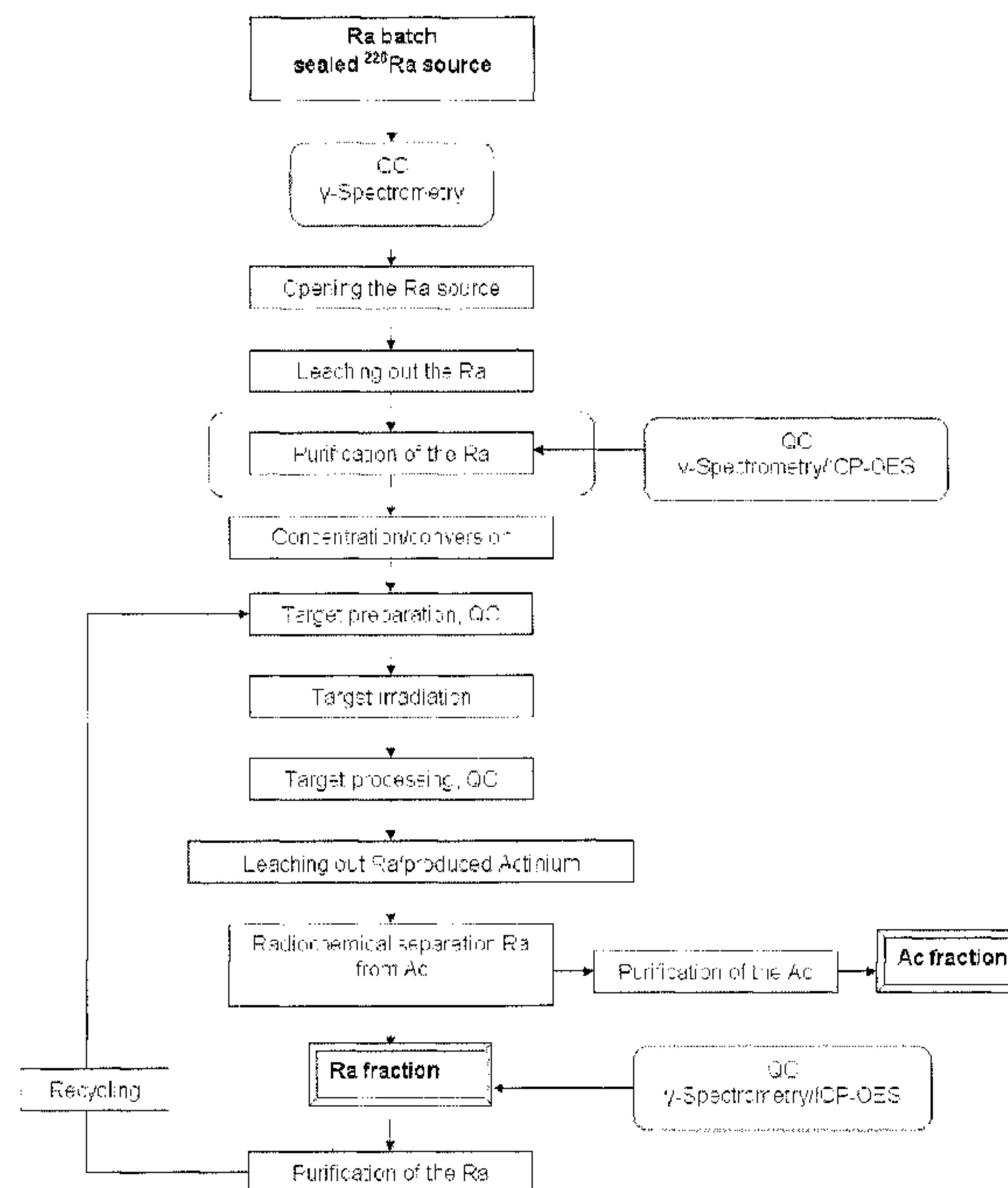




(22) Date de dépôt/Filing Date: 2007/09/06
(41) Mise à la disp. pub./Open to Public Insp.: 2008/03/13
(45) Date de délivrance/Issue Date: 2018/10/23
(62) Demande originale/Original Application: 2 662 932
(30) Priorité/Priority: 2006/09/08 (DE10 2006 042 191.4)

(51) Cl.Int./Int.Cl. *B01D 59/26* (2006.01),
B01D 15/08 (2006.01), *G21F 9/30* (2006.01),
G21G 1/10 (2006.01), *H05H 6/00* (2006.01)
(72) Inventeurs/Inventors:
KABAI, EVA, DE;
MORENO BERMUDEZ, JOSUE MANUEL, DE;
HENKELMANN, RICHARD, DE;
TURLER, ANDREAS, DE
(73) Propriétaire/Owner:
ACTINIUM PHARMACEUTICALS, INC., US
(74) Agent: BORDEN LADNER GERVAIS LLP

(54) Titre : PROCEDE POUR LA PURIFICATION DU RADIUM DE DIFFERENTES SOURCES
(54) Title: METHOD FOR THE PURIFICATION OF RADIUM FROM DIFFERENT SOURCES



(57) **Abrégé/Abstract:**

The present application is directed to a method for the purification of Radium, in particular ²²⁶Ra, for target preparation for an essentially pure ²²⁵Ac production from available radioactive sources, using an extraction chromatography in order to separate chemically similar elements such as Ba, Sr, and Pb from the desired Ra; wherein said extraction chromatography has an extractant system on the basis of a crown ether. The invention is further related to a method for recycling of ²²⁶Ra, for target preparation for ²²⁶Ac production from radium sources irradiated with accelerated protons (p,2n), after separation of the produced ²²⁵Ac. In this method a combination of the above extraction chromatography and a cation exchange chromatography is used. The obtained ²²⁶Ra is essentially free of the following chemical contaminants consisting of Ag, Al, As, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, Li, Mg, Mn, Na, Ni, Pb, Sr, V, Zn, and Ba.

Abstract

The present application is directed to a method for the purification of Radium, in particular ^{226}Ra , for target preparation for an essentially pure ^{225}Ac production from available
5 radioactive sources, using an extraction chromatography in order to separate chemically similar elements such as Ba, Sr, and Pb from the desired Ra; wherein said extraction chromatography has an extractant system on the basis of a crown ether. The invention is further related to a method for recycling of ^{226}Ra , for target preparation for ^{225}Ac production from radium sources irradiated with accelerated protons (p,2n), after separation of the
10 produced ^{225}Ac . In this method a combination of the above extraction chromatography and a cation exchange chromatography is used. The obtained ^{226}Ra is essentially free of the following chemical contaminants consisting of Ag, Al, As, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, Li, Mg, Mn, Na, Ni, Pb, Sr, V, Zn, and Ba.

15

20

Method for The Purification of Radium from Different Sources

This application is a divisional application of Canadian patent application number
5 2,662,932 filed September 6, 2007.

The present invention relates to a method for the purification of radium, in particular
 ^{226}Ra , for target preparation for ^{225}Ac production from available radioactive sources
according to claim 1 as well as to a method for recycling of ^{226}Ra , for target preparation for
 ^{225}Ac production from radium sources irradiated with accelerated protons (p,2n), after
10 separation of the produced ^{225}Ac .

The investigations and experimental work of the present invention was carried out at
the Technical University of Munich [TUM], Institute of Radiochemistry [RCM].

In particular, the radionuclide ^{225}Ac can be successfully used in nuclear medicine -
bound to tumor specific antibodies - in various clinical trials in the treatment of cancer,
15 particularly in form of its daughter nuclide ^{213}Bi .

Already in 1993, criteria for the selection of radionuclides for immunotherapy with α -
emitters and β -emitters were provided for the first time (GEERLINGS, M.W. (1993): Int. J.
Biol. Markers, 8, 180-186: "Radionuclides for radioimmunotherapy: criteria for selection")
where it turned out due to the difference in energy that the radioactivity of α -emitters to be
20 applied may be more than 1000 times lower than that of β -emitters, if a comparable effect is
to be achieved.

Moreover, in the above literature, the α -emitting radionuclides ^{225}Ac and its daughter
isotope ^{213}Bi turned out to be highly promising for the objects of radioimmunotherapy
alongside the in principle usable, however relatively poorly available or instable antibody
25 conjugate producing α -emitters: ^{211}At , ^{255}Fm , $^{212}\text{Bi}/^{212}\text{Pb}$, ^{224}Ra , ^{233}Ra .

One of the fundamental studies for the foundation of a radioimmunotherapy with α -
emitters is disclosed in GEERLINGS, M.W., KASPERSEN, F.M., APOSTOLIDIS, C. and
VAN DER HOUT, R. (1993): Nuclear Medicine Communications 14, 121-125, "The feasibility
of ^{225}Ac as a source of α -particles in radioimmunotherapy". Here it is described that ^{225}Ac
30 produced from ^{229}Th and the daughter isotope of ^{225}Ac , namely ^{213}Bi is suitable as isotope for
the radioimmunotherapy with α -emitters. As indications there are described in particular
cancer treatment and the treatment of micrometastases of malign tumors using tumor-
specific monoclonal antibodies as carriers for α -emitters.

A further study of KASPERSEN, F.M., BOS, E., DOORNMALEN, A.V., GEERLINGS, M.W., APOSTOLIDIS, C. and MOLINET, R. (1995): Nuclear Medicine Communications, 16, 468-476: "Cytotoxicity of ^{213}Bi - and ^{225}Ac -immunoconjugates" confirms and quantifies the cytotoxic effect of ^{213}Bi and ^{225}Ac with in vitro tests using the human epidermoid tumor cell line A431.

Moreover, it is suggested to use ^{213}Bi for the treatment of malignant diseases of the blood system, and in the meantime, various radioimmunotherapeutic approaches with ^{225}Ac and ^{213}Bi for the treatment of cancer are in various phases of clinical trials.

The medical-clinical significance of the present invention for the preparation of ^{225}Ac form ^{226}Ra by means of accelerated protons may be seen for example from two promising therapeutic approaches:

On the one hand, JURCIC, J.G., LARSON, S.M., SGOUROS, G., McDEVITT, M.R., FINN, R.D., DIVGI, C.R. Åse, M.B., HAMACHER, K.A., DANGSHE, M., HUMM, J.L., BRECHBIEL, M.W., MOLINET, R., SCHEINBERG, D.A. (2002) in Blood, 100, 1233-1239 report a significant success in the treatment of patients with acute myelogenous leukaemia (AML) and chronic myelogenous leukaemia (CML) by using ^{213}Bi , which is bound to HuM195, a formulation of a monoclonal anti-CD33-antibody, which was developed for the humane medicine. This study was the first proof-of-concept where a human being was treated with a systemic radioimmunotherapy comprising an α -emitter, which is transported to a tumor specific cellular target.

On the other hand, HUBER, R., SEIDL, C., SCHMID, E., SEIDENSCHWANG, S., BECKER, K.-F., SCHUMACHER, C., APOSTOLIDIS, C., NIKULA, T., KREMMER, E., SCHWAIGER, M. and SENEKOWITSCH-SCHMIDTKE, R. (2003): Clinical Cancer Research (Suppl.) 9, 1s-6s: "Locoregional α -Radioimmunotherapy of Intraperitoneal Tumor Cell Dissemination Using a Tumor-specific Monoclonal Antibody" report the therapeutic effectivity of ^{213}Bi -d9MAB – with low bone marrow toxicity – and the possible application of a locoregional therapy for patients who suffer from gastric carcinoma, who express d9-E-Cadherine.

More results of studies and partial aspects in this matter are shown in: Roswitha HUBER, doctorate dissertation in the Faculty of Veterinary Medicine submitted to the Ludwig-Maximilians-University of Munich, July 18, 2003: "Bewertung der lokoregionalen Radioimmuntherapie disseminierter Tumorzellen des diffusen Magenkarzinoms mit einem ^{213}Bi gekoppelten tumorspezifischen Antikörper im Mausmodell" (Evaluation of a locoregional

radioimmunotherapy of disseminated tumor cells of the diffuse gastric carcinoma with a ^{213}Bi bound tumor specific antibody in the mouse model).

According to HUBER 2003, each year 18 out of 100 000 Germans come down with gastric carcinoma alone. In Japan, even 126 out of 100 000 people are affected. This means
 5 about 156 000 incidences per year in Japan alone. There, as well as in China, Taiwan and Korea, gastric carcinoma is one of the most frequent causes of death in consequence of a tumor.

