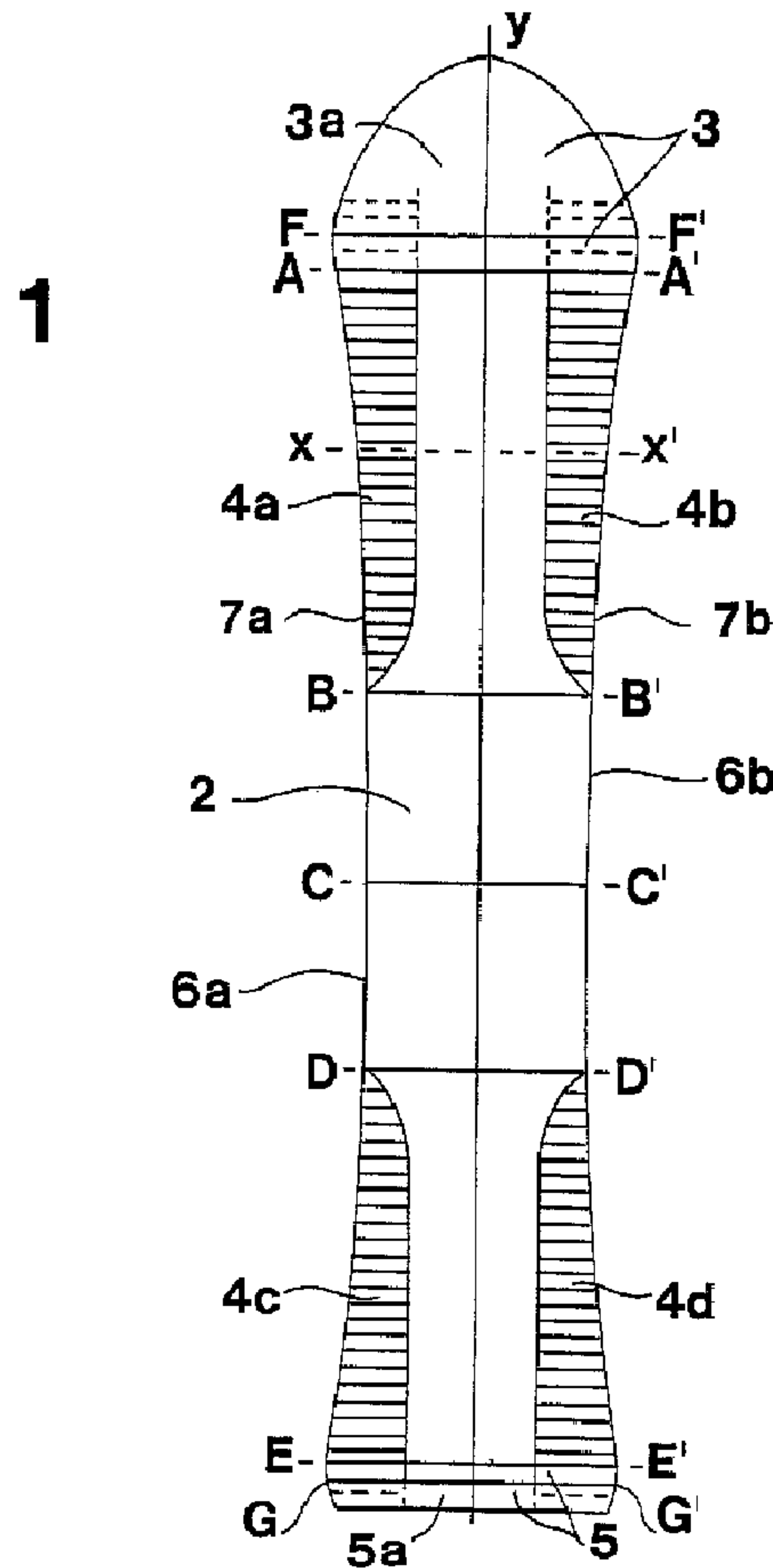




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(54) Titre : PAIRE DE SKIS ALPINS
(54) Title: AN ALPINE PAIR SKI



(57) Abrégé/Abstract:

An Alpine pair ski (1) comprises a flat first sliding surface (2) and lateral surfaces (6a, b) provided with an approximately continuous concave sidecut between a first transition line A-A' defining the transition from a main section to a front section (3) and a second



(57) Abrégé(suite)/Abstract(continued):

transition line E-E' defining the transition from the main section to a rear section (5), the course of a lower lateral edge (7a, b) between the transition lines A-A' and E-E' approximating a continuous curve. The sole on both sides of first sliding surface (2) comprises additional sliding surfaces (4) which extend upwards from the edge of the first sliding surface (2) to the lower lateral edges (7a, b) of the ski with an uplift (H_s) whose value at a point on the lower lateral edge (7a, b) of the ski is given by the length of the perpendicular from this point to said plane of the sole. The additional sliding surfaces (4) extend in the longitudinal direction of the ski at least from the first and second transition lines A-A' and E-E' respectively towards a transversal line C-C' behind the middle of the ski and in that section of the ski where the binding is attached, the width of the ski at the line C-C' being equal to the smallest width of the ski between line A-A' and E-E'. The uplift (H_s) in a lower lateral edge (7a, b) on the additional sliding surfaces (4) substantially increases with the ski's increasing width in the direction of the lines A-A' and E-E' respectively.



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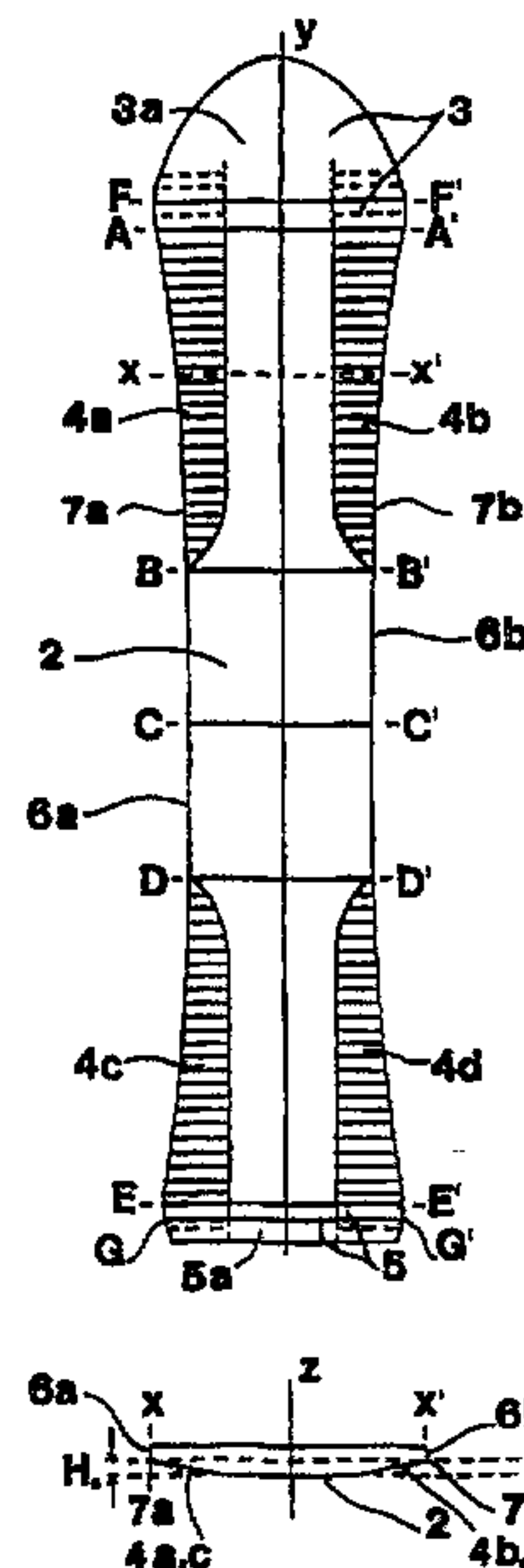
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(54) Title: AN ALPINE PAIR SKI

(57) Abstract

An Alpine pair ski (1) comprises a flat first sliding surface (2) and lateral surfaces (6a, b) provided with an approximately continuous concave sidecut between a first transition line A-A' defining the transition from a main section to a front section (3) and a second transition line E-E' defining the transition from the main section to a rear section (5), the course of a lower lateral edge (7a, b) between the transition lines A-A' and E-E' approximating a continuous curve. The sole on both sides of first sliding surface (2) comprises additional sliding surfaces (4) which extend upwards from the edge of the first sliding surface (2) to the lower lateral edges (7a, b) of the ski with an uplift (H_s) whose value at a point on the lower lateral edge (7a, b) of the ski is given by the length of the perpendicular from this point to said plane of the sole. The additional sliding surfaces (4) extend in the longitudinal direction of the ski at least from the first and second transition lines A-A' and E-E' respectively towards a transversal line C-C' behind the middle of the ski and in that section of the ski where the binding is attached, the width of the ski at the line C-C' being equal to the smallest width of the ski between line A-A' and E-E'. The uplift (H_s) in a lower lateral edge (7a, b) on the additional sliding surfaces (4) substantially increases with the ski's increasing width in the direction of the lines A-A' and E-E' respectively.



AN ALPINE PAIR SKI

5 The invention concerns an Alpine pair ski with a front section including an upturned tip, a rear section including an end portion, and a main section with a sole which comprises, with reference to a plane of the sole with the ski's camber reduced to zero e.g. by applying a load to the ski, a flat first sliding surface which extends on both sides of the ski's central longitudinal axis Y at least to the front and rear sections respectively, and where the ski's lateral surfaces are provided with an approximately continuous concave sidecut between a first transition line A-A' defining the transition from the main section to the front section and a second transition line E-E' defining the transition from the main section to the rear section of the ski, the course of a lower lateral edge between the transition lines A-A' and E-E' approximating a continuous curve with a radius of curvature in any arbitrary point between the first and second transition line of 80 m or less.

15 In NO-PS 172 170 there is disclosed an Alpine pair ski which on a maximum 20 cm long front section of the main section has lateral surfaces whose lower edges diverge so greatly upwards in relation to the sliding surface and outwards sideways in relation to the ski's longitudinal axis that at the transition between the main section and the tip the ski has a width which is 15-70% greater than the width at the transition between this front section and the rest of the main section and where the lower edge of each lateral surface at the transition between the main section and the tip is located at a vertical distance above the plane of the sliding surface on the greater part of the main section, this vertical distance being at least 10% of the increase in width from the transition between the said front section and the main section to the transition between the main section and the tip.

The object of this known ski was to make it possible to turn with the least possible loss of kinetic energy, since the ski does not cut too deeply into the snow surface but nevertheless permits a good grip to be obtained when skidding.

30 Recent developments in the various branches of Alpine skiing, however, have involved not only an increase in speed, but also a considerable intensification of the demands on turning technique. In general the branches of Alpine skiing have become more extreme and this places increasing demands on the design of the skis. The above-mentioned known ski has an extreme outward curve in a front,

20 cm long section, this outward curve being out of proportion with the rest of the ski's outward curve. The extreme outward curve will make such a ski unstable during high speed and lead to problems with vibration. In addition the prior art ski will also lack a clean cutting edge, which means that the track
5 which the front part of the ski carves in the snow will not be utilized by the rear sections of the ski.

The object of the present invention is therefore to provide a pair of Alpine skis which avoid the above-mentioned and other disadvantages and thus also make it possible to perform fairly tight turns at high speed without the ski edging or
10 throwing up snow.

These objects are obtained according to the invention with a pair of Alpine skis which are characterized in that the sole on both sides of the first sliding surface comprises additional sliding surfaces which extend upwards from the edge of the first sliding surface to the lower lateral edges of the ski with an
15 uplift whose value at a point on the lower lateral edge of the ski is given by the length of the perpendicular from this point to said plane of the sole, the additional sliding surfaces extending in the longitudinal direction of the ski at least from the first and second transition lines A-A' and E-E' respectively towards a transversal line C-C', substantially perpendicular to the central
20 longitudinal axis Y behind the middle of the ski and in that section of the ski where the binding is attached, the width of the ski at the line C-C' being equal to the smallest width of the ski between line A-A' and E-E', the additional sliding surfaces thus extending on each side over a length which is at least 20% of the length of the main section between the lines A-A' and E-E', and such that
25 the length of the additional sliding surfaces in the main section from line A-A' toward line C-C' in any case is at least 20 cm, and that the uplift in a lower lateral edge on the additional sliding surfaces substantially increases with the ski's increasing width in the direction of the lines A-A' and E-E' respectively, with the result that in each case the uplift at A-A' is at least 1/2000 (one two
30 thousandth) of the length of the first sliding surface between the lines A-A' and E-E'.

