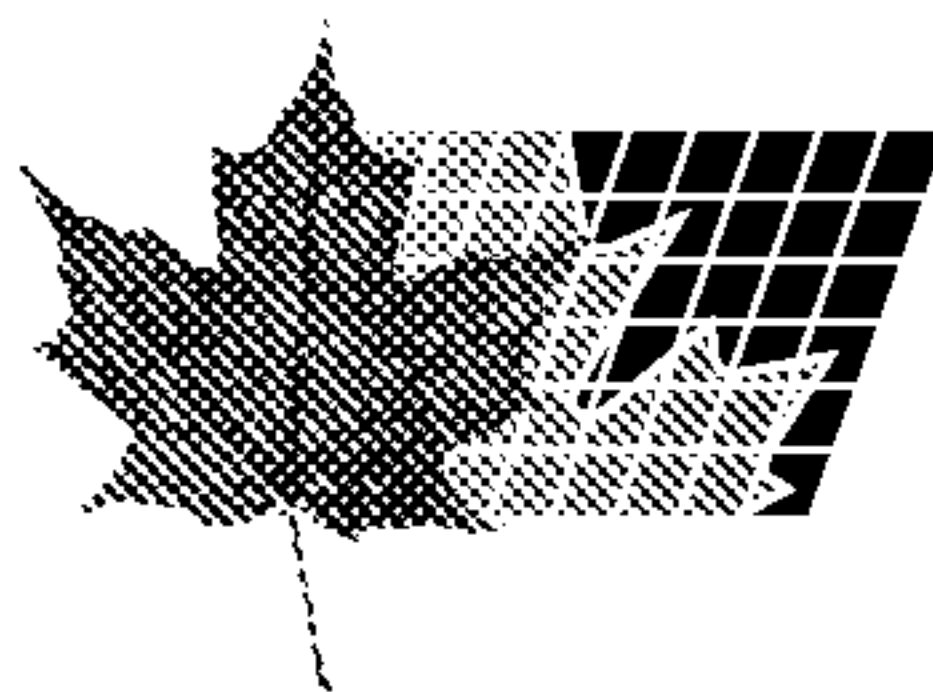




(11) (21) (C) **2,225,504**
(22) 1997/12/22
(43) 1998/06/30
(45) 2000/05/09

(72) PAFFENHOLZ, Josef, US

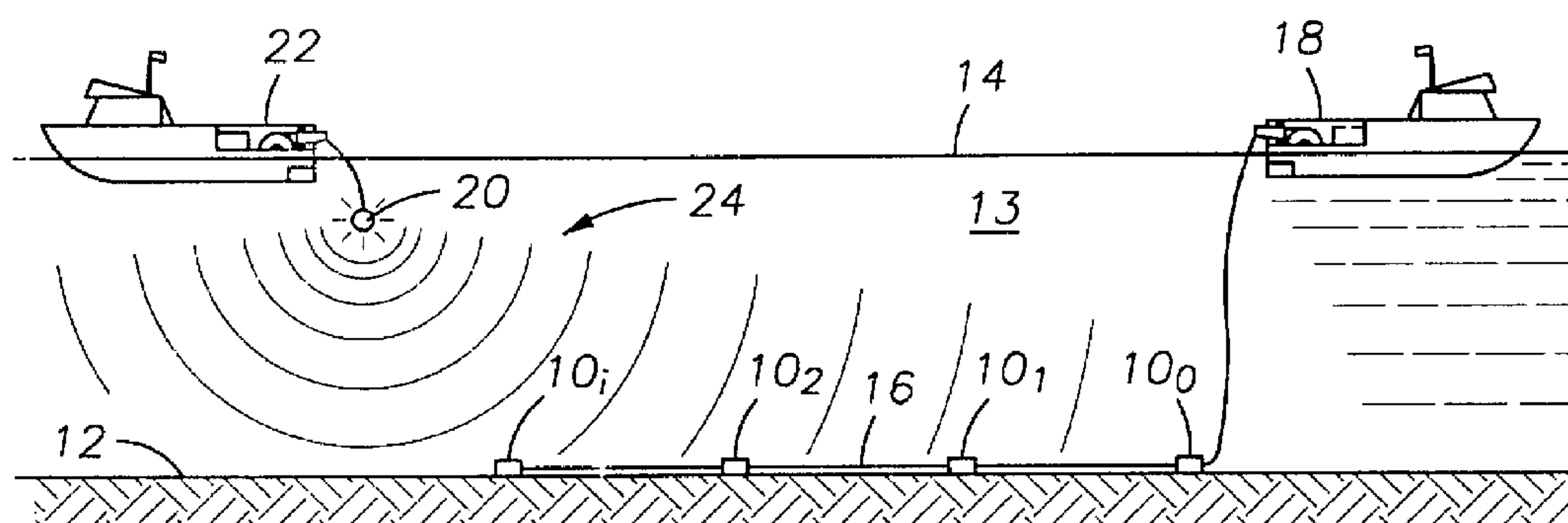
(73) Western Atlas International, Inc., US