Up to now the application of cytostatica within a chemotherapy seemed to be the most promising therapeutic way however, the side effects are significant.

10 The radioimmunotherapy, in contrast, uses protein structures located on the membrane, that are expressed by tumor cell lines in order to bind cytotoxic active substances via a carrier. Mostly, an overexpression of the binding molecule at the tumor cell is central to a radioimmunotherapy. The target molecule for the tumor associated antibodies is thus also expressed to a lower extend in physiologic cells of the organism. This implies
 15 that any therapeutic agent for radiotherapy also binds to these cells.

Particularly, in the treatment of acute or chronic myelogenous leukaemia the meaning of the present invention takes effect, namely for the preparation of a suitable α -emitter, namely ^{225}Ac which forms through decay reaction the bound, for example, to a tumor specific antibody.

20 The ^{213}Bi atom decays via β -decay to ^{213}Po , which releases its α -decay energy of 8,4 MeV with a half life of 4 μs in the tissue within a distance of 80 μm when decaying and thus kills effectively cells in its immediate neighborhood due to its high linear energy transfer.

The so called locoregional application enables a quick binding of ^{213}Bi bound tumor specific antibody to the tumor antigens with maximal therapeutic success and minimal
 25 toxicity.

One of the few α -emitter which fulfill the relevant therapeutic criteria is the nuclide pair $^{213}\text{Bi}/^{213}\text{Po}$ with a half-life of 45,6 min (^{213}Bi). The photon emission of ^{213}Bi with 440 KeV additionally permits an in vivo scintiscanning of the patient.

Nowadays, accelerated proton irradiation of ^{226}Ra can be used to produce ^{225}Ac . In
 30 cyclotrons, developed for the first time 1931, electrically charged particles are moving on spiral shaped orbits in magnetic flux lines.

In particular, protons can be accelerated with the help of a cyclotron with currents that are high enough to such high velocities that they can be used in experimental and applied nuclear physics for the production of isotopes in a quantitative scale.

EP 0 752 709 B1 describes, for example, a method for producing actinium-225 from
5 Radium-226, whereby accelerated protons are projected in a cyclotron onto a target of radium-226, so that the instable compound nucleus ^{227}Ac is transformed into actinium-225 while emitting two neutrons (p,2n-reaction), whereby after a waiting period, during which the actinium-226, which has been created simultaneously due to the emission of only one neutron, decays mostly due to its considerably shorter half-life and actinium is chemically
10 separated, so that a relatively pure isotope Ac-225 is obtained. The ^{226}Ra target used according to the procedure of EP 0 752 709 B1 is not specified in detail there.

EP 0 962 942 A1 also describes a method for producing Ac-225 by irradiation of ^{226}Ra with cyclotron accelerated protons having an energy of 10 to 20 MeV.

Although it is already possible to achieve good actinium-225-yields with the targets
15 according to EP 0 962 942 A1, it has turned out in practice that this target construction can heat itself under certain conditions due to the proton beam in such a way that the silver capsule tears open and might thus both destroy the target and contaminate the peripheral compounds.

In order to solve these target problems, the inventors of the present inventions have
20 designed two different improved radium targets for the production of radionuclides by means of accelerated protons, on the basis of the prior art of EP 0 962 942 A1.

The one target preparation, a method of electrodeposition of ^{226}Ra -material is disclosed in Applicant's German patent application, DE 103 47 459 B3, published on May 25, 2005, the other one, an evaporation-dispensing system, is disclosed in Applicant's German
25 patent application, DE 10 2004 022 200 A1, published on December 1, 2005.

Applicant's methods of target preparation provide the finally desired ^{225}Ac -product on an Aluminum surface, and in a mixture of different radionuclides.

Nevertheless, the final product contains unconverted ^{226}Ra and other Ra isotopes. In addition, different decay products of actinium occur as well as nuclear conversions of
30 contaminating elements such as Al.

Impurities in the Al mesh measured by k_0 -Based Neutron Activation Analysis ($k_0\text{INAA}$) are given in Table 1:

Table 1

Element	Content [μg/g]	Element	Content [μg/g]
Fe	1302	La	0.69
Cr	701	W	0.2
Ni	0.2	Sb	0.07
Ga	145	Th	0.18
Zn	39	Br	0.11
Na	9	Sm	0.08
Mo	3.5	As	0.06
U	1.3	Sc	0.02
Co	2.0	Au	0.002
Ce	1.8		

Particularly important is to minimize the content of Sr and Ba which lead to the production of radioisotopes of Y and La, respectively.

5 The typical main chemical impurities in the radium available from radioactive ampoules used in the experiments (claimed as secondary standards) is given in Table 2.

Table 2

ELEMENT	mg/mg _{Ra} *
Ba	0.63
Ca	0.59
Na	0.46
Zn	0.08

* mgI/mgRa – mg impurity per mg radium

10

Several radioisotopes are produced as a result of nuclear reactions type (p,n) or (p,2n) on impurities like Ba, Ca, Fe, Zn, Sr, Pt, V, Ti, Cr, Mg, Mn, Na and Cu which can be present in the Al carrier (foil, mesh) and/or in the Ra deposit. The radionuclides of major contribution to the total gamma activity excluding ²²⁶Ra and daughters are typically the following: ⁵⁵Co, ⁵⁶Co, ⁶⁷Ga, ⁵⁷Ni, ⁵¹Cr, ⁴⁸V, ⁵²Mn, ⁵⁴Mn, ⁶⁵Zn.

15

In addition, disturbing radiochemical impurities are ^{210}Po and ^{210}Pb resulting from the following decay chain: **Ra-226 (alpha)** $\rightarrow$ Rn-222(alpha) $\rightarrow$ Po-218 (alpha) $\rightarrow$ Pb-214 (beta) $\rightarrow$ Bi-214 (beta) $\rightarrow$ Po-214 (alpha) $\rightarrow$ **Pb-210 (beta)** $\rightarrow$ Bi-210 (beta) $\rightarrow$ **Po-210 (alpha)** $\rightarrow$ Pb-206 (stable).

5 To summarize, however, despite the already optimized target systems as provided by Applicant's German patent applications DE 103 47 459 B3, published on May 25, 2005 and DE 10 2004 022 200 A1, published on December 1, 2005, the final ^{225}Ac -product still contains significant amounts of inorganic, radionuclidic and organochemical impurities, which render the obtained ^{225}Ac product unsuitable for direct medical or pharmaceutical application.

10 A purification of the ^{225}Ac product is suggested in German patent application DE 10 2006 008 023 A1, published on August 30, 2007 and filed on 21.02.2006 by the Applicant of the present application, and having the title "Method for Purification of ^{225}Ac from Irradiated ^{226}Ra -Targets".

Moreover starting from pure radium as raw material, the contaminations in the
15 produced actinium can be significantly reduced.

The general aspects of the radioanalytical separation of radium were formerly summarized by KIRBY H.W. and SALUTSKY M.L (1964) "The radiochemistry of radium", NAS-NS-3057.

Between the known procedures can be found those applying Mme CURIE's classical
20 method based on co-precipitation (with barium sulphate) for isolating radium from pitchblende and fractional crystallization for separating radium from its chemical homologue barium (CURIE M. -Nobel Lecture 1911, Stockholm). The same procedure was used to revise the atomic mass of radium by HÖNIGSCHMID O. (1911) Mitteilungen aus dem Institute für Radiumforschung – „Revision des Atomgewichtes des Radiums und Herstellung
25 von Radiumstandardpräparaten“ and HÖNIGSCHMID O. and SACHTLEBEN R. (1934), – Z. anorg. u. allg. Chem, Bd. 221, S. 65-82 supported by GERLACH W. and RIEDL E. (1934), - Z. anorg. u. allg. Chem, Bd 221, S. 103-108. Others were using the precipitation method with concentrated nitric acid. The disadvantage of this method is due to the difficulty in handling fuming nitric acid. Later on, other precipitation agents were also more or less successfully
30 applied like oxalate, carbonate or chromate (SALUTSKY M.L. and STITES J.G (1955), - Ind. Eng. Chem., Vol. 47 No. 10, pp. 2162-2166).

All these tedious classical methods have the disadvantage that the complete isolation of radium is only possible after several repetitions of the mentioned procedure but allow the

isolation of high quantities of radium. For example is well known that Mme Curie isolated the radium after hundred and more fractional crystallization steps.

Afterwards, new chemical methods were tested and successfully applied for separation/concentration of small amounts of radium in a more efficient way. In-between can
5 be found chromatography, ion exchange, organic extraction or extraction chromatography.

The use of one of these modern methods for separation/purification of radium is described in several scientific works like those of TOMPKINS E.R. (1948), - J. Am Chem Soc. Vol 70, No. 10, pp. 3520-3522, POWER W.H. et al. (1959), - Anal. Chem. Vol. 31, No 6, 1077-1079, NELSON F. (1964), - J. Chromat. 16 , pp. 403, CHIARIZIA R. et al. (1995), -
10 Solv Extr. Ion. Exch. 13 (6) 1063-1082, WLODZIMIRSKA B., BARTOS B., BILEWITZ A. (2003), - Radiochim. Acta 91, 9, MOON D.S., BURNETT B. (2003), - Appl. Rad. Isot 59, pp. 288, HAGERMANN F. (1950), - J. Am Chem, Soc. 72 p768, BURNETT W., CABLE P. (1995), - Radioactivity and Radiochemistry Vol. 6, No. 3, pp 36-44 etc.

Due to its chemical properties, one of the frequently used methods for radium
15 purification from the above mentioned ones is the cation exchange chromatography.

The difficulty of the radium purification procedure based on cation exchange is due to the limitations regarding the eluting agents. Usually this method implies the use of complexing agents to facilitate the separation and increase the decontamination factors. In VDOVENKO V.M. and DUBASOV Y.U. (1973), "Analytical chemistry of radium", John Wiley
20 & Sons, GLEASON G. (1980), "An improved ion exchange procedure for the separation of barium from radium", Ann. Arbor Science Publishers Inc. pp. 47-50 and SAMUELSON O. (1963), "Ion exchange separations in analytical chemistry", John Wiley & Sons as well as TOMPKINS E.R. (1951), US-554649 this type of purification with complexing agents is well detailed.

25 The main difference between the enumerated classical and modern separation techniques is the amount of radium used for testing. The classical methods were successfully applied on high amounts of radium while the modern methods were generally tested for trace or low level radium contents.

In this particular application, the final form of the radium (up to 100 mg level) used for
30 target preparation is preferably an acidic solution in HNO₃, free from any complexing agent. Thus, the proposed purification step based on cation exchange omits any use of such complexing agents.

