

(19) AUSTRALIAN PATENT OFFICE

(54) Title

A method and control system for reducing the fatigue loads in the components of a wind turbine subjected to asymmetrical loading of the rotor plane

(51)⁶ International Patent Classification(s)

F03D 7/04 (2006.01) 20060101AFI2007092

F03D 7/04

OBHEP

PCT/DK2006/000153

(21) Application No: 2006339899

(22) Application Date: 2006 .03 .16

(87) WIPO No: W007/104306

(43) Publication Date : 2007 .09 .20

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(56) Related Art

EP 0995904

WO 2004/074681

US 4161658

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
20 September 2007 (20.09.2007)

PCT

(10) International Publication Number
WO 2007/104306 A1

(51) International Patent Classification:
F03D 7/04 (2006.01)

(21) International Application Number:
PCT/DK2006/000153

(22) International Filing Date: 16 March 2006 (16.03.2006)

(25) Filing Language: English

(26) Publication Language: English

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(81) Designated States (unless otherwise indicated, for every
kind of national protection available): AB, AG, AL, AM,
AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN,

CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI,
GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE,
KG, KM, KN, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV,
LY, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NG, NI,
NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG,
SK, SL, SM, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US,
UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every
kind of regional protection available): ARIPO (BW, GH,
GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM,
ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM),
European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI,
FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, NL, PL, PT,
RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA,
GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Declaration under Rule 4.17:

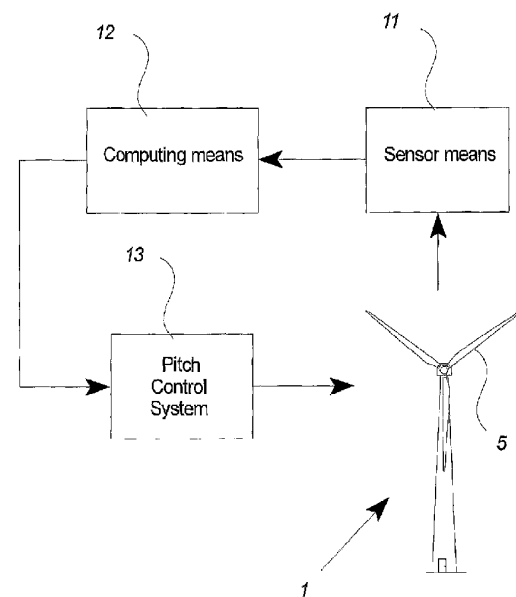
— of inventorship (Rule 4.17(iv))

Published:

with international search report

For two letter codes and other abbreviations, refer to the "Guid
ance Notes on Codes and Abbreviations" appearing at the begin-
ning of each regular issue of the PCT Gazette.

(54) Title: A METHOD AND CONTROL SYSTEM FOR REDUCING THE FATIGUE LOADS IN THE COMPONENTS OF A
WIND TURBINE SUBJECTED TO ASYMMETRICAL LOADING OF THE ROTOR PLANE



(57) Abstract: The invention relates to a method for reducing fatigue loads in the components of a wind turbine subjected to asymmetrical loading of its rotor, comprising the steps of: repeatedly collecting and storing load data of the rotor, determining a load distribution function for the rotor from said stored data, deriving a plurality of periodic functions from said load distribution function, determining actions for the wind turbine control means for reducing the fatigue load of the wind turbine components from said derived plurality of periodic functions, and implementing of said determined actions on the wind turbine control means. The invention also relates to a control system as well as a wind turbine and wind park.

WO 2007/104306 A1

A METHOD AND CONTROL SYSTEM FOR REDUCING THE FATIGUE
LOADS IN THE COMPONENTS OF A WIND TURBINE SUBJECTED TO
ASYMMETRICAL LOADING OF THE ROTOR PLANE

5 **Field of invention**

The present invention relates to a method for reducing fatigue loads in the components of a wind turbine, a control system for reducing the fatigue loads in the components of the wind turbine subjected to asymmetrical loading of the rotor plane, a wind turbine and a wind park.

10 **Description of the related art**

A reference herein to matter which is given as prior art is not to be taken as an admission that that matter was, in Australia, known or that it was part of the common general knowledge as at the priority date of any of the claims.

15 Wind turbine controllers have been deployed in wind turbines for years with the purpose of controlling the overall power output.

The power output from a modern wind turbine can be controlled by means of a control system for regulating the pitch angle of the rotor blades. The rotor rotation speed and power output of the wind turbine can hereby be initially controlled e.g. before a transfer to a utility grid through power converting
20 means. An advantage of this control is a protection of the rotor from rotating at an excessive speed at high wind speeds and save the rotor blades from excessive loads.

Especially for large rotor diameters, the distribution of the wind inflow profile can be non-uniform over the area of the rotor, resulting in a non-uniform load
25 to each rotor blade as a function of one full rotation, as well as asymmetrical out of plane loadings for the drive train of the wind turbine. For a free wind inflow situation the wind shear distribution is approximately linear and the said load as a function of rotation is of nearly sinusoidal behavior with a frequency equal to the rotor rotation frequency. In order to keep a more constant load on
30 the rotor blades, pitch control functions have been applied to wind turbine pitch

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controllers, where a rotor-cyclic correction with a frequency equal to the rotor rotation has been added to the overall pitch angle setting of the individual rotor blades.

5 Any obstacles within certain up wind distance of a wind turbine create a wake for the wind turbine and consequently eliminate the free wind inflow situation. An example of an obstacle may be other wind turbines, as a wind turbine always cast a wake in the downwind direction.

10 Especially in wind parks this fact may significantly influence the inflow on wind turbines situated in the down wind direction. This results in a more complex wind shear distribution than compared to a free wind inflow situation. The said complex wind distribution profile can result in wind turbulence and in turn fluctuating fatigue loads on the wind turbine components. So in order to avoid too much wind turbulence around the turbines, downstream wind turbines are spaced relative far apart resulting in very area consuming wind parks.

15 It is therefore desirable to provide a method and a technique that allows an improved wind turbine control strategy in relation to more complex wind shear distribution.

Summary of the invention

20 According to the present invention there is provided a method for reducing fatigue loads in the components of a wind turbine subjected to asymmetrical loading of the rotor of the wind turbine, comprising the steps of:

- repeatedly collecting and storing load data of the rotor of the wind turbine,
- 25 determining a load distribution function for the rotor from said stored data,
- deriving and processing a plurality of periodic functions on different multiple integers of the rotor frequency from said load distribution function,
- determining actions for a wind turbine control means for reducing the fatigue load of the wind turbine components from said derived and processed
- 30 plurality of periodic functions, and

implementing said determined actions in the wind turbine control means.