(51) Int.Cl.⁶ G01V 1/38

(30) 1996/12/31 (08/777,229) US

(54) **METHODE DE MESURE DE LA REFLECTIVITE DU FOND DE
L'EAU**

(54) **METHOD FOR MEASURING THE WATER BOTTOM
REFLECTIVITY**



(57) Le temps de traversée d'une couche d'eau dans les deux sens, τ , est obtenu à partir de capteurs sismiques bimode en corrélant les transformées de Fourier de la somme et de la différence des signatures de vitesse et de pression. La transformation en Z de τ permet d'évaluer l'une des deux variables de Backus, Z_w . La seconde variable est R_b , le coefficient de réflectivité du fond de l'eau. Les transformées fréquentielles des signatures somme et différence ci-dessus sont multipliées chacune par l'opérateur de Backus $(1 + R_b Z_w)^2$ après l'initialisation de R_b et les produits sont soumis à des corrélations itérées jusqu'à ce que la fonction de corrélation converge vers un minimum. R_b est perturbé après chaque itération. La valeur de convergence de R_b est le coefficient de réflectivité local du fond de l'eau.

(57) The two-way water-layer travel time, τ , is derived from dual-mode seismic sensor data by cross-correlating the Fourier transforms of the sum and difference of the velocity and pressure signatures. The Z-transform of τ evaluates one of the two Backus variables, Z_w . The second variable is R_b , the water bottom reflectivity coefficient. The frequency-domain transforms of the above summed and differenced signatures are each multiplied by the Backus operator $(1 + R_b Z_w)^2$ after initializing R_b and the products are iteratively cross-correlated until the correlation function converges to a minimum. R_b is perturbed after each iteration. The value of R_b upon convergence is the local water bottom reflectivity coefficient.

ABSTRACT

The two-way water-layer travel time, τ , is derived from dual-mode seismic sensor data by cross-correlating the Fourier transforms of the sum and difference of the velocity and pressure signatures. The Z-transform of τ
5 evaluates one of the two Backus variables, Z_w . The second variable is R_b , the water bottom reflectivity coefficient. The frequency-domain transforms of the above summed and differenced signatures are each multiplied by the Backus operator $(1+R_b Z_w)^2$ after initializing R_b and
10 the products are iteratively cross-correlated until the correlation function converges to a minimum. R_b is perturbed after each iteration. The value of R_b upon convergence is the local water bottom reflectivity coefficient.

METHOD FOR MEASURING THE WATER BOTTOM REFLECTIVITY

5 The present invention is a method for measuring the sea-floor reflectivity coefficient from seismic reflection data gleaned from routine dual-sensor seismic data-acquisition operations using an ocean bottom cable.

10 In the art of seismic exploration, numbers of spaced-apart seismic sensors are distributed over a designated area of survey. In deep water, the sensors may be towed through the water in a streamer cable. In shallow water on the order of 150 meters deep or less and in the context of this disclosure, as shown in
15 Figure 1, sensors such as $10_0, 10_1, 10_2, \dots, 10_i$ (where $i+1$ is the number of sensors deployed) may be laid directly on the sea floor 12 beneath a body of water 13. The sensors, 10_i , are mechanically and electrically or optically interconnected by signal communication
20 channels in a bottom cable 16. The cable and its included communication channels are further coupled to data-recording and processing equipment mounted aboard a seismic service ship such as 18, as is well known in the art.

