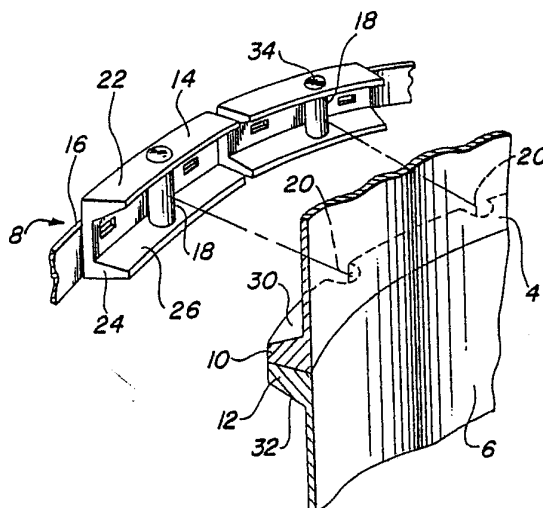




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(54) Title: CLAMPING CONNECTION ASSEMBLY FOR SPACECRAFT**(57) Abstract**

A clamping connection assembly for separable parts of a spacecraft is provided and includes a tension belt for securing a plurality of retainers against camming surfaces on flange members on separable spacecraft component parts. The other peripheral edges of the flange members have detents to respectively receive a single shear pin mounted on each of the retainers. The shear pins receive any shear and torsional forces and transmit them between the structural parts of the spacecraft components without creating additional forces on the tension belt.

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CLAMPING CONNECTION ASSEMBLY FOR SPACECRAFT

1

BACKGROUND OF THE INVENTION1. Field of the Invention

The present invention is directed to a clamping
5 connection assembly for retaining separable component
parts of a spacecraft and more particularly, to a
V-clamp connection assembly capable of preventing
relative rotational movement and transmitting shear and
torsional forces without changing the axial load
10 created by a tension strap used to retain the separable
components of a spacecraft.

2. Description of the Prior Art

Connection assemblies, for example, those
15 that retain separable parts of a spacecraft, provide
important structural links in the primary load path of
a spacecraft during both boost and ascent flight and
also, if necessary, during re-entry. For example,
satellites frequently jettison a portion of their
20 structure, such as a propulsion motor, as it is lifted
into a permanent orbit. As can be readily appreciated,
spacecraft connection assemblies must be designed not
only for low weight, but also for extremely high
reliability due to the high cost of the spacecraft
25 launch and the general inaccessibility to rectify any
errors.

As this particular field of art has advanced
from the 1950's to the present day, there has been a
recognition of the design requirement of minimizing the
30 component parts that can fail. Even today with the
realization of the launching of satellites and spacecraft
from the Space Shuttle, the high cost involved in

1 employing a human being in space still requires a
connection assembly design that will be automatic,
without human intervention and with an extremely high
reliability. Likewise the design criteria of minimizing
5 weight remains as important as ever giving the high
cost of transmitting the payload of a spacecraft into
outer space. Designers in this field have recognized
the desirability of using tension band clamping
assemblies, instead of exploding connecting assemblies,
10 to hold together separable components of a spacecraft
and thereby minimizing any pyro-shock that could
adversely vibrate the payload of the spacecraft, such
as electronic components.

 In the 1960's, a connection assembly design
15 referred to as the Marman Band was proposed which
included a plurality of V-retainers or wedged shaped
shoe members that provided a V-clamping to flanges
positioned on the exterior surfaces of separable
component parts of the spacecraft. A pair of separable
20 tension bands were joined together by a pair of
spaced pyrotechnic tension bolts that could adjustably
vary the tension straps that held the V-band coupling
members. The tension straps were utilized to create
inwardly radial forces on the V-shaped retainers which
25 would, in turn, wedge the flanges of cylindrical housing
structures of separable component parts of the spacecraft
in an axial direction. This V-band coupling was
basically configured to transfer axial loads and bending
moments across the resulting structural joint of the
30 connection assembly. Small shear torque loads were
transferred across the joint by relying on friction
that would exist between the flange surfaces and the
retainer wedges. If the spacecraft was to be subject
to considerable forces that would produce large shear
35 torque loads, either keys were inserted between the

1 flanges or the friction load that was applied during
the loading of the tension straps, had to be carefully
controlled to take into consideration the magnitude of
the shear torque forces that were to be expected.

