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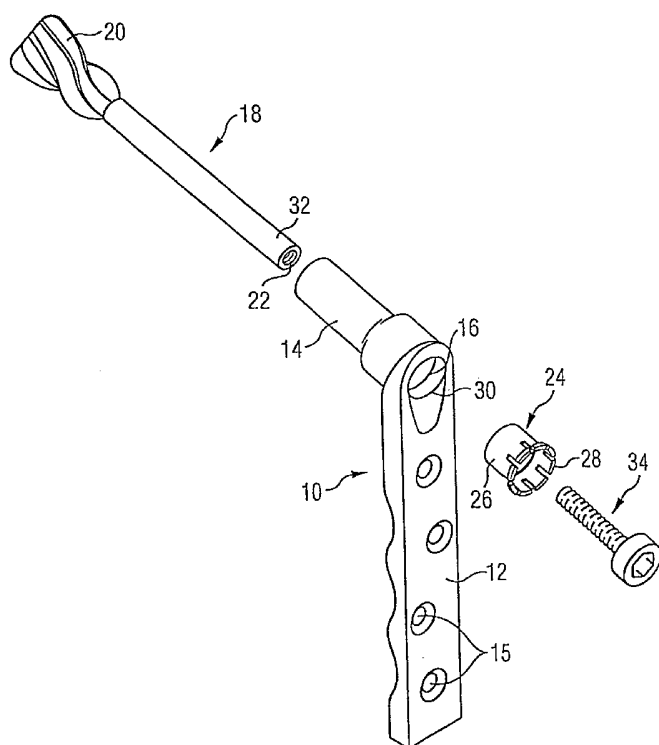
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(54) Title: DEVICE FOR ROTATIONAL STABILIZATION OF BONE SEGMENTS



(57) Abstract: A device for rotational stabilization of bone segments comprising a bone plate (10), a bone lag screw (18), and a locking collar (50). The bone lag screw (18) has a bone-engagement end (20), a distal end, and a keyed cross-sectional profile (32), the bone-engagement end (20) configured for engaging a first bone segment. The bone plate (10) has a flat portion (12) for engaging a second bone segment and a barrel portion (14) having an internal bore for slidably receiving the lag screw (18). The locking collar (50) has a keyed internal profile (21) that mates with the keyed cross-sectional profile (32) of the lag screw (18) to rotationally couple the locking collar (50) and the lag screw (18) when the lag screw (18) is inserted through the locking collar (50), and an outer surface configured and dimensioned for free rotation, in a first position, within the internal bore (16) of the bone plate barrel portion (14) and frictionally engaging, in a second position, the internal bore (16) of the bone plate barrel portion (14) to resist or prevent rotation of the collar (50) relative to the bone plate (10), and thereby resist or prevent rotation of the lag screw (18) relative to the bone plate (10). The frictional engagement is achieved by a deformation of the distal end (56) of the locking collar (50) within the internal bore (16) of the bone plate (10). This deformation is achieved by the application of force to the collar in the proximal direction.



WO 03/028567 A1



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**DEVICE FOR ROTATIONAL
STABILIZATION OF BONE SEGMENTS**

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RELATED APPLICATIONS

This application is a continuation-in-part of currently pending United States Patent Application Serial No. 09/542,821, filed April 4, 2000.

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FIELD OF THE INVENTION

The present invention relates generally to connection devices, and, more particularly, to a bone connection device for rotational stabilization of bone segments.

BACKGROUND OF THE INVENTION

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Devices for the repair of large bone fractures (e.g., fractures of the femoral neck) have generally consisted of some combination of a lag screw with a side plate and some means for attaching these two components to one another and to the fractured bone segments. The ability to rotationally lock a lag screw (also known as a “hip screw”) relative to its side plate is very important in such devices because rotational movement of the lag screw relative to the side plate following implantation can cause premature wear of the bone fragment and result in loosening of the system prior to complete healing.

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Prior art devices have attempted to rotationally lock installed lag screws using keys, pins, rings, splines, etc. *See e.g.*, U.S. Patents 5,007,910 and 5,514,138 to Anapliotis, et al. and McCarthy, respectively. The additional operation time and tools required to align and properly install such equipment has fueled a desire for a simpler and more effective device for aligning and rotationally locking the lag screw relative to the side plate. Such a device would reduce surgical operation time and complexity and provide a more effective and efficient mechanism for rotationally locking a lag screw to its corresponding side plate – an obvious benefit to both orthopaedic physicians and patients.

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SUMMARY OF THE INVENTION

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In a preferred embodiment, the present invention is a device for rotational stabilization of bone segments comprising: a bone lag screw having a bone-engagement end, a distal end, and a keyed cross-sectional profile, the bone-engagement end configured for engaging a first bone segment; a bone plate having a flat portion for engaging a second bone

segment and a barrel portion having an internal bore for slidably receiving the lag screw;
and a locking collar having a keyed internal profile that mates with the keyed cross-sectional
profile of the lag screw to rotationally couple the locking collar and the lag screw when the
lag screw is inserted through the locking collar, and an outer surface configured and
5 dimensioned for (1) free rotation, in a first position, within the internal bore of the bone
plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of
the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone
plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. The
locking collar may be cylindrical, and the outer surface of the locking collar may be formed
10 with a taper. The taper of the outer surface of the locking collar may range from about 0
degrees to about 10 degrees. The taper of the outer surface of the locking collar may be
defined by a major diameter and a minor diameter, a distal end of the collar having the
major diameter, and a proximal end of the collar having the minor diameter.

The internal bore of the bone plate barrel portion may also be formed with a
15 taper and the taper of the outer surface of the locking collar may be of the same degree and
profile as the taper of the internal bore of the bone plate barrel portion. In one specific
example, an impact force on the distal end of the locking collar frictionally locks the tapered
outer surface of the locking collar to the tapered inner surface of the bone plate internal
bore, preventing further rotation of the collar relative to the bone plate, and thereby
20 preventing further rotation of the lag screw relative to the bone plate. This frictional
locking is known as the Morse Taper effect. The components described above (i.e., lag
screw, bone plate, locking collar) may be formed of any bio-compatible material, but are
preferably of stainless steel, titanium alloy, or titanium.

Alternatively, the outer surface of the locking collar may be formed with a
25 reverse taper defined by a major diameter and a minor diameter, a proximal end of the collar
having the major diameter, and a distal end of the collar having the minor diameter. The
locking collar, in the second position, may then be frictionally engaged in a proximal section
of the internal bore of the bone plate by a force in a distal direction (i.e., a force directed
away from, rather than toward, the patient's body), such as that applied with a slide-
30 hammer.