Further features and advantages of the pair of Alpine skis according to the invention are apparant from the appendent claims.

The invention will now be described in more detail in connection with embodiments and with reference to the attached drawing.

Fig. 1 is a schematic plan view of an Alpine pair ski according to the present invention.

5 Fig. 2a-c is a cross section of the ski in fig. 1, viewed along line x-x'.

Figs. 3 and 4 are a plan view of different designs of the sole of the ski according to the present invention.

Fig. 5a-c is a side elevation of the skis in figs. 1, 3 and 4.

10 Figs. 6-8 are a plan view of further designs of the sole of the ski according to the present invention.

The embodiments of the ski according to the invention and as shown in the figures are all of a symmetrical ski. However, the ski according to the invention could also be an asymmetric ski, of which more shall be said later. The following discussion is, however, limited to embodiments of a ski that is
15 symmetrical around a central longitudinal axis and as shown in figs. 1-8.

Fig. 1 shows an Alpine pair ski 1 according to the present invention. The ski 1 has a main section with a sole which is located between the perpendicular transition lines A-A' and E-E' on a central longitudinal axis Y of the ski, line A-A' defining the transition to a front section 3 and line E-E' the transition to a
20 short, slightly upturned rear section 5 of the ski 1. The sole in the main section of the ski between A-A' and E-E' comprises a first sliding surface 2. Usually all skis have a longitudinal camber, that is, the ski has an upward curvature when unloaded. When the design load, i.e. the weight of the skier is applied to the ski, the camber is reduced towards zero and the sole of the ski will be resting in a
25 plane, which in the following description will be regarded as defined by the sliding surface 2. This sliding surface 2 extends substantially symmetrically about the ski's central longitudinal axis Y. On both sides of the sliding surface 2 there are provided additional sliding surfaces 4a, b, c, d which extend between the first sliding surface 2 and the lateral surfaces 6a, b of the ski which in the
30 representation in fig. 2 meet the sole in the lower lateral edges 7a, b, which is best illustrated in the section taken through x'-x' in fig. 1 and illustrated in one

of the figures 2a-c. In fig. 1 the first sliding surface 2 in the section between A-A' and a transverse line B-B' is limited by lateral edges substantially parallel to the central longitudinal axis Y and the section between E-E' and an additional transverse line D-D' has been given a corresponding form. In the section
5 between B-B' and D-D' the first sliding surface 2 extends all the way until it meets the lateral surfaces 6a, 6b in the respective lower lateral edges 7a and 7b. The additional sliding surfaces 4a-d thus extend from the first sliding surface 1 towards the lower lateral edges 7a and 7b in those sections of the sole which are located between A-A' and B-B' respectively and between D-D' and E-E'
10 respectively. The distance between A-A' and B-B' and D-D' and E-E' should together comprise at least 20% of the length of the ski between A-A' and E-E', and preferably 50% or more, depending on the desired functional performance of the ski.

As is known per se the lateral surface of the ski 1 between A-A' and E-E' is
15 provided with a concave sidecut in the direction of the ski's central longitudinal axis Y, thus causing the section of the ski between A-A' and E-E' to be substantially indented. The transversal line C-C' which is located between A-A' and E-E' is situated approximately at the middle of the ski or slightly behind it, approximately where the binding is located. C-C' is perpendicular to the ski's
20 central longitudinal axis Y and can represent a transversal axis X orthogonal to the central longitudinal axis Y, the X,Y plane thus simultaneously defining the plane of the first sliding surface. Over the width of the ski the transverse line C-C' has an extension which in any case equals the minimum width of the ski between A-A' and E-E'.

25 As shown in fig. 1, the transition line A-A' as mentioned marks the transition to a front section 3 including the upturned tip 3a of the ski. The curve of the sidecut has a turning point at the line A-A'. The width of the ski however increases towards a transversal line F-F' marking the transition to the tip 3a and usually also defining the maximum width of the ski. Depending on the
30 parameters chosen for the sidecut, distance between A-A' and F-F' may be very small, but usually lies between 2 and 5 cm.

Similarly the transition line E-E' as mentioned marks the transition to a rear
section 5 with the curve of the sidecut having a turning point in E-E'. The transversal line G-G' marks the transition to a usually upturned end portion 5a of
35 the ski.

- The sidecut or outward curve of the ski's lateral surfaces 6a and 6b between A-A' and E-E' follows approximately the line of a continuous curve and can be approximately defined by congruent circular arcs or elliptic arcs on each side of the ski's central longitudinal axis Y. In the case of congruent circles C-C' forms an extension of the radius of the circle and the lower lateral edges 7a, 7c between the circular arcs A-A' and E-E' respectively. Similarly the transversal line C-C' can be the extension of the ellipse's minor axis and the lower lateral edges 7a, 7b the elliptic arcs which extend on each side of the point of intersection between C-C' and the lower lateral edges 7a, 7b.
- It should be understood that the sidecut of the lateral surfaces 6a and 6b can deviate slightly from a perfect circular arc or elliptic arc and may, for example, be larger or smaller than this. In general, however, this deviation should not be greater than in the case where, by means of two points in one of the lower lateral edges 7a, 7b, a 20 cm long section is defined, as measured on the central longitudinal axis Y, in this lower lateral edge, a circle which is drawn through the end points of this section together with its midpoint should have a radius which does not exceed 80 metres. If the sidecut of the lateral surfaces 7a and 7b between A-A' and E-E' is defined by circular arcs as described above, the radius of the defining circle should not deviate by more than $\pm 20\%$ from the imaginary circle which can be drawn through the starting and end points together with the midpoint of the randomly selected section on one of the lower lateral edges 7a or 7b. Similarly it is the case that, when the sidecut of the lateral edges 6a and 6b is defined by elliptic arcs, the radii of curvature in the elliptic arc within a corresponding randomly selected section should not deviate by more than $\pm 20\%$ from the radius of the imaginary circle which passes through the starting and end points together with the midpoint of this section.

Thus the degree of sidecut between A-A' and E-E' can be modified in such a way that for instance the portion of the ski which is located closer to A-A' than B-B' deviates from the defining circular or elliptic arcs. In theory, the sidecut of the lateral surfaces 6a and 6b could also be produced by the lateral surfaces being composed of short, straight surfaces, with the result that the lower lateral edges 7a and 7b would appear as the sides of a polygon, but it will be obvious that these sides of the polygon of course will approximate the continuous curve which defines the sidecut of the lateral surfaces, whether this is a circular arc, an elliptic arc or another continuous curve.

Finally each of the lateral surfaces 6a, b could be defined by mutually deviating curved shapes, for example by an ellipse and a circle respectively. This would give the ski a slight asymmetry about the central longitudinal axis Y and is not shown in the figures, but will be discussed below.

5 The additional sliding surfaces 4a-4d which extend from the edge of the first sliding surface 2 towards the lower lateral edges 7a and 7b have been provided with an upward curve or an uplift H_1 from the edge of the first sliding surface 2 towards these lateral edges, as is best illustrated in one of the figures 2a-c. Thus the lateral edges 7a, 7b will be located above the plane of the first sliding
10 surface 2 at a distance which is indicated by H_1 in fig. 2a-c and further in fig. 5a-c. The additional sliding surfaces 4a, b, c, d thus extend from the first sliding surface 2 with an upward curve towards the lower lateral edges 7a, b, and the line of the additional sliding surfaces 4a, b, c, d can thus be a straight oblique line or chamfering as illustrated in fig. 2a, but also in cross section form a
15 concave section as illustrated in fig. 2b or have a convex form towards the plane of the first sliding surface as illustrated in fig. 2c.

It is preferred that the additional sliding surfaces should have a form as illustrated in fig. 2a, since it is assumed that it is this form which gives the ski its best characteristics. It will also be possible to combine two or more forms. For
20 example, a rectilinear form could develop into a concave section form near the lower lateral edge.

Moreover the uplift H_1 should be in proportion to the increase in width of the ski which is obtained from the sidecut of the lateral surfaces, thus causing the uplift H_1 in a lower lateral edge to increase with the width of the ski in the
25 direction of A-A' and E-E' respectively. In other words, in fig. 1 the uplift at B-B' is zero, increasing towards A-A' in such a manner that the uplift curve at A-A' in each case constitutes at least one two thousandth ($1/2000$) of the distance between A-A' and E-E'. At the edge of the first sliding surface 2, i.e. the line or curve which defines the transition between the first sliding surface 2 and the
30 additional sliding surfaces 4a, b, c, d the uplift is of course zero, the additional sliding surfaces thus together having an upward curve in the direction of the lower lateral edges 7a, b while at the same time this upward curve increases in the direction of A-A' and E-E' respectively. Thus the additional sliding surfaces are raised above the plane of the first sliding surface to a degree which
35 substantially increases with the increasing width of the ski.

The first sliding surface 2 as well as the additional sliding surfaces 4a-4d shall at least extend to the transition lines A-A' and E-E', but may optionally be extended into the front section 3 and the rear section 5, terminating at the lines F-F' and G-G', respectively, as indicated in e.g. figs. 2, 3 and 4. In this case the uplift of the lower lateral edges 7a, 7b between A-A' and F-F' should be at least as large as the uplift in A-A'. Correspondingly the uplift H_s of the lower lateral edges 7a, 7b between E-E' and G-G' should be at least as large as the uplift in E-E'.

In fig. 1 the first sliding surface 2 extends to the lower lateral edge in the section between B-B' and D-D and here there is naturally no uplift. In other words the uplift of the additional sliding surfaces 4a, b, c, d is reduced to zero at D-D and B-B' respectively.

The uplift as defined at a random point on the lower lateral edge 7a, b can preferably be given as an approximate linear function of the increase in the width of the ski between C-C' and a perpendicular in the plane of the ski or its sole the central longitudinal axis Y at this point, the uplift being represented by the following formula

$$H_s = K_1 + K_2 \cdot \Delta X + M(y)$$

Here H_s is the upward curve in mm, K_1 and K_2 appropriate selected constants, ΔX the increase in width and $M(y)$ a function of the distance, i.e. the length of the ski between C-C' and the said perpendicular, since the functional value $|M(y)|$ should be less than 1 mm.

In calculating the ski the coordinate axes can preferably be located in such a manner that the Y axis is as illustrated in fig. 1 and C-C' constitutes the orthogonal X-axis, the X,Y plane defining the plane of the first sliding surface. As a basis for the calculation of the increase in width, i.e. the sidecut of the lower lateral surfaces 6a and 6b, congruent circular arcs or elliptic arcs can be used as described and the increase in width can then easily be calculated as a value ΔX for a corresponding increase ΔY in the length of the ski.

As a supplement to the description, in tables 1-5 numerical examples are given of the calculation of a symmetrical Alpine pair ski according to the present

invention, on the basis of selected parameters for the width of the ski at C-C' and the length of the ski between C-C' and A-A' and C-C' and E-E' respectively. The sidecut of the lateral surfaces has been defined by selecting the radius of a circle or the major and minor axes of an ellipse respectively.

5 Fig. 3 illustrates a second embodiment of the ski 1, where the sliding surface 2 is distinguished from that in fig. 1 by being limited by straight lines between A-A' and E-E' parallel to the ski's central longitudinal axis Y. The additional
10 sliding surfaces 4e, f thus extend between the lower lateral surfaces 6a, b and the first sliding surface 2 on both sides of this and along the entire length of the ski between A-A' and E-E' or between F-F' and G-G' if preferred, the lower
lateral edges 7a, b over the entire distance between A-A' and E-E' thus obtaining an uplift. Here too the uplift increases with the increasing width of the ski in the
15 direction of A-A' and E-E', the uplift in each case thus having a minimum value in the lateral edges at C-C'. At the same time the uplift in C-C' should not be too great since otherwise the ski may acquire an unsatisfactory edge grip in the
middle, and it should have a maximum of 2 mm and preferably not more than 1 mm.

