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(54) Title: BIODEGRADABLE MICROSPHERES INCORPORATING RADIONUCLIDES

(57) Abstract: A crosslinked CCN/CMC microsphere comprising a stably incorporated radionuclide. The microsphere can be prepared by droplet microfluidics and used in a method for radiation treatment comprising the administration of microspheres with incorporated radionuclide.



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## **BIODEGRADABLE MICROSPHERES INCORPORATING RADIONUCLIDES**

### **RELATED APPLICATIONS**

[0001] This application claims priority to U.S. Application No. 62/490,464, filed April 26, 2017, the entire contents of which are incorporated herein by reference.

### **TECHNICAL FIELD**

[0002] This invention relates to materials such as microspheres, microdroplets and microparticles, and in turn, to materials that can be used to deliver radionuclides to the body. In another aspect, the invention relates to embolic microspheres formed of crosslinked cellulose and chitosan polymers.

### **BACKGROUND**

[0003] Many attempts have been made to locally administer radioactive materials to cancer patients as a form of therapy. In some of these, the radioactive materials have been incorporated into small particles, seeds, wires and similar related configurations that can be directly implanted into the cancer. See, for instance, "Treatment of unresectable intrahepatic cholangiocarcinoma with yttrium-90 radioembolization: A systematic review and pooled analysis", AI-Adra, et al. EJSO J. Cancer Surg. 41(2015): 120-127.

[0004] Microparticles for such use have taken a variety of forms, and have been made from a similar variety of materials. For example, microspheres are available under the tradenames TheraSphere® Yttrium-90 Glass Microspheres (available from Biocompatibles UK, Ltd, a BTG International company), as well as SIR-Spheres® microspheres, available from Sirtex Medical. See also PCT application no. W02002034300A1 (Sirtex Medical) which describes microspheres that are said to comprise a polymer and a stably incorporated radionuclide such as radioactive yttrium, and having a diameter in the range of from 5 to 200 microns. The patent describes a method of preparing such microspheres by step of combining a polymeric matrix and a radionuclide for a time and under conditions sufficient to stably incorporate the radionuclide in the matrix to produce a particulate material.

[0005] On a separate subject, processes often referred to as droplet microfluidics have been described that allow the formation of microdroplets from various materials, and for various

purposes. One of the key advantages of droplet-based microfluidics is the ability to use droplets as incubators for single cells. See, for instance, Joensson, et al., *Droplet Microfluidics-A Tool for Single-Cell Analysis*, *Angewandte Chemie* 51(49): 12176-12192, December 3, 2012.

[0006] Various techniques have been described for forming polymer microparticles by droplet microfluidics as well. See, for instance, Serra et al., *Engineering Polymer Microparticles by Droplet Microfluidics*, *J. Flow Chem* 3(3):66-75 (2013).

[0007] On yet another subject, US Patent No. 8,617,132 (Golzarian, et al) described, *inter alia*, the preparation and use of embolic materials that generally comprise carboxymethyl chitosan (CCN) crosslinked with carboxymethyl cellulose (CMC). The resulting microspheres can optionally include a therapeutic agent such as doxorubicin.

### SUMMARY

[0008] In one aspect, the present invention provides a crosslinked CCN/CMC microsphere comprising a stably incorporated radionuclide. In one preferred aspect, the invention provides a microsphere and incorporated radionuclide prepared by means of droplet microfluidics. In yet another preferred aspect, the invention provides a method for radiation treatment comprising the administration of microspheres with incorporated radionuclide.

[0009] The present invention provides microspheres comprising crosslinked CCN/CMC and a radionuclide such as radioactive yttrium. In a preferred embodiment, the microspheres are prepared by the use of droplet microfluidics, and to the use of these microspheres in the treatment of cancer in humans and other mammals.