According to the present invention there is also provided a control system for reducing the fatigue loads in the components of a wind turbine subjected to

5 asymmetrical loading of the rotor plane of the wind turbine, comprising:

data collecting and storing means for repeatedly collecting and storing load data of the rotor of the wind turbine,

wind turbine control means for controlling the power capture of the wind turbine, and

10 data processing means for processing said collected load data of the rotor of the wind turbine and providing a control output accordingly,

said data processing means being adapted to determine a load distribution function for the rotor of the wind turbine from said stored load data, deriving and processing a plurality of periodic functions on different multiple
15 integers of the rotor frequency from said load distribution function, determining actions, based on said plurality of periodic functions, for said wind turbine control means for reducing fatigue loads on the wind turbine components, and providing a control output accordingly to the wind turbine control means.

Hereby it is possible to reduce the fluctuating loads on the wind turbine
20 components which facilitate less mechanical wear and tear on the most load-exposed parts of the wind turbine which in turn results in less required service, fewer break-downs and a prolonged life-span for the wind turbine. Alternatively it is hereby possible to increase the power capture of the wind turbine and maintain a low load on the rotor or combinations hereof.

25 In an aspect of the invention, said derived plurality of periodic functions is sinusoidal and/or cosinusoidal functions. By using derived sinusoidal and/or cosinusoidal functions, it is possible to approximate a pitch correction in close proximity of the desired.

In another aspect of the invention, the frequencies of said plurality of periodic
30 functions is limited series of different integer multiples of the rotor frequency e.g. up to four times the rotor frequency such as any of first, second, third and

3a

fourth multiply of the rotor frequency or combinations of at least two of said multiplies. By using limited series of periodic functions it is possible to quickly establish a pitch correction in close proximity of the desired, without requiring significant computational power.

- 5 In another aspect of the invention, at least an amplitude component and a phase component are determined for each of said derived periodic functions. Determining said amplitude and phase components facilitates the overall data processing in the computing means and facilitates the link in time and azimuth location between the asymmetrical rotor load and the corrective pitch action.
- 10 In another aspect of the invention, said plurality of periodic functions includes at least one function with a frequency equal to the rotor frequency. By including

periodic functions with a frequency equal to rotor frequency, it is possible to approximate a pitch correction close to the desired, simplified in a free or near free wind inflow situation.

5 In another aspect of the invention, said plurality of periodic functions includes at least one function with a frequency equal to four times the rotor frequency. By including periodic functions with a frequency equal to four times the rotor frequency, it is possible to approximate a pitch correction close to the desired, simplified in a partly or full wake situation.

10

In another aspect of the invention, said plurality of periodic functions are derived by means of a Discrete Fourier Transform applied to the load distribution function. By using Discrete Fourier Transformation to derive said plurality of periodic functions, it is possible to use well known, fast and liable programming techniques to implement
15 the program code on the computing means.

In another aspect of the invention, said plurality of periodic functions are derived by means of inverse relations between first periodic harmonic and measured blade modal amplitudes.

20

In another aspect of the invention, said plurality of periodic functions are derived by means of successive band-pass filtering applied to the load distribution function.

In another aspect of the invention, said plurality of periodic functions are derived by
25 means of a Recursive Least Square estimator applied to the load distribution function.

In another aspect of the invention, said load data are collected by measuring the blade root bending moments whereby a representative measurement can be obtained
30 preferable with already existing sensor means.

In another aspect of the invention, said bending moments are measured for at least one blade. By doing measurements on one blade only, data can be used to establish a optimized pitch correction applied to all blades, assuming that all rotor blades undergoes the same asymmetrical load as a function of one full rotor turn.

5

In another aspect of the invention, said bending moments are measured for more than one blade e.g. two blades of the wind turbine. By doing measurements on more than one blade, optimal individual pitch correction can be applied to each individual blade.

10

In another aspect of the invention, said bending moments are measured in two substantially perpendicular directions.

In another aspect of the invention, said load data are collected by measuring the angle of attack for the blades whereby a representative measurement can be obtained preferable with existing measuring means.

15

In another aspect of the invention, said load data are collected by measuring the forces on a wind turbine main shaft such as a low or high speed shaft.

20

In another aspect of the invention, said load forces on said shaft are measured in two substantially perpendicular directions.

In another aspect of the invention, said wind turbine control means comprises a blade pitch control mechanism in order to be able to implement said determined actions.

25

In another aspect of the invention, said load forces are measured continuous or for a predetermined period of time, depending on the degree and speed of variations in the wind inflow situation and on the necessity for measurement and control.

30

In another aspect of the invention, said predetermined period of time equals 0.01 to 0.5 full rotations of the rotor, preferably in the range from 0.1 to 0.3 full rotations of the rotor depending on necessity here for.

- 5 In another aspect of the invention, said predetermined period of time equals 0.5 to 6 full rotations of the rotor, preferably in the range from 0.75 to 3 full rotations of the rotor depending on necessity here for.

10 The invention also relates to a control system as well as a wind turbine and wind park.

Figures

The invention will be described in the following with reference to the figures in which

15

fig. 1 illustrates a large modern wind turbine including three wind turbine blades in the wind turbine rotor,

20

fig. 2 illustrates a reference system for measuring the Azimuth angle ψ . The azimuth ψ is defined by the position of blade 1,

fig. 3a illustrates schematically an example for direction of wind turbine rotor blade load measurements,

25

fig. 3b illustrates a coordinate reference system for measuring the wind turbine rotor blade loads,

fig. 4 illustrates schematically an embodiment of a control system for controlling the pitch angles of the wind turbine blades,

30

- fig. 5a illustrates the out of plane moment loads on the rotor blades of a 3 bladed wind turbine as a result of an idealized linear wind shear distribution between a rotor blade top position ($\psi = 0$ [rad]) and downward position ($\psi = \pi$ [rad]) corresponding to a free wind inflow situation,
- fig. 5b illustrates the transformed moment loads, m_{tilt} , m_{yaw} , as a function of azimuth for one full rotor rotation and as a result of the said linear wind shear distribution,
- fig. 6 illustrates the pitch angle error between a desired step function and a rotor-cyclic pitch angle regulation,
- fig. 7 illustrates schematically the functionality of the invented adaptive pitch system in a pitch controlled wind turbine,
- fig. 8a illustrates the out of plane moment loads on the rotor blades of a 3 bladed wind turbine as a result of a horizontal step shear corresponding to an idealized half wake inflow situation,
- fig. 8b illustrates the transformed moment loads, m_{tilt} , m_{yaw} , as a function of azimuth for one full rotor rotation and as a result of the said horizontal step shear,
- fig. 9 illustrates the difference between actual transformed moment loads m_{tilt} , m_{yaw} and filtered moment loads $m_{\text{tilt}}^{(h)}$ and $m_{\text{yaw}}^{(h)}$ as a result of a horizontal step shear corresponding to an idealized half wake inflow situation,

fig. 10 illustrates the pitch angle error between a desired step function and a harmonic pitch angle regulation, including a truncated number of harmonic components

5 Detailed description

Fig. 1 illustrates a modern wind turbine 1 with a tower 2 and a wind turbine nacelle 3 positioned on top of the tower.