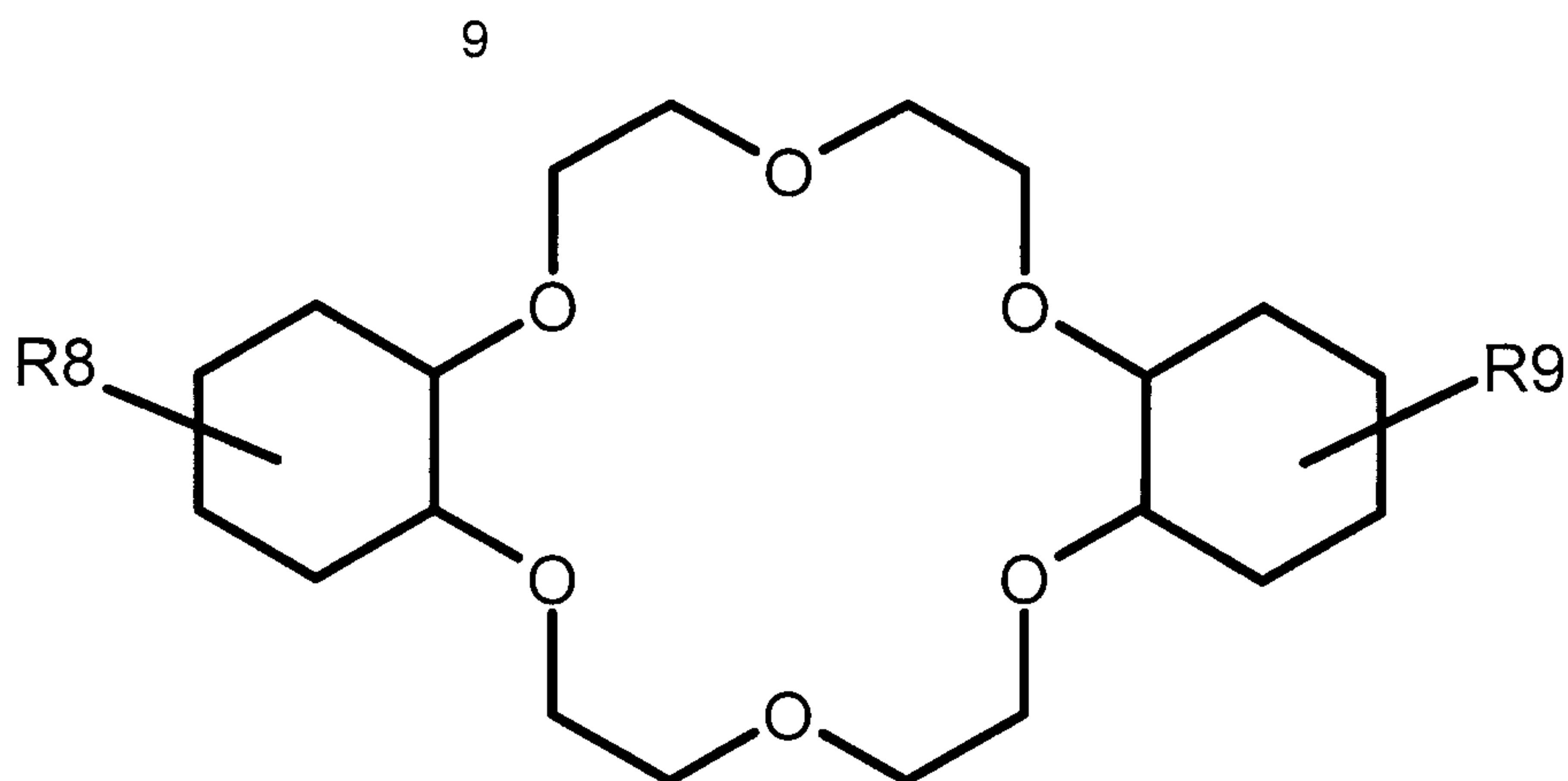
This method of the purification of radium is based on the retention of radium on a special cation exchange resin and elution of the possible contaminants. Formerly in van der WALT T.N. and STRELOW F.W.E. (1983), Anal. Chem. Vol. 55, pp.212-216 as well as in STRELOW F.W.E. (1985), -Anal. Chem. Vol. 57, pp. 2268-2271 it was demonstrated the usefulness of these resins for other purposes.

In the present invention this step was successfully tested to purify radium until some milliCuries, while the extraction chromatographic method was applied until hundreds of micrograms of radium.

Starting from the above explained problem of possible radium impurities, it is the object of the present invention to provide radium, and in particular ^{226}Ra , with a purity, suitable for cyclotron target preparation for ^{225}Ac production from available radioactive sources.

This problem is solved by a method for the purification of radium, in particular ^{226}Ra , for target preparation, particularly cyclotron target preparation, for ^{225}Ac production from available radioactive sources, comprising the following steps:

- a) detecting the quality of the Ra material to be purified;
- b) leaching out Ra with a mineral acid from its storage vessel at least one time;
- c) carrying out at least one extraction chromatography in order to separate chemically similar elements such as Ba and Sr from the desired Ra;
- d) wherein said extraction chromatography in step c) is carried out on a solid support material having an extractant system coated thereon, comprising at least one compound in accordance with general formula I in at least one compound in accordance with general formula II,



Formula I



Formula II

5

wherein in formula I:

R8 and R9 independently is H, C₁ – C₆ alkyl, or t-butyl;

and

wherein in formula II:

10

R10 is C₄ to C₁₂ alkyl; and wherein HNO₃ or HCl is used as mobile phase;

e) recovering Ra from the early fractions, whereas Ba and Sr are contained in fractions with higher retention time and the Pb is retained on the extractant system;

15

f) pooling Ra fractions; and

g) concentrating the purified Ra-containing fractions.

According to the present invention, the Pb is retained on the extractant and can only be removed using high concentrated HCl or complexing agents such as EDTA.

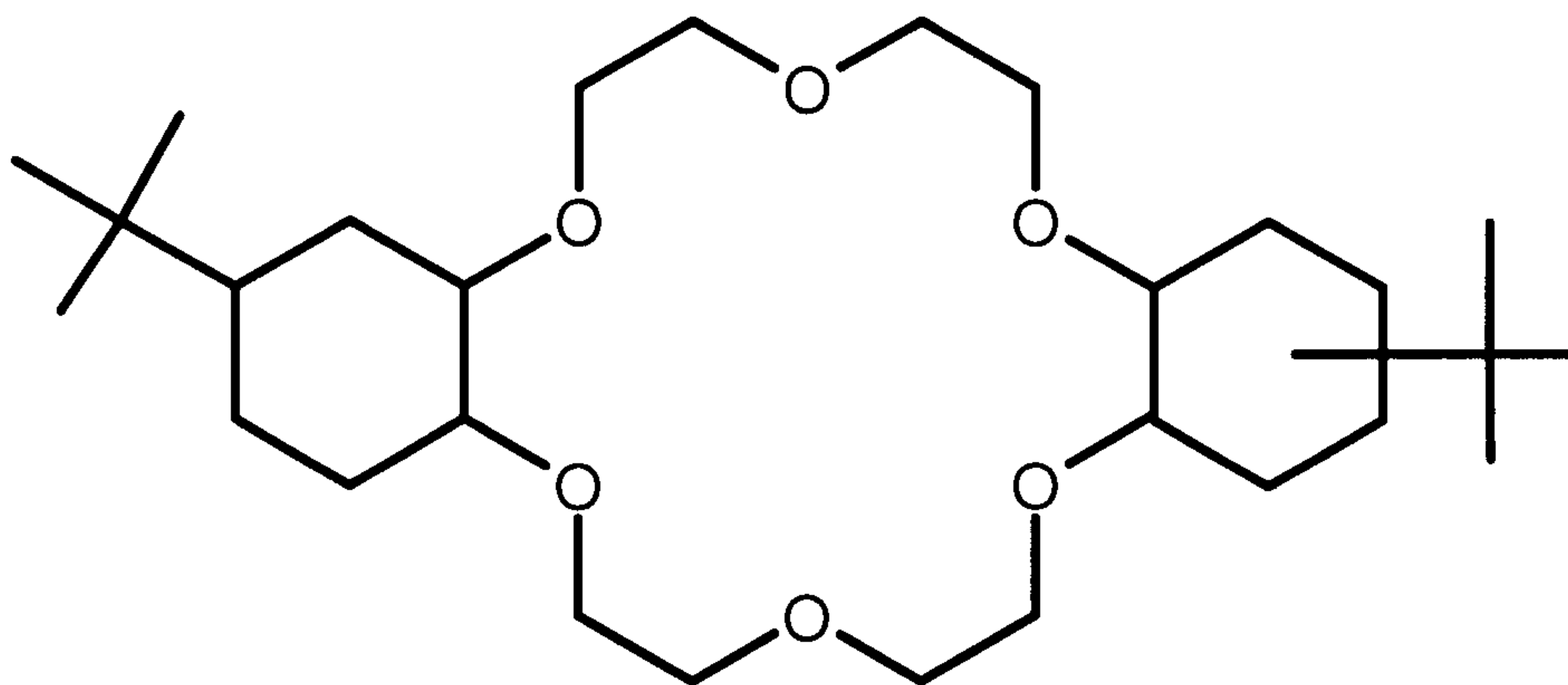
In a preferred method according to the invention, wherein HNO_3 , in particular 0.1 M HNO_3 is used for the accomplishment of step b) and/or in step d) HNO_3 or HCl is used as said mobile phase in a concentration range of 0.1 M to 4 M, in particular 1 M.

5 An appropriate tool for concentration of Ra-containing starting or stock solutions is a rotary evaporator.

Dried or highly concentrated residues are redissolved in a minimum volume of a mineral acid, in particular HNO_3 , preferably 0.1 M HNO_3 .

10 In a preferred embodiment of the present invention, the natural decay product ^{222}Rn is removed from the Ra material, in particular during an evaporation step. Such an evaporation step is e.g. the evaporation within a rotary evaporator. As Rn retaining medium activated carbon traps are used.

In practice, a method using an extractant system having a crown ether in accordance with formula III has proven to be advantageous:



Formula III

15 in 1-octanol.

A particularly preferred extractant system is 4,4'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.

20 Another preferred extractant system is 4,5'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.

In practice, it is preferred to use a commercially available resin such as "Sr Resin" made by EICHRON, the extractant in the stationary phase is a crown ether: 4, 4'(5')-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.

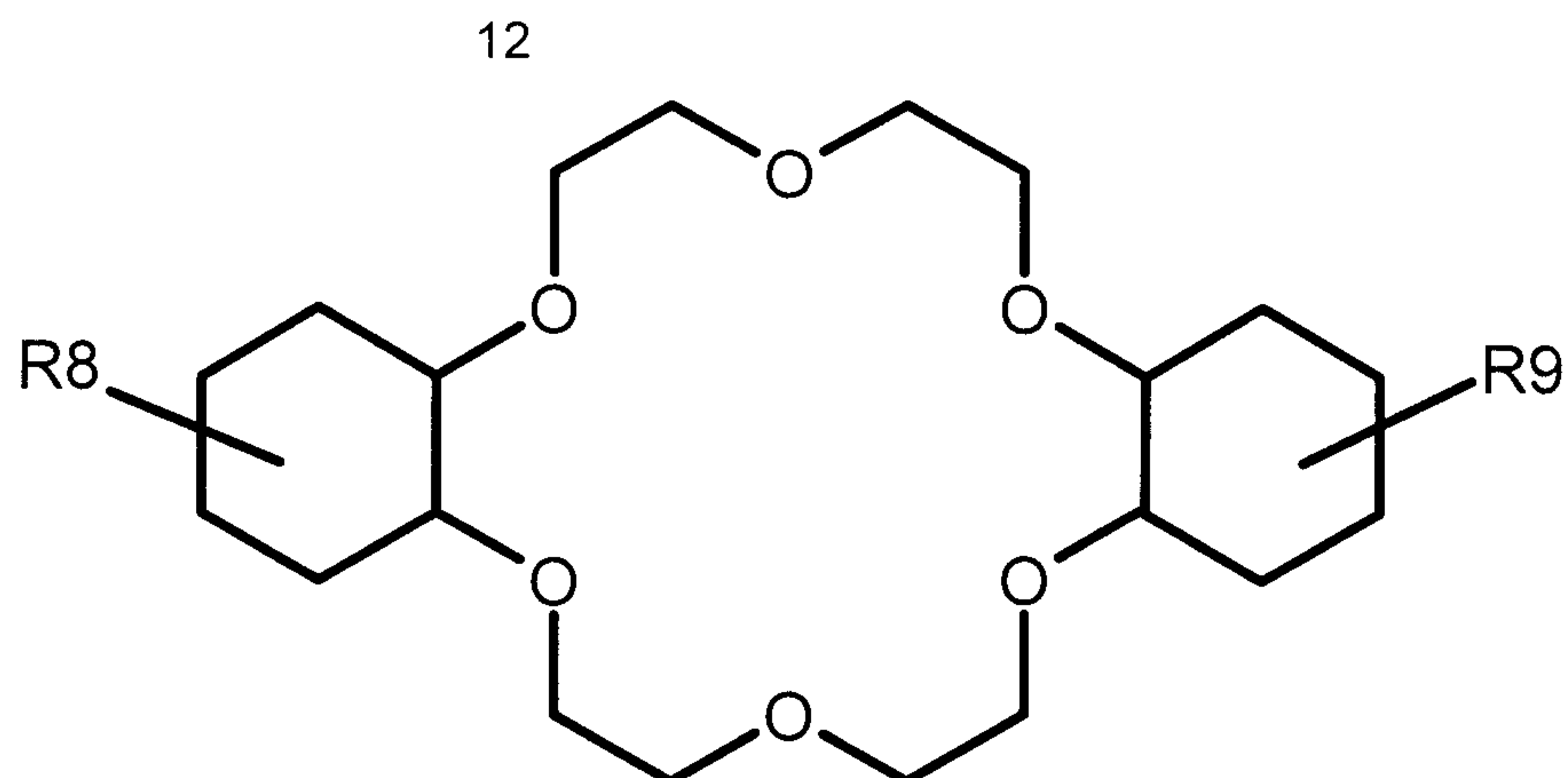
Typically, the detection of the quality of the Ra material is carried out by γ -spectrometry, in particular in situ γ -spectrometry, and by Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES).