### DETAILED DESCRIPTION

[0010] The present disclosure describes a plurality of microspheres that include carboxymethyl chitosan (CCN) crosslinked with carboxymethyl cellulose (CMC). The microspheres are biocompatible, bioresorbable, and biodegradable. In accordance with examples of this disclosure, CCN and CMC may be crosslinked without use of a small molecule crosslinking agent to form microspheres that are substantially free of small molecule crosslinking agent. While the use of a small molecule crosslinking agent facilitates crosslinking reactions, some small-molecule crosslinking agents may be toxic or have other adverse effects on cells or tissue in the body of the patient. By omitting small molecule crosslinking agents, such potential

adverse effects may be avoided. In fact, in some examples, the crosslinking reaction between CMC and CCN may be carried out without a small molecule crosslinking agent and at relatively low temperatures (e.g., about 40 °C) in a water and oil emulsion.

[0011] CCN is substantially non-toxic and biodegradable. Chitosan breaks down in the body to glucosamine, which can be substantially absorbed by a patient's body. Similarly, CMC is substantially non-toxic and biodegradable. Thus a crosslinked polymer formed by CCN and CMC is expected to be substantially non-toxic (e.g., biocompatible) and biodegradable (or bioresorbable). Additionally, because the crosslinked CCN and CMC microsphere is formed from two polymers, the mechanical properties, such as compressibility, of the crosslinked molecule are expected to be sufficient for use of the particles as abrasive agents.

[0012] The plurality of microspheres described herein may be used for any suitable purpose, e.g., for radioactive embolization. Because the plurality of microspheres are biocompatible and biodegradable, the microspheres may be acceptable for use within the body, and may degrade after use, which may reduce environmental contamination by the microspheres.

[0013] The ingredient may include, for example, a therapeutic or diagnostic radionuclide, optionally in combination with one or more additional ingredients, such as an antibiotic, antimicrobial, antifungal, or the like. For example, the ingredient may include a therapeutic radionuclide, such as yttrium-90.

[0014] In some examples, the microspheres comprising CCN and CMC may be formed according to the technique described in US Patent No. 8,617,132, the disclosure of which is incorporated herein by reference. Initially, CMC is at least partially oxidized to form partially oxidized CMC. In one reaction a single CMC monomer (repeating unit), which is part of a chain comprising  $n$  repeating units, is reacted with  $\text{NaIO}_4$  (sodium periodate to oxidize the C-C bond between carbon atoms bonded to hydroxyl groups to form carbonyl (more particularly aldehyde) groups. In some examples, the reaction may be carried out at about 250C. Some or all repeating units within the CMC polymer may be oxidized. For example, some repeating units may not be oxidized at all, and may still include two hydroxyl groups the reaction is performed. Other monomers may be oxidized, and may include two carbonyl groups. The CMC may include a weight average molecular weight of between about 50,000 daltons (Da; equivalent to grams per mole (g/mol)) and about 800,000 Da. In some examples, a weight average molecular weight of the CMC may be about 700,000 g/mol.

[0015] The degree of oxidation of the CMC may be affected by, for example, the molar ratio of NaIO<sub>4</sub> to CMC repeating units. In some examples, the molar ratio of NaIO<sub>4</sub> molecules to CMC repeating units may be between about 0.1:1 and about 0.5:1 (NaIO<sub>4</sub>:CMC repeating unit). Particular examples of molar ratios of NaIO<sub>4</sub> molecules to CMC repeating units include about 0.1:1, about 0.25:1, and about 0.5:1. An increased molar ratio of NaIO<sub>4</sub> molecules to CMC repeating units may result in greater oxidation of the CMC, which in turn may lead to greater crosslinking density when CMC is reacted with CCN to form the microspheres. Conversely, a decreased molar ratio of NaIO<sub>4</sub> molecules to CMC repeating units may result in lesser oxidation of the CMC, which in turn may lead to lower crosslinking density when CMC is reacted with CCN to form the microspheres. In some examples, the crosslinking density may be approximately proportional to the degree of oxidation of the CMC. In some examples, a greater crosslinking density may lead to microspheres with greater mechanical strength (e.g., fracture strain).