In fig. 4 the lower sliding surface is still limited by straight, parallel lines, but preferably in the vicinity of C-C' the first sliding surface 2 is moved right out to
20 the lower lateral edge and touches it at the point of intersection between C-C' and the lower lateral edges 7a, 7b. In this case the uplift is zero or practically zero at C-C', but increases again from C-C' towards A-A' and E-E' in relation to the increasing width, i.e. the outward curve of the lateral edges towards A-A' and E-E'.

25 Fig. 5a-5c is a side elevation of the skis in figs. 1, 3 and 4 respectively. The degree of the uplift H_s in the longitudinal direction is illustrated and indicated by the line of the lower lateral edge 7 in the lateral surface 6 of the ski. In fig. 5a there is no uplift in that section of the ski which is located between B-B' and D-D', while in fig. 5b it can be seen that the lateral edge has an uplift H_s which
30 reaches a minimum at C-C', whereupon it increases in the direction of A-A' and E-E' respectively. Finally fig. 5c shows that the uplift H_s decreases from A-A' and E-E' respectively towards C-C' until it becomes zero at the point where C-C' meets the lower lateral edge 7.

Other examples of possible designs of the sole with the first sliding surface 2 and the additional sliding surfaces 4 are illustrated in fig. 6, where the first sliding surface 2 between A-A' and B-B' and also between D-D' and E-E' is limited by lines which cause the sliding surface 2 to converge from the lower lateral edges 7a, b in B-B' and D-D' respectively and towards A-A' and E-E' respectively. Thus in the section between B-B' and D-D', in this case the first sliding surface extends to the lower lateral edge 7a, b of the ski and consequently the uplift of the lower lateral edge between B-B' and D-D' is zero.

In fig. 7 the first sliding surface 2 converges towards A-A' and E-E' respectively and just touches the lower lateral edges 7a and 7b at the point of intersection between C-C' and the lower lateral edges 4A, 4B,, the uplift at C-C' thus becoming zero and otherwise increases gradually from C-C' towards A-A' and E-E' respectively.

Fig. 8 illustrates an embodiment of the ski according to the invention in which the first sliding surface 2 is provided with a contour which is closer to the embodiment shown in fig. 4, but differs from this in that the edges of the first sliding surface 2 are not parallel lines, but converge from C-C' in the direction of A-A' and E-E' respectively. Thus the first sliding surface 2 has a maximum width at C-C', but this maximum width is less than the width of the ski at C-C' and consequently the additional sliding surfaces 4e,f extend on each side of the first sliding surface 2 over the entire length of the ski between A-A' and E-E', the lower lateral edge in C-C' thus having an uplift which is not zero and from C-C' increases with the increase in width in the direction of A-A' and E-E' respectively.

It will be obvious to a person skilled in the art that further designs of the form of the sliding surfaces are possible within the scope of the invention and they need not be limited to those designs illustrated in the figures. However, experience shows that for an Alpine pair ski with good turning characteristics and which are easy for even a skier with little experience to manoeuvre, the embodiment illustrated in fig. 4, in which the first sliding surface 2 is partially limited by straight parallel lines and extends to the lower lateral edge at C-C', appears to be particularly appropriate. However, it should be noted that the embodiments in figs. 1 and 4 are practically similar, so the uplift H_s in C-C' and its vicinity is at a minimum.

As mentioned above the ski according to the invention may be asymmetrical about the central longitudinal axis Y. The asymmetry may be obtained in different ways. For instance the sidecut of each of the lower edges may be dissimilar, such that the radius of curvature between the transition lines A-A' and E-E' in an arbitrary point on a lower lateral edge 7a, 7b is different from the radius of the curvature in a corresponding arbitrary point on the other lower lateral edge 7a; 7b when the arbitrary points are lying on a line orthogonal to the central longitudinal axis Y of the ski. If the sidecut of the lateral surfaces 6a, 6b is similar, the asymmetry may be provided by moving the lateral surfaces in mutually opposite directions towards the front and the rear of the ski, respectively. In any case, the resulting transition lines A-A', E-E' will be non-perpendicular to the ski's central axis Y, and also possibly mutual non-parallel lines. The merits of an asymmetrical ski is, however, a matter of discussion among persons skilled in the art. An asymmetrical ski may, however, offer some advantage when it is considered that the turning radius of the inner edge of the leading ski in a turn will be less than the turning radius of the outer edge. The table 6 gives a numerical example of calculation of an asymmetrical Alpine pair ski according to the present invention on the basis of selected parameters for the length of the ski between C-C' and A-A' and C-C' and E-E', respectively.

The Alpine pair ski according to the present invention offers a number of advantages over known skis of a similar type. As already mentioned, the sidecut of the lateral surfaces, i.e. the outward curve, permits the ski to make very sharp turns without throwing up snow. If the preferred sidecut of the lateral surfaces follows the curvature in a circular arc or elliptic arc, it will be possible to deviate from this arc form in order to compensate for dynamic conditions which arise when the ski is in use, i.e. primarily torsional forces and bending forces. In practice this indicates that the sidecut of the lateral surfaces should increase slightly more than the radius of curvature of the arc indicates, the closer one comes to A-A'. This will give the ski a clean cutting edge and will mean that the track carved by the ski's front section can also be used by the ski's rear section.

If a ski is completely rigid, even a fairly small sidecut of the lateral surfaces 6a, 6b, i.e. a small outward curve, will result in the ski losing contact with the snow surface in the midsection when it is edged in order to turn. The greater the sidecut and outward curve, the more flexible a ski with a flat sole must be in order to obtain a good edge grip on the midsection of the ski. If the outward curve is too great, a flat ski requires such a low degree of flexural rigidity that it

is of no practical use. With the ski according to the present invention the use of an uplift in the lower lateral edges will permit a combination of a high degree of sidecut, i.e. a substantial outward curve, while retaining a reasonable degree of flexural rigidity and thereby a good edge grip, since the uplift in the lower lateral edges of the ski according to the present invention is adapted all the way to the sidecut or outward curve of the lateral surfaces. It is known in the prior art that a given sidecut or outward curve can be compensated for by, amongst other things, reducing the flexural rigidity in the direction of the ski's tip and rear edge and partly also by reducing the torsional rigidity in the same directions. In addition the present invention provides a ski in which the outward curve is compensated by a corresponding uplift in the lower lateral edge. There is agreement amongst those skilled in the art that a sidecut can offer considerable advantages and according to the present invention it is possible to make this sidecut relatively substantial, since in any case the uplift compensates for the increased sidecut without necessitating a reduction of the flexural rigidity or torsional rigidity in the direction of the ski's tip or rear end, as was previously the case. According to the present invention, therefore, the uplift employed should increase with the increase in width, i.e. with the outward curve of the lateral surfaces due to their sidecut, and in such a manner that the uplift increases with the increasing distance from C-C' towards the tip and rear edge of the ski. In the case of the ski according to the present invention, however, in sections around C-C' the sidecut and outward curve are extremely moderate, with the result that if the flat sliding surface extends all the way to the lower lateral edges in this section of the ski, and the transverse line C-C' is located in the plane of the first sliding surface 2, in practice a substantial section of the sole on both sides of C-C' will also be located in the plane of the first sliding surface 2, this sliding surface thus extending all the way to the lower lateral edge 7a, 7b on both sides, even though it may in theory be considered ideal for the uplift of the lateral edges 7a, 7b to constantly increase with the increasing width from C-C' in the direction of A-A' and E-E' respectively.

As is well known to those skilled in the art, a substantial sidecut results in an excessively strong edge grip at front and rear parts of the ski, which in turn causes the front part of ski to be inclined to carve into the snow, while at the same time vibrations occur in the ski. Previously, however, the desire for a good edge grip has caused the designers to relinquish the idea of giving the lateral edges an uplift, while at the same time choosing to refrain from making the sidecut too great. According to the present invention a ski is provided which

permits an edge grip to be obtained which is neither too great nor too small, since the uplift of the lower lateral edge increases with an increasing outward curve. The result is that the ski acquires a highly favourable shape even with a substantial sidecut, while at the same time there is no necessity to reduce
5 flexural rigidity or torsional rigidity, and hence the ski according to the present invention retains the good dynamic properties normally found in a ski with a slight sidecut.

It has been shown to be particularly advantageous for the first sliding surface 2 between A-A' and E-E' or at least from A-A' or E-E' towards C-C' to be limited
10 by straight lines parallel to the central longitudinal axis when the ski has curved lateral surfaces 6a, 6b. The outward curve in the section between lines C-C' and E-E' combined with a flat sliding surface over the entire sole will for instance exhibit a greater gliding resistance due to the increase in width of the ski between C-C' and E-E' in this case. It is thus evident that the ski according to
15 the present invention wherein the width of the first gliding surface 2 is independent of the sidecut, may also offer advantages when gliding or skiing approximately straight ahead.

In certain snow conditions the fact that the first, flat sliding surface 2 has some degree of limitation in relation to the sole's total surface will provide a better
20 glide. When the lower lateral edges 7a, b of the ski according to the present invention are provided with an uplift, this requires the flat sliding surface to be limited. This too is a factor which offers advantages when gliding or skiing approximately straight ahead.

Known skis which have a high degree of sidecut and a substantial outward curve
25 and a flat sliding surface can prove dangerous for a skier at high speed, especially in flat sections where it will be easy for the ski to "catch" an edge. This problem has proved to be particularly relevant after a nasty and widely reported Alpine skiing accident at Garmisch-Partenkirchen in the winter of 1994, but it can be eliminated to a considerable extent by using a ski according to the
30 present invention whose lateral edges are provided with a harmonic uplift in relation to the outward curve. For instance in a ski with a flat sole, in transition from a left turn to a right turn (or vice versa), the grip will change almost instantaneously from the left to the right edge, but with ski according to the invention, the grip of the left edge is gradually reduced, while the right edge
35 grip subsequently gradually increases.

Examples

The attached tables 1-6 give examples of numerical calculation of the pair of Alpine skis according to the present invention.

5 In the first example which is found in table 1, the ski has a length of 2050 mm and a minimum width at C-C' of 55 mm. The outward curve of the lateral edges is calculated by means of a circle and an ellipse respectively and values for the ski's width in the various cases are specified at 50 mm intervals over a distance of 150 mm from the tip to the rear edge. The uplift as a function of the increases in width is found in columns 3-5 in the table, column 3 specifying an
10 uplift which increases linearly with the increase in width, column 4 an uplift which has a non-linear relation to the increase in width and column 5 an uplift which is in linear relation to the increase in width, but with the addition of a correction factor.

15 Example 2 concerns a ski with a length of 1900 mm and minimum width of 60 mm. The calculation results are presented in table 2 which is set up in the same way as table 1.

Example 3 concerns a ski with a length of 2100 mm and with a particularly substantial outward curve, especially at A-A'. The calculation results are presented in table 3 which is set up in the same way as table 1.

20 Example 4 concerns a ski with a length of 2090 mm and a relatively slight uplift. The calculation results are presented in table 4 which is set up in the same way as table 1. The ski according to table 4 is particularly suitable for skiing at high speed or when gliding or skiing approximately straight ahead. This is particularly the case when the value of the uplift is as specified in
25 column 5, since in this case a slight uplift is combined with a limitation of the first sliding surface 2.

Example 5 concerns a ski with a length of 2010 mm, being rather more extreme than the one in example 4, but with a moderate uplift. The calculation results are presented in table 4 which is set up in the same way as table 1.

30 Finally example 6 concerns an asymmetric ski with a length of 2020 mm. The calculation results are presented in table 6, where the second and fourth columns

give the half-widths of the ski on each side of the central longitudinal axis Y. The corresponding uplifts are given in columns three and five respectively. The asymmetry arises from choosing different radii of curvature for the lateral surfaces respectively.

- 5 It will be evident from the above description and the examples that within the scope of the invention it will be possible to design a large number of variant emodiments of the ski according to the invention and thus obtain a ski which is optimal in regard of different objectives and various conditions of use.

TABLE 1

Parameters for the calculation of "AN ALPINE PAIRSKI". All measurements are in millimeters

Total width at A-A	Total width at C-C	Length C-A	Length C-E	% uplift of the side edge relative to the increase of the total width	Calculated radius for a circle with arc through C and A and with center on the X-axis
90	55	1000	800	10,0	28580

Equation 1 Uplift (mm) = 10,0 % x Increase of Width
 Equation 2 Uplift (mm) = 10,0 % x Increase of Width + 0,3mm
 Equation 3 $Y^2/A^2 + X^2/B^2 = 1$ (Ellipse)
 where A = 2000 and B = 130,7
 All three equations are valid between A-A' and E-E' only.

