0.0000$ $M_x = 0.4981$
 $\alpha = 0.1603$ $M_y = 0.2090$
 1') $R = 0.8511$ $M_x = -0.0000$
 $\alpha = 0.6251$ $M_y = -0.4811$

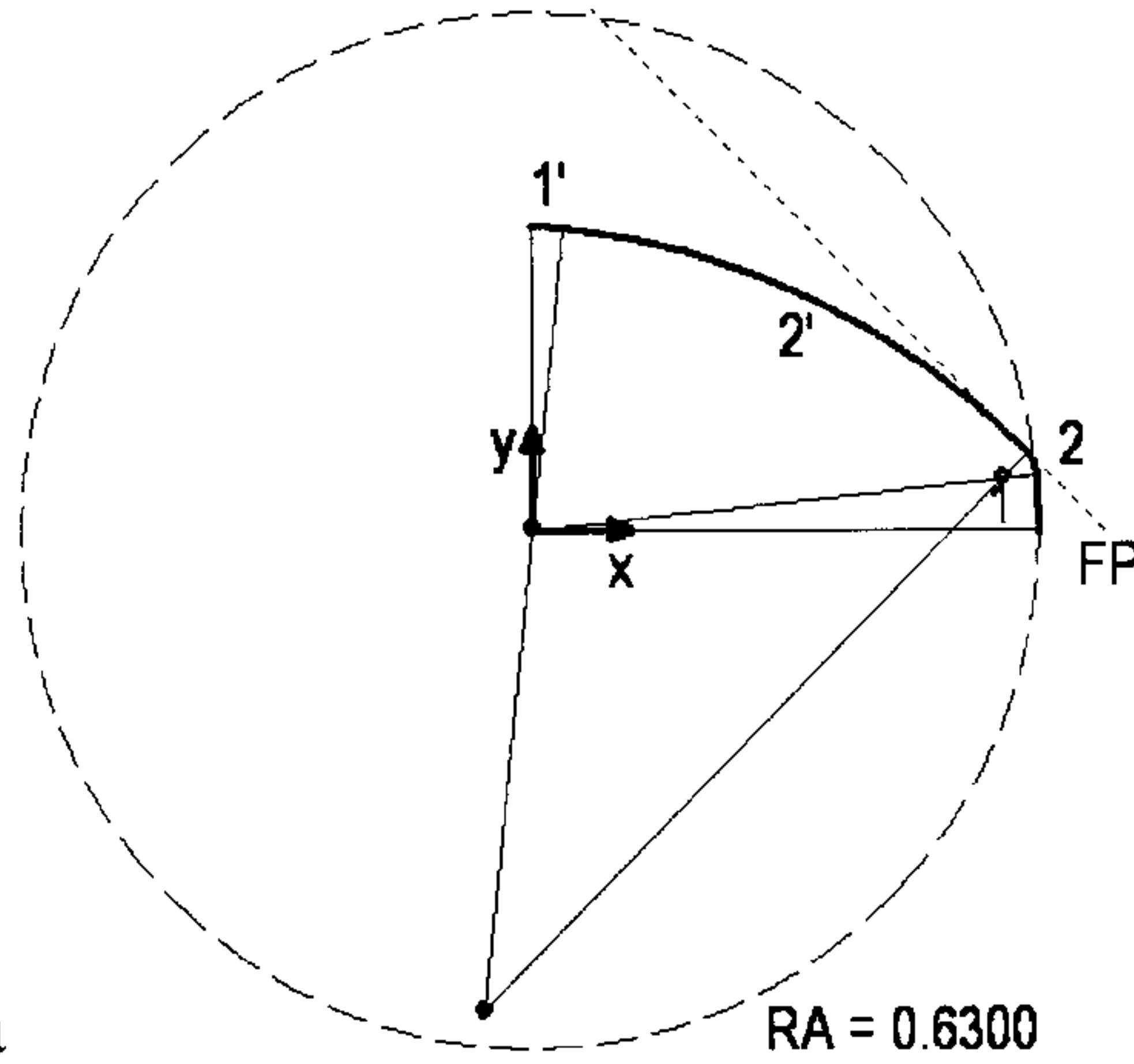


Figure 31a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.6300$ | $Mx = 0.0000$ |
| | $\alpha = 0.1051$ | $My = 0.0000$ |
| 2) | $R = 0.0460$ | $Mx = 0.5808$ |
| | $\alpha = 0.6803$ | $My = 0.0613$ |
| 2') | $R = 0.9540$ | $Mx = -0.0613$ |
| | $\alpha = 0.6803$ | $My = -0.5808$ |
| 1') | $R = 0.3700$ | $Mx = 0.0000$ |
| | $\alpha = 0.1051$ | $My = 0.0000$ |

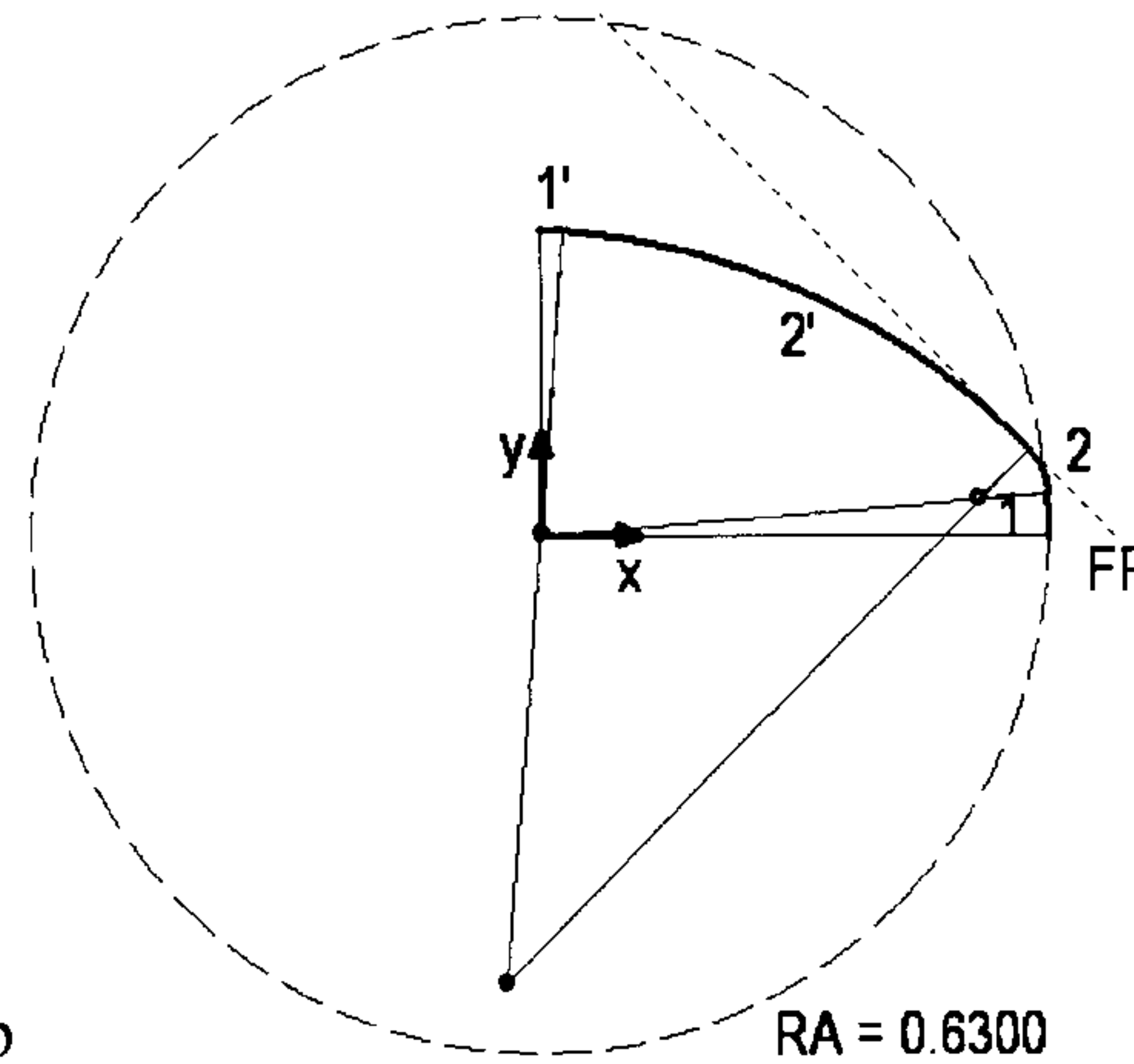


Figure 31b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.6300$ | $Mx = 0.0000$ |
| | $\alpha = 0.0788$ | $My = 0.0000$ |
| 2) | $R = 0.0870$ | $Mx = 0.5413$ |
| | $\alpha = 0.7066$ | $My = 0.0428$ |
| 2') | $R = 0.9130$ | $Mx = -0.0428$ |
| | $\alpha = 0.7066$ | $My = -0.5413$ |
| 1') | $R = 0.3700$ | $Mx = 0.0000$ |
| | $\alpha = 0.0788$ | $My = 0.0000$ |

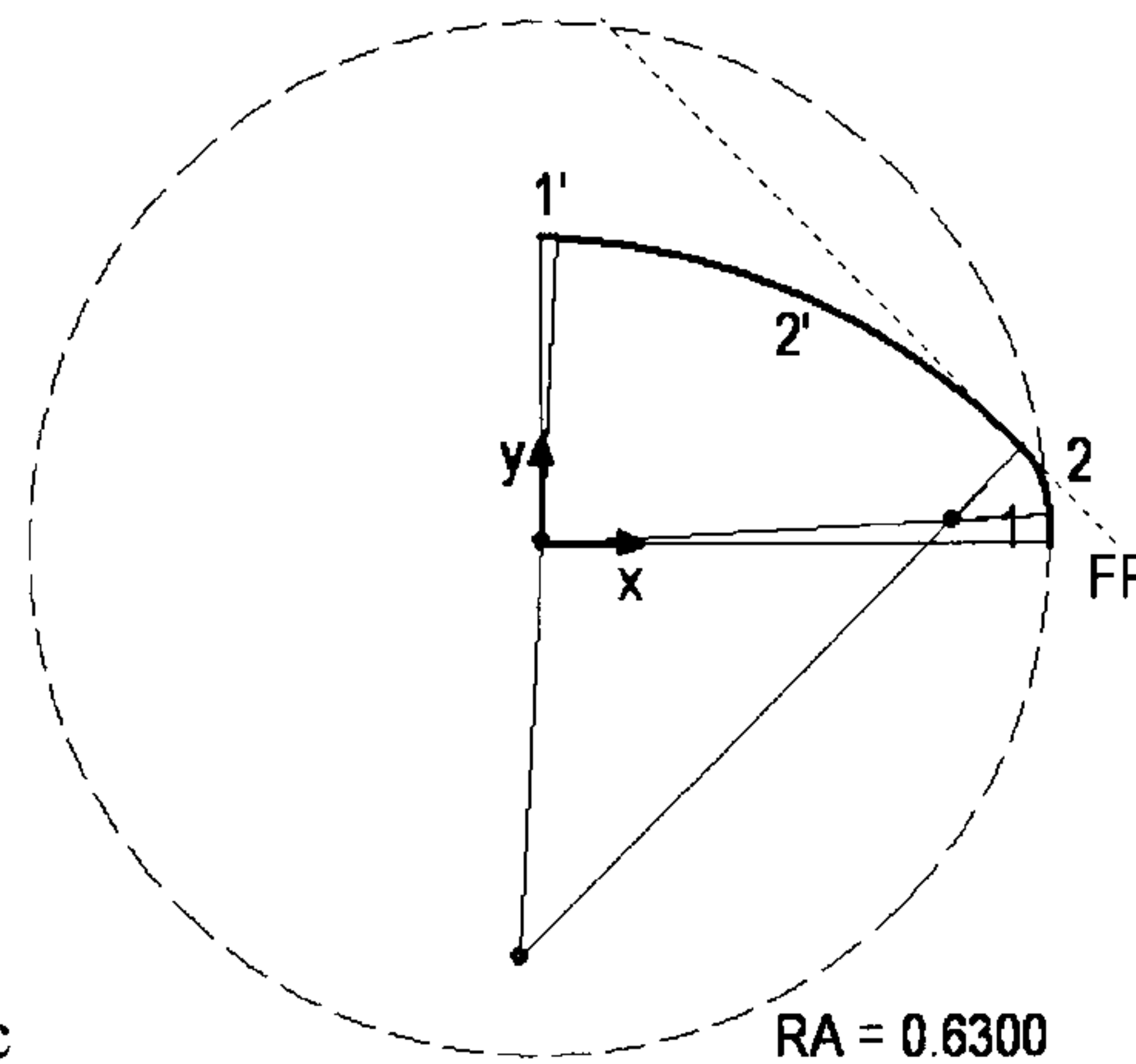


Figure 31c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.6300$ | $Mx = 0.0000$ |
| | $\alpha = 0.0526$ | $My = 0.0000$ |
| 2) | $R = 0.1236$ | $Mx = 0.5057$ |
| | $\alpha = 0.7328$ | $My = 0.0266$ |
| 2') | $R = 0.8764$ | $Mx = -0.0266$ |
| | $\alpha = 0.7328$ | $My = -0.5057$ |
| 1') | $R = 0.3700$ | $Mx = 0.0000$ |
| | $\alpha = 0.0526$ | $My = 0.0000$ |

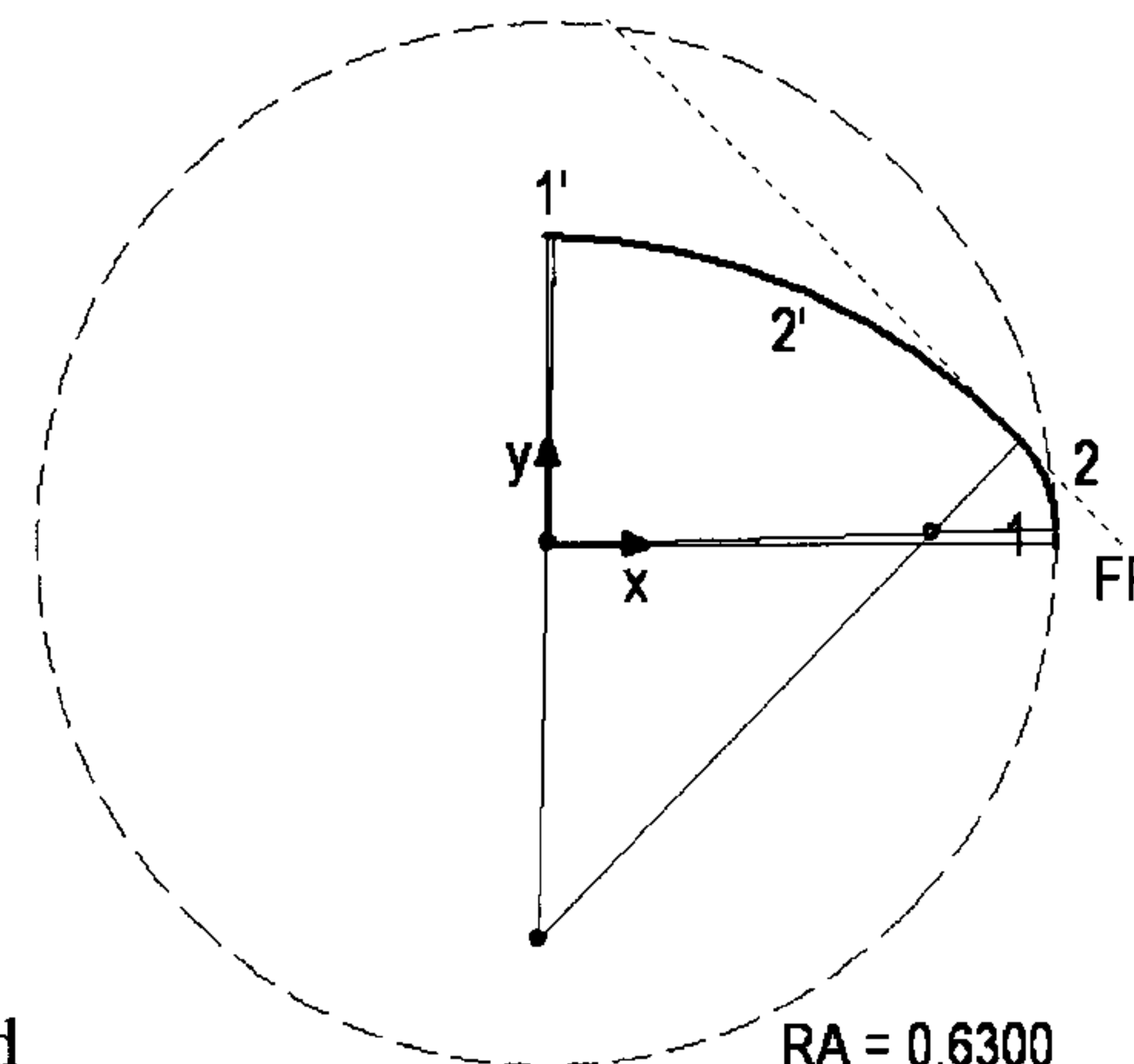


Figure 31d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.6300$ | $Mx = 0.0000$ |
| | $\alpha = 0.0263$ | $My = 0.0000$ |
| 2) | $R = 0.1565$ | $Mx = 0.4733$ |
| | $\alpha = 0.7591$ | $My = 0.0124$ |
| 2') | $R = 0.8435$ | $Mx = -0.0124$ |
| | $\alpha = 0.7591$ | $My = -0.4733$ |
| 1') | $R = 0.3700$ | $Mx = 0.0000$ |
| | $\alpha = 0.0263$ | $My = 0.0000$ |

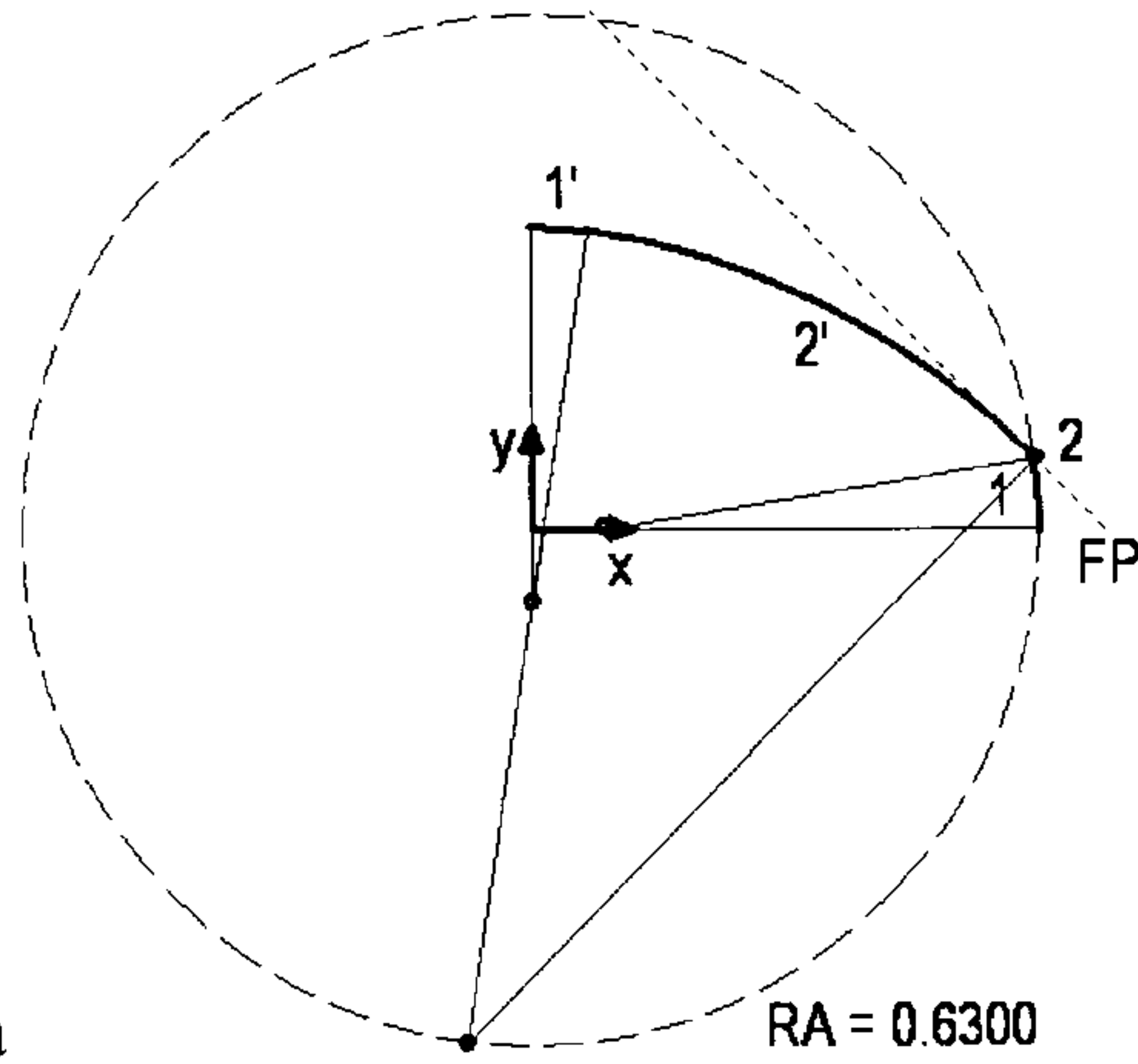


Figure 32a

- 1) $R = 0.5412$ $M_x = 0.0888$
 $\alpha = 0.1551$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.6235$
 $\alpha = 0.6303$ $M_y = 0.0836$
 2') $R = 1.0000$ $M_x = -0.0836$
 $\alpha = 0.6303$ $M_y = -0.6235$
 1') $R = 0.4588$ $M_x = 0.0000$
 $\alpha = 0.1551$ $M_y = -0.0888$

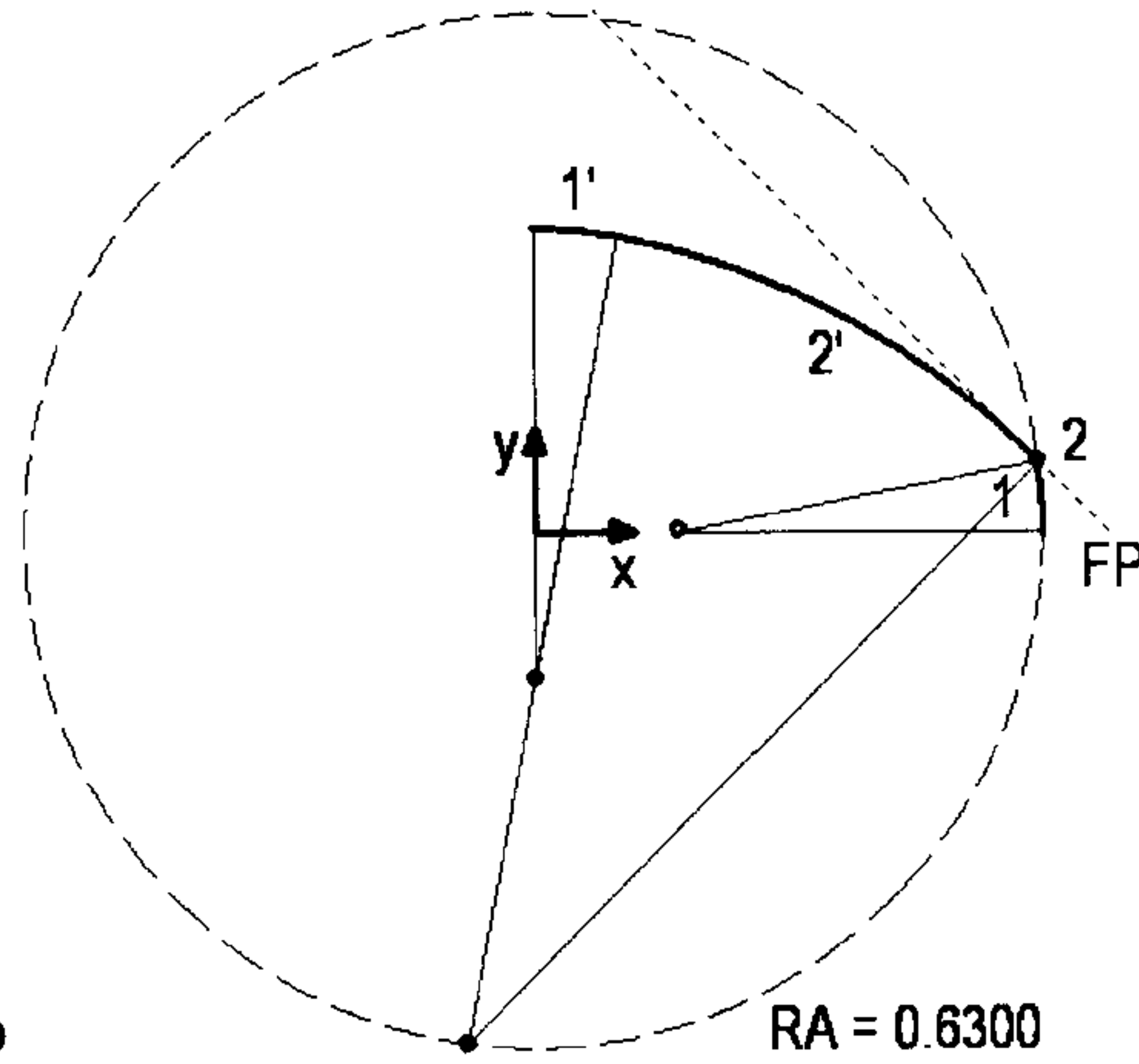


Figure 32b

- 1) $R = 0.4525$ $M_x = 0.1775$
 $\alpha = 0.1894$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.6219$
 $\alpha = 0.5960$ $M_y = 0.0852$
 2') $R = 1.0000$ $M_x = -0.0852$
 $\alpha = 0.5960$ $M_y = -0.6219$
 1') $R = 0.5475$ $M_x = 0.0000$
 $\alpha = 0.1894$ $M_y = -0.1775$

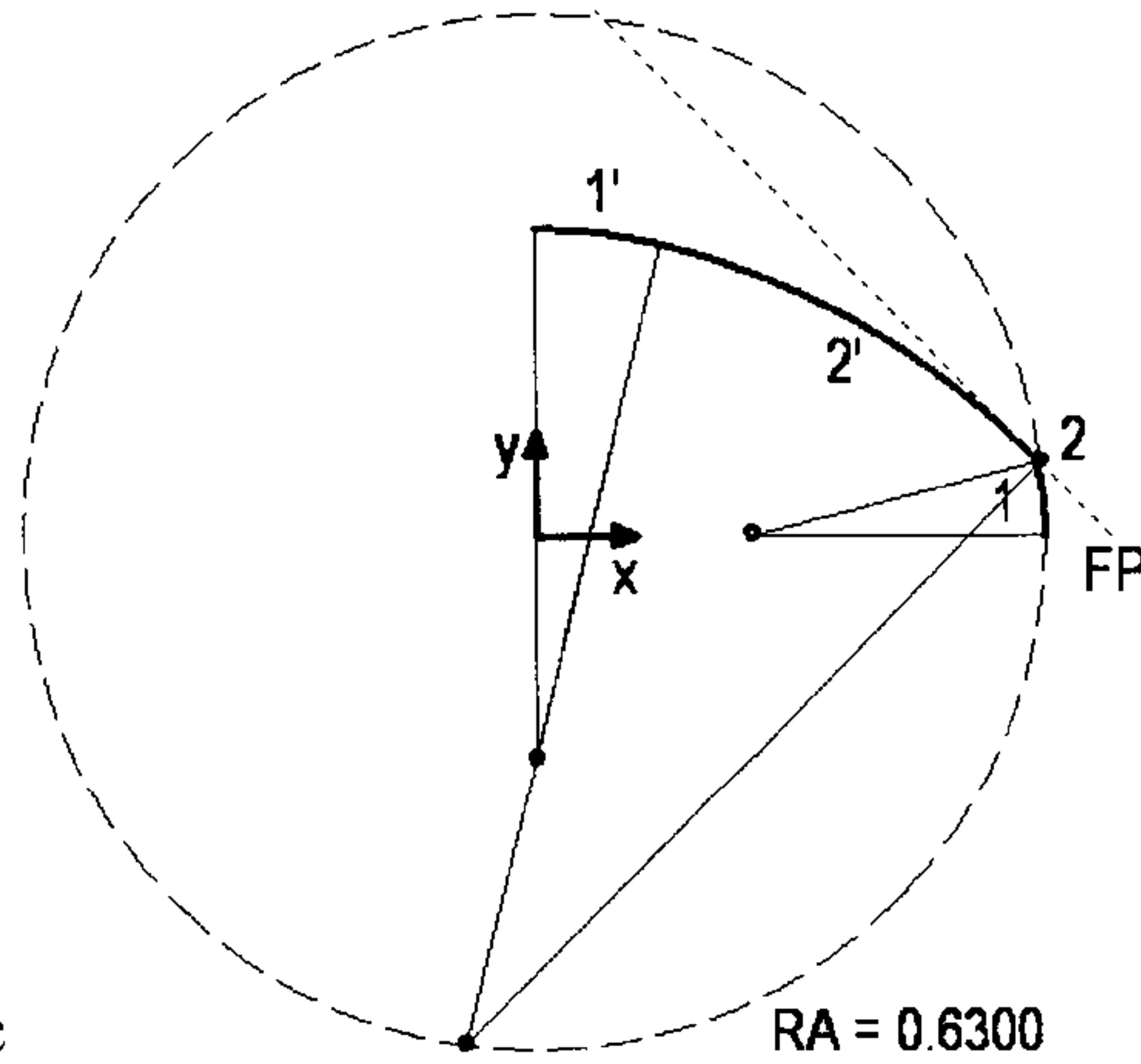


Figure 32c

- 1) $R = 0.3637$ $M_x = 0.2663$
 $\alpha = 0.2441$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.6192$
 $\alpha = 0.5413$ $M_y = 0.0879$
 2') $R = 1.0000$ $M_x = -0.0879$
 $\alpha = 0.5413$ $M_y = -0.6192$
 1') $R = 0.6363$ $M_x = 0.0000$
 $\alpha = 0.2441$ $M_y = -0.2663$

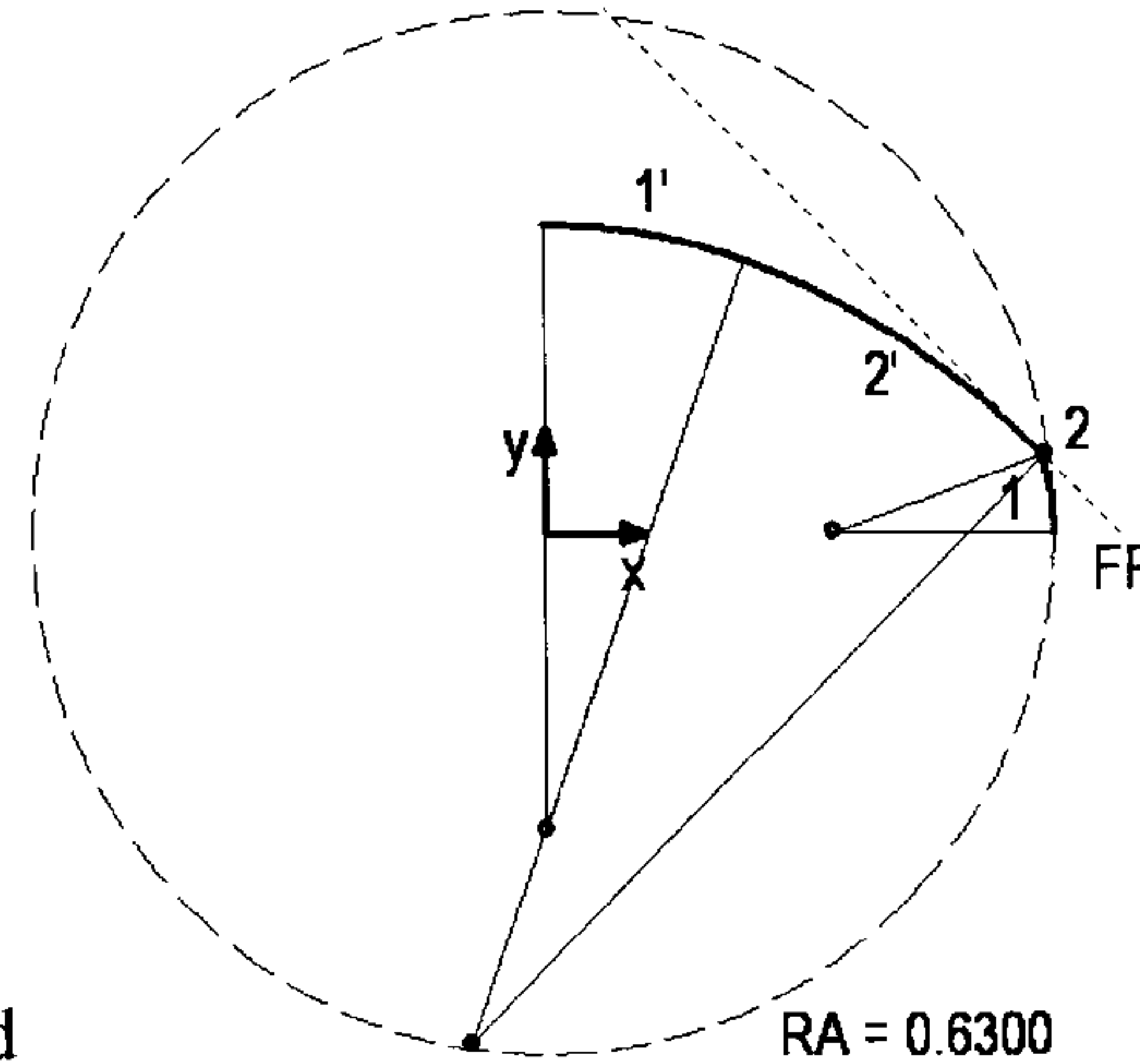


Figure 32d

- 1) $R = 0.2749$ $M_x = 0.3551$
 $\alpha = 0.3470$ $M_y = 0.0000$
 2) $R = 0.0000$ $M_x = 0.6136$
 $\alpha = 0.4384$ $M_y = 0.0935$
 2') $R = 1.0000$ $M_x = -0.0935$
 $\alpha = 0.4384$ $M_y = -0.6136$
 1') $R = 0.7251$ $M_x = 0.0000$
 $\alpha = 0.3470$ $M_y = -0.3551$

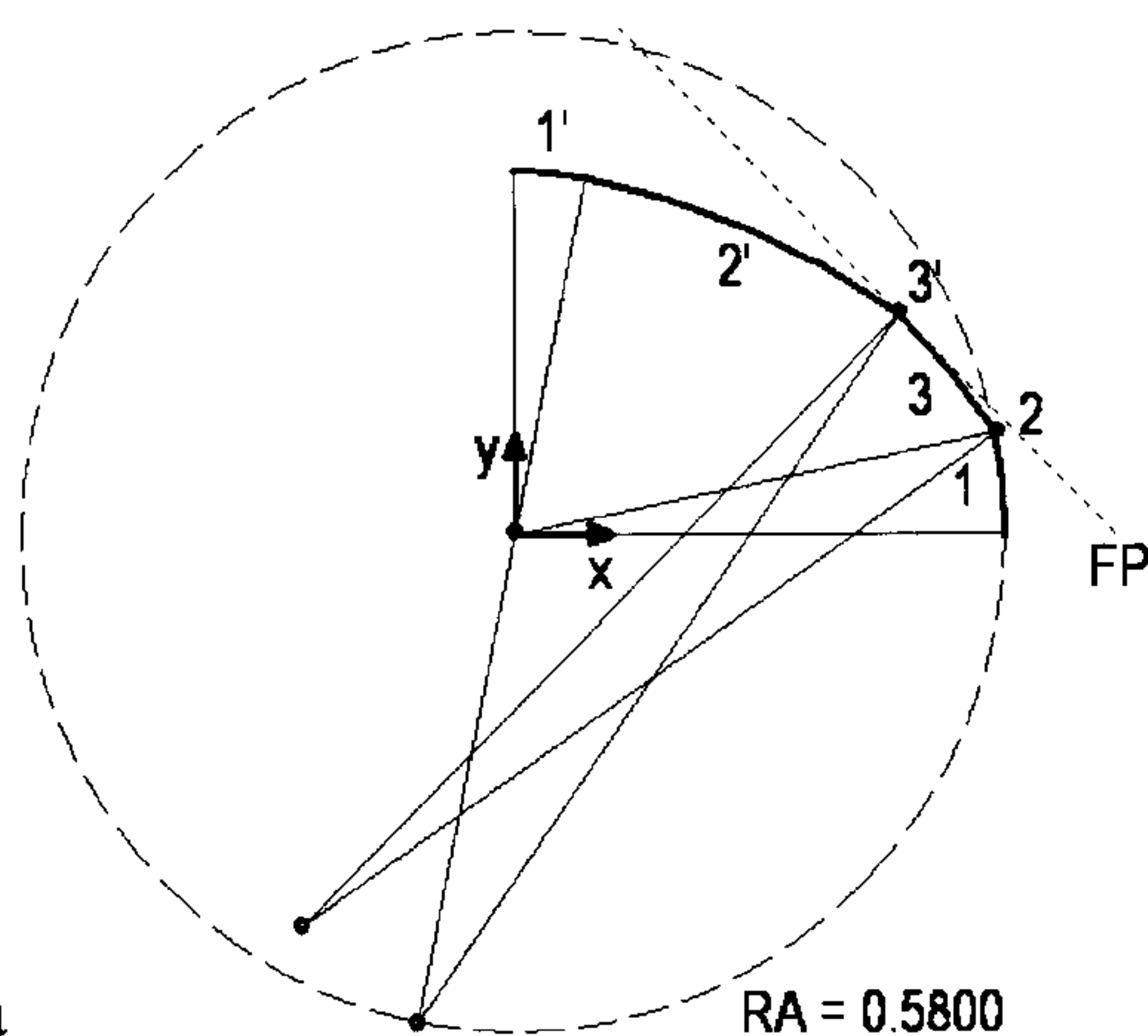


Figure 33a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5681$ |
| | $\alpha = 0.4056$ | $My = 0.1170$ |
| 3) | $R = 1.0000$ | $Mx = -0.2523$ |
| | $\alpha = 0.1767$ | $My = -0.4548$ |
| 3') | $R = 0.0000$ | $Mx = 0.4548$ |
| | $\alpha = 0.1767$ | $My = 0.2523$ |
| 2') | $R = 1.0000$ | $Mx = -0.1170$ |
| | $\alpha = 0.4056$ | $My = -0.5681$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

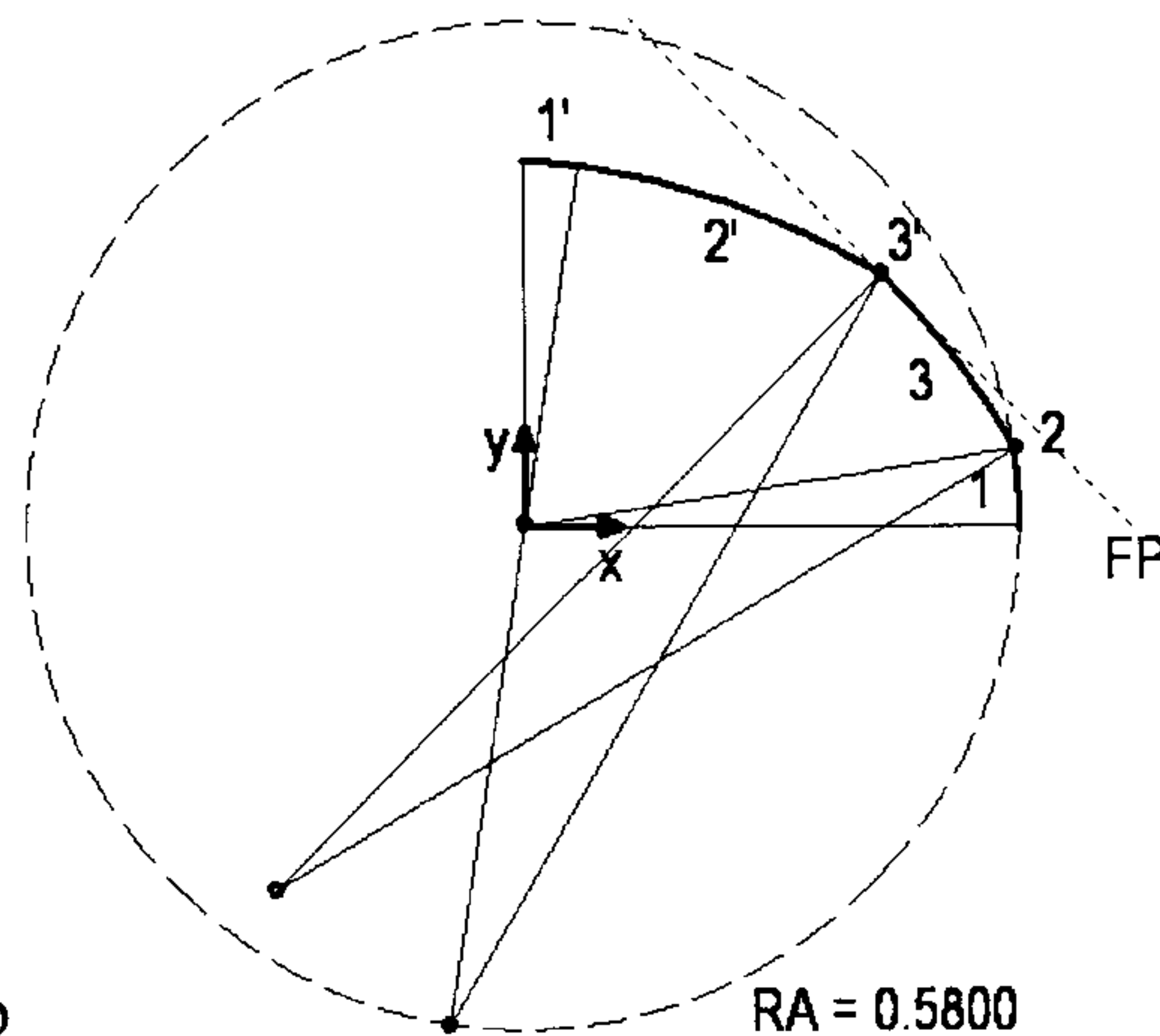


Figure 33b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5733$ |
| | $\alpha = 0.3779$ | $My = 0.0880$ |
| 3) | $R = 1.0000$ | $Mx = -0.2894$ |
| | $\alpha = 0.2552$ | $My = -0.4177$ |
| 3') | $R = 0.0000$ | $Mx = 0.4177$ |
| | $\alpha = 0.2552$ | $My = 0.2894$ |
| 2') | $R = 1.0000$ | $Mx = -0.0880$ |
| | $\alpha = 0.3779$ | $My = -0.5733$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

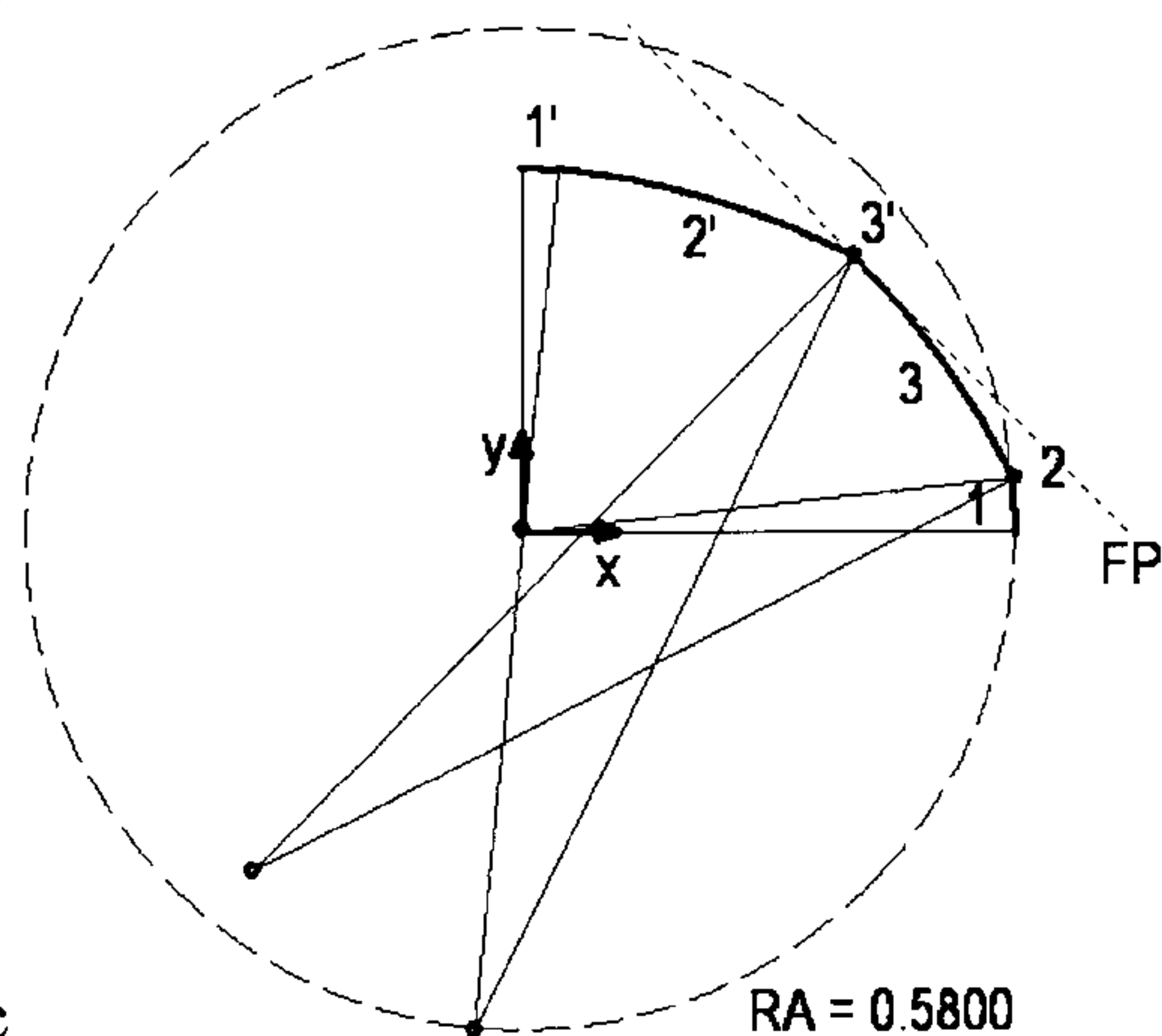


Figure 33c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5770$ |
| | $\alpha = 0.3650$ | $My = 0.0588$ |
| 3) | $R = 1.0000$ | $Mx = -0.3161$ |
| | $\alpha = 0.3188$ | $My = -0.3910$ |
| 3') | $R = 0.0000$ | $Mx = 0.3910$ |
| | $\alpha = 0.3188$ | $My = 0.3161$ |
| 2') | $R = 1.0000$ | $Mx = -0.0588$ |
| | $\alpha = 0.3650$ | $My = -0.5770$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

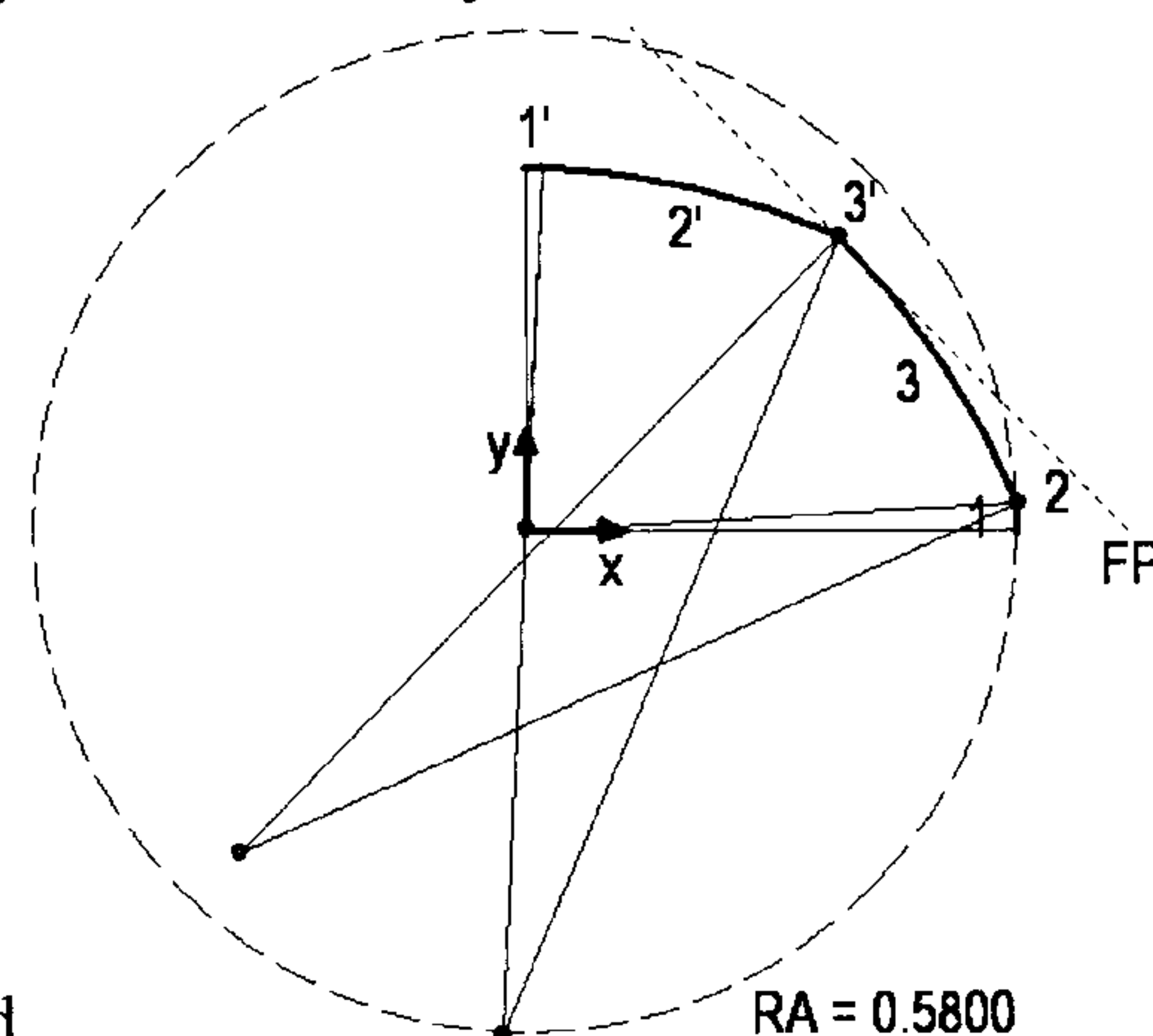


Figure 33d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5792$ |
| | $\alpha = 0.3594$ | $My = 0.0294$ |
| 3) | $R = 1.0000$ | $Mx = -0.3378$ |
| | $\alpha = 0.3752$ | $My = -0.3693$ |
| 3') | $R = 0.0000$ | $Mx = 0.3693$ |
| | $\alpha = 0.3752$ | $My = 0.3378$ |
| 2') | $R = 1.0000$ | $Mx = -0.0294$ |
| | $\alpha = 0.3594$ | $My = -0.5792$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

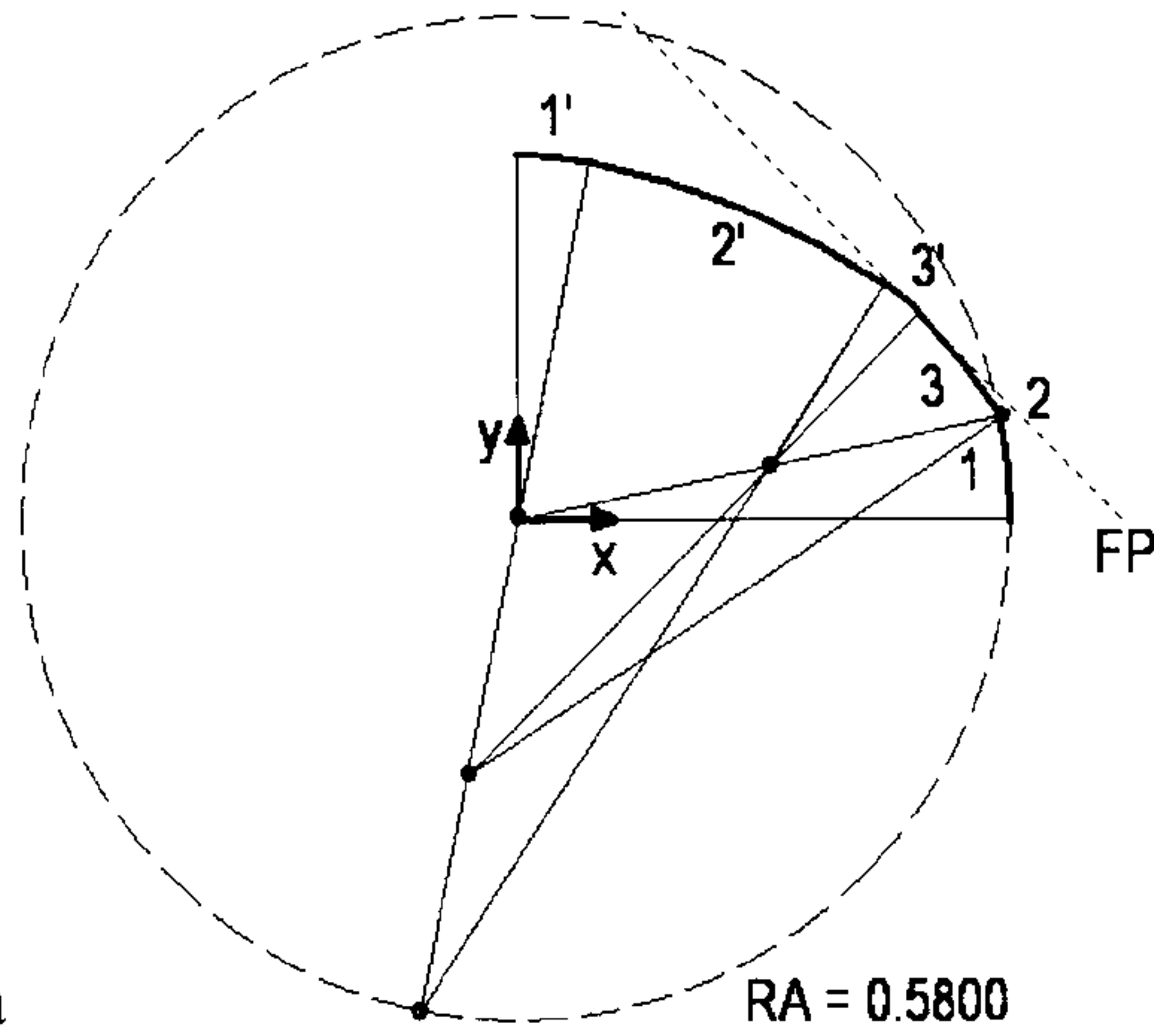


Figure 34a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5681$ |
| | $\alpha = 0.3782$ | $My = 0.1170$ |
| 3) | $R = 0.7500$ | $Mx = -0.0587$ |
| | $\alpha = 0.2041$ | $My = -0.2948$ |
| 3') | $R = 0.2500$ | $Mx = 0.2948$ |
| | $\alpha = 0.2041$ | $My = 0.0587$ |
| 2') | $R = 1.0000$ | $Mx = -0.1170$ |
| | $\alpha = 0.3782$ | $My = -0.5681$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