[0016] CCN may be prepared by reacting chitosan to attach -CH<sub>2</sub>COO- groups in place of one of the hydrogen atoms in an amine group or a hydroxyl group, as illustrated in Reaction 2 of the above-cited '132 patent. In the product of Reaction 2, each R is independently either H or -CH<sub>2</sub>COO-. Similar to oxidation of CMC shown in Reaction 1, the extent of the addition of the -CH<sub>2</sub>COO- may affect the crosslink density when the CCN is reacted with the partially oxidized CMC to form the microspheres. The extent of the addition of the -CH<sub>2</sub>COO- may be affected, for example, by the ratio of ClCH<sub>2</sub>COOH to CCN repeating units. In general, a greater ratio of -CH<sub>2</sub>COO- to CCN repeating units may result in a greater extent of the addition of -CH<sub>2</sub>COO-, which a lesser ratio of -CH<sub>2</sub>COO- to CCN repeating units may result in a lesser extent of the addition of -CH<sub>2</sub>COO-.

[0017] In some examples, the ratio of x:y in the CCN may be about 3:1 (i.e., monomers of "x" form about 75% of the chitosan and monomers of "y" form about 25% of the chitosan), although other ratios may also be used. In some examples, the chitosan starting material may have a molecular weight between about 190,000 g/mol and about 375,000 g/mol. In some examples, Reaction 2 may be performed by stirring the reaction mixture at 500 rpm for about 24 hours at about 25°C, followed by stirring the reaction mixture at 500 rpm for about 4 hours at about 50°C.

[0018] Once the partially oxidized CMC and the CCN have been prepared, each is mixed in a

respective amount of a solvent, such as water. For example, 0.1 milligram (mg) of partially oxidized CMC may be mixed in 5 milliliter (ml) of water to form a first 2% weight/volume (w/v) solution. Similarly, 0.1 mg of CCN may be mixed in 5 ml of water to form a second 2% w/v solution. Of course, solvents other than water may be used, and solutions having other concentrations of partially oxidized CMC or CCN, respectively, may be utilized. For example, saline or phosphate-buffered saline (PBS) may be utilized as alternative solvents. The solvent used in the partially oxidized CMC solution may be the same as or different than the solvent used in the CCN solution. The solutions may have concentrations of partially oxidized CMC or CCN between about 0.5% w/v and about 3% w/v. The concentration of the partially oxidized CMC solution may be the same as or different from the concentration of the CCN solution.

**[0019]** As discussed above, the crosslinking reaction of the CMC and CCN may proceed without use of a small-molecule crosslinking agent, such as glutaraldehyde. This may be advantageous, because in some examples, a small-molecule crosslinking agent may be toxic to a patient which uses products including the microspheres. In this way, the microspheres formed from CCN crosslinked with CMC may be substantially free of any small-molecule crosslinking agent.

**[0020]** In some examples, the crosslinking reaction between CMC and CCN may proceed under relatively benign conditions. For example, the crosslinking reaction may be carried out at ambient pressures and ambient temperatures (e.g., room temperature). In some examples, the reaction may be carried out at a temperature above ambient, such as, for example, 40 °C. Example ranges of temperatures in which the crosslinking reaction may be performed include between about 20 °C and about 70 °C, and at about 40 °C or about 65 °C. In some examples, a lower reaction temperature may necessitate a longer reaction time to result in substantially similar diameter microspheres, or may result in smaller microspheres after a similar amount of time.

**[0021]** One advantage of performing the reaction at a temperature above room temperature may be the removal of water from the reaction mixture during the course of the reaction. For example, performing the crosslinking reaction at a temperature of about 65 °C may result in evaporation of water as the crosslinking reaction proceeds.