10 The wind turbine rotor, comprising at least one blade such as three wind turbine blades 5 as illustrated, is connected to the hub 4 through pitch mechanisms 16. Each pitch mechanism includes a blade bearing and pitch actuating means which allows the blade to pitch in relation to the wind. The pitch process is controlled by a pitch controller as will be further explained below.

15

The blades 5 of the wind turbine rotor are connected to the nacelle through the low speed shaft 4 which extends out of the nacelle front.

As illustrated in the figure, wind over a certain level will activate the rotor and allow
20 it to rotate in a perpendicular direction to the wind. The rotation movement is converted to electric power which usually is supplied to the transmission grid as will be known by skilled persons within the area.

Fig. 2 illustrates how the Azimuth angle Ψ is measured as the angle between a
25 virtual vertical line thru the centre of the low speed shaft 4 and a virtual line defined by the two endpoints: a – the centre of the low speed shaft 4a, and b – the tip point of the rotor blade 7. The Azimuth angle is measured for one reference rotor blade e.g. blade 1 as a function of time and position.

30 Fig. 3a illustrates one rotor blade 5 of a wind turbine connected to the nacelle 3 through the low speed shaft 4 which extends out of the nacelle front.

The rotor blade is loaded by a wind force $F_{load}(t)$ dependent of e.g. the wind direction relative to the rotor blade, the area of the rotor blade, the pitch of the rotor blade etc. The said wind force which literally tries to break off the nacelle from the tower or the foundation produces a load bending moment m_x in the low speed shaft 4 and in the root of rotor blade 10 around its centerline 8.

Fig. 3b illustrates a formalized diagram of the in situ forces acting on one rotor blade illustrates the center point of the low speed shaft 4a, the horizontal centerline of the low speed shaft 8a, the vertical centerline of the rotor blade through the center point of the low speed shaft 9, a summarized wind force $F_{load}(t)$ and the direction of the load bending moment (or out of plane moment) m_x of blade number x.

Fig. 4 illustrates schematically a preferred embodiment of a control system for controlling the pitch angles of the wind turbine blades

Data of the wind turbine 1 are measured with sensor means 11 such as pitch position sensors, blade load sensors, azimuth sensors etc. The measured sensor data are supplied to computing means 12 in order to convert the data to a feedback signal. The feedback signal is used in the pitch control system 13 for controlling the pitch angle by establishing control values for controlling said at least one wind turbine blade 5.

The computing means 12 preferably includes a microprocessor and computer storage means for continuous control of the said feedback signal.

By continuously measuring the present load moments values on the rotor-blades, calculating an desired optimal pitch angle setting and feeding this information to the pitch control system in a closed feedback loop it is possible to optimize the control values to (substantially) to control the rotor at the design limits of the wind turbine and especially the design limits of the wind turbine blades.

An example of prior art for controlling out of plane moment loads on wind turbine blades of a wind turbine is here described.

- 5 The blade root loads $M_R = [m_1 \ m_2 \ m_3]^T$ on the rotor blades of a 3 bladed wind turbine are defined as a result of a given linear wind shear distribution between a rotor blade top position ($\psi = 0$) and down-ward position ($\psi = \pi$) corresponding closely to an idealized free wind inflow situation.

- 10 Fig. 5a illustrates a typical picture of said moments for free inflow conditions.

Transforming M_R into a coordinate system defined by the tilt, yaw and thrust equivalent directions, the respective moments loads m_{tilt} , m_{yaw} , m_{sum} become:

$$\begin{aligned}
 15 \quad m_{\text{tilt}} &= m_1 \cdot \cos(\Psi) + m_2 \cdot \cos\left(\Psi + \frac{4}{3}\pi\right) + m_3 \cdot \cos\left(\Psi + \frac{2}{3}\pi\right) \\
 m_{\text{yaw}} &= -m_1 \cdot \sin(\Psi) - m_2 \cdot \sin\left(\Psi + \frac{4}{3}\pi\right) - m_3 \cdot \sin\left(\Psi + \frac{2}{3}\pi\right) \\
 m_{\text{sum}} &= m_1 + m_2 + m_3
 \end{aligned}$$

- For the loads illustrated in figure 5a, the said transformed moment loads, m_{tilt} , m_{yaw} ,
 20 are illustrated in fig. 5b as a function of one full rotation of the rotor. For this idealized example of a prior art, m_{tilt} , m_{yaw} are constant.

- The close to sinusoidal behavior of M_R as illustrated in fig. 5a will result in fatigue loads on the rotor blades. A technique to partly compensate for these altering loads
 25 on the rotor blades can therefore be to individually control the rotor blades during a full rotation of a blade in order to level the distribution of wind forces i.e. a rotor blade is pitched less into the wind at the top than at the bottom of the rotating movement performed by the rotor including the blades.

Due to this close relation between M_R and the desired controlling of the pitch angle, the desired pitch control signal is also a function of the Azimuth angle i.e. a sinusoidal function on a frequency equal to the rotor-rotation frequency. This technique is called cyclic or rotor-cyclic pitch of the wind turbine blades i.e. a cyclic change of the pitch angle during a full rotation of a blade.

When the rotor blade enters a wake it is exposed to a step-like shearing force. This has been confirmed by actual measurements on wind turbines. Still in order to keep a constant load on the rotor blades under this condition, said rotor-cyclic pitch control can be applied resulting in a basic optimization of the load. But as the affected load is of step-like behavior and the said rotor-cyclic pitch control is of sinusoidal behavior there will always occur a non negligible alternating force on the rotor blades.

This is illustrated in Fig. 6 for said idealized half-wake situation. The curve 14 illustrates a desired abrupt change in pitch angle control and the curve 15 illustrates an actual corrective pitch angle control applied by the said rotor-cyclic pitch technique. Due to the difference between the two curves, an angle error 16 is introduced still resulting in a possibility of increased fatigue loads on the rotor blades.

20

An example of the present invention for controlling out of plane moment loads on wind turbine blades of a wind turbine is here described.

Fig. 7 illustrates for the present invention a preferred embodiment of the said control system for controlling the pitch angles of the wind turbine blades.

25

The moment loads $M_R = [m_1 \ m_2 \ m_3]^T$ on the rotor blades and the azimuth angle ψ is measured by the sensor means and feed to the computer means.

