



(86) Date de dépôt PCT/PCT Filing Date: 2010/12/22
(87) Date publication PCT/PCT Publication Date: 2011/06/30
(85) Entrée phase nationale/National Entry: 2012/06/15
(86) N° demande PCT/PCT Application No.: EP 2010/070494
(87) N° publication PCT/PCT Publication No.: 2011/076849
(30) Priorité/Priority: 2009/12/23 (EP09180557.2)

(51) Cl.Int./Int.Cl. *H02M 3/22* (2006.01),
H02M 3/335 (2006.01)
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(54) Titre : CONVERTISSEUR CC/CC MIS A LA TERRE
(54) Title: GROUNDABLE DC/DC CONVERTER

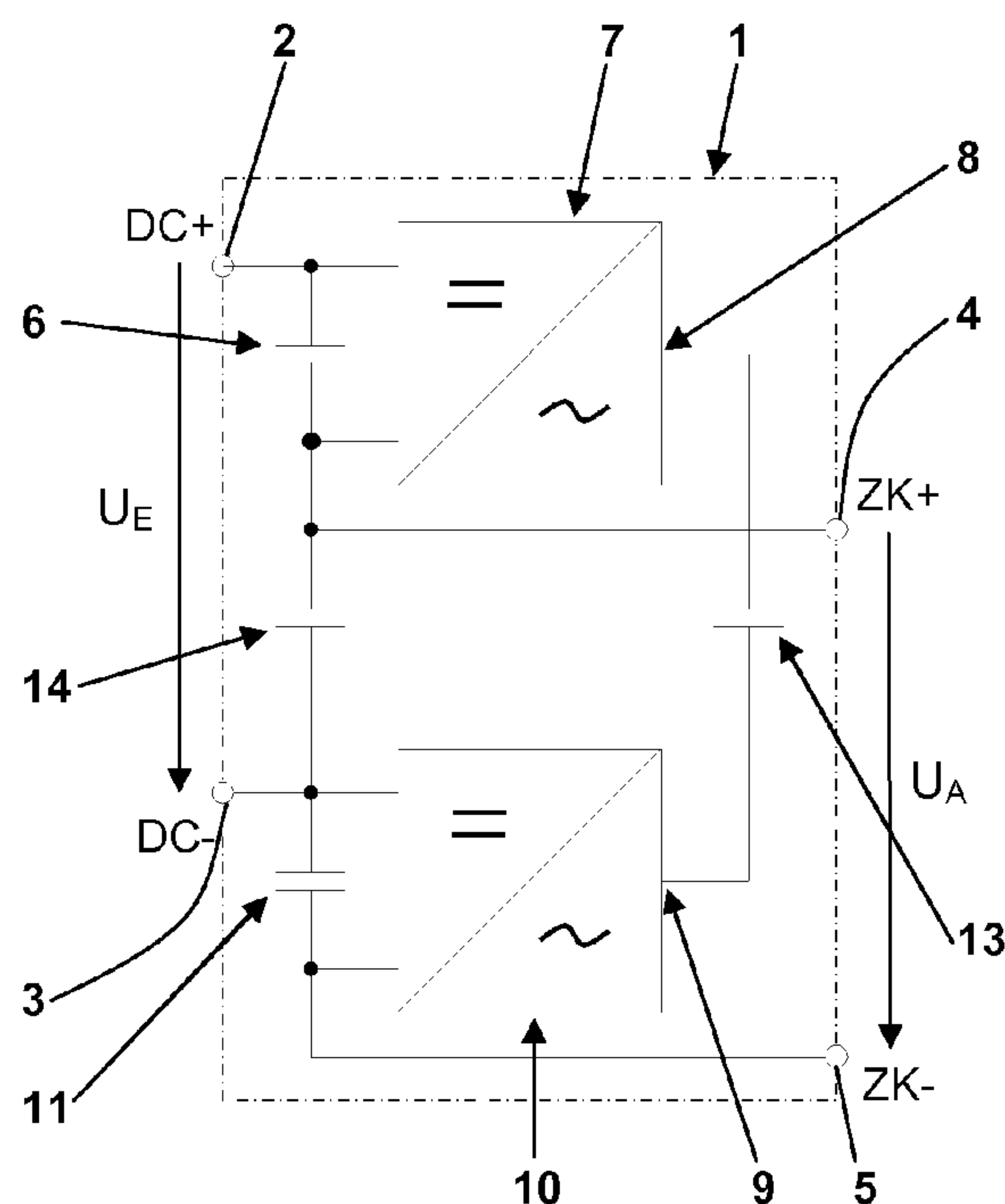


Fig. 1

(57) **Abrégé/Abstract:**

A DC/DC converter (1) comprises: two input terminals (2, 3) for a DC input voltage (U_E); two output terminals (4, 5) for a DC output voltage (U_A); an inverter (7) converting a DC voltage into an AC voltage; and a rectifier (10) converting an AC voltage from the

(57) **Abrégé(suite)/Abstract(continued):**

inverter into a DC voltage between a first one of the input terminals (3) and a first one of the output terminals (5). At least one galvanically isolating element is