25 A sound source 20, which may be operated from a shooting ship 22, generates an acoustic wavefield 24 in the water at a succession of designated stations over the survey area. The source-station spacing is usually 25 to 50 meters, comparable to the spacing of the

seismic sensors 10_i mounted on or in the bottom cable
16. The wavefield propagates radially in all directions
to insonify sub-bottom earth layers (not shown in Figure
1) whence the wavefield is reflected back towards the
5 sea floor 12 where it is detected by the sensors 10_i .
The sensors convert the mechanical earth motions or
water pressure variations, due to the reflected seismic
wavefield, to amplitude-modulated electrical signals.
The signals are recorded for archival storage and,
10 perhaps, partially processed in ship-borne data-
recording equipment following discretization, all
functions which are well known to the art. The recorded
seismic data are processed to provide a representation
of the topography of selected sub-sea strata using any
15 well known data-processing sequence.

Sensors used in marine seismic exploration are
usually pressure-sensitive hydrophones. For certain
projects, particularly those using ocean-bottom cables,
geophones that are responsive to particle velocity may
20 be used in combination with the hydrophones in the form
of dual-mode sensors.

For purposes of this disclosure, the term *dual-mode*
means sensors such as 26 and 28, Figure 2, which are of
different genera but which are used jointly to register
25 a common seismic wavefield. They may either be mounted
together in a single case, such as 29, or they may be
separate packages that are laid closely next to each
other on the water bottom. In some instances,
accelerometers may be substituted in place of or in
30 combination with the hydrophones. Accelerometers are
responsive to changes in particle velocity with respect
to time.

Reference will be made to seismic signatures. For
purposes of this disclosure, a seismic signature is
35 defined as the variation in phase and amplitude,
expressed in the time domain, of the signal level of a
quantity under consideration such as water pressure or

particle velocity. The unqualified term *velocity* means the velocity of propagation of an acoustic wavefield through a medium of interest. The term *pressure signature* refers to the pressure variation, usually in a fluid, due to the passage of a compressional wavefront. The term *velocity signature* refers to the variation in particle velocity in a medium due to the passage of a wavefront. Seismic signatures are displayed on time-scale traces where the trace excursion or variation in trace density is a measure of signal amplitude.

Seismic signals are usually contaminated by noise which may be random or coherent. Noise is defined as any unwanted signal such as the random noise of a ship's screw, marine-life conversations, wind noise or crashing of waves. Random noise of that type may be reduced by temporal or spatial filtering.

The acoustic wavefields are not only reflected from subsurface earth strata but may also be reflected multiple times between the sea floor and the sea surface such as ray path 30, Figure 2 much like the multiple reflections as seen in the mirrors on opposite walls of a barber shop. Both the sea floor and the sea surface are efficient reflectors having a coefficient of reflection that may approach unity. Reflections from the water surface, also referred to as ghost reflections, may have a very high amplitude and often reside in the same part of the seismic spectrum as desired primary reflections. Multiple reflections of whatever type constitute a severe type of coherent noise that is not necessarily amenable to attenuation by temporal or spatial filtering. Interbed multiples from deep-seated strata, such as 32 of Figure 3, may further complicate matters.

This disclosure is concerned with measuring the ocean bottom reflectivity coefficient for the purpose of attenuating so-called first-order peg-leg multiples. According to R. E. Sheriff's *Encyclopedic Dictionary of*

Exploration Geophysics, 1991 edition, a peg-leg multiple is defined as a multiple reflection involving successive reflection between different interfaces so that its travel path is non-symmetric. Figure 3 shows
 5 various examples of possible multiple trajectories. The first, second and fourth trajectories are representative of first-order peg-leg multiples, involving surface (ghost) reflections, and which are amenable to treatment by the methods of this invention. The third trajectory
 10 represents an inter-bed multiple. The fourth trajectory also illustrates the effect of reverberation where the wavefield is initially trapped within the water layer.