M_R is transformed into a coordinate system defined by the tilt, yaw and thrust equivalent direction $M_T = [m_{\text{tilt}} \ m_{\text{yaw}} \ m_{\text{sum}}]^T = T \cdot M_R$

30

Where:

$$T = \begin{bmatrix} \cos(\Psi) & \cos\left(\Psi + \frac{4}{3}\pi\right) & \cos\left(\Psi + \frac{2}{3}\pi\right) \\ -\sin(\Psi) & -\sin\left(\Psi + \frac{4}{3}\pi\right) & -\sin\left(\Psi + \frac{2}{3}\pi\right) \\ 1 & 1 & 1 \end{bmatrix}$$

The inverse relation is given by: $M_R = T^{-1} \cdot M_F$

5

M_F is data processed by a filter (II) to $M_F^{[h]}$, deriving and processing a plurality of harmonic functions on different multiple integers of the rotor frequency (ω_{nom}) in order to adapt the pitch angle control system to minimize the fluctuations on measured load data in such a way, that the loads on the rotor blades are kept constant or nearly constant.

10

A preferred embodiment of said data processing filter (H) is a Recursive Least Square (RLS) Estimator with exponential forgetting. This is a mathematical optimization technique that attempts to find a best fit to a set of data by attempting to minimize the sum of the squares of deviation between a set of observed data and a set of expected data.

15

The RLS processing algorithm is based on a few key-operators and can in a computer simulation be implemented after the following algorithm:

20

Simulation:

$$\varphi(t) = \begin{bmatrix} 1 & \cos(\omega_{nom} t) & \sin(\omega_{nom} t) & \cos(2\omega_{nom} t) & \sin(2\omega_{nom} t) & \cos(3\omega_{nom} t) & \sin(3\omega_{nom} t) \\ & & & \cos(4\omega_{nom} t) & \sin(4\omega_{nom} t) \end{bmatrix}^T$$

$$\theta = [a_0 \quad a_1 \quad b_1 \quad a_2 \quad b_2 \quad a_3 \quad b_3 \quad a_4 \quad b_4]^T$$

25

$R = 9 \times 9$ matrix initialized with zero elements

$G = 9 \times 1$ vector initialized with zero elements

13

$$\mu = 1/k_0$$

```

for p = 1..N          (p is expressed as simulation step
                        number, 1, 2, 3..)
5      t = p · Ts
      for i=1..3  (iteration over mtilt, myaw and msum)
          G(i) = (1 - μ) G(i) + μ φ(t) MF(i)
          R(i) = (1 - μ) R(i) + μ φ(t) φ(t)T
          θ(i) = (R(i))-1 G(i)
10      MF(i) = φ(t)T θ(i)
      end
end
end

```

In the above computer simulation example:

```

15  ωnom = the nominal cyclic rotor frequency
     φ    = the harmonic analysis vector (here including components up to the 4th
           harmonic)
     θ    = the harmonic amplitudes
     R    = is a 9×9 matrix, initialized with zero elements
20  G     = is a 9×1 vector, initialized with zero elements
     Ts  = the simulation step time
     μ    = a forgetting factor
     k0  = a positive integer defining the forgetting factor

```

25 It is worth noting that the said RLS filter is adaptive which yields that the output of the filter changes as a response to a change on the input.

A practical applied version of the data processing comprises computing means for digital data acquisition, harmonic analysis, RLS filter computation, data storage and D/A converting, continuously or for a predetermined period of time.

- 5 Due to time-delays in the sensor means, in the computer means and in the pitch control system, the corrective pitch angle control signal is time shifted in relation to the measured blade loads M_R . To correct for this, $M_F^{(h)}$ is time shifted equivalently to synchronize i.e. $M_{FS}^{(h)} = \text{timeshift}(M_F^{(h)})$

- 10 A general time shift of a sum of harmonic signals can be realized as follows:

$$s(t) = \sum_{i=1}^n a_i \cos(\omega_i t) + b_i \sin(\omega_i t)$$

so

$$s(t + \tau) = \sum_{i=1}^n P^{(i)T} C^{(i)}(t) Q^{(i)}(\tau) \quad , (1 \times 2) \times (2 \times 2) \times (2 \times 1) = (1 \times 1)$$

- 15 where:

$$P^{(i)} = [a_i \ b_i]^T$$

$$C^{(i)}(t) = \begin{bmatrix} \cos(\omega_i t) & -\sin(\omega_i t) \\ \sin(\omega_i t) & \cos(\omega_i t) \end{bmatrix}$$

20

$$Q^{(i)}(\tau) = [\cos(\omega_i \tau) \ \sin(\omega_i \tau)]^T$$

The filtered and time shifted signal $M_{FS}^{(h)}$ is transformed from the fixed reference system back to the rotating reference system by $M_R^{(h)} = T^{-1} \cdot M_{FS}^{(h)}$.

25

The signal $M_R^{[b]}$ is multiplied with a gain for the conversion to radians i.e.

$\beta_{dem}^{[b]} = \text{Gain} M_R^{[b]}$ and is added to the collective pitch demand signal $\beta_{dem}^{[c]}$.

Fig. 8a illustrates as an example moment loads $M_R = [m_1 \ m_2 \ m_3]^T$ on the rotor blades of a 3 bladed wind turbine as a result of a horizontal step shear corresponding to an idealized half wake inflow situation.

Transforming M_R into a coordinate system defined by the tilt, yaw and thrust equivalent direction, the respective moments loads m_{tilt} , m_{yaw} , m_{sum} become:

$$\begin{aligned} m_{\text{tilt}} &= m_1 \cdot \cos(\Psi) + m_2 \cdot \cos\left(\Psi + \frac{4}{3}\pi\right) + m_3 \cdot \cos\left(\Psi + \frac{2}{3}\pi\right) \\ m_{\text{yaw}} &= -m_1 \sin(\Psi) - m_2 \sin\left(\Psi + \frac{4}{3}\pi\right) - m_3 \cdot \sin\left(\Psi + \frac{2}{3}\pi\right) \\ m_{\text{sum}} &= m_1 + m_2 + m_3 \end{aligned}$$

m_{tilt} , m_{yaw} , are illustrated in fig. 8b as a function of one full rotation of the rotor.

Periodic functions like the functions illustrated in fig. 8b can be resolved as an infinite sum of sines and cosines called a Fourier series and can in this case generally be expressed as:

$$m(\Psi) = \frac{a_0}{2} + a_1 \cos(\Psi) + b_1 \sin(\Psi) + a_2 \cos(2\Psi) + b_2 \sin(2\Psi) + a_3 \cos(3\Psi) + b_3 \sin(3\Psi) \dots$$

where:

$$a_i = \frac{1}{\pi} \int_0^{2\pi} m(\Psi) \cos(i\Psi) d\Psi$$

$$b_i = \frac{1}{\pi} \int_0^{2\pi} m(\Psi) \sin(i\Psi) d\Psi \quad \text{for } i = 0, 1, 2, 3, \dots$$

The computation of Fourier series is known as Harmonic Analysis.