The barrel portion of the bone plate may be angled relative to the flat
portion, and the device may be configured and adapted for repair of fractures of the femoral
neck (i.e., hip bone). It should be pointed out, however, that the device is generally
applicable to any type of bone fracture where rotational stabilization is important. In
35 addition, the locking collar may be formed with a plurality of partial lengthwise slots

extending from a distal end of the collar toward the proximal end of the collar. The lag screw may be formed with a cancellous screw thread, or it may be formed with a plurality of helically twisted blades.

In one variation of this embodiment, the device may further comprise a threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or titanium.

In another embodiment, the invention is a device for rotational stabilization of bone segments comprising: a bone lag screw having a bone-engagement end and a distal end, the bone-engagement end configured for engaging a first bone segment; a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an internal bore for slidably receiving the lag screw, part of the internal bore having a taper; and a cylindrical locking collar having a hollowed cylindrical interior, a keyed internal profile that mates with the keyed cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and a tapered outer surface configured and dimensioned for (1) free rotation, in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. An impact force on the distal end of the locking collar frictionally locks the tapered outer surface of the locking collar to the tapered inner surface of the bone plate internal bore, preventing further rotation of the collar relative to the bone plate, and thereby preventing further rotation of the lag screw relative to the bone plate. This frictional locking is known as the Morse Taper effect. The taper of the outer surface of the locking collar may range from about 0 degrees to about 10 degrees, and may be defined by a major diameter and a minor diameter, a distal end of the collar having the major diameter, and a proximal end of the collar having the minor diameter. The barrel portion of the bone plate may be angled relative to the flat portion, and the device may be configured and adapted for repair of fractures of the femoral neck (i.e., hip bone), but is generally applicable to any type of bone fracture where rotational stabilization is important. The components described above (i.e., lag screw, bone plate, locking collar) may be formed of any biocompatible material, but are preferably formed of

stainless steel, titanium alloy, or titanium. In addition, the locking collar may be formed with a plurality of partial lengthwise slots extending from the distal end of the collar toward the proximal end of the collar. The taper of the outer surface of the locking collar may be of the same degree and profile as the taper of the internal bore of the angled barrel portion.

5 In an alternative arrangement, the outer surface of the locking collar may be formed with a reverse taper defined by a major diameter and a minor diameter, a proximal end of the collar having the major diameter, and a distal end of the collar having the minor diameter. The locking collar, in the second position, may then be frictionally engaged in a proximal section of the internal bore of the bone plate by a force in a distal direction (i.e., a
10 force directed away from, rather than toward, the patient's body), such as that applied with a slap-hammer.

 The device may further comprise a threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts the distal end
15 of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or titanium.

 In still another preferred embodiment, the invention is a device for rotational stabilization of bone segments comprising a bone lag screw having a bone-engagement end, a distal end, and a keyed cross-sectional profile, the bone-engagement end configured for
20 engaging a first bone segment; a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an internal bore for slidably receiving the lag screw; and a locking collar having a proximal end, a distal end, a keyed internal profile and a deformable portion at the distal end; wherein the keyed internal profile mates with the keyed
25 cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and the deformable portion is configured and dimensioned for (1) free rotation, in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of the bone plate barrel portion to resist or prevent rotation of the collar
30 relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. An axial impact force in the proximal direction on the distal end of the locking collar frictionally locks the deformable portion of the locking collar to the inner surface of the bone plate internal bore, preventing further rotation of the collar relative to the bone plate, and thereby preventing further rotation of the lag screw relative to the bone
35 plate. The locking collar may be substantially cylindrical, and the deformable portion of the

locking collar may have a maximum diameter at the distal end of the locking collar and taper toward a proximal end of the locking collar, forming an angle of about 20° with a longitudinal axis (about 70° with a vertical axis) of the locking collar. The maximum diameter may be greater than the internal diameter of the internal bore when the locking collar is in the first position. The internal bore of the bone plate barrel portion may have a circumferential groove at a distal end which engages the distal end of the locking collar such that the collar freely rotates within the internal bore of the barrel in the first position. The deformable portion may also include a plurality of deformable tabs extending part of the distance from the distal end of the locking collar toward the proximal end of the locking collar. These deformable tabs, which may be spaced about the circumference of the distal end of the locking collar, may also have flat portions at the distal end of the locking collar and taper toward the proximal end of the locking collar.

The barrel portion of the bone plate may be angled relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck. As in the previous embodiments, the lag screw may be formed with a cancellous screw thread or a plurality of helically twisted blades, and the lag screw, bone plate, and locking collar may be formed of stainless steel, titanium alloy, or titanium.

The device may further comprise a threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts the distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or titanium.

In still another preferred embodiment, the invention provides an improved method for rotationally stabilizing bone segments utilizing a bone lag screw and a bone plate, the improvement comprising: sufficiently locking the bone screw to the bone plate by frictional engagement to rotationally stabilize the bone segments relative to one another. The method may further comprise: inserting a locking collar into a barrel portion of a bone plate; inserting a lag screw through the locking collar and barrel portion; rotationally coupling the locking collar and the lag screw; attaching the bone-engagement end of the lag screw to a first bone segment; and impacting the locking collar to frictionally engage an outer surface of the locking collar to the internal bore to resist or prevent further rotation of the collar relative to the bone plate, and thereby prevent further rotation of the lag screw relative to the bone plate. In one variation, a deformable distal end of the locking collar

frictionally engages the internal bore to resist or prevent further rotation of the collar relative to the bone plate, and thereby prevent further rotation of the lag screw relative to the bone plate.

5 **BRIEF DESCRIPTION OF THE DRAWINGS**

The present invention will be understood and appreciated more fully from the following detailed description, taken in conjunction with the drawings in which:

FIG. 1 is an isometric view of the disassembled components of the device in a preferred embodiment of the present invention;

10 FIG. 2 is a cross-sectional view of the bone plate and locking collar of one preferred embodiment of the present invention;

FIG. 3A is a cross-sectional view of the locking collar shown in FIG. 2;

FIG. 3B is a plan view of the locking collar shown in FIG. 2;

15 FIG. 4 is a cross-sectional view of the bone plate and locking collar of another preferred embodiment of the present invention;

FIG. 5A is a side view of the locking collar shown in FIG. 4;

FIG. 5B is a plan view of the locking collar shown in FIG. 4;

20 FIG. 5C is a cross-sectional view of the locking collar taken along line 5C-5C shown in FIG. 5B;

FIG. 6 is a cross-sectional view through a pair of bone segments demonstrating the application of one embodiment of the device of the present invention; and

FIG. 7 is a cross-sectional view through a pair of bone segments demonstrating the application of another embodiment of the device of the present invention.