Multiple reflections comprise a coherent noise field which somehow must be removed from seismic data.
 15 Multiple contamination is most troublesome in the presence of relatively flat-lying earth layers. Multiples cannot exist if the bedding planes of the respective strata exhibit significant dip on the order of 15° to 20° or more.

20 US patent 5,365,492, issued November 15, 1994, to William H. Dragoset and assigned to the assignee of this invention, teaches a method for canceling ghost reflections. In that method, a geophone and a hydrophone are co-located so as to see both the pressure
 25 signature and the velocity signature characteristic of a particular seismic transient. The pressure signature is adaptively filtered and subtracted from the velocity signature to isolate a nearly pure noise signature. The noise signature is added back to the velocity signature
 30 with opposite sign to clear away the embedded random noise, leaving a refined velocity signature. The refined velocity signature is scaled and summed with the pressure signature from the hydrophone to cancel the coherent noise of the ghost reflection. The step of
 35 scaling requires an accurate knowledge of the water-bottom reflectivity, a quantity that is merely estimated in that reference.

A similar method is taught by W. H. Rhuele in US patent 4,486,865 who reduces the ghost effect using dual-mode sensors. The output of one of the pair of sensors is gain-adjusted and filtered using a
5 deconvolution operator having a preselected amount of white noise added to the zero lag of the autocorrelation function. The deconvolved gain-adjusted signal is added to the signal output from the other sensor to cancel the ghost.

10 Patent 5,396,472, issued March 7, 1995 to Josef Paffenholz and assigned to the assignee of this invention, teaches a dual-sensor method for determining the water-bottom reflectivity coefficient for use in abating seismic signal contamination from first-order
15 peg-leg multiples. The method involves summing the pressure and velocity signals to determine only up-going energy. The up-going energy is transformed to the frequency domain and multiplied by an inverse Backus operator $(1+RZ)^2$. For a selected frequency, the total
20 energy is minimized for incremental values of the water-bottom reflectivity coefficient, R , using an iterative optimization computer routine assuming a water depth Z .

It is the intent of this disclosure to provide a convenient method for determining the water bottom
25 reflection coefficient and the water depth using the data derived from dual sensors.

This is a method for measuring the reflectivity coefficient, R_b , of an earth layer that defines the bottom of a water layer. The method uses routine
30 seismic data from each of a plurality of seismic sensor stations. Each sensor station is equipped with a dual-mode seismic sensor for detecting velocity and pressure signatures which are formatted in the time-space domain. The velocity and pressure signatures are resolved into
35 up-going and down-going wavetrains. The up-going and down-going wavetrains are transformed to the frequency/wave-number domain and iteratively cross

correlated. The time lag that maximizes the cross-correlation function is selected as the two-way wavefield travel time through the water layer and is entered as a component of the Z_w argument of a Backus operator $(1+R_b Z_w)^2$. The R_b component is initialized with a value embraced by the inequality $-1 < R_b < +1$. The initialized Backus operator is multiplied by the respective up-going and down-going transforms, whereupon the products are iteratively cross-correlated, discretely perturbing R_b after each iteration. The final value for R_b , upon convergence to a minimum, is the reflectivity coefficient at the selected sensor station.

The novel features which are believed to be characteristic of the invention, both as to organization and methods of operation, together with the objects and advantages thereof, will be better understood from the following detailed description and the drawings wherein the invention is illustrated by way of example for the purpose of illustration and description only and are not intended as a definition of the limits of the invention:

FIGURE 1 is a schematic view of the manner of deployment of ocean bottom cables and dual mode sensors;

FIGURE 2 shows the trajectories of a ghost reflection and a primary reflection with respect to a dual mode sensor;

FIGURE 3 illustrates several different first-order peg-leg multiple trajectories.

Figures 1-3 were discussed earlier but occasional reference hereinafter may be made thereto.