It is seen from the equation of $m(\Psi)$ that the Fourier series consists of a non-alternating component, components that alternate according to the basic parameter Ψ and a plurality of periodic functions of different integer multiples of the basic frequency. The weighted Fourier coefficients a_i, b_i determine the amplitude of each harmonic frequency in the original signal.

The said RLS estimator data processes a truncated number of periodic functions derived by the harmonic analysis e.g. the first four multiple harmonics of the basic rotor frequency. The purpose of the RLS estimator is to produce an output signal that is feed to the pitch control system in order to minimize the energy in the load signal M_R i.e. to minimize the fluctuating loads on the rotor blades.

For this idealized example the input signals 17, 19 representing the loads moments m_{tilt} , and m_{yaw} of M_F respectively are illustrated in figure 9. The output signals $m_{\text{tilt}}^{(h)}$ and $m_{\text{yaw}}^{(h)}$ of $M_F^{(h)}$ are represented by 18, 20 respectively. The said RLS filter has processed the first four multiple harmonics of the basic frequency.

The filtered signal $M_F^{(h)}$ is time shifted to a signal $M_{FS}^{(h)}$ and transformed from the fixed reference system back to the rotating reference system by $M_R^{(h)} = T^{-1} \cdot M_{FS}^{(h)}$

where:

$$T = \begin{bmatrix} \cos(\Psi) & \cos\left(\Psi + \frac{4}{3}\pi\right) & \cos\left(\Psi + \frac{2}{3}\pi\right) \\ -\sin(\Psi) & -\sin\left(\Psi + \frac{4}{3}\pi\right) & -\sin\left(\Psi + \frac{2}{3}\pi\right) \\ 1 & 1 & 1 \end{bmatrix}$$

Finally the filtered signal $M_R^{(h)}$ is gain $(\beta_{dem}^{(h)})$ adjusted added to an overall pitch angle control signal $\beta_{dem}^{(c)}$ defined by a wind turbine speed controller and the summarized control signal β_{dem} is feed to the pitch controller that effectuates the desired actions.

- 5 Fig. 10 illustrates a data processed pitch control signal, e.g. $m_1^{(h)}$ of $M_R^{(h)}$, from the example above, corresponding to an idealized half- wake situation. The curve 14 illustrates a desired abrupt change in pitch angle control and the curve 22 illustrates an actual corrective pitch angle control applied by the said rotor-cyclic pitch technique. The difference between the two curves is
10 illustrated by 21.

- The invention has been exemplified above with reference to specific examples of a wind turbine with a control system for controlling the wind turbine blades by pitch mechanisms. However, it should be understood that the invention is not limited to the particular examples described above but may be designed
15 and altered in a multitude of varieties within the scope of the invention e.g. in using other formulas and/or measuring data as a supplement.

- Throughout the description of this specification the word "comprise" and variations of that word, such as "comprises" and "comprising", are not intended to exclude other additives or components or integers.

20

Reference list

In the drawings the following reference numbers refer to:

- | | | |
|----|----------|---|
| | 1. | Wind turbine or wind turbine system |
| 5 | 2. | Wind turbine tower |
| | 3. | Wind turbine nacelle |
| | 4. | Low speed shaft |
| | 4a. | Center point of the low speed shaft |
| | 5. | Wind turbine rotor blade |
| 10 | 6. | Wind turbine rotor with at least one blade |
| | 7. | Tip point of a wind turbine rotor blade |
| | 8. | Centerline of the low speed shaft |
| | 8a. | Formalized centerline of the low speed shaft |
| | 9. | Vertical center line of the rotor blade through the center point of the |
| 15 | | low speed shaft |
| | 10. | Root of wind turbine rotor blade' |
| | 11. | Sensor means |
| | 12. | Computing means |
| | 13. | Pitch control system |
| 20 | 14. | Example of a desired step pitch angle |
| | 15. | Example of an actual rotor-cyclic correction of the pitch angle |
| | 16. | Angle error – rotor-cyclic angle correction |
| | 17. | Idealized m_{tilt} |
| | 18. | Filtered m_{tilt} |
| 25 | 19. | Idealized m_{yaw} |
| | 20. | Filtered m_{yaw} |
| | 21. | Angle error – harmonic angle correction |
| | 22. | Example of an actual harmonic correction of the pitch angle |
| | ψ . | Azimuth angle for rotor blade 1 relative to a fixed vertical reference |
| 30 | | position |

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

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1. A method of reducing fatigue loads in the components of a wind turbine subjected to asymmetrical loading of the rotor of the wind turbine, comprising the steps of:
 - repeatedly collecting and storing load data of the rotor of the wind turbine,
 - determining a load distribution function for the rotor from said stored data,
 - deriving and processing a plurality of periodic functions on different multiple integers of the rotor frequency from said load distribution function,
 - determining actions for a wind turbine control means for reducing the fatigue load of the wind turbine components from said derived and processed plurality of periodic functions, and
 - implementing said determined actions in the wind turbine control means.
2. A method according to claim 1 wherein the frequencies of said plurality of periodic functions are different integer multiples of the rotor frequency.
3. A method according to any one of the preceding claims, wherein for each derived periodic function at least an amplitude component and a phase component is determined.
4. A method according to any one of the preceding claims, wherein said plurality of periodic functions includes at least one function with a frequency equal to the rotor frequency and at least one function with a frequency equal to four times the rotor frequency.
5. A method according to any one of the preceding claims, wherein said plurality of periodic functions is derived by means of a Discrete Fourier Transform applied to the load distribution function.
6. A method according to any one of the preceding claims, wherein said plurality of periodic functions are derived by means of inverse relations between first periodic harmonic and measured blade modal amplitudes.

7. A method according to any one of the preceding claims, wherein said plurality of periodic functions are derived by means of successive band-pass filtering, applied to the load distribution function.

5 8. A method according to any one of the preceding claims, wherein said plurality of periodic functions are derived by means of a Recursive Least Square estimator applied to the load distribution function.

10 9. A method according to any one of the preceding claims, wherein said load data are collected by measuring blade root bending moments.

10. A method according to any one of the preceding claims, wherein said load forces are measured continuously or for a predetermined period of time.

15 11. A method according to claim 10, wherein said predetermined period of time is in the range from 0.01 to 0.5 full rotations of the rotor.

12. A method according to claim 10, wherein said predetermined period of time is in the range from 0.5 to 6 full rotations of the rotor.