Purified Ra-fractions of the extraction chromatography are conveniently concentrated
5 by evaporation to dryness, in particular by means of a spiral-line heater or silicon heater.

It is a further object of the present invention to provide an effective method for recycling of ^{226}Ra , for cyclotron target preparation for ^{225}Ac production from radium targets irradiated with accelerated protons (p,2n), after separation of the produced ^{225}Ac .

This problem is solved by a method comprising the following steps:

- 10 a) detecting the quality of a Ra-containing solution to be purified being provided in a mineral acid solution;
- b) concentrating the Ra-containing solution by evaporation;
- c) removing trace amounts of organic compounds by means of a prefilter column wherein said prefilter column is an inert solid support material.
- 15 d) carrying out at least one cation exchange chromatography in order to separate the Ra from the main chemical contaminants, wherein said cation exchange chromatography in step d) is carried out on an acidic cation exchanger, and preferably on an acidic macroporous type cation exchanger.
- 20 e) washing the cation exchange resin with low molar mineral acid to remove the main chemical contaminants;
- f) eluting Ra from the cation exchange resin with high molar mineral acid wherein such fractions still contain chemically similar elements such as Ba and Sr;
- 25 g) pooling and concentrating the partially purified Ra fractions; and
- h) subjecting the partially purified Ra-containing fractions to at least one extraction chromatography, wherein said extraction chromatography step is carried out on a solid support material having an extractant system coated thereon, comprising at least one compound in accordance with
30 general formula I in at least one compound in accordance with general formula II,



Formula I



Formula II

5

wherein in formula I:

R8 and R9 independently is H, C₁ – C₆ alkyl, or t-butyl;

and

wherein in formula II:

R10 is C₄ to C₁₂ alkyl; and wherein HNO₃ or HCl is used

10

as mobile phase;

i) recovering Ra from the early fractions, whereas Ba and Sr are contained in fractions with higher retention time;

j) pooling Ra fractions; and

k) concentrating the purified Ra-containing fractions.

15

In a method according to the present invention, the Ra in step a) of the Ra recycling is provided in HCl or HNO₃, in particular, HNO₃ within a concentration range of 0.1 M to 4 M or HCl within a concentration range of 0.1 to 4 M and/or in step h) HNO₃ or HCl is used as said mobile phase in a concentration range of 0.1 M to 4 M, in particular 1 M.

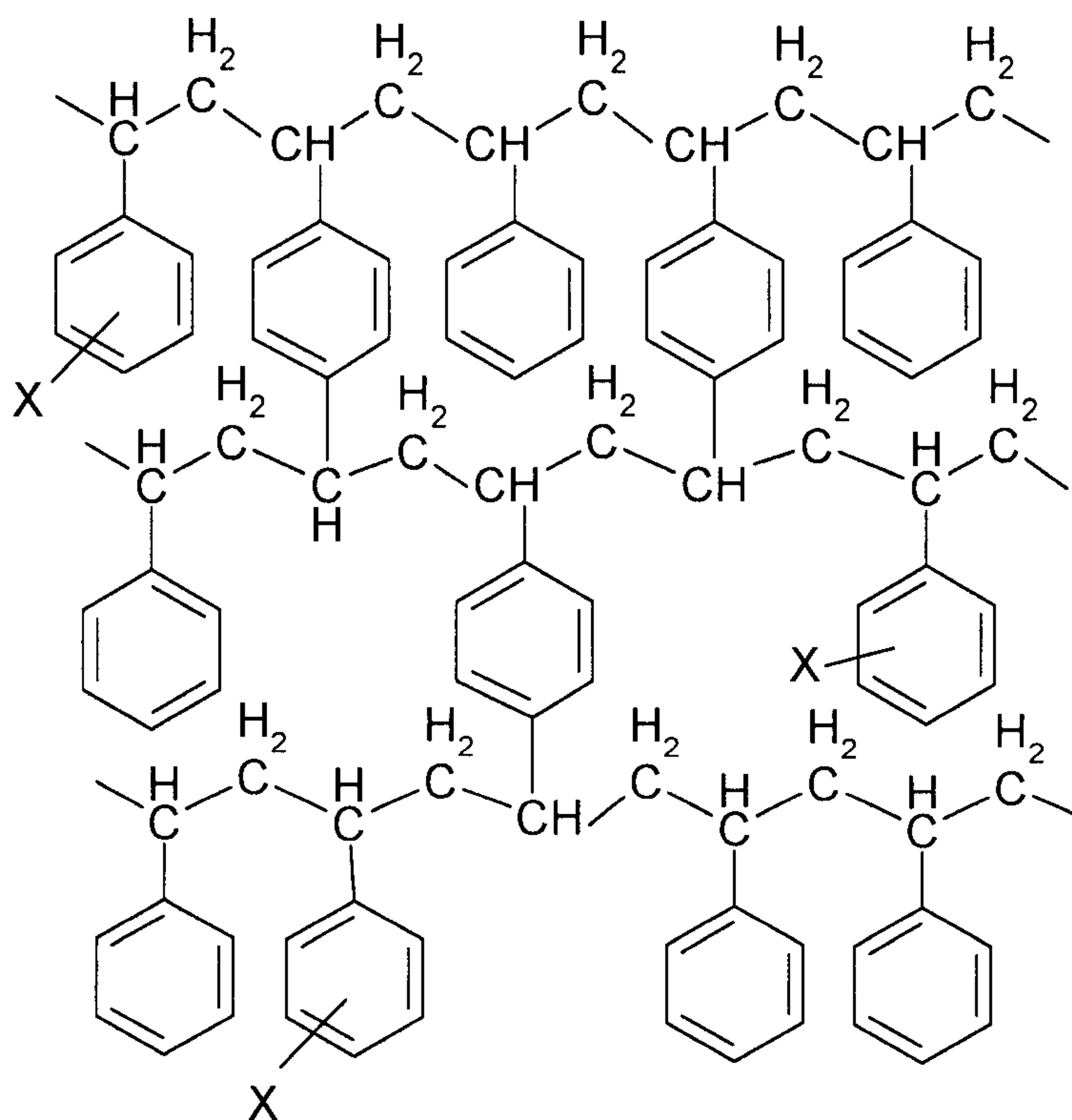
In a preferred method according to the invention, the main chemical contaminants are selected from the group consisting of Ag, Al, As, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, Li, Mg, Mn, Na, Ni, Pb, Sr, V, Zn, as well as mixtures thereof.

It is advantageous to carry out the concentration steps by evaporation, in particular by means of a rotary evaporator and/or by means of a spiral-line heater or silicon heater.

In a preferred method of the present invention the decay product ^{222}Rn is removed from the ^{226}Ra material, in particular during an evaporation step using activated carbon traps.

To elute the Ra from the used cation exchange resin, a high molar mineral acid, with a concentration range of 2 to 10 M, in particular, 3 to 8 M, preferably about 4 M, and as preferred mineral acid, HNO_3 is used.

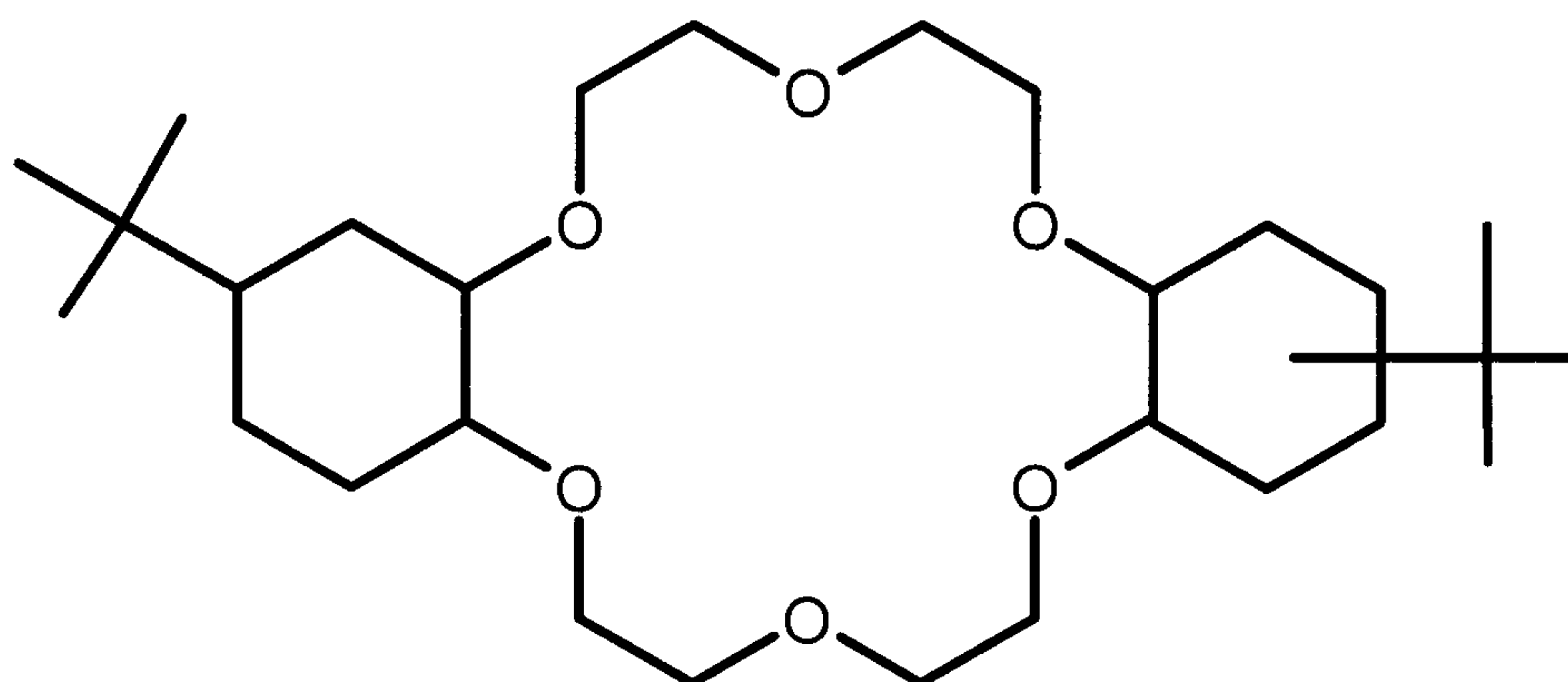
A suitable cation exchange material is based on a cation exchanger being an acidic cation exchange resin in accordance with the following formula, and preferably an acidic macroporous type cation exchanger



wherein in the above Formula : X is SO_3H^+ .

In practice, for the cation exchange step it is preferred to use a commercially available resin such as "AG-MP50" resin from Bio-Rad Laboratories, Inc.

After the cation exchange step, it is a preferred embodiment of the present invention concerning the Ra recycling to use an extractant system in form of a crown ether in accordance with formula III, for the further purification:



Formula III

in 1-octanol.

Using this system, it is a preferred embodiment of the present invention to use as extractant system 4,4'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol or 4,5'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.

It is further preferred that the solid support in feature h) is selected from the group consisting of, porous silica, inert organic polymers, preferably an acrylic ester non-ionic polymer.

For the irradiation of radium compounds completely capsulated in a metallic target cup sufficient amounts of radium have to be available with adequate quality. The procedure regarding the target preparation per se is already known by WO 2005/105160, WO 2005/039647, EP1673492. To cover the needs of radium, two sources of radium were used: from existing (available) radioactive sources and from recycling after irradiation of radium at the cyclotron and its separation from actinium.

The procedure of the present invention describes a method aiming to prepare/purify radium either from existing radioactive sources or from irradiated recycled radium. The purified radium has to correspond to the quality which allows its subsequent irradiation.