25 **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS**

Reference is now made to FIG. 1, which is an isometric view of the disassembled components of one embodiment of the device of the present invention. The device allows a lag screw (or hip screw) to be aligned and rotationally locked within the bore of a bone repair plate. While the device is described in the context of hip fracture repair, it should be pointed out that the device may also be used in the repair of other bone fractures, such as knee joint fractures.

30 A side plate **10** has a flat portion **12** for attachment to the femur shaft (not shown) and an angled barrel portion **14** having an internal bore **16**. The flat portion **12** has holes **15** (which may be self-compressing screw holes) for connection to the femoral shaft
35 using screws or other coupling means. The internal bore **16** is formed with a taper or cone,

as will be explained below with reference to FIG. 2. A lag screw **18** has a drilling portion **20** at a bone-engagement end and a threaded internal bore **22** at a distal end. The lag screw **18** may be formed with a conventional cancellous screw thread **46** (as shown in FIG. 5), or may be formed with a plurality of helically twisted blades (as shown in FIG. 1), for example
5 such as that disclosed in U.S. Patent No. 5,741,256 to Bresina, incorporated herein by reference. With regard to the descriptions of the elements of the present invention, it should be pointed out that the terms "proximal" and "distal" are defined with relation to the body of the patient (i.e., the person receiving the bone stabilization device). For example, the term "proximal" is used to describe that portion of a given element closer to the center
10 of the patient's body, and the term "distal" refers to that portion of the element further away from the center of the patient's body.

In one embodiment, a locking collar **24** has a hollow cylindrical interior and an outer surface **26** formed with a taper. The taper of the outer surface **26** of locking collar **24**, ranging from about 0 degrees to about 10 degrees, is of the same degree and profile as
15 the taper of the internal bore **16**. The locking collar **24** also has a circumferential lip **28** (see FIG. 3A) at a distal end that mates with a circumferential groove **30** at a distal end of the internal bore **16**. When the locking collar **24** is introduced into the internal bore **16**, the circumferential lip **28** engages the circumferential groove **30**, such that the collar is axially restrained in the bore, but is free to rotate with respect to the bore. It should be noted that
20 the bone stabilization device may be supplied to physicians with the locking collar already engaged in the circumferential groove **30** of the bone plate internal bore **16**. The locking collar also has a keyed internal profile, as will be explained below with reference to FIG. 3B, that mates with a keyed cross-sectional profile **32** on the shaft of the lag screw **18**, to rotationally couple the locking collar **24** to the lag screw **18** when the lag screw is inserted
25 through the internal bore **16** and the locking collar **24**. The locking collar **24** also facilitates the proper alignment of the lag screw **18** and side plate **10**, while simultaneously permitting the screw **18** to rotate freely so that it can engage the bone segment during installation. This integral alignment function of the locking collar **24** eliminates the need for additional components or alignment tools.

30 After the locking collar **24** is placed within bore **16**, and the lag screw **18** is inserted through the collar and has satisfactorily engaged the bone, an impact force is applied to the exposed end of the collar (i.e., the distal end), causing the lip **28** to become disengaged from the groove **30**, and driving the collar proximally inward along the bore **16**, resulting in the tapered outer surface **26** of the locking collar becoming frictionally locked
35 with the tapered surface of the internal bore **16**. This frictional locking, known as the

Morse Taper effect, prevents further movement (both axial and rotational) of the collar **24** relative to the internal bore **16**, and so prevents further rotation of the lag screw **18**. This rotational stabilization of the lag screw relative to the bone plate will prevent premature wear of the bone fragments and loosening of the system prior to complete bone healing.

5 It should be noted that in an alternate embodiment, the bore may have a reverse taper, as compared to that of the embodiment illustrated in FIGS. 2, 3A and 3B. In this embodiment, the bore has its major diameter at the proximal end, its minor diameter at the distal end, and the collar **24** is locked in place at the proximal end of the internal bore **16** by a force in the distal direction, such as that applied by a slide-hammer.

10 At this point, the lag screw is rotationally fixed relative to the side plate **10** and locking collar **24**, but the lag screw may still slide axially relative to the collar and side plate. A compression screw **34** may be inserted into the threaded bore **22** of the lag screw, abutting the distal end of the locking collar **24** and drawing the lag screw axially in the distal direction, to join the separated bone segments (i.e., reducing the fracture) and promote the
15 desired healing. The elements described above may be formed of stainless steel, titanium alloy, titanium, or any other material with suitable strength and bio-compatibility.

 As described below and shown in FIGS. 4, 5A, 5B and 5C, in another preferred embodiment, a locking collar **50** has a deformable portion **52**. Upon application of an impact force to the exposed distal end of collar **50**, collar **50** is driven proximally
20 inward along bore **16** and deformable portion **52** becomes frictionally locked within internal bore **16**.

 Reference is now made to FIG. 2, which is a cross-sectional view of the side plate and locking collar of one preferred embodiment of the present invention. As discussed above, the side plate **10** has a flat portion **12** for connection to the femoral shaft and an
25 angled barrel portion **14** having an internal bore **16** for slidably receiving a lag screw (not shown). The bore **16** has a tapered surface **17** along part of its length. A locking collar **24** sits within the internal bore **16**, a circumferential lip **28** on the collar **24** rotatably engaging a circumferential groove **30** on the bore **16**. The collar **24** has a tapered outer surface **26**, with the same degree and profile as the tapered surface **17** of internal bore **16**. Prior to
30 insertion and alignment of the lag screw (not shown) and application of an impact force to the distal end **19** of the collar, the collar can rotatably slide within the bore **16**. The collar **24** has a keyed internal profile **21**, as shown most clearly in FIG. 3B, for mating and rotationally coupling with a corresponding keyed cross-sectional profile of the lag screw. Thus, upon insertion of the lag screw through the bore **16** and collar **24**, rotation of the lag
35 screw causes rotation of the locking collar **24** relative to the bore **16**. Upon application of

an impact force to distal end **19** of the collar, the tapered outer surface **26** of the collar becomes frictionally locked with tapered surface **17** of bore **16**. As described above, this is known as the Morse Taper effect.