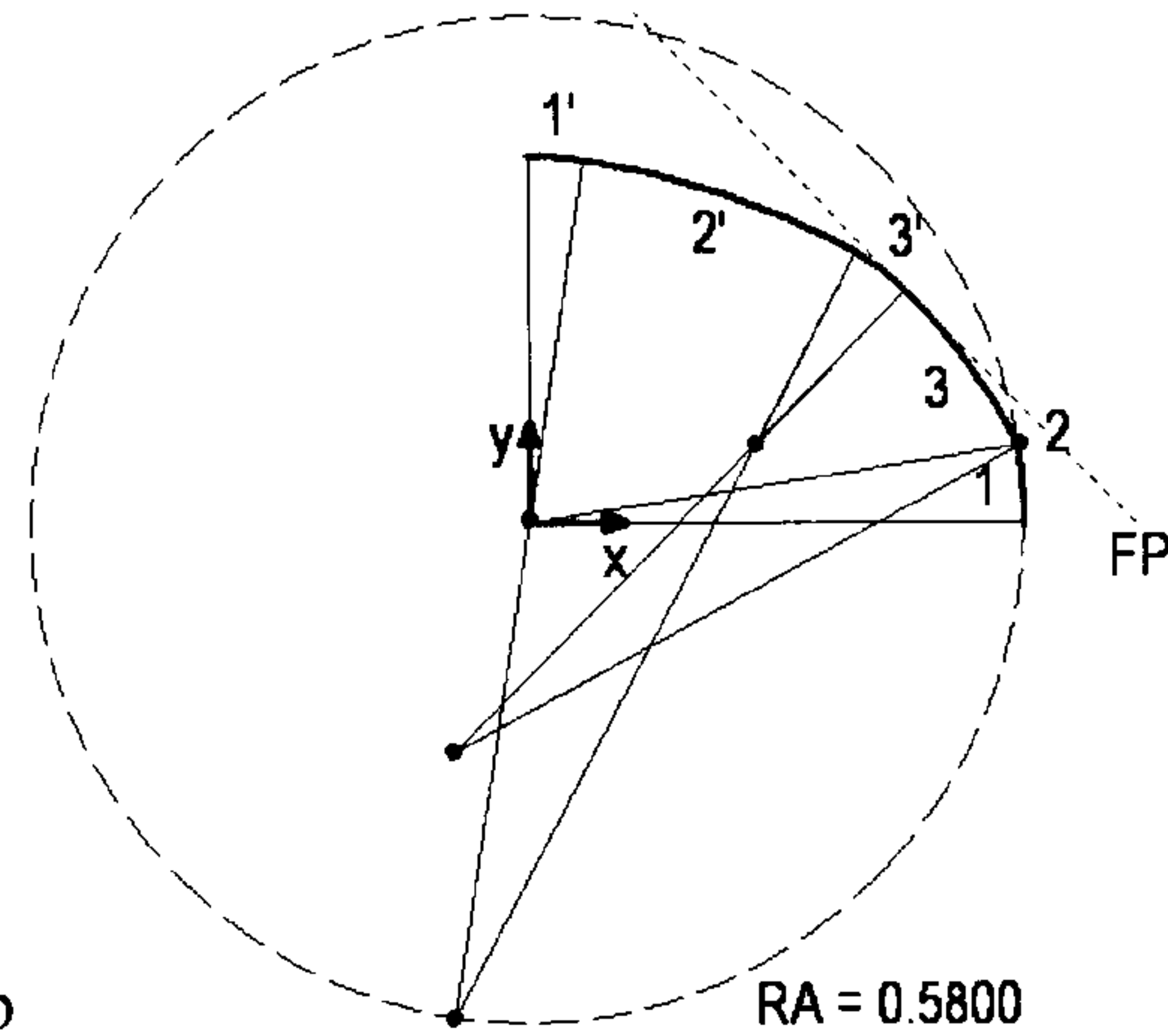


Figure 34b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5733$ |
| | $\alpha = 0.3381$ | $My = 0.0880$ |
| 3) | $R = 0.7500$ | $Mx = -0.0883$ |
| | $\alpha = 0.2949$ | $My = -0.2653$ |
| 3') | $R = 0.2500$ | $Mx = 0.2653$ |
| | $\alpha = 0.2949$ | $My = 0.0883$ |
| 2') | $R = 1.0000$ | $Mx = -0.0880$ |
| | $\alpha = 0.3381$ | $My = -0.5733$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

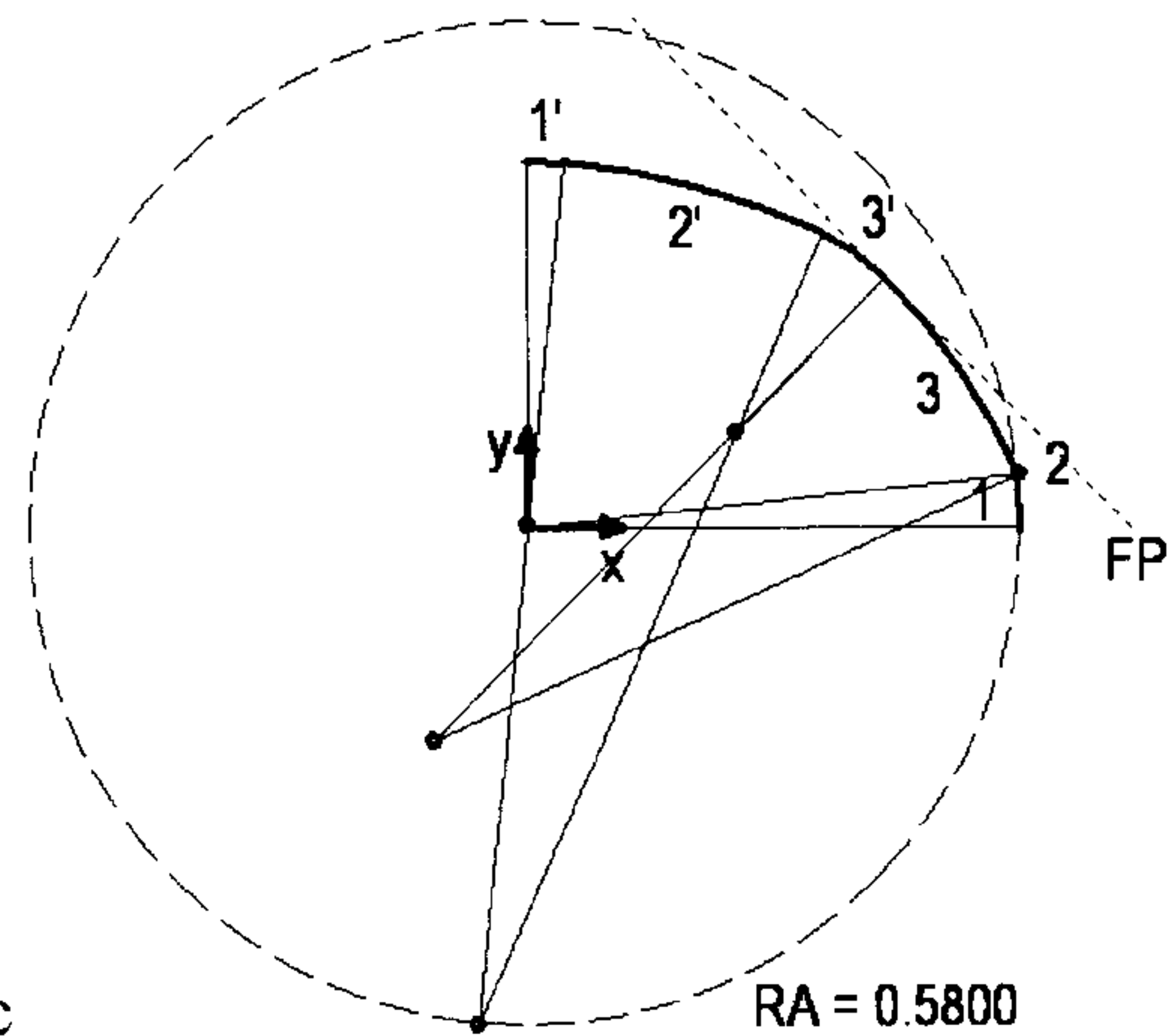


Figure 34c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5770$ |
| | $\alpha = 0.3151$ | $My = 0.0588$ |
| 3) | $R = 0.7500$ | $Mx = -0.1088$ |
| | $\alpha = 0.3687$ | $My = -0.2447$ |
| 3') | $R = 0.2500$ | $Mx = 0.2447$ |
| | $\alpha = 0.3687$ | $My = 0.1088$ |
| 2') | $R = 1.0000$ | $Mx = -0.0588$ |
| | $\alpha = 0.3151$ | $My = -0.5770$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

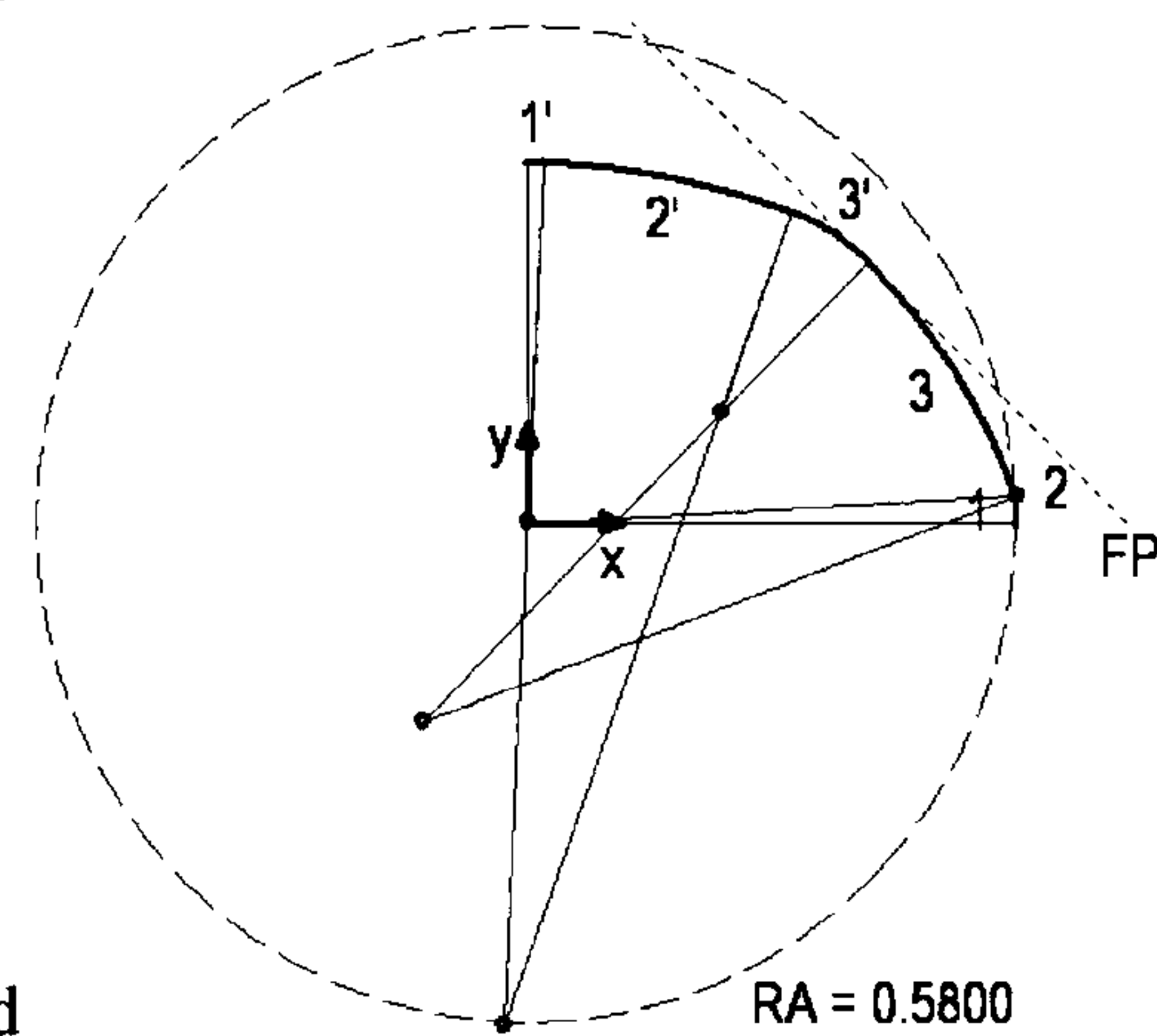


Figure 34d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5792$ |
| | $\alpha = 0.3004$ | $My = 0.0294$ |
| 3) | $R = 0.7500$ | $Mx = -0.1250$ |
| | $\alpha = 0.4342$ | $My = -0.2286$ |
| 3') | $R = 0.2500$ | $Mx = 0.2286$ |
| | $\alpha = 0.4342$ | $My = 0.1250$ |
| 2') | $R = 1.0000$ | $Mx = -0.0294$ |
| | $\alpha = 0.3004$ | $My = -0.5792$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

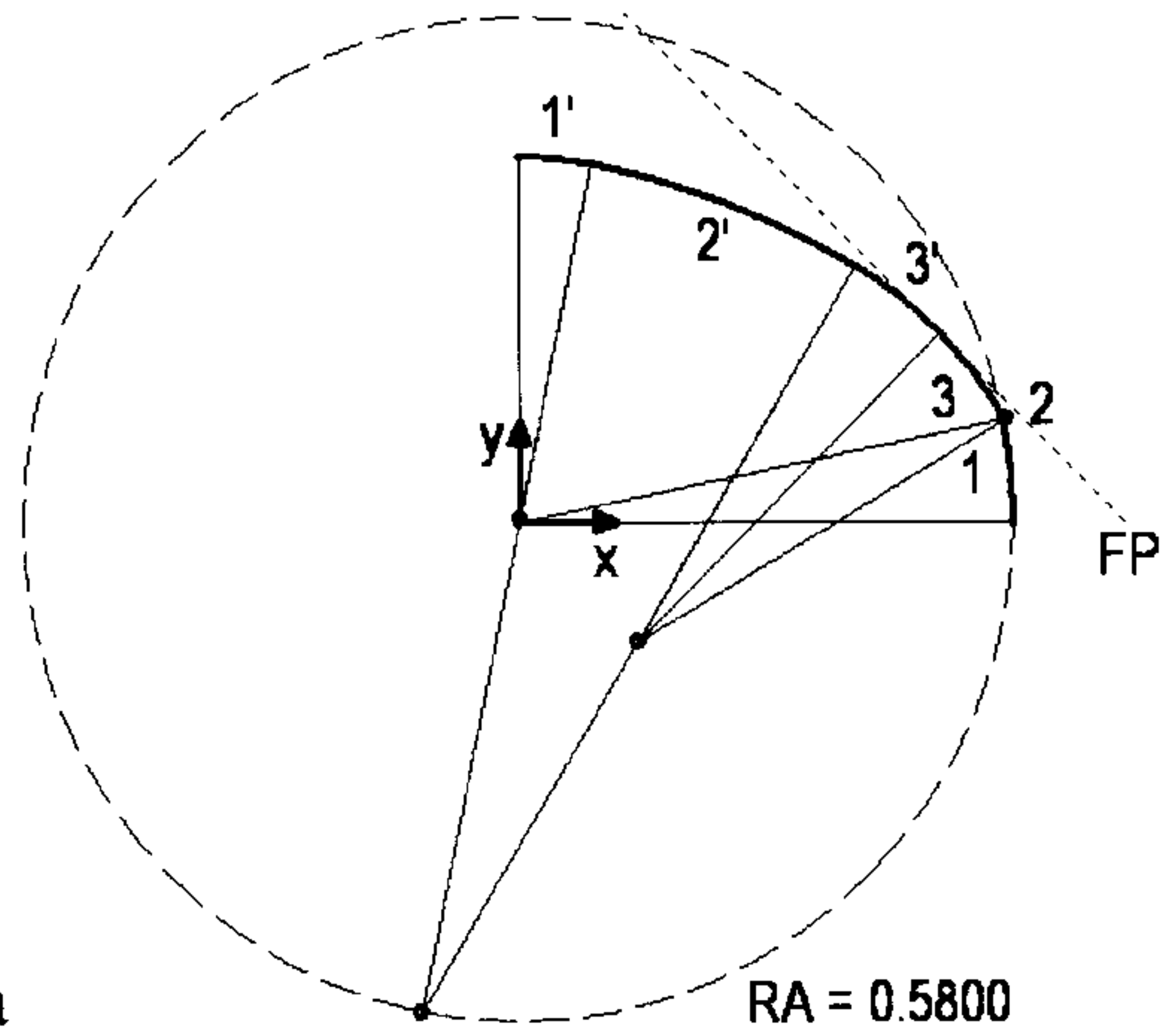


Figure 35a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5681$ |
| | $\alpha = 0.3321$ | $My = 0.1170$ |
| 3) | $R = 0.5000$ | $Mx = 0.1380$ |
| | $\alpha = 0.2502$ | $My = -0.1380$ |
| 3') | $R = 0.5000$ | $Mx = 0.1380$ |
| | $\alpha = 0.2502$ | $My = -0.1380$ |
| 2') | $R = 1.0000$ | $Mx = -0.1170$ |
| | $\alpha = 0.3321$ | $My = -0.5681$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

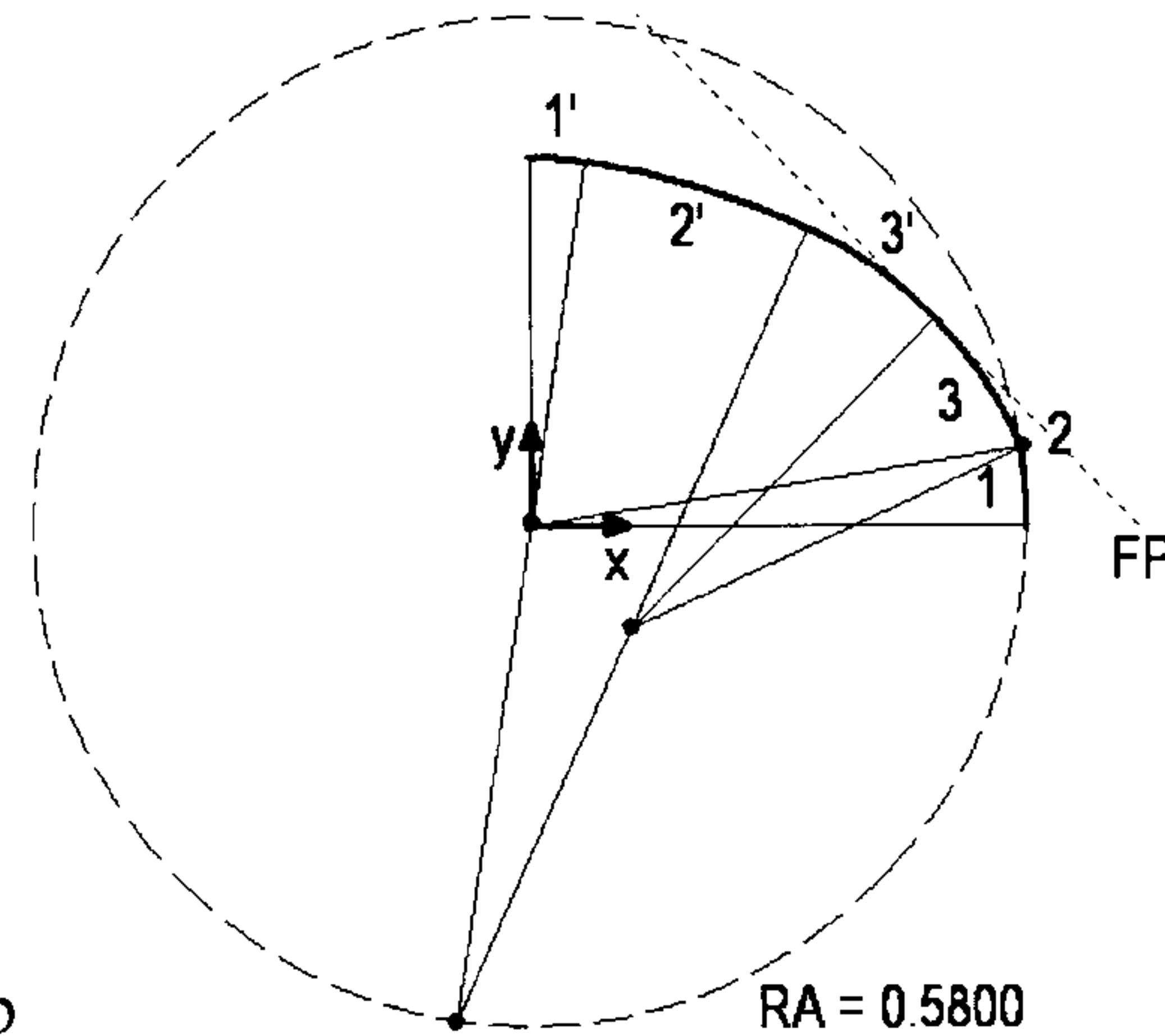


Figure 35b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5733$ |
| | $\alpha = 0.2712$ | $My = 0.0880$ |
| 3) | $R = 0.5000$ | $Mx = 0.1175$ |
| | $\alpha = 0.3619$ | $My = -0.1175$ |
| 3') | $R = 0.5000$ | $Mx = 0.1175$ |
| | $\alpha = 0.3619$ | $My = -0.1175$ |
| 2') | $R = 1.0000$ | $Mx = -0.0880$ |
| | $\alpha = 0.2712$ | $My = -0.5733$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

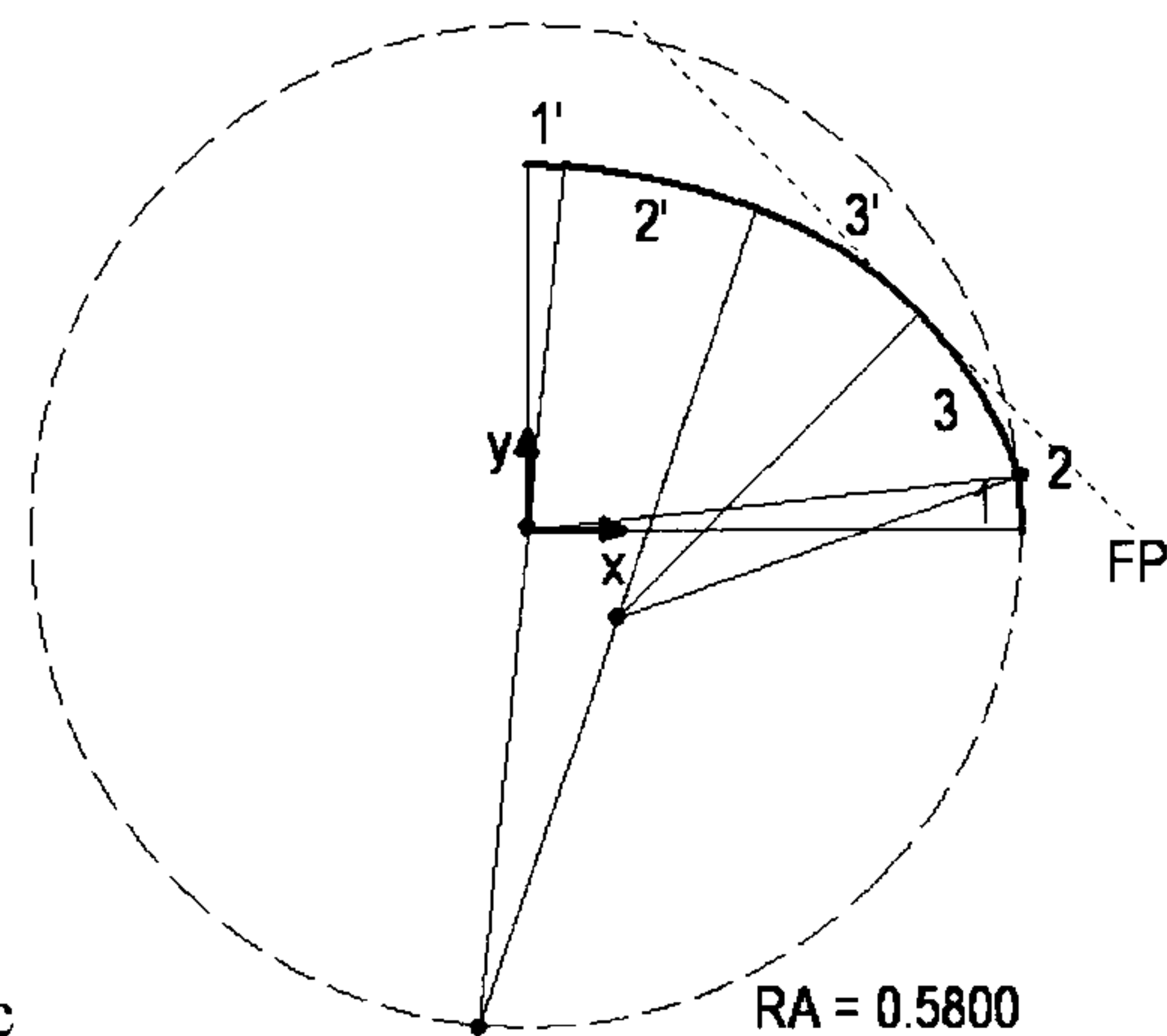


Figure 35c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5770$ |
| | $\alpha = 0.2309$ | $My = 0.0588$ |
| 3) | $R = 0.5000$ | $Mx = 0.1044$ |
| | $\alpha = 0.4529$ | $My = -0.1044$ |
| 3') | $R = 0.5000$ | $Mx = 0.1044$ |
| | $\alpha = 0.4529$ | $My = -0.1044$ |
| 2') | $R = 1.0000$ | $Mx = -0.0588$ |
| | $\alpha = 0.2309$ | $My = -0.5770$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

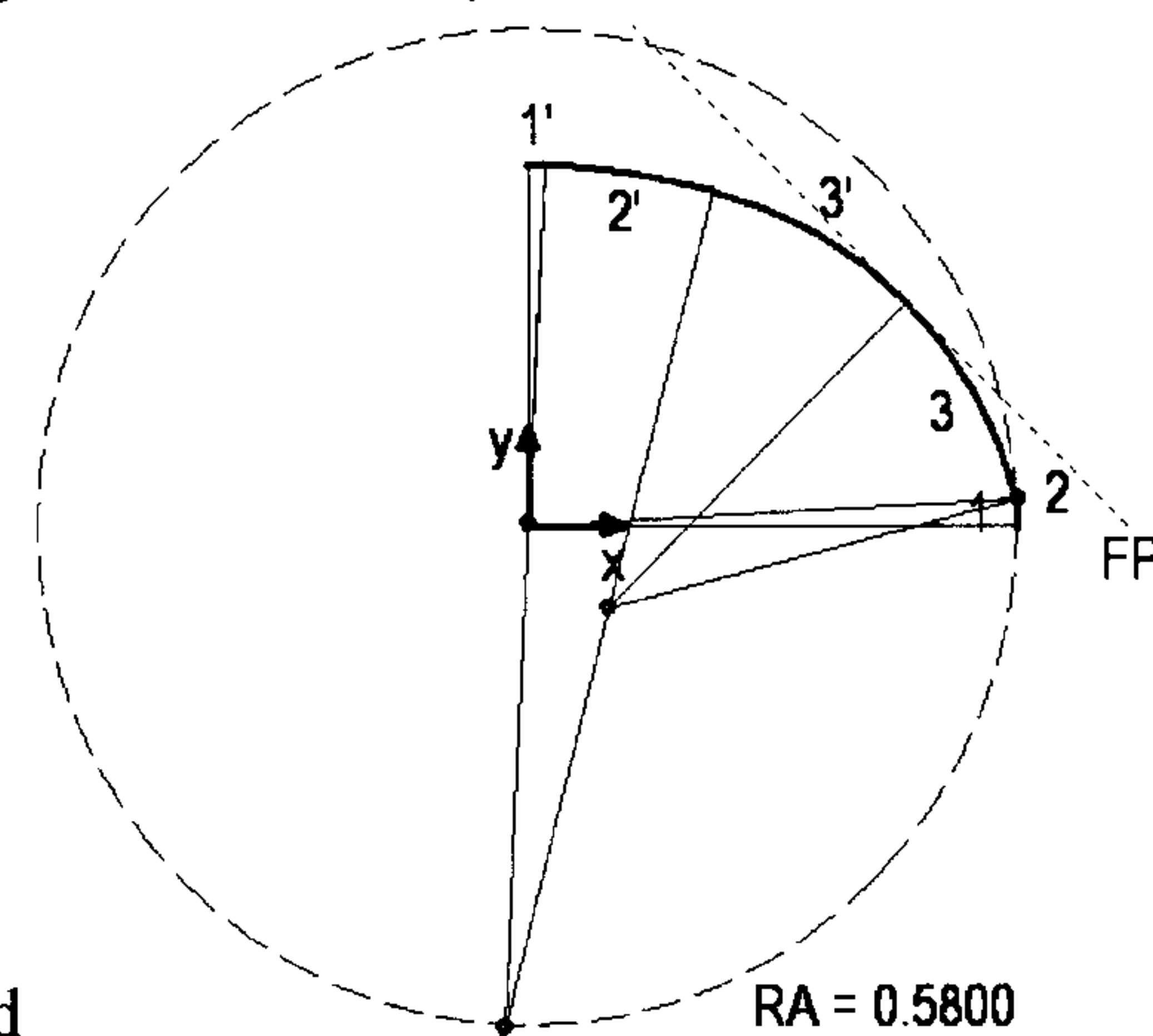


Figure 35d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.0000$ | $Mx = 0.5792$ |
| | $\alpha = 0.2007$ | $My = 0.0294$ |
| 3) | $R = 0.5000$ | $Mx = 0.0950$ |
| | $\alpha = 0.5339$ | $My = -0.0950$ |
| 3') | $R = 0.5000$ | $Mx = 0.0950$ |
| | $\alpha = 0.5339$ | $My = -0.0950$ |
| 2') | $R = 1.0000$ | $Mx = -0.0294$ |
| | $\alpha = 0.2007$ | $My = -0.5792$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

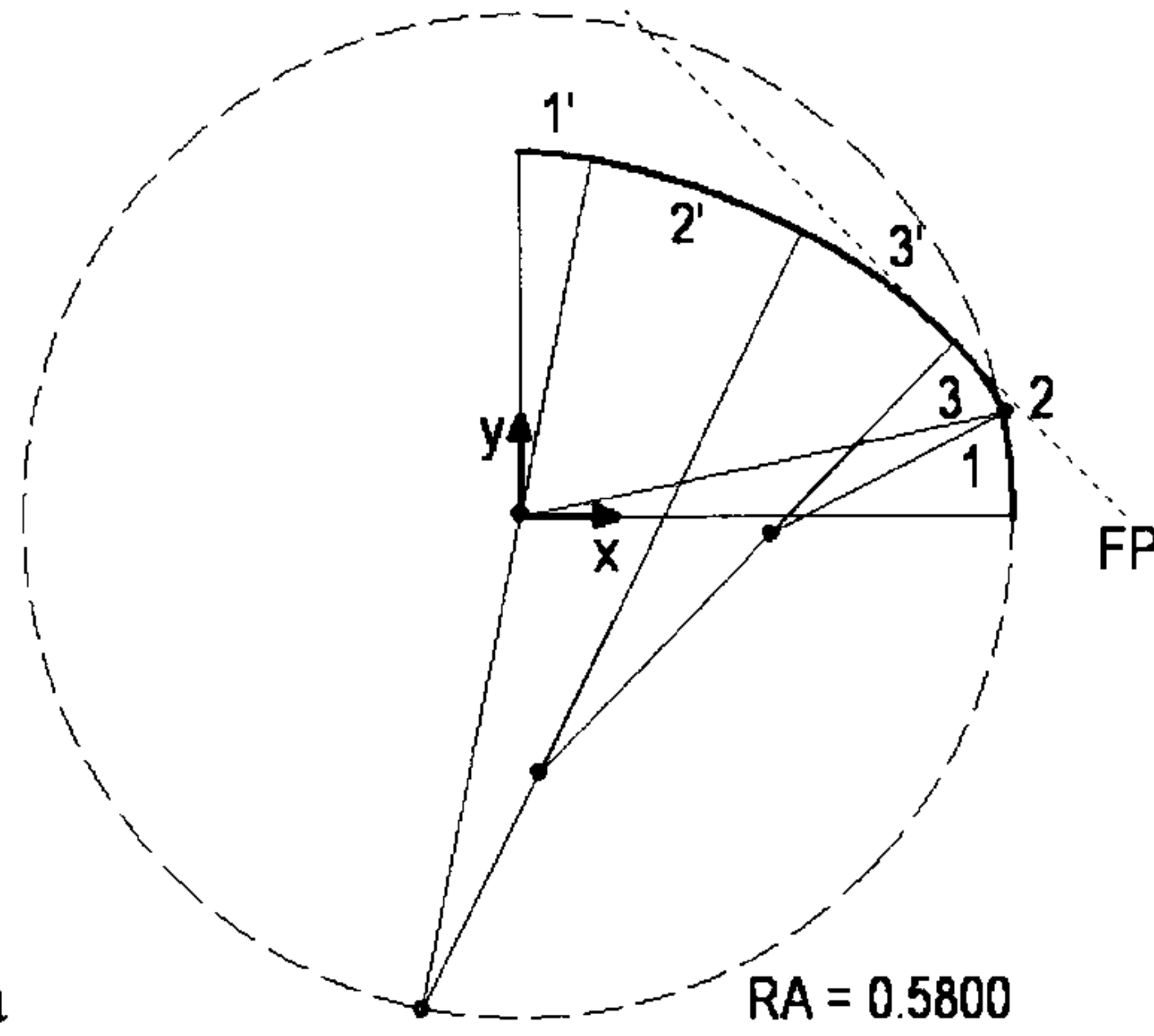


Figure 36a

1)	$R = 0.5800$	$Mx = 0.0000$
	$\alpha = 0.2032$	$My = 0.0000$
2)	$R = 0.0000$	$Mx = 0.5681$
	$\alpha = 0.2624$	$My = 0.1170$
3)	$R = 0.3069$	$Mx = 0.2939$
	$\alpha = 0.3198$	$My = -0.0207$
3')	$R = 0.6931$	$Mx = 0.0207$
	$\alpha = 0.3198$	$My = -0.2939$
2')	$R = 1.0000$	$Mx = -0.1170$
	$\alpha = 0.2624$	$My = -0.5681$
1')	$R = 0.4200$	$Mx = 0.0000$
	$\alpha = 0.2032$	$My = 0.0000$

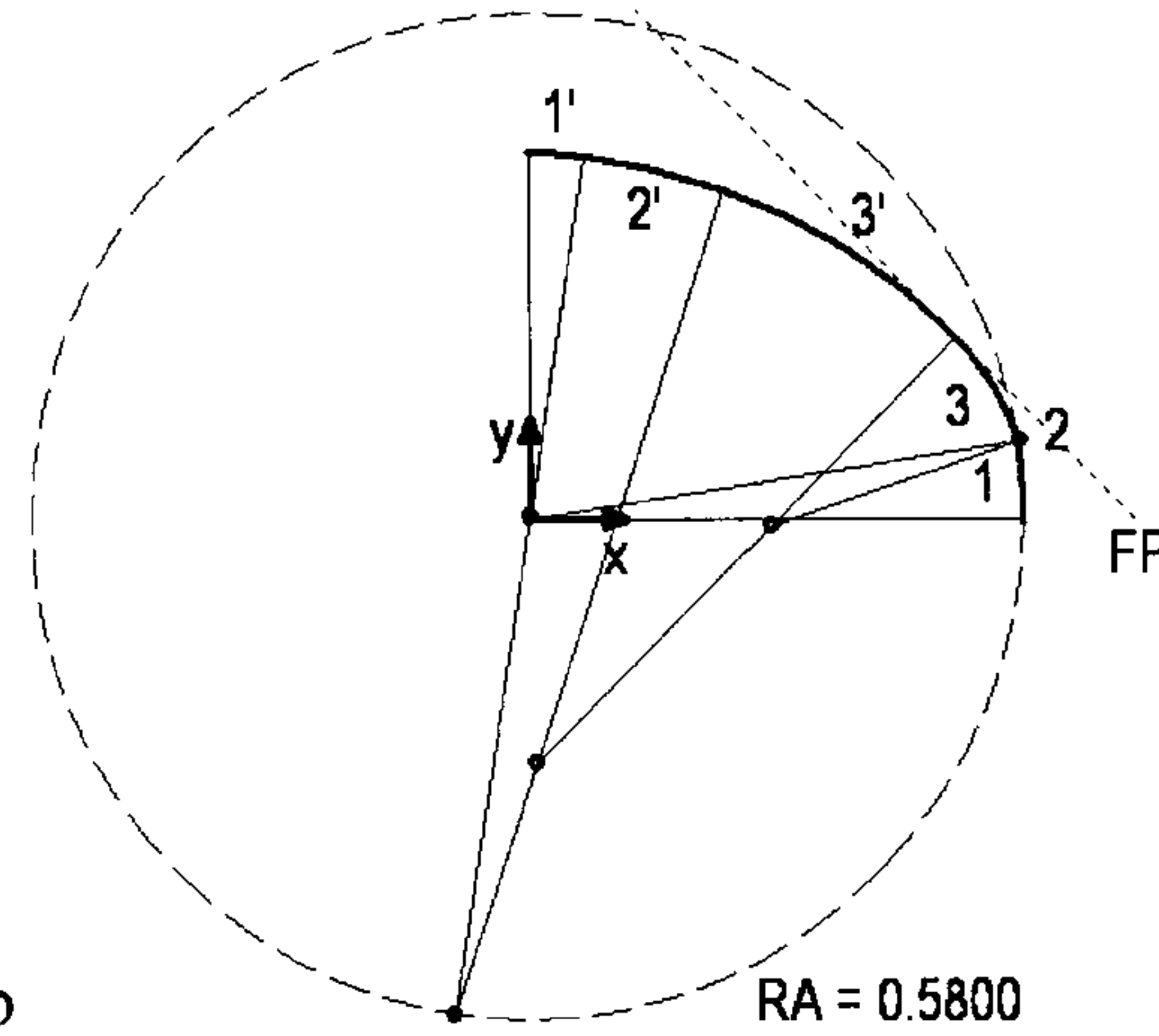


Figure 36b

1)	$R = 0.5800$	$Mx = 0.0000$
	$\alpha = 0.1524$	$My = 0.0000$
2)	$R = 0.0000$	$Mx = 0.5733$
	$\alpha = 0.1695$	$My = 0.0880$
3)	$R = 0.3069$	$Mx = 0.2822$
	$\alpha = 0.4635$	$My = -0.0090$
3')	$R = 0.6931$	$Mx = 0.0090$
	$\alpha = 0.4635$	$My = -0.2822$
2')	$R = 1.0000$	$Mx = -0.0880$
	$\alpha = 0.1695$	$My = -0.5733$
1')	$R = 0.4200$	$Mx = 0.0000$
	$\alpha = 0.1524$	$My = 0.0000$

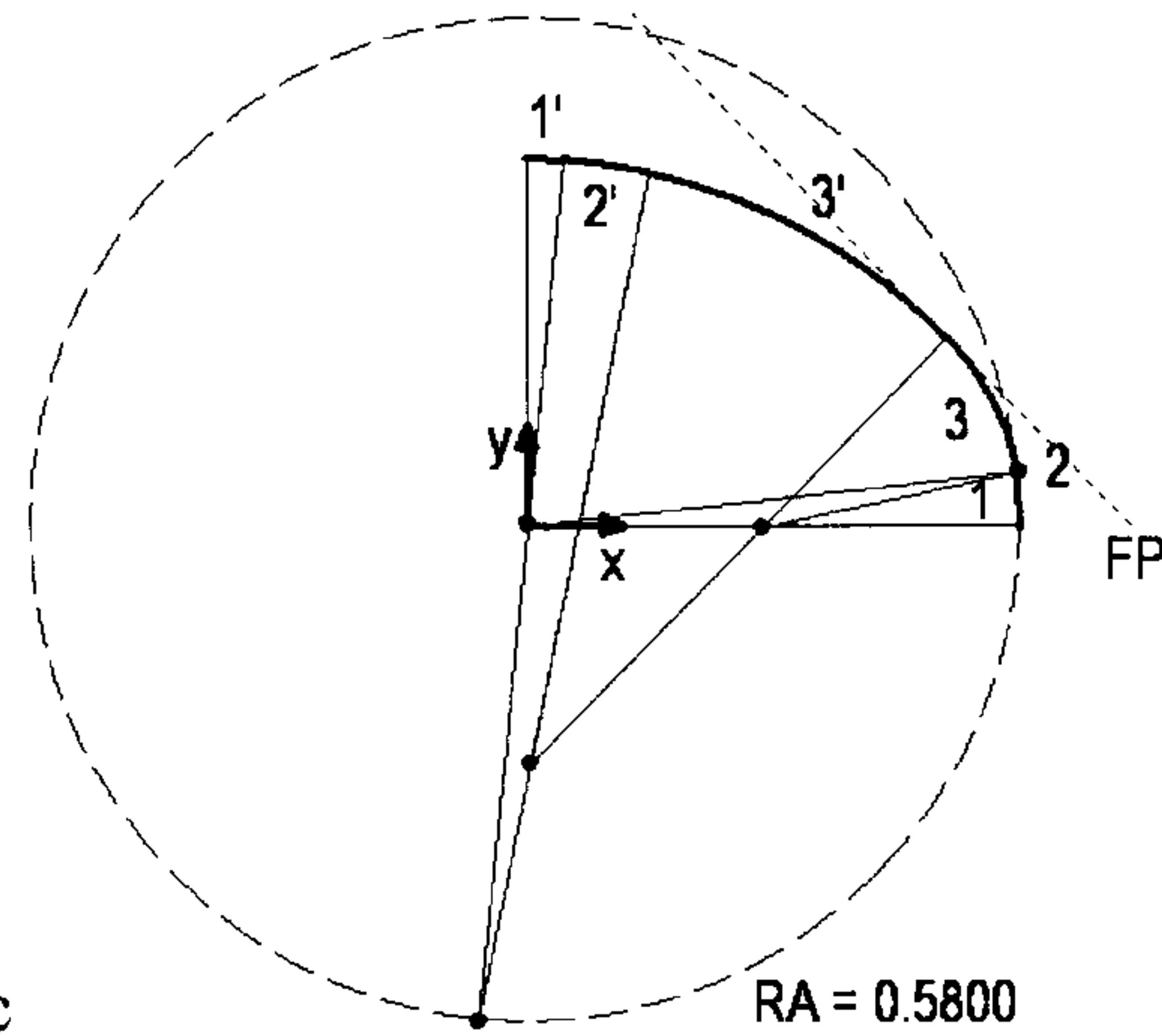


Figure 36c

1)	$R = 0.5800$	$Mx = 0.0000$
	$\alpha = 0.1016$	$My = 0.0000$
2)	$R = 0.0000$	$Mx = 0.5770$
	$\alpha = 0.1025$	$My = 0.0588$
3)	$R = 0.3069$	$Mx = 0.2765$
	$\alpha = 0.5813$	$My = -0.0034$
3')	$R = 0.6931$	$Mx = 0.0034$
	$\alpha = 0.5813$	$My = -0.2765$
2')	$R = 1.0000$	$Mx = -0.0588$
	$\alpha = 0.1025$	$My = -0.5770$
1')	$R = 0.4200$	$Mx = 0.0000$
	$\alpha = 0.1016$	$My = 0.0000$

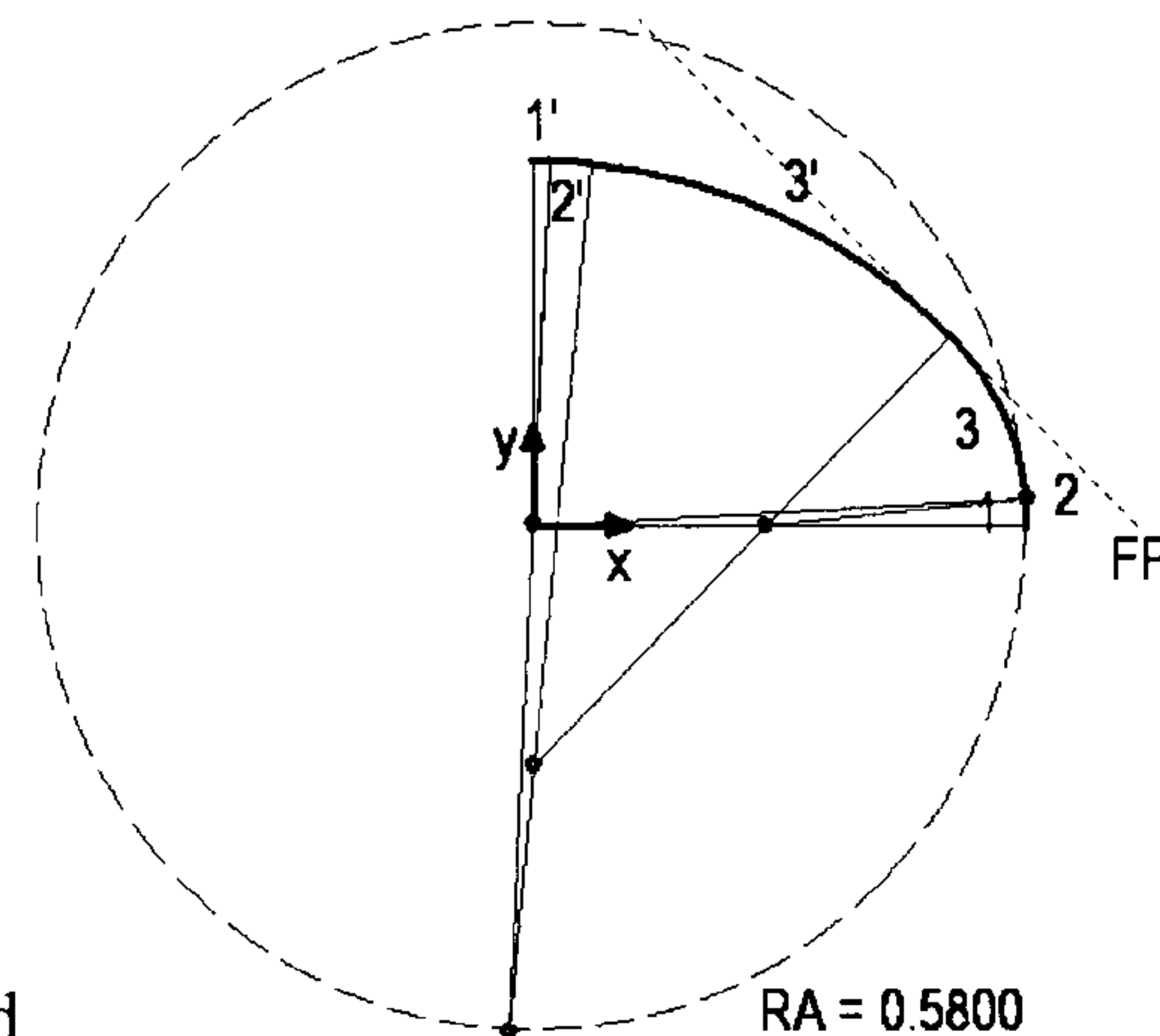


Figure 36d

1)	$R = 0.5800$	$Mx = 0.0000$
	$\alpha = 0.0508$	$My = 0.0000$
2)	$R = 0.0000$	$Mx = 0.5792$
	$\alpha = 0.0477$	$My = 0.0294$
3)	$R = 0.3069$	$Mx = 0.2739$
	$\alpha = 0.6869$	$My = -0.0007$
3')	$R = 0.6931$	$Mx = 0.0007$
	$\alpha = 0.6869$	$My = -0.2739$
2')	$R = 1.0000$	$Mx = -0.0294$
	$\alpha = 0.0477$	$My = -0.5792$
1')	$R = 0.4200$	$Mx = 0.0000$
	$\alpha = 0.0508$	$My = 0.0000$

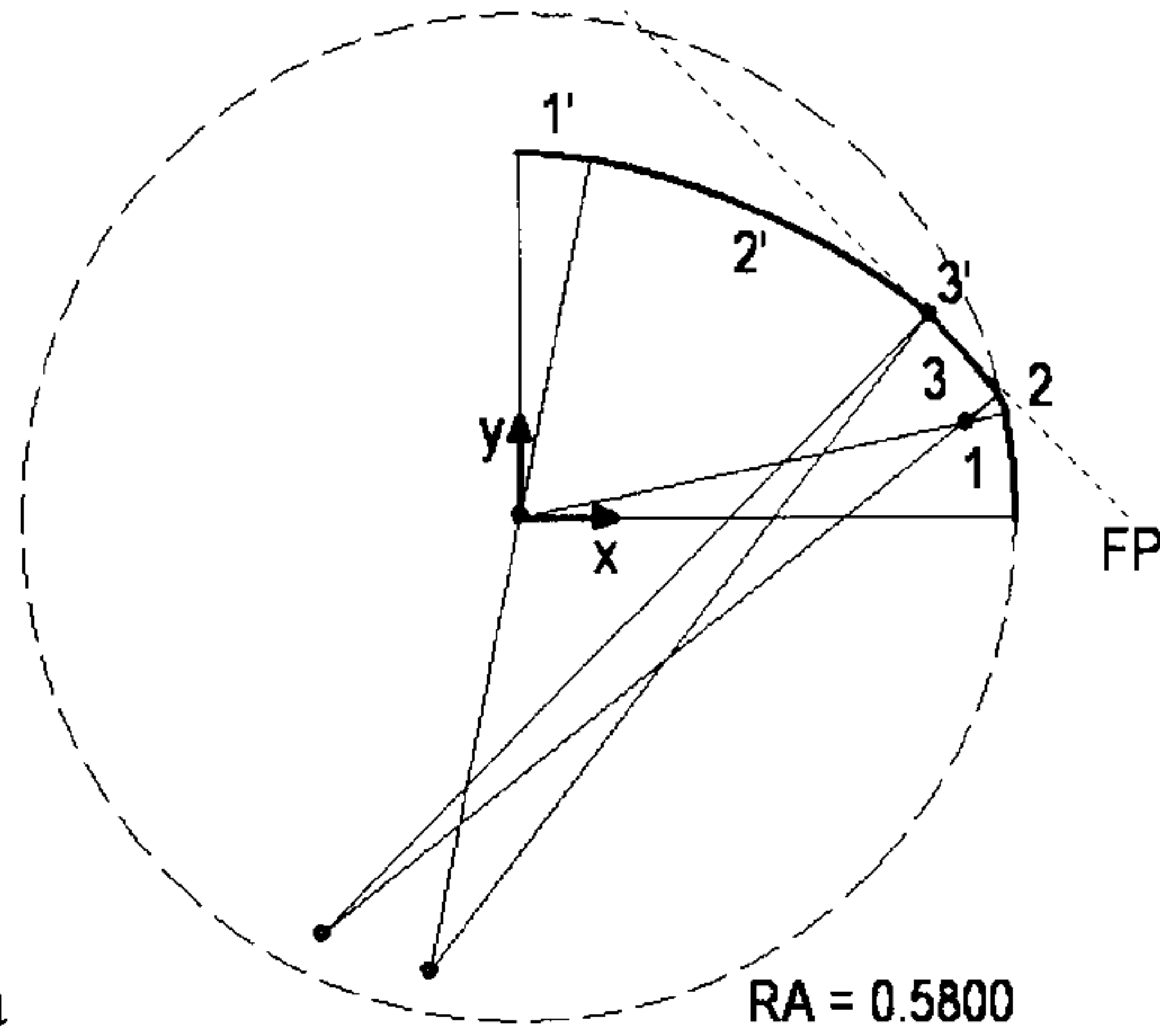


Figure 37a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0500$ | $Mx = 0.5191$ |
| | $\alpha = 0.4580$ | $My = 0.1069$ |
| 3) | $R = 1.0000$ | $Mx = -0.2307$ |
| | $\alpha = 0.1243$ | $My = -0.4764$ |
| 3') | $R = 0.0000$ | $Mx = 0.4764$ |
| | $\alpha = 0.1243$ | $My = 0.2307$ |
| 2') | $R = 0.9500$ | $Mx = -0.1069$ |
| | $\alpha = 0.4580$ | $My = -0.5191$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

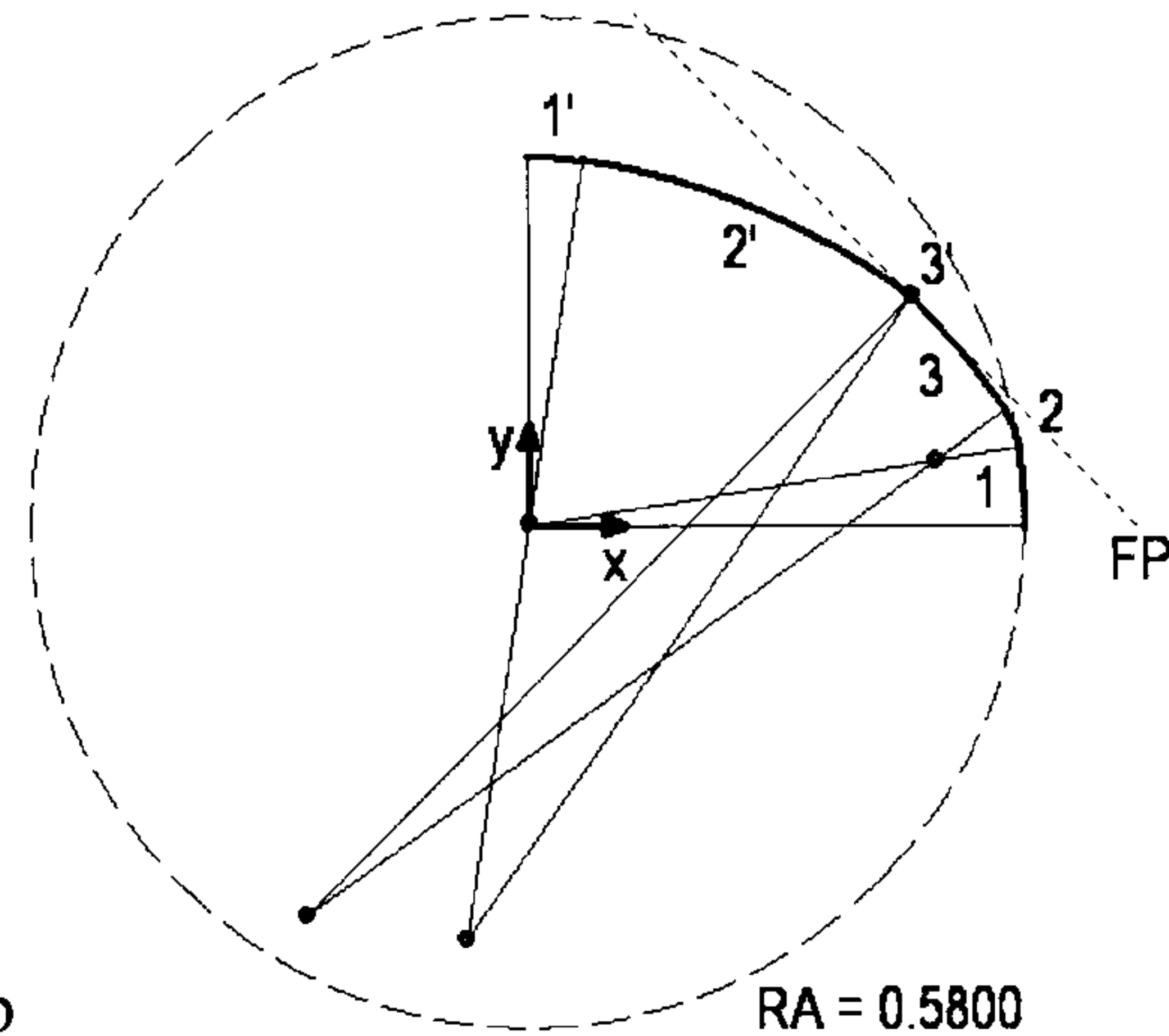


Figure 37b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.1000$ | $Mx = 0.4744$ |
| | $\alpha = 0.4628$ | $My = 0.0729$ |
| 3) | $R = 1.0000$ | $Mx = -0.2605$ |
| | $\alpha = 0.1702$ | $My = -0.4465$ |
| 3') | $R = 0.0000$ | $Mx = 0.4465$ |
| | $\alpha = 0.1702$ | $My = 0.2605$ |
| 2') | $R = 0.9000$ | $Mx = -0.0729$ |
| | $\alpha = 0.4628$ | $My = -0.4744$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