The radiochemical procedures which is proposed for the present application comprises the following:

- i. Preparation of ^{226}Ra from existing radioactive sources for target preparation;
- ii. Separation of the irradiated radium from the target support material (aluminium) and from most of the activation products by cation exchange chromatography;
- iii. Purification of Ra from other impurities which can interfere with the quality of the final product ^{225}Ac : like Ba or Sr, using extraction chromatography;
- iv. Quality control of the prepared/purified Ra fraction.

The invention refers to a procedure for the purification of ^{226}Ra in order to prepare radium targets for cyclotron irradiation. It comprises the following steps:

-Purification/recycling of Ra-226

- from available radioactive sources
- from irradiated radium targets;

- Implementation of the separation/purification procedure for high activity samples.

This is assuming the (almost) complete automation of the radiochemical process to minimize the manual handling of highly radiotoxic radium;

- Quality control of the prepared/purified radium.

The purification of the radium has to be done in a way which allows obtaining good recovery and high decontamination factors for the main contaminants. The purification procedure has to cover the separation of Ra from the aluminium as target support material, from the main contaminants resulting from activation and from contaminants which can influence the quality of the actinium (like Ba or Sr).

Further advantages and features are given by describing examples as well as the accompanying drawings.

Fig. 1. shows a general scheme of the production of ^{225}Ac via $^{226}\text{Ra}(p,2n)$ ^{225}Ac reaction;

Fig. 2. shows a preparation/purification scheme for ^{226}Ra from available radioactive sources in accordance with the invention;

Fig. 3. shows an elution profile of Ra and Ba on an Sr resin column from 1 M HNO_3 , 3.5x0.8cm, BV ~ 2 mL

Fig. 4. shows the recycling of radium from irradiated radium targets in schematic view;

Fig. 5. shows gamma spectra of the irradiated radium fraction before recycling; and

Fig. 6. shows gamma spectra of the irradiated radium fraction after recycling according to the invention

The general scheme of the production of actinium via $^{226}\text{Ra}(p,2n)^{225}\text{Ac}$ reaction is shown in Fig. 1.

A flow chart of the separation of Ra from the main activation products is presented in Fig 2.

For the purpose of producing ^{225}Ac via p,2n reaction with accelerated protons, the radium as target material has to correspond to very high purity; otherwise the amount of the obtained activation products among the produced actinium will increase dramatically after irradiation. Therefore, one of the primary goals in the present invention is to provide radium as pure as possible for radium targets preparation in order to minimize the quantity of possible contaminants/impurities.

To obtain radium with very high purity level there are two possibilities which will be illustrated in the Examples below:

Examples

A. Procedure for the preparation of ^{226}Ra from available radioactive sources

The general scheme of the radium preparation procedure from available radioactive sources in accordance to the present invention is shown in Fig. 2.

The commercially available radium sources at Curie or milliCurie level have various degrees of chemical and radionuclidic purity. The better the purity of the initial material is, the simpler the preparation/purification procedure. The quality management (QM) consists in an initial check of the radium purity and activity. Therefore, after the receipt of the radioactive material, a first quality control (QC) measurement is made, based on gamma spectrometry which allows an estimate of the total activity of radium and the main radionuclidic impurities. Working with mCi or higher levels of Ra the fastest way to check the activity given in the specification is by in-situ gamma-spectrometric measurements.

After the estimation of the activities of ^{226}Ra and the main radioisotopic impurities- if any - the samples are opened in a hermetically closed shielded glove-box. As for many of the radioactive sources, one of the common approaches to transport/store them is in dry form in closed glass ampoules. The radium sources closed in glass ampoules are opened and the radioactive material is leached out quantitatively from such ampoules. The opening of the ampoules is done using two different approaches: by crashing the ampoules or by

cutting and pouring out the dry radioactive material in order to leach the dried radium salt with diluted HNO_3 (GDCh conf: Kabai et al., 2005). Similar approaches were applied for analysis of I-129 or Tc-99 by Kabai et al. (2003) and for determination of Lu-177 impurities by Pawlak et al (2004) aiming to open ampoules with radioactive materials and wash out the radioactive component.

After the radium is leached out from an ampoule and dissolved in a minimum volume of 0.1 M HNO_3 , it is concentrated by evaporation in a rotary-evaporator and converted to the nitrate form. For closed radium sources the formed ^{222}Rn is in equilibrium with the mother nuclide ^{226}Ra . The presence of radon along with radium has to be avoided as much as possible because it is the main contributor to the effective dose which has to be minimized. Therefore, the evaporation step is also used for removing the formed radon.

Hereby, the evaporation of the radium is carried out in a safe closed system. Before release, the evacuated air is passed through two consecutive charcoal traps in order to retain the radon inside the glove-box, minimizing the amount of radon released.

In order to control the chemical purity of the radium, a small aliquot is taken from the solution sent to the rotary-evaporator.

This aliquot is diluted further and a quality control sample is analysed by spectrometric methods. The Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES) method was found to be suitable for this analysis having enough sensitivity for all the chemical contaminants expected in the radium solution.

The sample is concentrated close to dryness and it is re-dissolved in a few millilitres of 0.1 M HNO_3 . Then the solution is transferred to a V-vial by using high purity argon.. The last step it is repeated two-three times in order to wash out all the radium from the flask of the rotary-evaporator. The shielded V-vial containing the radium solution is evaporated to dryness using a spiral-line heater or a silicon heater. The V-Vial is closed with a phenolic cap, placed in a lead container and the activity of radium is estimated based on the second in-situ gamma-measurement. The so quantified radium in the thick wall V-vial is used for cyclotron target preparation or else sent to storage.

For the target preparation the V-Vial with the desired activity is opened again, and the radium salt dissolved in 0.1 M HNO_3 .

After complete homogenisation the solution is transferred to a dispenser. The dosage of the radium solution for target preparation is controlled through the dispenser. The V-vial is

washed two times with a few mL of 0.1 M HNO_3 in order to minimize the losses on the wall of the vial.

Table 2 as mentioned before, shows the typical ratios of impurities to radium obtained from radium ampoules. The main inactive impurities are Na, Ca, Ba and Zn while the radioisotopic purity is very high, usually more than 99 %. Only different activities of radium daughters could be measured in the gamma-spectra, depending on the time elapsed since the last radon evacuation.

If the radium had worse quality parameters, one-step purification would be applied based on Sr resin aiming to remove especially the barium present near the radium. In this case the radium is loaded in 1 M HNO_3 on a small Sr resin column (bedvolume- BV~ 2 mL) before complete drying in V-Vial. The radium is collected in BV 1- 4 then the barium has higher retention times and it occurs in the BV 5-10. The Sr will be retained on the column.

The elution profile of Ra and Ba on Sr resin column from 1 M HNO_3 , 3.5x0.8 cm, BV ~ 2 mL is shown in Fig. 3.

This purification step was successfully applied for radium amounts up to levels of several hundred micrograms.

B. Procedure for recycling of ^{226}Ra from irradiated radium targets

Another possibility to obtain pure radium is from recycling the radium, already being irradiated with accelerated protons for ^{225}Ac production. This approach is more complicated than the previous due to the fact that the irradiated radium has a much lower grade of purity than the original material. The general scheme of the applied radium recycling procedure is represented in Fig 4.

The procedure as developed is based on the chemical and radioisotopic composition of the radium fraction after the separation from actinium. The main chemical and radioisotopic contaminants present in the radium fraction after irradiation and separation from actinium - in particular in accordance with German patent application, DE 10 2006 008 023 A1, published on August 30, 2007 - are summarised in the Table 3 which shows the ratios of the corresponding element to the radium.

Table 3

Main chemical contaminants typically present in the irradiated radium fraction after the separation from actinium before recycling (mass ratios relative to the radium)

Element	mg Contam/mg Ra	Element	mg Contam/mg Ra
Ag	0.06	K	3.01
Al	172.2	Li	0.02
As	0.15	Mg	7.69
Ba	0.81	Mn	1.16
Be	0.06	Na	3.27
Bi	0.13	Ni	3.20
Ca	0.94	Pb	-
Cd	0.04	Rb	-
Co	0.42	Se	-
Cr	0.15	Sr	0.09
Cu	0.57	Tl	-
Fe	0.80	U	-
Ga	-	V	-
In	-	Zn	1.79

5

Starting from this composition and from the radioisotopic impurities present in the radium fraction, the objective of the present invention regarding the recycling is to provide a combined procedure based on a multi-step purification scheme which allows the separation of the radium from the contaminants according to Table 3. The proposed procedure is based upon a cation exchange combined with extraction chromatography.

10

In the present application, the final form of the radium used for target preparation is preferably an acidic solution in HNO_3 , free from any complexing agent. Thus, the proposed purification step based on cation exchange omits any use of such complexing agents.

15

In this procedure, after the separation of produced ^{225}Ac from irradiated radium, the radium fraction in 2 M HNO_3 is evaporated in order to concentrate it. Then the concentrated radium solution, which might contain some organic contaminants, is passed through a prefilter column (an inert solid support material) to remove trace amount of organic compounds. The cation exchange step included immediately after the prefilter column allows the separation of the radium from the main chemical contaminants like aluminium as target support material, Mg, Co, Ni, Zn and Fe. For this the original solution is first converted to 0.1 M HCl . Then the solution is passed through the Biorad™ AG-MP50 cation exchange resin. The resin is an acidic macroporous type cation exchange resin with high effective surface, approx 35 % porosity and a nominal capacity of 1.5 meq/mL. Therefore, it has higher

20

retention properties than a normal cation exchange resin. Thanks to these properties, the radium up to several mCi-s could be easily retained on 5-6 mL bed volume column from 0.1 M HCl media. Afterwards, the column is intensively washed with HCl having different molarities in order to elute any possible contaminant retained on the column. Finally, the strongly retained radium is eluted with approximately 150 mL 4 M HNO₃ solution.

The results show that under these experimental conditions the recovery of the radium is higher than 90 %. The obtained decontamination factors for Al are 10³, for transitional metals 10². In order to increase the decontamination factors of the contaminants relative to the radium a second column identical with the previous is introduced in the procedure. In this way it was possible to obtain high decontamination factors for all the transition metals. After the radium is eluted from the second column in 4 M HNO₃, it is evaporated until wet residues and is re-dissolved in 1 M HNO₃. Next, the radium in 1 M HNO₃ is used as feeding solution for an extraction chromatographic column filled with Sr resin (EICHROM). This resin allows the separation of the radium from barium and trace amount of strontium still present in the radium fraction.

The Ba is chemically similar to the radium. Therefore, it is very difficult to separate it on a cation exchange resin. The extraction chromatography gave the inventors the opportunity to separate radium from the barium usually present near the radium in the samples and to separate any strontium detected among radium. The separation on Sr resin was conducted with radium-barium mixtures up to several hundred micrograms.

The obtained chemical composition after the recycling process using two cation exchange columns and one Sr resin column is shown in Table 4. Based on these results can be concluded that the chemical purity of the radium was substantially improved during the multi-step procedure and it is comparable with that of the original, not irradiated radium.

Table 4

Main chemical contaminants typically present in the irradiated radium fraction after the separation from actinium and recycling (mass ratios relative to the radium)

Element	Imp/Ra [mg/mg]	Element	Imp/Ra [mg/mg]
Ag	0.06	K	-
Al	0.15	Li	-
As	-	Mg	0.03
Ba	0.04	Mn	0.01
Be	0.02	Na	4.43
Bi	-	Ni	0.03
Ca	0.63	Pb	-
Cd	0.02	Rb	-
Co	0.01	Se	-
Cr	0.04	Sr	0.02
Cu	0.03	Tl	-
Fe	0.06	U	-
Ga	-	V	-
In	-	Zn	0.06

5

It is evident that including more steps in the process, the quality of the radium can be further improved, but in the same time the recovery of the radium will decrease. To avoid this fact the presented radiochemical procedure will be tested for the separation of several milligrams of radium.

10

C. Implementation of the separation/purification procedure for high activity samples

To obtain the required amount of ^{225}Ac , hundreds of milligrams of radium have to be involved in the process. Working with the highly radiotoxic radium at hundred milligrams level is possible only with careful planning of the radiochemical processes. In order to minimize the exposure of the personnel, all the involved radiochemical processes has to be automated.

15

The automation of the radiochemical processes is realised taking into account the above described schemes and details.