arranged between the output (8) of the inverter (7) and the input (9) of the rectifier (10), and a capacity is operative between the output terminals (4, 5). The inverter (7) converts a partial DC voltage being smaller than the full DC input voltage (UE) and dropping over a capacity (6) which is operative between the second one of the input terminals (2) and the second one of the output terminals (4).

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau(43) International Publication Date
30 June 2011 (30.06.2011)(10) International Publication Number
WO 2011/076849 A1(51) International Patent Classification:
H02M 3/22 (2006.01) *H02M 3/335* (2006.01)(21) International Application Number:
PCT/EP2010/070494(22) International Filing Date:
22 December 2010 (22.12.2010)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
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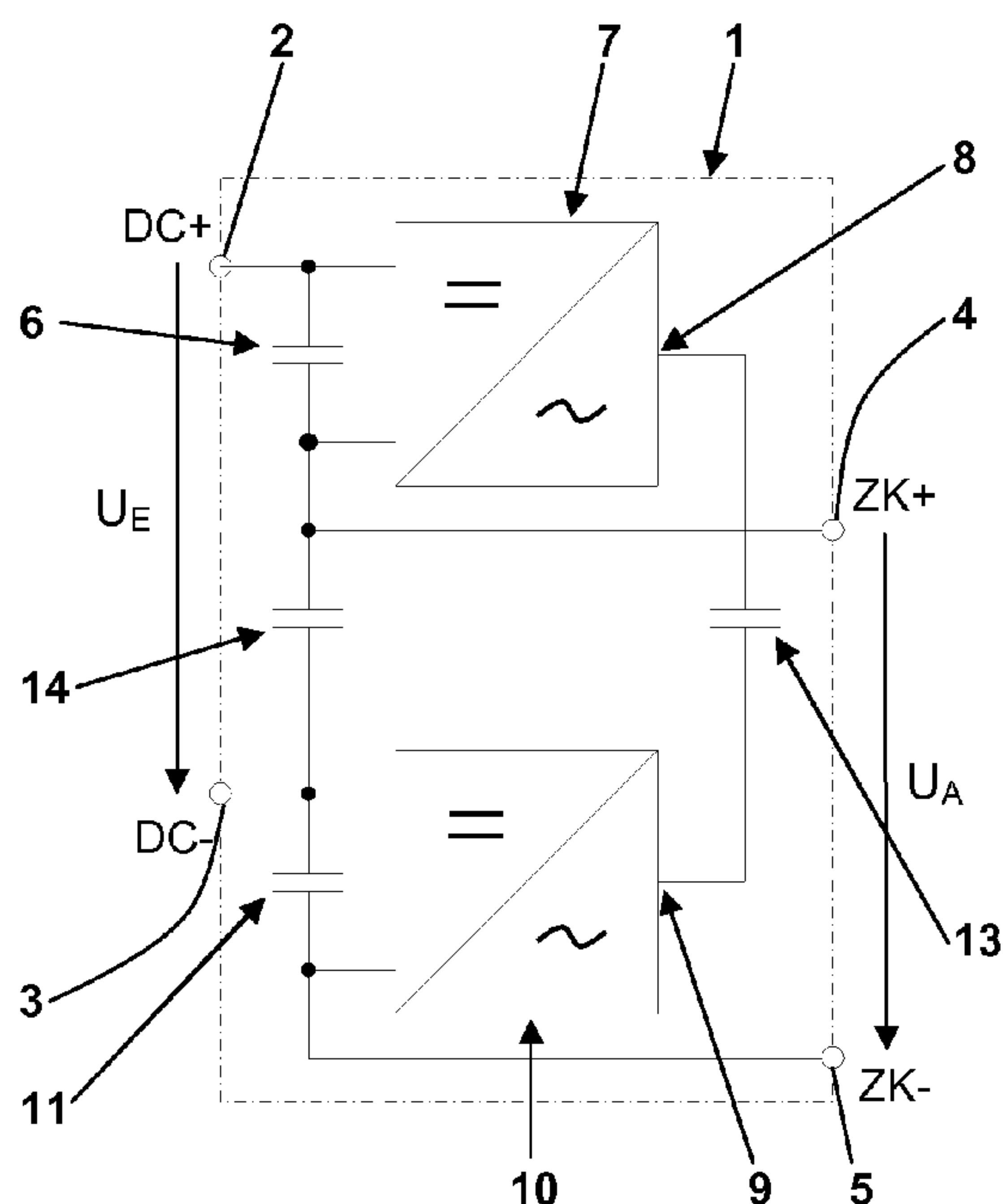
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(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PE, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK,