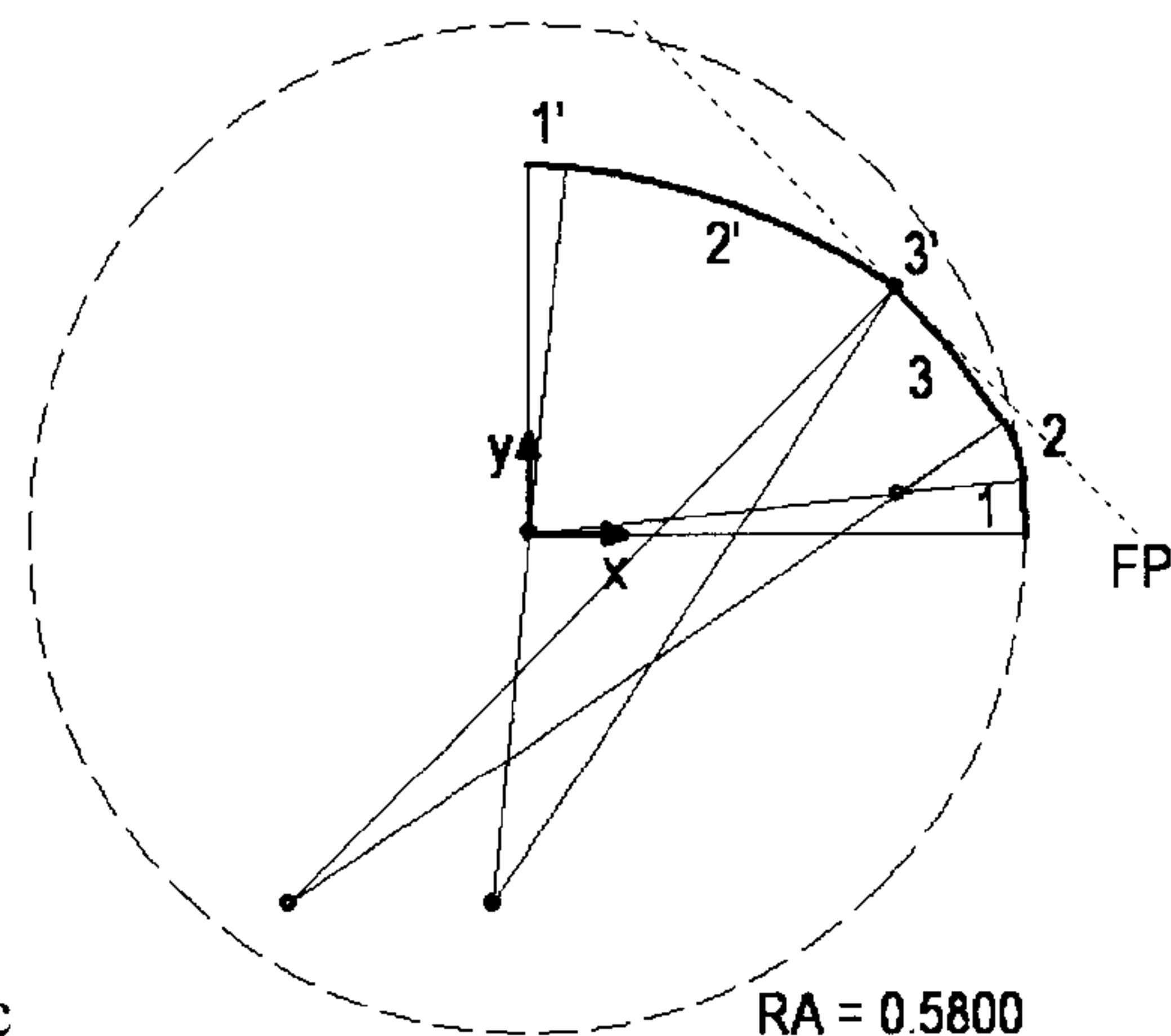


Figure 37c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.1500$ | $Mx = 0.4278$ |
| | $\alpha = 0.4854$ | $My = 0.0436$ |
| 3) | $R = 1.0000$ | $Mx = -0.2799$ |
| | $\alpha = 0.1984$ | $My = -0.4272$ |
| 3') | $R = 0.0000$ | $Mx = 0.4272$ |
| | $\alpha = 0.1984$ | $My = 0.2799$ |
| 2') | $R = 0.8500$ | $Mx = -0.0436$ |
| | $\alpha = 0.4854$ | $My = -0.4278$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

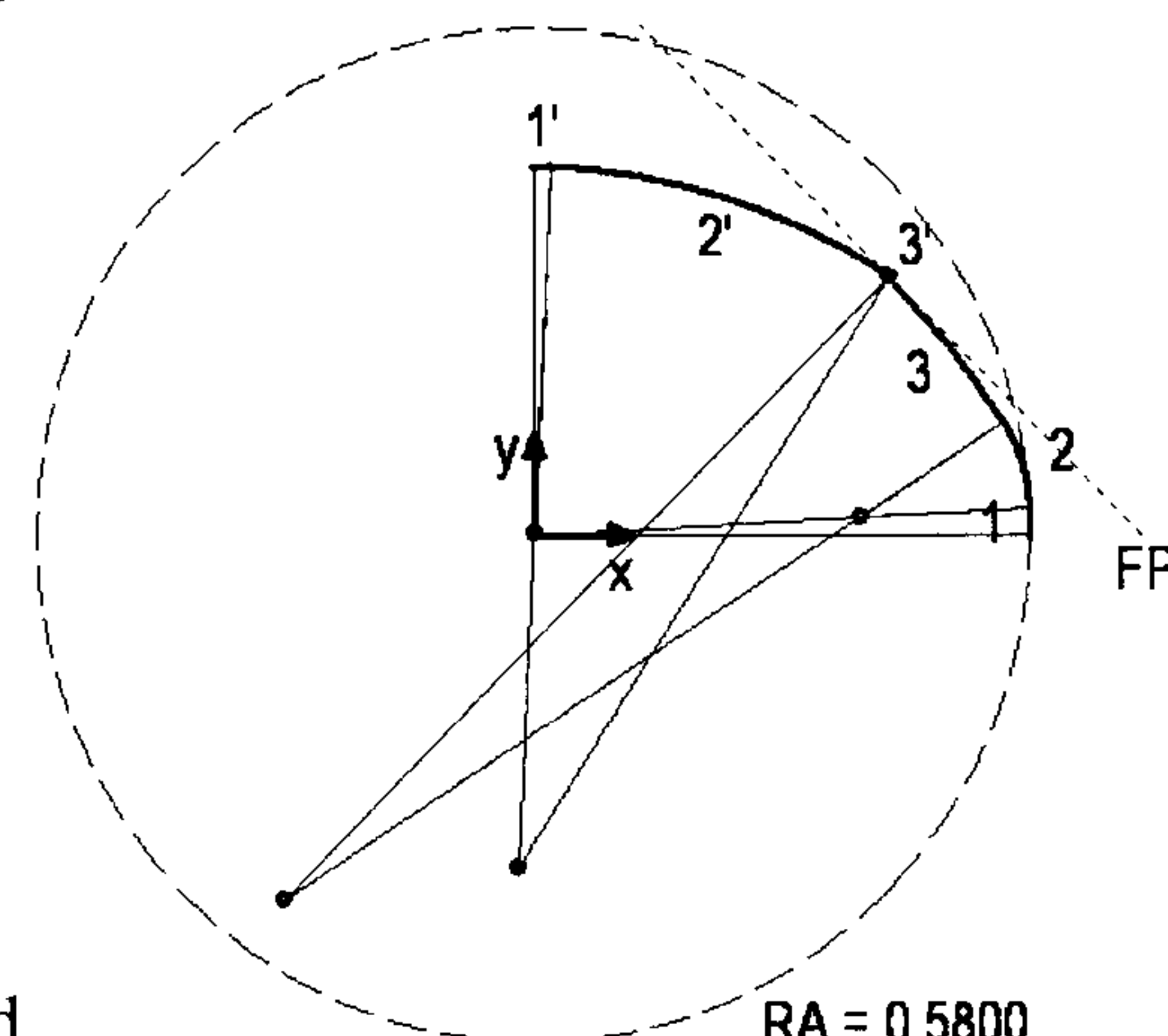


Figure 37d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.2000$ | $Mx = 0.3795$ |
| | $\alpha = 0.5220$ | $My = 0.0193$ |
| 3) | $R = 1.0000$ | $Mx = -0.2928$ |
| | $\alpha = 0.2126$ | $My = -0.4143$ |
| 3') | $R = 0.0000$ | $Mx = 0.4143$ |
| | $\alpha = 0.2126$ | $My = 0.2928$ |
| 2') | $R = 0.8000$ | $Mx = -0.0193$ |
| | $\alpha = 0.5220$ | $My = -0.3795$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

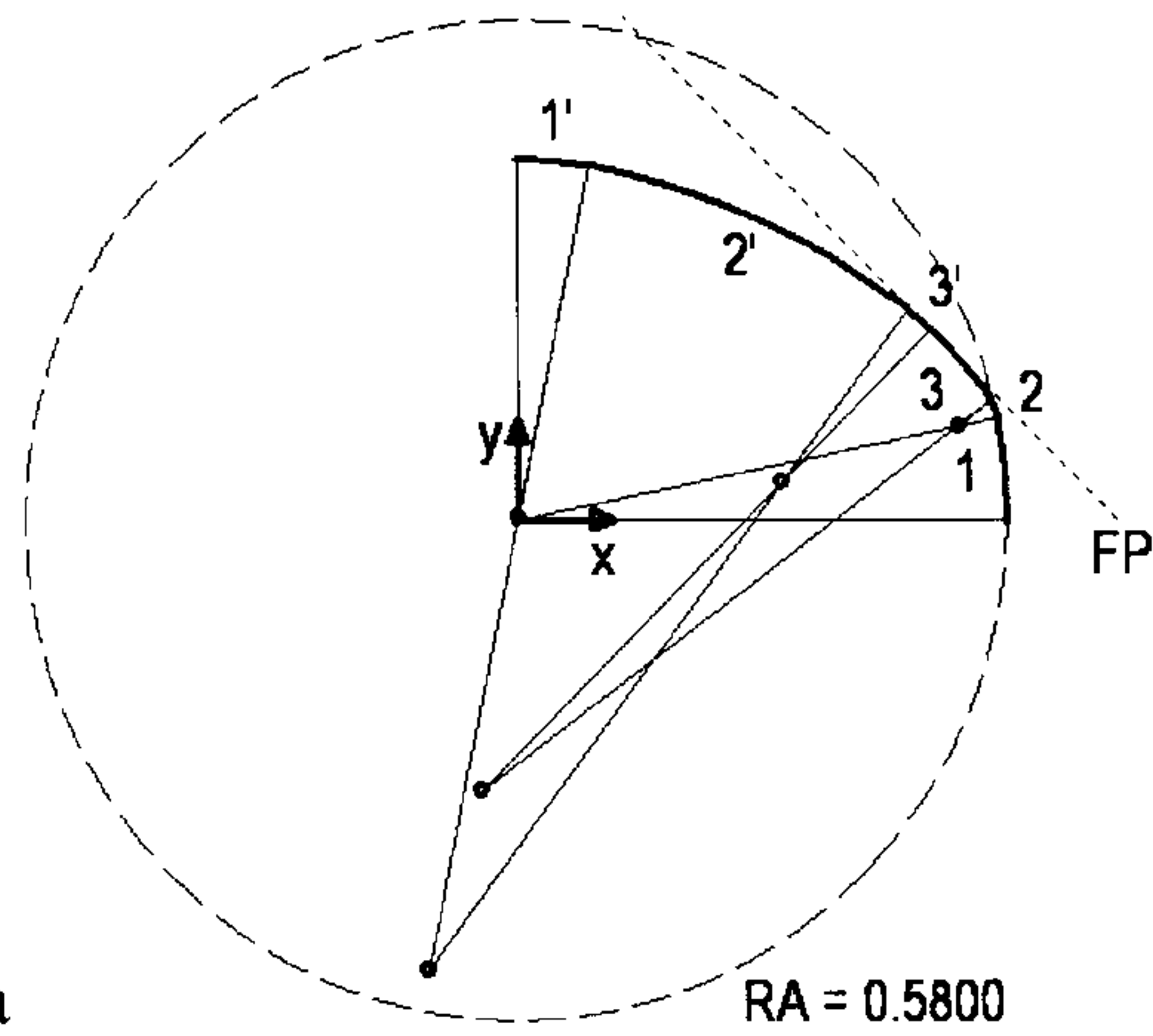


Figure 38a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0500$ | $Mx = 0.5191$ |
| | $\alpha = 0.4374$ | $My = 0.1069$ |
| 3) | $R = 0.7500$ | $Mx = -0.0421$ |
| | $\alpha = 0.1448$ | $My = -0.3114$ |
| 3') | $R = 0.2500$ | $Mx = 0.3114$ |
| | $\alpha = 0.1448$ | $My = 0.0421$ |
| 2') | $R = 0.9500$ | $Mx = -0.1069$ |
| | $\alpha = 0.4374$ | $My = -0.5191$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

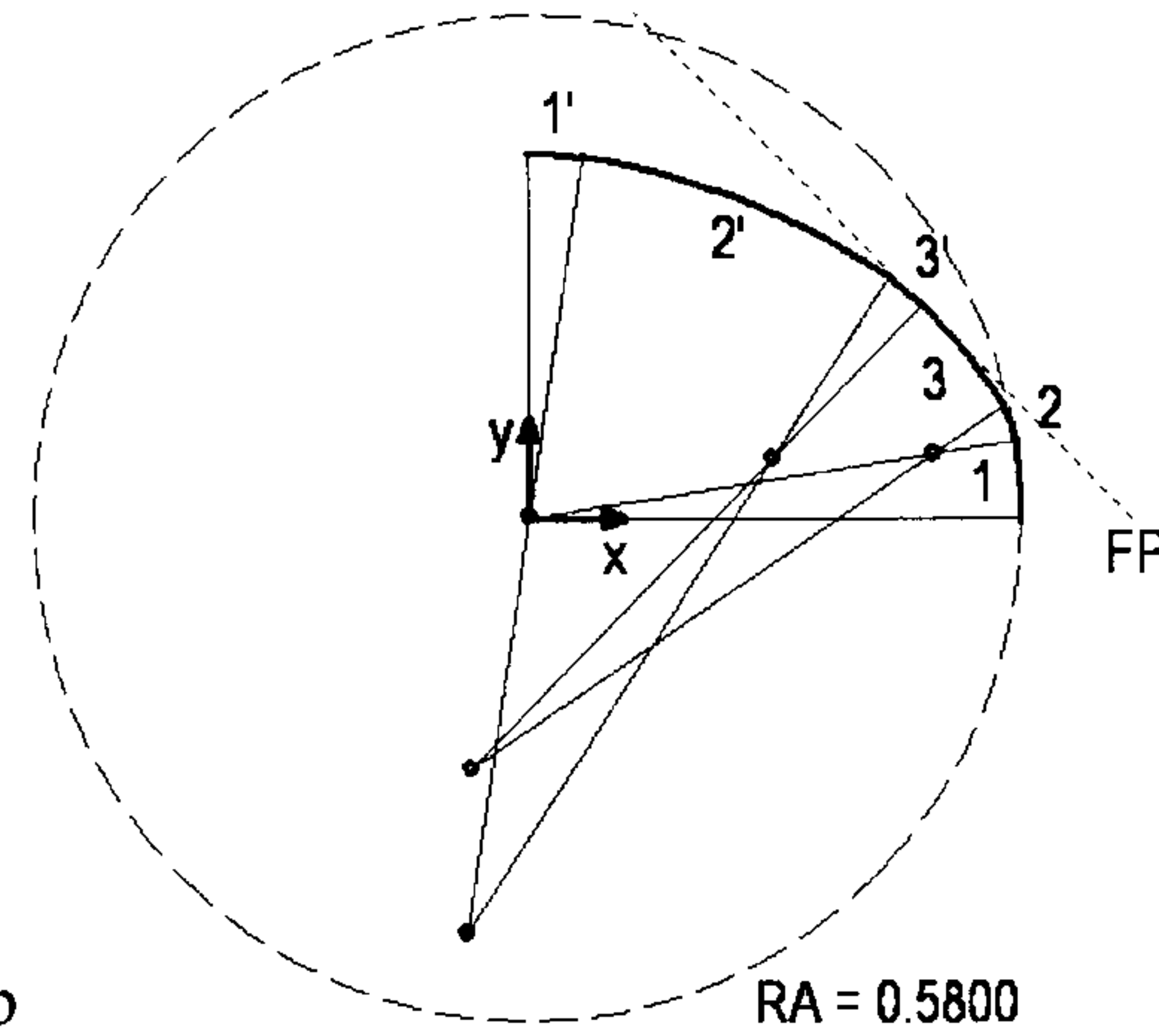


Figure 38b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.1000$ | $Mx = 0.4744$ |
| | $\alpha = 0.4327$ | $My = 0.0729$ |
| 3) | $R = 0.7500$ | $Mx = -0.0675$ |
| | $\alpha = 0.2004$ | $My = -0.2861$ |
| 3') | $R = 0.2500$ | $Mx = 0.2861$ |
| | $\alpha = 0.2004$ | $My = 0.0675$ |
| 2') | $R = 0.9000$ | $Mx = -0.0729$ |
| | $\alpha = 0.4327$ | $My = -0.4744$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

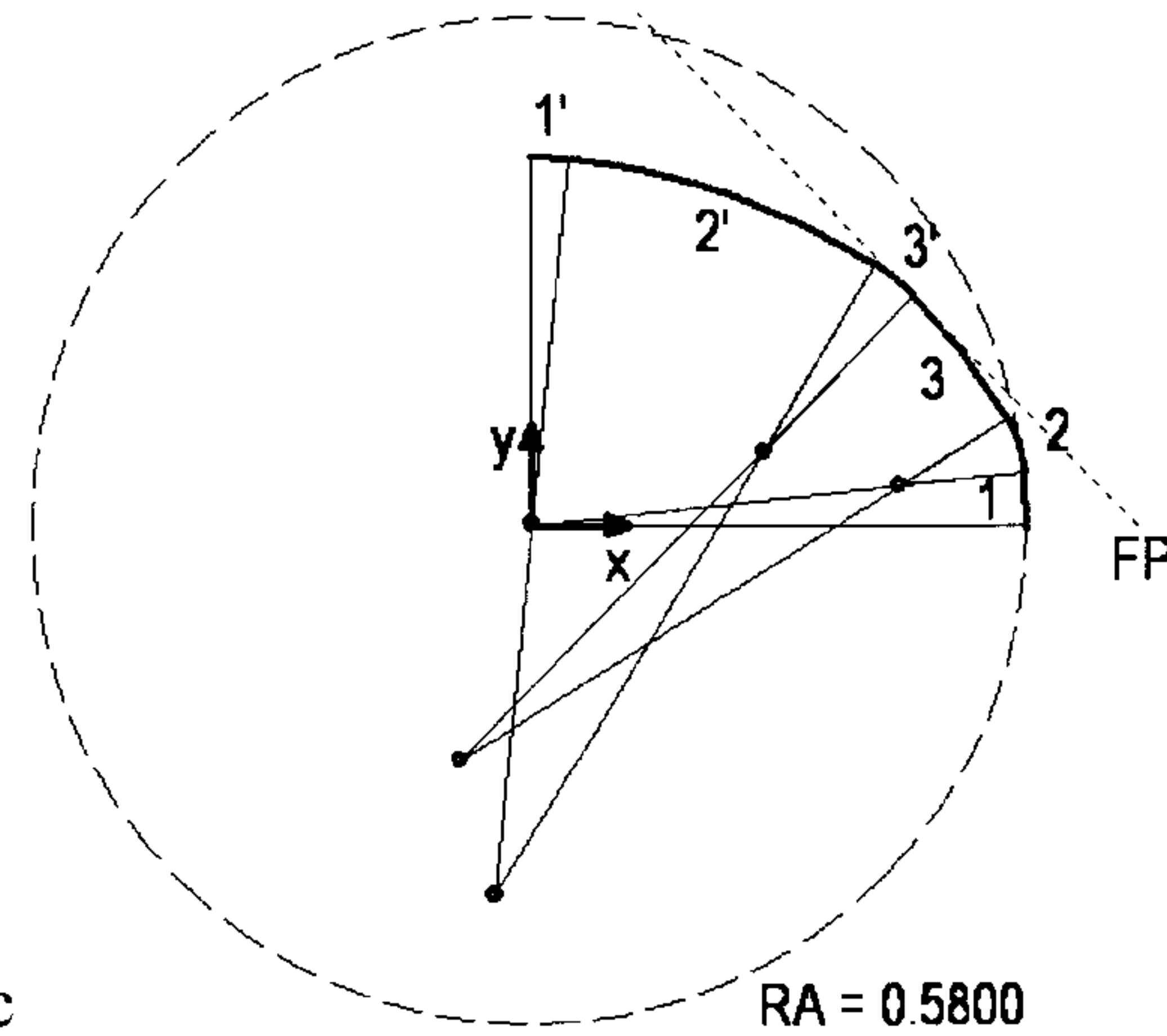


Figure 38c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.1500$ | $Mx = 0.4278$ |
| | $\alpha = 0.4475$ | $My = 0.0436$ |
| 3) | $R = 0.7500$ | $Mx = -0.0840$ |
| | $\alpha = 0.2363$ | $My = -0.2695$ |
| 3') | $R = 0.2500$ | $Mx = 0.2695$ |
| | $\alpha = 0.2363$ | $My = 0.0840$ |
| 2') | $R = 0.8500$ | $Mx = -0.0436$ |
| | $\alpha = 0.4475$ | $My = -0.4278$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

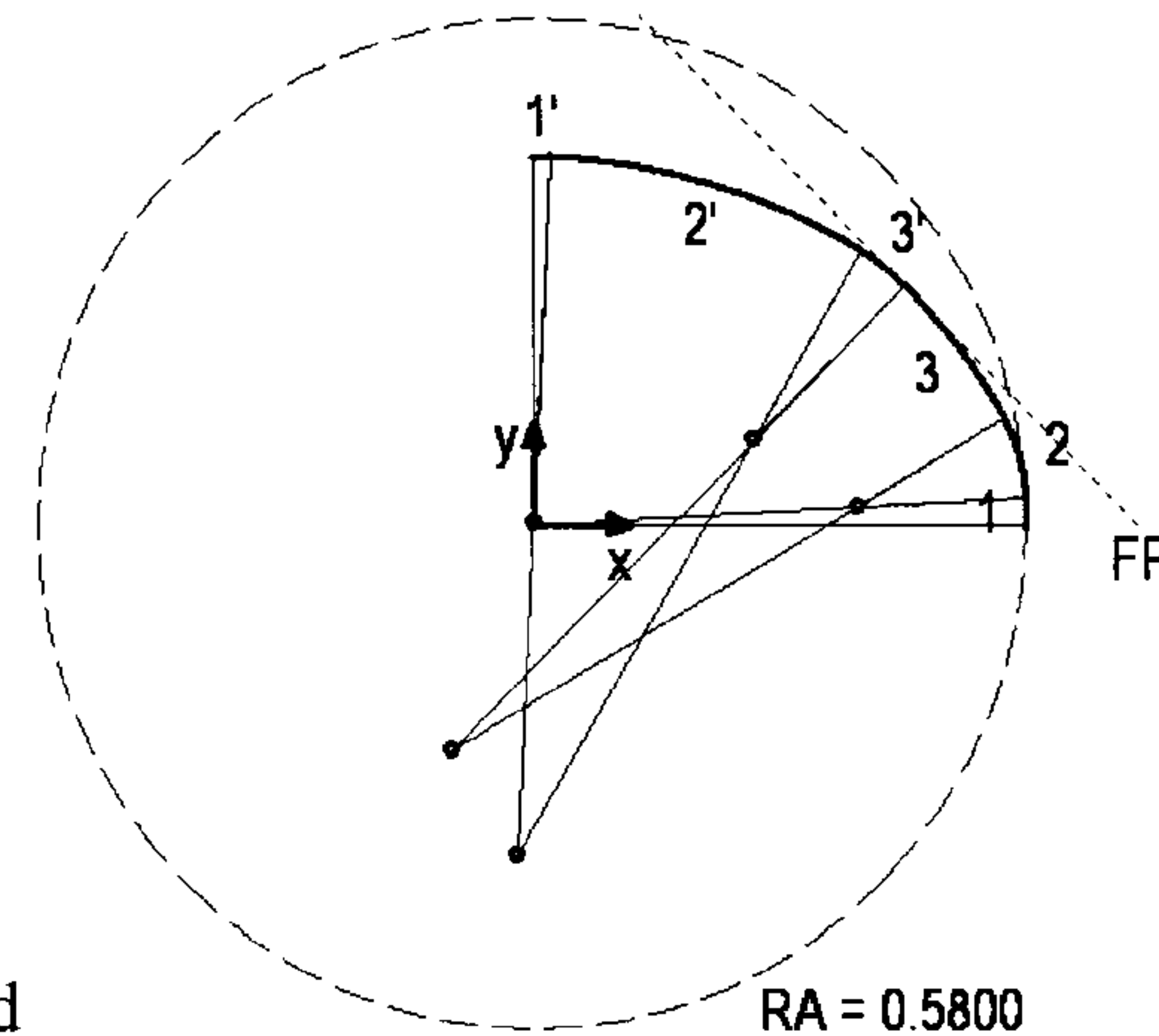


Figure 38d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.2000$ | $Mx = 0.3795$ |
| | $\alpha = 0.4780$ | $My = 0.0193$ |
| 3) | $R = 0.7500$ | $Mx = -0.0954$ |
| | $\alpha = 0.2566$ | $My = -0.2582$ |
| 3') | $R = 0.2500$ | $Mx = 0.2582$ |
| | $\alpha = 0.2566$ | $My = 0.0954$ |
| 2') | $R = 0.8000$ | $Mx = -0.0193$ |
| | $\alpha = 0.4780$ | $My = -0.3795$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

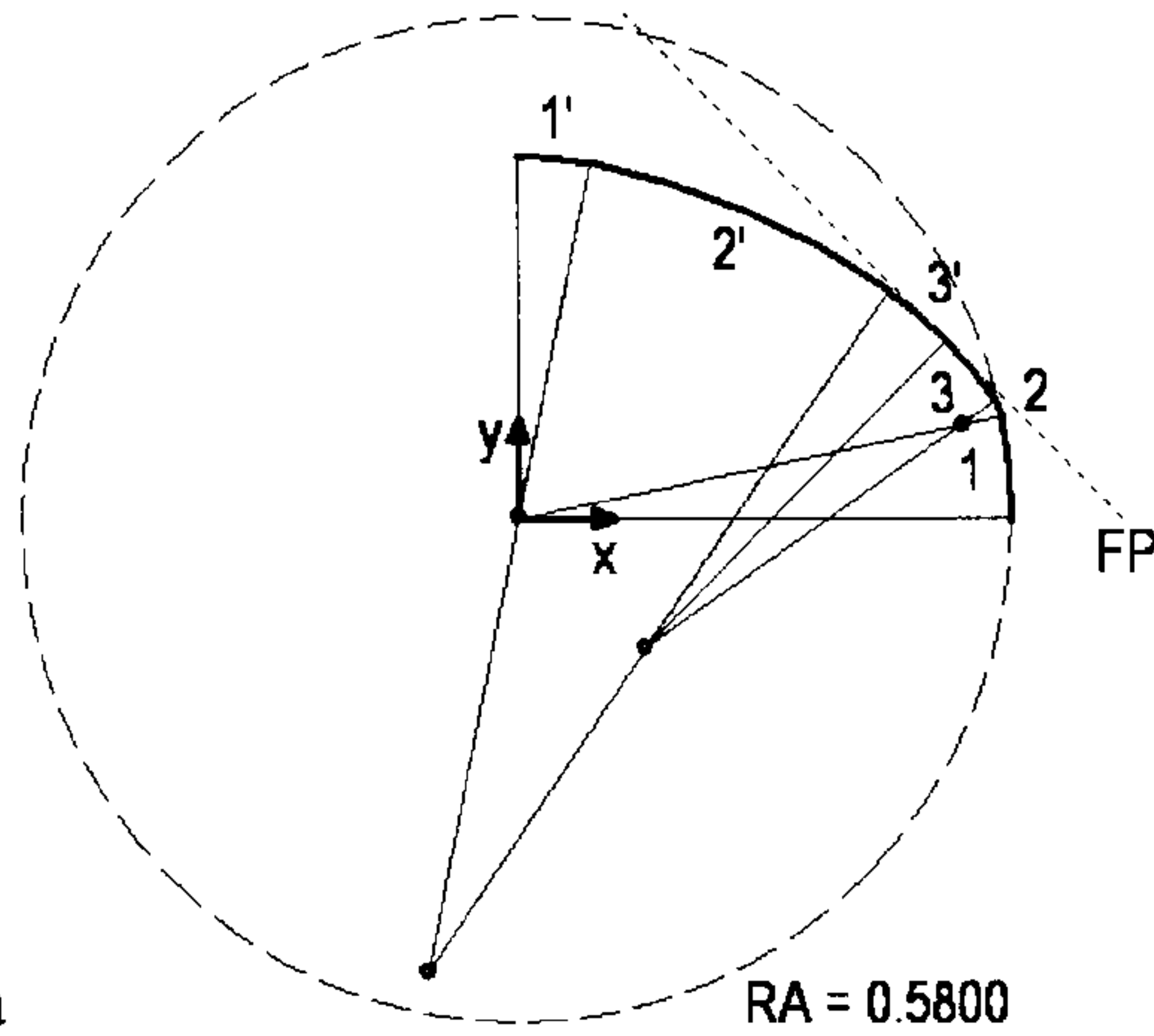


Figure 39a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |
| 2) | $R = 0.0500$ | $Mx = 0.5191$ |
| | $\alpha = 0.4015$ | $My = 0.1069$ |
| 3) | $R = 0.5000$ | $Mx = 0.1489$ |
| | $\alpha = 0.1807$ | $My = -0.1489$ |
| 3') | $R = 0.5000$ | $Mx = 0.1489$ |
| | $\alpha = 0.1807$ | $My = -0.1489$ |
| 2') | $R = 0.9500$ | $Mx = -0.1069$ |
| | $\alpha = 0.4015$ | $My = -0.5191$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.2032$ | $My = 0.0000$ |

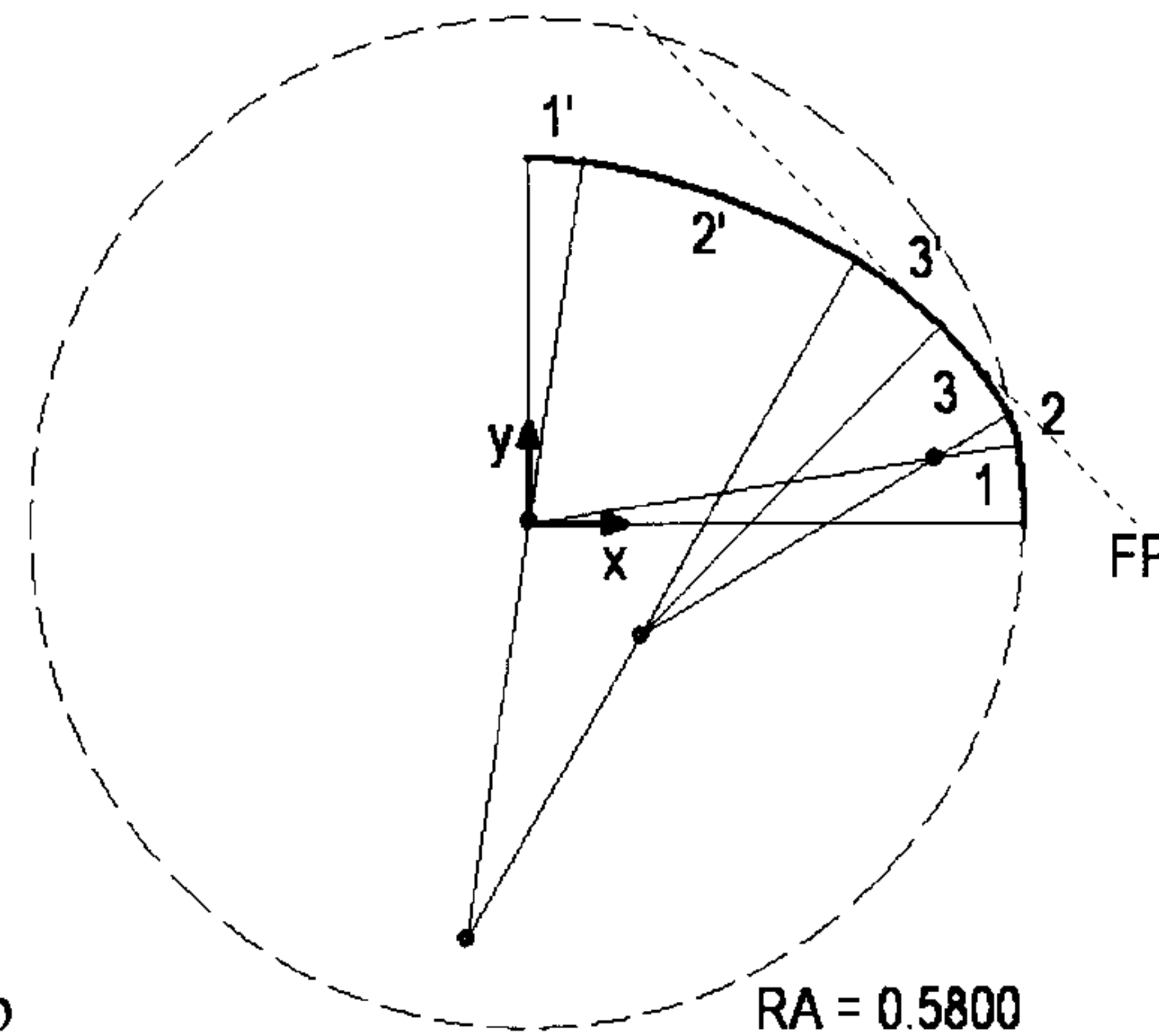


Figure 39b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |
| 2) | $R = 0.1000$ | $Mx = 0.4744$ |
| | $\alpha = 0.3773$ | $My = 0.0729$ |
| 3) | $R = 0.5000$ | $Mx = 0.1293$ |
| | $\alpha = 0.2557$ | $My = -0.1293$ |
| 3') | $R = 0.5000$ | $Mx = 0.1293$ |
| | $\alpha = 0.2557$ | $My = -0.1293$ |
| 2') | $R = 0.9000$ | $Mx = -0.0729$ |
| | $\alpha = 0.3773$ | $My = -0.4744$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1524$ | $My = 0.0000$ |

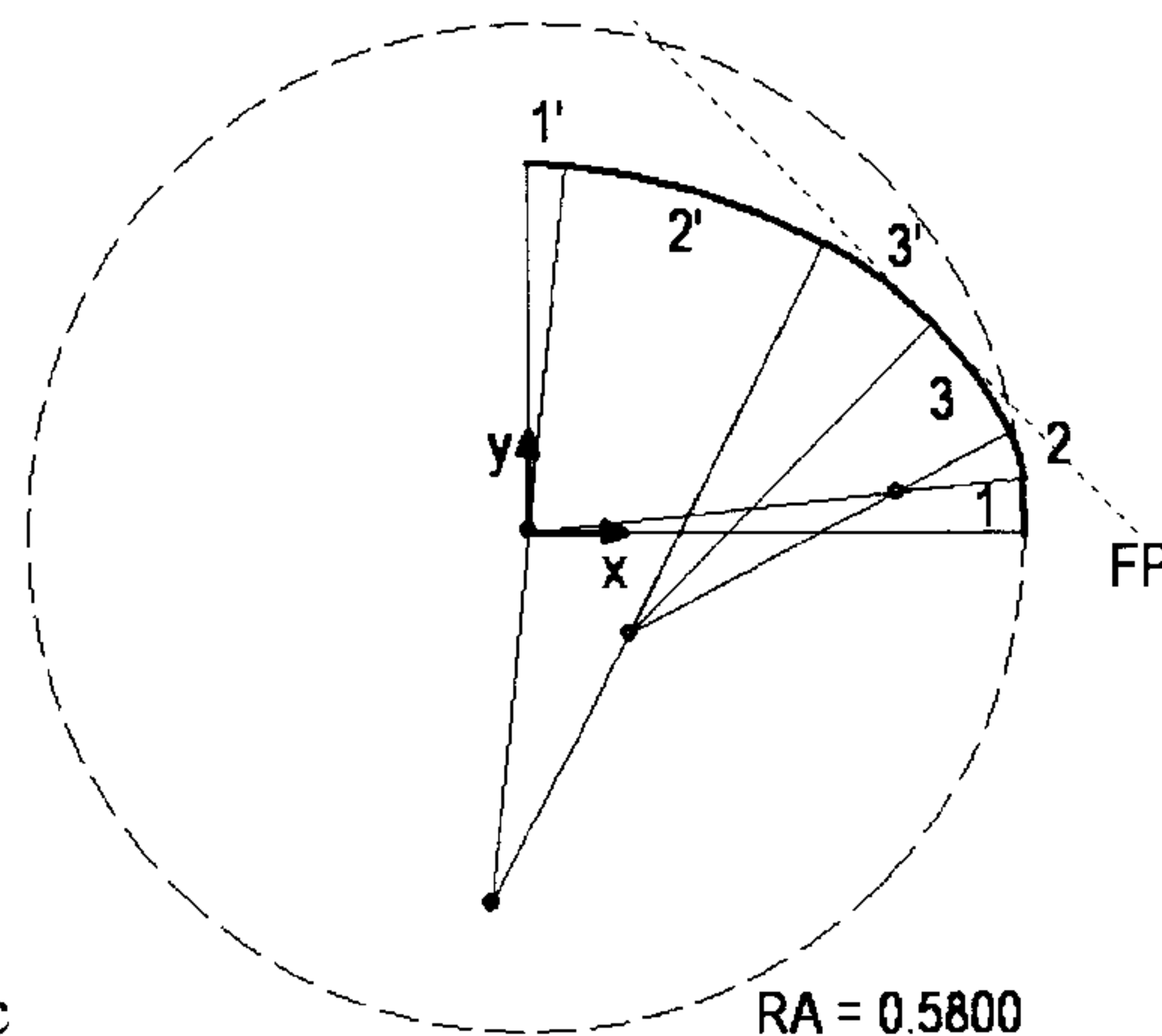


Figure 39c

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |
| 2) | $R = 0.1500$ | $Mx = 0.4278$ |
| | $\alpha = 0.3739$ | $My = 0.0436$ |
| 3) | $R = 0.5000$ | $Mx = 0.1166$ |
| | $\alpha = 0.3100$ | $My = -0.1166$ |
| 3') | $R = 0.5000$ | $Mx = 0.1166$ |
| | $\alpha = 0.3100$ | $My = -0.1166$ |
| 2') | $R = 0.8500$ | $Mx = -0.0436$ |
| | $\alpha = 0.3739$ | $My = -0.4278$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.1016$ | $My = 0.0000$ |

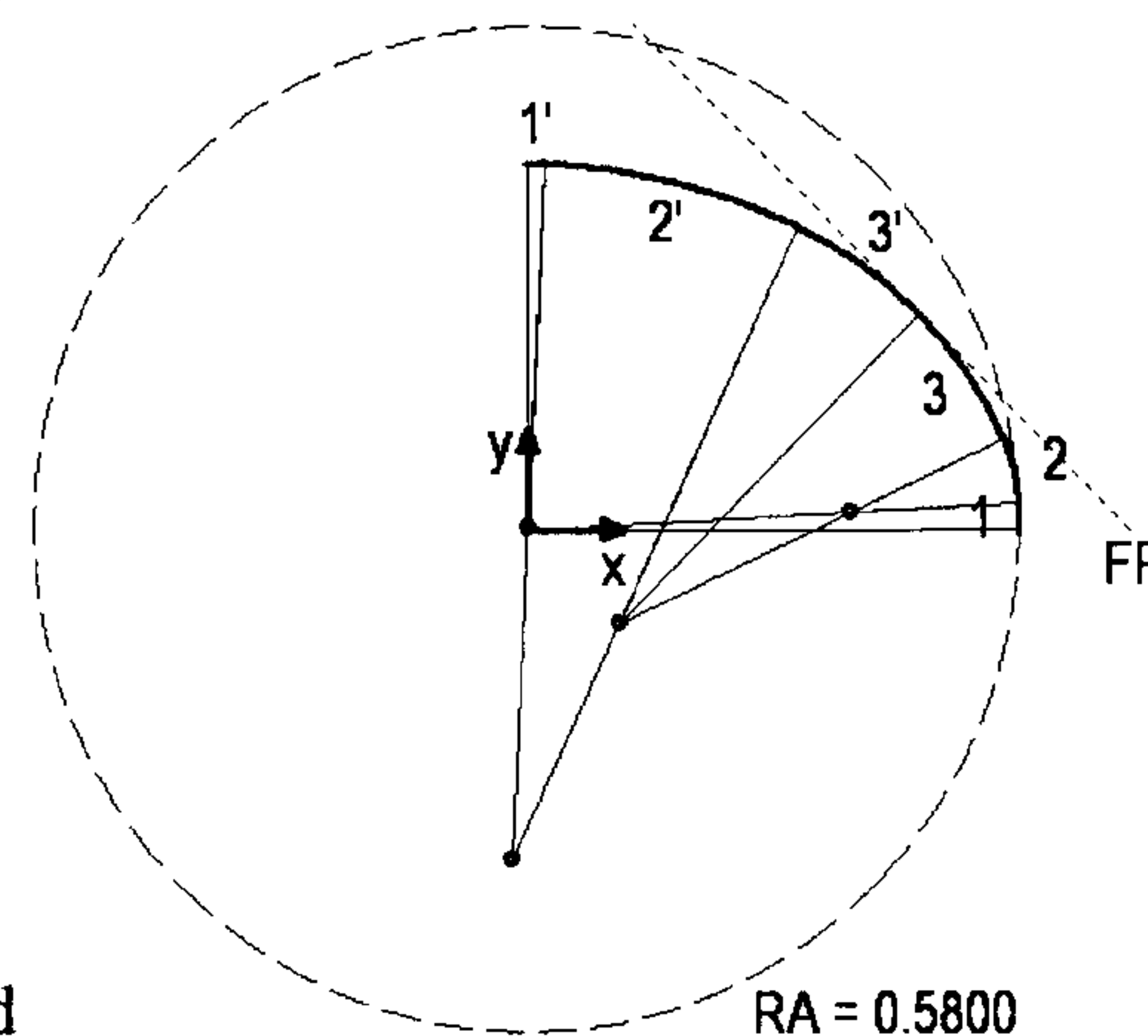


Figure 39d

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.5800$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |
| 2) | $R = 0.2000$ | $Mx = 0.3795$ |
| | $\alpha = 0.3864$ | $My = 0.0193$ |
| 3) | $R = 0.5000$ | $Mx = 0.1077$ |
| | $\alpha = 0.3482$ | $My = -0.1077$ |
| 3') | $R = 0.5000$ | $Mx = 0.1077$ |
| | $\alpha = 0.3482$ | $My = -0.1077$ |
| 2') | $R = 0.8000$ | $Mx = -0.0193$ |
| | $\alpha = 0.3864$ | $My = -0.3795$ |
| 1') | $R = 0.4200$ | $Mx = 0.0000$ |
| | $\alpha = 0.0508$ | $My = 0.0000$ |

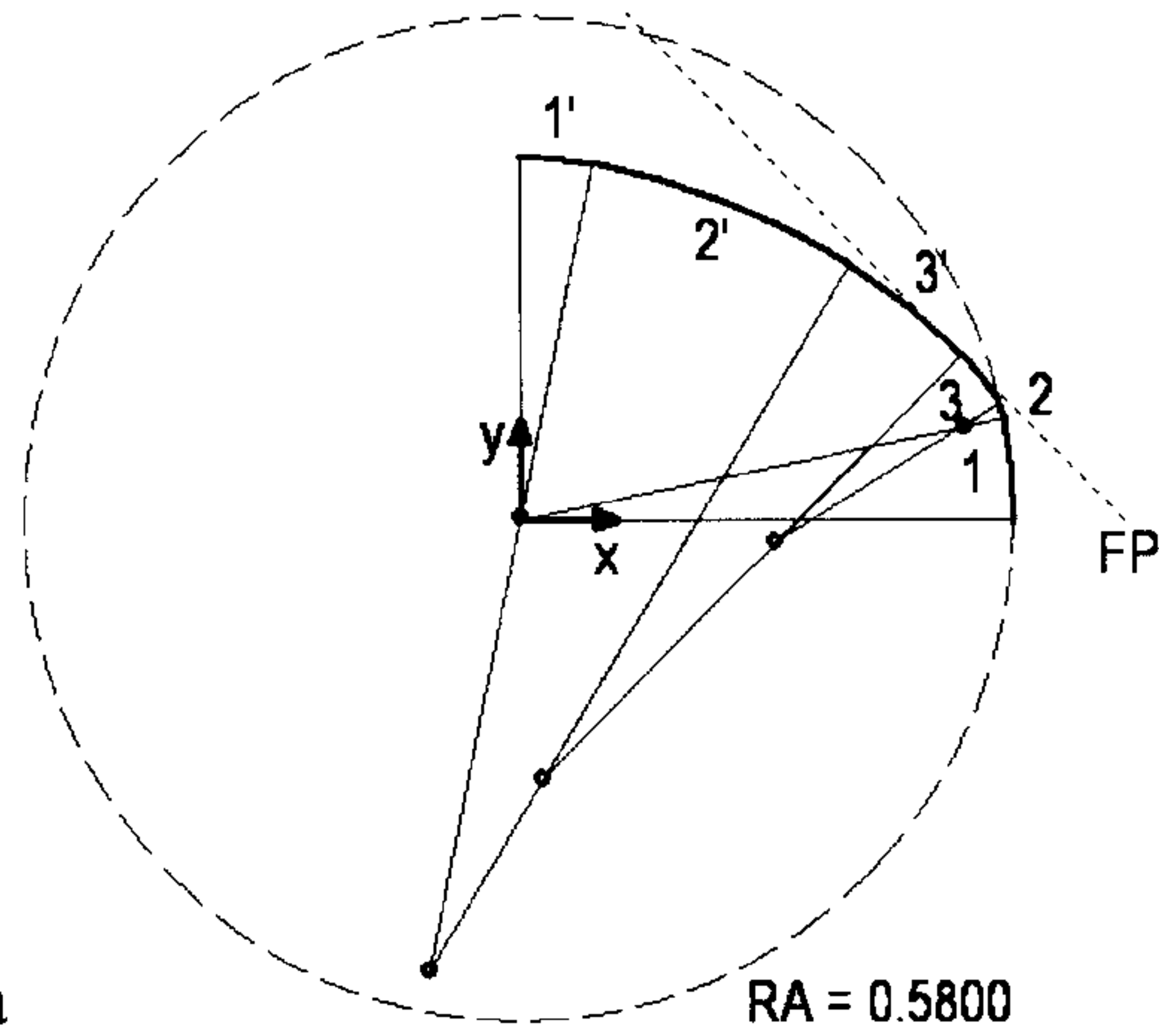


Figure 40a

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.2032$ | $M_y = 0.0000$ |
| 2) | $R = 0.0500$ | $M_x = 0.5191$ |
| | $\alpha = 0.3428$ | $M_y = 0.1069$ |
| 3) | $R = 0.3069$ | $M_x = 0.2996$ |
| | $\alpha = 0.2394$ | $M_y = -0.0264$ |
| 3') | $R = 0.6931$ | $M_x = 0.0264$ |
| | $\alpha = 0.2394$ | $M_y = -0.2996$ |
| 2') | $R = 0.9500$ | $M_x = -0.1069$ |
| | $\alpha = 0.3428$ | $M_y = -0.5191$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.2032$ | $M_y = 0.0000$ |

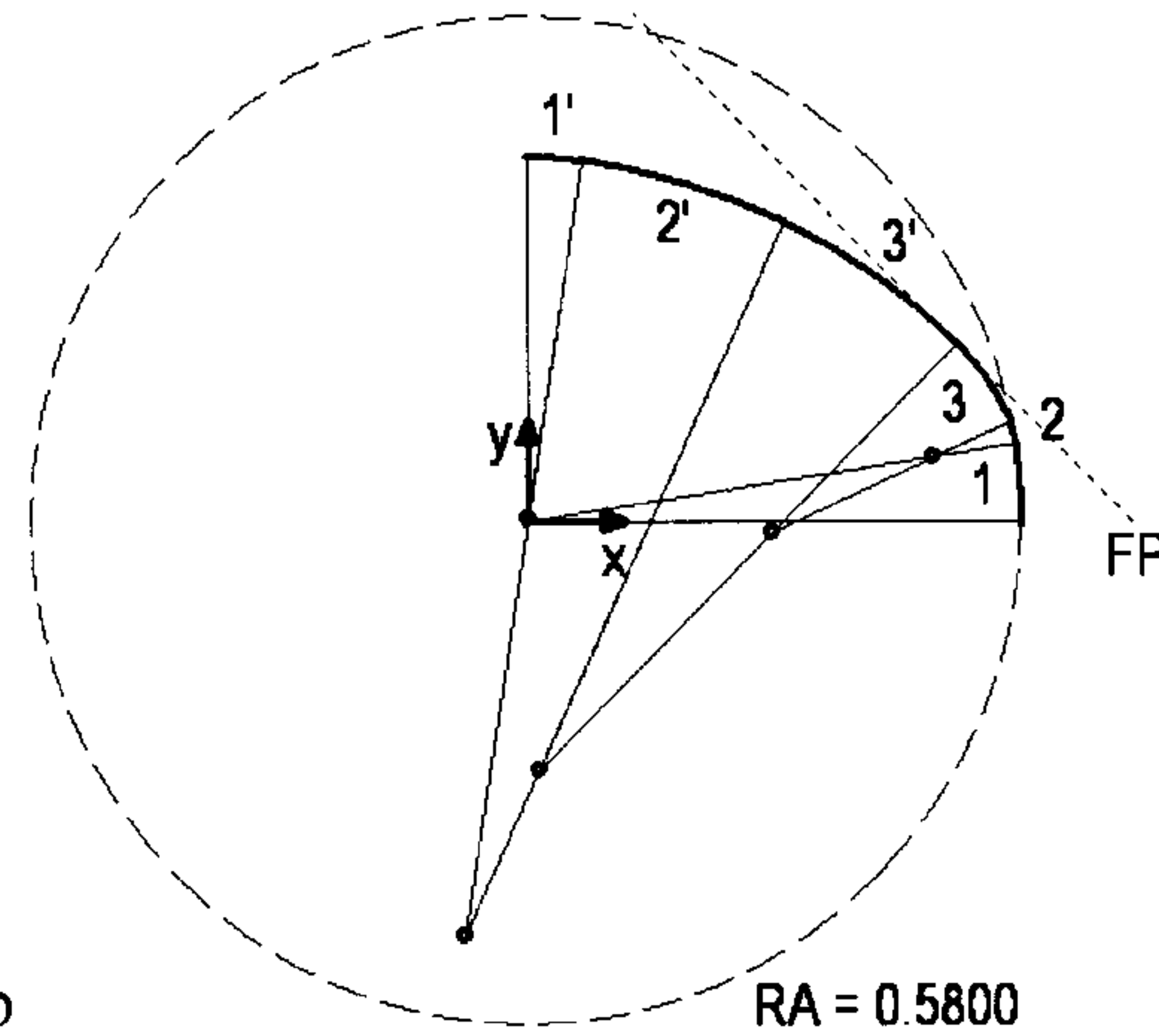


Figure 40b

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.1524$ | $M_y = 0.0000$ |
| 2) | $R = 0.1000$ | $M_x = 0.4744$ |
| | $\alpha = 0.2765$ | $M_y = 0.0729$ |
| 3) | $R = 0.3069$ | $M_x = 0.2863$ |
| | $\alpha = 0.3565$ | $M_y = -0.0132$ |
| 3') | $R = 0.6931$ | $M_x = 0.0132$ |
| | $\alpha = 0.3565$ | $M_y = -0.2863$ |
| 2') | $R = 0.9000$ | $M_x = -0.0729$ |
| | $\alpha = 0.2765$ | $M_y = -0.4744$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.1524$ | $M_y = 0.0000$ |

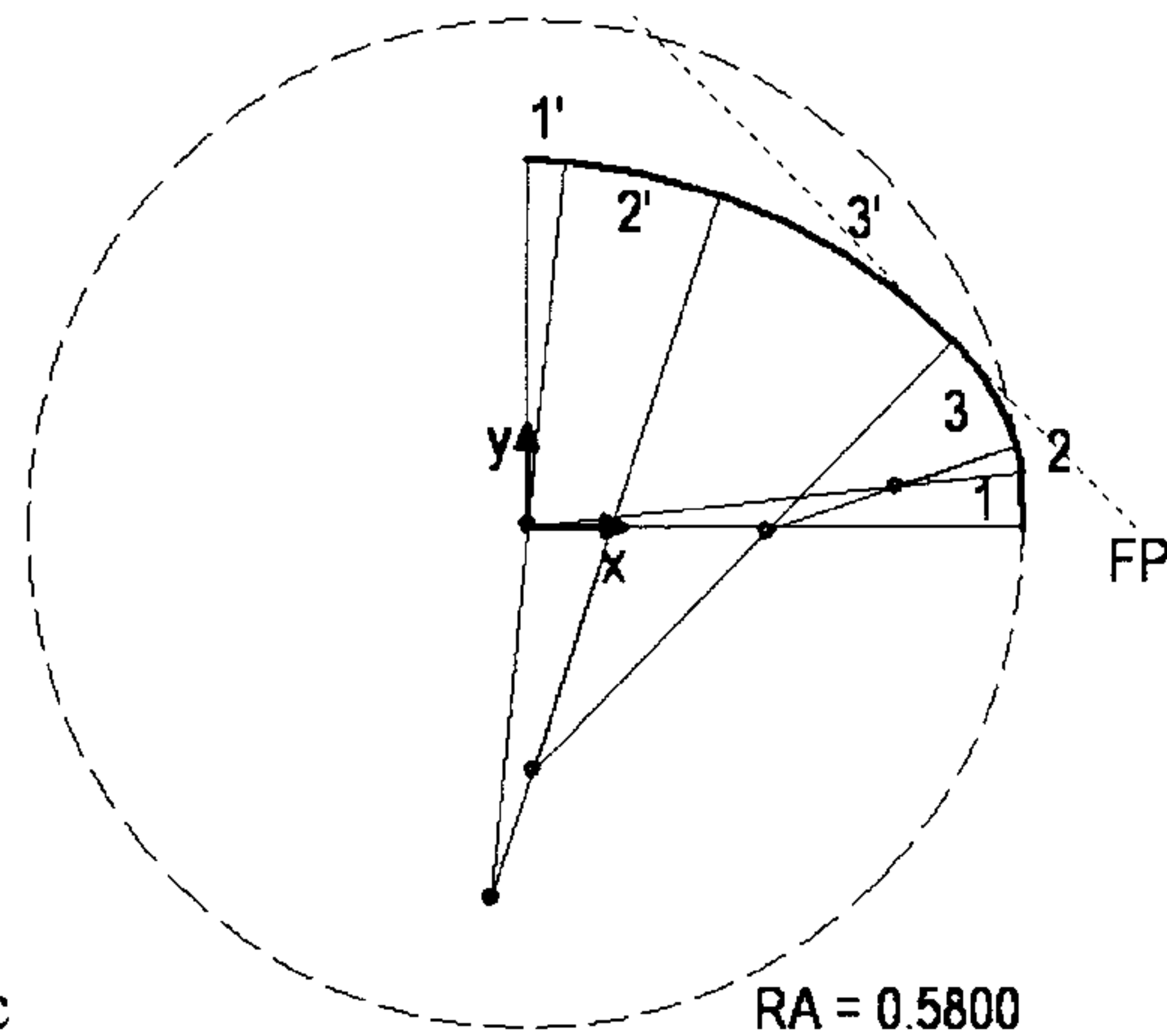


Figure 40c

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.1016$ | $M_y = 0.0000$ |
| 2) | $R = 0.1500$ | $M_x = 0.4278$ |
| | $\alpha = 0.2185$ | $M_y = 0.0436$ |
| 3) | $R = 0.3069$ | $M_x = 0.2789$ |
| | $\alpha = 0.4653$ | $M_y = -0.0057$ |
| 3') | $R = 0.6931$ | $M_x = 0.0057$ |
| | $\alpha = 0.4653$ | $M_y = -0.2789$ |
| 2') | $R = 0.8500$ | $M_x = -0.0436$ |
| | $\alpha = 0.2185$ | $M_y = -0.4278$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.1016$ | $M_y = 0.0000$ |