20

The implementation of the automation process is done based on the intensive collaboration of the Institute of Radiochemistry with the Institute for Machine Tools and

Industrial Management (*iwb*), both of the Technical University of Munich. In this respect, a continuous work is put into the automation plans of the radium preparation and recycling, respectively.

5 **D. Quality control (QC) of the purified/recycled radium**

The quality management of the product - actinium but also of the raw material, in this case of the radium is very important. The quality of the starting material will influence not only the quality and the yield of produced actinium but will define the radiochemical procedure applied for the recycling of the irradiated radium. Therefore, additional effort was
10 put in the quality control (QC) of the used radium as starting material but also during the purification/recycling process. QC was used at the beginning of the process to extend the characterization/prove the quality of the radium sources given in the official specification. Later on the quality control was done in order to verify the process efficiency.

In the QC the main aspects covered:

- 15 - the purity: including the chemical and radioisotopic purity, and
- the recovery of the purified/recycled radium.

The first aspect was conducted in order to assure that the purity of the radium is high enough to be safely irradiated by accelerated protons, and assure that the presence of different contaminants/impurities will not set back the yield of the irradiation and the post
20 irradiation treatments, respectively. Towards the purity check the radionuclidic and chemical purity analysis were performed.

From the point of view of the technique the radionuclidic purity of the radium from available radioactive sources was done by in-situ gamma-spectrometric measurements of the whole sample or by taking a small aliquot of the sample. For the identification of the main
25 chemical contaminants/impurities the same aliquot was analysed using Inductively Coupled Plasma - Optical Emission Spectrometry (ICP-OES). This method was used successfully to identify the chemical impurities expected in the radium fraction.

The second aspect - the recovery of the radium - is as much important as the first one. Due to the application of the multi-step radiochemical procedure, it is unavoidable to
30 lose radium during the process. In order to minimize the losses, the applied procedures should be as simple as possible, comprising the minimum number of steps necessary to achieve the purity requirements. The recovery of the radium was verified during the process by gamma-spectrometry.

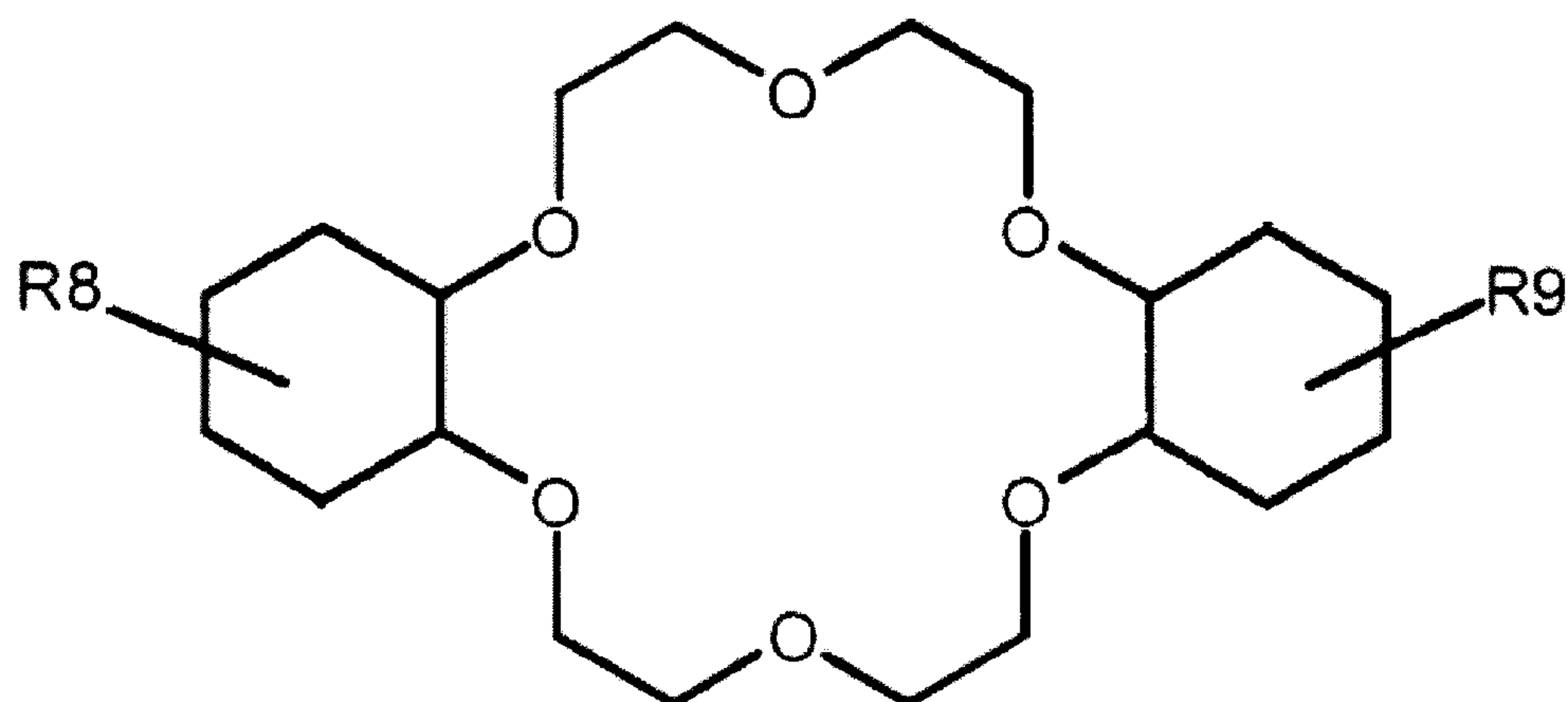
Fig. 5 and 6 show the typical gamma-spectra of the radium fraction before and after recycling. From the spectra could be observed that the originally present radioisotopes of the transitional metals: ^{55}Co , ^{56}Co , ^{57}Co , ^{67}Ga , ^{57}Ni , ^{51}Cr , ^{48}V , ^{52}Mn , ^{54}Mn , and ^{65}Zn were well separated after applying the above detailed radiochemical procedure. Other detected isotopes in the spectra of Fig. 5, such as ^{208}Tl , ^{212}Pb and ^{221}Fr are shortlived (half lifes from minutes to hours) isotopes which are not relevant for the further purification. The typical radioisotopic purity of the radium obtained by using the above described procedure was higher than 99 %.

In the spectra of Figs. 5 and 6 "Ann. Rad." means "annihilation radiation".

CLAIMS:

1. A method for recycling of ^{226}Ra (Ra), for target preparation for ^{225}Ac Actinium production from radium sources irradiated with accelerated protons (p,2n), after separation of the produced ^{225}Ac , comprising the following steps:

- a) determining the quality of a Ra-containing solution to be purified being provided in a mineral acid solution;
- b) concentrating the Ra-containing solution by evaporation;
- c) removing trace amounts of organic compounds by means of a prefilter column wherein said prefilter column is an inert solid support material;
- d) separating Ra from the main chemical contaminants, by performing at least one cation exchange chromatography using an acidic macroporous cation exchange resin;
- e) washing the acidic macroporous cation exchange resin with low molar mineral acid to remove chemical contaminants;
- f) eluting Ra from the acidic macroporous cation exchange resin with high molar mineral acid to generate partially purified Ra fractions;
- g) pooling and concentrating the partially purified Ra fractions; and
- h) subjecting the partially purified Ra-containing fractions to at least one extraction chromatography, wherein said extraction chromatography step is carried out on a solid support material having an extractant system coated thereon, comprising at least one compound in accordance with general formula I in at least one compound in accordance with general formula II,



Formula I



Formula II

wherein in formula I:

R8 and R9 independently is H, C₁ – C₆ alkyl, or t-butyl; and

wherein in formula II:

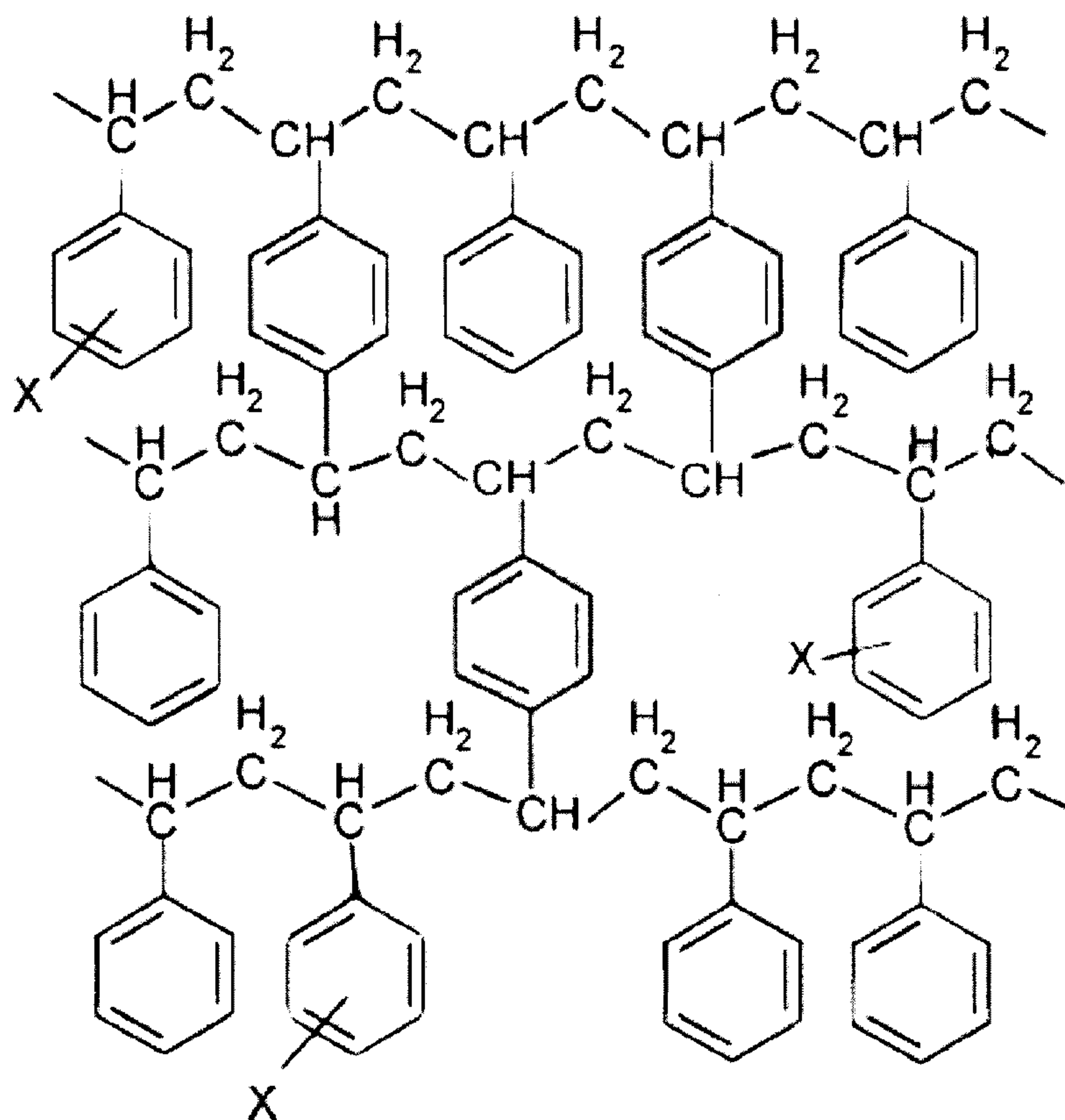
R10 is C₄ to C₁₂ alkyl; and wherein HNO₃ or HCl is used as a mobile phase,

- i) recovering Ra from early fractions, whereas Ba and Sr are contained in fractions with higher retention time;
- j) pooling Ra fractions; and
- k) concentrating the purified Ra fractions.