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(54) Title: GROUNDABLE DC/DC CONVERTER

**Fig. 1**(57) Abstract: A DC/DC converter (1) comprises: two input terminals (2, 3) for a DC input voltage (U_E); two output terminals (4, 5) for a DC output voltage (U_A); an inverter (7) converting a DC voltage into an AC voltage; and a rectifier (10) converting an AC voltage from the inverter into a DC voltage between a first one of the input terminals (3) and a first one of the output terminals (5). At least one galvanically isolating element is arranged between the output (8) of the inverter (7) and the input (9) of the rectifier (10), and a capacity is operative between the output terminals (4, 5). The inverter (7) converts a partial DC voltage being smaller than the full DC input voltage (U_E) and dropping over a capacity (6) which is operative between the second one of the input terminals (2) and the second one of the output terminals (4).

WO 2011/076849 A1



EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU,
LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK,
SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ,
GW, ML, MR, NE, SN, TD, TG).

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*before the expiration of the time limit for amending the
claims and to be republished in the event of receipt of
amendments (Rule 48.2(h))*

Published:

— *with international search report (Art. 21(3))*

GROUNDABLE DC/DC CONVERTER

CROSS REFERENCE TO RELATED APPLICATIONS

This application claims priority to co-pending European Patent Application No. EP 09 180 557.2 entitled "Erdungsfähiger DC/DC-Wandler", filed December 23, 2009.

FIELD OF THE INVENTION

The present invention generally relates to a DC/DC converter. Particularly the present invention generally relates to a DC/DC converter comprising: two input terminals for receiving a DC input voltage; two output terminals for providing a DC output voltage; an inverter converting a DC voltage into an AC voltage at its output; and a rectifier connected to the output of the inverter.

A DC/DC converter of this kind may be provided as part of an arrangement for feeding electrical energy from a photovoltaic power generator into a power grid. Here, the DC/DC converter may be connected to the input of an inverter which feeds the electrical energy coming from the photovoltaic power generator into an AC power grid. The present invention is not, however, confined to DC/DC converters for this specific application.

BACKGROUND OF THE INVENTION

Amongst other things, DC/DC converters may be used to convert a DC input voltage into a higher DC output voltage and/or to convert a unipolar input voltage into a bipolar output voltage.