The theory of multiple reflections and various methods for attenuating same is thoroughly discussed in the '472 patent. It was shown in that patent that first-order peg-leg multiples may be successfully eliminated by application of the inverse Backus operator to the frequency-domain sum of the velocity and pressure

signatures V and P, respectively in accordance with the steps:

$$\begin{aligned} \text{SUM} &= V + P, \\ S(Z) &= \text{FFT}(\text{SUM}), \\ 5 \quad S1(Z) &= S(Z) \times (1+R_b Z_w)^2. \end{aligned}$$

R_b is initialized to some value between -0.8 and +0.8. Z_w is initialized by introduction of the water layer thickness, a quantity that is somehow obtained independently. The total power of quantity $S1(Z)$ over a
10 selected bandwidth is then iteratively computed, discretely perturbing R_b after each iteration. The value of R_b at minimum power is the local water bottom reflection coefficient. A drawback to that method is the need for getting the water depth from some
15 independent source. Concomitantly, the computations are not very efficient.

In US patent Application 08/651,994, previously cited, and of which this application is a continuation-in-part, it was shown that the water depth can be
20 derived by resolving the velocity and pressure signatures (V and P) received by a dual-mode sensor by summing V and P to isolate the up-going signal $U = (V+P)$, and differencing V and P to sequester the down-going signal $D = (V-P)$. U and D are transformed from the t-x
25 domain to the f-k domain to provide the complex amplitude spectra $UP(Z)$ and $DN(Z)$ respectively. A time-delay operator τ is applied to $UP(Z)$ which is then cross-correlated with $DN(Z)$, discretely perturbing τ after each iteration. The lag time τ that maximizes the
30 cross-correlation function is the two-way travel time in the water layer. The Z transform of τ , $Z_w = e^{-i\omega\tau}$ may now be introduced into the inverse Backus operator $(1+R_b Z_w)^2$.

That method for measuring the water depth for use with the inverse Backus operator depends upon reception
35 of the ghost reflection as shown by the ray paths of Figure 2 and upon knowledge of the water-surface reflectivity coefficient, which is near unity and,

within the same environmental region, substantially a constant. Thus, one of the two Backus variables can be evaluated from the seismic-data harvest itself without recourse to independent foreign measurements.

5 As was shown in the '994 Patent Application, summation of the pressure and the velocity signatures isolates the up-going energy only, thus eliminating the receiver ghost. At sufficiently large travel times, it can be shown that the water-trapped reverberation has
 10 died off so that only the peg-leg reverberations described by the Backus operator $Bop=1/(1+R_bZ_w)^2$ remain. The peg-leg sequence can be eliminated if the up-going signature is multiplied by the inverse Backus operator $(1+R_bZ_w)^2$. In the '472 patent, the criterion to find the
 15 correct value for R_b , the other variable in the Backus operator, was to minimize the total power in the up-going signature after multiplication by the inverse Backus operator. Establishment of the minimal-power convergence limit is based on the premise that the
 20 contribution of the multiple reflections to the total spectral power is inversely proportional to multiple attenuation by the Backus operator. This invention offers a simpler, more direct approach to evaluating R_b .

 It will be recalled that the Z transform of the
 25 two-way travel time in the water layer, Z_w , was determined with the aid of the up-going and down-going complex amplitude spectra $UP(Z)$ and $DN(Z)$. It can be shown that, given the correct value for R_b and knowing Z_w as previously determined, the first-order peg-leg
 30 multiples are eliminated on both the up-going and down-going wavefields. That can be recognized by a minimum in the zero-lag cross correlation between the up-going and the down-going energy after multiplication of the respective quantities $UP(Z)$ and $DN(Z)$ by the inverse
 35 Backus operator, $(1+R_bZ_w)^2$.

 Thus, this invention offers a simple process for evaluating the Backus-operator variables, namely, the

COMPUTATION OF REFLECTIVITY COEFFICIENT
FOR ALL SHOT RECORDS

9

This invention has been described with a certain degree of specificity by way of example but not by way of limitation. For example, the dual-mode sensors may be deployed from buoys and the data may be transmitted
5 over ethereal communication channels instead of being hard-wired. Those skilled in the art will devise obvious variations to the examples given herein but which will fall within the scope of this invention.