20

13. A control system for reducing the fatigue loads in the components of a wind turbine subjected to asymmetrical loading of the rotor plane of the wind turbine, comprising:

data collecting and storing means for repeatedly collecting and storing load

25 data of the rotor of the wind turbine,

wind turbine control means for controlling the power capture of the wind turbine, and

data processing means for processing said collected load data of the rotor of the wind turbine and providing a control output accordingly,

30

said data processing means being adapted to determine a load distribution function for the rotor of the wind turbine from said stored load data, deriving and processing a plurality of periodic functions on different multiple integers of the rotor frequency from said load distribution function, determining actions, based on said plurality of periodic functions, for said wind turbine control means for reducing fatigue

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loads on the wind turbine components, and providing a control output accordingly to the wind turbine control means.

5 14. A control system according to claim 13, comprising means to collect and store data continuously or for a predetermined period of time.

10 15. A control system according to claims 13 or 14, comprising means to derive from said load distribution function a plurality of periodic functions with frequencies of different integer multiples of the rotor frequency.

15 16. A control system according to any one of claims 13 to 15, wherein said plurality of periodic functions includes at least one function with a frequency equal to the rotor frequency, and at least one function with a frequency equal to four times the rotor frequency.

17. A control system according to any one of claims 13 to 16, where said plurality of periodic functions is derived by means of harmonic analysis applied to said load distribution function.

20 18. A control system according to claim 14, or any one of claims 15 to 17 when dependent on claim 14, wherein said predetermined period of time is in the range from 0.01 to 0.5 full rotations of the rotor.

25 19. A control system according to claim 18, wherein said predetermined period is in the range from 0.75 to 3 full rotations of the rotor.

20. A control system according to claim 14, or any one of claims 15 to 17 when dependent on claim 14, wherein said predetermined period of time is in the range from 0.5 to 6 full rotations of the rotor.

30 21. A control system according to claim 20, wherein said predetermined period is in the range from 0.75 to 3 full rotations of the rotor.

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22. A control system according to any one of claims 13 to 21, comprising transducer means arranged to measure blade bending moments.

23. A wind turbine comprising a control system according to any one of claims 13 to 24 for reducing the fatigue loads in the components of the wind turbine subjected to asymmetrical loading of the rotor plane of the wind turbine.

24. A wind park comprising at least two wind turbines where at least one wind turbine is controlled with a system according to any one of claims 13 to 23 for reducing the fatigue loads in the components of the wind turbine subjected to asymmetrical loading of the rotor plane of the wind turbine.

25. A method for reducing fatigue loads in components of a wind turbine according to any one of the embodiments substantially as herein described with reference to the accompanying drawings.

26. A control system for reducing fatigue loads in components of a wind turbine according to any one of the embodiments substantially as herein described with reference to the accompanying drawings.

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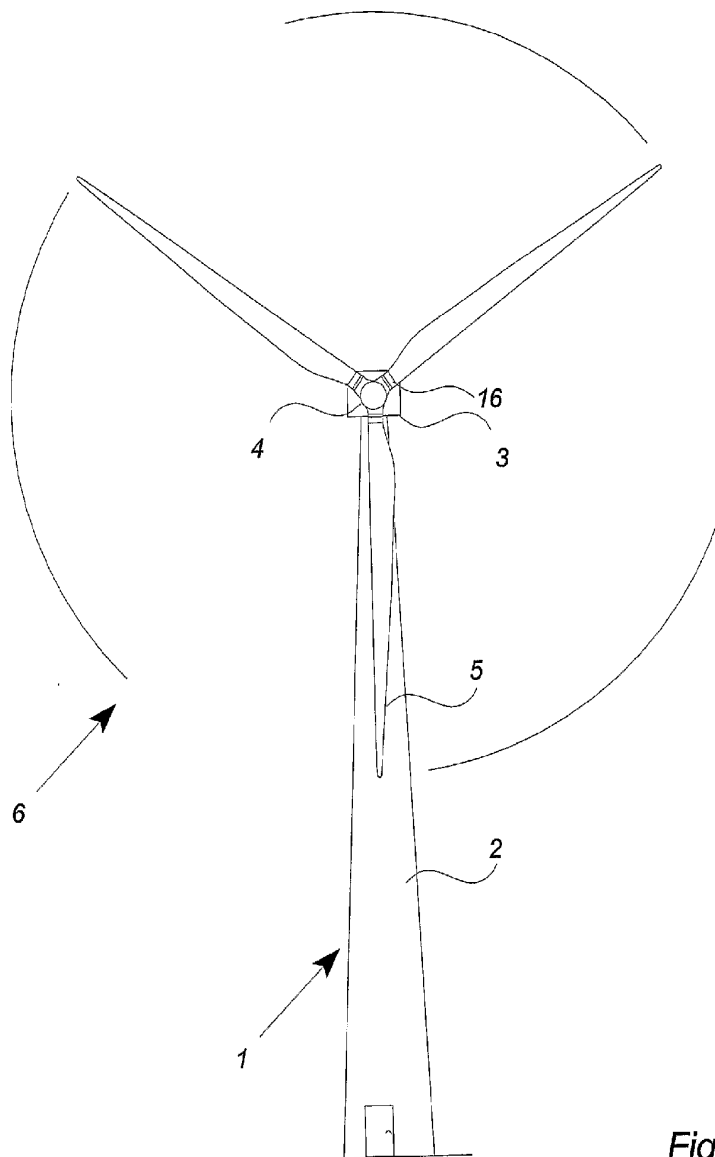
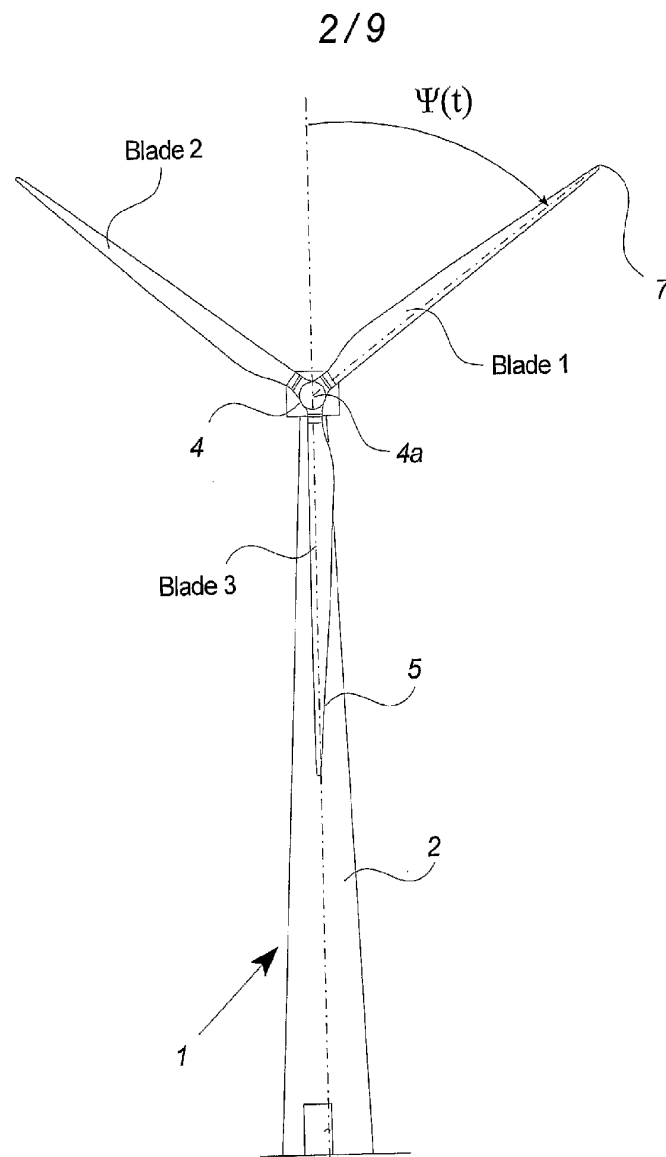
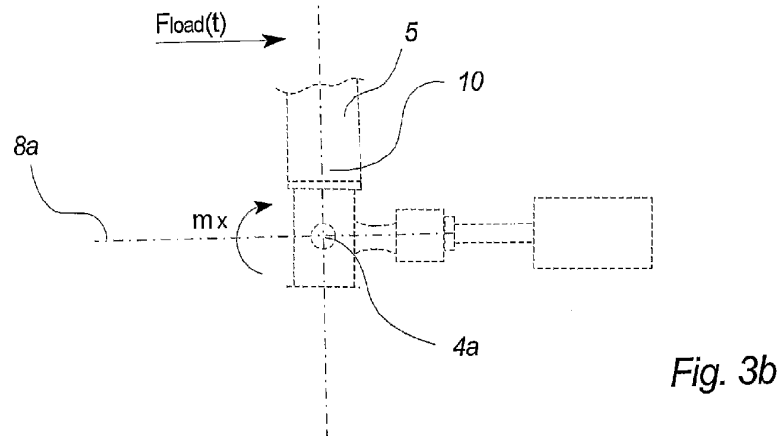
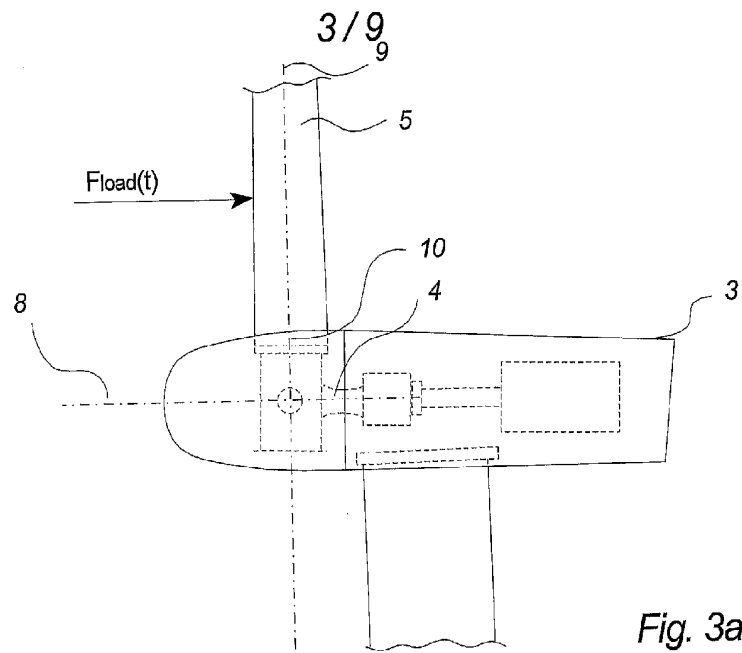