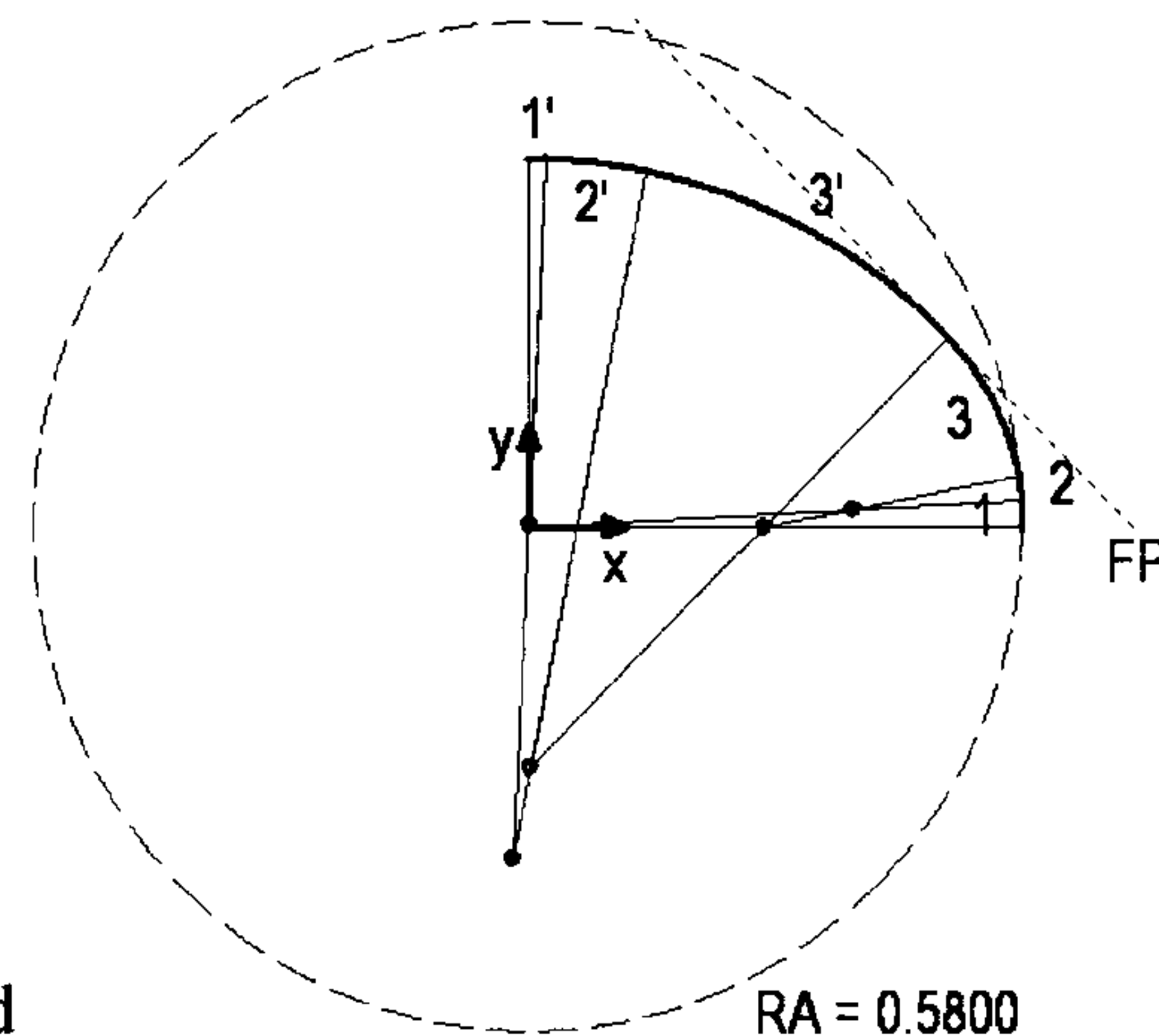


Figure 40d

- | | | |
|-----|-------------------|-----------------|
| 1) | $R = 0.5800$ | $M_x = 0.0000$ |
| | $\alpha = 0.0508$ | $M_y = 0.0000$ |
| 2) | $R = 0.2000$ | $M_x = 0.3795$ |
| | $\alpha = 0.1456$ | $M_y = 0.0193$ |
| 3) | $R = 0.3069$ | $M_x = 0.2747$ |
| | $\alpha = 0.5890$ | $M_y = -0.0016$ |
| 3') | $R = 0.6931$ | $M_x = 0.0016$ |
| | $\alpha = 0.5890$ | $M_y = -0.2747$ |
| 2') | $R = 0.8000$ | $M_x = -0.0193$ |
| | $\alpha = 0.1456$ | $M_y = -0.3795$ |
| 1') | $R = 0.4200$ | $M_x = 0.0000$ |
| | $\alpha = 0.0508$ | $M_y = 0.0000$ |

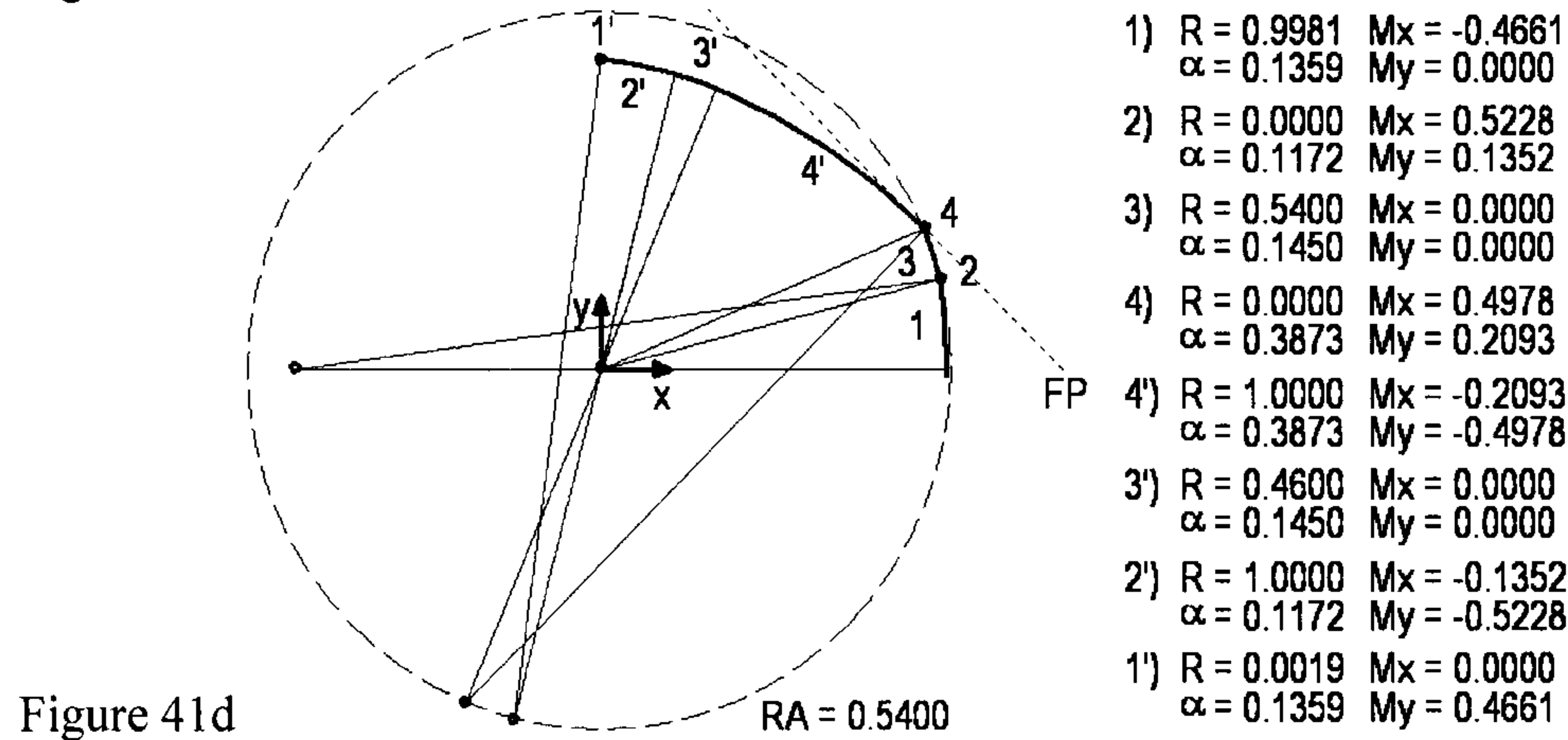
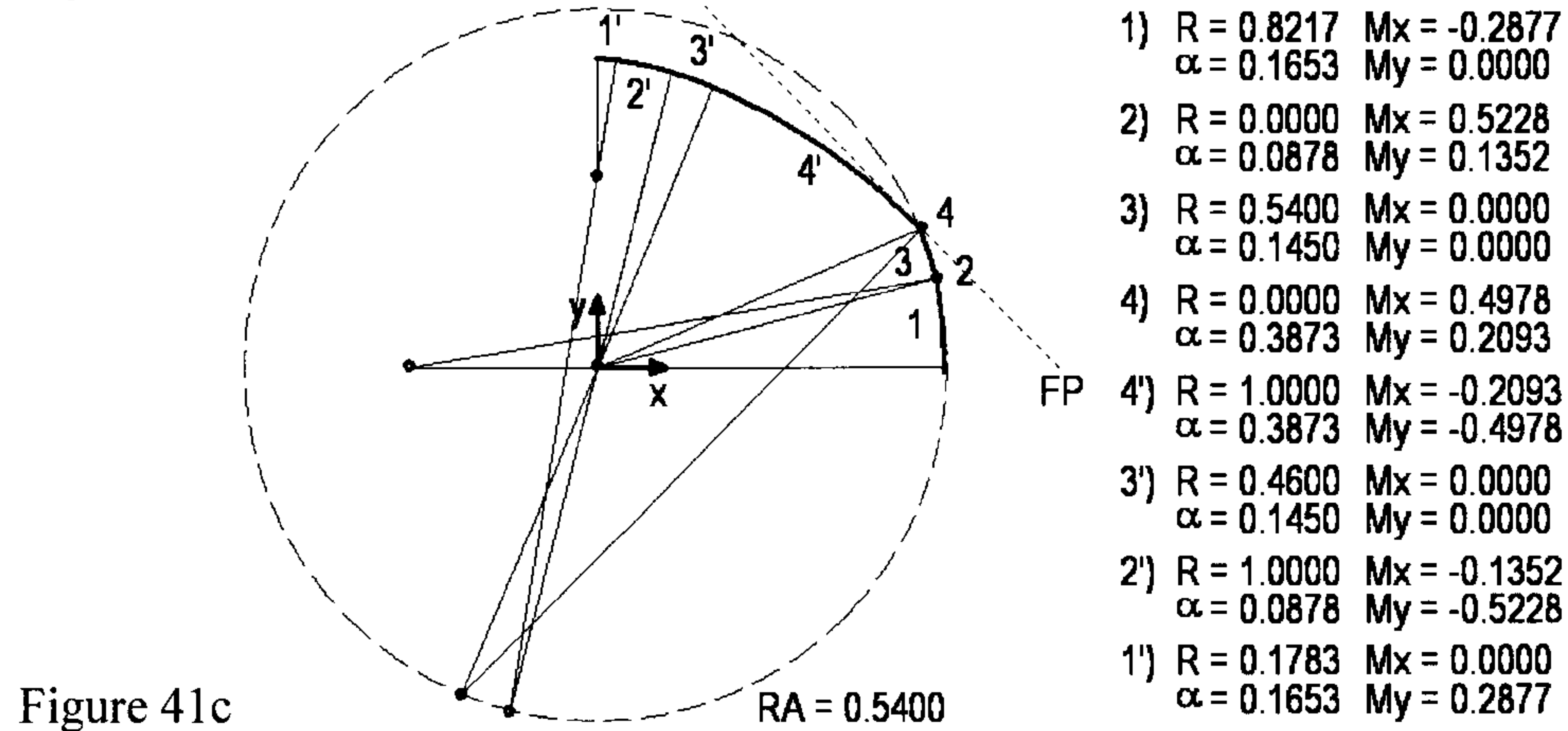
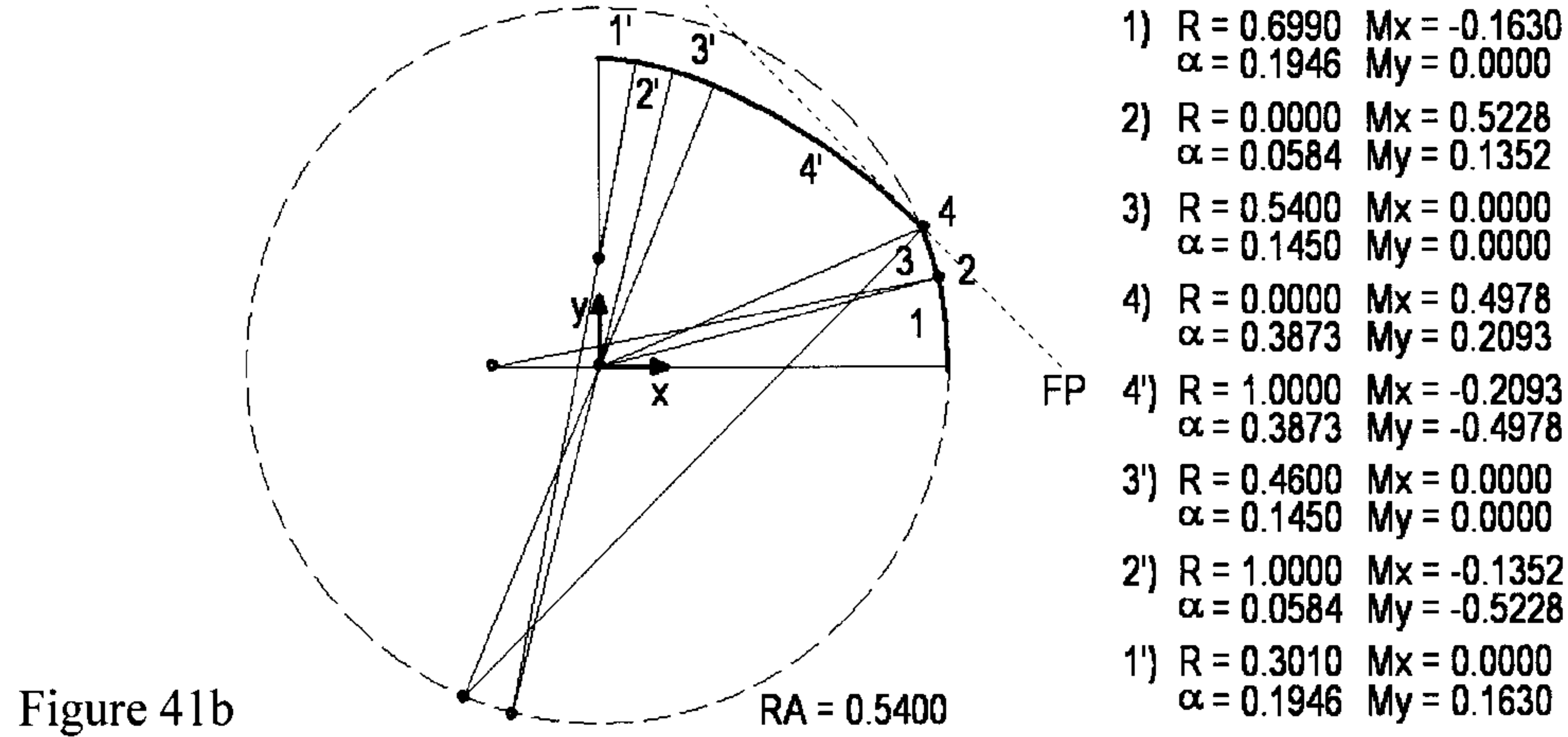
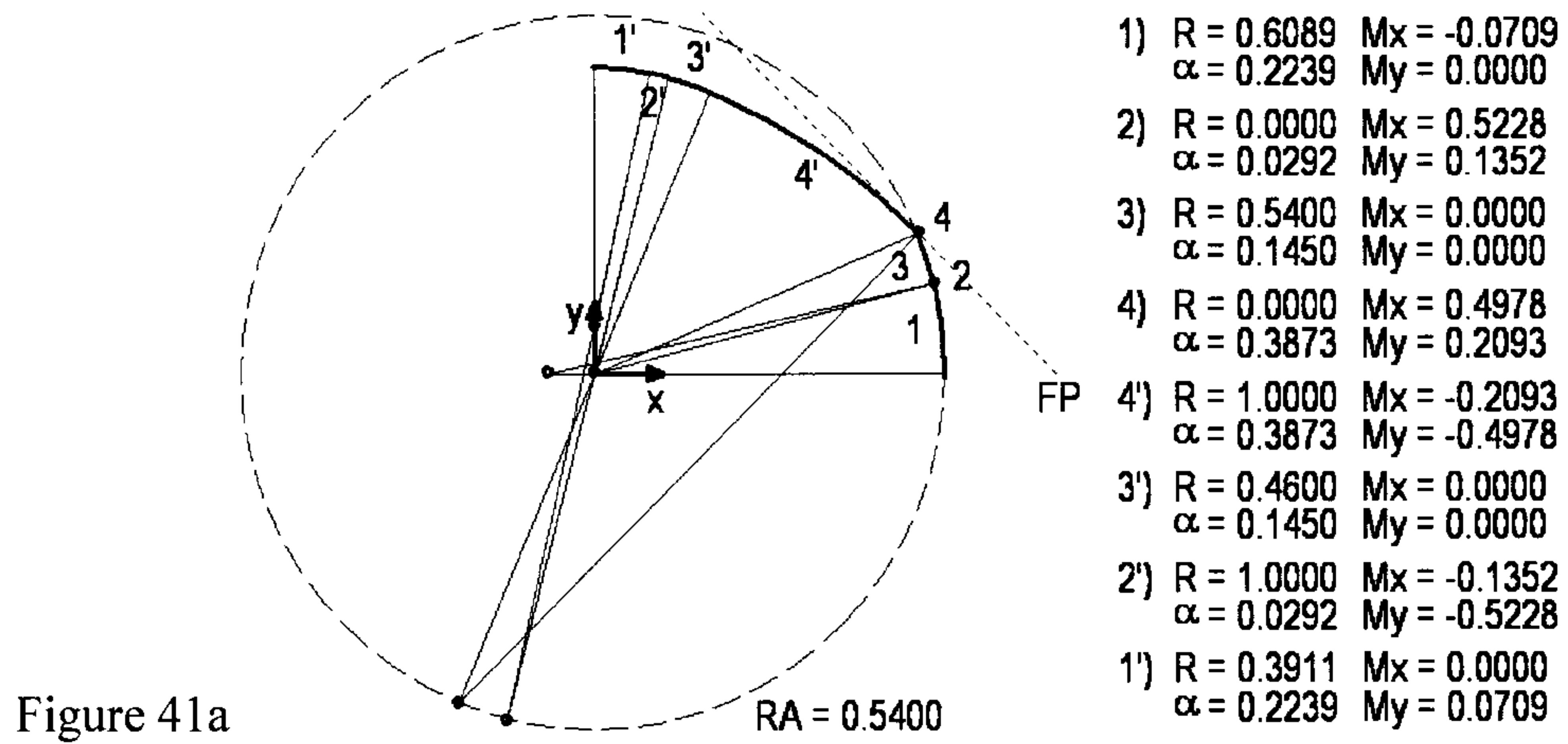
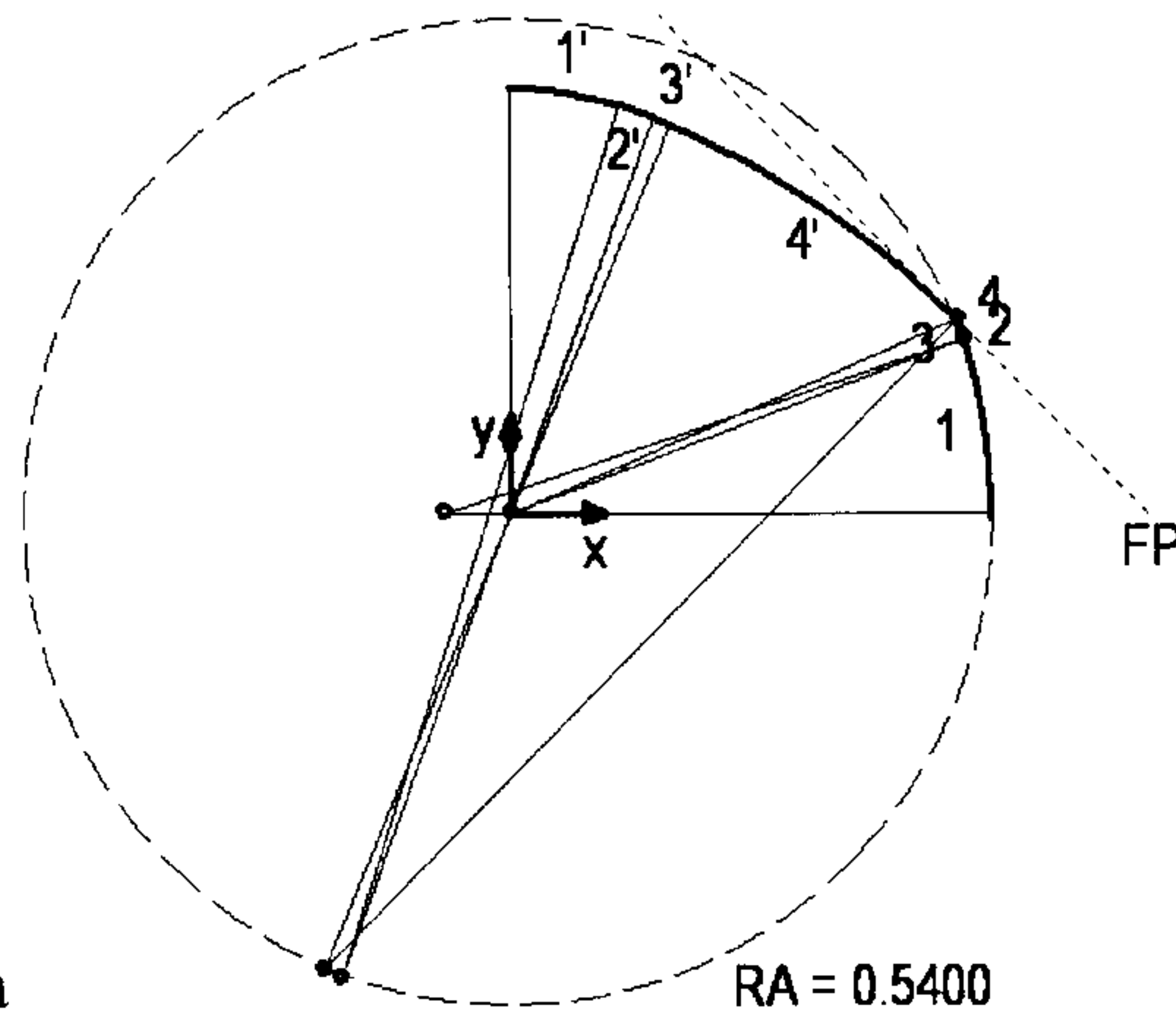
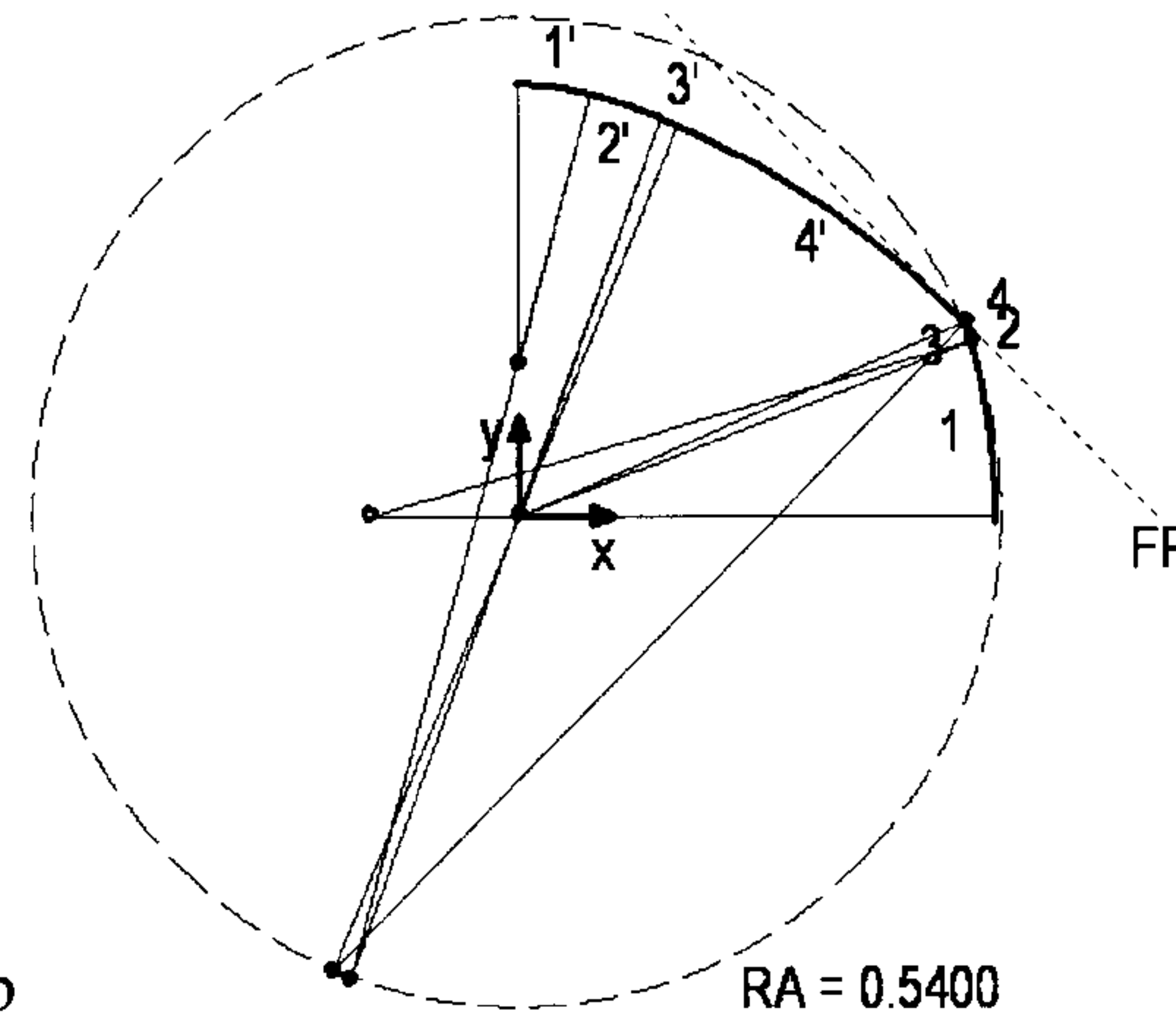


Figure 42a



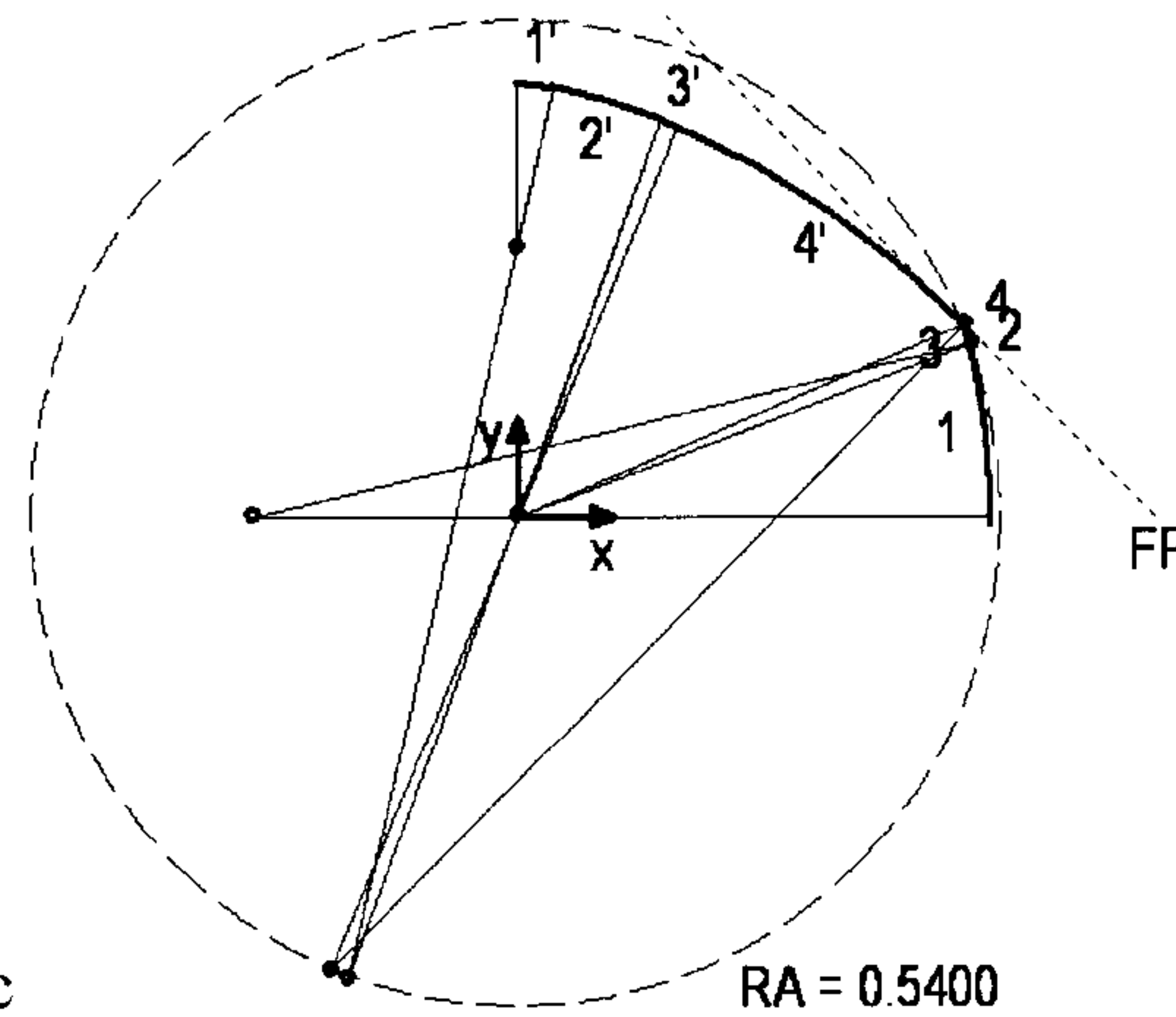
- 1) $R = 0.6080$ $Mx = -0.0720$
 $\alpha = 0.3149$ $My = 0.0000$
- 2) $R = 0.0000$ $Mx = 0.5061$
 $\alpha = 0.0413$ $My = 0.1883$
- 3) $R = 0.5400$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 4) $R = 0.0000$ $Mx = 0.4978$
 $\alpha = 0.3873$ $My = 0.2093$
- 4') $R = 1.0000$ $Mx = -0.2093$
 $\alpha = 0.3873$ $My = -0.4978$
- 3') $R = 0.4600$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 2') $R = 1.0000$ $Mx = -0.1883$
 $\alpha = 0.0413$ $My = -0.5061$
- 1') $R = 0.3920$ $Mx = 0.0000$
 $\alpha = 0.3149$ $My = 0.0720$

Figure 42b



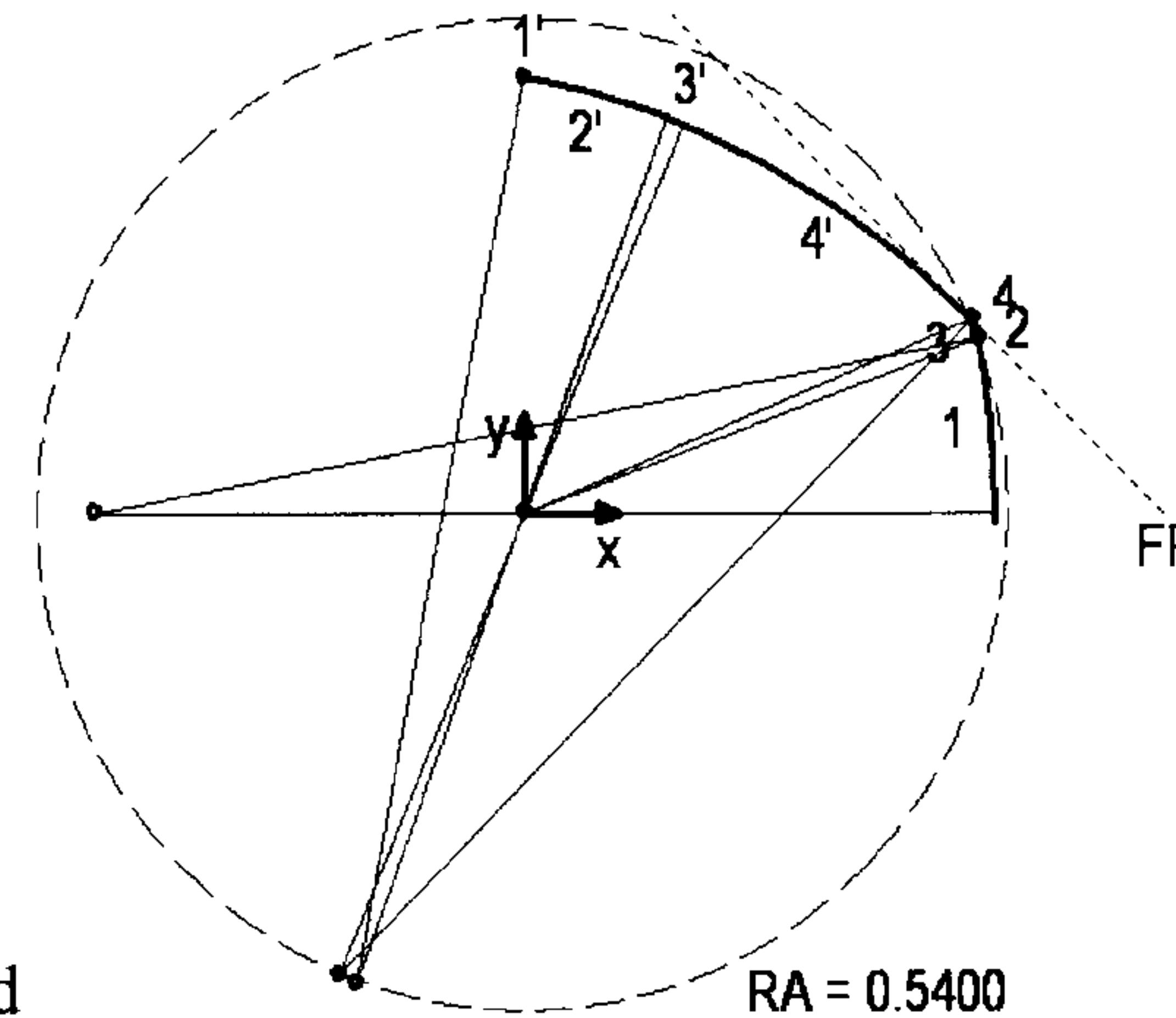
- 1) $R = 0.6976$ $Mx = -0.1656$
 $\alpha = 0.2734$ $My = 0.0000$
- 2) $R = 0.0000$ $Mx = 0.5061$
 $\alpha = 0.0829$ $My = 0.1883$
- 3) $R = 0.5400$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 4) $R = 0.0000$ $Mx = 0.4978$
 $\alpha = 0.3873$ $My = 0.2093$
- 4') $R = 1.0000$ $Mx = -0.2093$
 $\alpha = 0.3873$ $My = -0.4978$
- 3') $R = 0.4600$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 2') $R = 1.0000$ $Mx = -0.1883$
 $\alpha = 0.0829$ $My = -0.5061$
- 1') $R = 0.3024$ $Mx = 0.0000$
 $\alpha = 0.2734$ $My = 0.1656$

Figure 42c



- 1) $R = 0.8206$ $Mx = -0.2926$
 $\alpha = 0.2316$ $My = 0.0000$
- 2) $R = 0.0000$ $Mx = 0.5061$
 $\alpha = 0.1247$ $My = 0.1883$
- 3) $R = 0.5400$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 4) $R = 0.0000$ $Mx = 0.4978$
 $\alpha = 0.3873$ $My = 0.2093$
- 4') $R = 1.0000$ $Mx = -0.2093$
 $\alpha = 0.3873$ $My = -0.4978$
- 3') $R = 0.4600$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 2') $R = 1.0000$ $Mx = -0.1883$
 $\alpha = 0.1247$ $My = -0.5061$
- 1') $R = 0.1794$ $Mx = 0.0000$
 $\alpha = 0.2316$ $My = 0.2926$

Figure 42d



- 1) $R = 0.9995$ $Mx = -0.4755$
 $\alpha = 0.1895$ $My = 0.0000$
- 2) $R = 0.0000$ $Mx = 0.5061$
 $\alpha = 0.1667$ $My = 0.1883$
- 3) $R = 0.5400$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 4) $R = 0.0000$ $Mx = 0.4978$
 $\alpha = 0.3873$ $My = 0.2093$
- 4') $R = 1.0000$ $Mx = -0.2093$
 $\alpha = 0.3873$ $My = -0.4978$
- 3') $R = 0.4600$ $Mx = 0.0000$
 $\alpha = 0.0419$ $My = 0.0000$
- 2') $R = 1.0000$ $Mx = -0.1883$
 $\alpha = 0.1667$ $My = -0.5061$
- 1') $R = 0.0005$ $Mx = 0.0000$
 $\alpha = 0.1895$ $My = 0.4755$