Reference is now made to FIGS. 3A and 3B, which are sectional and plan views, respectively, of the locking collar of one preferred embodiment of the present invention. Locking collar **24** has a tapered outer surface **26**, with a distal end **19**, having the major diameter, and a proximal end **23**, having the minor diameter. The distal end comprises a flat outer face designed to correspond to the flat underside of the head of a compression screw (not shown). A circumferential lip **28** is provided at distal end **19** for engaging a groove on the internal bore of the side plate (see FIGS. 1 and 2). Collar **24** also has a keyed internal profile **21**, for mating with a corresponding keyed cross-sectional profile on the lag screw (not shown), and a plurality of lengthwise slots **27** extending from the distal end **19** toward the proximal end **23**. These slots **27** facilitate disengagement of the circumferential lip **28** from the circumferential groove on the internal bore of the side plate (not shown), after the lag screw is satisfactorily engaged with the bone. As discussed above, the collar **24** facilitates alignment and ensures proper orientation of the lag screw, while allowing the screw to rotate freely so that its drilling portion **20** can engage its respective bone fragment during installation. An impact force subsequently applied to distal end **19** frictionally locks the tapered outer surface **26** to the mating tapered surface of the side plate internal bore (see FIG. 2). The locking collar may be formed of stainless steel, titanium, titanium alloy or any other material with suitable strength and bio-compatible characteristics.

Reference is now made to FIG. 4, which is a cross-sectional view of the side plate and locking collar of another preferred embodiment of the present invention. As for the embodiment discussed above, the side plate **10** has a flat portion **12** for connection to the femoral shaft and an angled barrel portion **14** having an internal bore **16** for slidably receiving a lag screw (not shown). A locking collar **50** sits within the internal bore **16**, and a deformable portion **52** on the collar **50** rotatably engages a circumferential groove **30** on the bore **16**. Deformable portion **52** includes a plurality of deformable, lengthwise tabs **54** (shown more clearly in FIGS. 5A-5C discussed below) that extend partially along the axial extent of the deformable portion. These tabs **54** have initial flat portions **55** at the distal end **56** of collar **50** (where the height of tabs **54**, as measured radially from the axial centerline of the collar, is greatest) and then taper toward the proximal end **58** of collar **50** (where the height of tabs **54** is smallest), forming an angle of about 20° with a longitudinal axis (70° with a vertical). Flat portions **55** of tabs **54** may have a length of about 1.3 mm. Prior to

insertion and alignment of the lag screw (not shown) and application of an impact force to the distal end **56** of the collar, the collar can rotatably slide within the bore **16**. The collar **50** has a keyed internal profile **21**, as shown most clearly in FIG. 5B, for mating and rotationally coupling with a corresponding keyed cross-sectional profile of the lag screw.

5 Thus, upon insertion of the lag screw through the bore **16** and collar **50**, rotation of the lag screw causes rotation of the locking collar **50** relative to the bore **16**. Upon application of an impact force to distal end **56** of collar **50**, collar **50** is driven proximally inward along bore **16** causing the high portions of tabs **54** to come into contact with the walls of the internal bore **16**. With sufficient impact force, the tabs **54** will deform causing the collar **50**
10 to become frictionally locked (both axially and rotationally) with the internal bore **16**.

Reference is now made to FIGS. 5A, 5B and 5C, which are side, plan and sectional views, respectively, of the locking collar **50** of this preferred embodiment of the present invention. Locking collar **50**, which is substantially cylindrical, has a deformable portion **52**, which includes a plurality of deformable, partial lengthwise tabs **54** having initial
15 flat portions **55** at the distal end **56** and tapering toward the proximal end **58** of collar **50**. As shown in FIG. 5B, tabs **54** are spaced about the circumference of collar **50** at distal end **56**. As shown best in FIGS. 5A and 5B, deformable portion **52** has a maximum diameter at the distal end **56** of collar **50**. This diameter is greater than the diameter of the internal bore **16** of the bone plate barrel portion (see FIG. 4). Distal end **56** comprises an outer face,
20 which may be flat or concave, designed to correspond to the underside of the head of a compression screw (not shown). Deformable portion **52** engages a groove **30** on the internal bore of the side plate (see FIG. 4) allowing collar **50** to rotatably slide within the bore **16**. Collar **50** also has a keyed internal profile **21**, for mating with a corresponding keyed cross-sectional profile on the lag screw (not shown).

25 As discussed above, collar **50** facilitates alignment and ensures proper orientation of the lag screw, while allowing the screw to rotate freely so that its drilling portion **20** can engage its respective bone fragment during installation. An impact force subsequently applied to distal end **56** frictionally locks the deformable tabs **54** of deformable portion **52** to the inner surface of the side plate internal bore (see FIG. 2). This friction, or
30 interference, fit prevents further rotation of the collar **50** relative to the internal bore. The locking collar **50** may be formed of stainless steel, titanium, titanium alloy or any other material with suitable strength and bio-compatible characteristics.

Reference is now made to FIGS. 6 and 7 which demonstrate the application of the device of the present invention to repair a fracture of the femoral neck (i.e., hip). As
35 shown, the assembled device **40** is used to join two bone segments **41**, **42** (i.e., the femoral

head and the femoral shaft). A lag screw **18** having a bone-engagement end, a distal end, and a keyed cross-sectional profile over part of its length is provided. The bone-engagement end of lag screw **18**, which may have a plurality of helically twisted blades **45** (shown in FIG. 6) or a cancellous screw thread **46** (shown in FIG. 7), is configured for
5 engaging first bone segment **41** and the distal end has a threaded bore.

A side plate **10** is provided having a flat portion for engaging second bone segment **42** and an angled barrel portion **14** with an internal bore for slidably receiving the lag screw. A portion of the internal bore (not shown) has a taper and a distal end of the internal bore has a circumferential groove.

10 A cylindrical locking collar **24** or **50** (not shown) having a hollowed cylindrical interior and a keyed internal profile is also provided. In one embodiment, the collar has an outer surface formed with a taper defined by a major diameter and a minor diameter, a distal end of the collar having the major diameter, a proximal end of the collar having the minor diameter, and a circumferential lip at the distal end for engaging the
15 circumferential groove of the internal bore. In another embodiment, the collar has a deformable portion with a maximum diameter greater than the diameter of the internal bore, where the distal end of the locking collar also engages a circumferential groove of the internal bore.