5 Thus prior to the advent of the Space Shuttle,
the primary connection assembly relied upon for separable
spacecraft component parts were V-band couplings that
were encircled with tension straps to maintain an axial
loading between the spaceship component parts. Usually
10 the friction of the band and the axial loading friction
of the flanges or cylindrical structures of the spacecraft
component parts were relied upon to handle any shear
and torque forces.

The cause of the shear and torque forces resulted
15 from many separate sources such as transitory forces
due to the cyclic nature of a rocket burn particularly
in solid fuel rockets, variances in the center of gravity
of the fuel container during the burn-off, changes in
nozzle direction to control the rocket, changes in
20 trajectory of the rocket to achieve the desired orbit
path, flexing of the rocket itself during flight,
vibrations, etc. Usually, however, the ratio of the
longitudinal forces generated during flight to any
transverse loading was about 10:1.

25 However, a significant increase in shear and
torque forces occurred when spacecraft were to be
launched from the bay of the Space Shuttle. As can be
seen in FIG. 4, the spacecraft payload was positioned
offset from the principle rocket thrust from the rockets
30 102 and this position can produce force ratios that
approached a 1:1 ratio between the axial force loading
and the transverse loading. Additionally, the spacecraft
was usually mounted to be cantilevered from releasable
restrains that permitted additional transverse vibration
35 to be created, since the minimum number of restraining

1 points provided the least number of possible failure
points. Additionally, the Space Shuttle 100 also
required designing any clamping connection assembly to
take into consideration the possibility of re-entry
5 landing, if necessary, and its associated high transverse
loading.

When the magnitude of the transverse loading was
appreciated, attempts were made to add a spline between
the flanges of the separable component parts of the
10 spacecraft to resolve the problem. It was recognized
that in increasing the capacity of transmitting the
shear and torsional forces that an increase in the
possibility of seizing between the separable components
parts would occur. It was also recognized that metallic
15 parts that rub together had a higher probability of
seizing or even welding together in outerspace than
doing so on earth.

Additionally, the use of the Space Shuttle further
provided an ability to increase the diameter of spacecraft
20 as compared to rocket launched spacecraft and with the
larger diameters, there was a greater need to transmit
the shear and torsional forces and thereby prevent any
relative rotational movement between the separable
spacecraft component parts.

25 The increased shear carrying requirement for
shuttle launched spacecraft is derived as follows:

30

35

1 Transverse force balance

$$S = f \left(P_{ax} + \frac{4SH}{D} \right) \quad (1)$$

where

5 $S = mgT$ Transverse force

$P_{ax} = mgA$ Axial force

m = Spacecraft mass

D = clamp diameter

H = spacecraft center of weight above connection clamp

10 gT = transverse acceleration

gA = axial acceleration

f = coefficient of friction at clamp
(shear carrying requirement)

15 Substitution yields

$$f = \frac{1}{g_A/g_T + \frac{4H}{D}} \quad (2)$$

20 This equation (2) is best evaluated by inserting
typical values for a shuttle and expendable rocket
launched spacecraft as listed in Table 1.

TABLE 1

	<u>Load factors</u>		<u>Configuration parameters</u>		<u>Shear factor</u>
	gA	gT	H	D	f
25 Shuttle	4	6	40	90	.41
30 Expendable Rocket	16	1.5	30	36	.07

35

1 The shear factor for a shuttle launched spacecraft
far exceeds that of an expendable rocket and a factor
of 0.4 can not reliably be provided by friction. Thus,
a mechanical shear bearing member is needed.

5 An additional limitation in the design of
connection assemblies was the clear recognition that
the tension band design had reached a fairly developed
and reliable state of art and it was necessary in
resolving the problems presented by this increase in
10 shear and torsional forces that no additional load
would be asserted on the tension band that would require
further redesign.

One of the proposed prior art solutions to this
problem is illustrated in FIG. 7, wherein a connector
15 assembly 200 utilizes a series of aluminum wedge blocks
202 that are forced against the joint flange members
206 and 208 by a clamp tension band 204. The internal
surface of the flange member 206 has a series of conical
detents of approximately 60 in number, that are spaced
20 about the diameter of the flange, for receiving shear
cones 214 that are adjustably mounted on threaded shafts
212 journaled within threaded ports 210 in the lower
flange member 208. Thus, the individual shear cones
could be adjusted to eliminate any possible gap in the
25 detent on the flange member 206. It is necessary,
however, to ensure that no seizing or binding occurs
and therefore testing on appropriate and expensive test
jigs is required to determine if the shear cones are not
binding on the separable spacecraft component parts,
30 for example, by physically separating the component
parts during spacecraft testing. As can be readily
appreciated, the slanting surfaces of the cones which
were positioned at conical surfaces that subscribed at
an acute angle of 15° to 20°, provided, in effect,
35 camming surfaces and any shear load application as

1 well as misalignment would produce corresponding counter
axial forces that would increase the radial force load
on the tension band.