What is claimed is:

- 1 1. A method for measuring the reflectivity
- 2 coefficient, R_b , of an earth layer that defines the
- 3 bottom of a water layer, from observations, made at a
- 4 plurality of seismic sensor stations, of seismic
- 5 wavefields propagating within said water layer and
- 6 reflected from earth layers therebeneath, comprising:
- 7 a) at a selected dual-mode sensor station,
- 8 detecting the velocity signature, V , and the pressure
- 9 signature, P , of a reflected seismic wavefield and
- 10 formatting same as time-scale seismic traces;
- 11 b) resolving the pressure and velocity signatures
- 12 into up-going and down-going wavetrains U and D
- 13 respectively;
- 14 c) transforming U and D from the time domain to the
- 15 frequency domain to provide respective complex amplitude
- 16 spectra $UP(Z)$ and $DN(Z)$ derived from resolution of the
- 17 velocity and pressure signatures;
- 18 d) iteratively cross-correlating the $UP(Z)$ spectrum
- 19 with the $DN(Z)$ spectrum and selecting as a delay-time
- 20 operator, Z_w , the lag time that maximizes the cross-
- 21 correlation function;
- 22 e) introducing the delay time operator Z_w into a
- 23 Backus operator, $(1+R_b Z_w)^2$;
- 24 f) forming the products $UP1(Z) = UP(Z) \times (1+R_b Z_w)^2$
- 25 and $DN1(Z) = DN(Z) \times (1+R_b Z_w)^2$ after first initializing
- 26 R_b with a value embraced by the inequality $-1 < R_b < +1$;
- 27 g) iteratively cross-correlating $UP1(Z)$ with
- 28 $DN1(Z)$, discretely perturbing the R_b component of the
- 29 Backus operator after each iteration, until the cross-
- 30 correlation function converges to a minimum; and

31 h) upon convergence, designating the final value of
32 R_b as the local water-bottom reflection coefficient at
33 the selected dual-mode sensor station.

1 2. The method as defined by claim 1, comprising:
2 repeating steps a) through h) for all sensors at
3 all dual-mode sensor stations.

1 3. The method as defined by claim 1, comprising:
2 windowing the velocity and pressure signatures
3 prior to the step of resolving.

1 4. The method as defined by claim 1, comprising:
2 averaging the values for R_b from a plurality of
3 sensors within a preselected radius of each other.

Barrigar & Moss
81 Metcalfe Street
7th Floor
Ottawa, Ontario
Canada, K1P 6K7
Agents for the Applicant