**[0022]** An extent of crosslinking between molecules of CMC and CCN may affect mechanical properties of the resulting microsphere. For example, a greater crosslinking density generally may provide greater mechanical strength (e.g., fracture strain), while a lower crosslinking

density may provide lower mechanical strength (e.g., fracture strain). In some examples, the crosslinking density may be adjustable to provide a fracture strain of between about 70% and about 90%, as described below with respect to FIG. 7. The crosslinking density may also affect the degradation rate of the microsphere. For example, a greater crosslinking density may lead to a longer degradation time, while a lower crosslinking density may lead to a shorter degradation time. In some examples, the crosslink bonds may degrade through hydrolyzing of the C=N double bond.

**[0023]** As described above, the crosslinking reaction between CMC and CCN is a modified emulsion-crosslinking reaction. In some examples, an emulsion-crosslinking reaction may be rate-limited by transport of the CMC and CCN molecules, and may play a role in the reaction product (the crosslinked CMC and CCN) being microspheres.

**[0024]** The size of the microspheres may be affected by reaction conditions, such as, for example, a stirring speed, a reaction temperature, a concentration of the CMC and CCN molecules in the reaction emulsion, an amount of mixing of the emulsion, or a concentration of the surfactant in the emulsion. For example, increasing the concentration of each of the CMC and CCN solutions from 1.5% w/v to 2% w/v while keeping the oxidation degree of CMC at about 25% (about 25 oxidized repeating units per 100 total repeating units), the stirring speed at 600 revolutions per minute (rpm), the temperature at about SOC, the reaction time at about 12 hours, and the amount of Span 80 at about 0.3 ml/50 ml mineral oil, the average diameter of the microspheres may increase from about 600  $\mu\text{m}$  to about 1100  $\mu\text{m}$ . As another example, increasing the oxidation degree of CMC from about 10% to about 25% while keeping the concentration of each of the CMC and CCN solutions at about 1.5% w/v, the stirring speed at 600 rpm, the temperature at about SOC, the reaction time at about 12 hours, and the amount of Span 80 at about 0.3 ml/50 ml mineral oil, the average diameter of the microspheres may increase from about 510  $\mu\text{m}$  to about 600  $\mu\text{m}$ .

**[0025]** In some examples, the reaction conditions may be selected to result in microspheres with a mean or median diameter between about 40  $\mu\text{m}$  and about 2200  $\mu\text{m}$ . In some examples, the reaction conditions may be selected to result in microspheres with a mean or median diameter of less than about 2000  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 100  $\mu\text{m}$  and about 1200  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 100  $\mu\text{m}$  and about 300  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 300  $\mu\text{m}$  and

about 500  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 500  $\mu\text{m}$  and about 700  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 700  $\mu\text{m}$  and about 900  $\mu\text{m}$ , microspheres with a mean or median diameter of between about 900  $\mu\text{m}$  and about 1200  $\mu\text{m}$ , or microspheres with a mean or median diameter of between about 1600  $\mu\text{m}$  and about 2200  $\mu\text{m}$ . In some examples, the diameter of the microspheres may be measured using optical microscopy, approximated based on using one or more sieves, or the like.

[0026] Once the reaction has proceeded for a desired amount of time to produce microspheres with a desired mean or median diameter, the water in the emulsion may be substantially fully removed, if the water has not already been evaporated during the crosslinking reaction. The oil phase may then be removed, such as by decanting or centrifugation, and the microspheres may be washed. For example, the microspheres may be washed with Tween 80 solution. Finally, the microspheres may be stored in a liquid, such as water or saline, at a suitable temperature, such as between about 2 °C. and about 8 °C.

[0027] In some examples, the crosslinking reaction may produce a plurality of microspheres with diameters distributed about a mean or median. In some cases, it may be advantageous to isolate microspheres with diameters within a smaller range or microspheres with substantially a single diameter. In some examples, the microspheres may be separated according to diameter by wet sieving in normal saline through a sieve or sieves with predetermined mesh size(s).