2. The method according to claim 1, wherein the Ra-containing solution in step (a) comprises HCl or HNO₃.

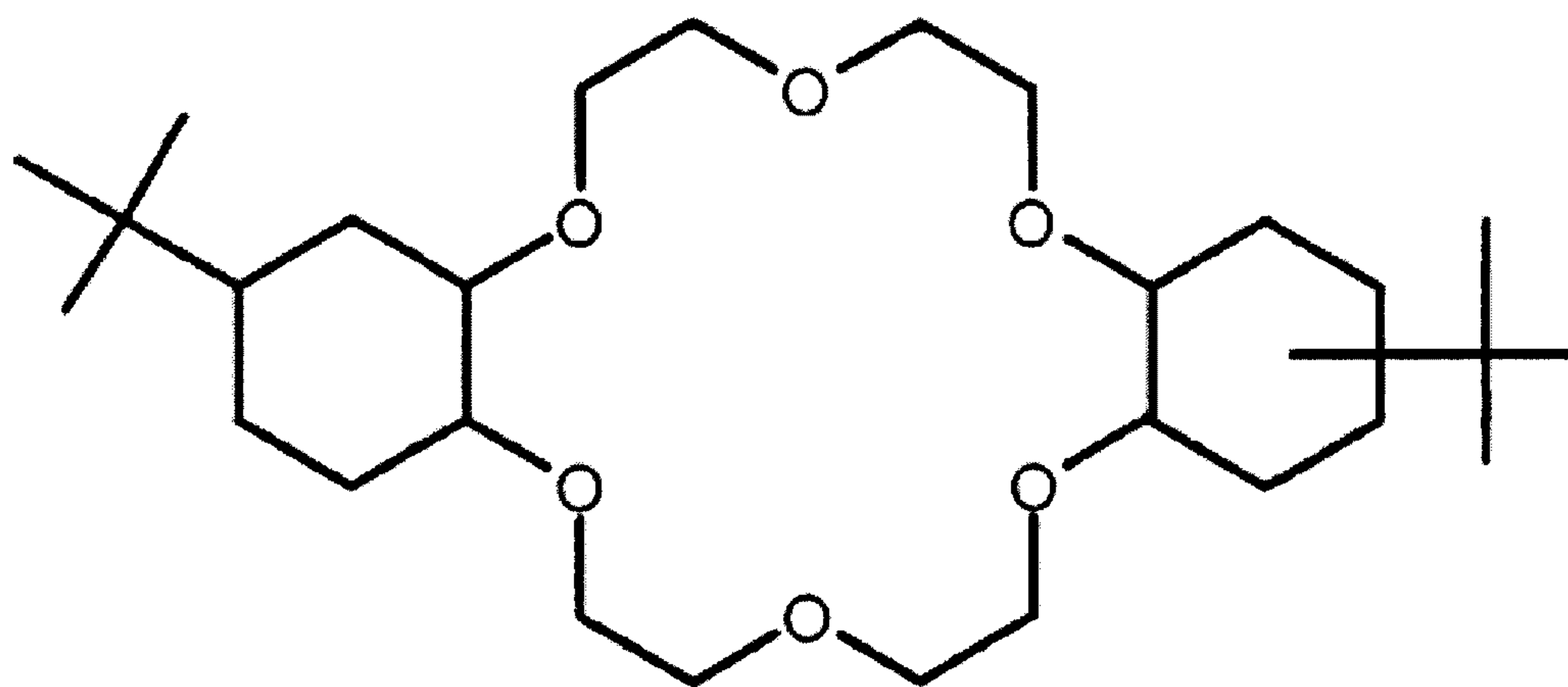
3. The method according to claim 1 or 2, wherein the HNO_3 is within a concentration range of 0.5 M to 4 M.
4. The method according to any one of claims 1 to 3, wherein the HCl is within a concentration range of 0.5 M to 4 M.
5. The method according to any one of claims 1 to 4, wherein HNO_3 or HCl is used as the mobile phase and has a concentration range of 0.1 M to 4 M.
6. The method according to claim 5, wherein HNO_3 or HCl is used as the mobile phase and has a concentration of about 1 M.
7. The method according to any one of claims 1 to 6, wherein the main chemical contaminants are selected from the group consisting of Ag, Al, As, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, Li, Mg, Mn, Na, Ni, Pb, Sr, V, and Zn, or mixtures thereof.
8. The method according to any one of claims 1 to 7, wherein the concentration steps are carried out by evaporation.
9. The method according to any one of claims 1 to 8, wherein ^{222}Rn decay products are removed from the Ra material, using one or more activated carbon traps.
10. The method according to any one of claims 1 to 9, wherein the concentration of the high molar mineral acid is 0.5 to 10 M.
11. The method according to claim 10, wherein the concentration of the high molar mineral acid is 1 to 8 M.
12. The method according to claim 11, wherein the concentration of the high molar mineral acid is 2 to 6 M.
13. The method according to claim 12, wherein the concentration of the high molar mineral acid is about 4 M.

14. The method according to any one of claims 1 to 13, wherein the high molar mineral acid is HNO_3 .
15. The method according to any one of claims 1 to 14, wherein the cation exchanger is an acidic cation exchange resin in accordance with the following formula:



wherein X is SO_3H^+ .

16. The method according to any one of claims 1 to 15 wherein the extractant system is a crown ether in accordance with formula III:



Formula III

in 1-octanol.

17. The method according to claim 16, wherein the extractant system is 4,4'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.
18. The method according to claim 16, wherein the extractant system is 4,5'-bis(t-butylcyclohexano)-18-crown-6 in 1-octanol.
19. The method according to any one of claims 1 to 18, wherein the solid support material in feature h) of claim 1 is selected from the group consisting of porous silica and inert organic polymers.
20. The method according to claim 19, wherein the inert organic polymer is an acrylic ester non-ionic polymer.