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
150	92,0	3,80	3,80	4,1	92,0	F-F'
200	90,0	3,50	3,50	3,8	90,0	A-A'
250	86,6	3,16	3,09	3,5	86,4	
300	83,3	2,83	2,70	3,1	83,0	
350	80,3	2,53	2,33	2,8	79,8	

TABLE 1 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
400	77,4	2,24	1,99	2,5	76,8	
450	74,7	1,97	1,66	2,3	74,1	
500	72,1	1,71	1,36	2,0	71,5	
550	69,8	1,48	1,07	1,8	69,2	
600	67,6	1,26	0,81	1,6	67,0	
650	65,6	1,06	0,57	1,4	65,1	
700	63,7	0,87	0,35	1,2	63,3	
750	62,1	0,71	0,15	1,0	61,7	
800	60,6	0,56	0,00	0,9	60,3	
850	59,3	0,43	0,00	0,7	59,0	
900	58,1	0,31	0,00	0,6	58,0	
950	57,2	0,22	0,00	0,5	57,1	
1000	56,4	0,14	0,00	0,4	56,3	
1050	55,8	0,08	0,00	0,4	55,7	
1100	55,3	0,03	0,00	0,3	55,3	
1150	55,1	0,01	0,00	0,3	55,1	
1200	55,0	0,00	0,00	0,3	55,0	C-C'
1250	55,1	0,01	0,00	0,3	55,1	

TABLE 1 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
1300	55,3	0,03	0,00	0,3	55,3	
1350	55,8	0,08	0,00	0,4	55,7	
1400	56,4	0,14	0,00	0,4	56,3	
1450	57,2	0,22	0,00	0,5	57,1	
1500	58,1	0,31	0,00	0,6	58,0	
1550	59,3	0,43	0,00	0,7	59,0	
1600	60,6	0,56	0,00	0,9	60,3	
1650	62,1	0,71	0,15	1,0	61,7	
1700	63,7	0,87	0,35	1,2	63,3	
1750	65,6	1,06	0,57	1,4	65,1	
1800	67,6	1,26	0,81	1,6	67,0	
1850	69,8	1,48	1,07	1,8	69,2	
1900	72,1	1,71	1,36	2,0	71,5	
1950	74,7	1,97	1,66	2,3	74,1	
2000	77,4	2,24	1,99	2,5	76,8	E-E'
2020	78,0	2,30	2,06	2,6	77,4	G-G'
2050	75,0	4,00	4,00	4,3	74,0	End

TABLE 2

Parameters for the calculation of "AN ALPINE PAIRSKI". All measurements are in millimeters

Total width at A-A	Total width at C-C	Length C-A	Length C-E	% uplift of the side edge relative to the increase of the total width	Calculated radius for a circle with arc through C and A and with center on the X-axis
85	60	950	700	7,2	36106

Equation 1 Uplift (mm) = 7,2 % x Increase of Width All three equations

Equation 2 Uplift (mm) = 7,2 % x Increase of Width + 0,3mm are valid between

Equation 3 $Y^2/A^2 + X^2/B^2 = 1$ (Ellipse) A-A' and E-E'

where A = 1800

and B = 83

only.

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
160	86,0	1,90	1,90	2,2	92,0	F-F'
200	85,0	1,80	1,80	2,1	85,0	A-A'
250	82,4	1,62	1,56	1,9	82,2	
300	80,0	1,44	1,33	1,7	79,7	

TABLE 2 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
350	77,7	1,28	1,12	1,6	77,3	
400	75,6	1,12	0,92	1,4	75,1	
450	73,6	0,98	0,73	1,3	73,1	
500	71,7	0,84	0,56	1,1	71,2	
550	70,0	0,72	0,39	1,0	69,5	
600	68,4	0,60	0,24	0,9	67,9	
650	66,9	0,50	0,11	0,8	66,5	
700	65,6	0,40	0,00	0,7	65,3	
750	64,4	0,32	0,00	0,6	64,2	
800	63,4	0,24	0,00	0,5	63,2	
850	62,5	0,18	0,00	0,5	62,3	
900	61,7	0,12	0,00	0,4	61,6	
950	61,1	0,08	0,00	0,4	61,0	
1000	60,6	0,04	0,00	0,3	60,6	
1050	60,3	0,02	0,00	0,3	60,3	
1100	60,1	0,00	0,00	0,3	60,1	
1150	60,0	0,00	0,00	0,3	60,0	C-C'

TABLE 2 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
1200	60,1	0,00	0,00	0,3	60,1	
1250	60,3	0,02	0,00	0,3	60,3	
1300	60,6	0,04	0,00	0,3	60,6	
1350	61,1	0,08	0,00	0,4	61,0	
1400	61,7	0,12	0,00	0,4	61,6	
1450	62,5	0,18	0,00	0,5	62,3	
1500	63,4	0,24	0,00	0,5	63,2	
1550	64,4	0,32	0,00	0,6	64,2	
1600	65,6	0,40	0,00	0,7	65,3	
1650	66,9	0,50	0,11	0,8	66,5	
1700	68,4	0,60	0,24	0,9	67,9	
1750	70,0	0,72	0,39	1,0	69,5	
1800	71,7	0,84	0,56	1,1	71,2	
1850	73,6	0,98	0,73	1,3	73,1	E-E'
1887	74,0	1,01	0,77	1,3	73,5	G-G'
1900	71,0	3,00	3,00	3,3	70,5	End

TABLE 3

Parameters for the calculation of "AN ALPINE PAIRSKI". All measurements are in millimeters

Total width at A-A	Total width at C-C	Length C-A	Length C-E	% uplift of the side edge relative to the increase of the total width	Calculated radius for a circle with arc through C and A and with center on the X-axis
120	60	1100	850	8,4	20182

Equation 1 Uplift (mm) =
Equation 2 Uplift (mm) =
Equation 3 $Y^2/A^2 + X^2/B^2 = 1$
where A = 1900 and B = 162,5

8,4 % x Increase of Width
8,4 % x Increase of Width + 0,3mm
(Ellipse)

All three equations are valid between A-A' and E-E' only.

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
170	121,5	5,30	5,30	5,6	121,5	F-F'
200	120,0	5,04	5,04	5,3	120,0	A-A'
250	114,7	4,59	4,50	4,9	114,1	
300	109,6	4,16	3,99	4,5	108,7	

TABLE 3 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
350	104,7	3,76	3,50	4,1	103,5	
400	100,2	3,37	3,04	3,7	98,8	
450	95,8	3,01	2,60	3,3	94,3	
500	91,7	2,66	2,19	3,0	90,2	
550	87,9	2,34	1,80	2,6	86,4	
600	84,3	2,04	1,44	2,3	82,9	
650	80,9	1,76	1,10	2,1	79,6	
700	77,8	1,50	0,79	1,8	76,6	
750	75,0	1,26	0,50	1,6	73,9	
800	72,4	1,04	0,24	1,3	71,5	
850	70,0	0,84	0,00	1,1	69,2	
900	67,9	0,67	0,00	1,0	67,3	
950	66,1	0,51	0,00	0,8	65,6	
1000	64,5	0,37	0,00	0,7	64,1	
1050	63,1	0,26	0,00	0,6	62,8	
1100	62,0	0,17	0,00	0,5	61,8	
1150	61,1	0,09	0,00	0,4	61,0	
1200	60,5	0,04	0,00	0,3	60,5	
1250	60,1	0,01	0,00	0,3	60,1	

TABLE 3 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
1300	60,0	0,00	0,00	0,3	60,0	C-C'
1350	60,1	0,01	0,00	0,3	60,1	
1400	60,5	0,04	0,00	0,3	60,5	
1450	61,1	0,09	0,00	0,4	61,0	
1500	62,0	0,17	0,00	0,5	61,8	
1550	63,1	0,26	0,00	0,6	62,8	
1600	64,5	0,37	0,00	0,7	64,1	
1650	66,1	0,51	0,00	0,8	65,6	
1700	67,9	0,67	0,00	1,0	67,3	
1750	70,0	0,84	0,00	1,1	69,2	
1800	72,4	1,04	0,24	1,3	71,5	
1850	75,0	1,26	0,50	1,6	73,9	
1900	77,8	1,50	0,79	1,8	76,6	
1950	80,9	1,76	1,10	2,1	79,6	
2000	84,3	2,04	1,44	2,3	82,9	
2050	87,9	2,34	1,80	2,6	86,4	
2100	91,7	2,66	2,19	3,0	90,2	
2150	95,8	3,01	2,60	3,3	94,3	
2170	96,8	3,09	2,70	3,4	95,3	
2200	88,0	5,00	5,00	5,0	86,5	
						E-E'
						G-G'
						End

TABLE 4

Parameters for the calculation of "AN ALPINE PAIRSKI". All measurements are in millimeters

Total width at A-A	Total width at C-C	Length C-A	Length C-E	% uplift of the side edge relative to the increase of the total width	Calculated radius for a circle with arc through C and A and with center on the X-axis
85	65	1050	800	5,0	55130

All three equations
are valid between
A-A' and E-E'
only.

Equation 1 Uplift (mm) = $5,0 \% \times \text{Increase of Width}$
Equation 2 Uplift (mm) = $5,0 \% \times \text{Increase of Width} + 0,3\text{mm}$
Equation 3 $Y^2/A^2 + X^2/B^2 = 1$ (Ellipse)
where $A = 2100$ and $B = 74,5$

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Trans- versal lines
180	85,5	1,10	1,10	1,4	85,5	F-F'
200	85,0	1,00	1,00	1,3	85,0	A-A'
250	83,1	0,91	0,88	1,2	83,0	
300	81,4	0,82	0,76	1,1	81,1	

TABLE 4 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
350	79,7	0,73	0,66	1,0	79,4	
400	78,1	0,66	0,55	1,0	77,8	
450	76,6	0,58	0,45	0,9	76,2	
500	75,2	0,51	0,36	0,8	74,8	
550	73,9	0,44	0,28	0,7	73,5	
600	72,7	0,38	0,20	0,7	72,3	
650	71,5	0,33	0,12	0,6	71,2	
700	70,5	0,27	0,06	0,6	70,2	
750	69,5	0,23	0,00	0,5	69,3	
800	68,7	0,18	0,00	0,5	68,5	
850	67,9	0,15	0,00	0,4	67,7	
900	67,2	0,11	0,00	0,4	67,1	
950	66,6	0,08	0,00	0,4	66,5	
1000	66,1	0,06	0,00	0,4	66,1	
1050	65,7	0,04	0,00	0,3	65,7	
1100	65,4	0,02	0,00	0,3	65,4	
1150	65,2	0,01	0,00	0,3	65,2	
1200	65,0	0,00	0,00	0,3	65,0	

TABLE 4 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Trans- versal lines
1250	65,0	0,00	0,00	0,3	65,0	C-C'
1300	65,0	0,00	0,00	0,3	65,0	
1350	65,2	0,01	0,00	0,3	65,2	
1400	65,4	0,02	0,00	0,3	65,4	
1450	65,7	0,04	0,00	0,3	65,7	
1500	66,1	0,06	0,00	0,4	66,1	
1550	66,6	0,08	0,00	0,4	66,5	
1600	67,2	0,11	0,00	0,4	67,1	
1650	67,9	0,15	0,00	0,4	67,7	
1700	68,7	0,18	0,00	0,5	68,5	
1750	69,5	0,23	0,00	0,5	69,3	
1800	70,5	0,27	0,06	0,6	70,2	
1850	71,5	0,33	0,12	0,6	71,2	
1900	72,7	0,38	0,20	0,7	72,3	
1950	73,9	0,44	0,28	0,7	73,5	
2000	75,2	0,51	0,36	0,8	74,8	
2050	76,6	0,58	0,45	0,9	76,2	E-E'
2060	76,8	0,59	0,47	0,9	76,4	G-G'
2090	74,0	3,00	3,00	3,0	74,0	End

TABLE 5

Parameters for the calculation of "AN ALPINE PAIRSKI". All measurements are in millimeters

Total width at A-A	Total width at C-C	Length C-A	Length C-E	% uplift of the side edge relative to the increase of the total width	Calculated radius for a circle with arc through C and A and with center on the X-axis
110	62	950	800	5,0	18814

All three equations
are valid between
A-A' and E-E'
only.