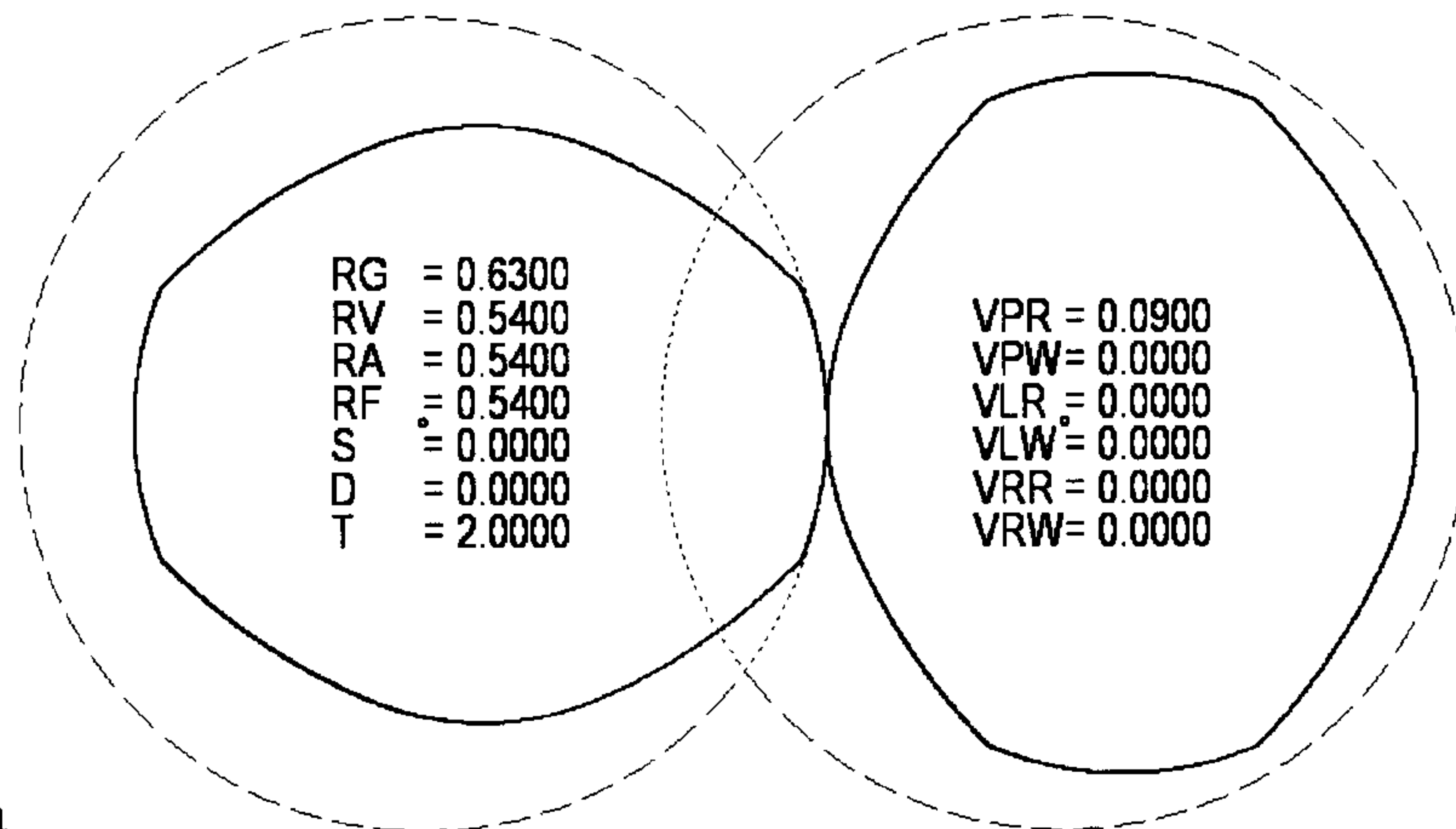


Figure 43a

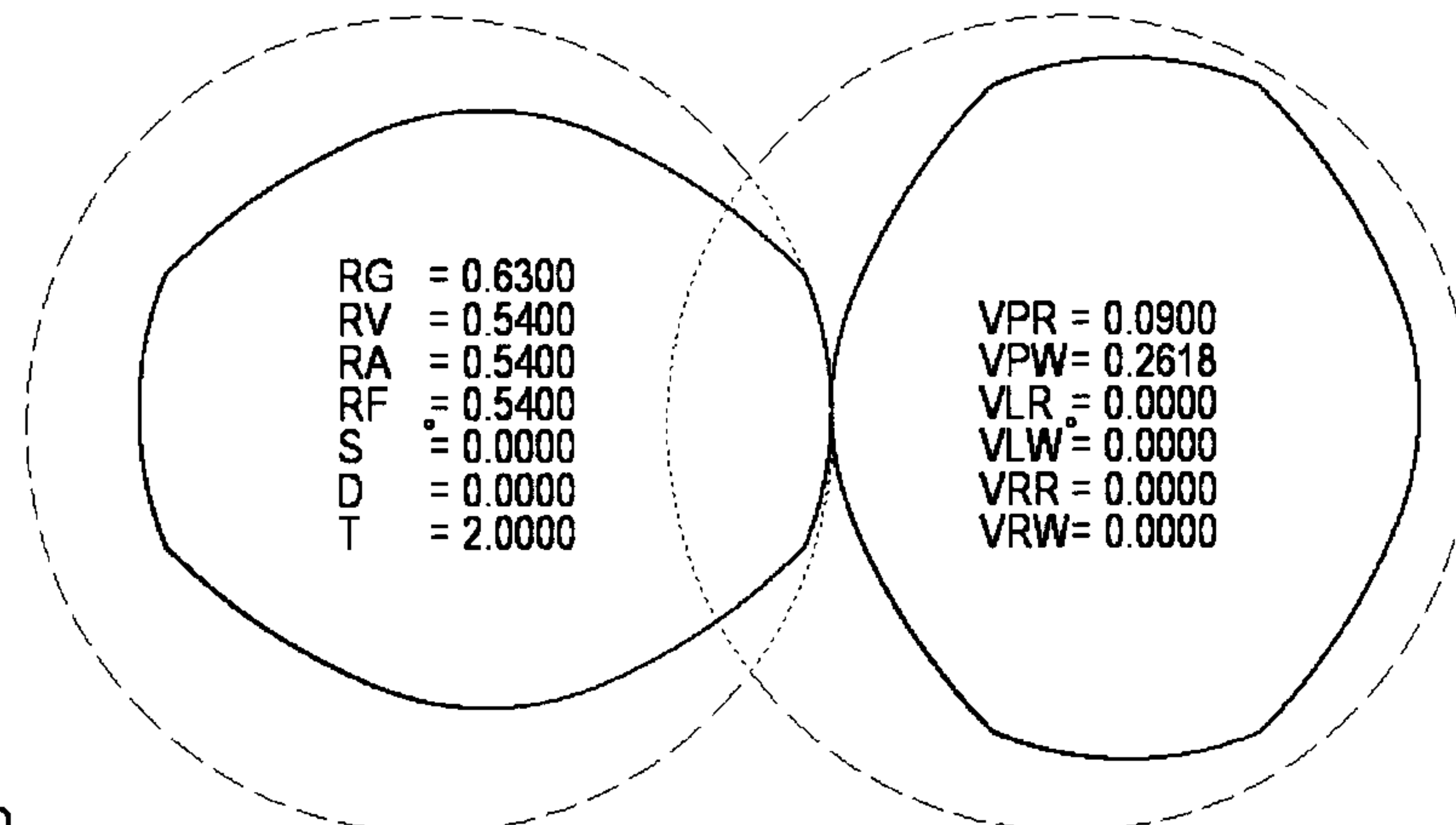


Figure 43b

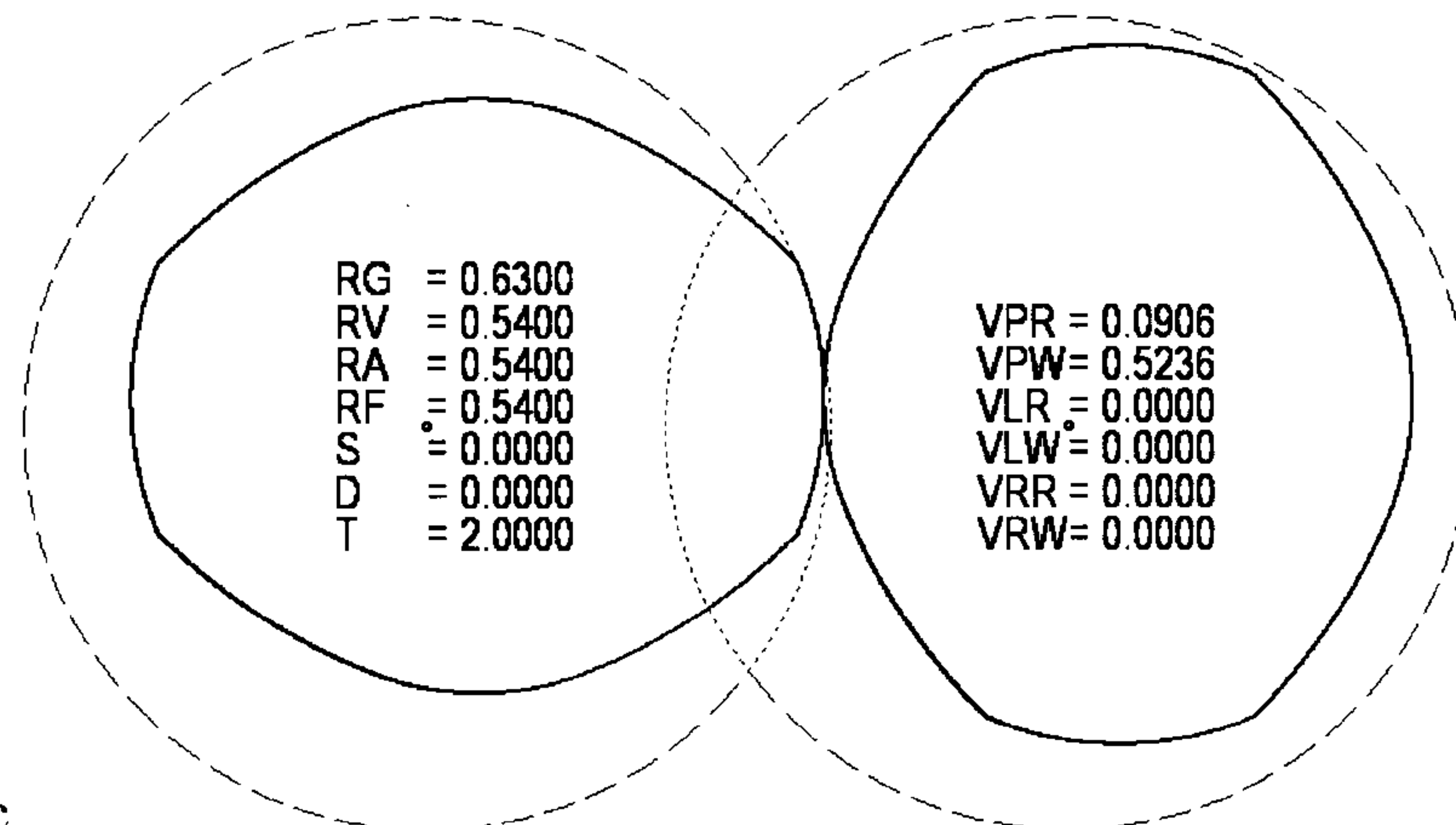


Figure 43c

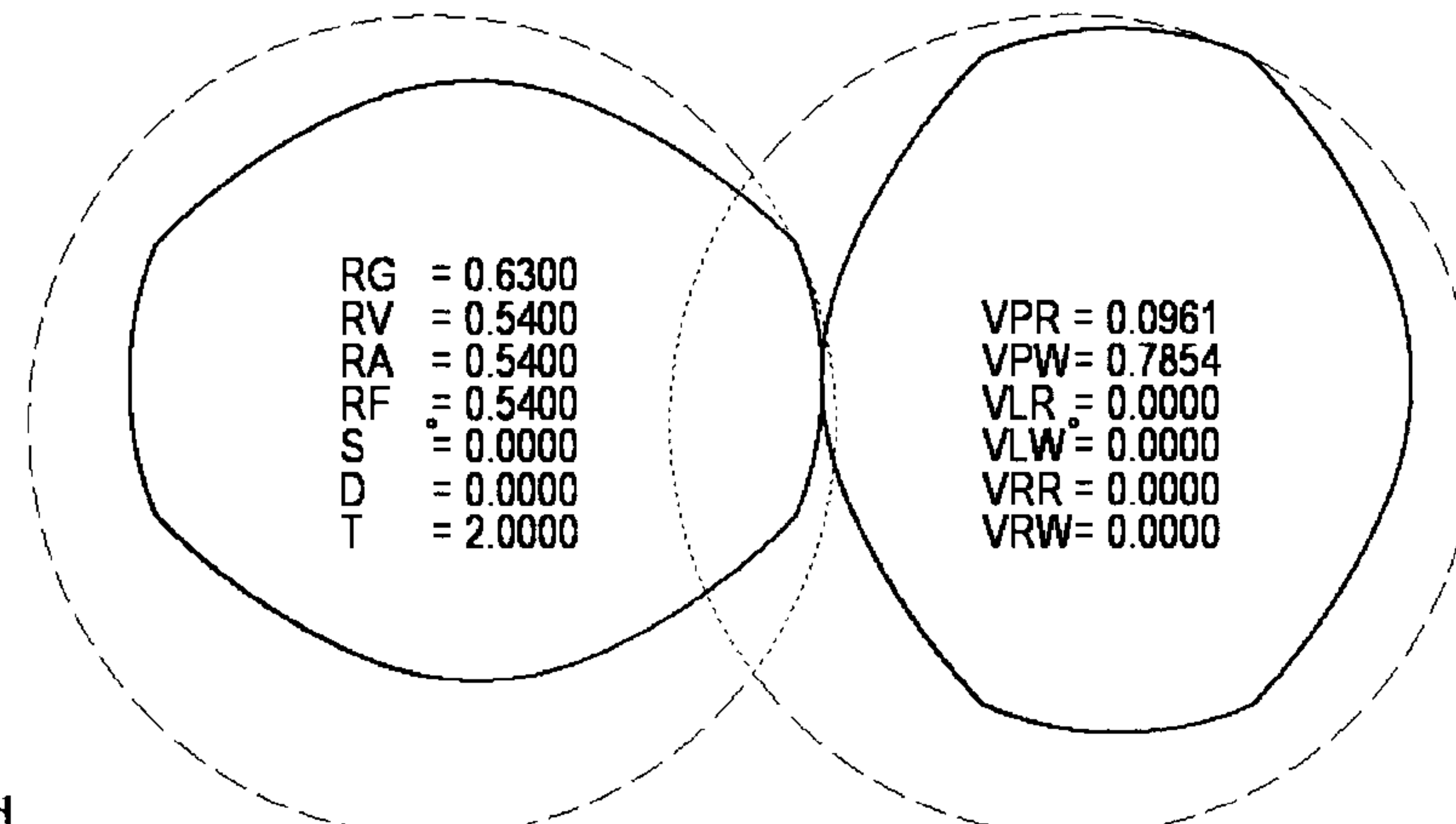


Figure 43d

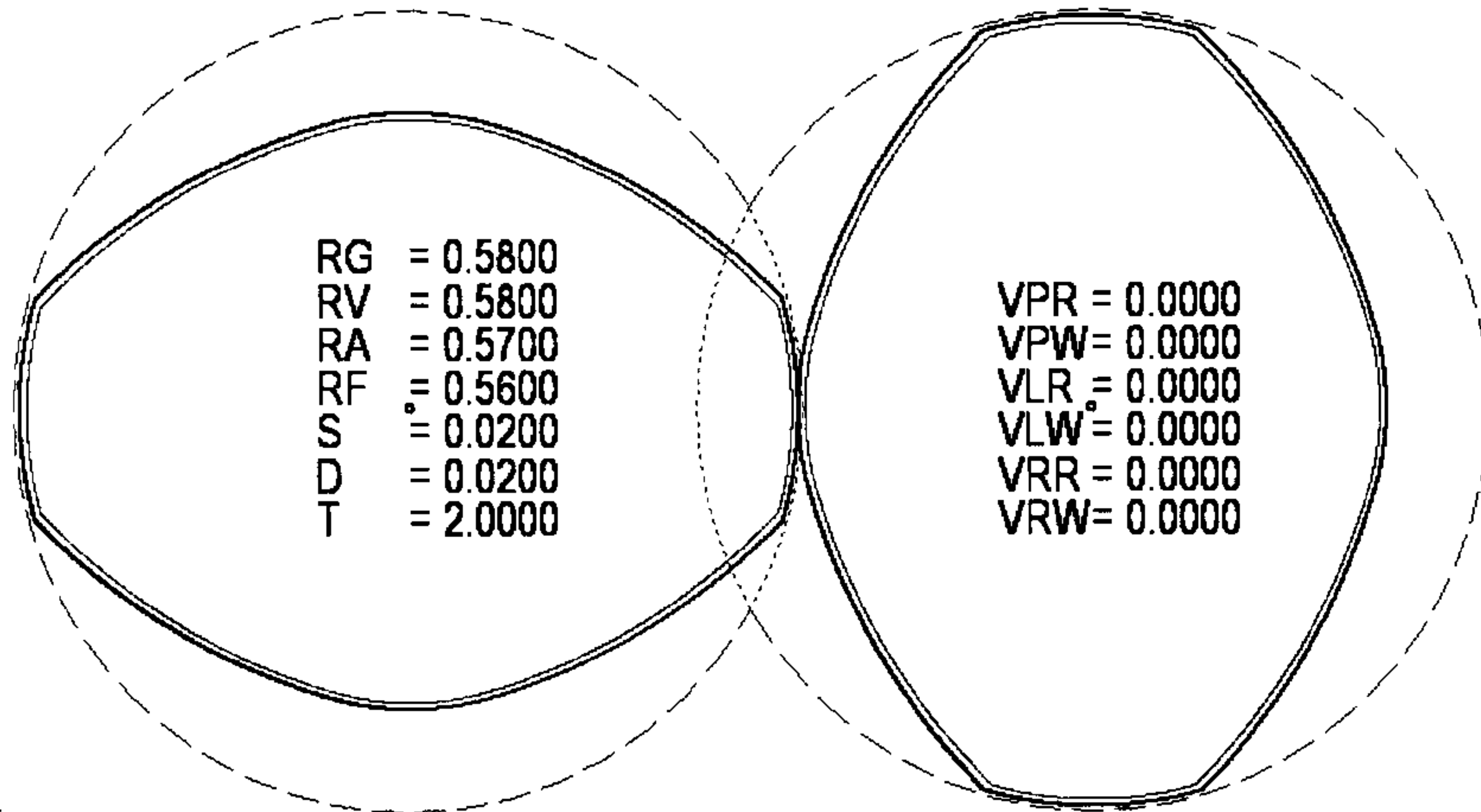


Figure 44a

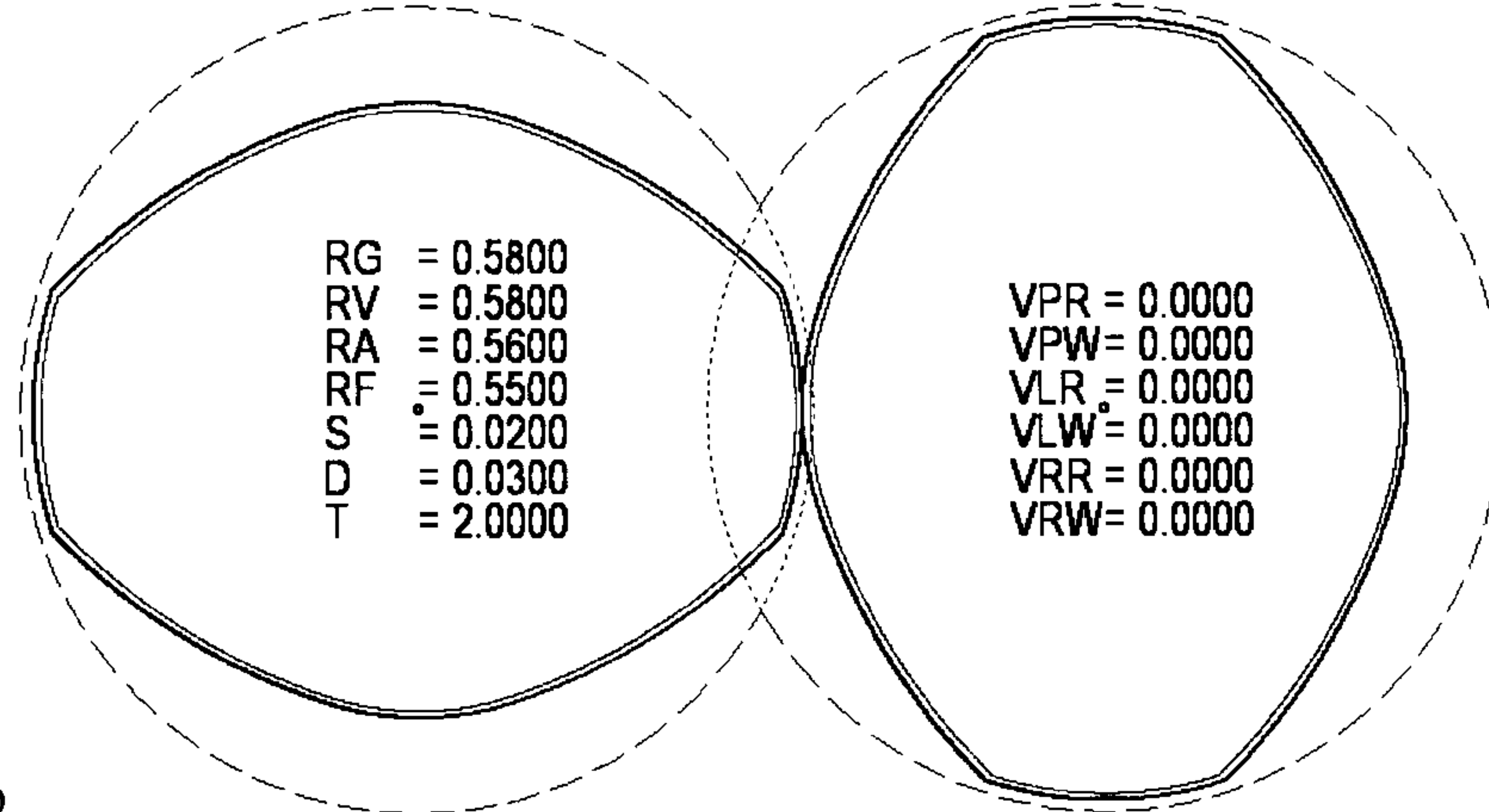


Figure 44b

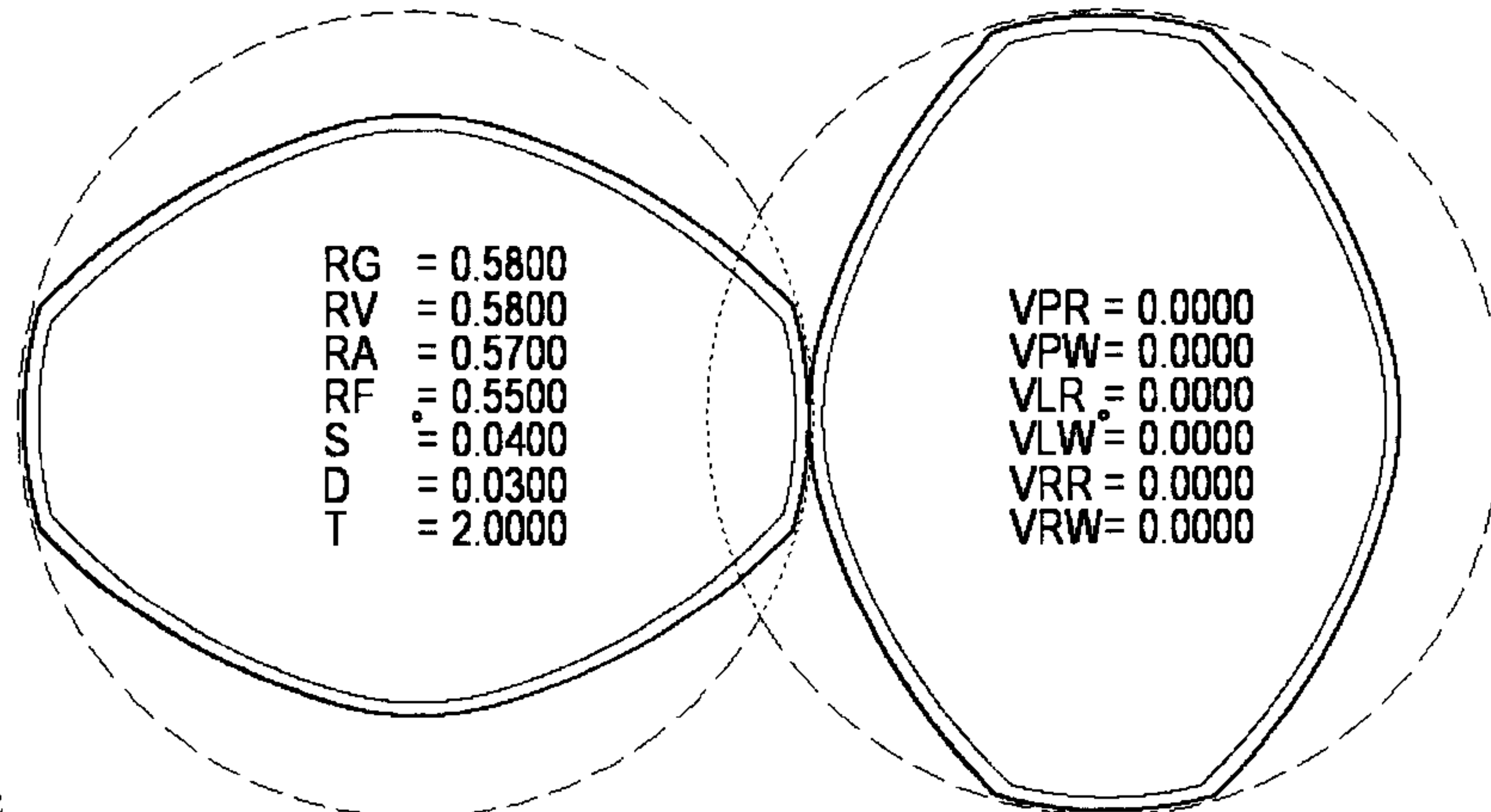


Figure 44c

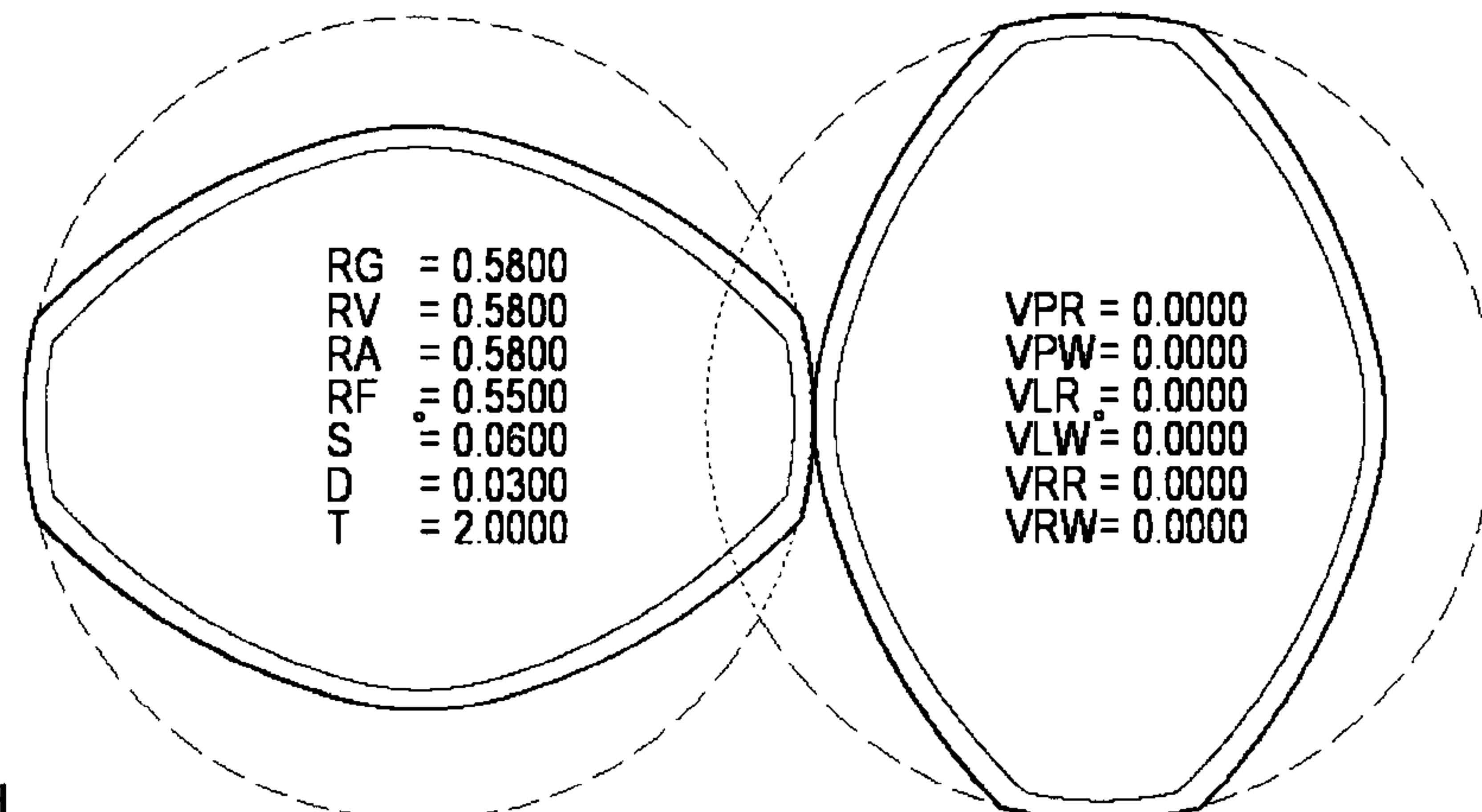


Figure 44d

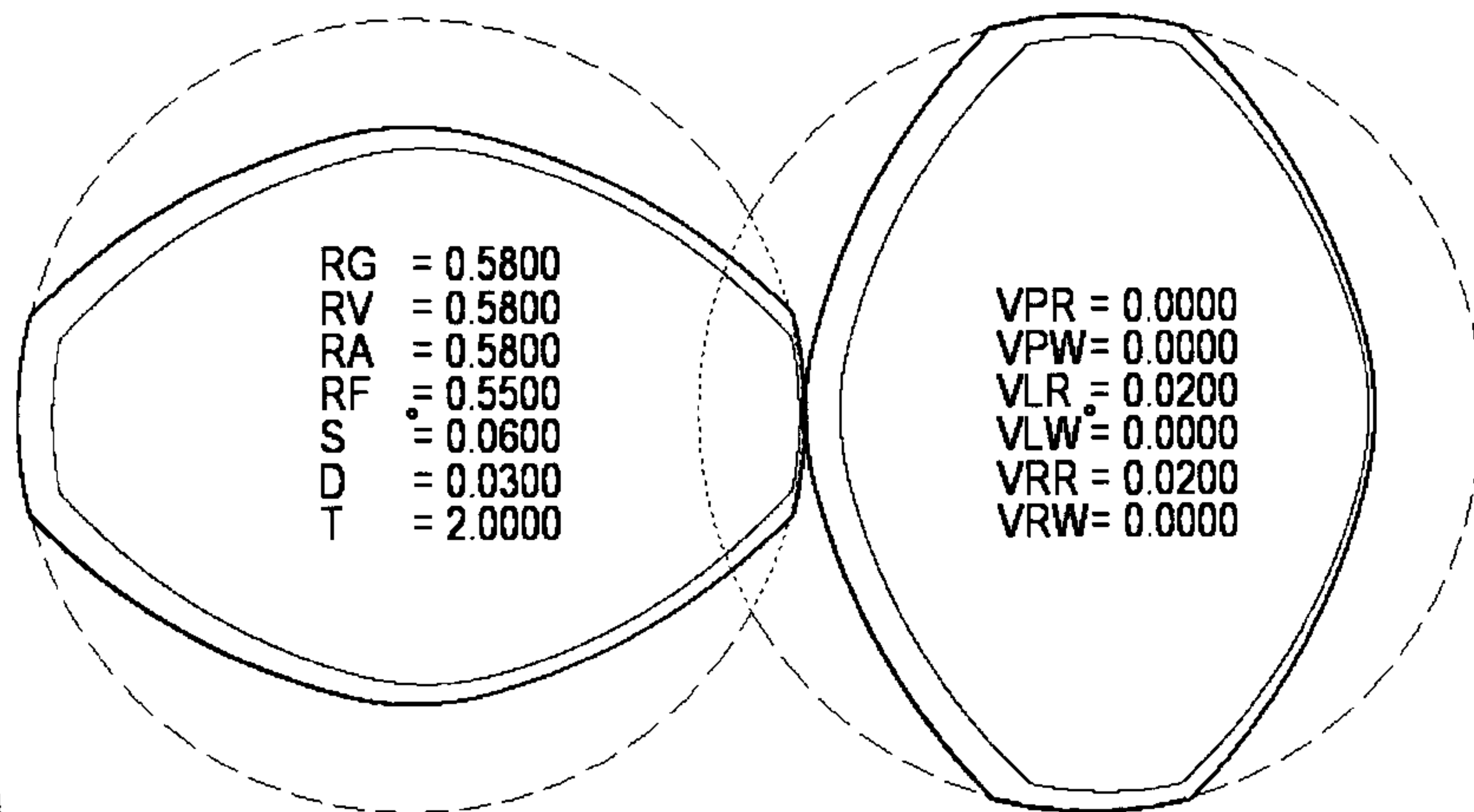


Figure 45a

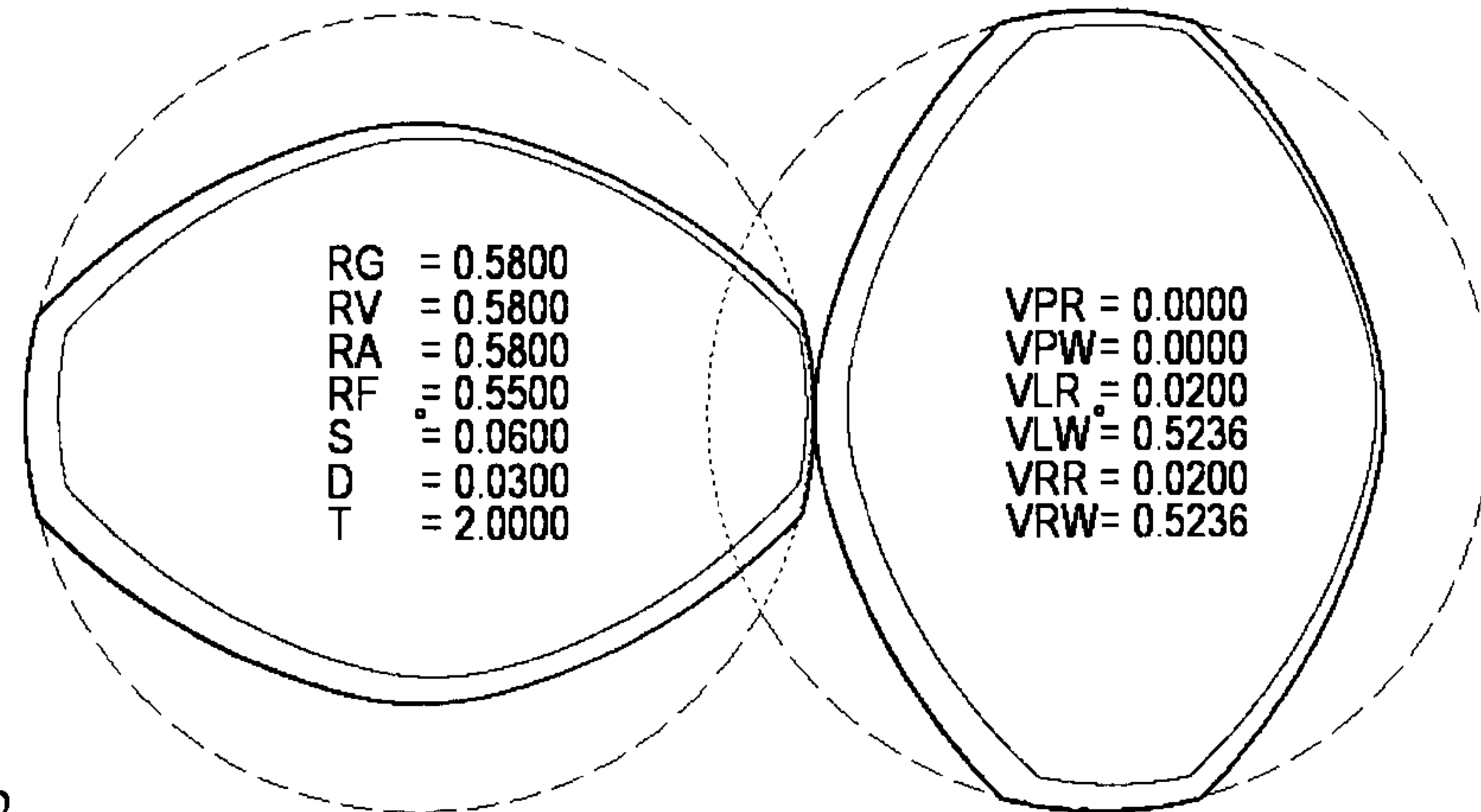


Figure 45b

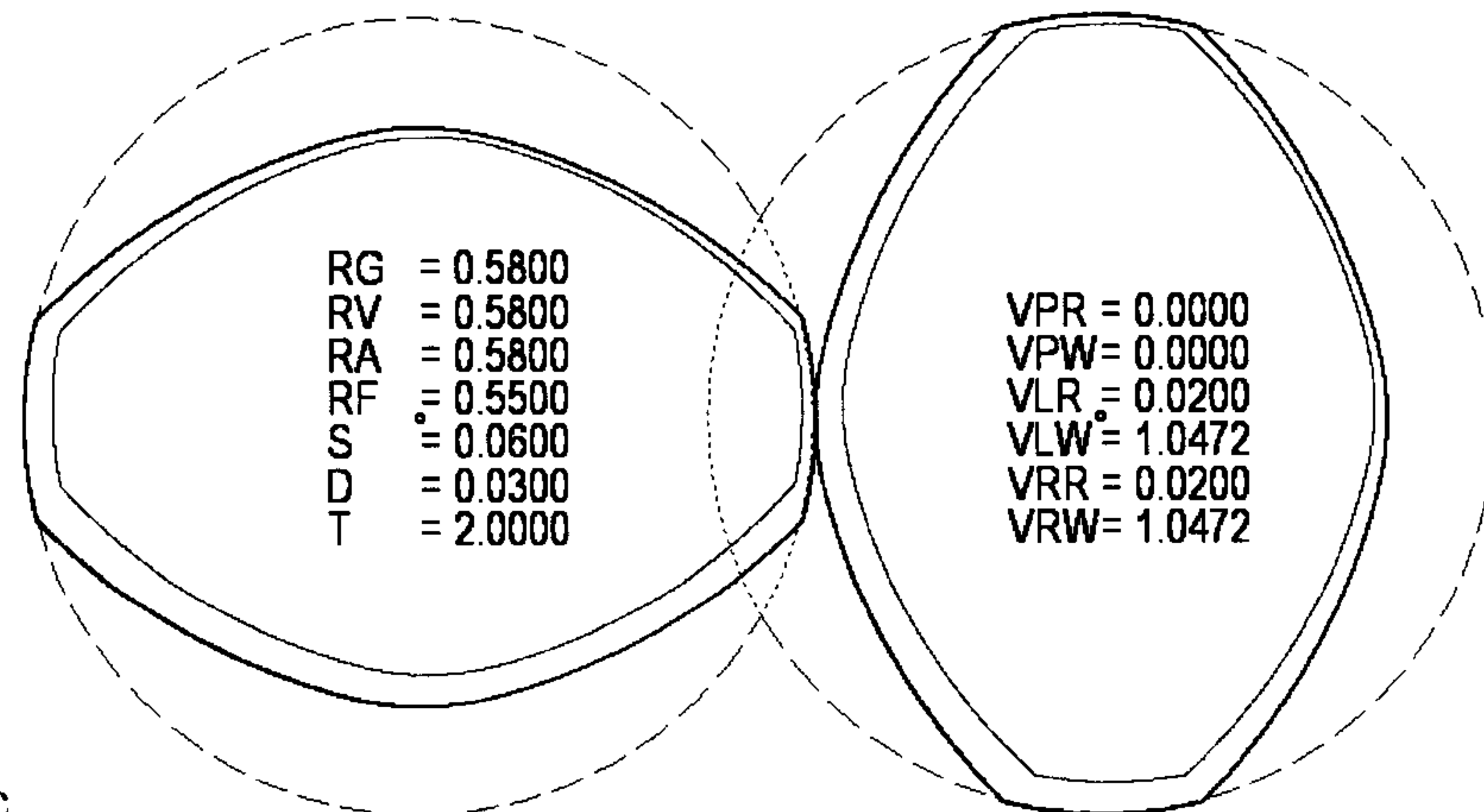


Figure 45c

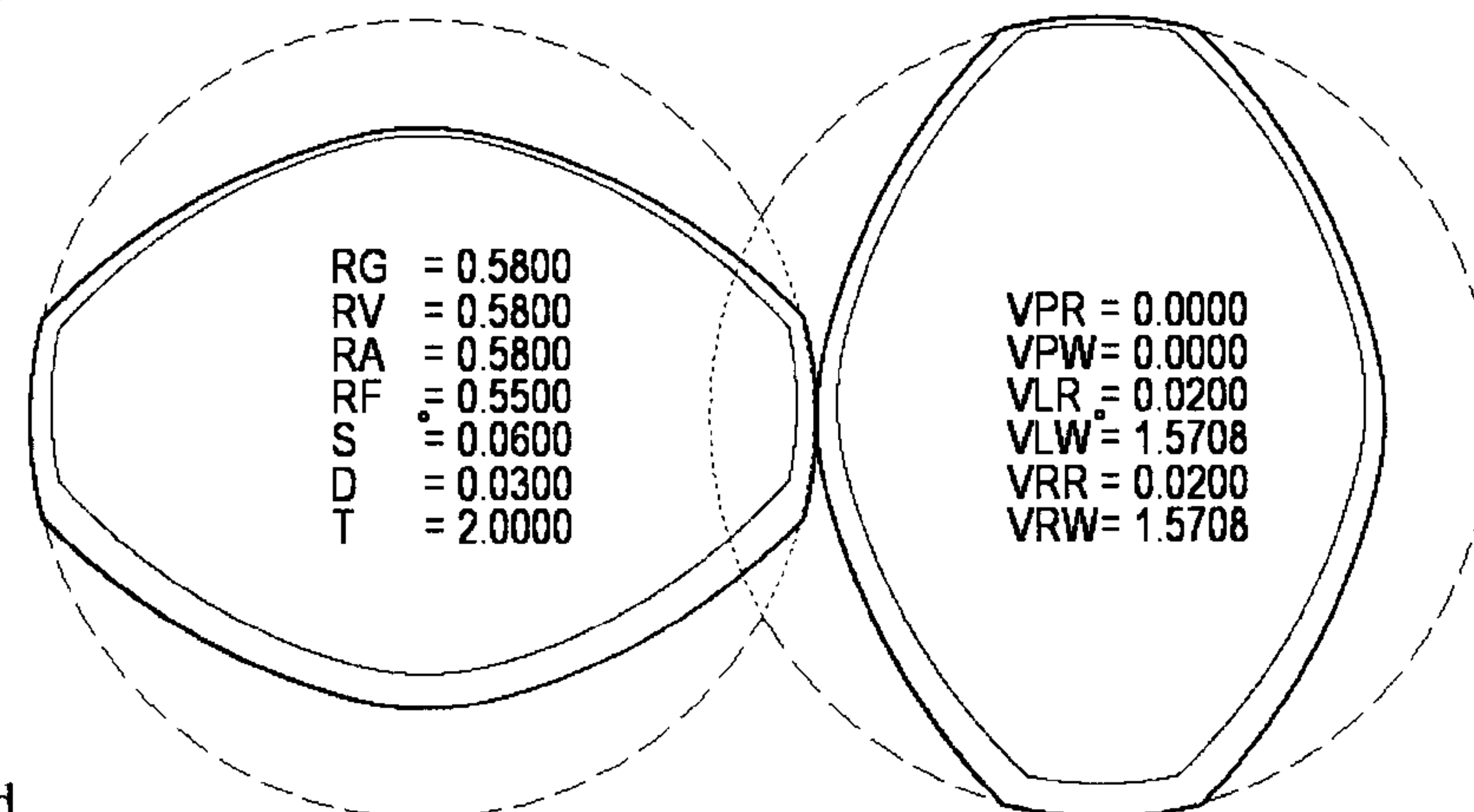


Figure 45d

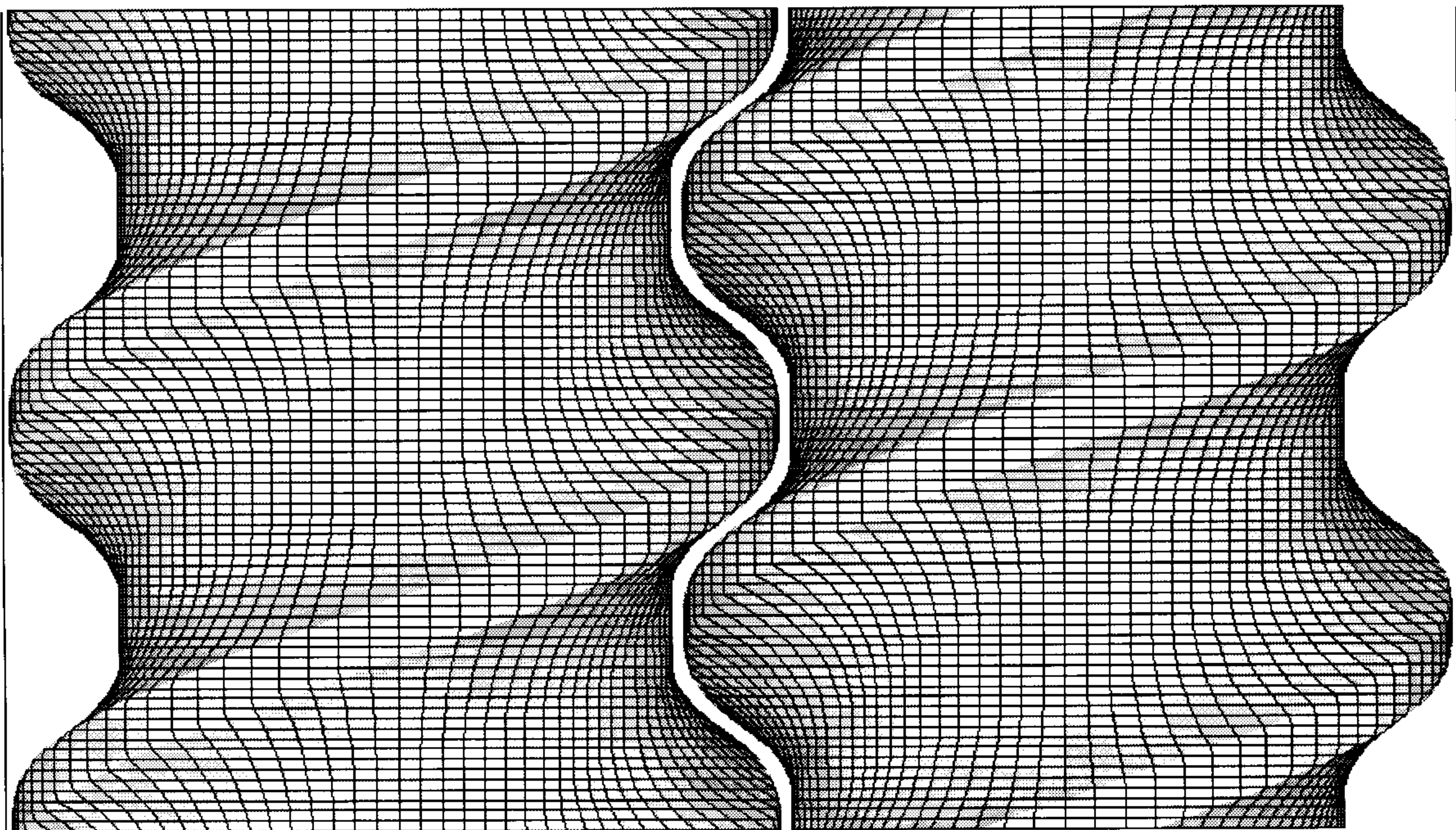
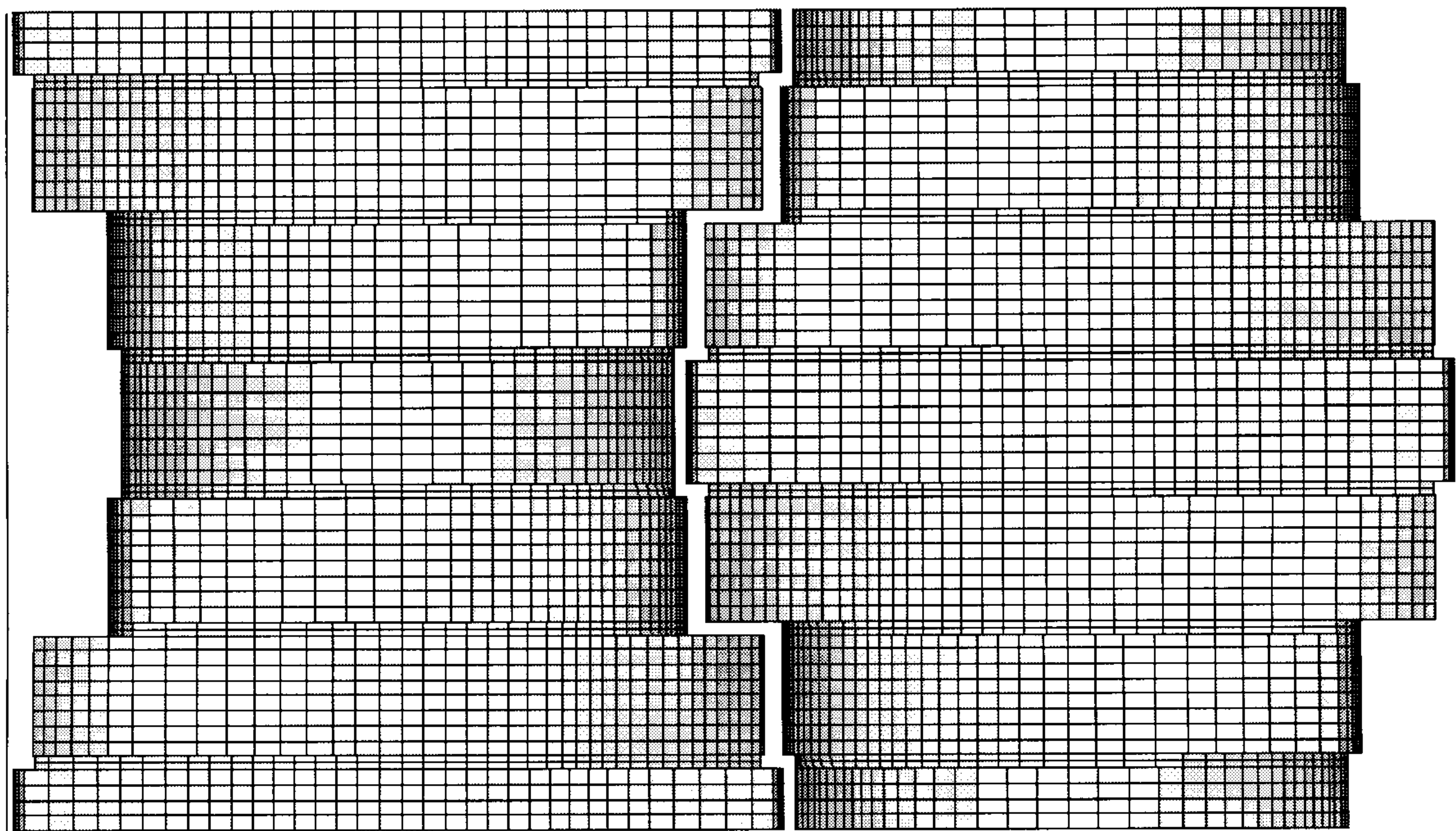


Figure 46a



5 Figure 46b

- 45 -

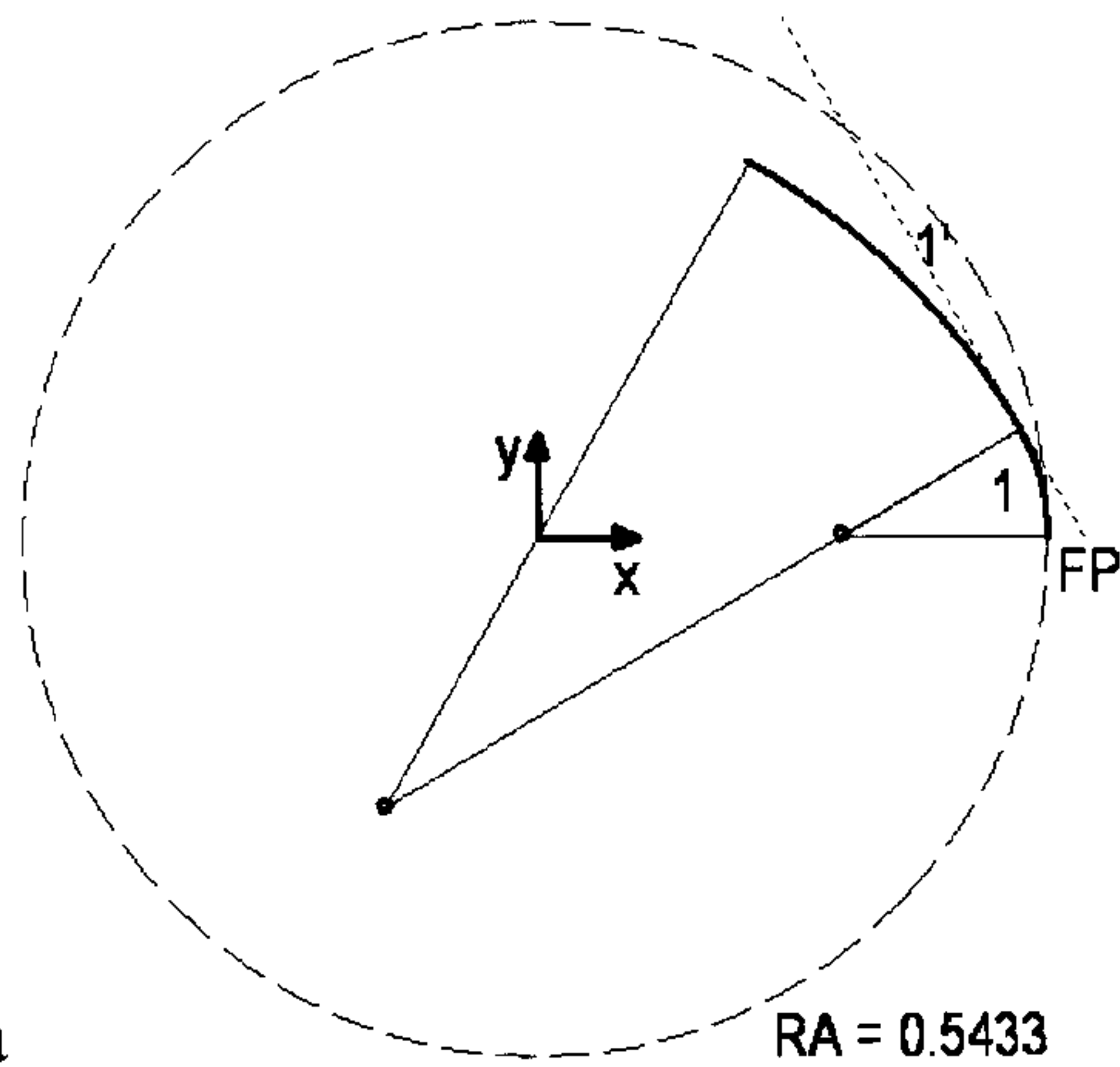


Figure 47a

$$\begin{aligned} 1) \quad R &= 0.2199 \quad M_x = 0.3234 \\ \alpha &= 0.5236 \quad M_y = 0.0000 \\ 1') \quad R &= 0.7801 \quad M_x = -0.1617 \\ \alpha &= 0.5236 \quad M_y = -0.2801 \end{aligned}$$

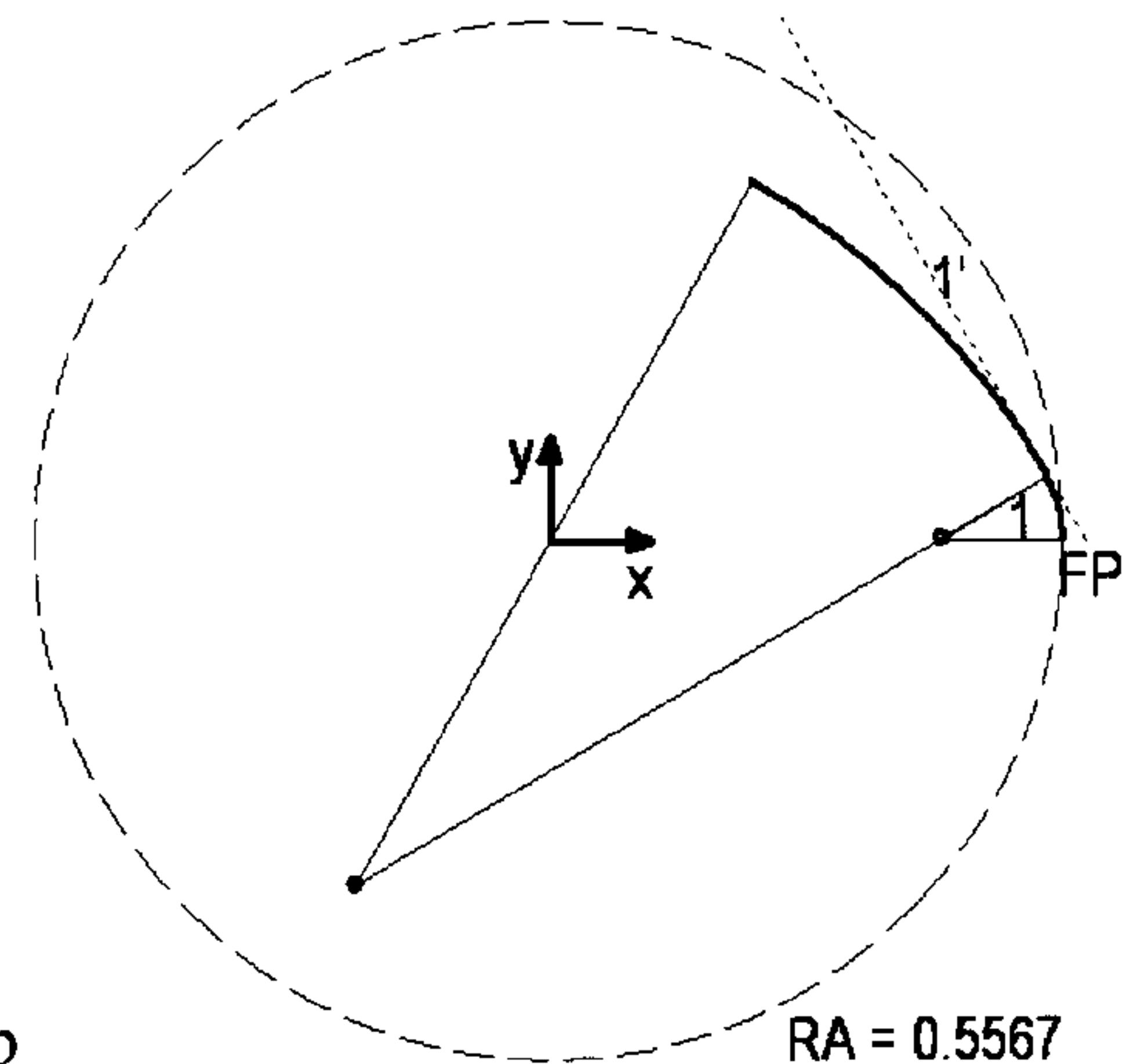


Figure 47b

$$\begin{aligned} 1) \quad R &= 0.1337 \quad M_x = 0.4229 \\ \alpha &= 0.5236 \quad M_y = 0.0000 \\ 1') \quad R &= 0.8663 \quad M_x = -0.2115 \\ \alpha &= 0.5236 \quad M_y = -0.3663 \end{aligned}$$

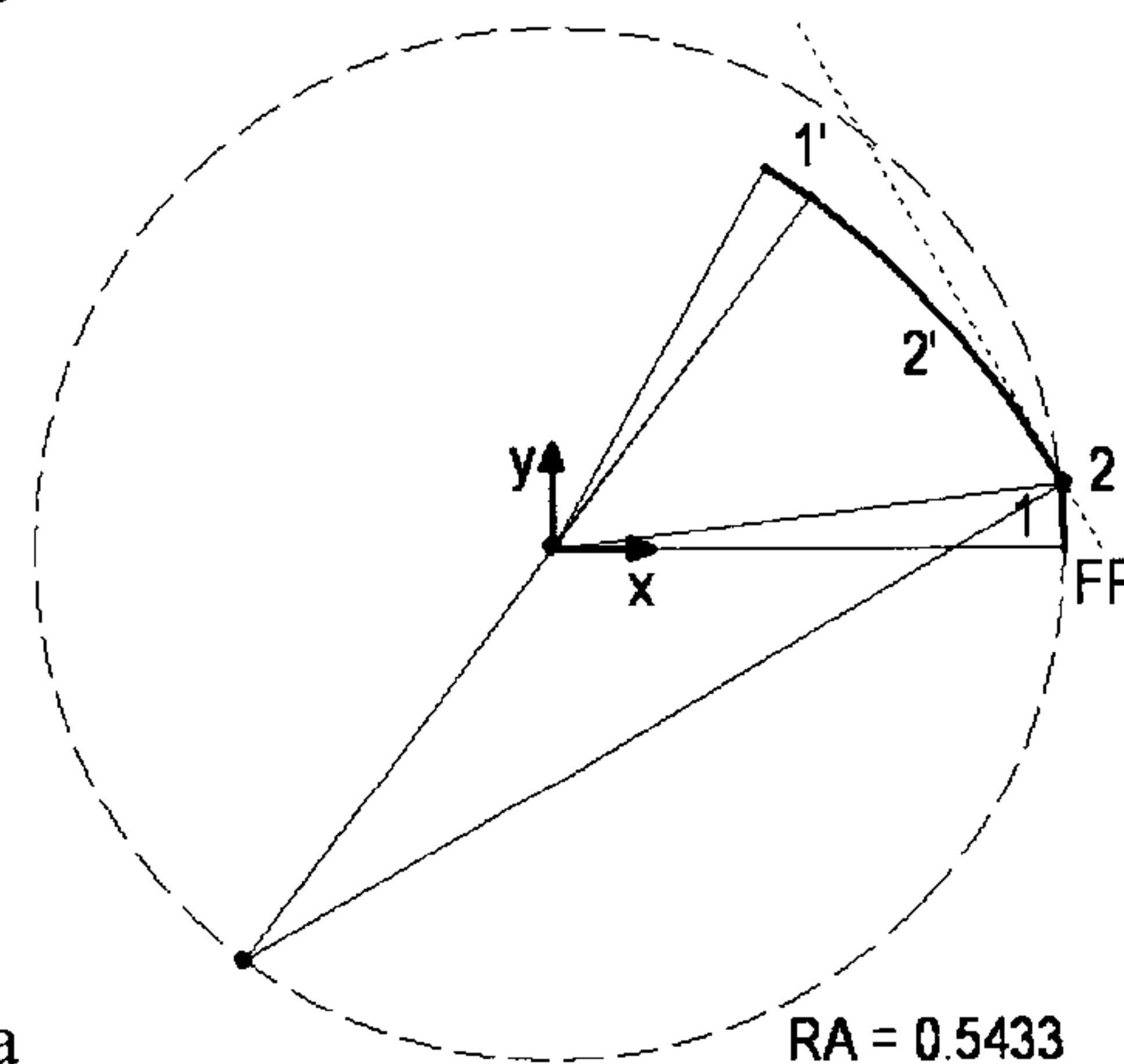


Figure 48a

$$\begin{aligned} 1) \quad R &= 0.5433 \quad M_x = 0.0000 \\ \alpha &= 0.1215 \quad M_y = 0.0000 \\ 2) \quad R &= 0.0000 \quad M_x = 0.5393 \\ \alpha &= 0.4021 \quad M_y = 0.0659 \\ 2') \quad R &= 1.0000 \quad M_x = -0.3267 \\ \alpha &= 0.4021 \quad M_y = -0.4341 \\ 1') \quad R &= 0.4567 \quad M_x = 0.0000 \\ \alpha &= 0.1215 \quad M_y = 0.0000 \end{aligned}$$

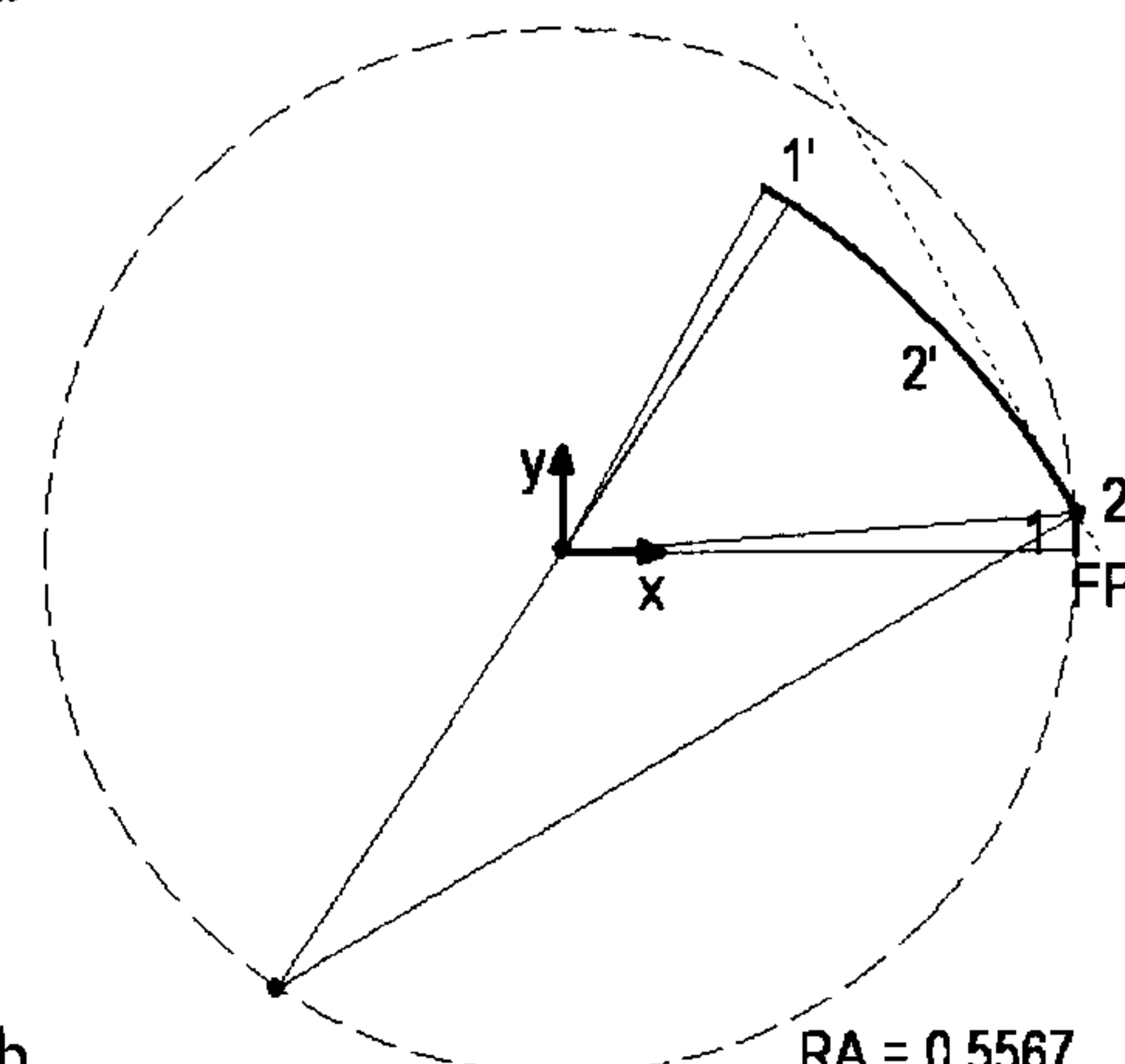


Figure 48b

$$\begin{aligned} 1) \quad R &= 0.5567 \quad M_x = 0.0000 \\ \alpha &= 0.0685 \quad M_y = 0.0000 \\ 2) \quad R &= 0.0000 \quad M_x = 0.5554 \\ \alpha &= 0.4551 \quad M_y = 0.0381 \\ 2') \quad R &= 1.0000 \quad M_x = -0.3107 \\ \alpha &= 0.4551 \quad M_y = -0.4619 \\ 1') \quad R &= 0.4433 \quad M_x = 0.0000 \\ \alpha &= 0.0685 \quad M_y = 0.0000 \end{aligned}$$

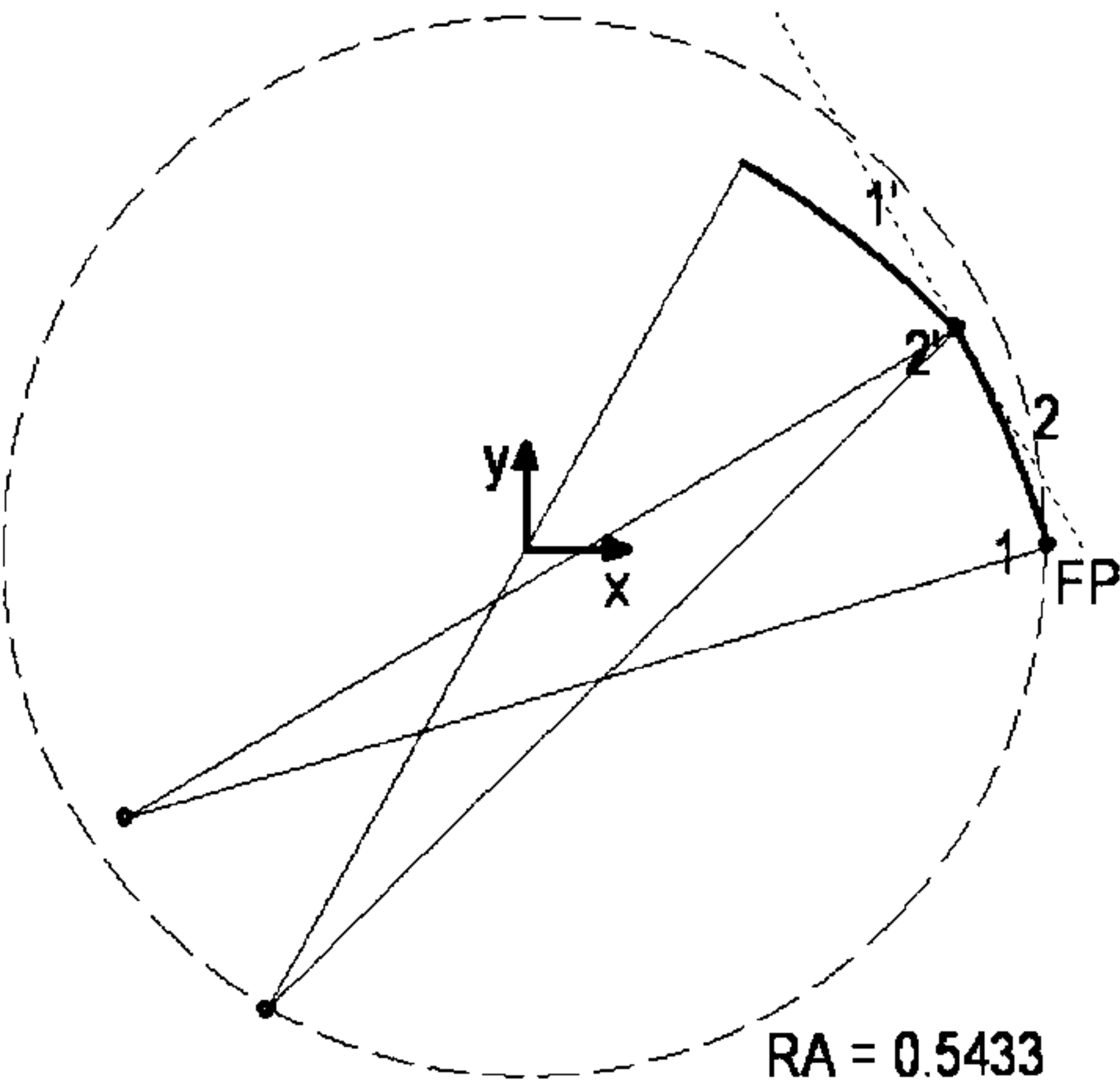


Figure 49a

- 1) $R = 0.0000$ $Mx = 0.5433$
 $\alpha = 0.2803$ $My = 0.0000$
- 2) $R = 1.0000$ $Mx = -0.4176$
 $\alpha = 0.2433$ $My = -0.2766$
- 2') $R = 0.0000$ $Mx = 0.4484$
 $\alpha = 0.2433$ $My = 0.2234$
- 1') $R = 1.0000$ $Mx = -0.2717$
 $\alpha = 0.2803$ $My = -0.4705$