[0028] This invention relates to a crosslinked CMC/CCN microsphere that comprises a polymer, particularly a polymer and a radionuclide, as well as to a method for the production thereof, and to methods for the use of this particulate material. In one particular aspect, this invention relates to microspheres which comprise a polymer and a radionuclide such as radioactive yttrium, and to the use of these microspheres in the treatment of cancer and related conditions in humans and other mammals. See, for instance, W02002034300, the disclosure of which is incorporated herein by reference.

[0029] The crosslinked CMC/CCN microsphere of this invention can be designed to be administered into the arterial blood supply of an organ to be treated, whereby it becomes entrapped in the small blood vessels of the target organ and irradiates it. An alternate form of administration is to inject the polymer based crosslinked CMC/CCN microsphere directly into the target organ or a solid tumor to be treated.

[0030] The crosslinked CMC/CCN microsphere of the present invention therefore has utility in

the treatment of various forms of cancer and tumors, but particularly in the treatment of primary and secondary cancer of the liver and the brain. When microspheres or other small particles are administered into the arterial blood supply of a target organ, it is desirable to have them of a size, shape and density that results in the optimal homogeneous distribution within the target organ. If the microspheres or small particles do not distribute evenly, and as a function of the absolute arterial blood flow, then they may accumulate in excessive numbers in some areas and cause focal areas of excessive radiation. It has been shown that microspheres of about 25 microns to about 50 microns in diameter have the best distribution characteristics when administered into the arterial circulation of the liver.

**[0031]** If the particles are too dense or heavy, then they will not distribute evenly in the target organ and will accumulate in excessive concentrations in areas that do not contain the cancer. It has been shown that solid, heavy microspheres distribute poorly within the parenchyma of the liver when injected into the arterial supply of the liver. This, in turn, decreases the effective radiation reaching the cancer in the target organ, which decreases the ability of the radioactive microspheres to kill the tumor cells.

**[0032]** For radioactive crosslinked CMC/CCN microsphere to be used successfully for the treatment of cancer, the radiation emitted should be of high energy and short range. This ensures that the energy emitted will be deposited into the tissues immediately around the crosslinked CMC/CCN microsphere and not into tissues which are not the target of the radiation treatment. In this treatment mode, it is desirable to have high energy but short penetration beta-radiation which will confine the radiation effects to the immediate vicinity of the particulate material. There are many radionuclides that can be incorporated into microspheres that can be used for SIRT. Of particular suitability for use in this form of treatment is the unstable isotope of yttrium (Y-90).

**[0033]** Yttrium-90 decays with a half life of 64 hours, while emitting a high energy pure beta radiation. However, other radionuclides may also be used in place of yttrium-90 of which the isotopes of holmium, samarium, iodine, iridium, phosphorus, rhenium are some examples.

**[0034]** Microspheres of this invention can be provided using any suitable means. See, for instance, Serra et al., 2013 (cited above), the disclosure of which is incorporated herein by reference. For instance, they can be prepared by either heterogeneous polymerization processes (suspension, supercritical fluid) or by precipitation processes in a non-solvent. Preferably,

however, the microspheres are prepared using microfabrication techniques that enable the preparation of very efficient emulsification microstructured devices which, along with capillaries of small dimensions, allow emulsifying a fluid in another immiscible fluid. Thus, droplets or bubbles, with an extremely narrow size distribution (the coefficient of variation of the particle size distribution is typically lower than 5%) can be continuously produced and dispersed in a continuous fluid flowing within these microfluidic devices. If the 'to be dispersed' phase is composed of a polymerizable liquid, the droplets can be hardened downstream either by thermally or photo-induced polymerization. Over conventional processes, microfluidic-assisted processes offer the possibility not only to precisely control the size of the particle but also its shape, morphology and composition. At least two different categories of microsystem are suitable for the emulsification of a polymerizable liquid. In the first one, both continuous and dispersed fluids flow inside microchannels, while in the second one, the continuous phase flows inside a tube and the dispersed phase inside a capillary of small dimensions. The emulsification mechanism, which is quite similar for these two categories of microsystem, proceeds from the break-up of a liquid thread into droplets when the to-be-dispersed phase is sheared by the continuous and immiscible phase.