The system is assembled by inserting the cylindrical locking collar into the
20 internal bore of the bone plate so that it rotatably engages the internal bore. As discussed above, the system may be supplied to physicians with the locking collar already engaged in the internal bore of the bone plate, thus eliminating the need for physicians or technicians to insert the collar into the bore of the bone plate. The lag screw **18** is inserted into the locking collar, such that the keyed cross-sectional profile of the lag screw mates with the
25 keyed internal profile of the locking collar to rotationally couple the locking collar and the lag screw. After proper engagement of the lag screw **34** with the first bone segment **41**, the distal end of the locking collar (not shown) is impacted using a mallet-type instrument, frictionally locking the collar within the angled barrel portion **14** of the side plate **10**. This frictional locking prevents further rotation of the collar relative to the bone plate, and
30 thereby prevents further rotation of the lag screw relative to the bone plate. In an alternative arrangement, the collar is locked in place by a force in the distal direction, such as that applied by a slap-hammer. The side plate **10** would typically be anchored to the femoral shaft **42** using bone screws **44** (formed of stainless steel, titanium or titanium alloy). A compression screw **34** would then be inserted into the threaded bore (see FIG. 1) of the lag
35 screw, abutting the locking collar and axially drawing bone segment **41** toward bone

segment 42 (see FIGS. 6 & 7). Alternatively, the side plate 10 may be affixed to the femoral shaft prior to impact of the locking collar.

While the present invention has been described with reference to the preferred embodiments, those skilled in the art will recognize that numerous variations and modifications may be made without departing from the scope of the present invention. This is especially true with regard to the shape and configuration of the bone plate and lag screw, which can be adjusted according to the type and location of the bone segments to be joined. Accordingly, it should be clearly understood that the embodiments of the invention described above are not intended as limitations on the scope of the invention, which is defined only by the following claims.

THE CLAIMS:

What is claimed is:

- 5 1. A device for rotational stabilization of bone segments comprising:
a bone lag screw having a bone-engagement end, a distal end, and a keyed
cross-sectional profile, the bone-engagement end configured for
engaging a first bone segment;
a bone plate having a flat portion for engaging a second bone segment and a
10 barrel portion having an internal bore for slidably receiving the lag
screw; and
a locking collar having a proximal end, a distal end, a keyed internal profile
and a deformable portion at the distal end;
wherein the keyed internal profile mates with the keyed cross-sectional profile of the lag
15 screw to rotationally couple the locking collar and the lag screw when the lag screw is
inserted through the locking collar, and the deformable portion is configured and
dimensioned for (1) free rotation, in a first position, within the internal bore of the bone
plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of
the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone
20 plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate.
2. The device of claim 1, wherein the locking collar, in the second position, is
frictionally engaged in the internal bore of the bone plate by deformation of the deformable
portion within the internal bore of the bone plate.
- 25 3. The device of claim 2, wherein the deformation of the deformable portion of
the locking collar within the internal bore of the bone plate is achieved by application of a
force on the locking collar in a proximal direction.
- 30 4. The device of claim 3, wherein the deformable portion has a maximum
diameter at the distal end of the locking collar.
5. The device of claim 4, wherein the deformable portion tapers from the distal
end of the locking collar toward the proximal end of the locking collar.

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6. The device of claim 5, wherein the locking collar has a longitudinal axis and the tapered, deformable portion forms an angle of about 20° with the longitudinal axis.

5 7. The device of claim 6, wherein the deformable portion includes a plurality of deformable tabs extending part of the distance from the distal end of the locking collar toward the proximal end of the locking collar.

10 8. The device of claim 7, wherein the deformable tabs have flat portions at the distal end of the locking collar and taper toward the proximal end of the locking collar.

9. The device of claim 7, wherein the distal end of the locking collar has a circumference, and the plurality of deformable tabs are spaced about the circumference.

15 10. The device of claim 7, wherein the locking collar, in the second position, is frictionally engaged in the internal bore of the bone plate by deformation of the deformable tabs.

20 11. The device of claim 4, wherein the internal bore of the bone plate barrel portion has a diameter, and the maximum diameter of the deformable portion, when the collar is in the first position, is greater than the diameter of the internal bore.

12. The device of claim 1, wherein the locking collar is substantially cylindrical.

25 13. The device of claim 1, wherein the barrel portion of the bone plate is angled relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck.

30 14. The device of claim 1, wherein the lag screw is formed with a cancellous screw thread.

15. The device of claim 1, wherein the lag screw is formed with a plurality of helically twisted blades.

35 16. The device of claim 1, wherein the lag screw, bone plate, and locking collar are formed of stainless steel, titanium alloy, or titanium.

17. The device of claim 1, further comprising:
a threaded bore in the distal end of the lag screw; and
a compression screw insertable into the threaded bore of the lag screw.

5 18. The device of claim 17, wherein the compression screw, when threaded into the threaded bore of the lag screw, abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments.

10 19. The device of claim 17, wherein the compression screw is formed of stainless steel, titanium alloy, or titanium.

20. A device for rotational stabilization of bone segments comprising:
a bone lag screw having a bone-engagement end, a distal end, and a keyed
cross-sectional profile, the bone-engagement end configured for
15 engaging a first bone segment;
a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an internal bore for slidably receiving the lag screw; and
a substantially cylindrical locking collar having a proximal end, a distal end,
20 a hollowed cylindrical interior, a keyed internal profile and a plurality of deformable tabs at the distal end;

wherein the keyed internal profile mates with the keyed cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and the locking collar is configured and dimensioned for
25 (1) free rotation, in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate.

30 21. The device of claim 20, wherein the locking collar has a maximum diameter at its distal end.

35 22. The device of claim 21, wherein each of the deformable tabs has a flat portion at the distal end of the locking collar and tapers from the flat portion toward the proximal end of the locking collar.

23. The device of claim 22, wherein the locking collar has a longitudinal axis and the deformable tabs taper at 20° to the longitudinal axis.

24. The device of claim 20, wherein the distal end of the locking collar has a circumference, and the plurality of deformable tabs are spaced about the circumference.

25. The device of claim 21, wherein the internal bore of the bone plate barrel portion has a diameter, and the maximum diameter of the locking collar, when the collar is in the first position, is greater than the diameter of the internal bore.

26. The device of claim 20, wherein the locking collar, in the second position, is frictionally engaged in the internal bore of the bone plate by deformation of the deformable tabs within the internal bore of the bone plate.

27. The device of claim 26, wherein the deformation of the deformable tabs of the locking collar within the internal bore of the bone plate is achieved by application of a force on the locking collar in a proximal direction.

28. The device of claim 20, wherein the barrel portion of the bone plate is angled relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck.

29. The device of claim 20, wherein the lag screw, bone plate, and locking collar are formed of stainless steel, titanium alloy, or titanium.

30. The device of claim 20, further comprising:
a threaded bore in the distal end of the lag screw; and
a compression screw insertable into the threaded bore of the lag screw.

31. The device of claim 30, wherein the compression screw, when threaded into the threaded bore of the lag screw, abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments.

32. The device of claim 30, wherein the compression screw is formed of a stainless steel, titanium alloy, or titanium.

33. The device of claim 20, further comprising a circumferential groove at a distal end of the internal bore of the bone plate barrel portion which engages the distal end of the locking collar such that the collar freely rotates within the internal bore of the barrel in the first position.