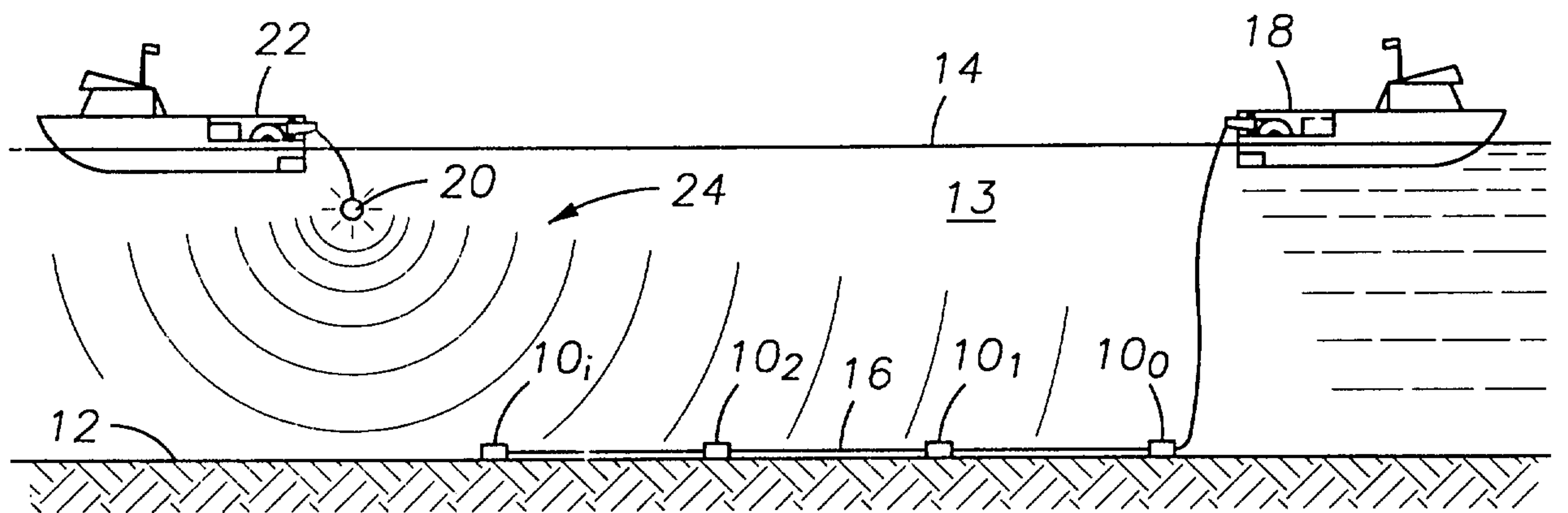


FIG. 1

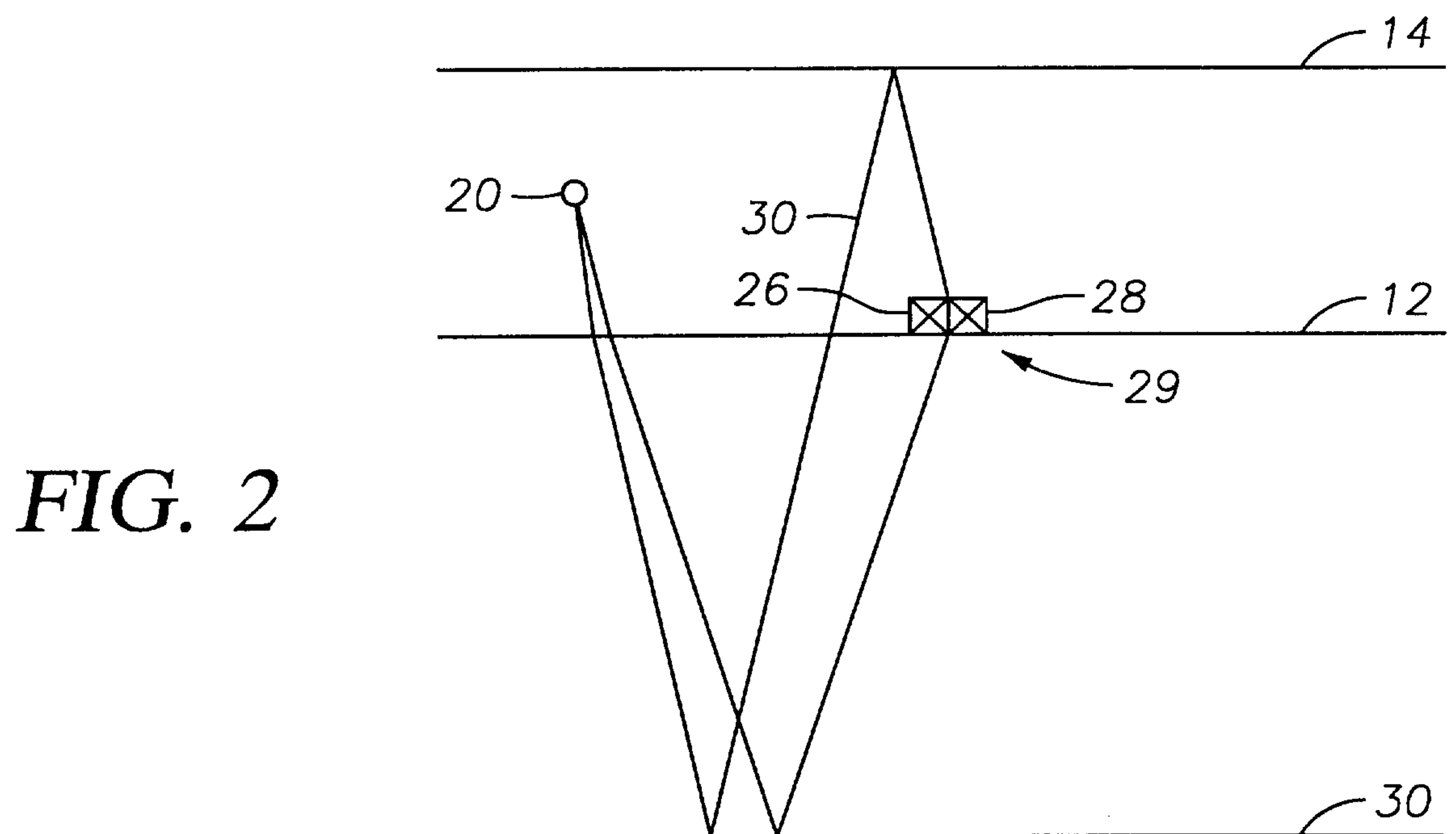