Equation 1 Uplift (mm) =
Equation 2 Uplift (mm) =
Equation 3 $Y^2/A^2 + X^2/B^2 = 1$ (Ellipse)

where A = 1600

and B = 122,8

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Trans- versal lines
160	112,0	2,60	2,55	2,9	112,0	F-F'
200	110,0	2,40	2,34	2,7	110,0	A-A'
250	105,1	2,15	2,02	2,5	104,5	
300	100,4	1,92	1,72	2,2	99,5	

TABLE 5 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
350	96,0	1,70	1,43	2,0	94,9	
400	91,9	1,50	1,16	1,8	90,7	
450	88,1	1,30	0,91	1,6	86,8	
500	84,5	1,12	0,68	1,4	83,2	
550	81,1	0,96	0,46	1,3	79,9	
600	78,1	0,80	0,27	1,1	77,0	
650	75,3	0,66	0,08	1,0	74,3	
700	72,8	0,54	0,00	0,8	71,9	
750	70,5	0,43	0,00	0,7	69,8	
800	68,5	0,33	0,00	0,6	67,9	
850	66,8	0,24	0,00	0,5	66,4	
900	65,3	0,17	0,00	0,5	65,0	
950	64,1	0,11	0,00	0,4	63,9	
1000	63,2	0,06	0,00	0,4	63,1	
1050	62,5	0,03	0,00	0,3	62,5	
1100	62,1	0,01	0,00	0,3	62,1	

TABLE 5 (cont.)

Distance from the tip	Total width calculated from lower lateral edges following a circular path	Uplift of the lower lateral edges according to Equation 1	Uplift of the lower lateral edges nonlinear to the increase in width	Uplift of the lower lateral edges according to Equation 2	Total width calculated from lower lateral edges following an elliptic path	Transversal lines
1150	62,0	0,00	0,00	0,3	62,0	C-C'
1200	62,1	0,01	0,00	0,3	62,1	
1250	62,5	0,03	0,00	0,3	62,5	
1300	63,2	0,06	0,00	0,4	63,1	
1350	64,1	0,11	0,00	0,4	63,9	
1400	65,3	0,17	0,00	0,5	65,0	
1450	66,8	0,24	0,00	0,5	66,4	
1500	68,5	0,33	0,00	0,6	67,9	
1550	70,5	0,43	0,00	0,7	69,8	
1600	72,8	0,54	0,00	0,8	71,9	
1650	75,3	0,66	0,08	1,0	74,3	
1700	78,1	0,80	0,27	1,1	77,0	
1750	81,1	0,96	0,46	1,3	79,9	
1800	84,5	1,12	0,68	1,4	83,2	
1850	88,1	1,30	0,91	1,6	86,8	
1900	91,9	1,50	1,16	1,8	90,7	
1950	96,0	1,70	1,43	2,0	94,9	E-E'
1970	97,0	1,75	1,50	2,1	96,0	G-G'
2010	90,0	4,00	3,80	4,3	89,0	End

TABLE 6

Parameters for the calculation of "AN ALPINE PAIRSKI", asymmetric version. All measurements are in millimeters

Left side of the Left ski = Right side of the Right ski
 Right side of the Left ski = Left side of the Right ski
 Starting from the central longitudinal axis Y

Halfwidth: $A(LL)-S = A'(RR)-S =$	50	Corresponding radius	23760
Halfwidth: $A(RL)-S = A'(LR)-S =$	52	Corresponding radius	21499
Halfwidth $C-S$ (both sides are chosen equal) =	31		

Length $A-C =$	Length $A'-C' =$	950
Length $C-E =$	Length $C'-E' =$	800
	$N =$	12

Uplift (one side) = $N\% \times$ Width increase at the same side.

Distance from the tip	Halfwidth for the Left side of the Left ski and the Right side of the Right ski	Uplift in the lower lateral edge of the Left side of the Left ski and the Right side of the Right ski	Halfwidth for the Right side of the Left ski and the Left side of the Right ski	Uplift in the lower lateral edge of the Right side of the Right ski and the Left side of the Left ski	Total width	Transversal lines
170	50,7	2,5	52,8	2,7	103,5	F-F'
200	50,0	2,3	52,0	2,5	102,0	A-A'
250	48,1	2,0	49,8	2,3	97,9	

TABLE 6 (cont.)

Distance from the tip	Halfwidth for the Left side of the Left ski and the Right side of the Right ski	Uplift in the lower lateral edge of the Left side of the Right ski of the Right ski	Halfwidth for the Right side of the Left ski and the Left side of the Right ski of the Right ski	Uplift in the lower lateral edge of the Right side of the Left ski and the Left side of the Right ski of the Right ski	Total width	Transversal lines
300	46,2	1,8	47,8	2,0	94,0	
350	44,5	1,6	45,9	1,8	90,4	
400	42,8	1,4	44,1	1,6	86,9	
450	41,3	1,2	42,4	1,4	83,7	
500	39,9	1,1	40,8	1,2	80,7	
550	38,6	0,9	39,4	1,0	78,0	
600	37,4	0,8	38,0	0,8	75,4	
650	36,3	0,6	36,8	0,7	73,1	
700	35,3	0,5	35,7	0,6	71,0	
750	34,4	0,4	34,7	0,4	69,1	
800	33,6	0,3	33,8	0,3	67,4	
850	32,9	0,2	33,1	0,3	66,0	
900	32,3	0,2	32,5	0,2	64,8	
950	31,8	0,1	31,9	0,1	63,8	
1000	31,5	0,1	31,5	0,1	63,0	
1050	31,2	0,0	31,2	0,0	62,4	
1100	31,1	0,0	31,1	0,0	62,1	
1150	31,0	0,0	31,0	0,0	62,0	C-C'

TABLE 6 (cont.)

Distance from the tip	Halfwidth for the Left side of the Left ski and the Right side of the Right ski	Uplift in the lower lateral edge of the Left side of the Left ski and the Right side of the Right ski	Halfwidth for the Right side of the Left ski and the Left side of the Right ski	Uplift in the lower lateral edge of the Right side of the Left ski and the Left side of the Right ski	Total width	Transversal lines
1200	31,1	0,0	31,1	0,0	62,1	
1250	31,2	0,0	31,2	0,0	62,4	
1300	31,5	0,1	31,5	0,1	63,0	
1350	31,8	0,1	31,9	0,1	63,8	
1400	32,3	0,2	32,5	0,2	64,8	
1450	32,9	0,2	33,1	0,3	66,0	
1500	33,6	0,3	33,8	0,3	67,4	
1550	34,4	0,4	34,7	0,4	69,1	
1600	35,3	0,5	35,7	0,6	71,0	
1650	36,3	0,6	36,8	0,7	73,1	
1700	37,4	0,8	38,0	0,8	75,4	
1750	38,6	0,9	39,4	1,0	78,0	
1800	39,9	1,1	40,8	1,2	80,7	
1850	41,3	1,2	42,4	1,4	83,7	
1900	42,8	1,4	44,1	1,6	86,9	
1950	44,5	1,6	45,9	1,8	90,4	E-E'
1980	45,0	1,7	46,5	1,9	91,5	G-G'
2020	42,0	4,0	43,5	4,0	85,5	End

CLAIMS:

1. An Alpine ski with a front section including an upturned tip, a rear section including an end portion, and a main section with a sole which comprises, with reference to a plane of the sole with a camber of the ski reduced to zero, a flat first sliding surface which extends on both sides of a central longitudinal axis Y of the ski at least to the front and rear sections respectively, and where lateral surfaces of the ski are provided with an approximately continuous concave sidecut between a first transition line A-A' defining a transition from the main section to the front section and a second transition line E-E' defining a transition from the main section to the rear section of the ski, and wherein lower lateral edges between the transition lines A-A' and E-E' approximate continuous curves with a radius of curvature in any arbitrary point between the first and second transition lines of at most 80 m,

wherein the sole on both sides of the first sliding surface comprises additional sliding surfaces which extend upwards from an edge of the first sliding surface to the lower lateral edges of the ski with an uplift H_s whose value at a point on one of the lower lateral edges of the ski is given by a length of a perpendicular from this point to said plane of the sole, the additional sliding surfaces extending in a longitudinal direction of the ski at least from the first and second transition lines A-A' and E-E', respectively, towards a transversal line C-C', substantially perpendicular to the central longitudinal axis Y behind the middle of the ski and in a section of the ski where a binding is attached, a width of the ski at the line C-C' being equal to a smallest width of the ski between lines A-A' and E-E', the additional sliding surfaces extending on each side over a length which is at least 20% of a length of the main section between the lines A-A' and E-E', such that the length of the additional sliding surfaces in the main section from line A-A' toward line C-C' is at least 20 cm, and that the uplift H_s in the lower lateral edges on the additional sliding surfaces substantially increases with an increasing width of the ski in a direction of the lines A-A' and E-E'

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respectively, whereby the uplift H_s at A-A' is at least 1/2000 of a length of the first sliding surface between the lines A-A' and E-E'.

2. An Alpine ski according to claim 1,

wherein the additional sliding surfaces are extended beyond the first transition line A-A' into the front section and terminate at a transversal line F-F' substantially perpendicular to the central longitudinal axis Y, the line F-F' defining a transition from the first and additional sliding surfaces in the front section to the upturned tip, the lower lateral edges each having a turning point at the line A-A', providing a continuous transition from a concave sidecut in the main section to a convex sidecut in the front section,

and wherein the uplift of the lower lateral edges of the ski in the front section between the transition lines A-A' and F-F' at any point is at least as large as the uplift at the transition line A-A'.

3. An Alpine ski according to claim 1,

wherein the additional sliding surfaces are extended beyond the second transition line E-E' into the rear section and terminate at a transversal line G-G' substantially perpendicular to the central longitudinal axis Y, the line G-G' defining a transition from the first and additional sliding surfaces in the rear section to the end portion, the lower lateral edges each having a turning point at the line E-E', providing a continuous transition from a concave sidecut in the main section to a convex sidecut in the rear section,

and wherein the uplift of the lower lateral edges of the ski in the rear section between the lines E-E' and G-G' at any point is at least as large as the uplift at the transition line E-E'.

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4. An Alpine ski according to claim 1,
wherein the ski is symmetrical about the central longitudinal axis Y, the lines of transition A-A', E-E', F-F', G-G' as well as the transversal line C-C' all being perpendicular to the axis Y.
5. An Alpine ski according to claim 4,
wherein the sidecut of the lower lateral edges between the transition lines A-A', E-E' is approximately equivalent to a curvature of congruent arcs in circles where a section of the circumference defines the lower lateral edges between the transition lines A-A', E-E', and the transversal line C-C' constitutes an extension of a radius in each of the circles, the radii of the circles within arbitrarily selected sections 20 cm in length between lines A-A' and E-E' not deviating by more than $\pm 20\%$ from a radius of an imaginary circle which passes through the starting and end points together with the middle of the arbitrarily selected section between A-A' and E-E'.
6. An Alpine ski according to claim 4,
wherein the sidecut of the lower lateral edges between the transition lines A-A', E-E' is approximately equivalent to a curvature of congruent arcs of ellipses where a section of the circumference defines the lower lateral edges between the transition lines A-A', E-E', and the transversal line C-C' constitutes an extension of the ellipses' minor axis, the radii of curvature of the ellipses within arbitrarily selected sections 20 cm in length between lines A-A' and E-E' not deviating by more than $\pm 20\%$ from a radius of an imaginary circle which passes through the starting and end points together with the middle of the arbitrarily selected section between A-A' and E-E'.
7. An Alpine ski according to claim 1,
wherein the uplift H_s at the transition line A-A' constitutes at least $1/1000$ of a length of the first sliding surface.

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8. An Alpine ski according to claim 1,

wherein the lower lateral edges at an arbitrary point between the transition lines A-A' and E-E' have a radius of curvature of maximum 40 meters.

9. An Alpine ski according to claim 1,

wherein the uplift H_s as defined at an arbitrary point on the lower lateral edges is given as an approximately linear function of the increase in the width of the ski between the transversal line C-C' and the perpendicular on the central longitudinal axis at this point, the uplift H_s being obtained from the following formula:

$$H_s = K_1 + K_2 \cdot \Delta X + M(y)$$

where H_s is the uplift in millimetres, K_1 and K_2 are suitable selected constants, ΔX is the increase in width and $M(y)$ is a function of the distance (the length of the ski) between line C-C' and said perpendicular, so that the functional value $|M(y)| < 1$ mm.