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1/5

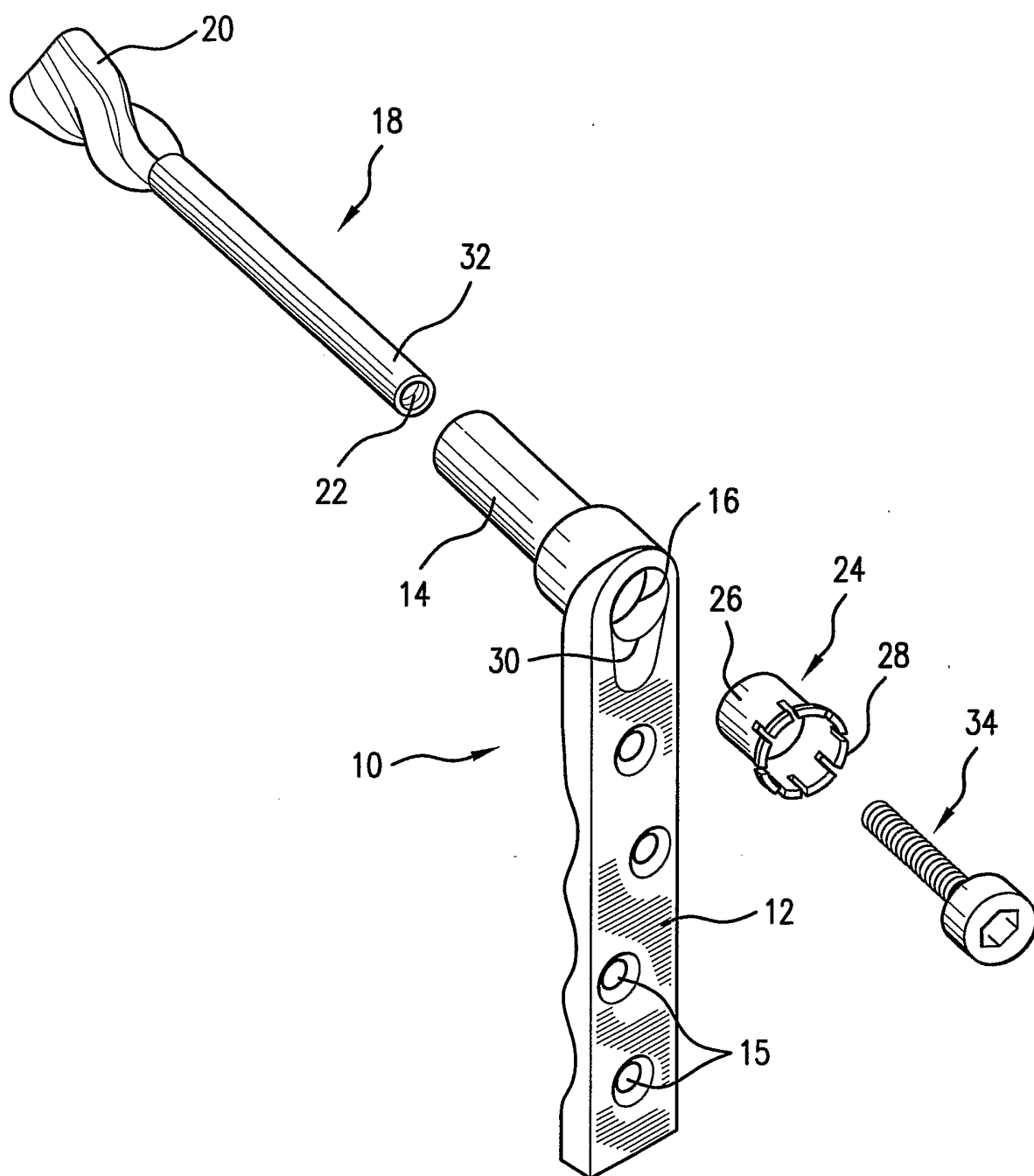


FIG. 1

2/5

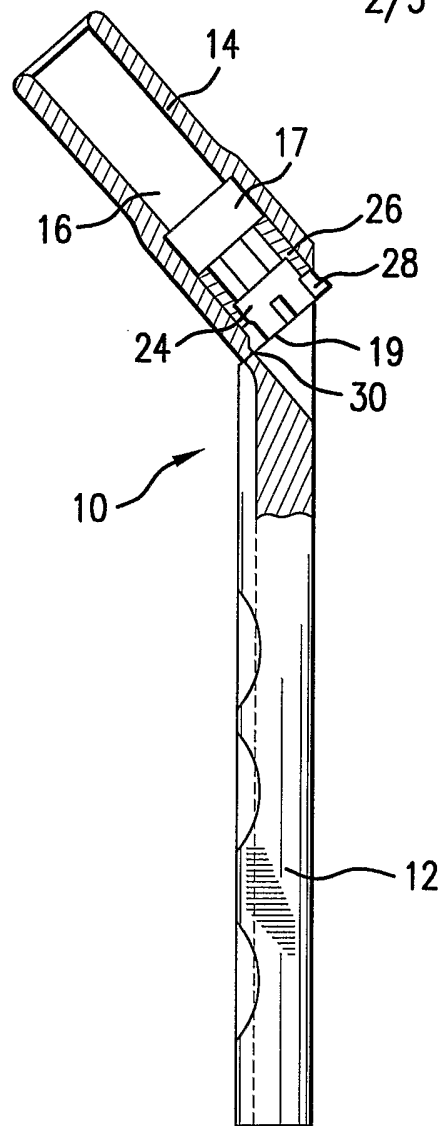


FIG. 2

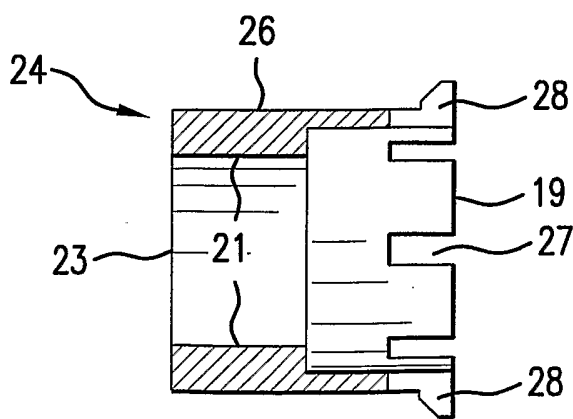


FIG. 3A

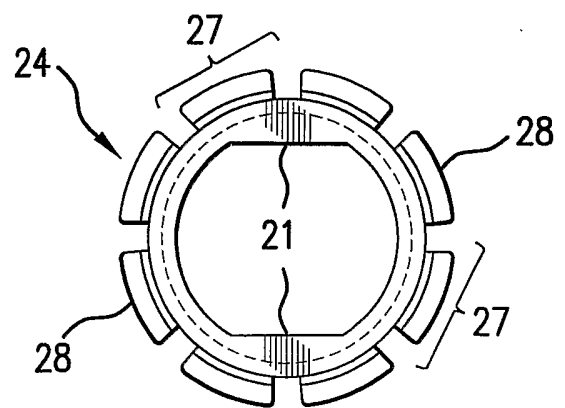


FIG. 3B

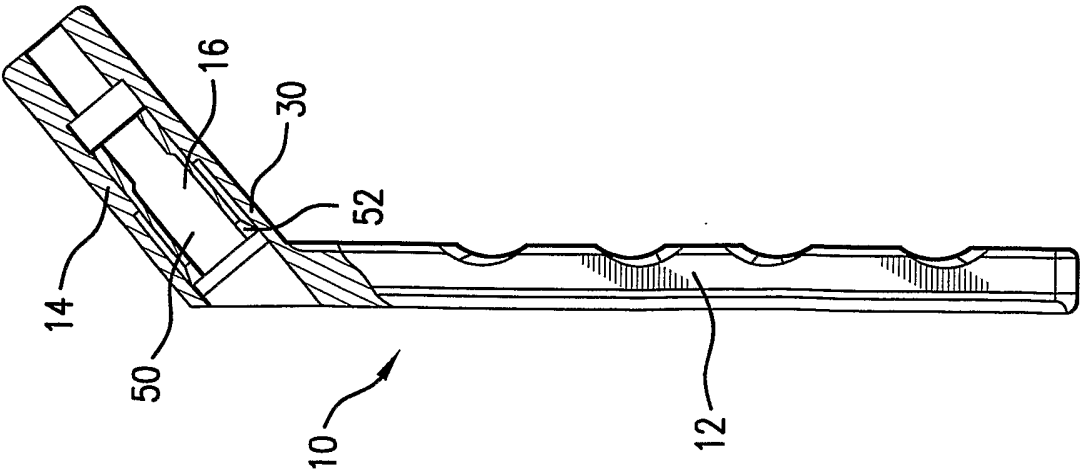


FIG. 4

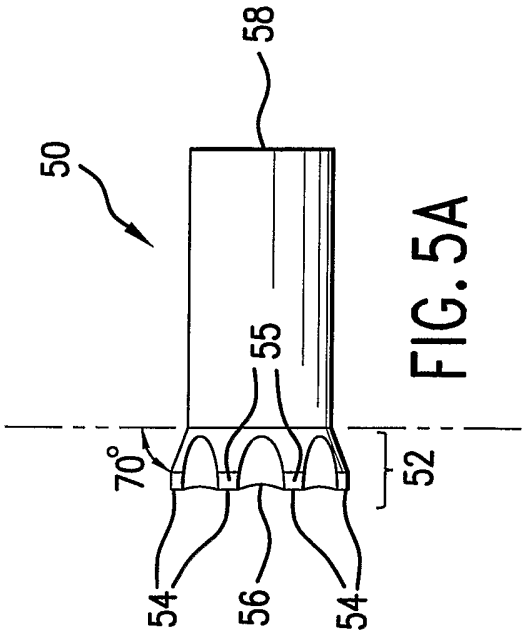


FIG. 5A

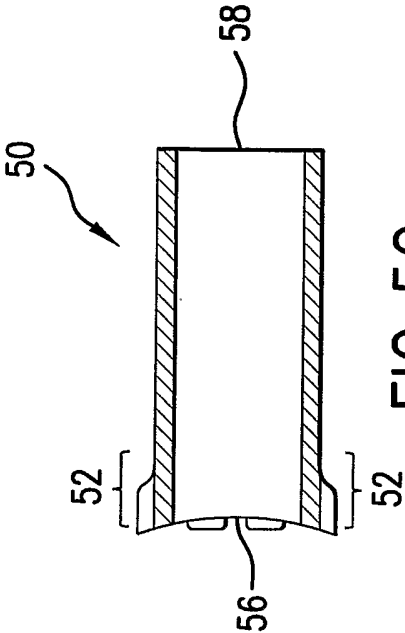


FIG. 5C

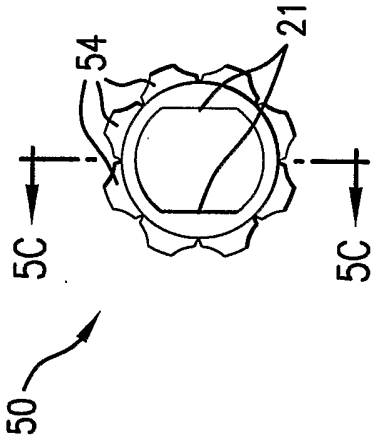


FIG. 5B

4/5

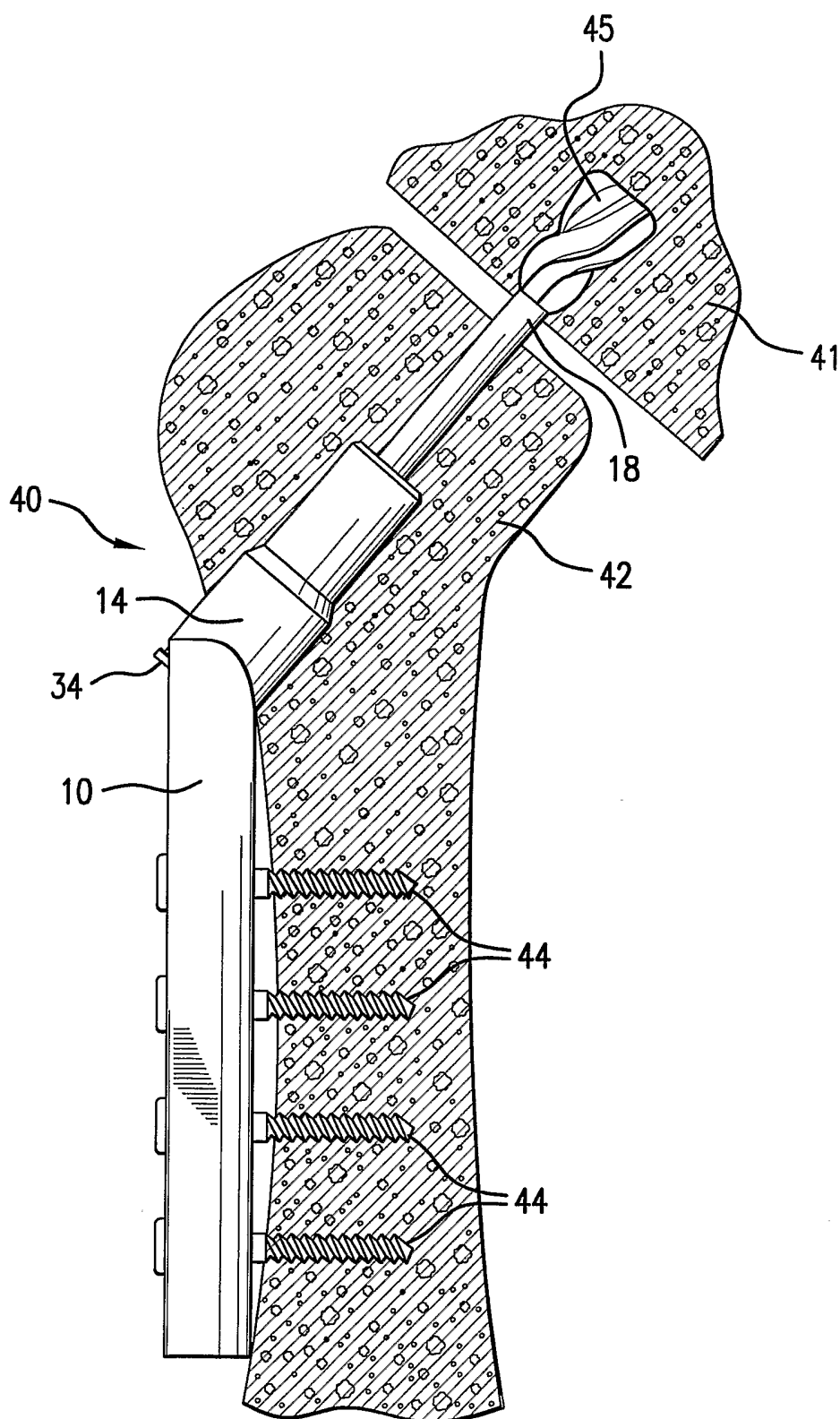


FIG. 6

5/5