**[0035]** A variety of microchannel-based devices can be used, including for instance, a terrace-like microchannel device, a T-junction microchannel device, and a flow-focusing microchannel device. These devices are usually microfabricated, thanks to semiconductor related like technologies. Thus, lithographic processes are commonly employed to etch into silicon, glass, or polydimethylsiloxane (PDMS) microchannels in which the continuous and dispersed phases flow. Over capillary-based devices, microchannel-based systems offer some unique features. Microsystems with channel widths as low as few tens of microns can be obtained. Mask lithographic techniques allow for a perfect alignment of the microchannels and complex microstructures.

**[0036]** Upstream and downstream functionalities (flow distribution, selective droplets fusion, droplet scissions, etc.) are easily implemented. Finally, chips with multiple microstructures can be designed for increasing the overall production of polymer particles.

**[0037]** A variety of capillary-based devices can also be used, including a co-flow capillary device, a cross-flow capillary device, and a flow-focusing capillary device. All the above microchannel-based devices are designed such that the dispersed phase is in direct contact with

the wall of the device before being emulsified by the continuous phase. So the device material should be carefully chosen or modified to avoid a phase inversion. This phenomenon is observed when the dispersed phase has a greater affinity for the material than the continuous phase; i.e., when the dispersed phase wets preferentially the walls. As a result, the continuous phase is emulsified by the dispersed phase and droplets of continuous phase are formed. This phase inversion can be avoided by selecting a proper material hydrophilic for hydrophobic droplets) or by modifying locally the properties of the material at the very location where droplets of dispersed phase are formed. However, the latter procedure requires an additional step in the microfabrication process. Additionally, one can use capillary-based devices to deliver the dispersed phase in the very center line of the continuous phase flow so that the droplets never meet with the device walls. Moreover, these capillary based devices solve for the clogging of microchannels that can be encountered in the above microchannel-based devices as well as for the possibility to get O/W or W/O emulsion with a single microsystem.

**[0038]** Simple morphologies like beads and capsules can be obtained from the abovementioned microfluidic devices. However, in addition to the greater control over the size, these devices also allow for the production of specific polymer particles, which characteristics (morphology and composition) are likely to be difficult to obtain in conventional batch reactors dispersed phase has a greater affinity for the material than the continuous phase, i.e., when the dispersed phase wets preferentially the walls. As a result, the continuous phase is emulsified by the dispersed phase and droplets of continuous phase are formed. This phase inversion can be avoided by selecting a proper material size and size distribution can be obtained.

**[0039]** Droplet size can be controlled by various means, including in articular operating parameters such as dispersed and continuous velocities, internal capillary diameter, the viscosity of dispersed and continuous phases, and surface tension. In one example, and preferred embodiment, the microspheres are provided by the application of a capillary-based microsystem that allows the preparation of polymeric microparticles of different shapes (e.g., spheres and rods) and/or with different morphologies (e.g., Janus and core-shell particles).

**[0040]** Capillary-based microsystems can be convenient to produce polymeric capsules (average size of 300 1- $\mu$ m) and to investigate effect of operating and composition parameters on the morphology of the membrane. These parameters can be easily changed, and a small

amount as low as 1 ml of the dispersed phase is required to investigate capsules characteristics.

[0041] Given the present description, those skilled in the art will be able to prepare polymeric materials according to the present invention in any suitable form, e.g., in the form of spherical or janus-like microparticles. These microparticles exhibit some specific properties which arise from either the narrow size distribution or from their morphology that cannot be achieved when they are prepared by more conventional synthetic methods.