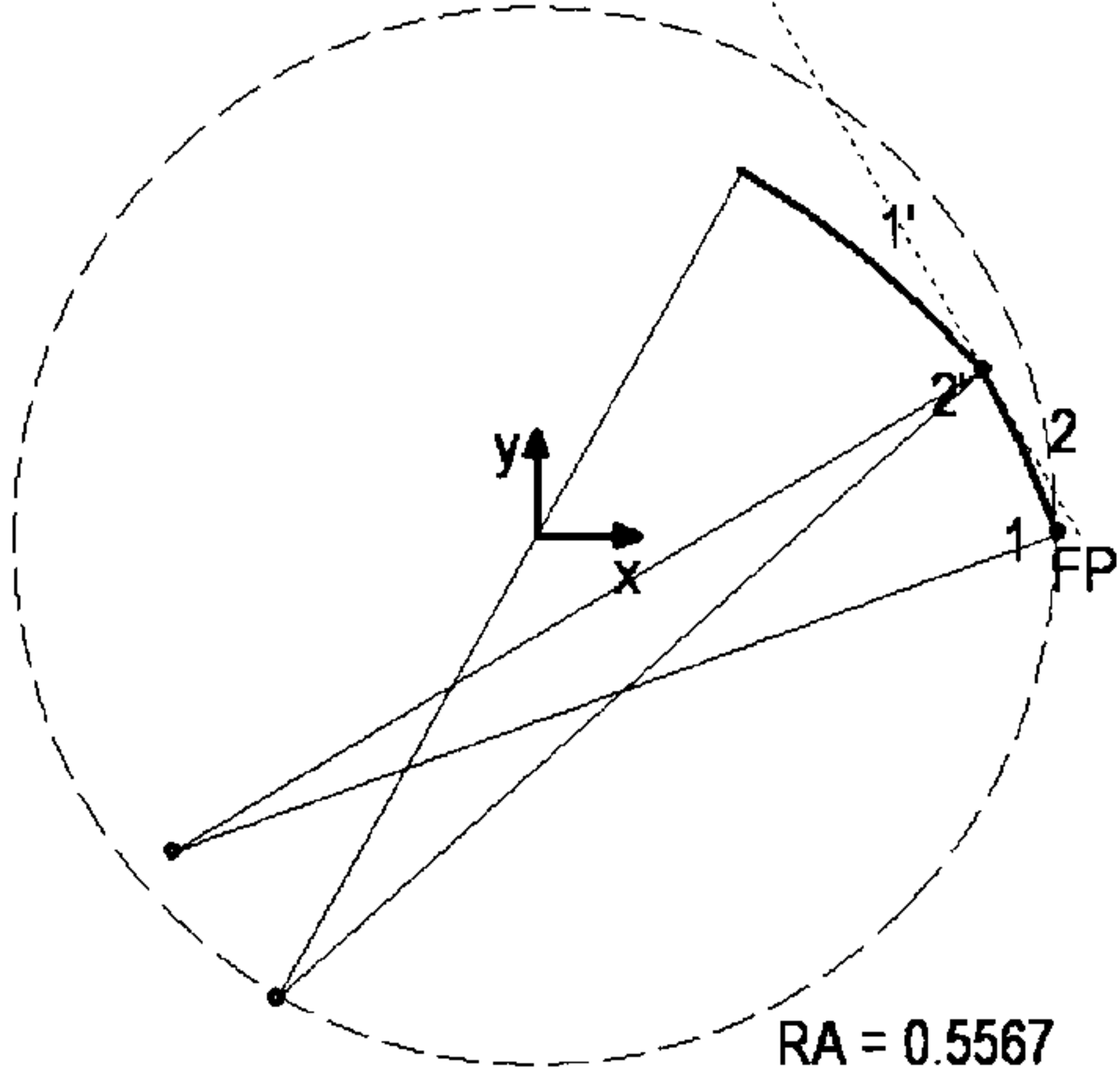


Figure 49b

- 1) $R = 0.0000$ $Mx = 0.5567$
 $\alpha = 0.3340$ $My = 0.0000$
- 2) $R = 1.0000$ $Mx = -0.3881$
 $\alpha = 0.1896$ $My = -0.3278$
- 2') $R = 0.0000$ $Mx = 0.4779$
 $\alpha = 0.1896$ $My = 0.1722$
- 1') $R = 1.0000$ $Mx = -0.2783$
 $\alpha = 0.3340$ $My = -0.4821$

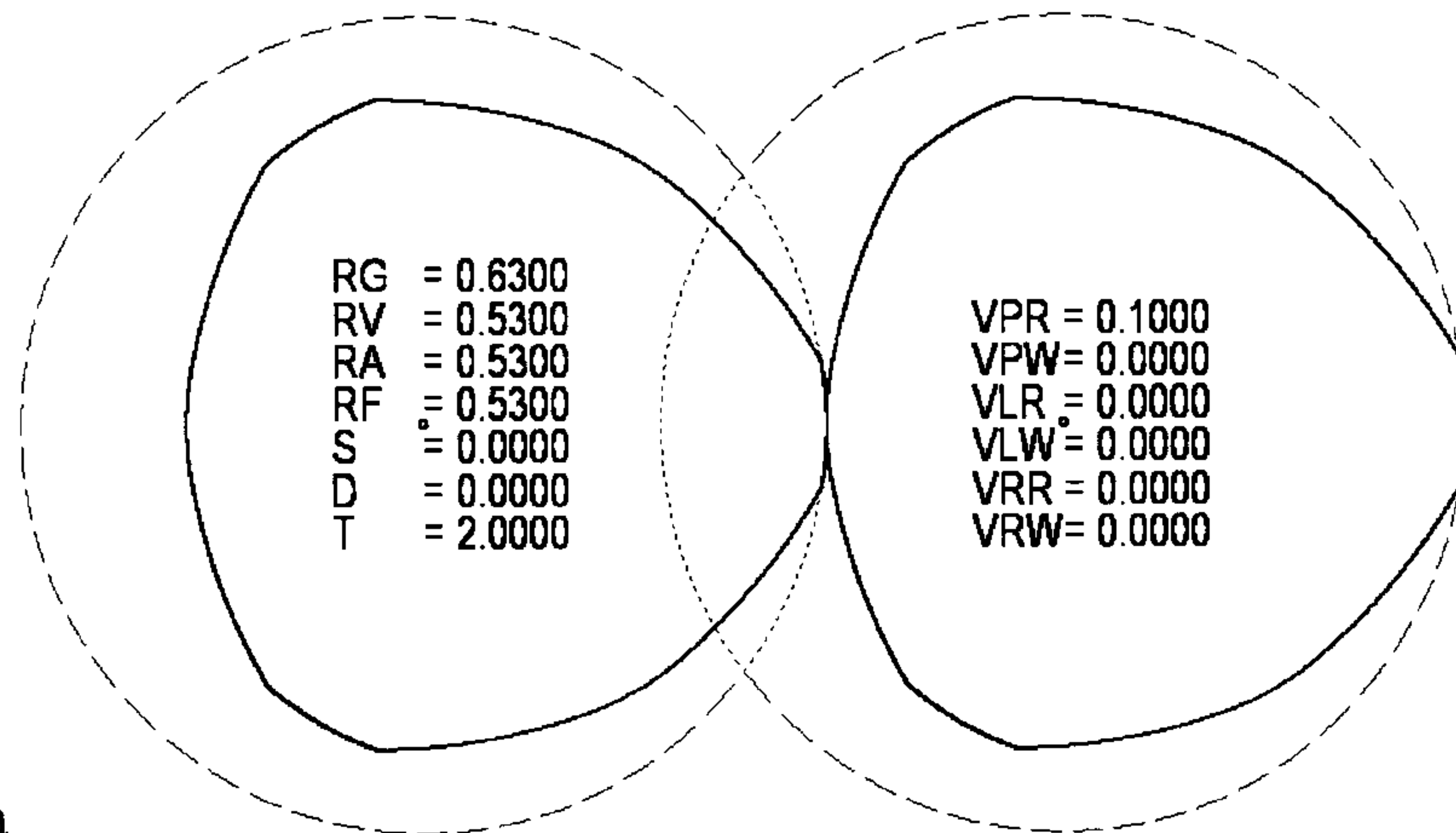


Figure 50a

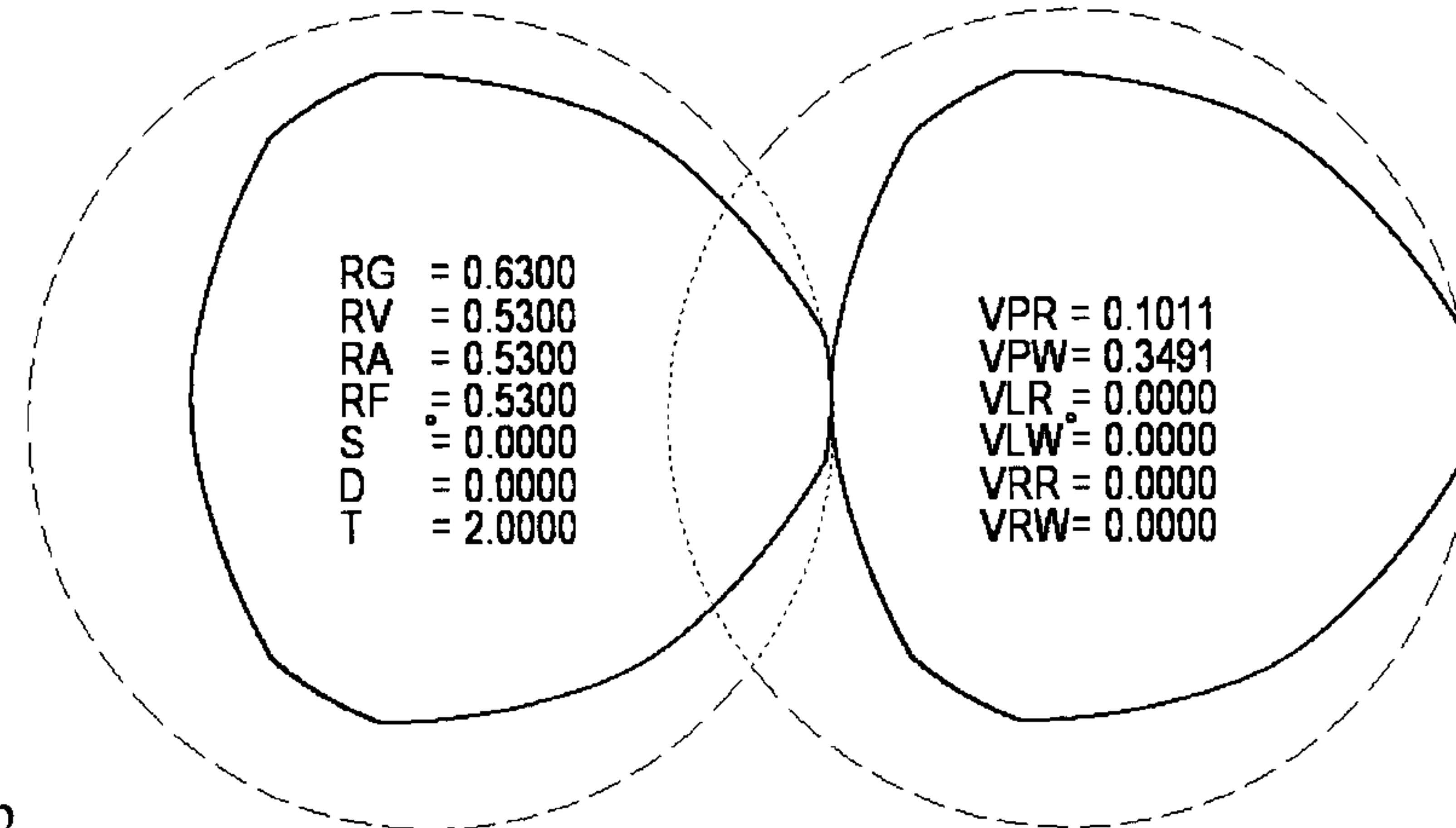


Figure 50b

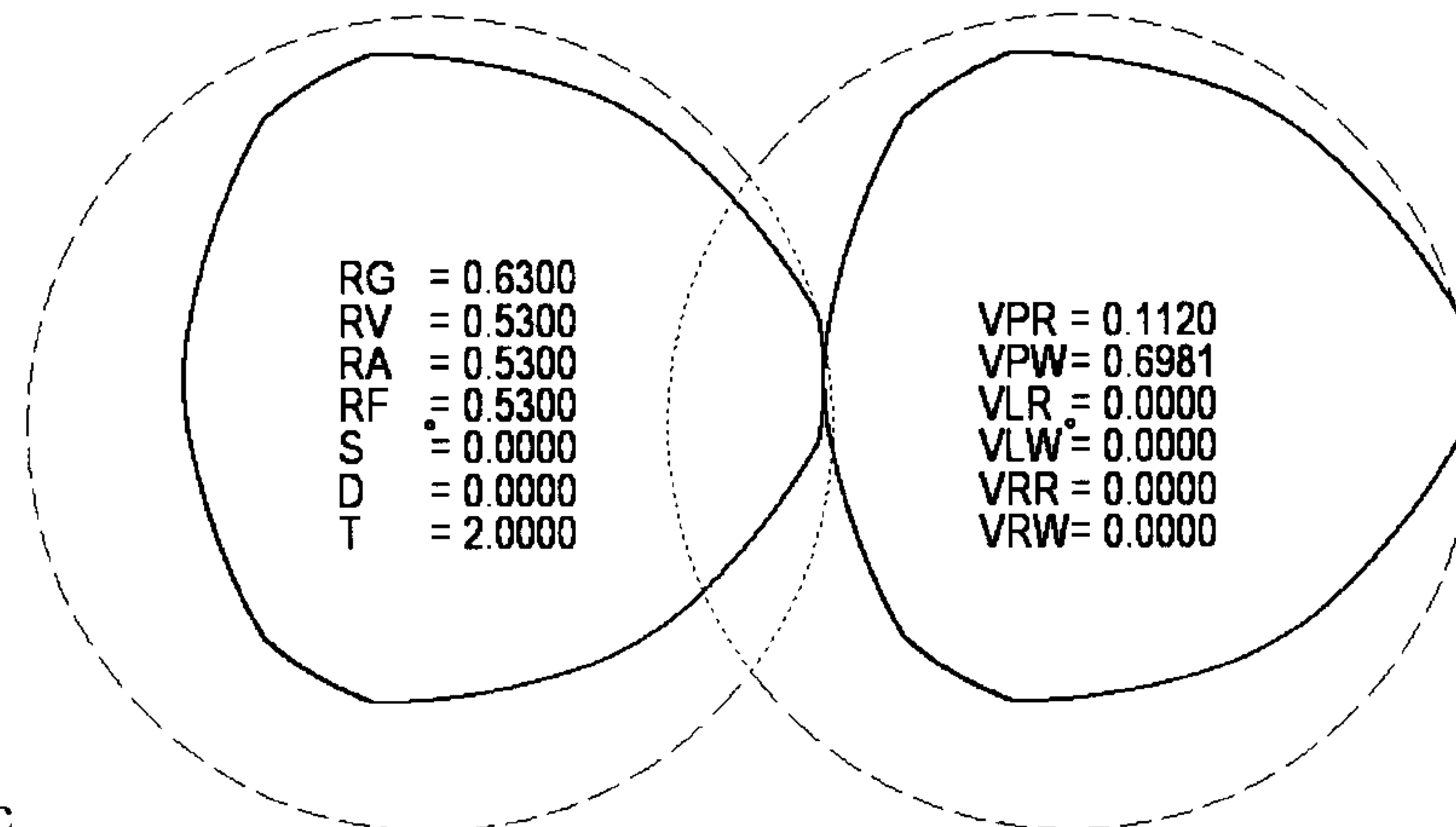


Figure 50c

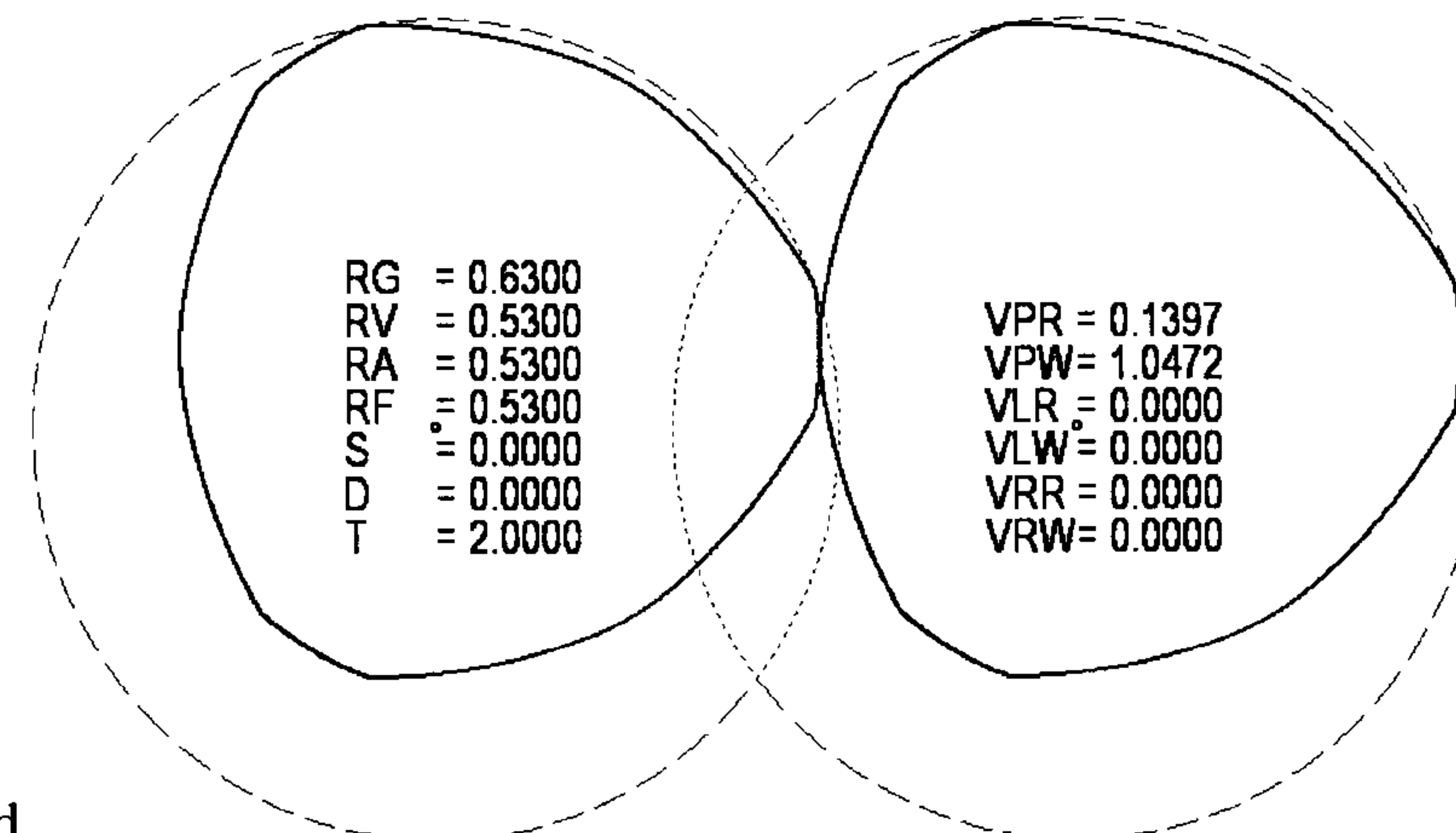


Figure 50d

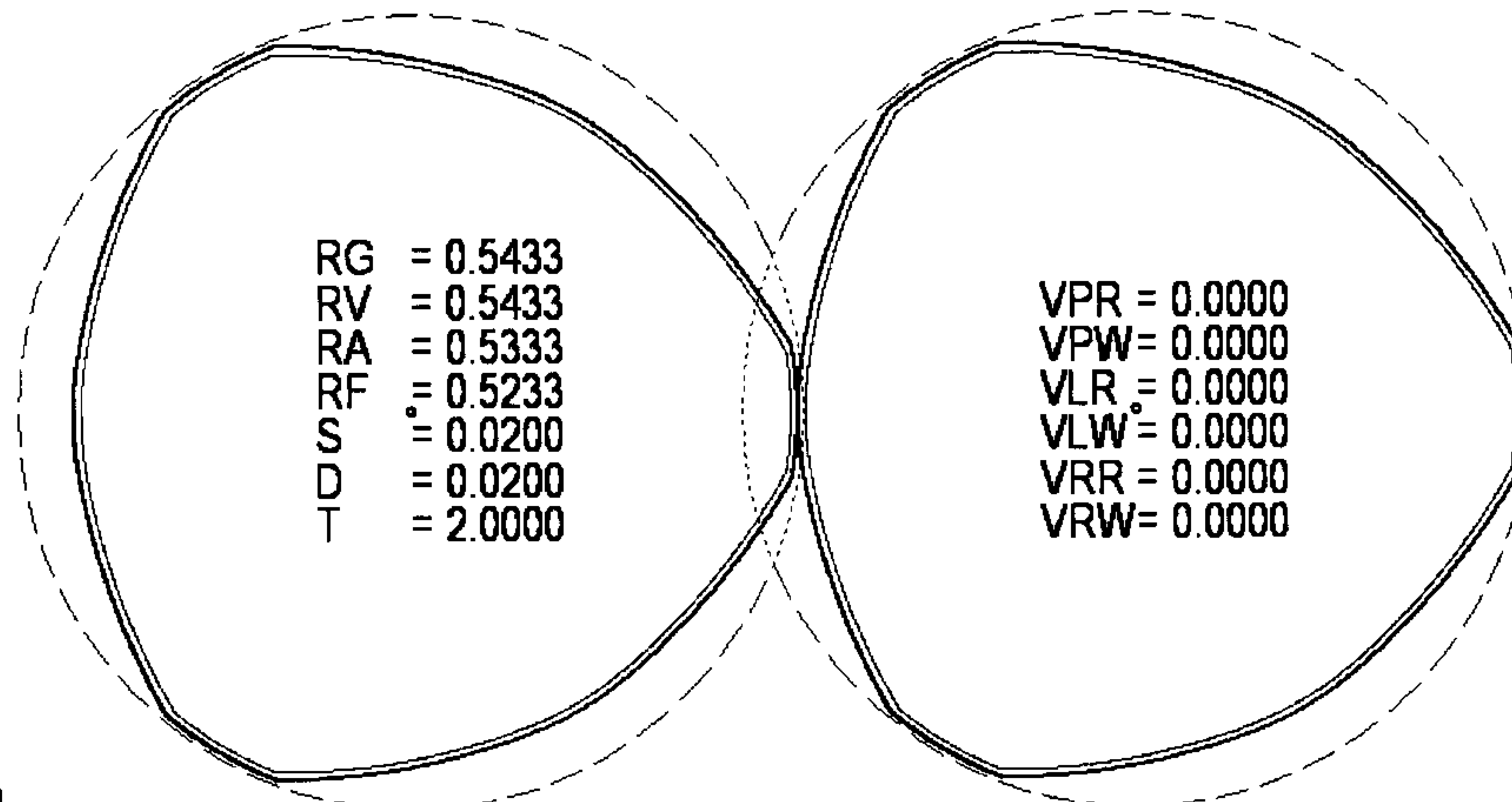


Figure 51a

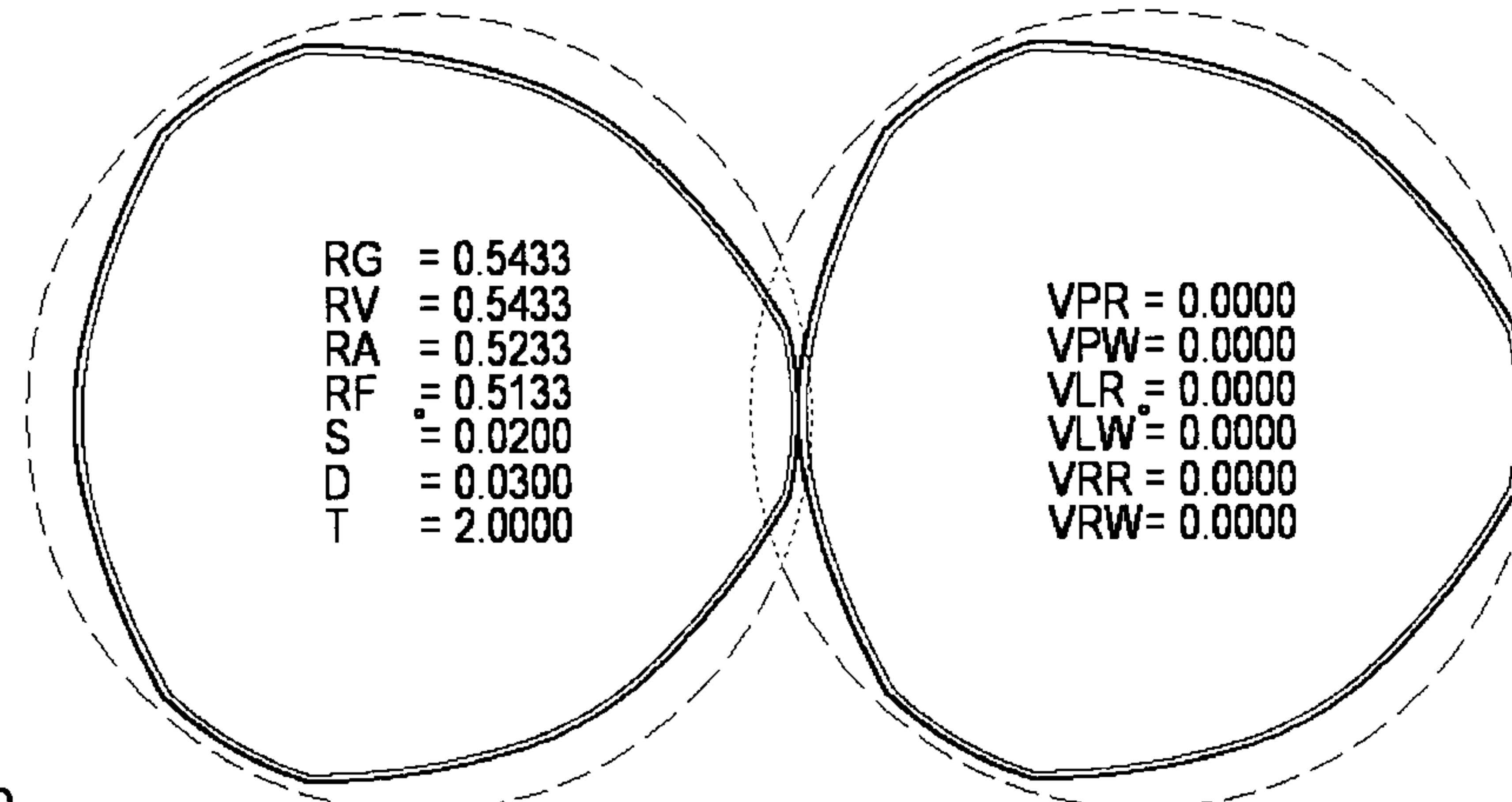


Figure 51b

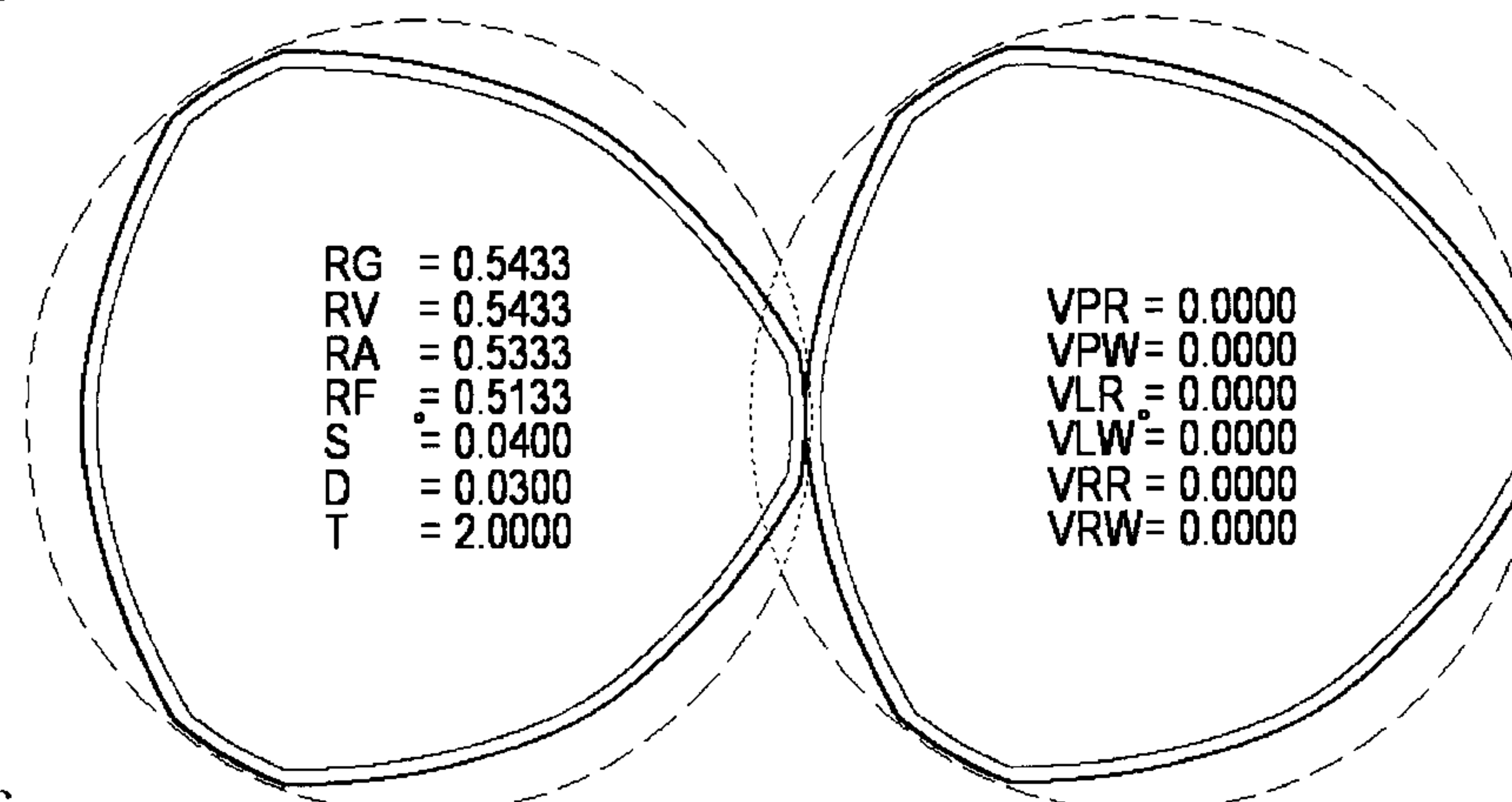


Figure 51c

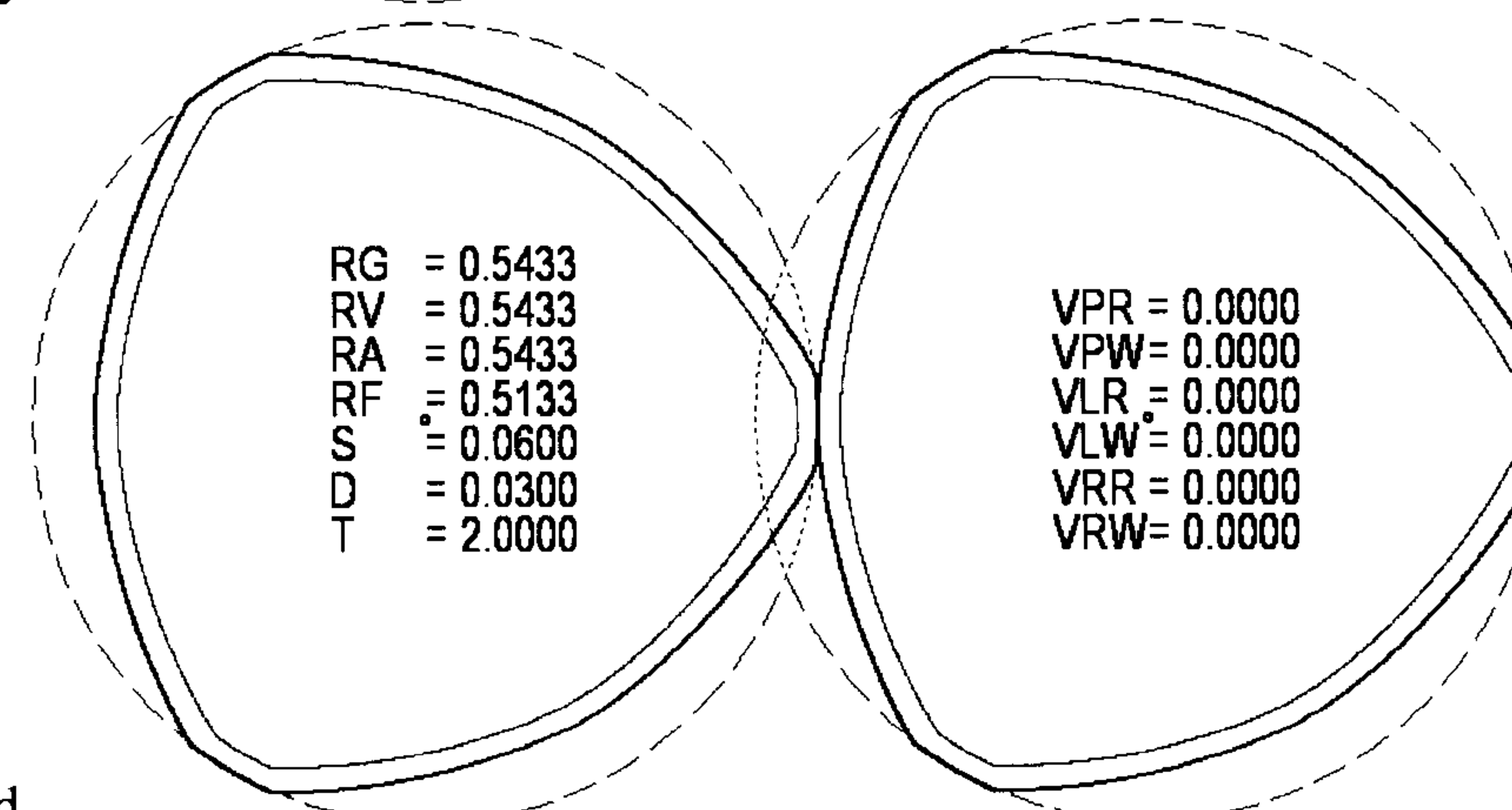


Figure 51d

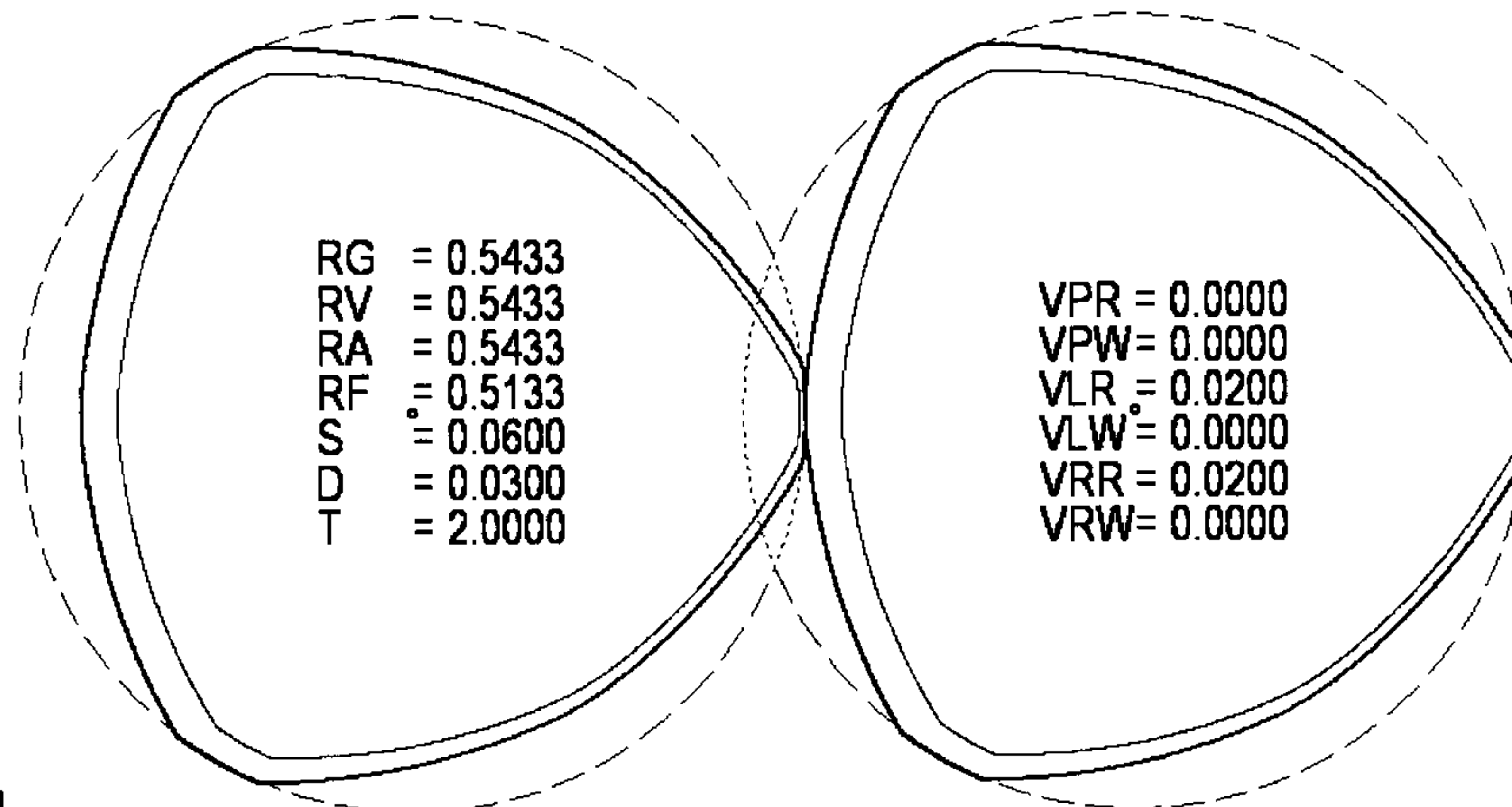


Figure 52a

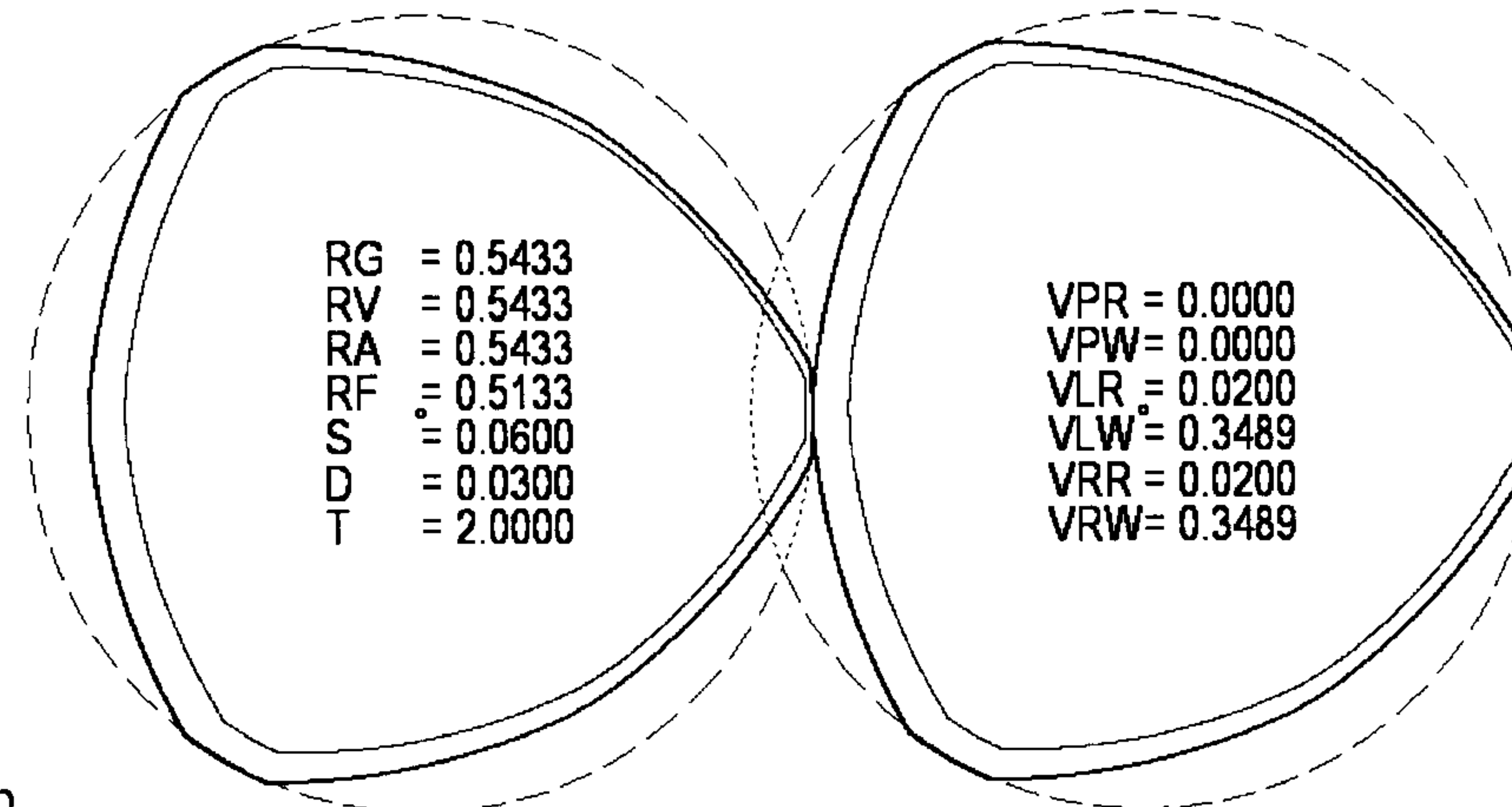


Figure 52b

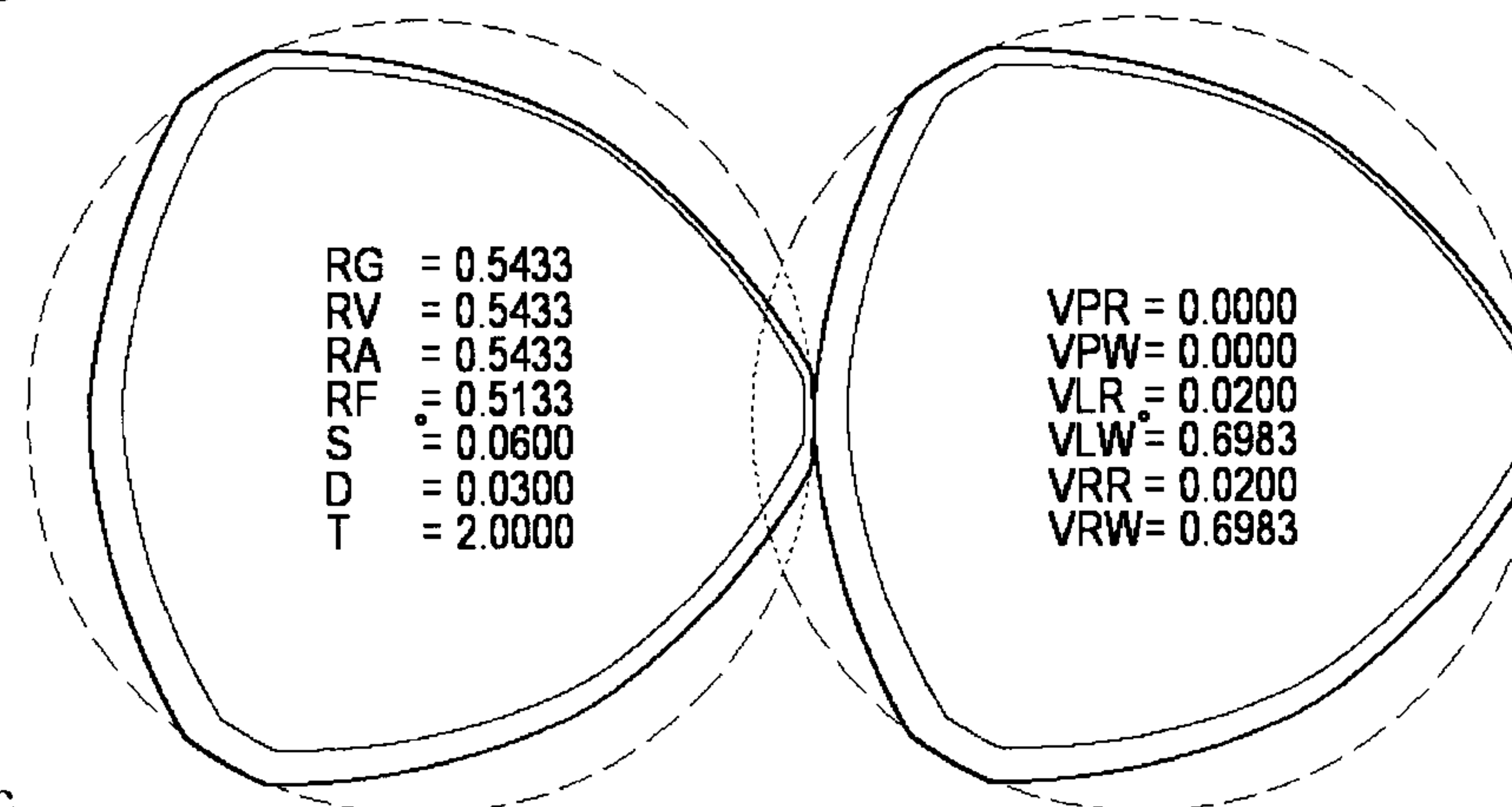


Figure 52c

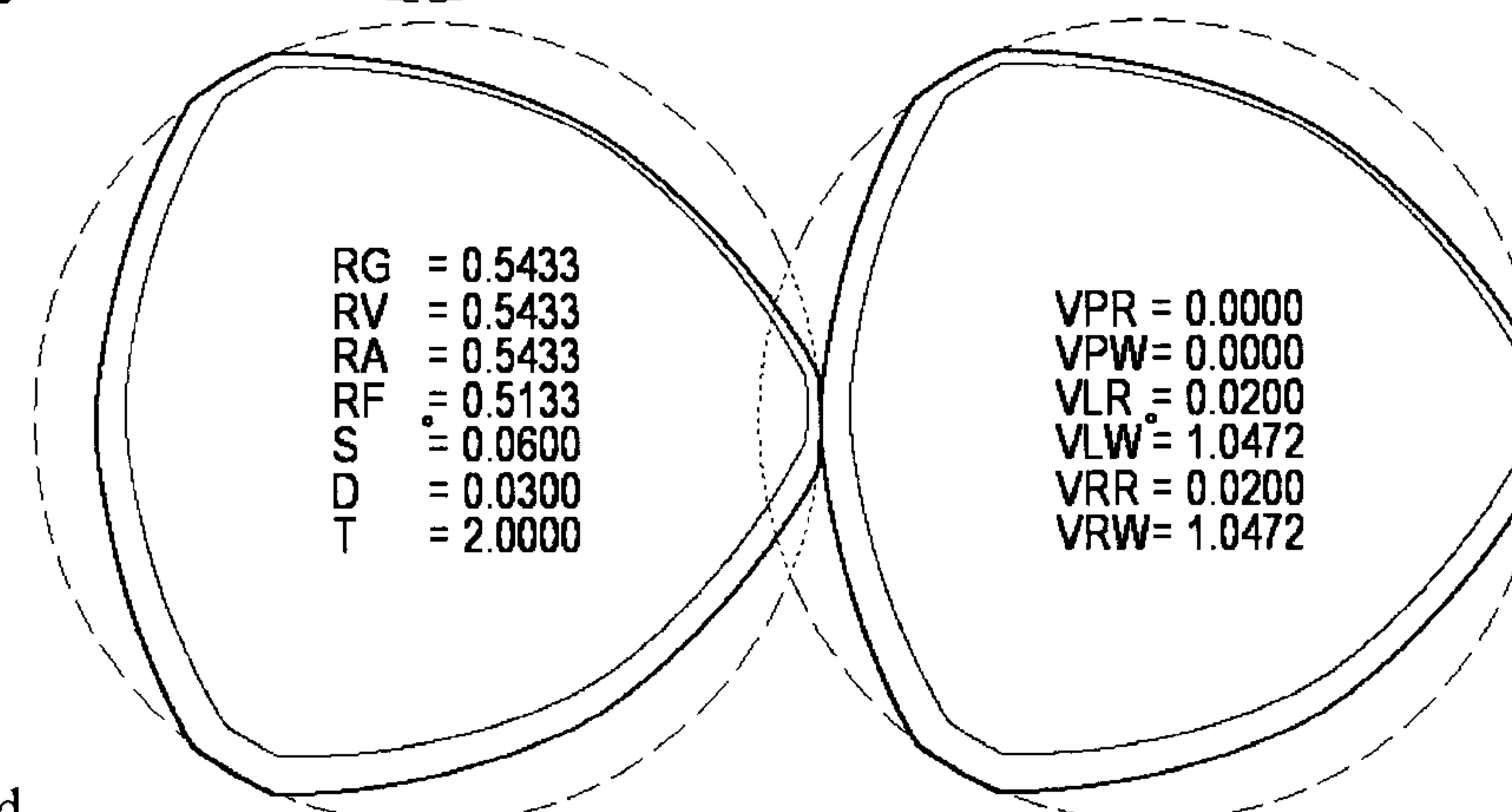


Figure 52d

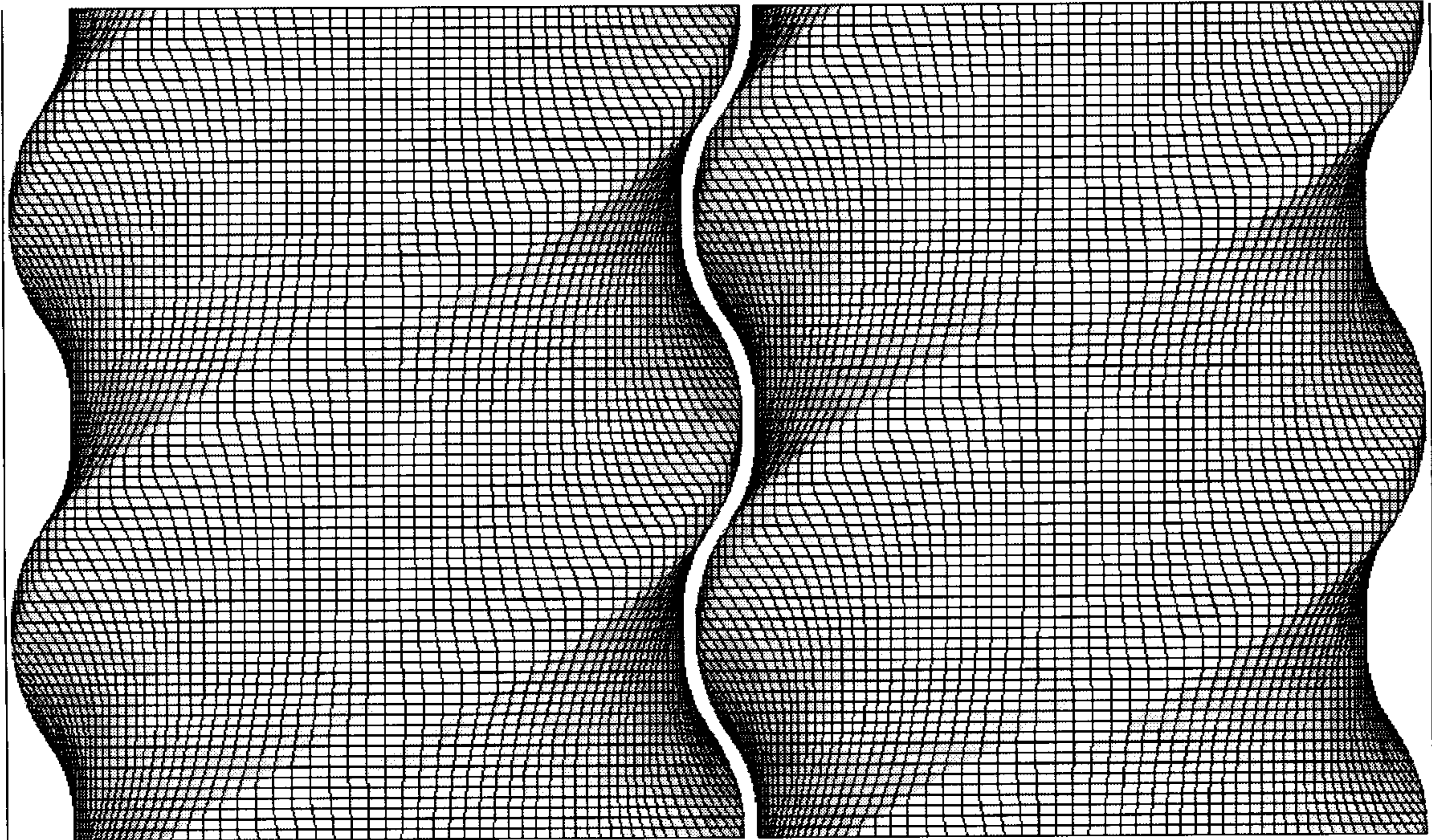
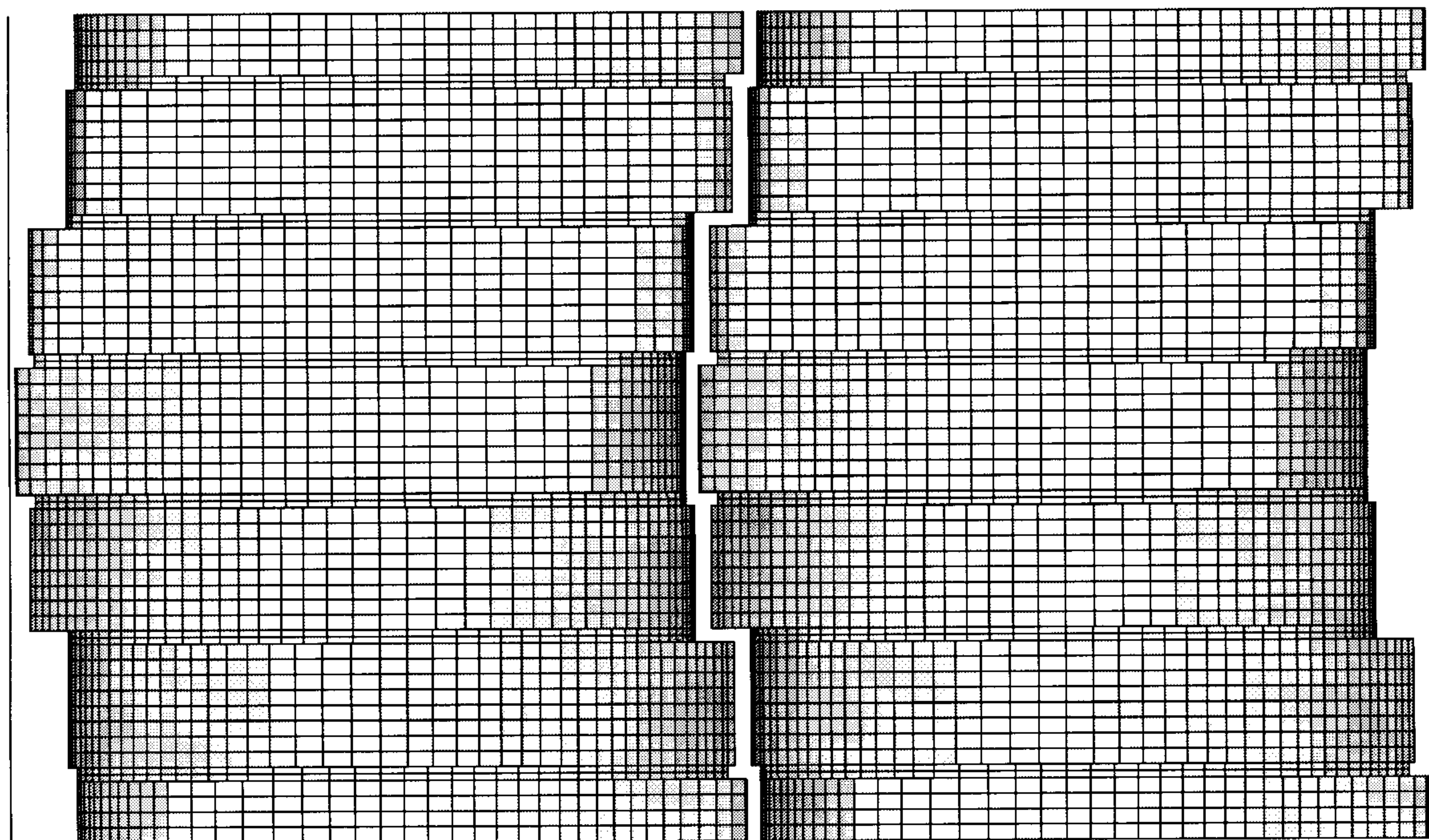
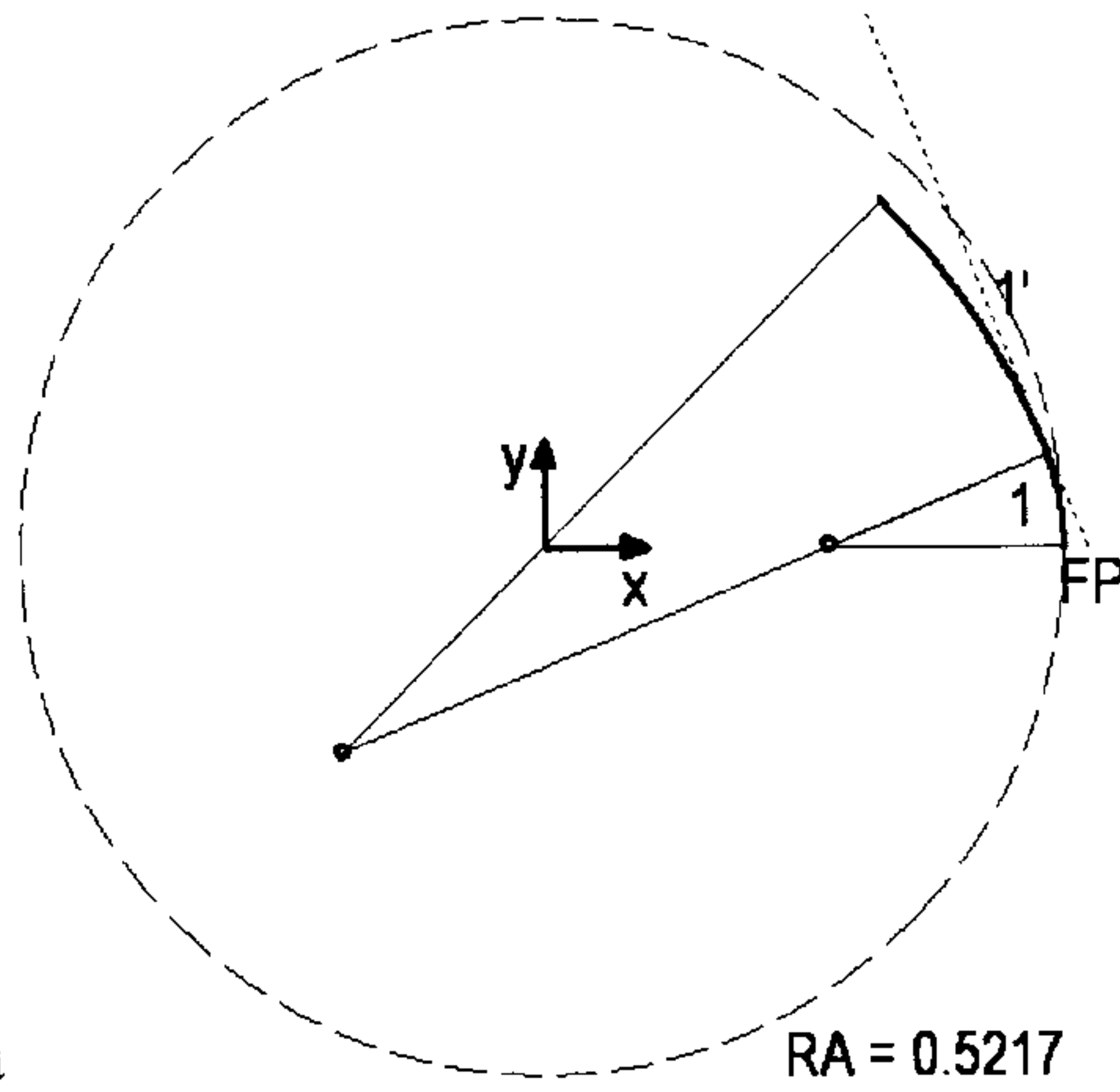