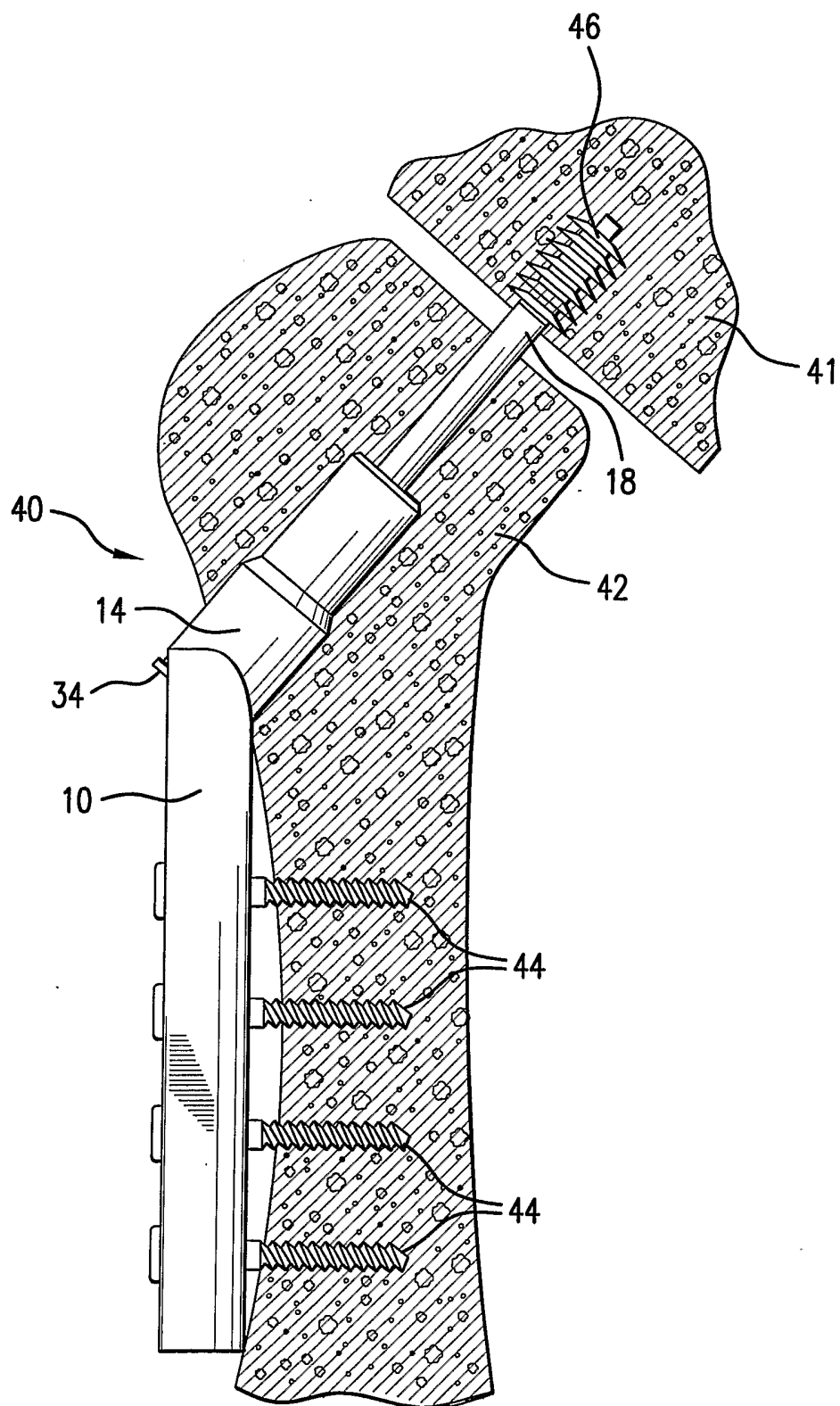


FIG. 7

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 02/30929

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 A61B17/74

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHEDMinimum documentation searched (classification system followed by classification symbols)
IPC 7 A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 530 355 A (GRIGGS CALVIN) 23 July 1985 (1985-07-23) column 3, line 34 - line 40 column 3, line 56 - column 4, line 20 column 5, line 46 - line 58 figures 1-5 -----	1,20



Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

° Special categories of cited documents :

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- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- *&* document member of the same patent family

Date of the actual completion of the international search

13 December 2002

Date of mailing of the international search report

07/01/2003

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 02/30929

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