Thus there is still a need in this aerospace
5 field to improve the clamping connection assembly that
is used to hold two separable component parts of a
spacecraft together.

SUMMARY OF THE INVENTION

10 The present invention provides a clamping
connection assembly for a spacecraft having first and
second separable spacecraft components that are held
together by a releasable tension strap. Each of the
spacecraft components have flange members with exterior
15 camming surfaces and contact surfaces. The respective
contact surfaces can be planar and smooth, which is
consistent with successful prior art designs that have
been proven through repetitive experiences in outerspace.
A plurality of retainer members or free floating wedges
20 of a clamping connection assembly are used for
transmitting the radial forces of the tension strap to
the respective flange members of the first and second
spacecraft component parts.

In the preferred embodiment, a single shear pin
25 can be mounted to extend between the retainer member
camming surfaces to entirely restrain the shear and
torsional forces without increasing the axial load in
the tension strap and further, without locking the
connection assembly and thereby prohibit a predetermined
30 release from the smooth contact surfaces. Detents on
the outer peripheral edges of each of the flange members
of the spacecraft component parts are complementarily
designed to receive the shear pins. Finally, leaf
springs can bias the shear pins into the detents.

35

1 The objects and features of the present invention
will become readily apparent from the following detailed
description taken in conjunction with a preferred
embodiment thereof, with reference to the accompanying
5 drawings, in which like parts are designated by like
reference numerals and in which:

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic side elevational view of a
10 spacecraft embodying the present invention;

FIG. 2 is a partial plan view of a clamping
connection assembly;

FIG. 3 is a schematic exploded view of the
connection assembly of the present invention;

15 FIG. 4 is a schematic side elevational view of a
Space Shuttle and rocket;

FIG. 5 is a perspective cut away side view of
the present invention;

20 FIG. 6 is a partial cross-sectional side view of
a portion of the present invention; and

FIG. 7 is a side cross-sectional view of an
example of prior art.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

25 The following description is provided to enable
any person skilled in the aerospace industry to make
and use the invention, and it sets forth the best mode
contemplated by the inventor of carrying out the
invention. Various modifications, however, will remain
30 readily apparent to those skilled in the above art,
since the generic principles of the present invention
are applied herein specifically to provide a relatively
economical and easily manufactured clamping connector
assembly for spacecraft.

35

1 In accomplishing the design criteria of the
present invention, the shear load carrying feature of
the design does not alter the V-clamp band tension nor
the forces applied to the wedge retainer member.
5 Equally important, the solution offered by the present
invention not only does not depend upon friction, but
further permits a separation testing of the shear pins as
part of the test of the V-clamp release without
requiring special testing jigs. As will be appreciated
10 the shear carrying capabilities of the present invention
is ensured even when the flanges between the separable
component parts of the spacecraft gap.

 Referring to FIG. 1, a conceptual schematic view
of a spacecraft 2, such as a satellite, is disclosed
15 having at least a first separable component part 4 and
a second separable component part 6. For example, the
orbiting satellite 4 could be separated from a propulsion
motor 6 upon the release of a clamping connection
assembly 8.

20 Referring to FIGS. 3 and 5, a first flange 10 is
providing on the spacecraft component part 4 and a
second flange 12 is provided on the second spacecraft
component part 6. The exterior surfaces or the upper
and lowermost surfaces in the axial direction (A-A)
25 have camming surfaces 30 and 32, respectively. The
intermediate contact surfaces 31 are preferably smooth
and planar. The outer periphery of the flanges are
cylindrical and are provided with detents 20. A retainer
or wedge clamping member 14 has upper and lower retainer
30 flanges 22 and 24 that support internal retainer camming
surfaces 26 and 28 of a complimentary design for
interfacing with the exterior camming surfaces 30 and
32 of the spacecraft's flange members 10 and 12.