## EXAMPLES

### Example 1. Preparation of yttrium-containing microspheres by emulsion.

[0042] Partially Oxidized CMC and CCN are prepared in the manner described in Examples 1 and 4 of US Patent No. US 8,617, 132, the disclosure of which is incorporated herein by reference. About 0.075 g of CCN-1 is mixed in about 5 ml of water to form a 1.5% w/v CCN-1 solution. Similarly, about 0.075 g OCMC-1 is mixed in about 5 ml water to form a 1.5% w/v OCMC-1 solution. The CCN-1 and OCMC-1 solutions are then mixed. Yttrium-90 is obtained by irradiating Yttrium oxide to produce yttrium-90 from the nuclear reaction  $Y-89(n, \gamma)Y-90$ . Yttrium-90 has a half life of 64 hours. The yttrium ( $^{90}Y$ ) oxide is then dissolved in 0.1 M sulphuric acid with gentle heating and stirring to form a clear, colourless solution of yttrium ( $^{90}Y$ ) sulphate. The Yttrium ( $^{90}Y$ ) sulphate is incorporated into the polymer solution and the mixture is used as the dispersed phase. The amount of yttrium ( $^{90}Y$ ) sulphate that added is determined by limiting the radioactivity of each microsphere in the range of  $3.75-7.5 \times 10^{-8}$  GBq. The mixture is added to about 50 ml mineral oil containing between 0.2 ml and 0.5 ml sorbitane monooleate to form an emulsion, and the emulsion is homogenized for about 15 minutes. The mixture is then stirred overnight at 40-60°C to form crosslinked microspheres. Then oil is decanted, and the microspheres can be washed with 5% Tween 80 followed by 0.9% saline.

[0043] The mean diameter of the microspheres, measured in normal saline by a light microscope, is determined to be between 20 and 60 microns in diameter. The maximum energy of the beta particles is 2.27MeV, and the maximum range of emissions in tissue is between about 2 and 15 mm. The half life is 64.1 hours. In therapeutic use, requiring the isotope to decay to infinity, 94% of the radiation is delivered within about 7 to about 11 days.

The polymer matrix is substantially bioresorbed within 15 to 20 days.

Example 2. Preparation of yttrium-containing microspheres by droplet microfluidics.

**[0044]** Partially Oxidized CMC and CCN are prepared in the manner described in Examples 2 and 4 of US Patent No. US 8,617, 132, the disclosure of which is incorporated herein by reference. About 0.075 g of CCN-1 is mixed in about 5 ml of water to form a 1.5% w/v CCN-1 solution. Similarly, about 0.075 g OCMC-1 is mixed in about 5 ml water to form a 1.5% w/v OCMC-1 solution. The CCN-1 and OCMC-1 solutions are then mixed. Yttrium-90 is obtained by irradiating Yttrium oxide to produce yttrium-90 from the nuclear reaction  $Y-89(n, \gamma) Y-90$ . The yttrium ( $^{90}Y$ ) oxide is then dissolved in 0.1 M sulphuric acid with gentle heating and stirring to form a clear, colourless solution of yttrium ( $^{90}Y$ ) sulphate. The Yttrium ( $^{90}Y$ ) sulphate is incorporated into the polymer solution and the mixture will be used as the disperse phase. The amount of Yttrium ( $^{90}Y$ ) sulphate added is determined by limiting the radioactivity of each microsphere in the range of  $3.75-7.5 \times 10^{-8}$  GBq. Mineral oil containing between 0.4-1% sorbitane monooleate will be used as a continuous phase. Microspheres in the size range of 20-60  $\mu\text{m}$  are prepared with the co-flow capillary-based microsystem (Serra et al., 2013).