FIG. 2

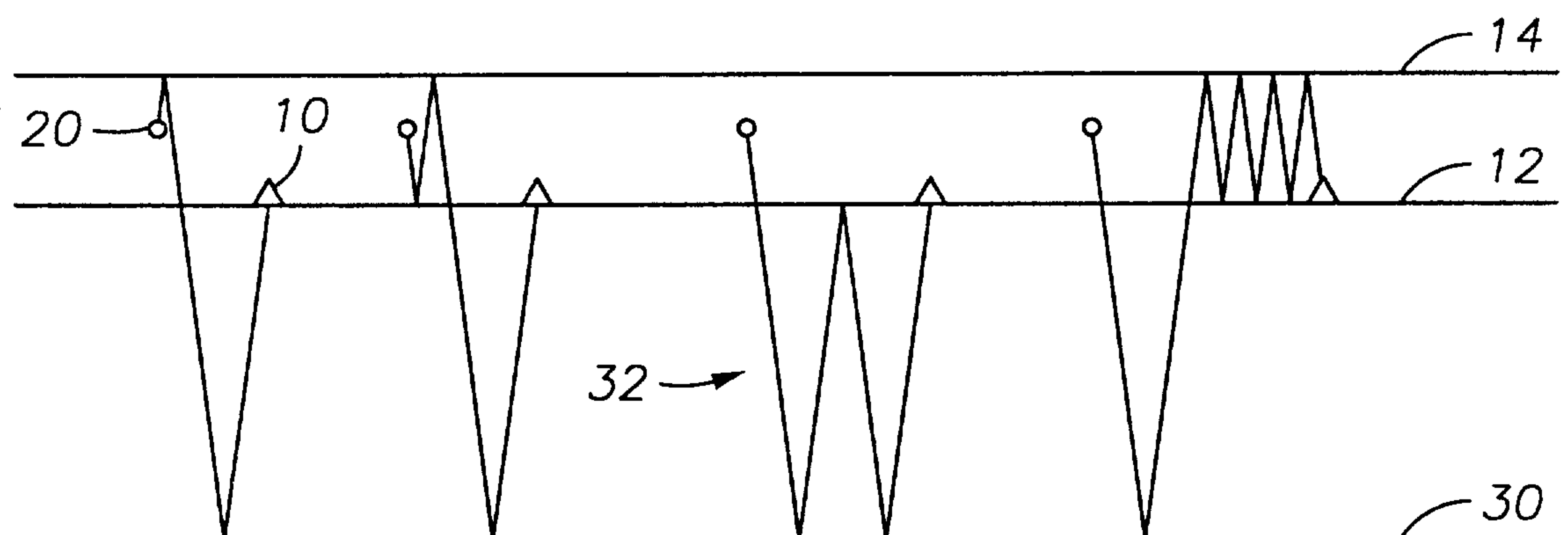


FIG. 3