10. An Alpine ski according to claim 1,

wherein a width of the first sliding surface at the transverse line C-C' is equal to the width of the ski at C-C' and wherein the uplift of the lower lateral edges at C-C' is zero.

11. An Alpine ski according to claim 1,

wherein the first sliding surface extends to the lower lateral edges of the ski in a section of the sole on both sides of the transversal line C-C' and between a second transversal line B-B' in a section of the sole from line C-C' to line A-A' and a third transversal line D-D' in a section from line C-C' to line E-E', the uplift H_s of the lateral edges between lines B-B', D-D' being zero.

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12. An Alpine ski according to claim 1, where the first sliding surface extends substantially symmetrically about the ski's central longitudinal axis and wherein a width of the first sliding surface is less than the width of the ski, the additional sliding surfaces on both sides of the first sliding surface extending along the entire sole between the transition lines A-A', E-E', the uplift H_s of the lower lateral edges at the transversal line C-C' being at most 2 mm.

13. An Alpine ski according to claim 1,

wherein the additional sliding surfaces and the first sliding surface are extended beyond the first transition line A-A' into the front section and terminate at a transversal line F-F' substantially perpendicular to the central longitudinal axis Y, the line F-F' defining a transition from the first and additional sliding surfaces in the front section to the upturned tip, the lower lateral edges each having a turning point at the line A-A', providing a continuous transition from a concave sidecut in the main section to a convex sidecut in the front section,

and wherein the uplift of the lower lateral edges of the ski in the front section between the transition lines A-A' and F-F' at any point is at least as large as the uplift at the transition line A-A'.

14. An Alpine ski according to claim 1,

wherein the additional sliding surfaces and the first sliding surface are extended beyond the second transition line E-E' into the rear section and terminate at a transversal line G-G' substantially perpendicular to the central longitudinal axis Y, the line G-G' defining a transition from the first and additional sliding surfaces in the rear section to the end portion, the lower lateral edges each having a turning point at the line E-E', providing a continuous transition from a concave sidecut in the main section to a convex sidecut in the rear section,

- 38 -

and wherein the uplift of the lower lateral edges of the ski in the rear section between the lines E-E' and G-G' at any point is at least as large as the uplift at the transition line E-E'.