**[0045]** Microdroplets and subsequent yttrium core polymer shell microparticles are obtained from capillary based microfluidic devices consisting in different arrangement of capillaries single, co-axial, and side-by-side having small inner diameters (ca. 20-150  $\mu\text{m}$ ). Either of two devices can be used, including a co-flow and a flow-focusing microsystem. At the capillary tip, the to-be-dispersed phase, composed of a monomer solution admixed with an initiator, is sheared by the continuous phase to form, in the dripping regime, droplets of same volume with a regular frequency up to several tens of Hz. Depending on the capillaries arrangement, single, double, or janus droplets are produced. All microsystems are composed of capillaries with hydrophilic or hydrophobic inner walls, T-junctions and tubing.

**[0046]** Formation of droplet is observed under an optical microscope equipped with a CCD camera capturing up to 200 fps at a full resolution of 648 x 488 pixels. Application of these capillary-based microsystems allows the preparation of polymeric microparticles of different shapes including spheres and rods. One can also produce microparticles with

different morphologies, including janus and core-shell whose shell thickness can be tuned simply by adjusting the operating conditions (mainly continuous and dispersed phase flow rates).

[0047] The preformed microspheres are collected in a container with the mineral oil and the aqueous phase of the emulsion is allowed to evaporate over night at about 40- 60C with constant stirring. Then microspheres are then filtered, and washed with 5% Tween 80 followed by 0.9% saline.

## CLAIMS

1. A composition comprising crosslinked CMC/CCN microspheres comprising a stably incorporated radionuclide.
2. The composition according to claim 1 wherein the radionuclide comprises yttrium-90.
3. The composition according to any previous claim wherein the microsphere has been prepared by droplet microfluidics.
4. The composition according to any previous claim wherein the microsphere is adapted to substantially release the radionuclide over a period of between about 7 to about 11 days.
5. The composition according to any previous claim wherein the polymer matrix is substantially bioresorbed within 15 to 20 days.
6. A method of making a composition according to claim 1, the method selected from the group consisting of emulsion formation and droplet microfluidics.
7. A method of treating the body, comprising the steps of providing a composition according to claim 1, and delivering the composition to a site within the body.

INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US 18/29555

A. CLASSIFICATION OF SUBJECT MATTER  
 IPC(8) - A61K 51/06, A61K 51/12, A61K 103/32, A61L 31/06, C08L 1/28, C08L 5/08 (2018.01)  
 CPC - A61K 51/065, A61K 51/1244, A61K 51/1255, A61K 51/1251, A61L 31/041, C08L 1/286, C08L 5/08, C08J 3/24

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
See Search History Document

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
See Search History Document

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)  
See Search History Document

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 2011/0082427 A1 (GOLZARIAN et al), 07 April 2011 (07.04.2011), para [0004]-[0005], [0009], [0136].	1-3, 6-7
Y	US 2014/0274945 A1 (COVIDIEN LP), 18 September 2014 (18.09.2014), para [0009], [0012], [0020], [0189].	1-3, 6-7
Y	US 2008/0041715 A1 (LANPHERE et al), 21 February 2008 (21.02.2008), figures 1-3; para [0004]-[0005], [0016], [0029], [0031], [0039]-[0041], [0081]-[0082].	3

Further documents are listed in the continuation of Box C. See patent family annex.

\* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier application or patent but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search 03 July 2018	Date of mailing of the international search report <b>20 JUL 2018</b>
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Name and mailing address of the ISA/US Mail Stop PCT, Attn: ISA/US, Commissioner for Patents P.O. Box 1450, Alexandria, Virginia 22313-1450 Facsimile No. 571-273-8300	Authorized officer: Lee W. Young PCT Helpdesk: 571-272-4300 PCT OSP: 571-272-7774
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INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 18/29555

Box No. **II** Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1.  Claims Nos.:  
because they relate to subject matter not required to be searched by this Authority, namely:
  
2.  Claims Nos.:  
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
  
3.  Claims Nos.: 4-5  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box No. **III** Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1.  As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2.  As all searchable claims could be searched without effort justifying additional fees, this Authority did not invite payment of additional fees.
3.  As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
  
4.  No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

- Remark on Protest**
- The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.
  - The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.
  - No protest accompanied the payment of additional search fees.