Figure 53a

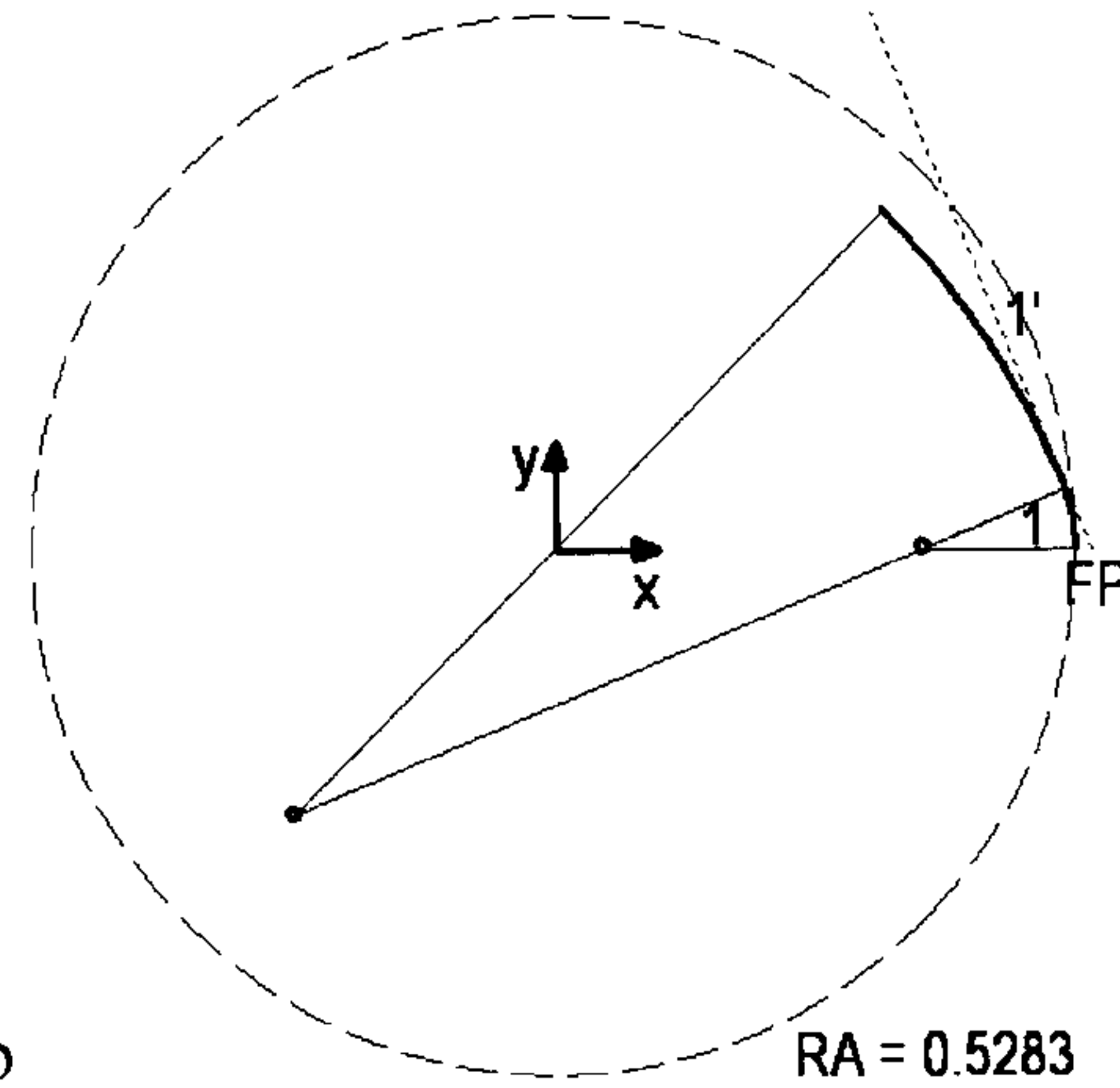


5 Figure 53b

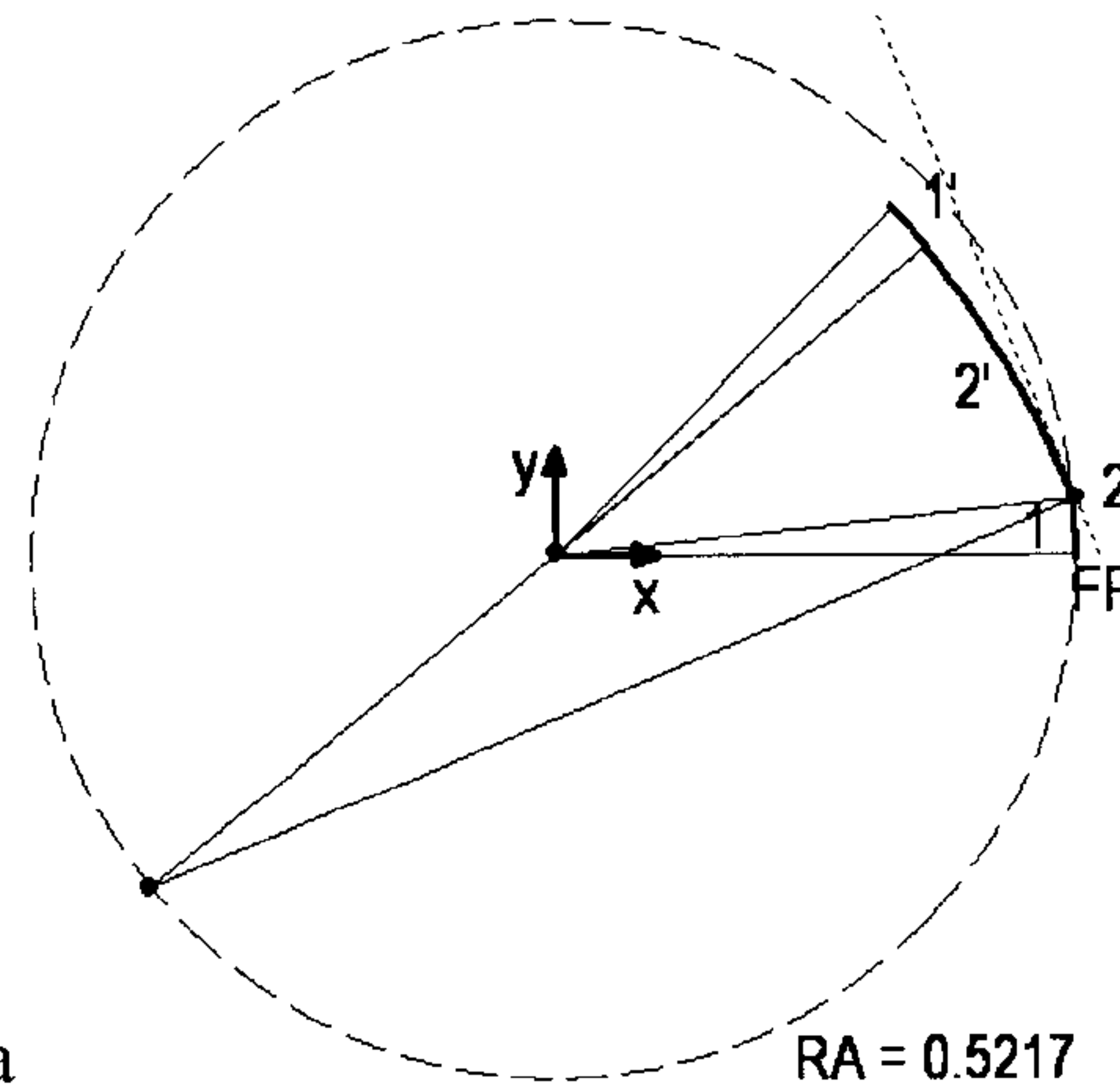
- 51 -



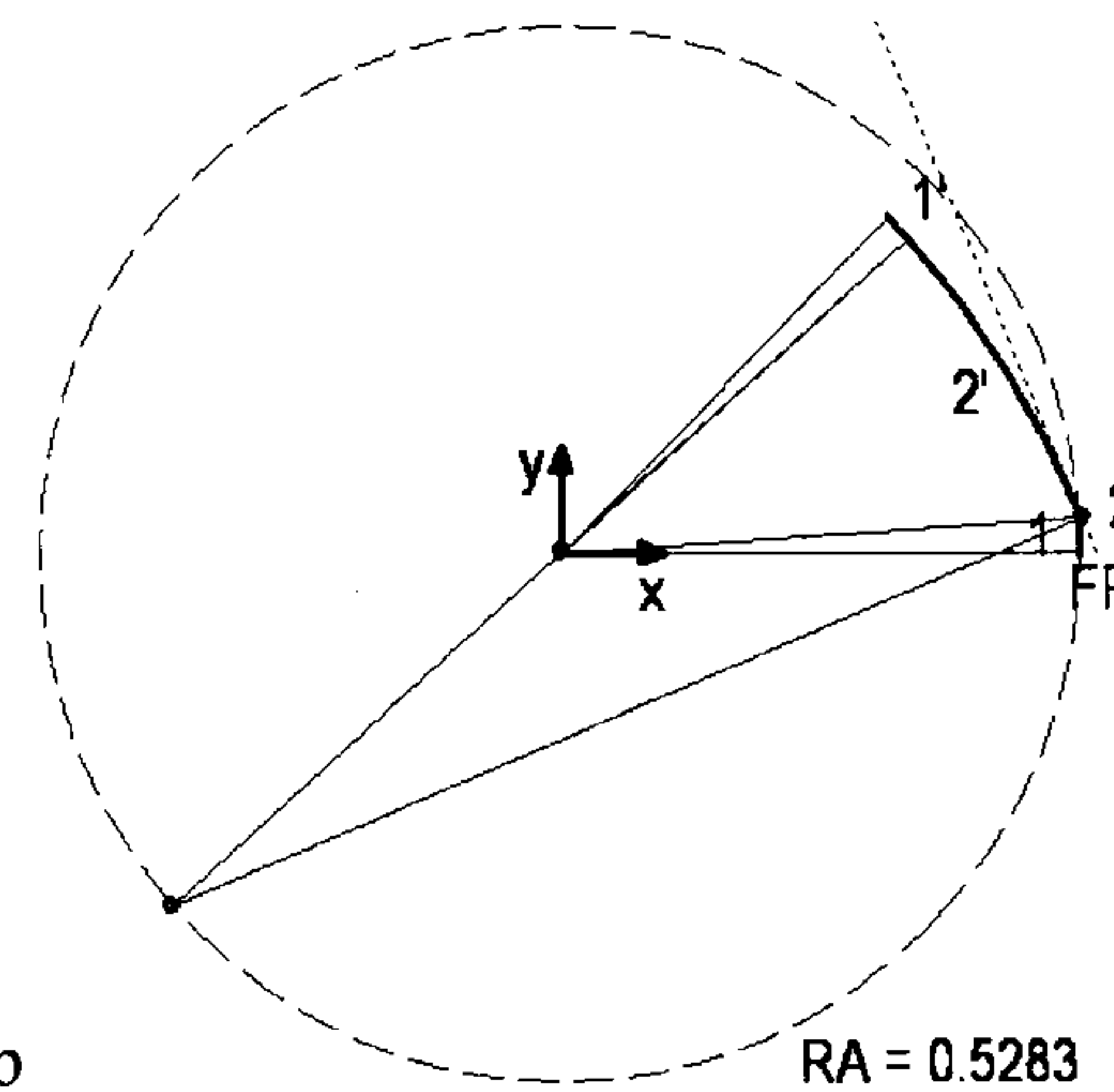
$$\begin{aligned} 1) \quad R &= 0.2371 \quad Mx = 0.2845 \\ \alpha &= 0.3927 \quad My = 0.0000 \\ 1') \quad R &= 0.7629 \quad Mx = -0.2012 \\ \alpha &= 0.3927 \quad My = -0.2012 \end{aligned}$$



$$\begin{aligned} 1) \quad R &= 0.1562 \quad Mx = 0.3722 \\ \alpha &= 0.3927 \quad My = 0.0000 \\ 1') \quad R &= 0.8438 \quad Mx = -0.2632 \\ \alpha &= 0.3927 \quad My = -0.2632 \end{aligned}$$



$$\begin{aligned} 1) \quad R &= 0.5217 \quad Mx = 0.0000 \\ \alpha &= 0.1035 \quad My = 0.0000 \\ 2) \quad R &= 0.0000 \quad Mx = 0.5189 \\ \alpha &= 0.2892 \quad My = 0.0539 \\ 2') \quad R &= 1.0000 \quad Mx = -0.4050 \\ \alpha &= 0.2892 \quad My = -0.3288 \\ 1') \quad R &= 0.4783 \quad Mx = 0.0000 \\ \alpha &= 0.1035 \quad My = 0.0000 \end{aligned}$$



$$\begin{aligned} 1) \quad R &= 0.5283 \quad Mx = 0.0000 \\ \alpha &= 0.0637 \quad My = 0.0000 \\ 2) \quad R &= 0.0000 \quad Mx = 0.5273 \\ \alpha &= 0.3290 \quad My = 0.0337 \\ 2') \quad R &= 1.0000 \quad Mx = -0.3966 \\ \alpha &= 0.3290 \quad My = -0.3490 \\ 1') \quad R &= 0.4717 \quad Mx = 0.0000 \\ \alpha &= 0.0637 \quad My = 0.0000 \end{aligned}$$

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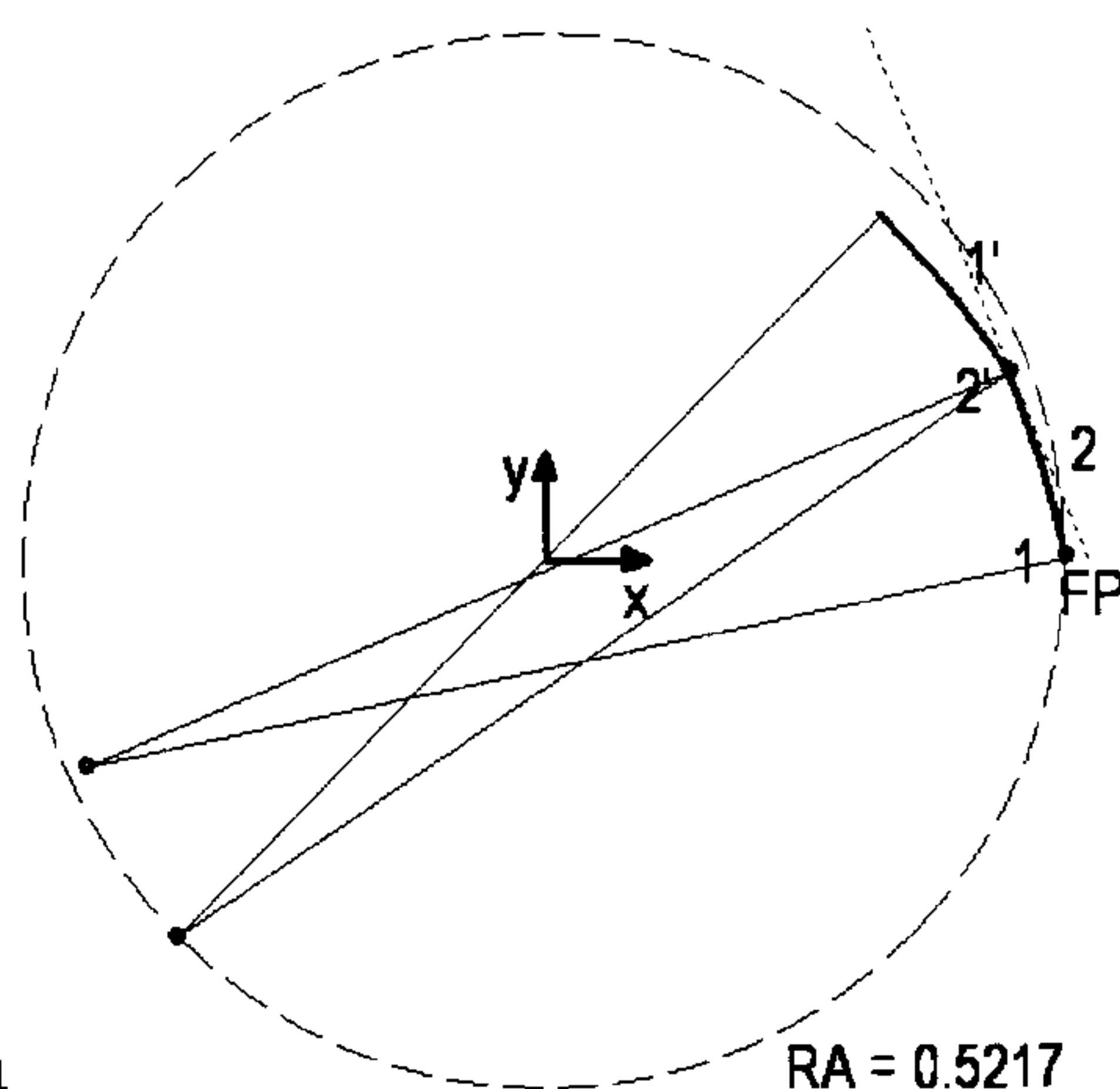


Figure 56a

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.5217$ |
| | $\alpha = 0.2024$ | $My = 0.0000$ |
| 2) | $R = 1.0000$ | $Mx = -0.4579$ |
| | $\alpha = 0.1903$ | $My = -0.2010$ |
| 2') | $R = 0.0000$ | $Mx = 0.4659$ |
| | $\alpha = 0.1903$ | $My = 0.1816$ |
| 1') | $R = 1.0000$ | $Mx = -0.3689$ |
| | $\alpha = 0.2024$ | $My = -0.3689$ |

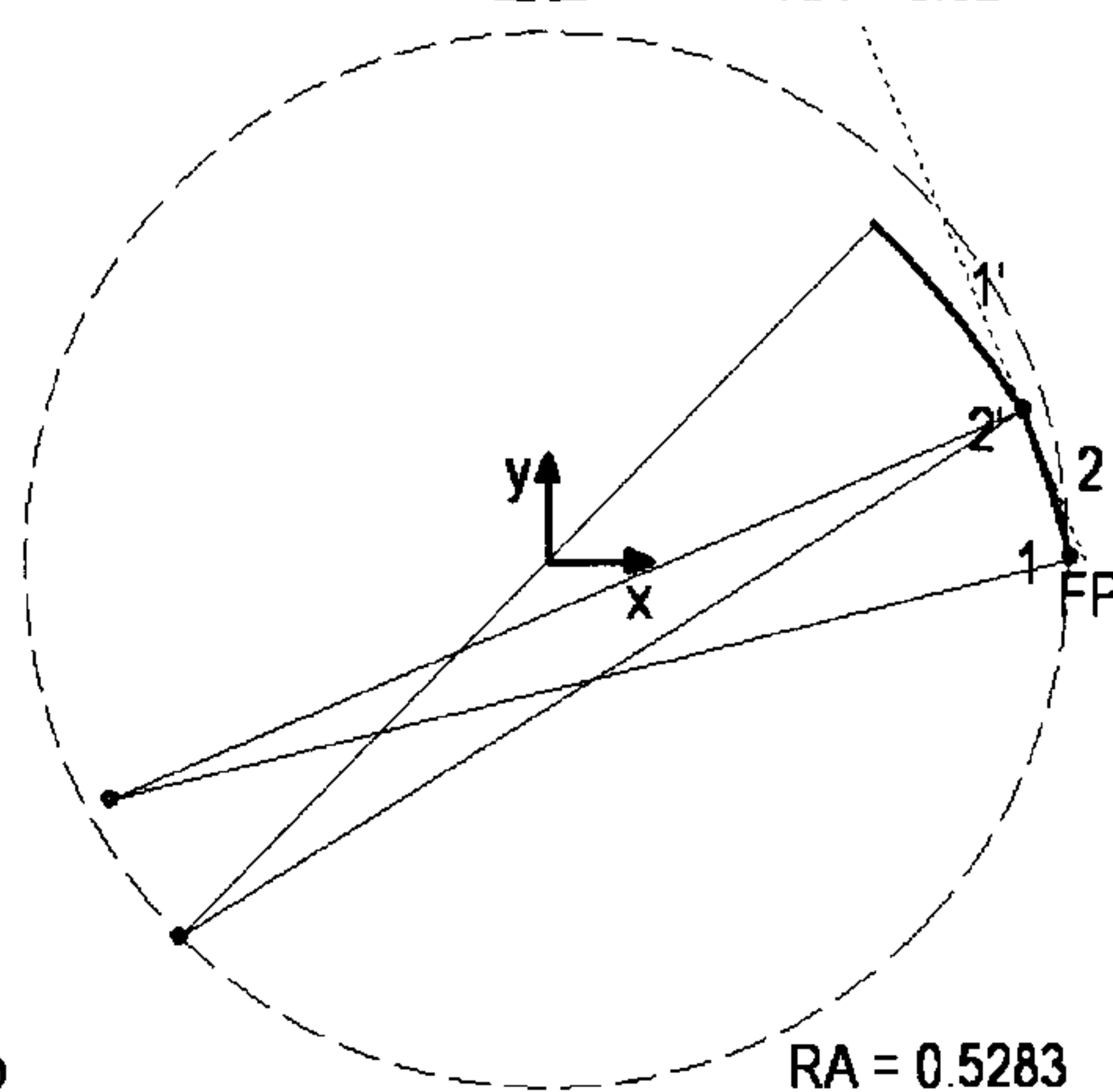


Figure 56b

- | | | |
|-----|-------------------|----------------|
| 1) | $R = 0.0000$ | $Mx = 0.5283$ |
| | $\alpha = 0.2384$ | $My = 0.0000$ |
| 2) | $R = 1.0000$ | $Mx = -0.4434$ |
| | $\alpha = 0.1543$ | $My = -0.2361$ |
| 2') | $R = 0.0000$ | $Mx = 0.4805$ |
| | $\alpha = 0.1543$ | $My = 0.1466$ |
| 1') | $R = 1.0000$ | $Mx = -0.3736$ |
| | $\alpha = 0.2384$ | $My = -0.3736$ |