fig. 1

1

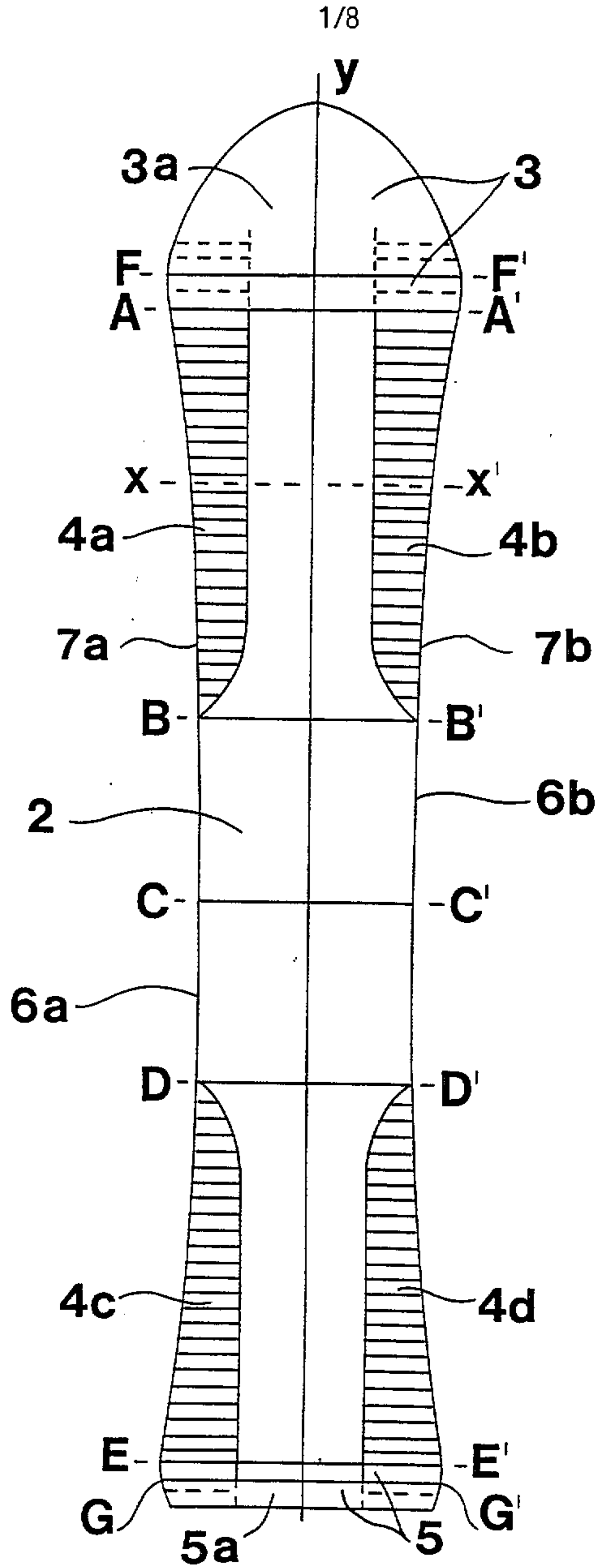


fig. 2a

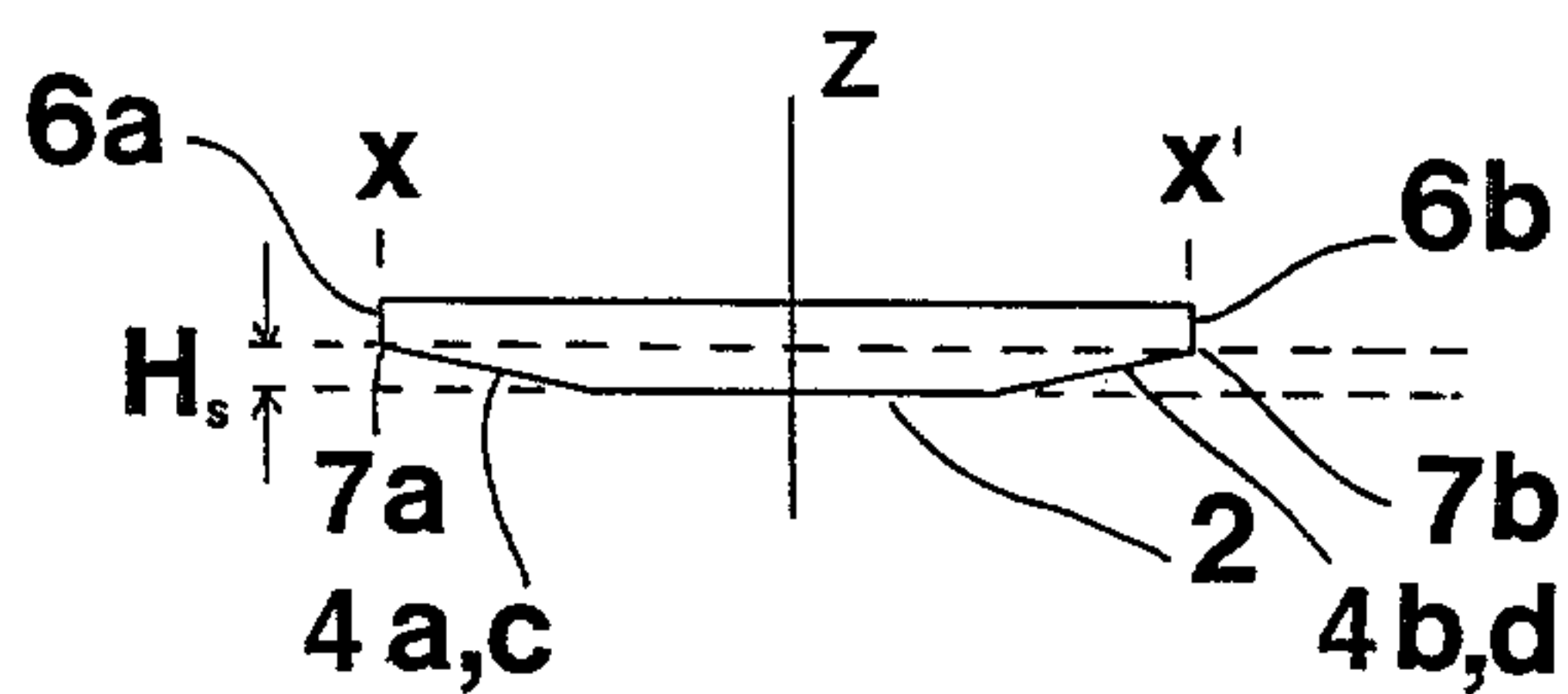


fig. 2b

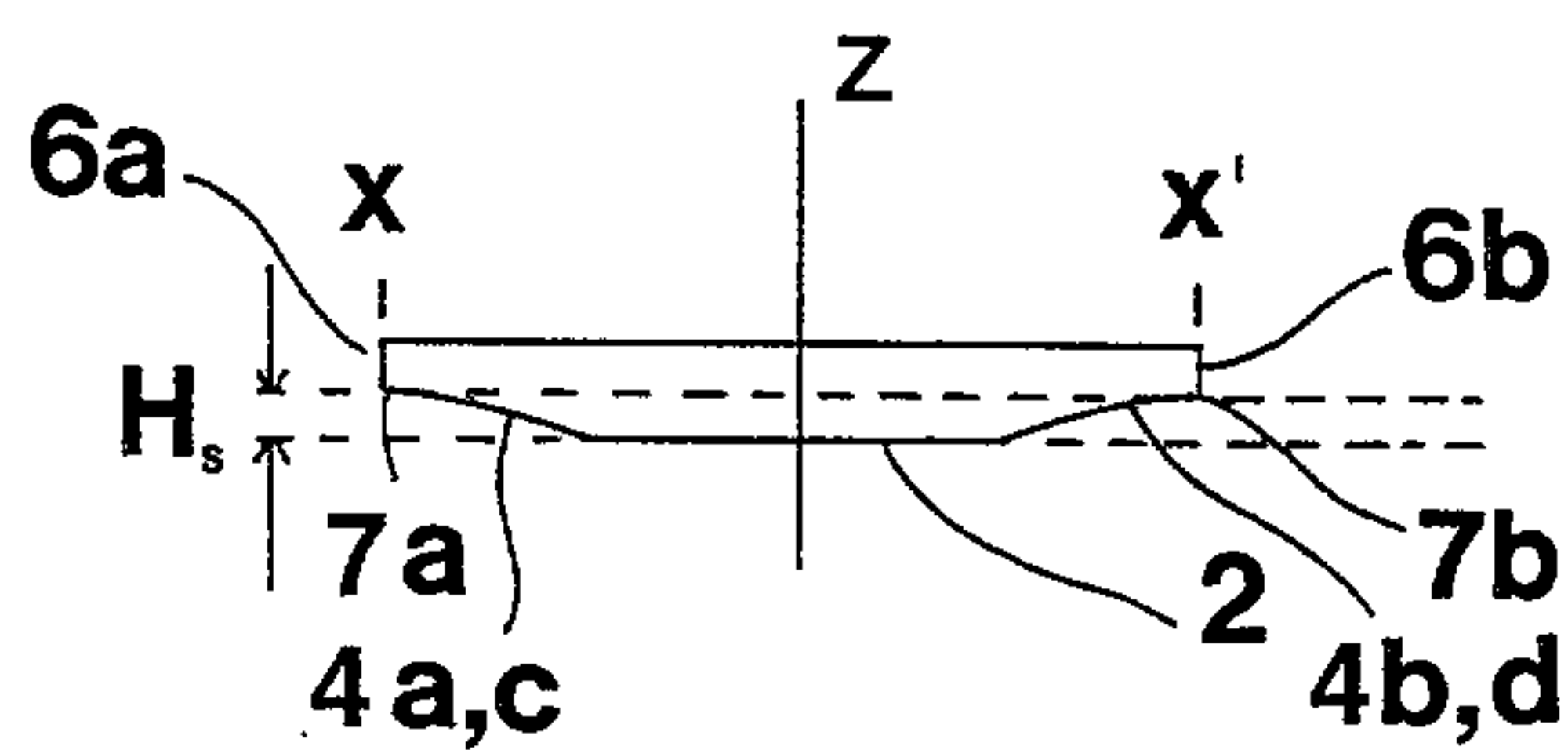


fig. 2c

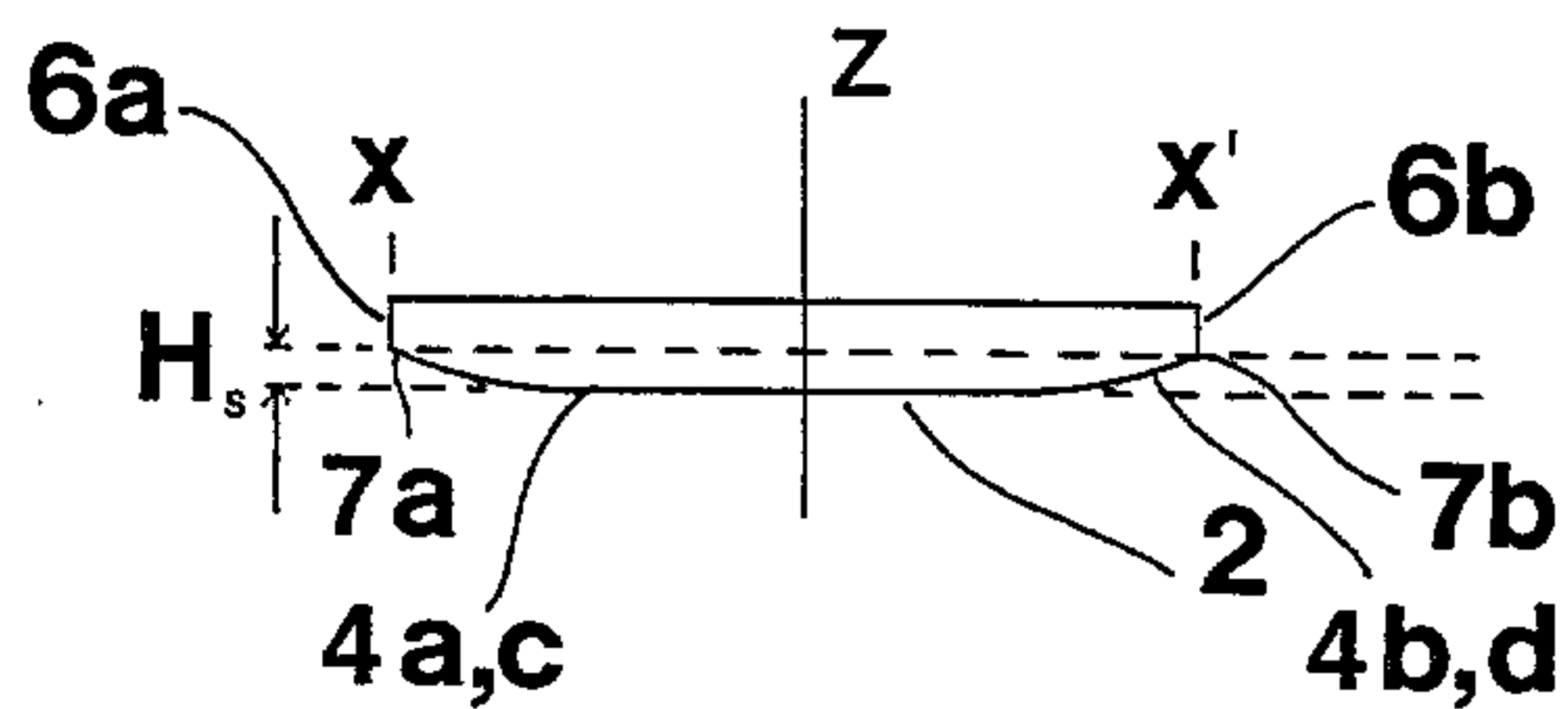


fig.3

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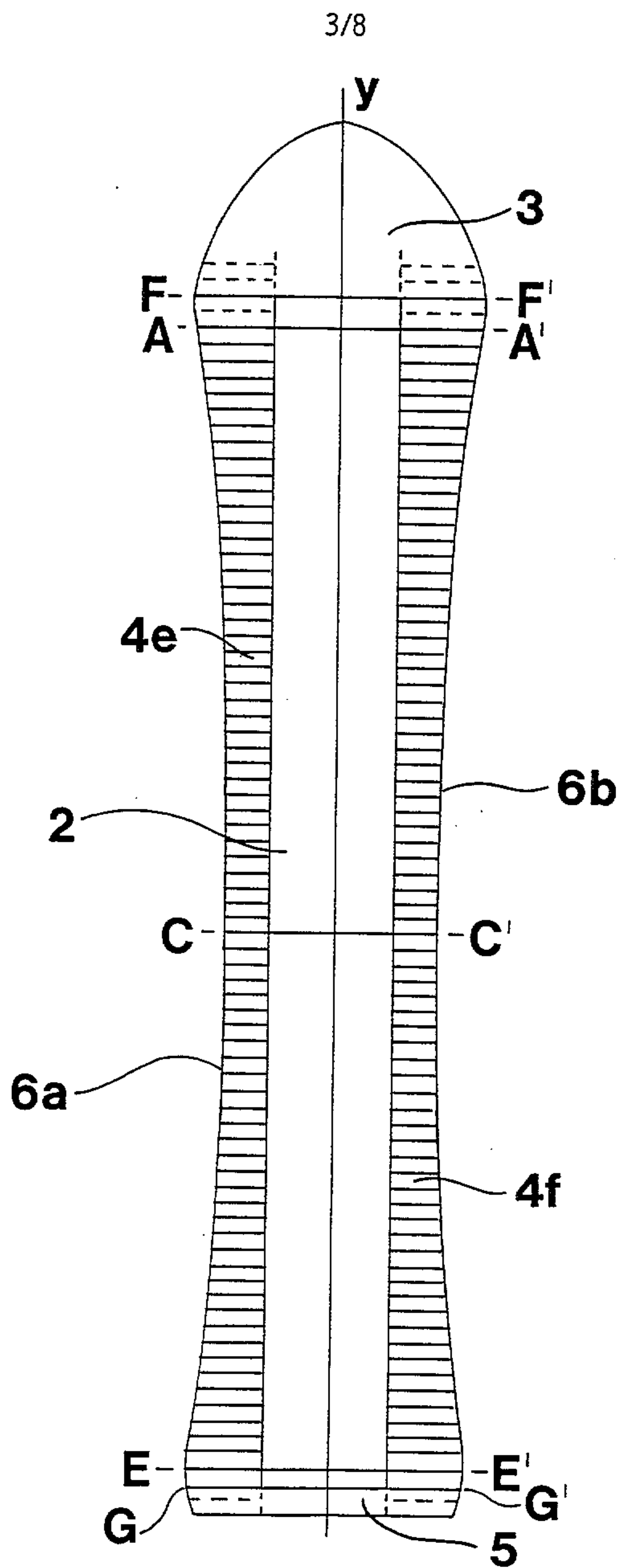
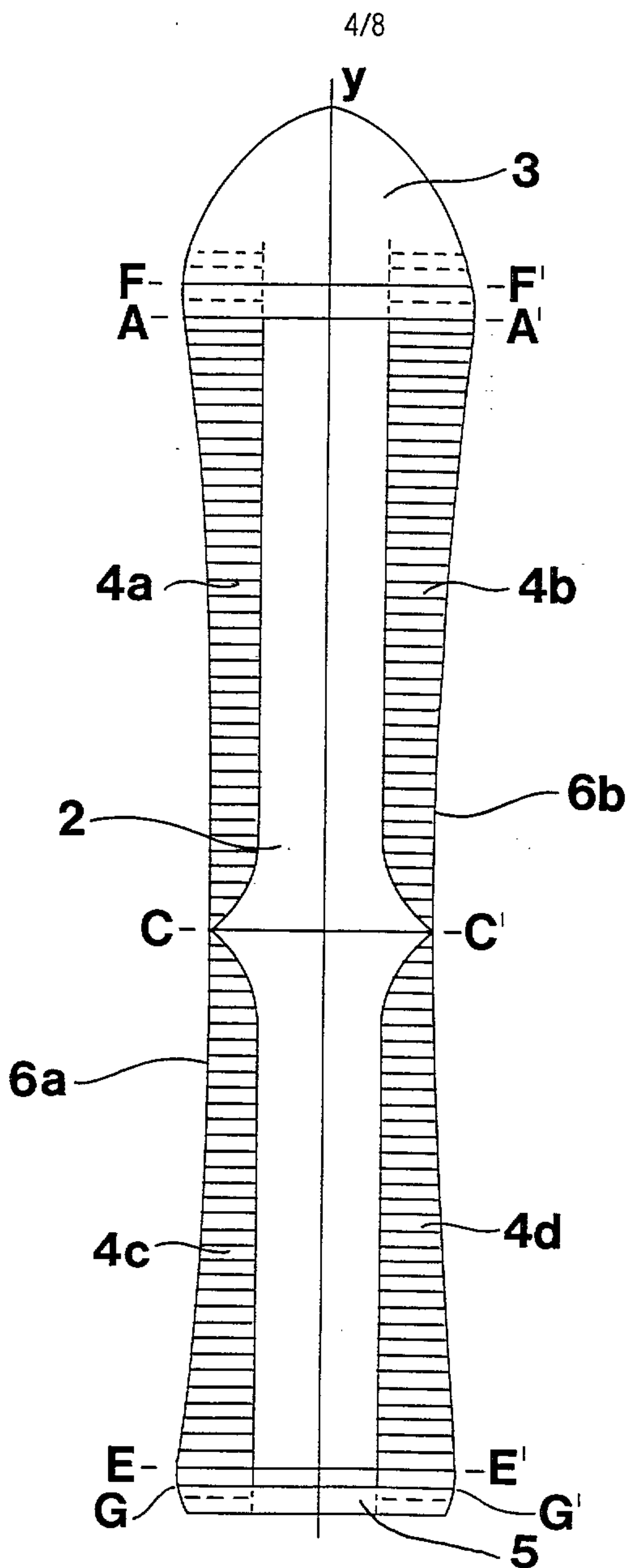