Fig. 1

*Fig. 2*



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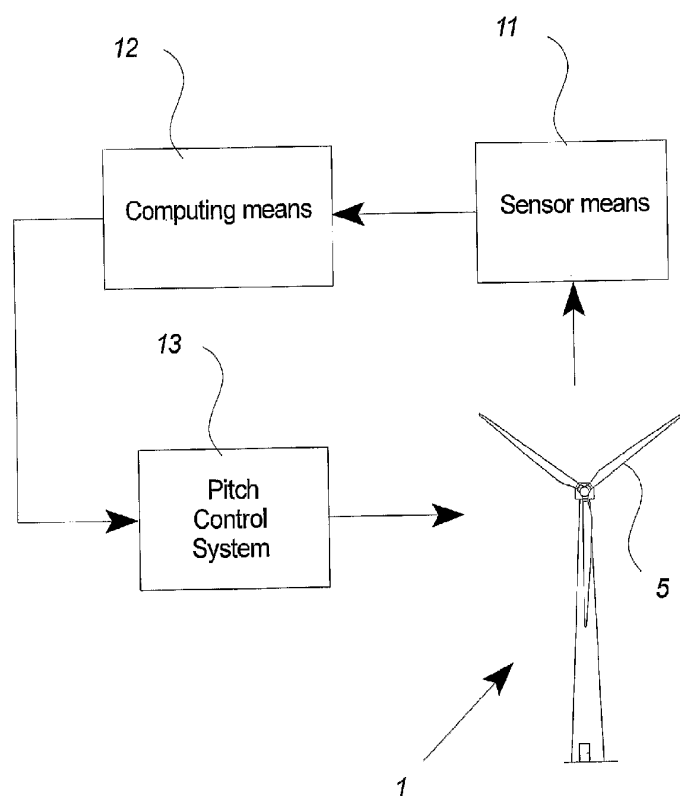


Fig. 4

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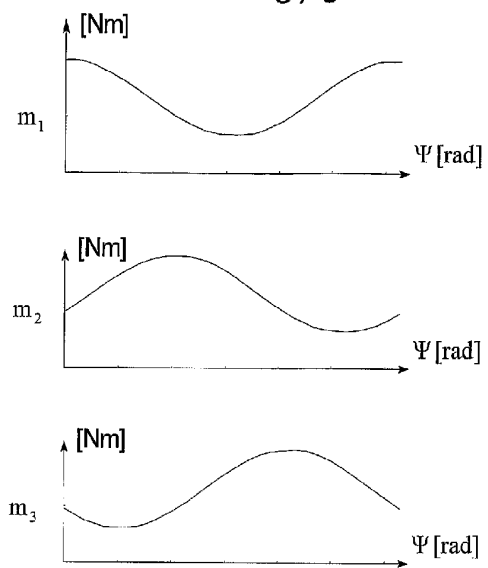