Fig. 1

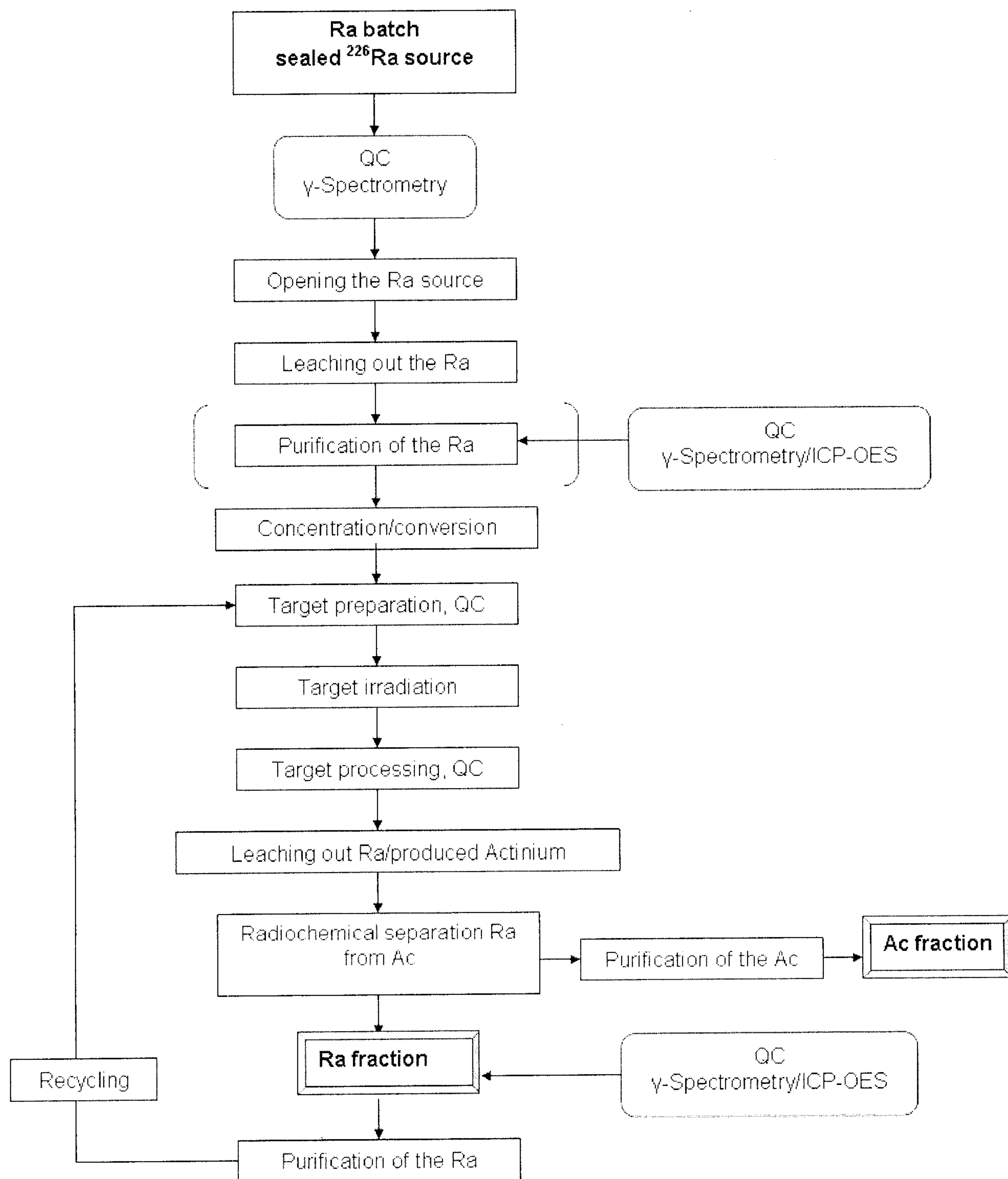


Fig. 2

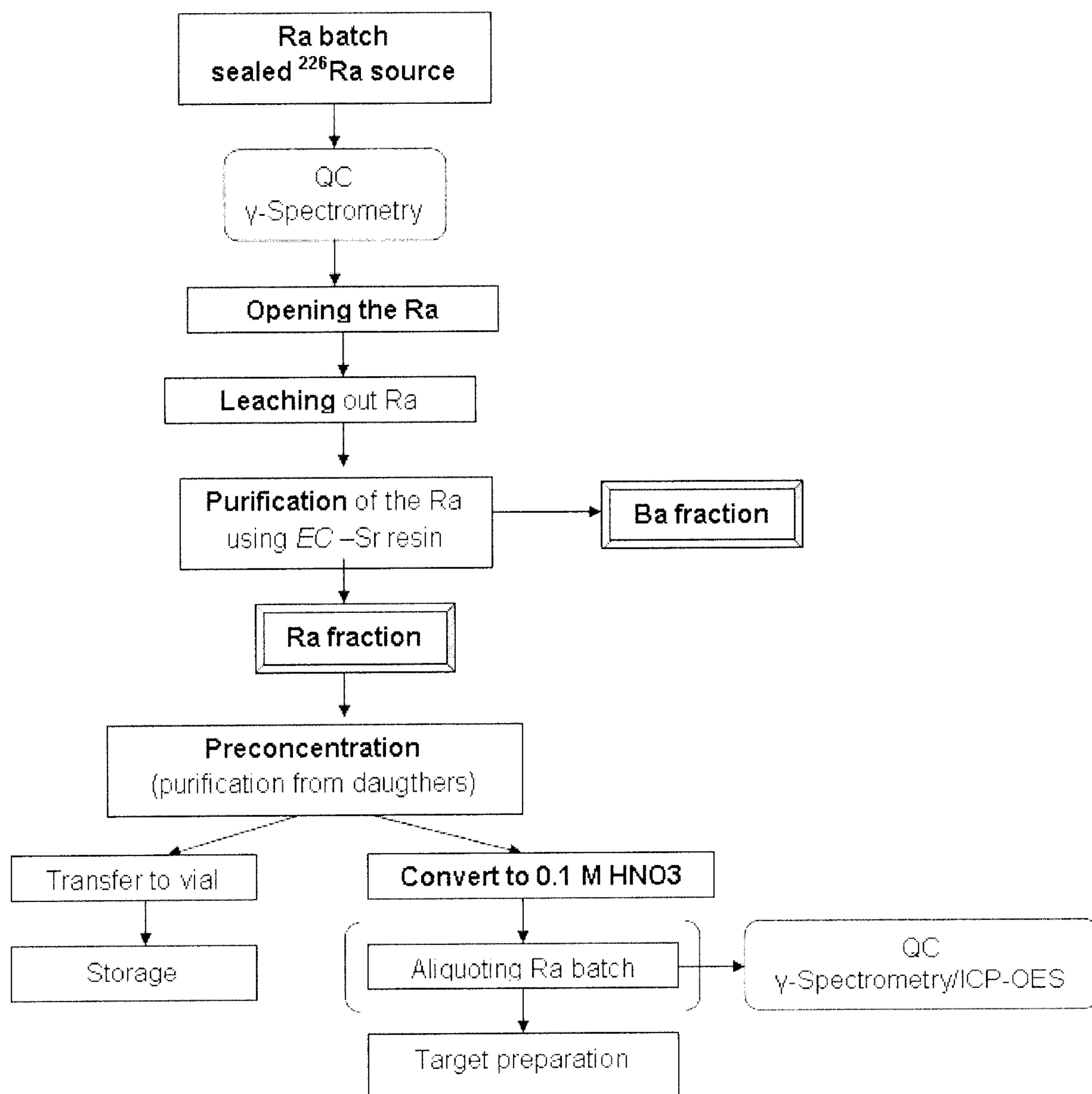


Fig. 3

Elution profile of Ra and Ba on Sr resin column

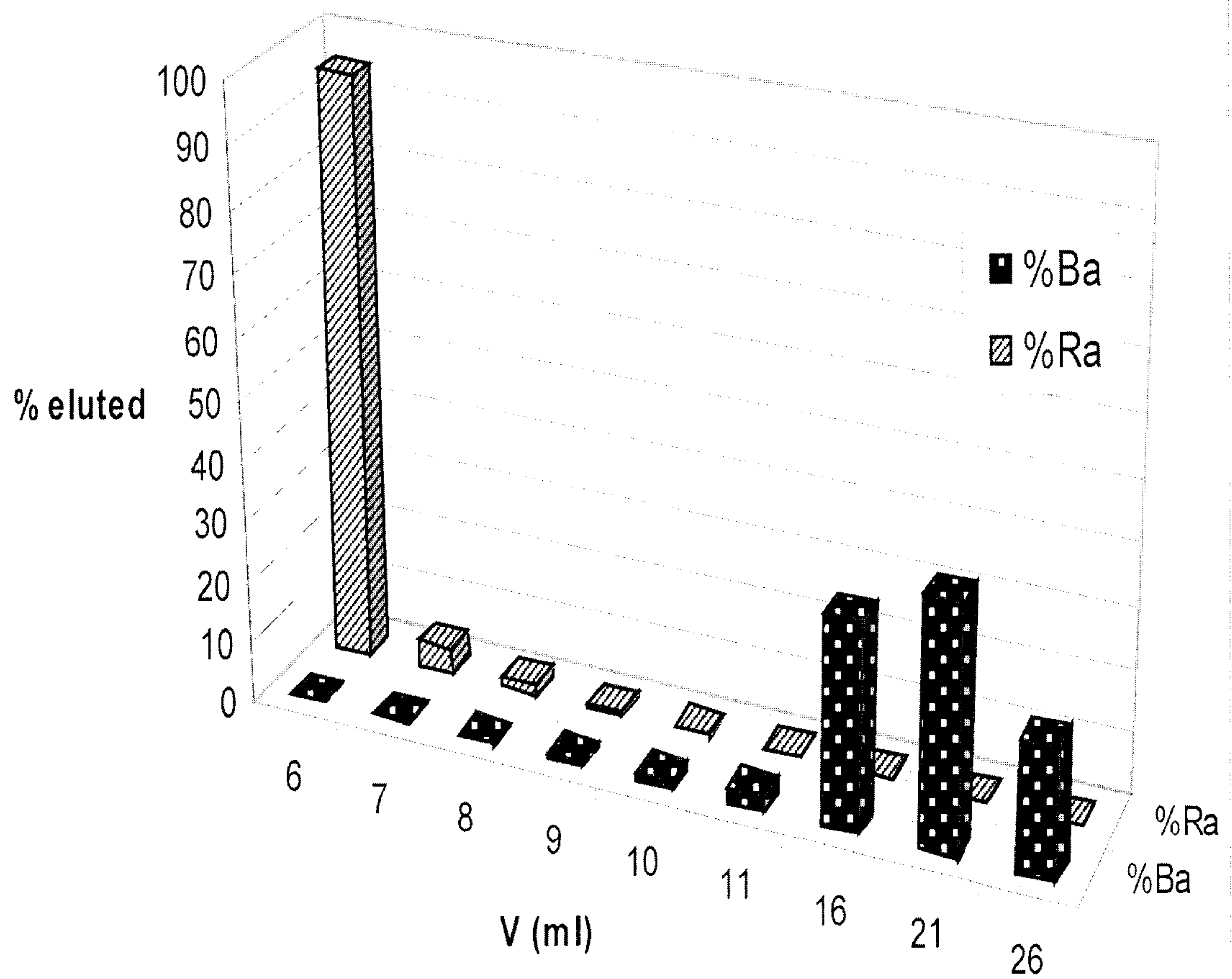


Fig. 4

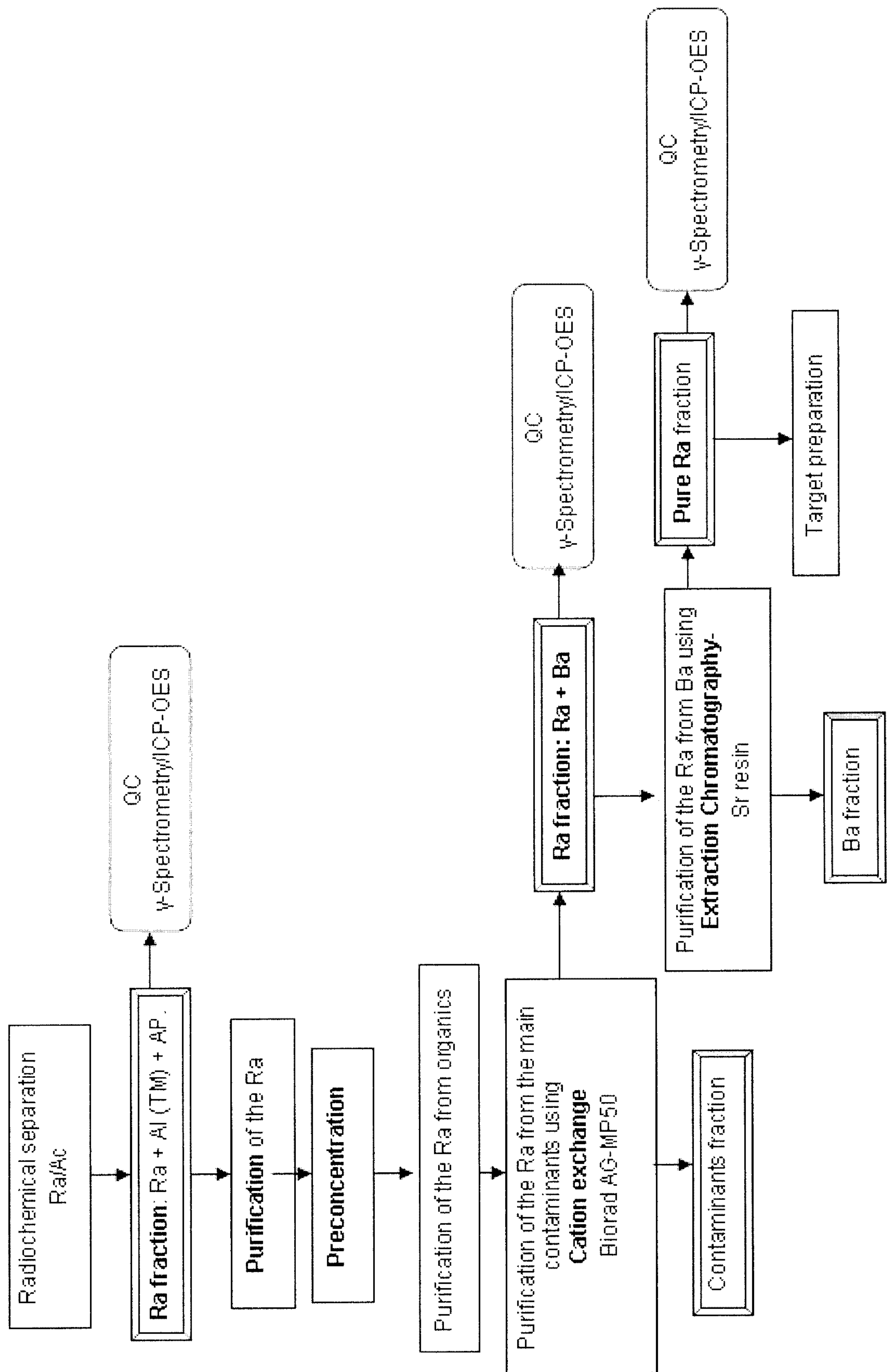


Fig. 5

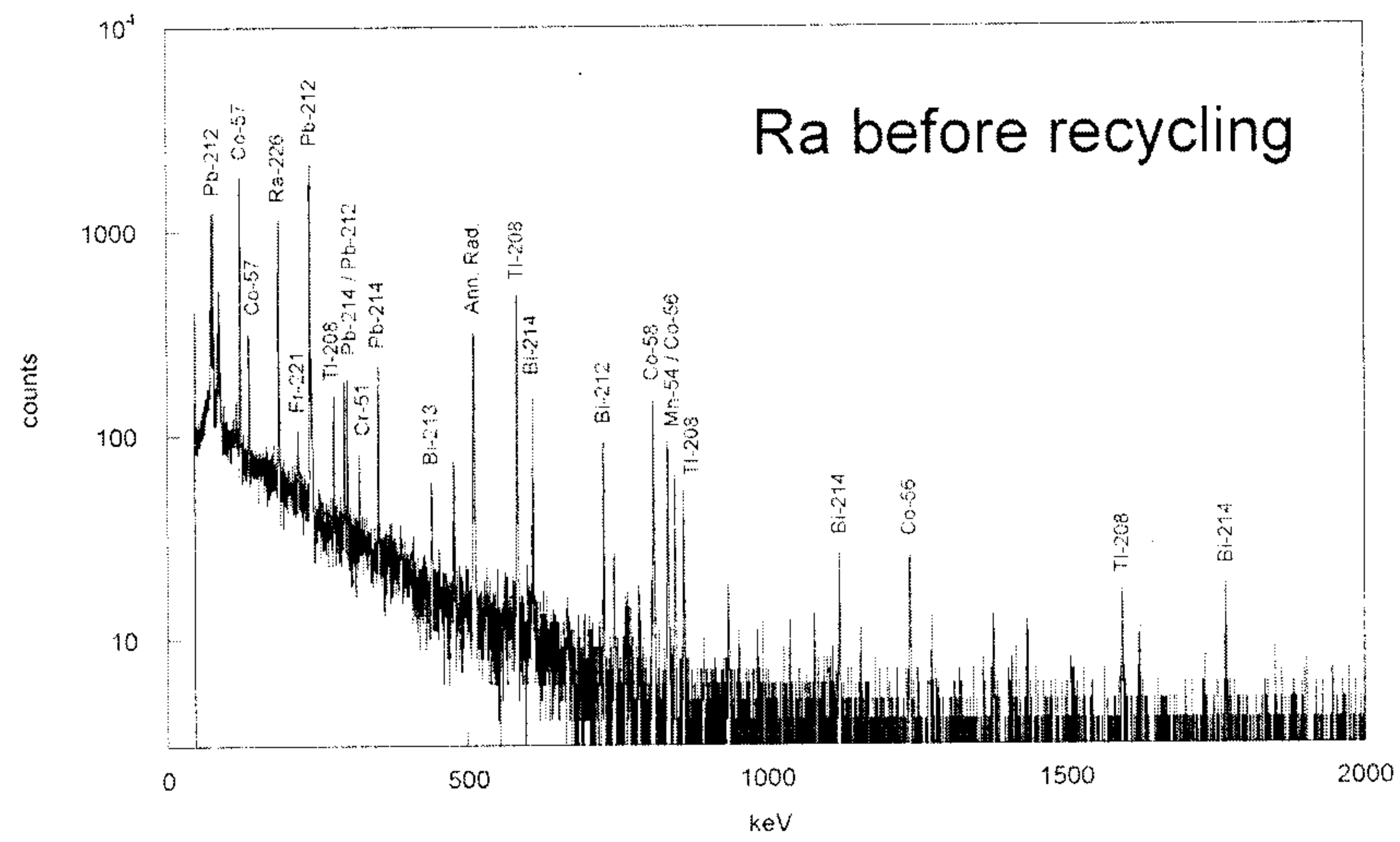


Fig. 6