1 A tension strap or belt 16 of, for example, a titanium
 material, as known in the art, is used to produce the
 axial forces that are applied through the retaining
 members 14 that are peripherally spaced about the
 5 circumference of the flanges 10 and 12. The tension
 strap 16 creates inward radial forces on the roughly
 V-shaped retainer member 14 which in turn wedges the
 flanges 10 and 12 to load the contact surfaces 31 in an
 axial direction, A-A as shown in FIG. 1. As mentioned
 10 earlier, the retainer member 14 is designed basically
 to transfer axial loads and bending moments across the
 structural joint between the separable component parts
 4 and 6 of the spacecraft.

The two principal types of loading carried across
 15 the V-band coupling are axial tension or compression,
 P_{ax} , and bending moment M . Both of these loadings may
 be combined and expressed as a load intensity N per
 linear unit of joint circumference $2\pi R$:

20 Axial load intensity N_p :

$$N_p = \frac{P_{ax}}{2\pi R}$$

Bending load intensity N_M :

25
$$N_M = \frac{M \cos \phi}{\pi R^2}$$
 where ϕ is measured from the
 line of the applied moment
 vector

Maximum total load intensity N :

30
$$N = \frac{P_{ax}}{2\pi R} + \frac{M}{\pi R^2}$$

35

1 Temperature correction factors and design safety
factors may be applied to define a maximum design load
or load intensity. This maximum design load will then
form the basis for sizing the V-coupling retainers and
5 the spacecraft flanges. Typically, all structural
elements were required to sustain critical design
loading without a permanent material set and in order
to preclude vibratory impact and slipping within a V-
coupling joint, clamp elastic characteristics and
10 preloading were usually selected such that both flange
and flange/retainer separation did not occur.

 The wedging force applied by a V-coupling retainer
member 14 as a result of strap tension is proportional
to the V-angle, that is, the smaller the flange angle
15 the smaller the requirement on the band tension for
transferring a specific load across the coupling joint.
As may be readily appreciated, smaller tension loads
are desirable for achieving a lightweight clamp connection
design. Consideration of friction and concern for
20 locking of the retainer member 14 to the respective
flanges 10 and 12 that are under axial loads, establish
a lower limit for the angle.

 The basic V-coupling design is not configured for
the transfer of shear and torque forces other than by
25 friction. The prior art has attempted to address these
design considerations through the use of splines or
retractable shear cones to assist in carrying any large
shear and/or torsion loads. This design approach
affects the proven performance of the basic V-coupling
30 heretofore relied upon in the prior art and it adds the
need for separation testing to ensure release of the
coupling. As can be readily appreciated, the present
invention is not required to alter these design features
of a clamping connector assembly nor does it increase
35 the demands upon the tension strap 16 and retainer
member 14.

1 Referring to FIG. 2, a partial plan view of a
clamping connector assembly 8 is disclosed and illustrates
the plurality of floating retainer members 14 that are
spaced about the circumference of the spacecraft. Pyro
5 bolts 44 can adjust the tension through a threaded
tightener assembly 46. Usually the tension band 16 is
hammered, in an attempt to equalize the forces about the
circumference, while the clamping tension is increased
through the tightener assembly 46. The shear pins 18,
10 for example, as shown in FIGS. 5 and 6, are mounted in
apertures 34 on the respective retainer flanges 22 and
24. These apertures can be of a relatively loose
tolerance to permit radial movement of the shear pins
18. Additionally, the configuration of the shear pins
15 can be of a cross-sectional circular or oblong
configuration, as shown in FIGS. 5 and 6 as long as
they don't provide a camming surface relative to the
flange detents 20 to increase the radial loading on the
tension band 16. Spring members, such as leaf springs
20 40, can be used to bias the shear pins in a radially
inward direction while permitting sufficient outer
radial movement for any variances in tolerances between
the shear pin and its corresponding detent 20 on the
outer peripheral edges of the retainer flanges 22 and
25 24. A mounting bracket 36 can be mounted on retention
heads 42 on the shear pins 18 and serve to guide or
retain the tension band 16. While not shown, mounting
brackets to catch or retain the parts of the clamping
connection assembly after release are used.

30 As an alternative design, not disclosed in the
drawings, the retention flanges 22 and 24 of the retainer
member 14 can carry appropriate detents to interface with
bosses or shear projections mounted on the upper and lower
surfaces of the first and second flanges of the spacecraft
35 component parts. Thus, the smooth planar contact

1 surface can be retained between the flanges while the
bosses can interface with detents on the flanges of the
retainer member 14 for transmitting the shear and
torsional forces and preventing relative rotational
5 movement between the flange members. Thus, while the
preferred embodiment uses shear pins extending between
the retainer flanges 22 and 24, means can be provided
on the flange member and the retainer member for
cooperatively preventing relative movement between the
10 flange members and thus, transmit the shear and torsional
forces. Such a design, however, may require redesign
of the retainer member since it would now be subject to
bending moments.