Fig. 5a

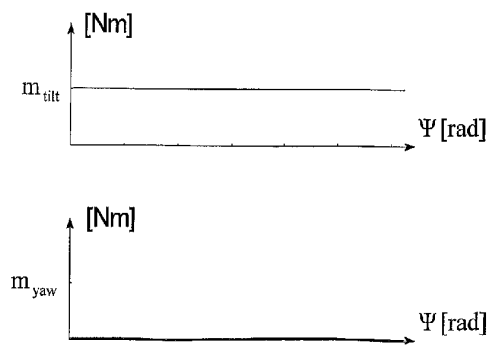
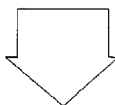


Fig. 5b

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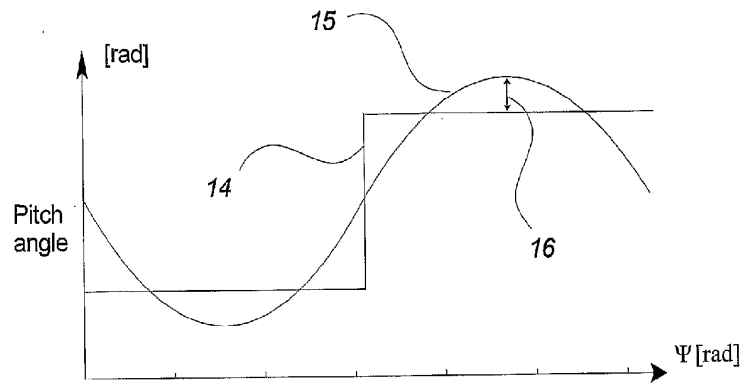


Fig. 6

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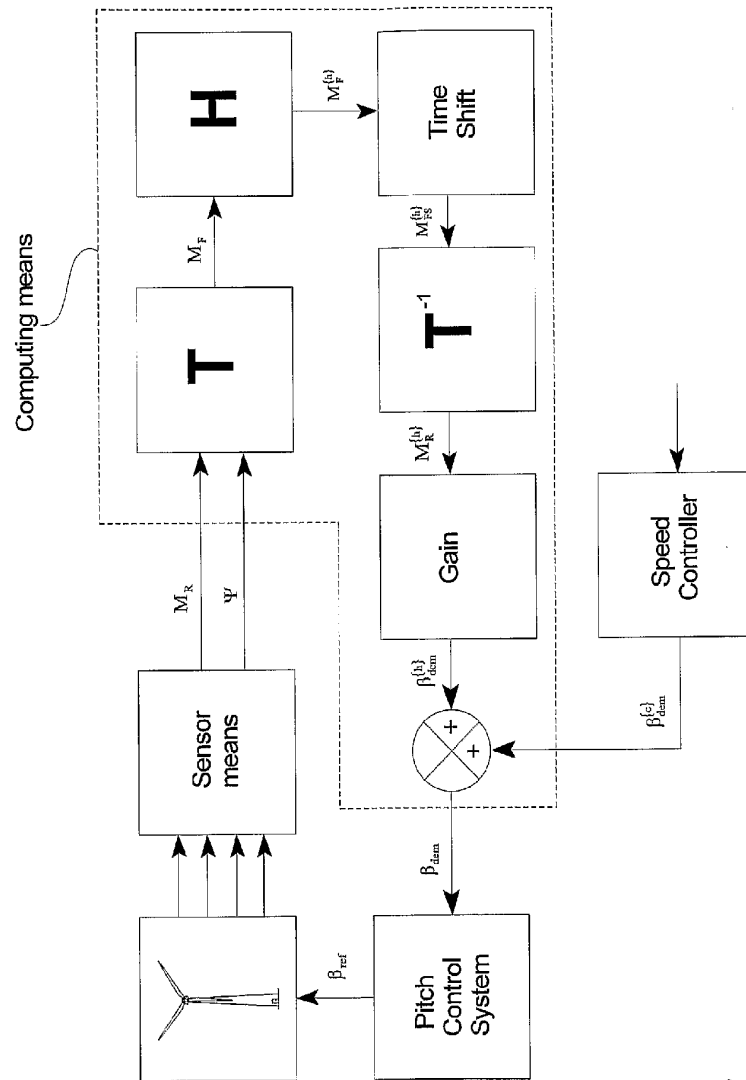


Fig. 7

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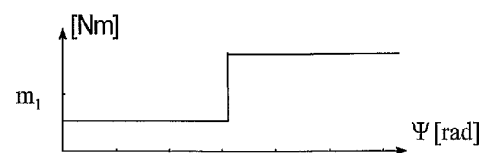


Fig. 8a

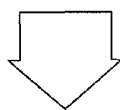


Fig. 8b

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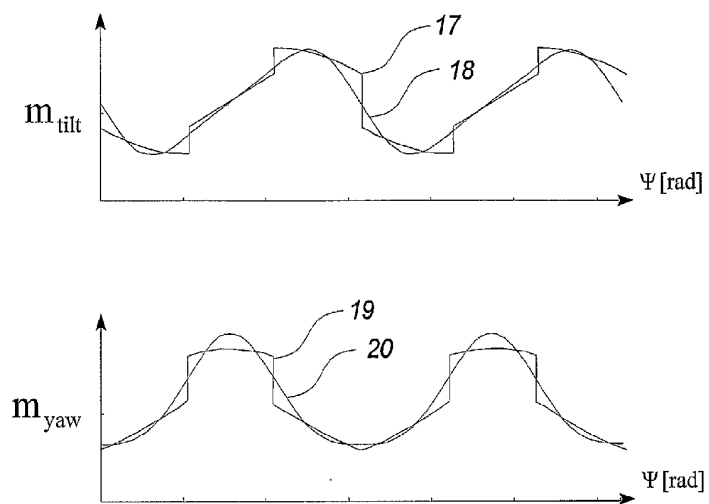


Fig. 9

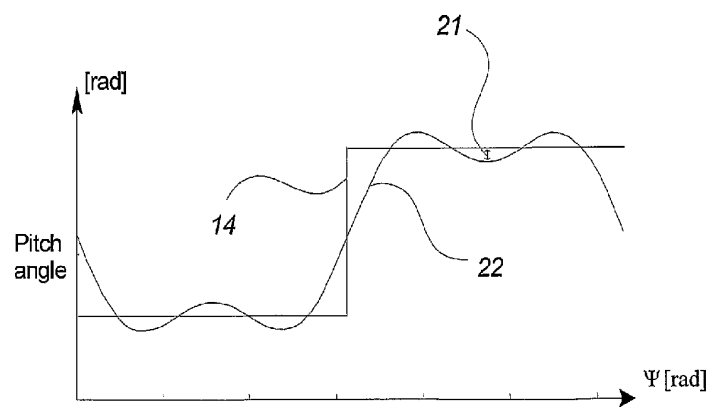


Fig. 10