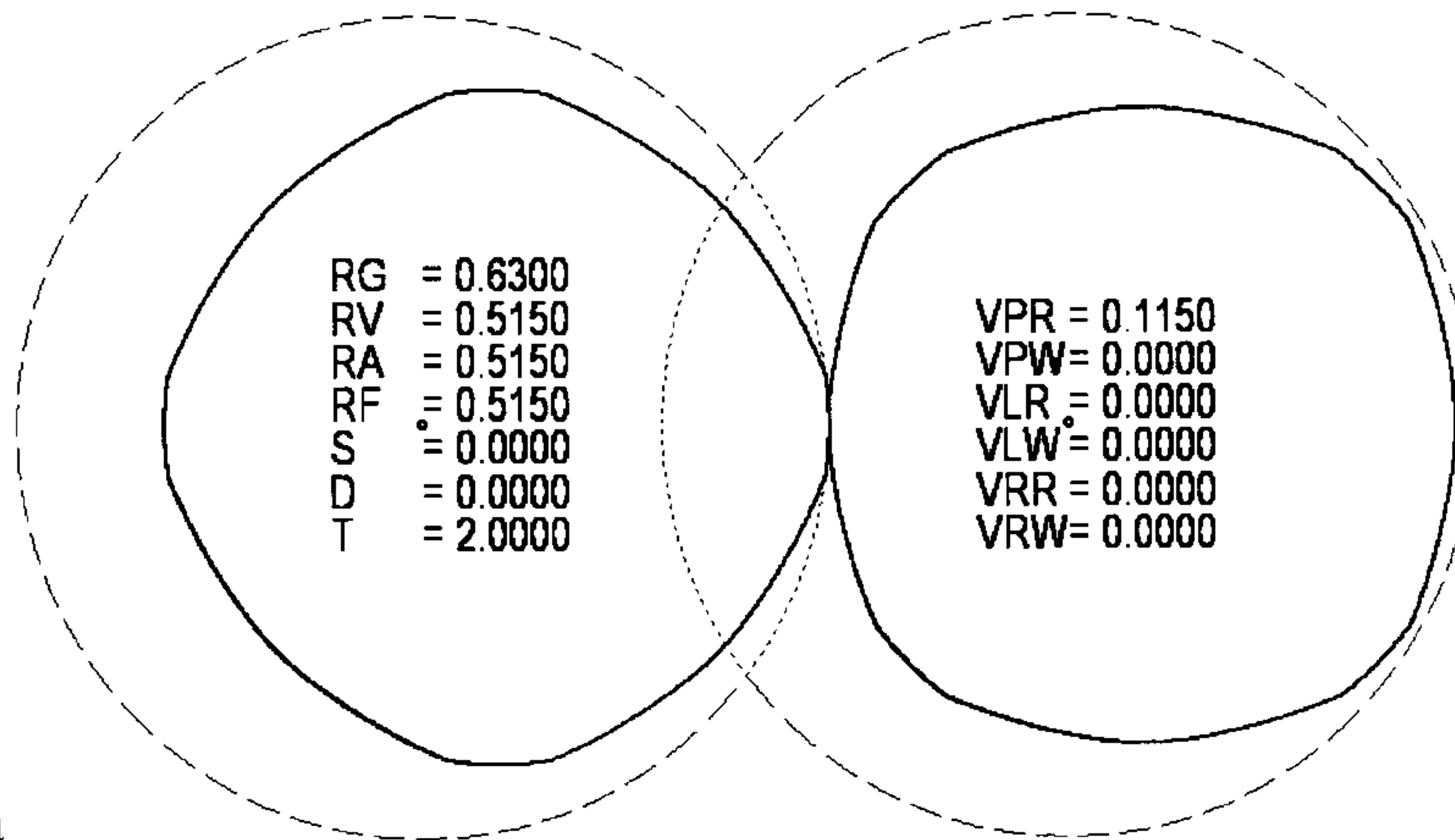


Figure 57a

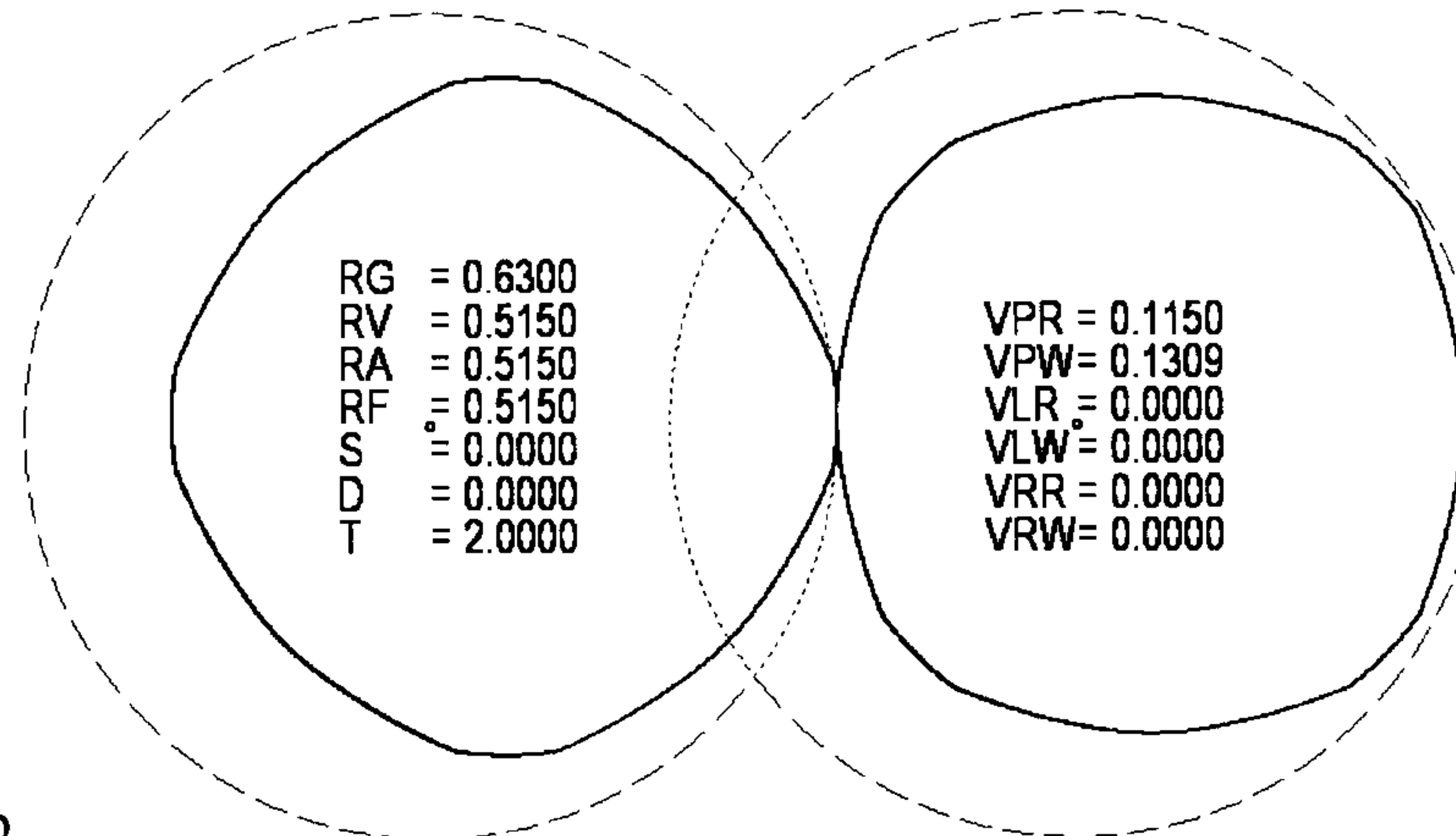


Figure 57b

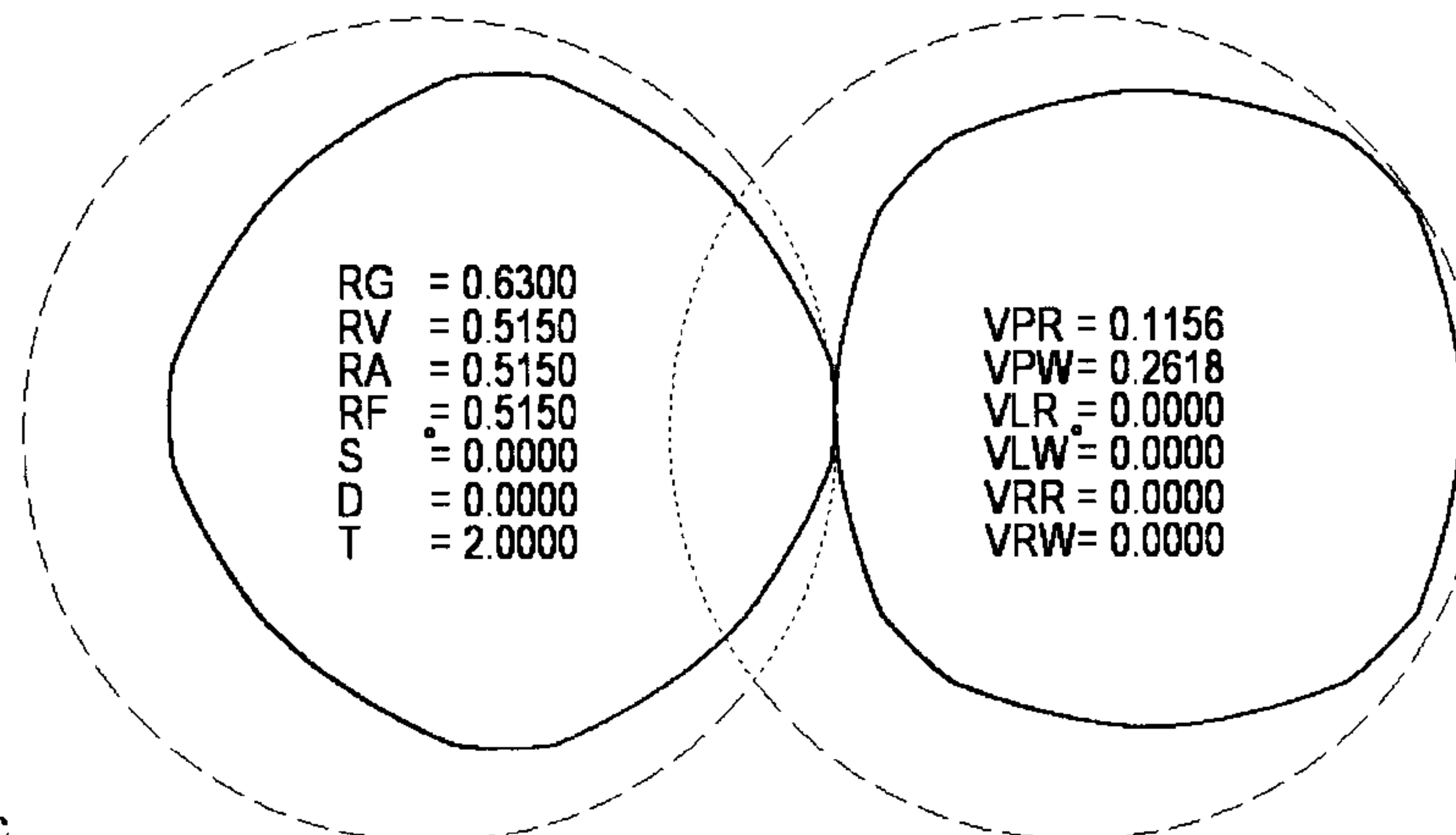


Figure 57c

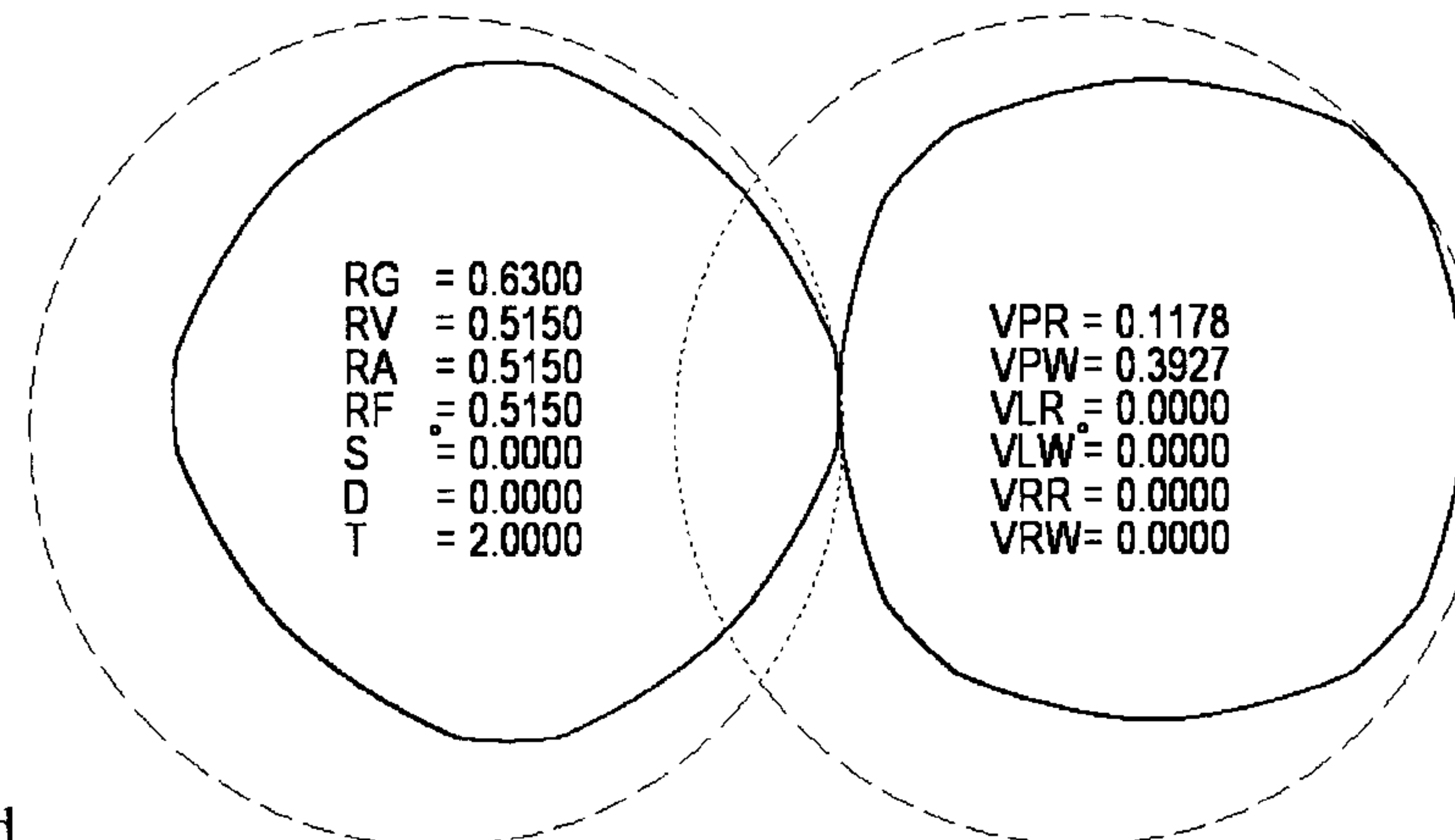


Figure 57d

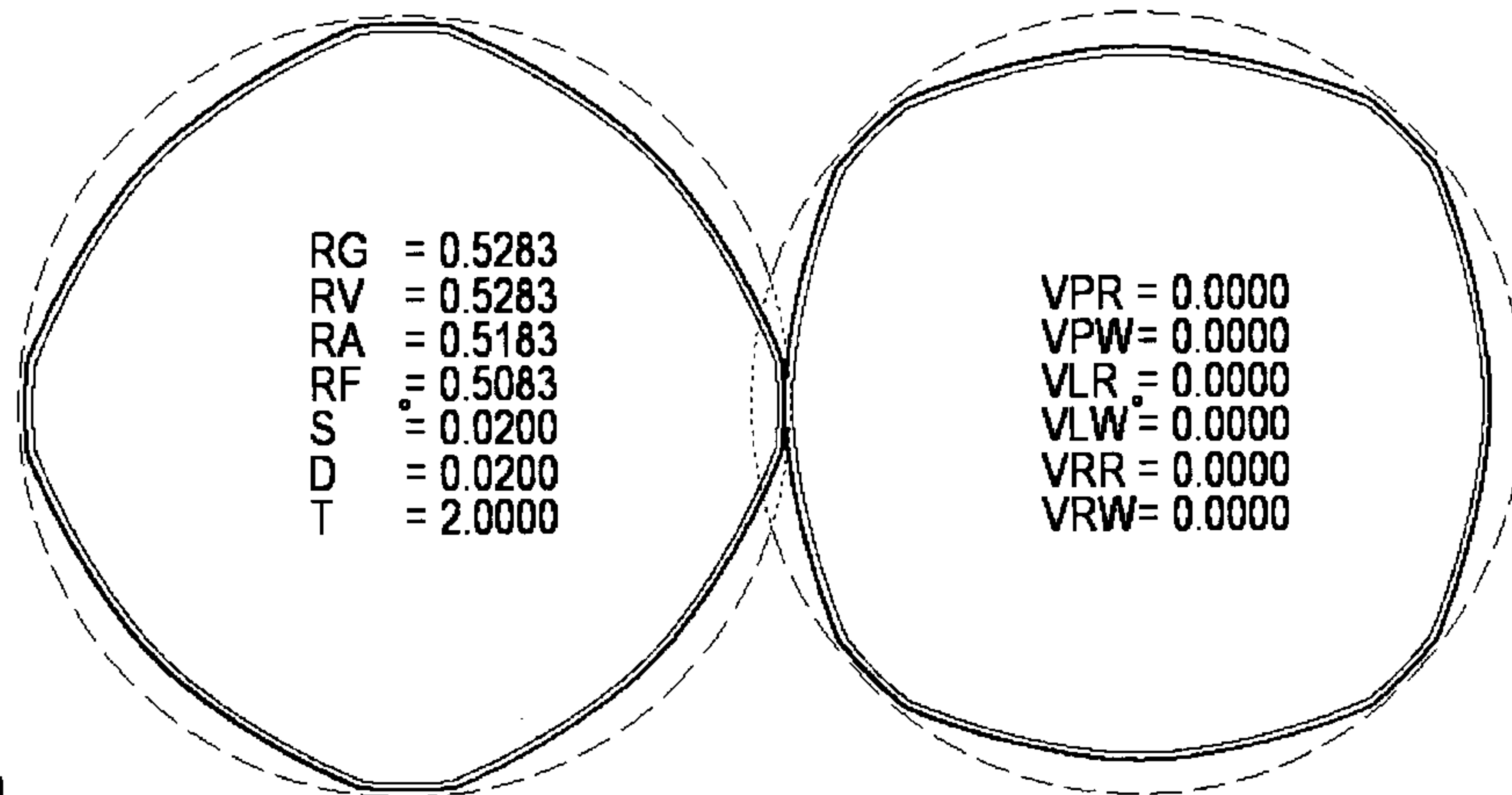


Figure 58a

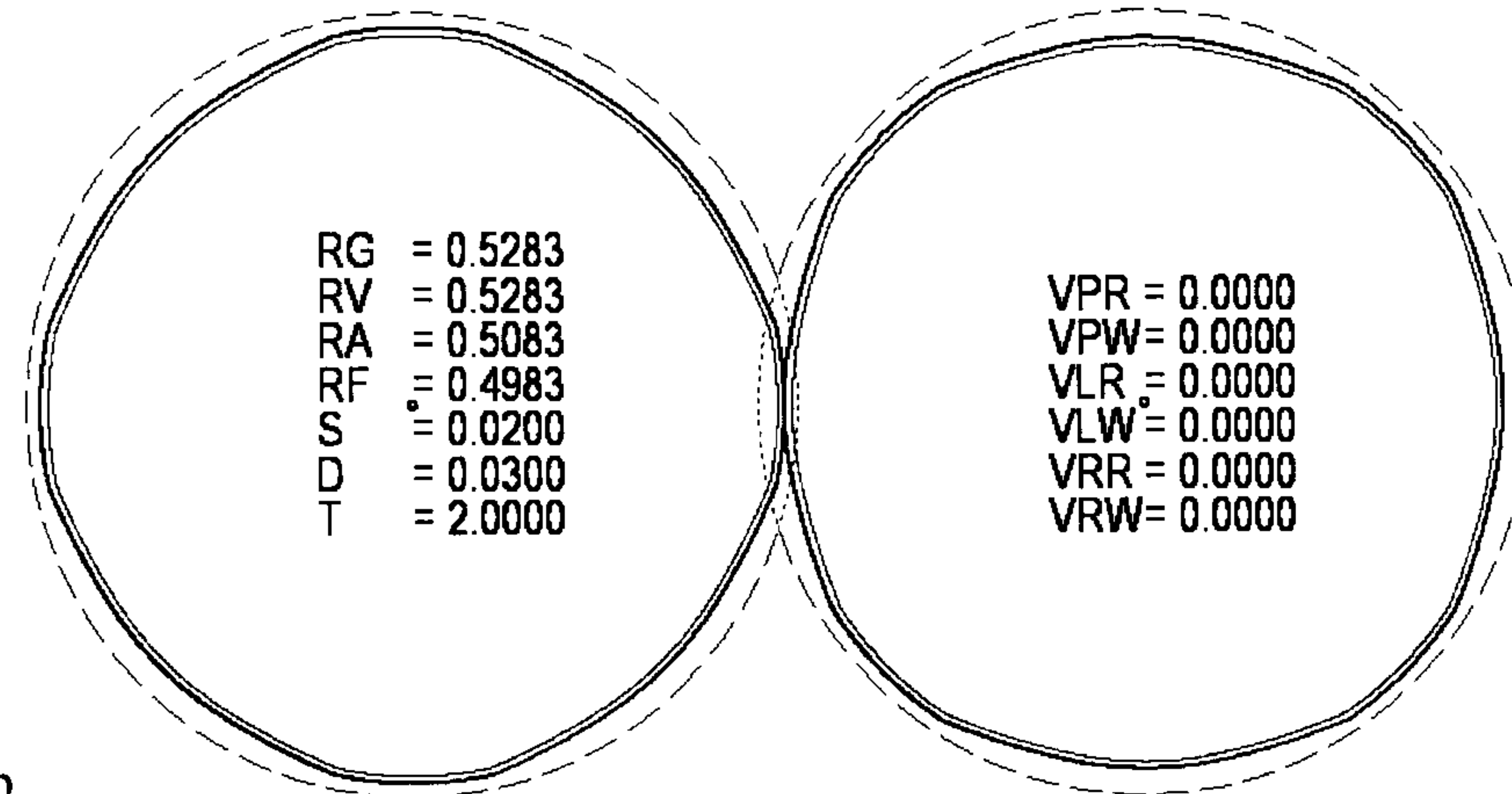


Figure 58b

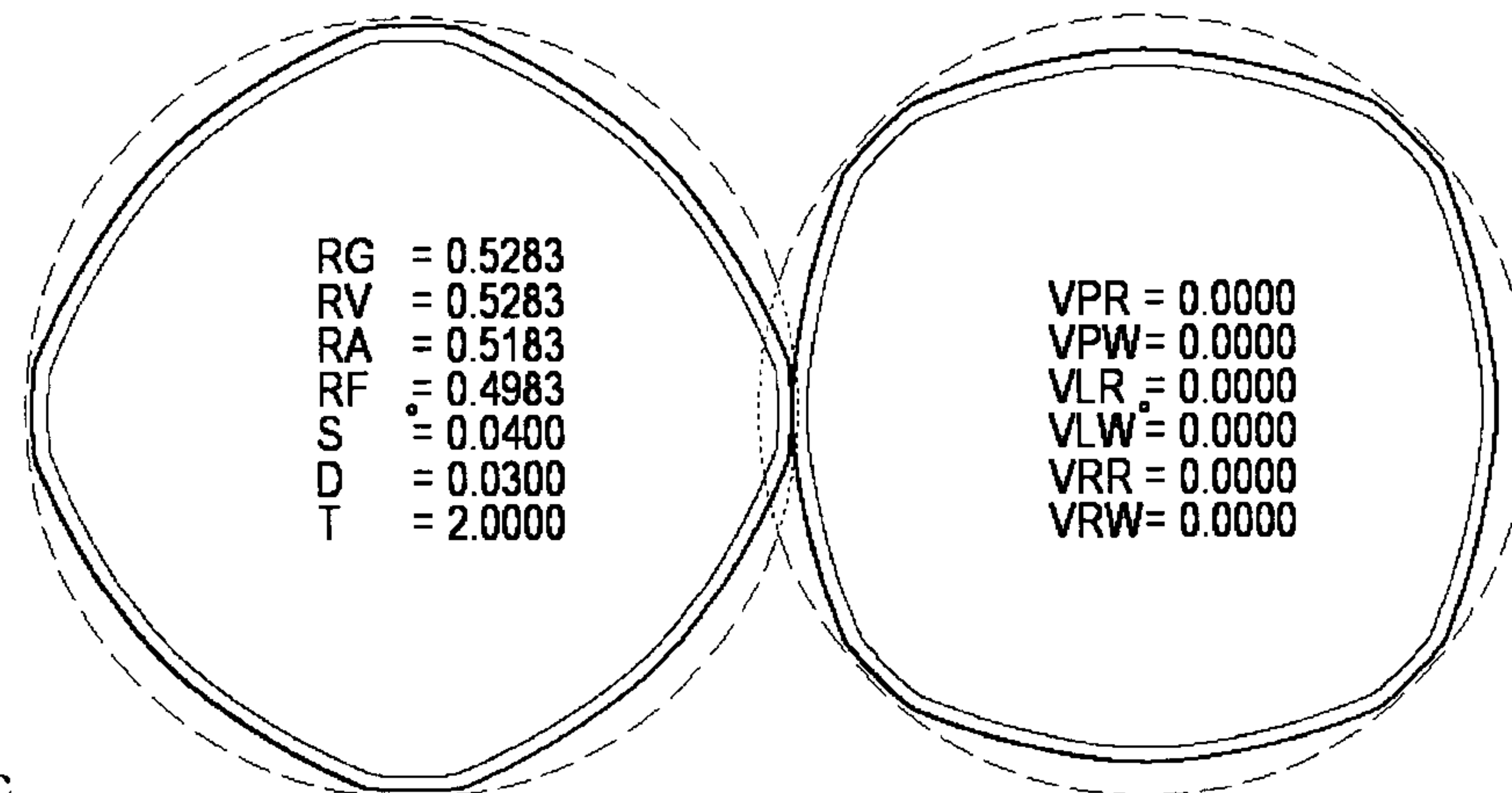


Figure 58c

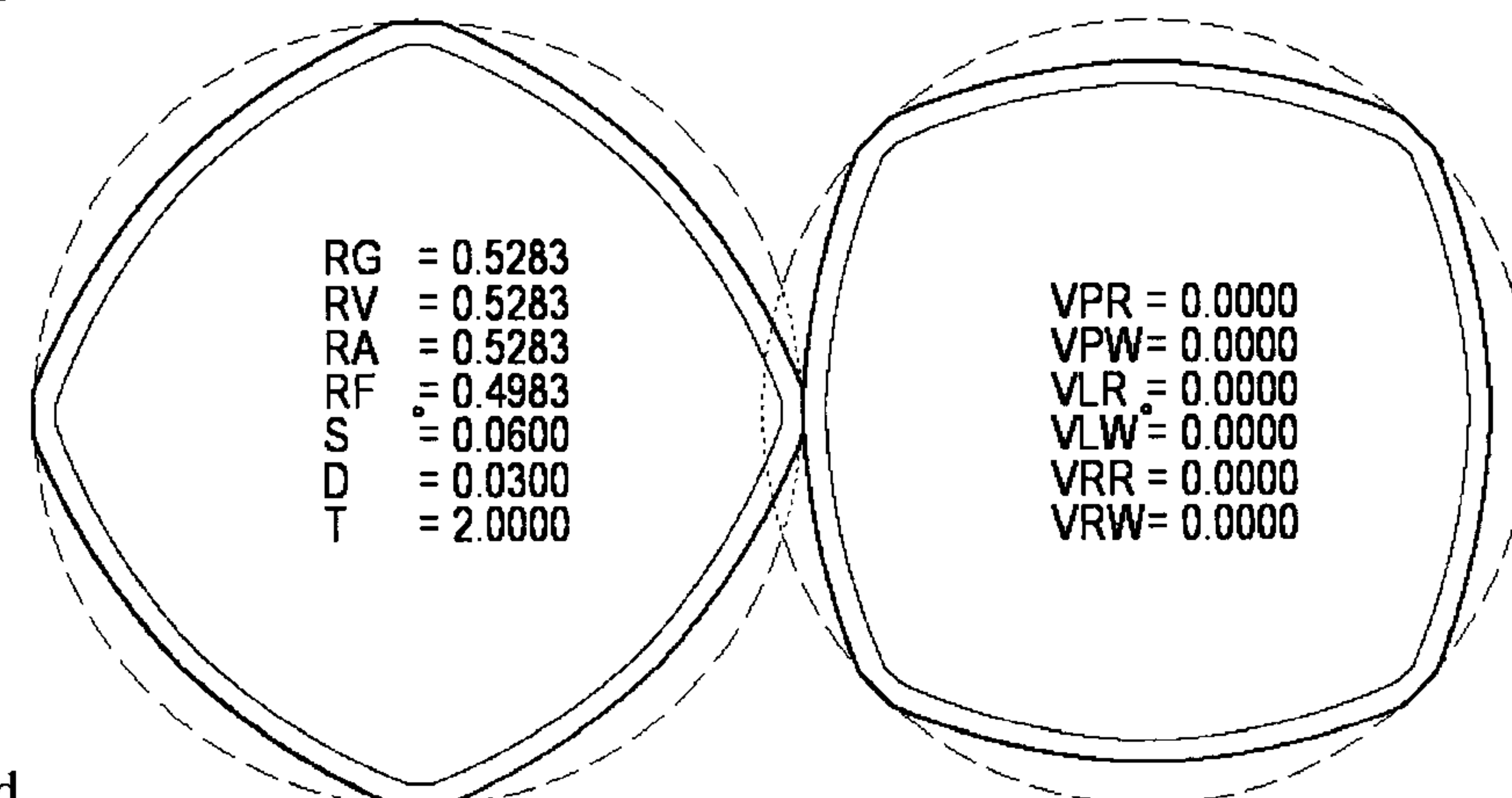


Figure 58d

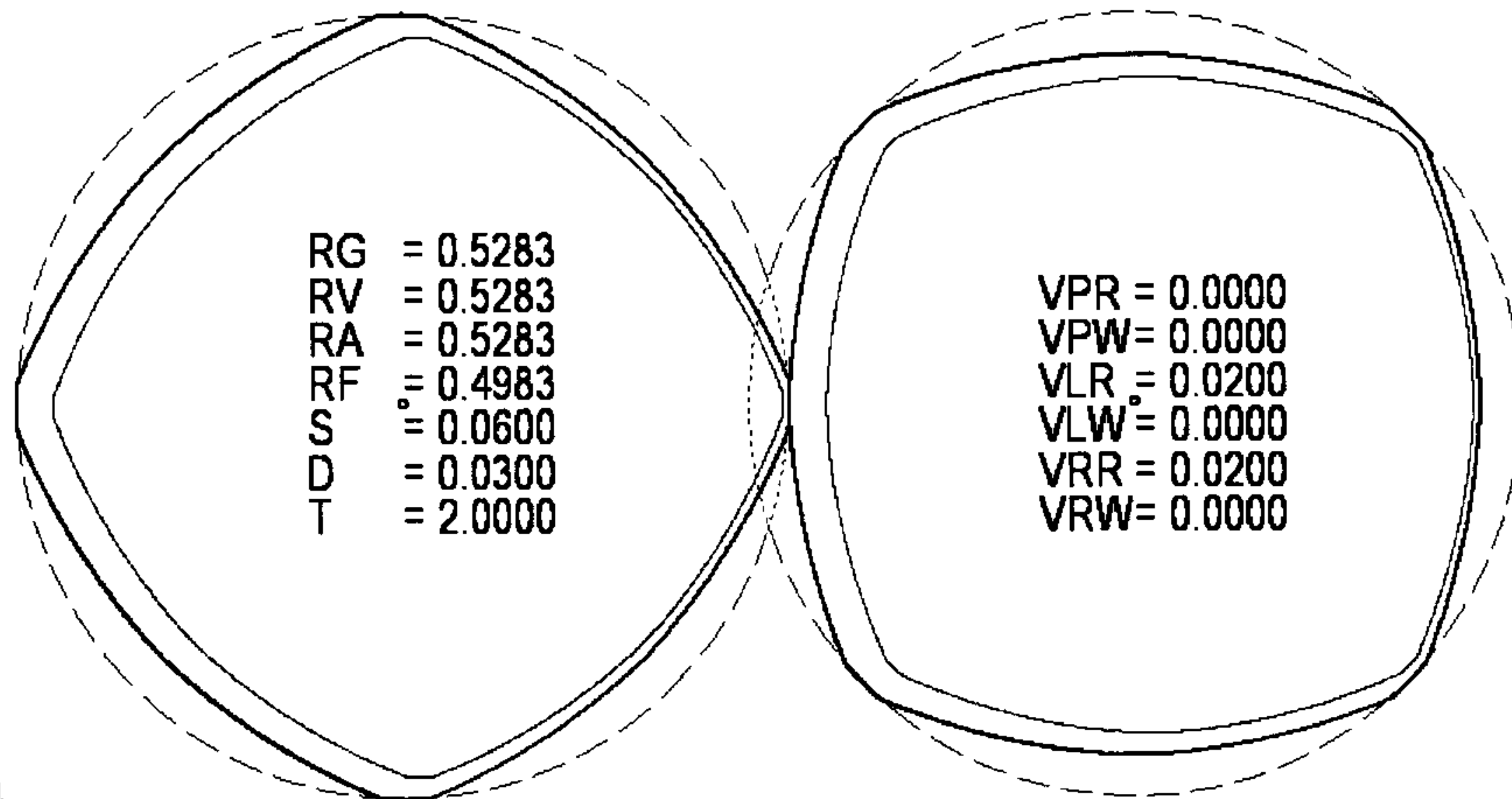


Figure 59a

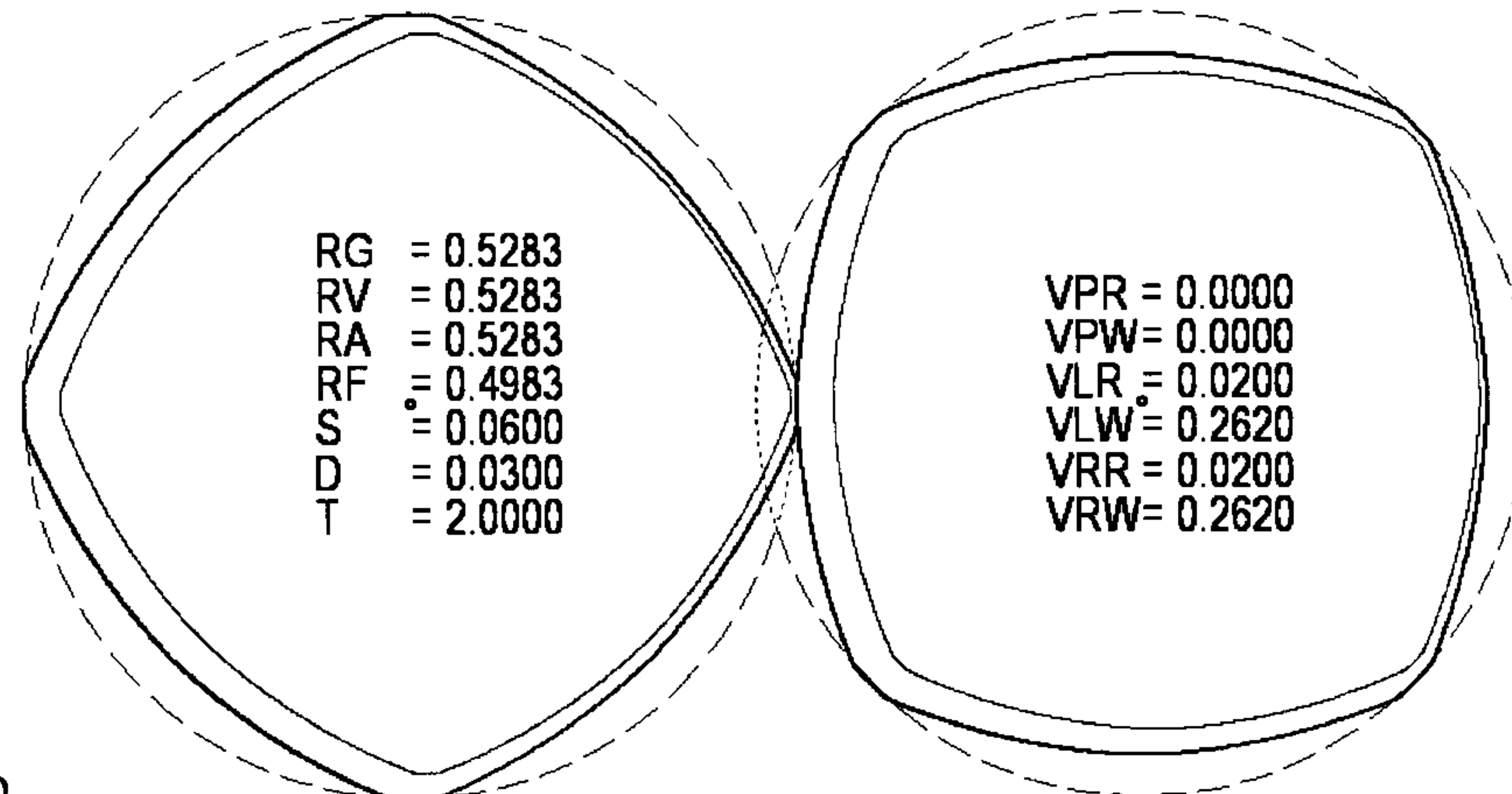


Figure 59b

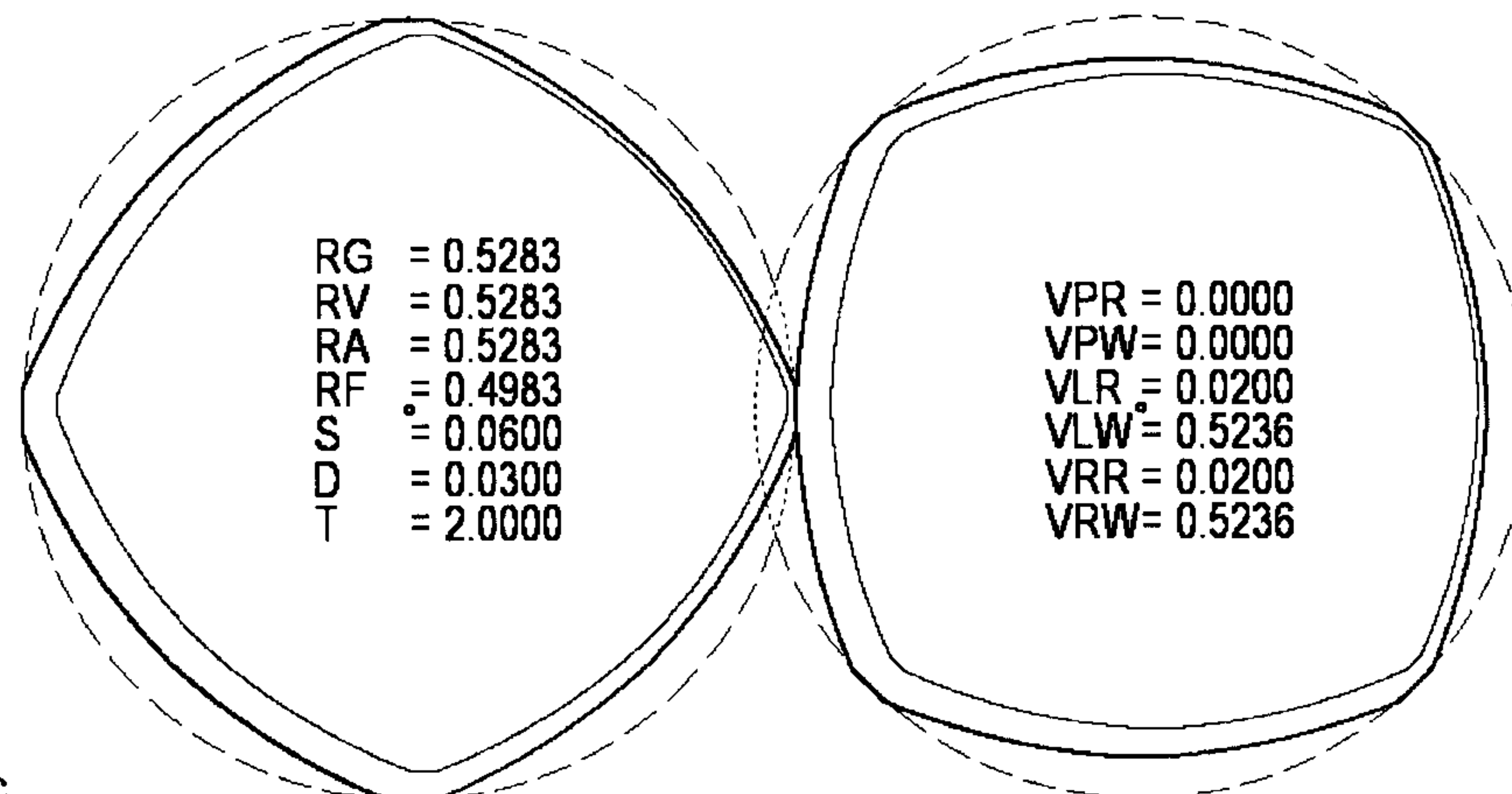


Figure 59c

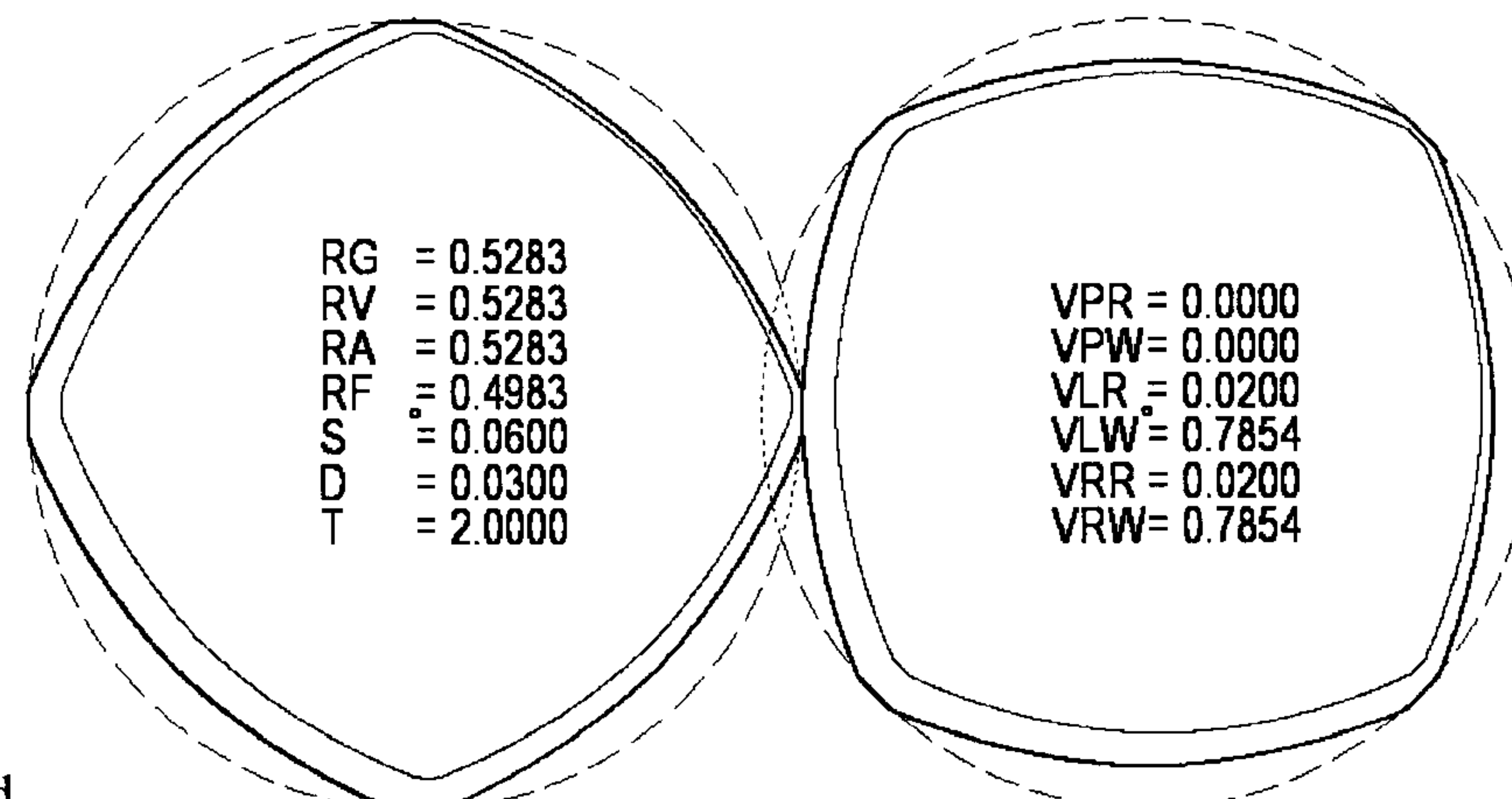


Figure 59d

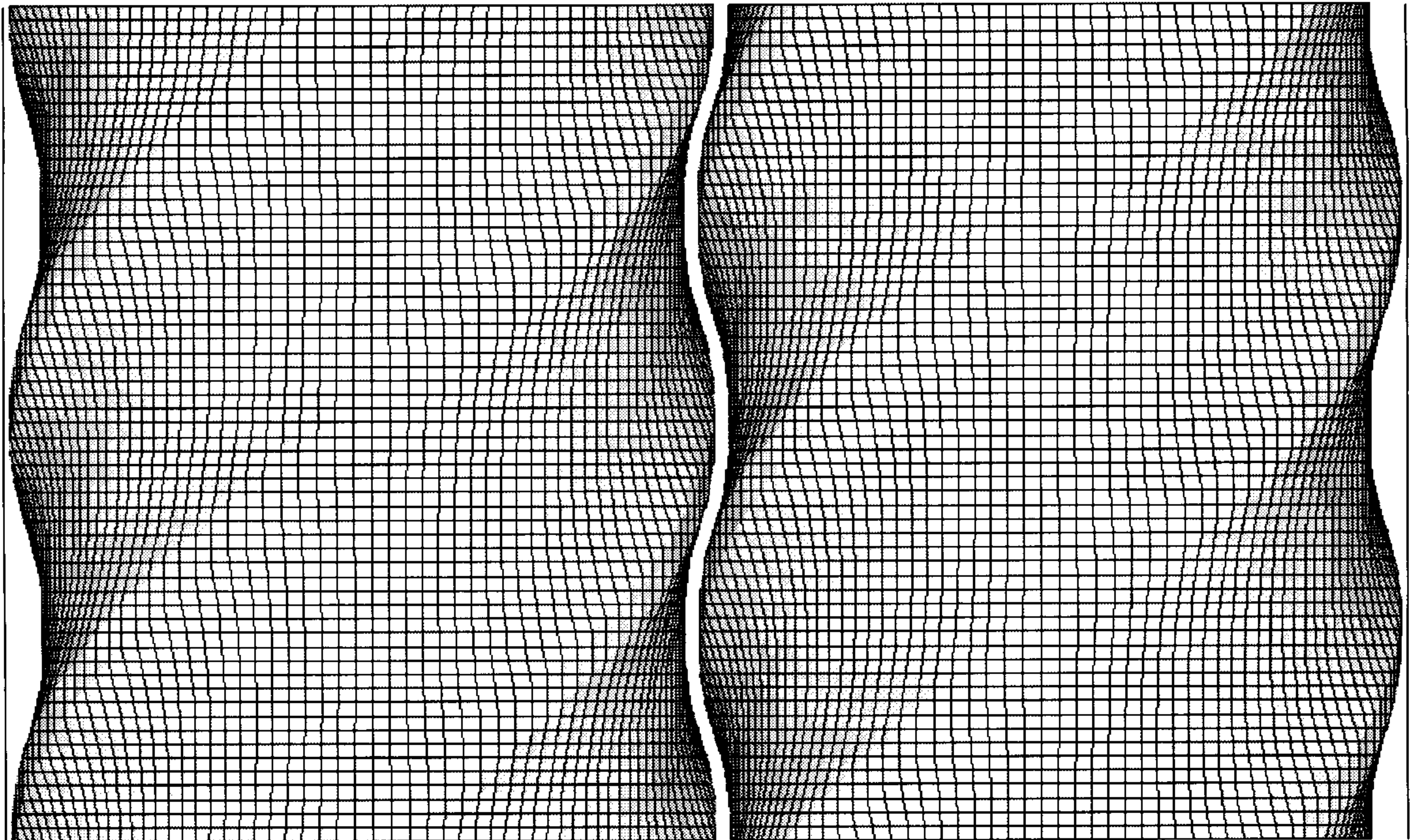
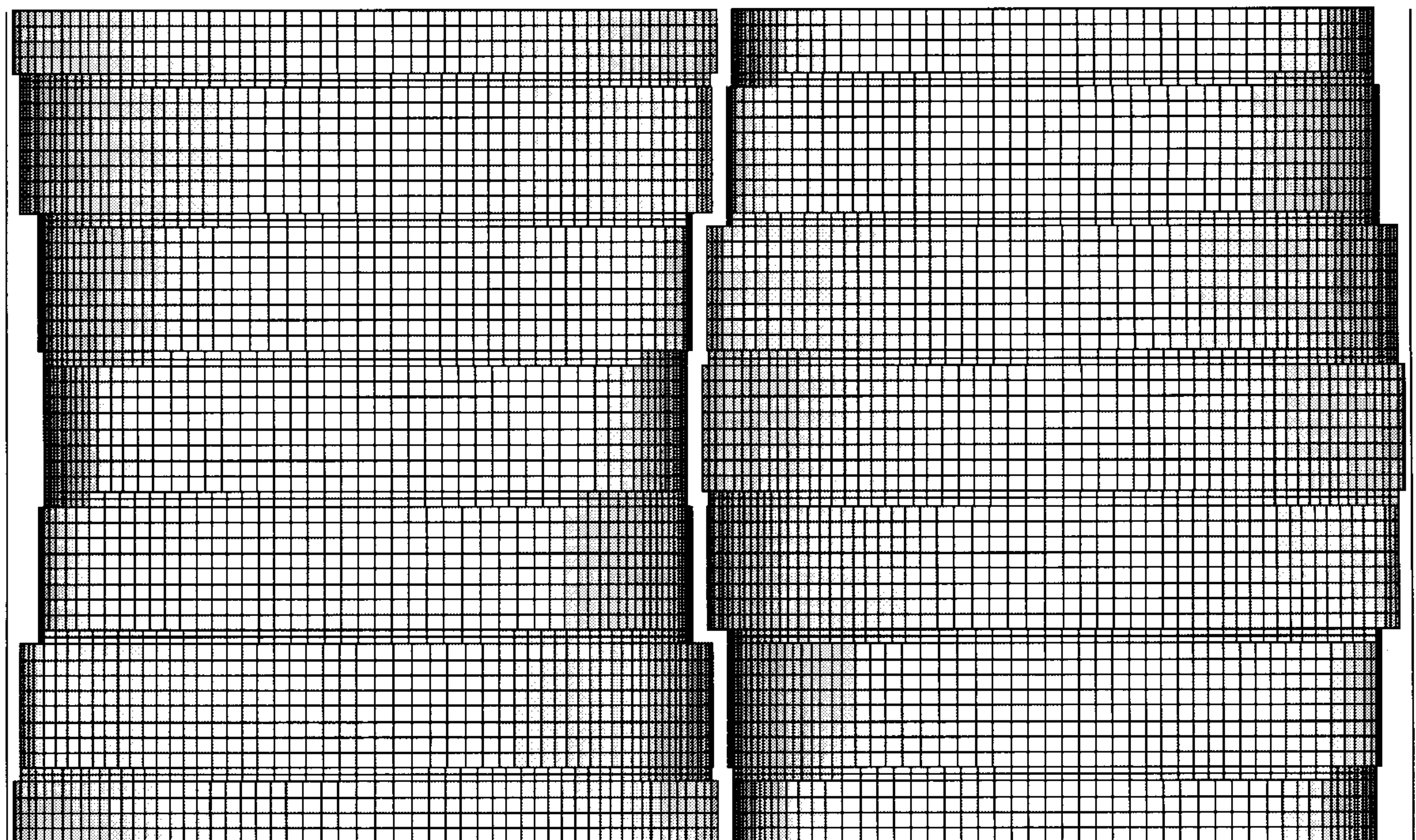


Figure 60a



5 Figure 60b

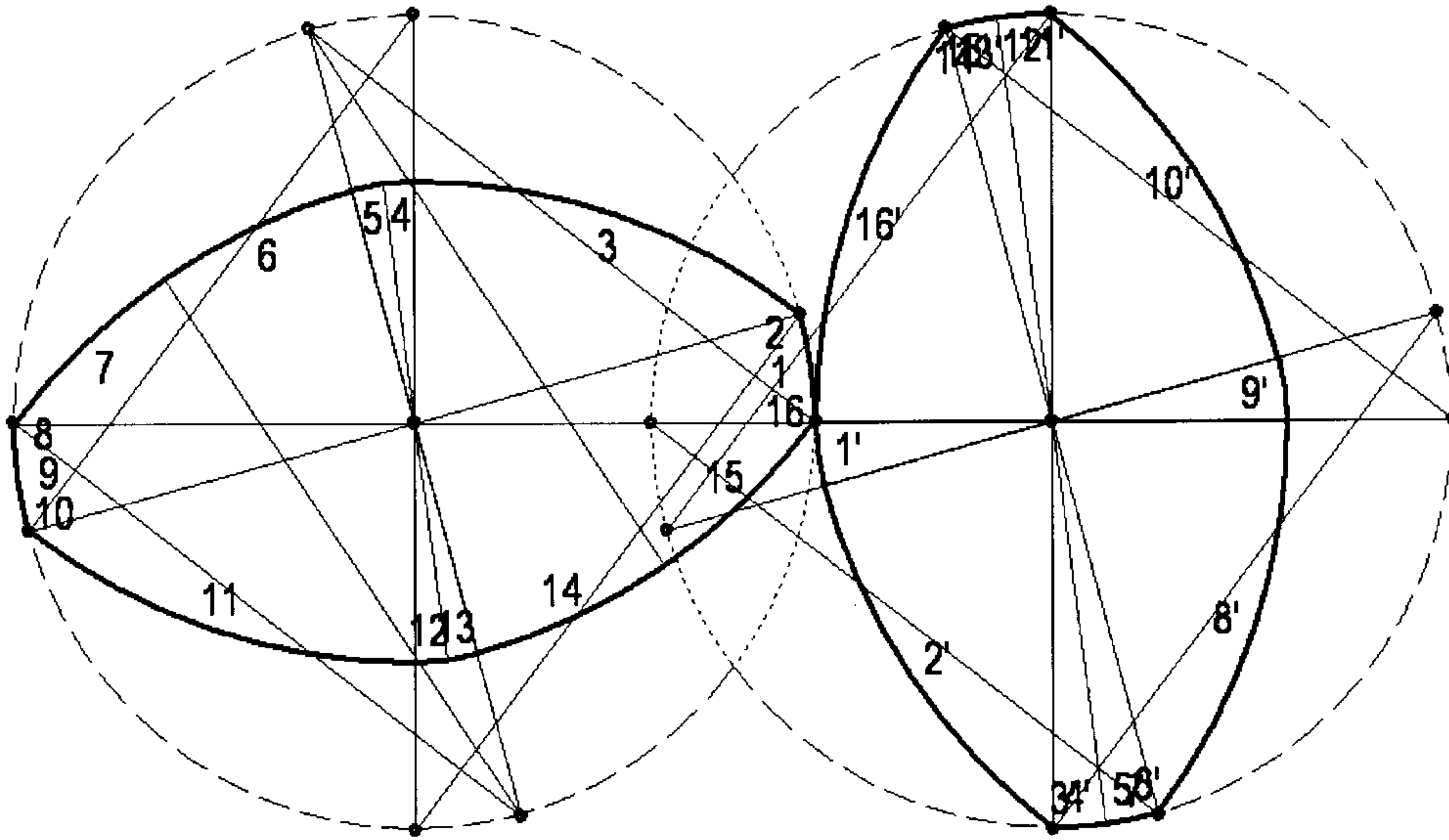


Figure 61a

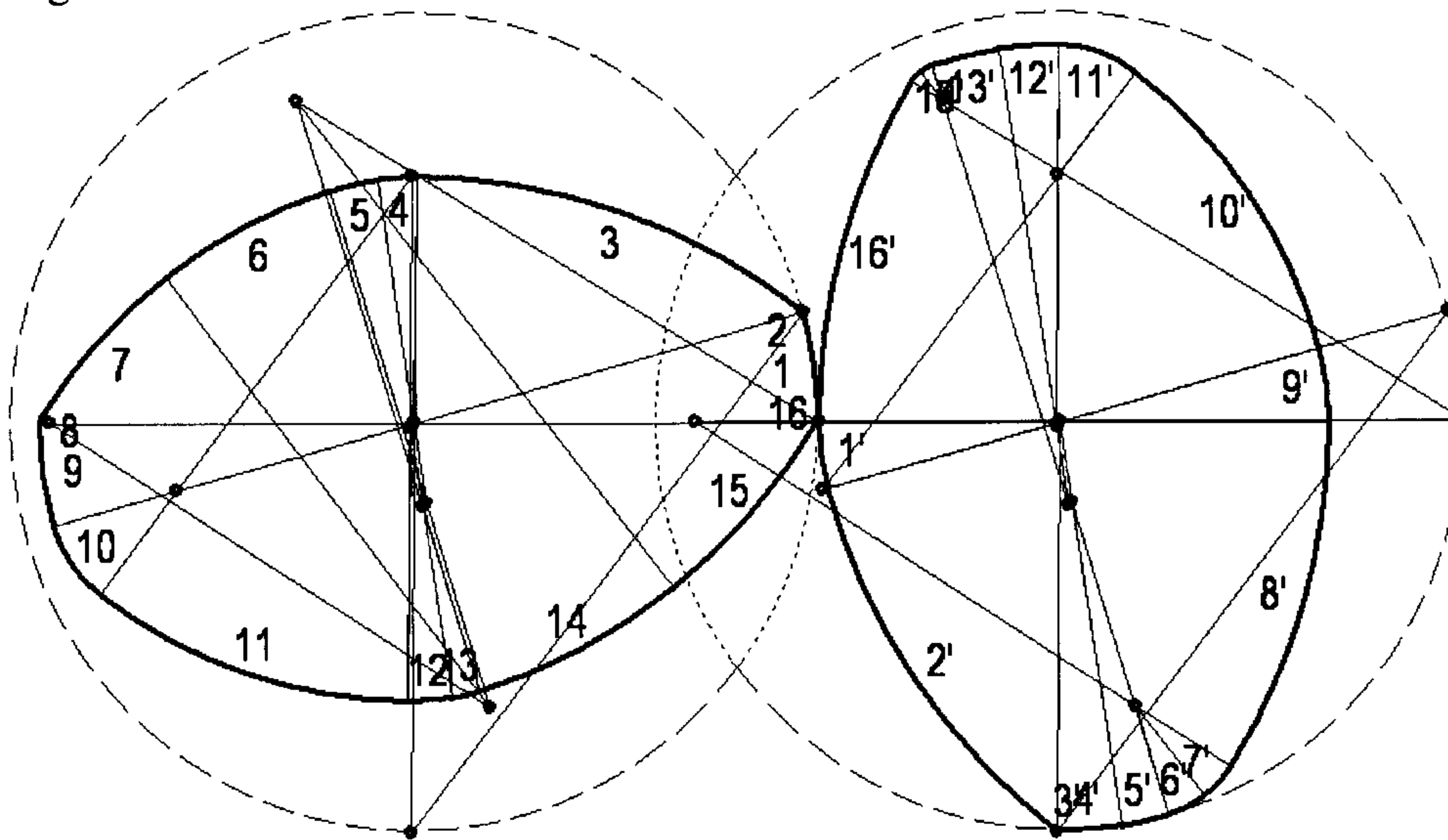


Figure 61b

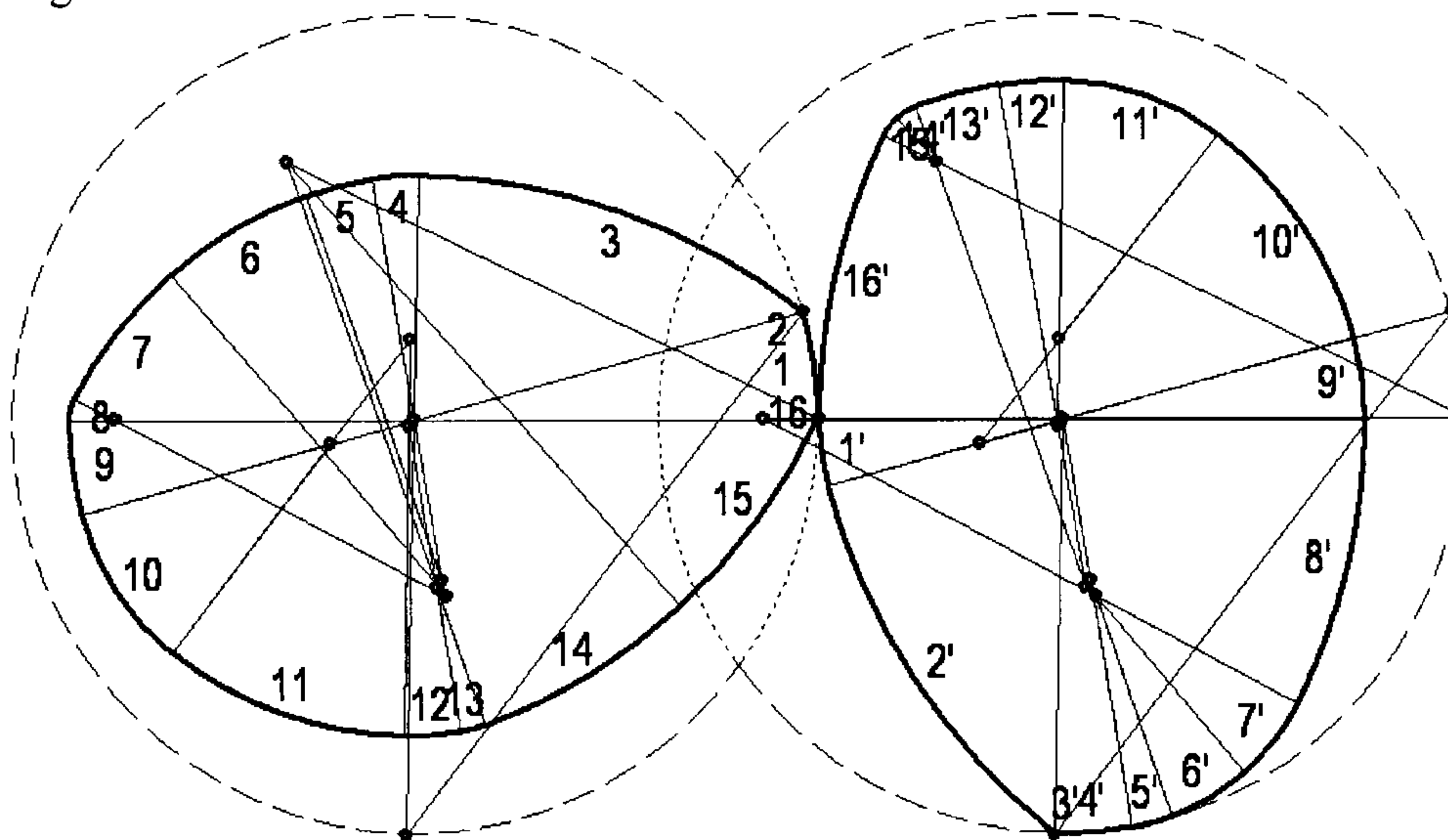


Figure 61c

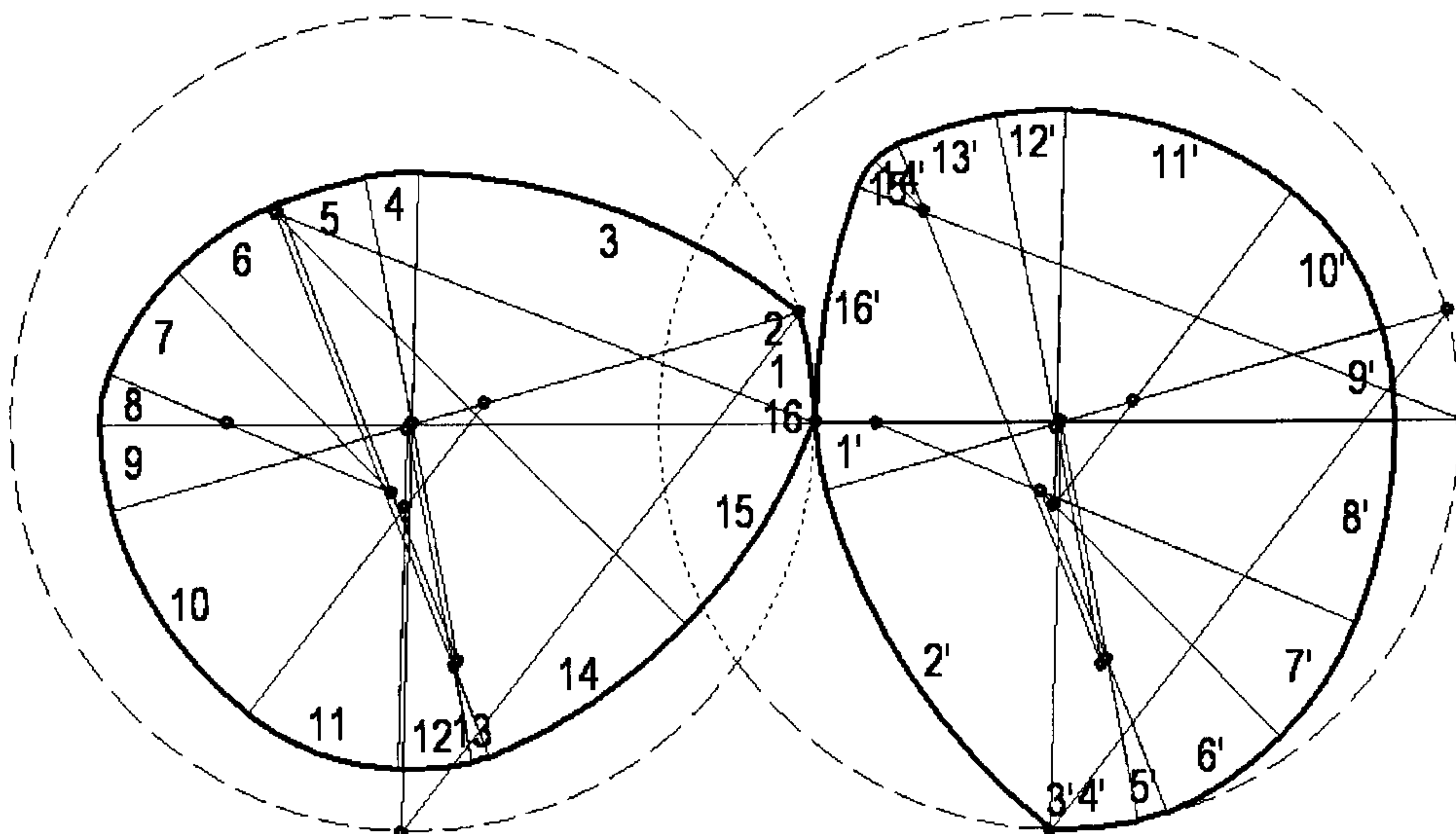


Figure 61d

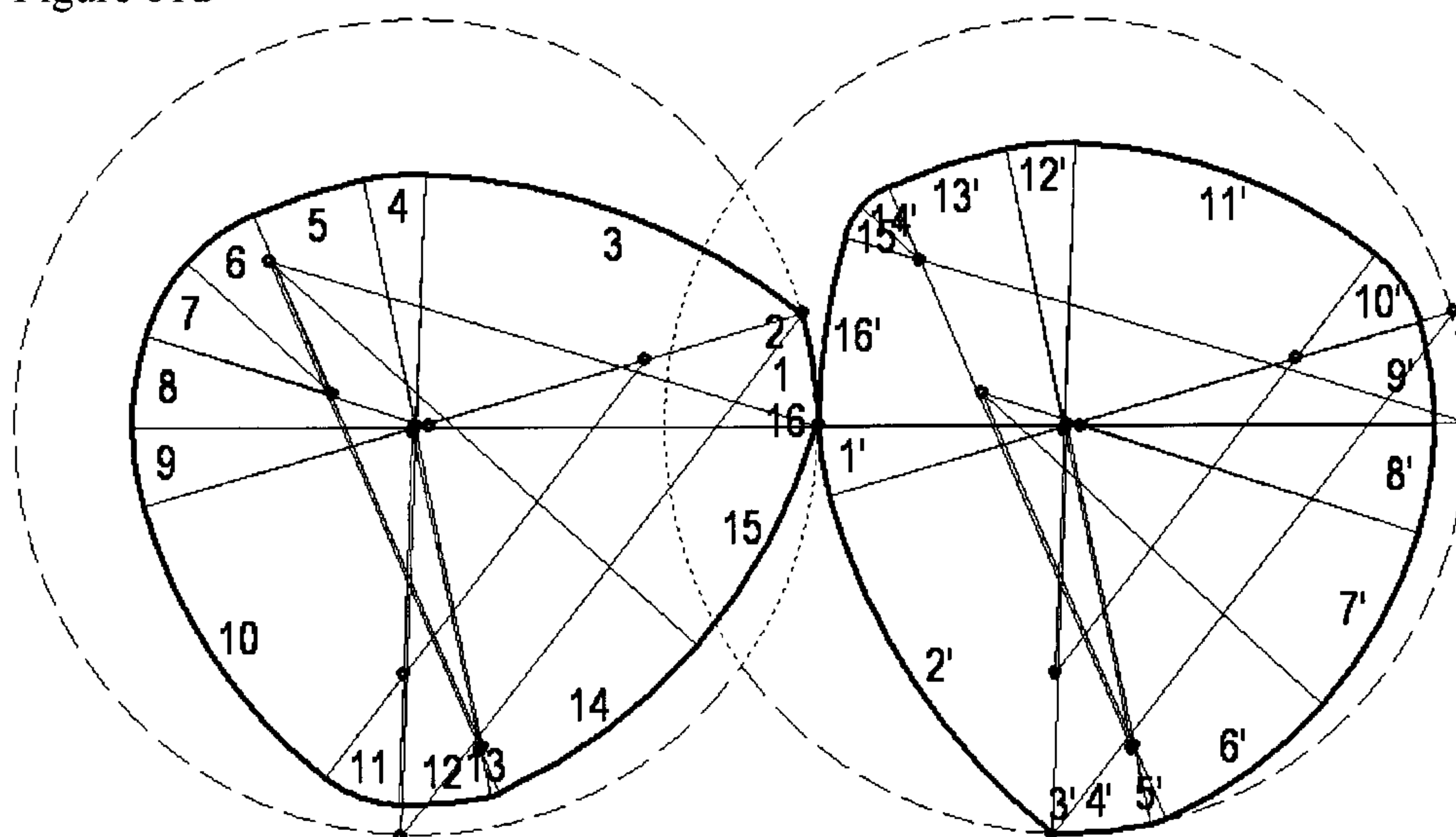
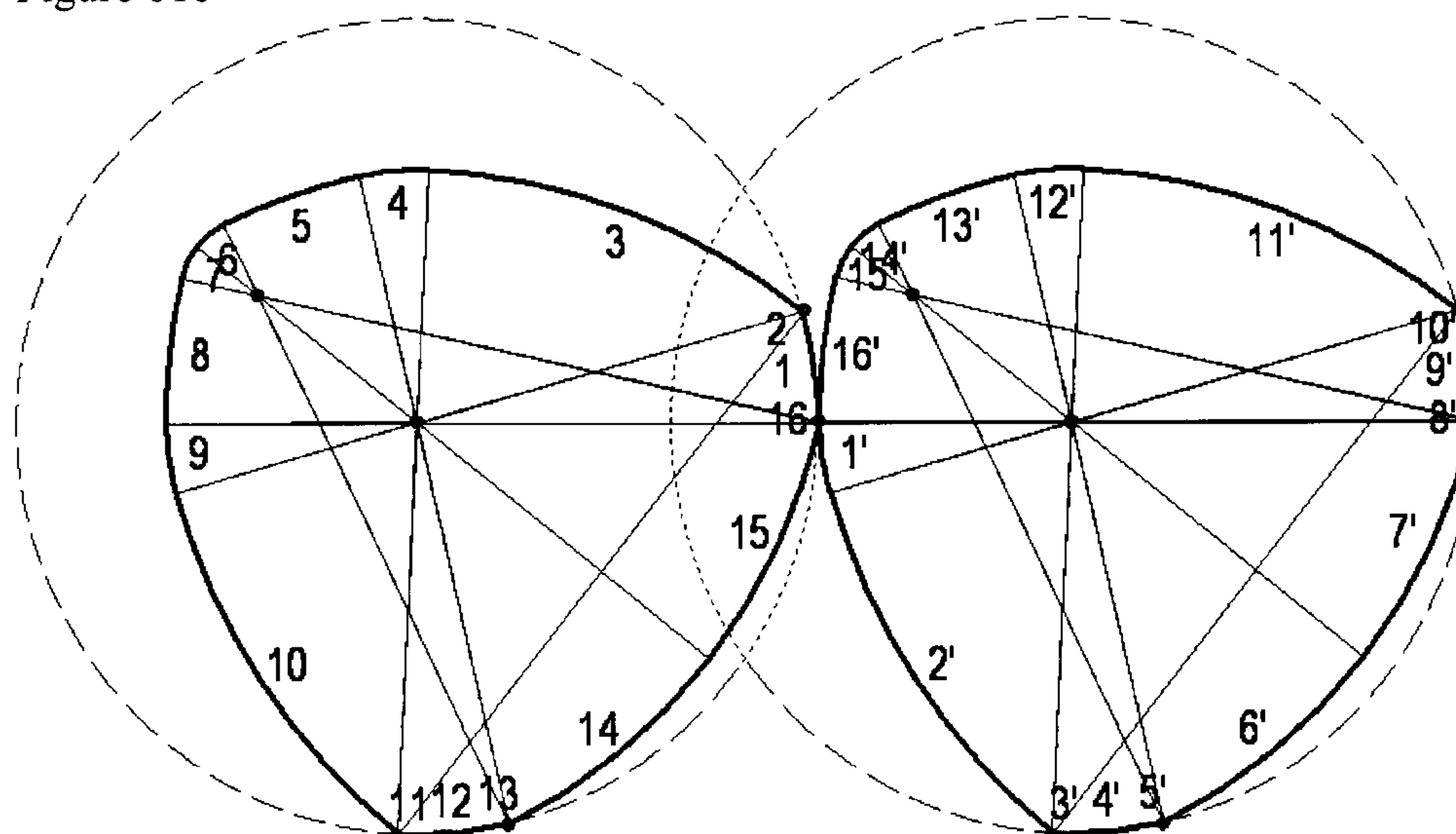


Figure 61e



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Figure 61f

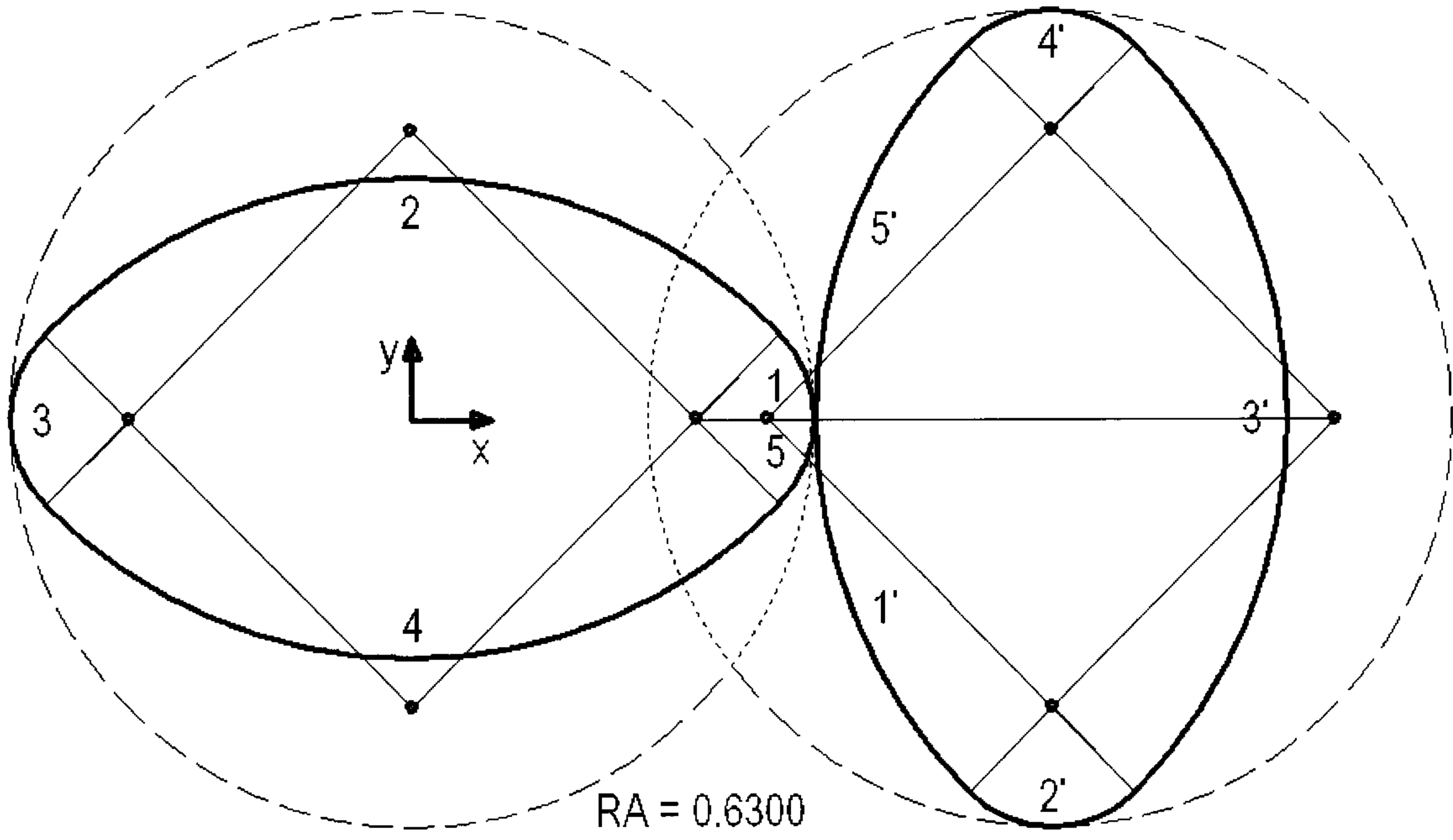
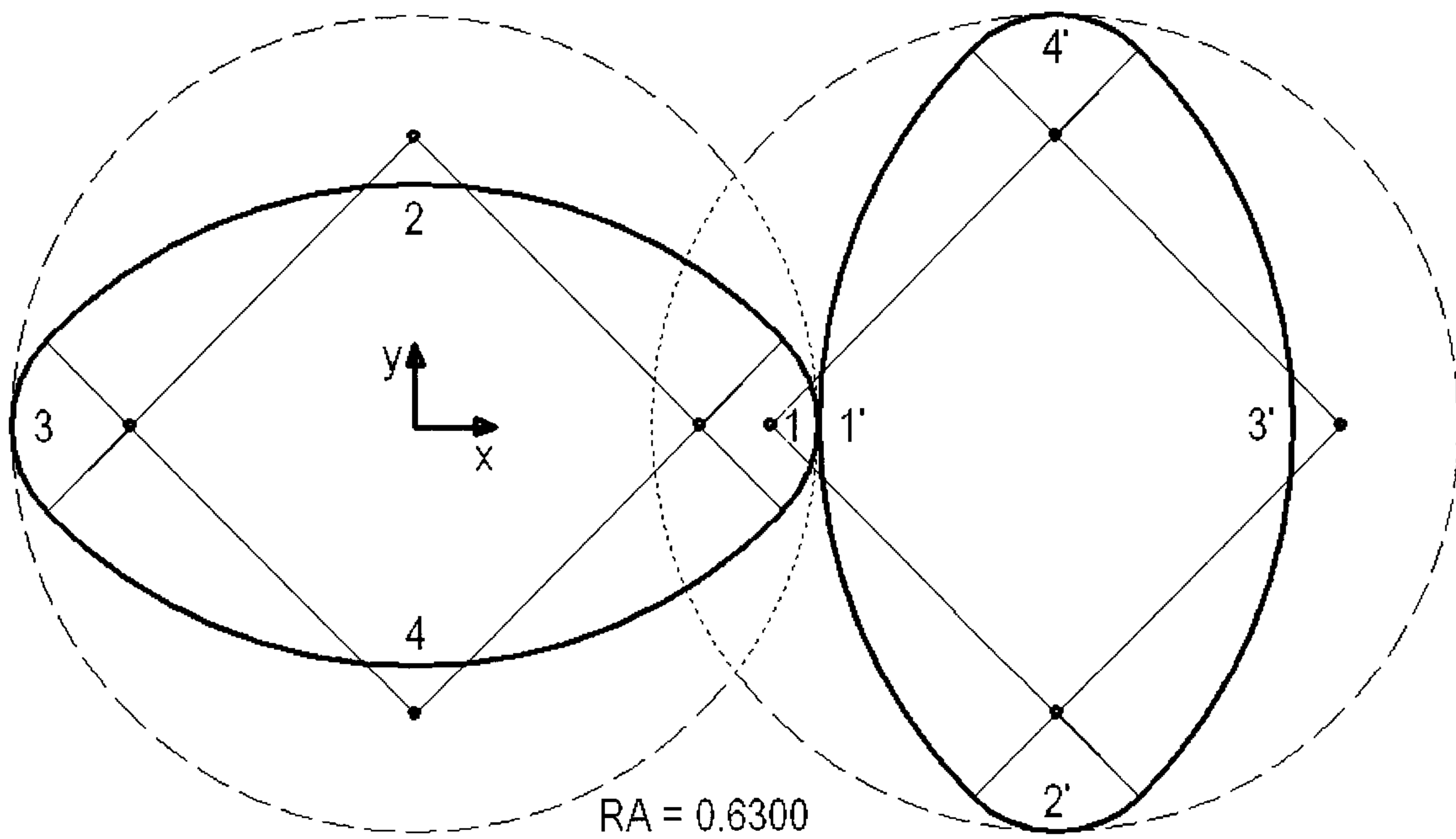
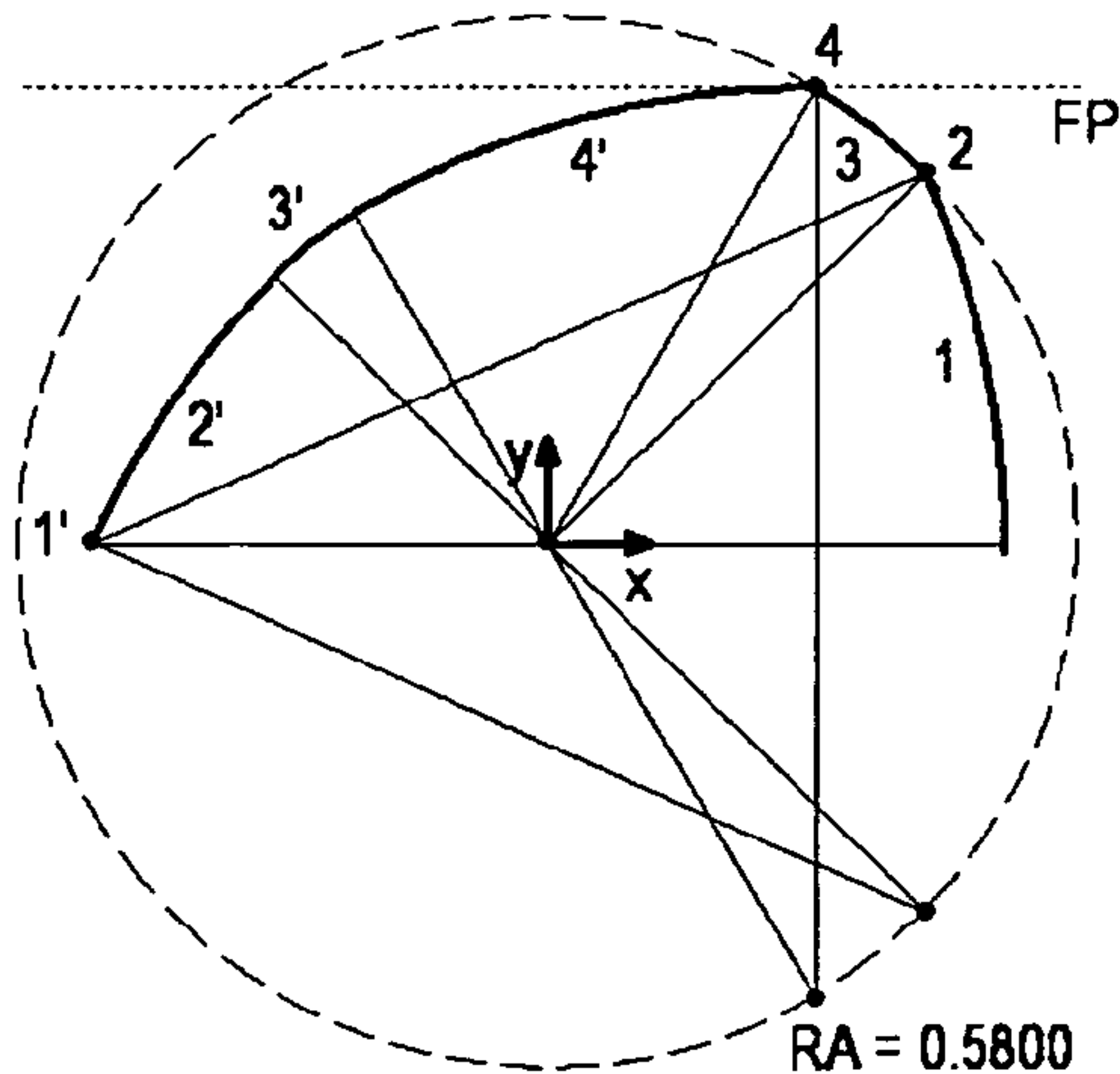


Figure 62a



5 Figure 62b



Figur 17d

1)	$R = 0.9999$	$M_x = -0.4998$
	$\alpha = 0.4187$	$M_y = 0.0000$
2)	$R = 0.0000$	$M_x = 0.4137$
	$\alpha = 0.3580$	$M_y = 0.4065$
3)	$R = 0.5800$	$M_x = 0.0000$
	$\alpha = 0.2627$	$M_y = 0.0000$
4)	$R = 0.0000$	$M_x = 0.2939$
	$\alpha = 0.5315$	$M_y = 0.5000$
4')	$R = 1.0000$	$M_x = 0.2939$
	$\alpha = 0.5315$	$M_y = -0.5000$
3')	$R = 0.4200$	$M_x = 0.0000$
	$\alpha = 0.2627$	$M_y = 0.0000$
2')	$R = 1.0000$	$M_x = 0.4137$
	$\alpha = 0.3580$	$M_y = -0.4065$
1')	$R = 0.0001$	$M_x = -0.4998$
	$\alpha = 0.4187$	$M_y = 0.0000$