fig.4

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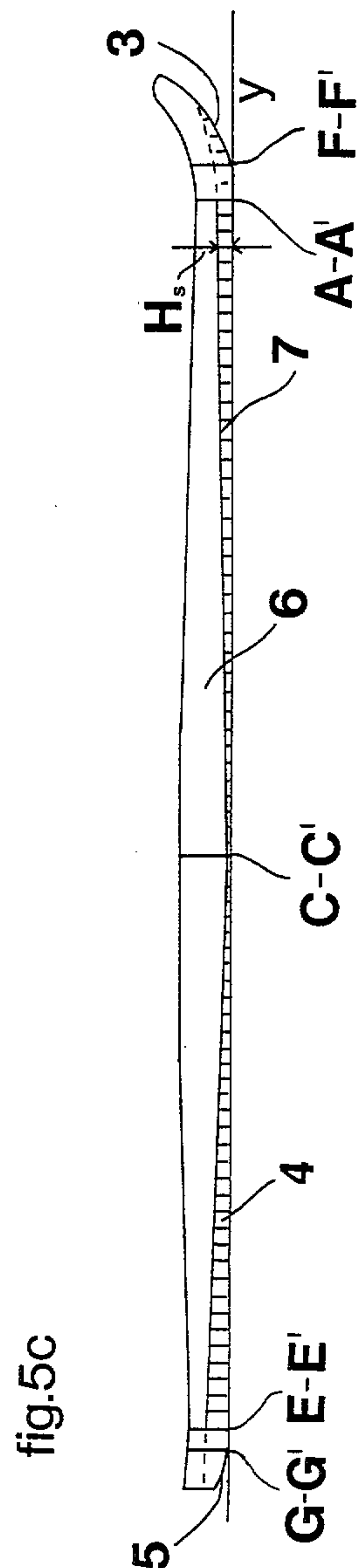
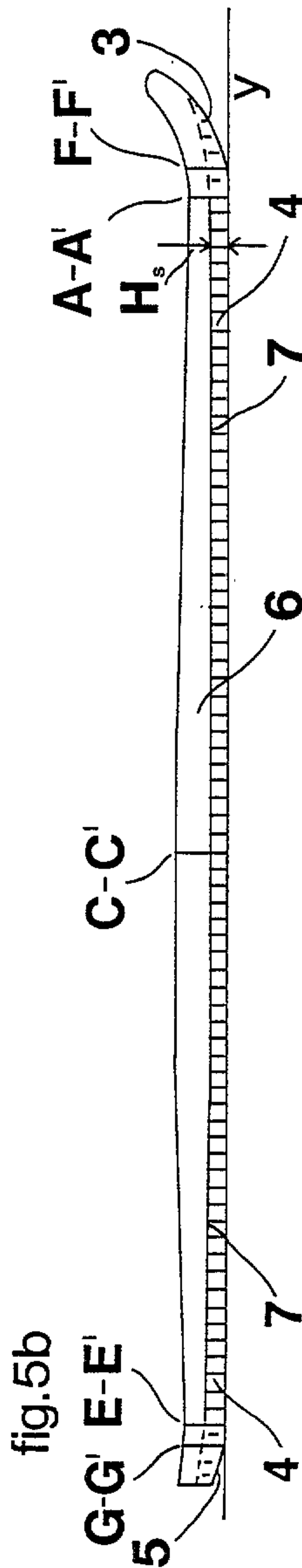
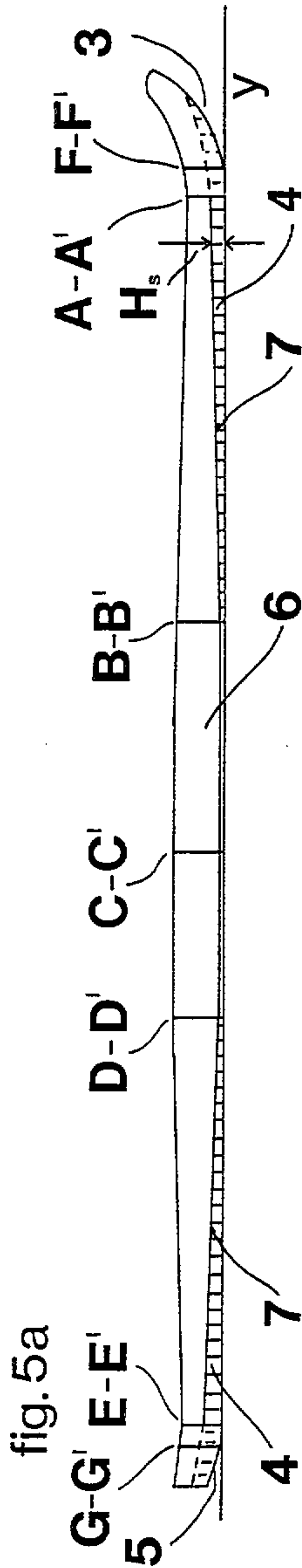


fig.6

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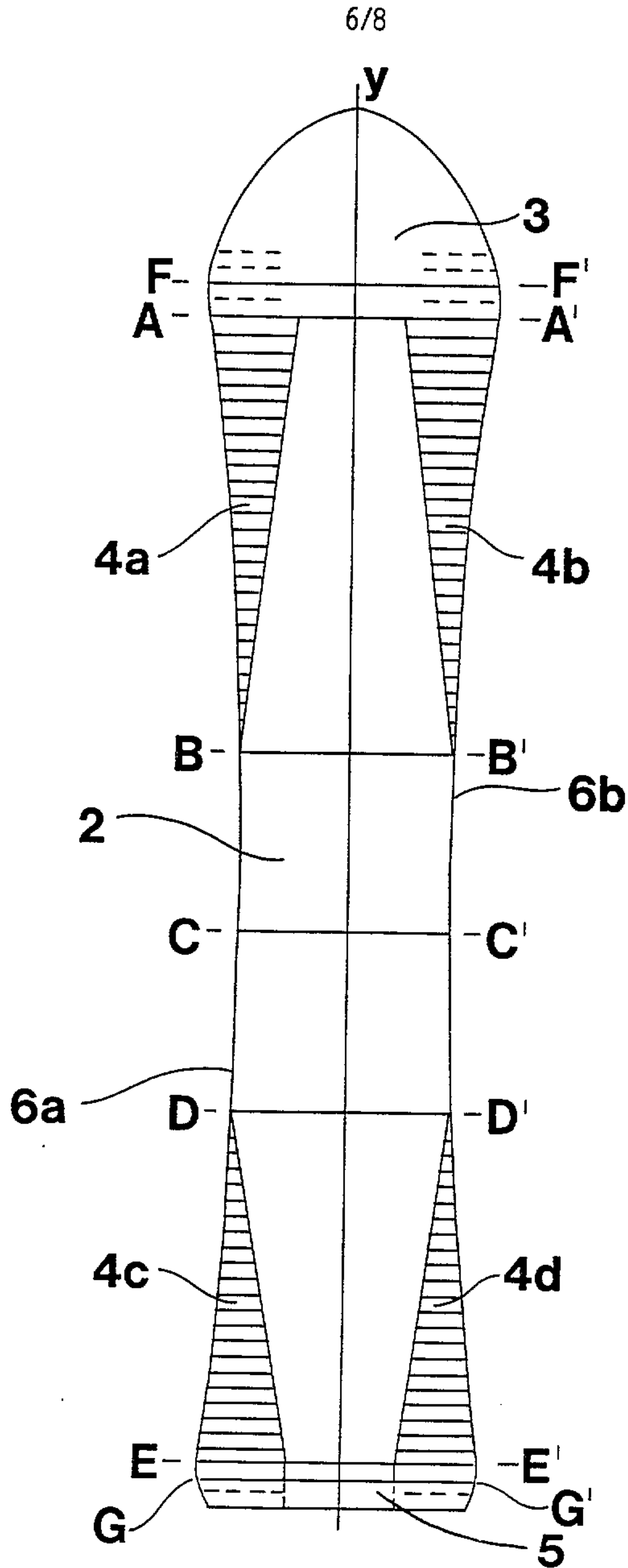


fig.7

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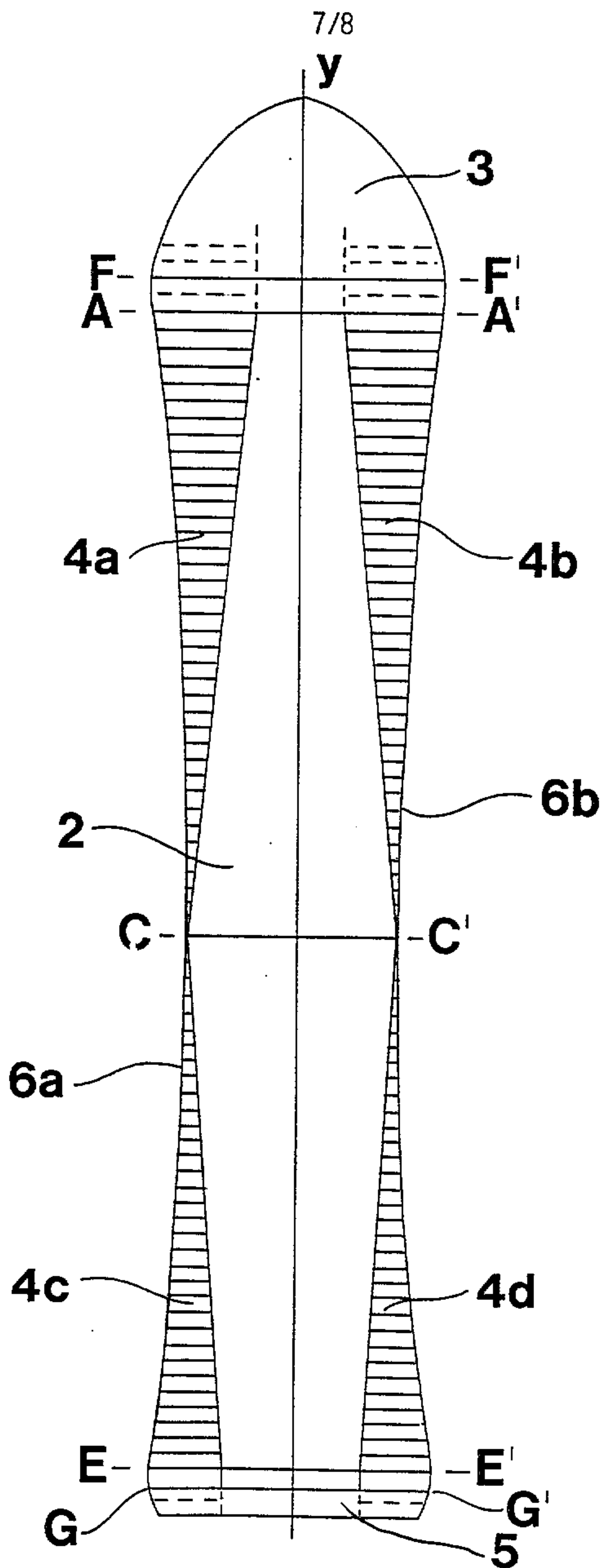
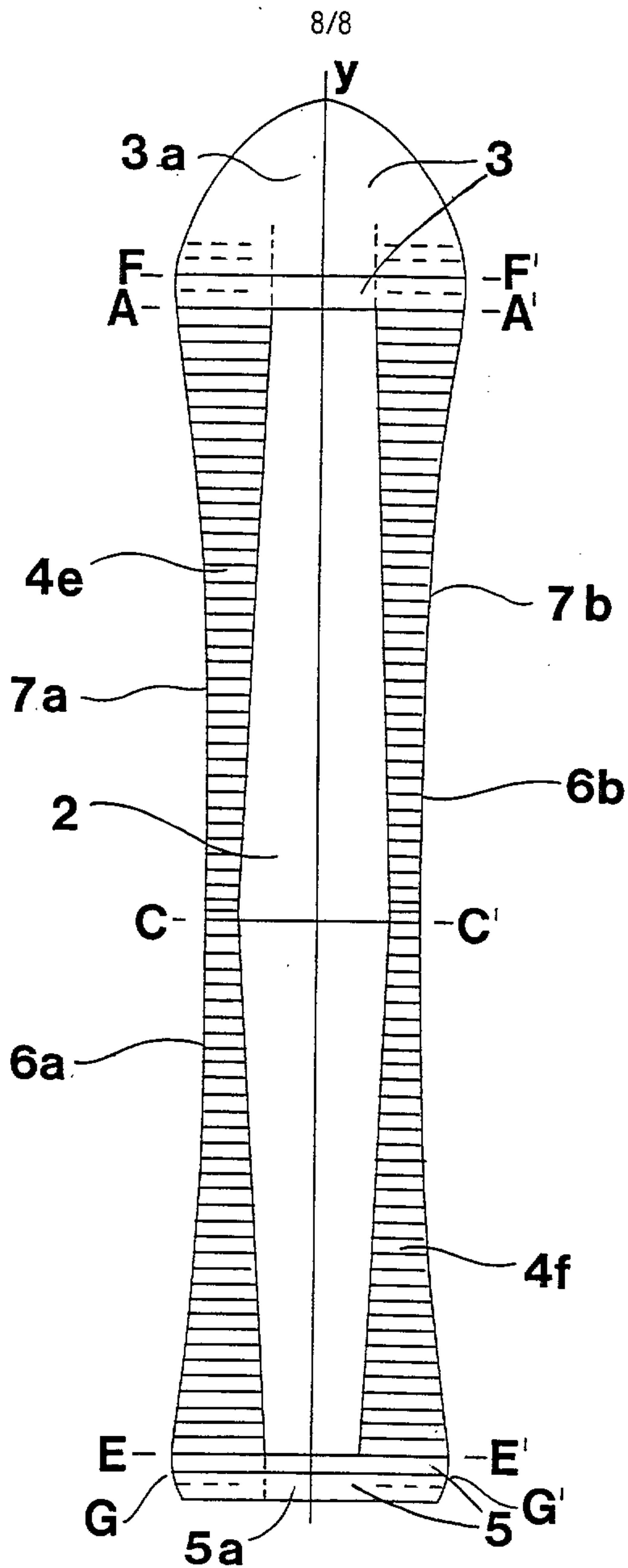


fig.8

1



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