While the above embodiments fully disclose the
15 advantages and features of the present invention, it
should be readily understood that a person skilled in
this field, once provided with these teachings, would
be capable of variance therefrom. Accordingly, the
scope of the present invention should be determined in
20 accordance with the following claims, wherein I claim:

25

30

35

CLAIMSWhat is Claimed is:

- 1 1. In a spacecraft having first and second
separable components joined by a tension strap V-clamp
assembly so as to be held together along an axial
direction while subject to both axial loads and bending
5 moments, the improvement of a connection assembly
comprising:
 a first flange member having a first detent
on the first spacecraft component;
 a second flange member having a second detent
10 on the second spacecraft component;
 a retainer member for transmitting the radial
force of the tension strap to the first and second flange
members to hold them together; and
 a shear pin mounted on the retainer member
15 for engaging the complimentary first and second detents,
the shear pin and detents cooperatively preventing
relative rotational movement between flange members,
the shear pin being capable of transmitting shear and
torsional forces without increasing the axial load
20 created by the tension strap or locking the connection
assembly to prohibit a predetermined release.
- 1 2. The invention of Claim 1 wherein the detent
on each flange member extends from a respective contact
surface to a camming surface along a peripheral edge of
the flange member.
- 1 3. The invention of Claim 2 wherein the retainer
member includes first and second retention flanges each
including an aperture, the shear pin being loosely
 journaled within the respective apertures.

1 4. The invention of Claim 3 further including a
spring member to bias the shear pin to one side of the
apertures.

1 5. In a spacecraft having first and second
separable components joined by a releasable tension
strap so as to be held together along an axial direction,
while subject to both axial loads and bending moments,
5 the improvement of a connection assembly comprising:

 a first flange member on the first spacecraft
component having a first camming surface and a second
contact surface, the first surface being positioned at
an acute angle to the second surface;

10 a second flange member on the second spacecraft
component, having a first camming surface and a second
contact surface complimentary to the first flange member
contact surface, the first surface being positioned at
an acute angle to the second surface, the respective
15 contact surfaces being smooth;

 a retainer member, for transmitting the radial
force of the tension strap to the first and second flange
members to hold them together, having a pair of
complimentary camming surfaces to co-act with the first
20 camming surfaces of the first and second flange members
to create an axial force from the radial force of the
tension strap; and

 means on the first and second flange members
and retainer member for cooperatively preventing relative
25 rotational movement between the smooth contact surfaces
of the flange members, including on the retainer member
at least a shear pin capable of restraining shear and
torsional forces, without increasing the axial load
created by the tension strap or locking the connection
30 assembly to prohibit a predetermined release of the

smooth contact surfaces and at least a pair of complimentary detents positioned on the peripheral edges of the flange members for receiving the shear pin.

1 6. The invention of Claim 5 wherein the retainer member includes a first and second retention flange having apertures, the shear pin being loosely journaled within the respective apertures.

1 7. The invention of Claim 6 further including a spring member to bias the shear pin to one side of the aperture.

1 8. In a spacecraft having first and second separable components joined by a releasable tension strap so as to be held together along an axial direction, while subject to both axial loads and bending moments,
5 the improvement of a connection assemblies positioned about the spacecraft, each of them comprising:
 a first flange member on the first spacecraft component having a first camming surface and a second contact surface, the first surface being positioned at
10 an acute angle to the second surface;

 a second flange member on the second spacecraft component, having a first camming surface and a second contact surface complimentary to the first flange member contact surface, the first surface being positioned at
15 an acute angle to the second surface, the respective contact surfaces being planar and smooth;

 a plurality of retainer members, for transmitting the radial force of the tension strap to the first and second flange members to hold them
20 together, each having a pair of retention flanges with

complimentary camming surfaces to co-act with the first camming surfaces of the first and second flange members to create an axial force from the radial force of the tension strap; and

25 means on the first and second flange members and each retainer member for cooperatively preventing relative rotational movement between the smooth contact surfaces of the flange members, including on the retainer member at least a shear pin extending between the
30 retainer member camming surfaces capable of restraining shear and torsional forces, without increasing the axial load created by the tension strap nor locking the connection to prohibit a predetermined release of the smooth contact surfaces and at least and no more than a
35 pair of complimentary detents, one on each of the outer peripheral edges of the first and second flange members for receiving the shear pin.

1 9. The invention of Claim 8 wherein each retainer member includes a first and second retention flange having apertures, the shear pin being loosely journaled within the respective apertures.

1 10. The invention of Claim 9 further including a spring member to bias the shear pin to one side of the aperture.

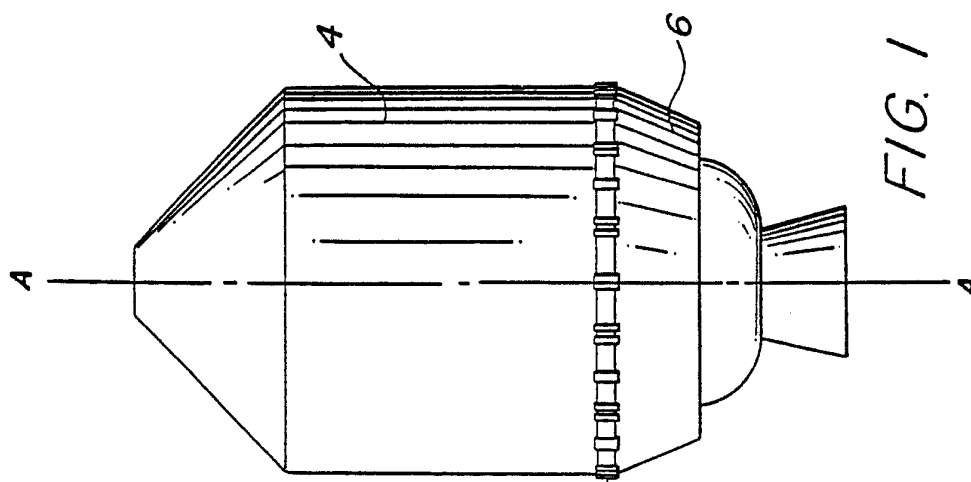


FIG. 1

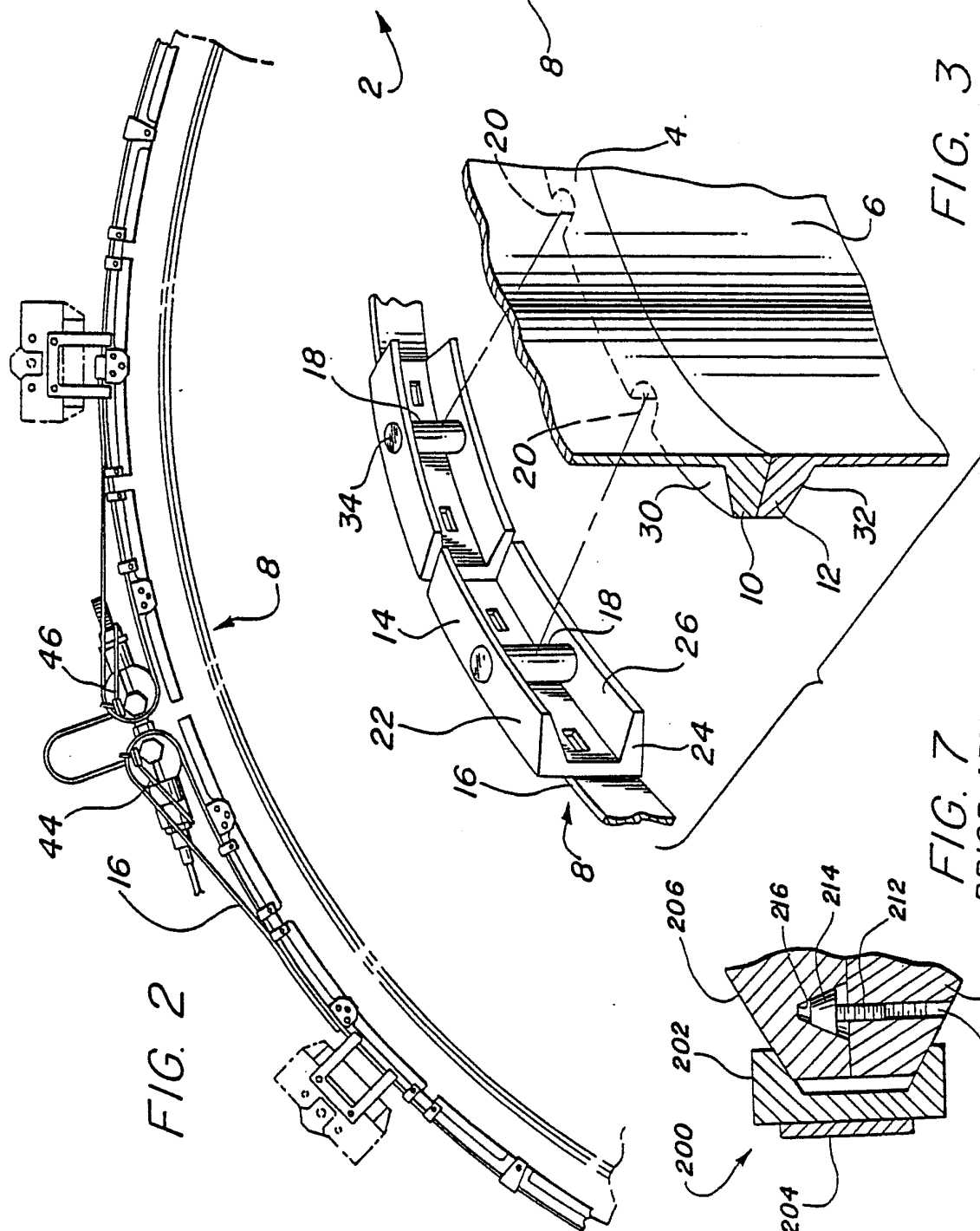


FIG. 3

FIG. 7
PRIOR ART

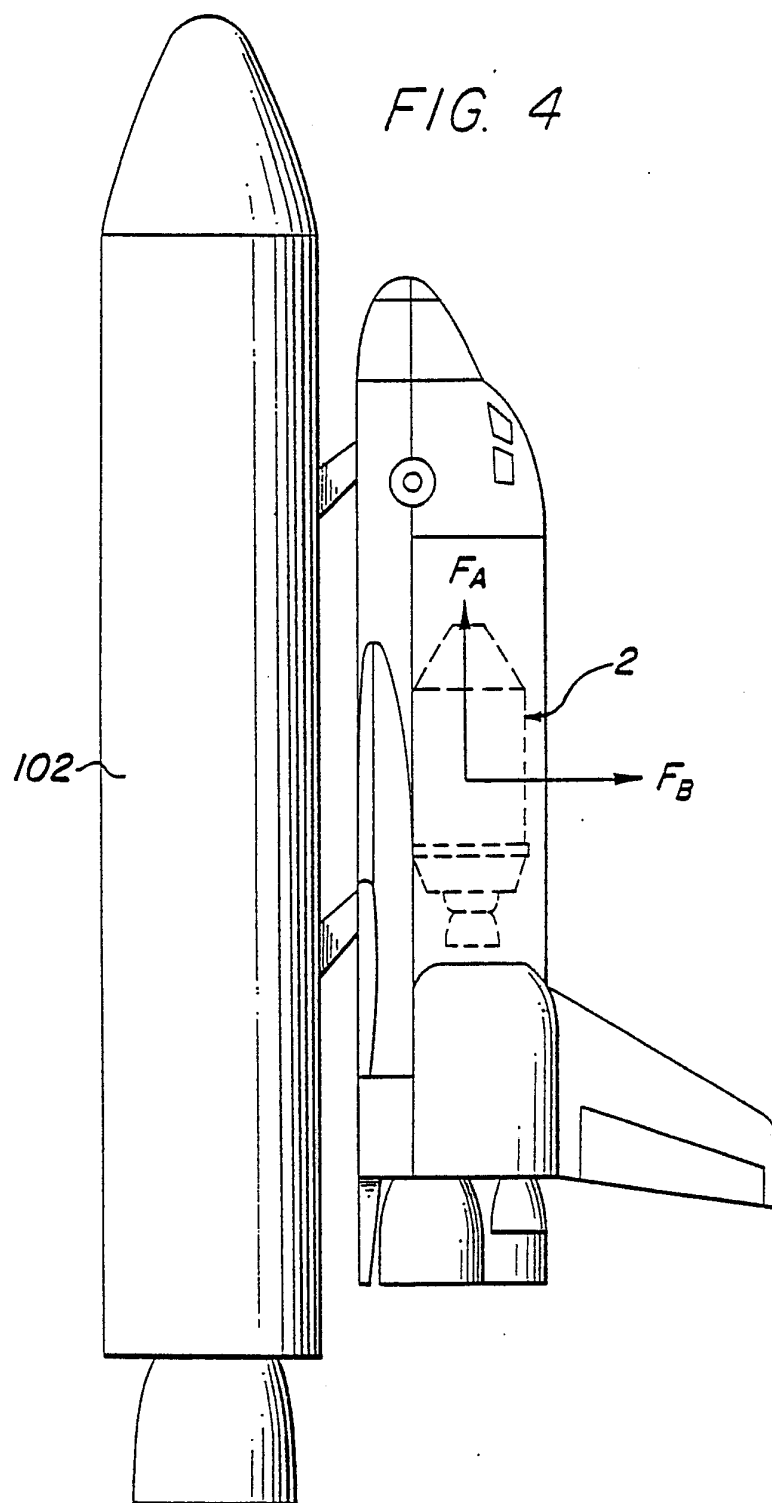


FIG. 5

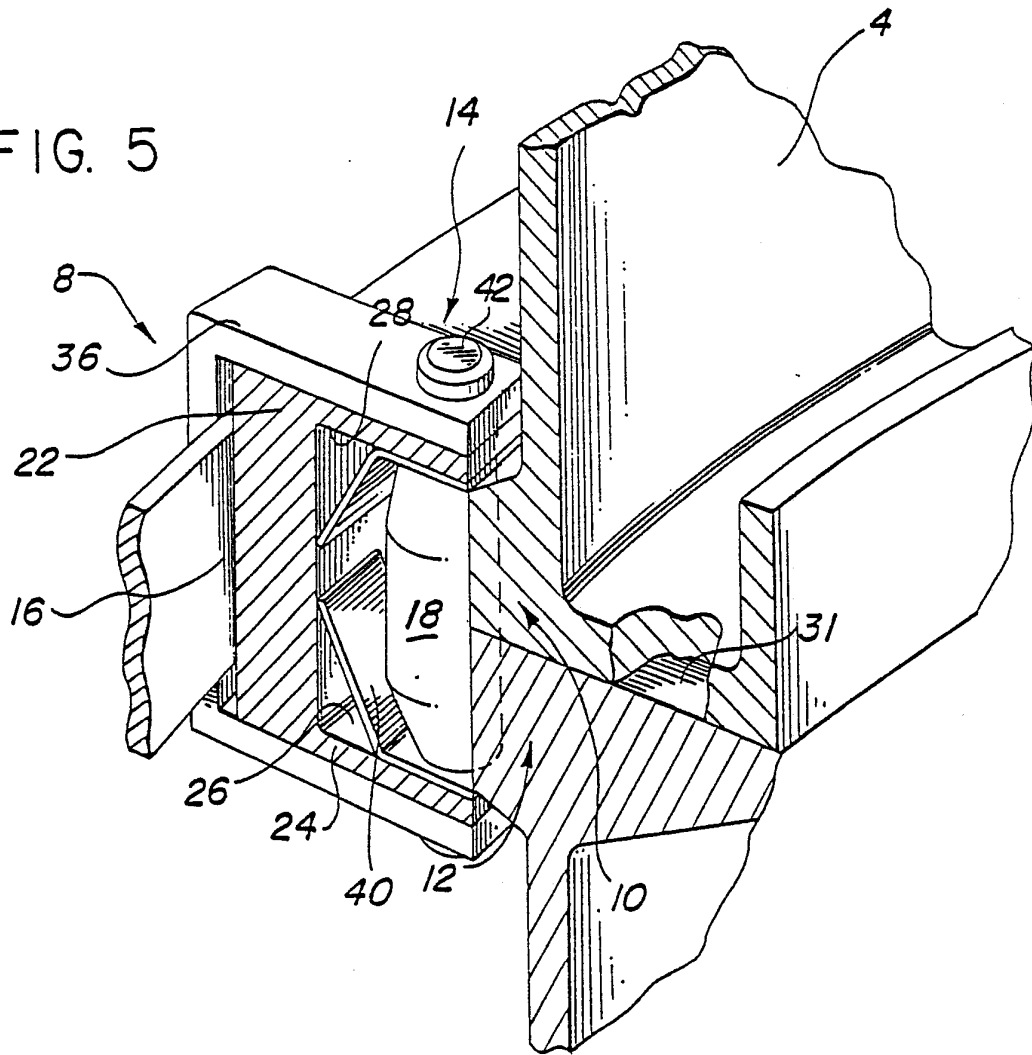


FIG. 6