In a DC/DC converter known from Yi-Cherng Lin; Der-Cherng Liaw: Parametric study of a resonant switched capacitor DC-DC converter, Electrical and Electronic Technology, 2001, TENCON. Proceedings of IEEE Region 10 International Conference, Volume 2, 2001,

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pages 710-716, an inverter half-bridge converts the DC input voltage applied between two input terminals into an AC voltage. This AC voltage is converted back into a DC voltage by a rectifier bridge comprising two diodes. The resulting DC voltage is applied between one of the two input terminals and one of two output terminals and thus increases the DC output voltage over the DC input voltage. Between the output of the inverter half-bridge and the input of the rectifier bridge a resonant circuit is formed which comprises a capacitor capacitively decoupling the rectifier half-bridge from the inverter bridge, and an inductor. The resonant circuit has a resonant frequency defined by its components. To the end of operating the DC/DC converter with the lowest possible losses, two switches in the inverter half-bridge are switched in phase opposition at this resonant frequency. It is also advantageous for low-loss operation in this known DC/DC converter that only half the electrical energy is fed through the inverter bridge, through the resonant circuit and through the rectifier bridge in order to achieve the desired doubling of the DC output voltage over the DC input voltage. However, the reference potential of the DC input voltage remains the same, in that whichever are the input and output terminals, between which the rectifier bridge does not increase the voltage, they are always at the same potential. Also, in view of the very high voltages which are produced by present-day photovoltaic systems, in order to reduce the current loading on conductors carrying power, there is not always any point in doubling the voltage such as performed by the known DC/DC converter.

EP 1 971 018 A1 discloses a DC/DC converter at the input of an inverter. In this DC/DC converter two capacitors which are connected in series and grounded at their center point are charged to provide a bipolar voltage between two output terminals. To this end, a boost converter which charges one of the two capacitors and an inverting buck-boost converter which charges the other capacitor are connected to two input terminals. Thus, the DC output voltage across the two capacitors has a basic conversion ratio of two relative to

the DC input voltage between the input terminals. As already mentioned, there is not always any point in this increase in voltage. However, it is useful that this known DC/DC converter converts a unipolar DC input voltage into a bipolar DC output voltage. As a result, one of the input terminals, which is connected to the connecting point of the two capacitors, can be grounded to only have, in a connected photovoltaic power generator, either positive or negative electric potentials relative to ground, as desired. Some photovoltaic power generators require such a potential regime for optimum performance and lifetime. However, another disadvantage of this known DC/DC converter is that the inverting buck-boost converter only performs the inversion when its switch is actually being opened and closed. Buck and boost converters, however, basically only operate at optimum efficiency if their switches are actuated as little as possible.

EP 2023475 A1 discloses a DC/DC converter at the input of a pulsed inverter for converting a DC input voltage provided by a grounded DC power source, particularly a photovoltaic generator, into an AC output voltage. The DC/DC converter comprises a resonant inverter converting the full DC input voltage into at least two bipolar intermediate output voltages. The bipolar intermediate output voltages are each supplied via a rectifier diode bridge to one part of a split DC voltage link, which has a grounded center and which the DC/DC converter shares with the pulsed inverter. Thus, the link voltage of the DC voltage link has a basic conversion ratio of two relative to the DC input voltage.

A need remains for a DC/DC converter which, with a minimum amount of apparatus and with minimal power losses, is capable of converting a unipolar DC input voltage into a bipolar DC output voltage without necessarily having to increase the DC voltage.

SUMMARY OF THE INVENTION

The present invention provides a DC/DC converter comprising: two input terminals for receiving a DC input voltage; two output terminals for providing a DC output voltage; an inverter converting a DC voltage into an AC voltage at its output; and a rectifier connected to the output of the inverter at its input end and connected between a first one of the input terminals and a first one of the two output terminals at its output end, the rectifier converting an AC voltage applied to its input into a DC voltage between the first one of the two input terminals and the first one of the two output terminals. In the DC/DC converter, at least one galvanically isolating element is being arranged between the output of the inverter and the input of the rectifier; a capacity is operative between the two output terminals; and the inverter converts a partial DC voltage dropping over a capacity which is operative between the second one of the two input terminals and the second one of the two output terminals, the partial DC Voltage being smaller than the full DC input voltage.

Other features and advantages of the present invention will become apparent to one with skill in the art upon examination of the following drawings and the detailed description. It is intended that all such additional features and advantages be included herein within the scope of the present invention, as defined by the claims.

BRIEF DESCRIPTION OF THE DRAWINGS

The invention can be better understood with reference to the following drawings. The components in the drawings are not necessarily to scale, emphasis instead being placed upon clearly illustrating the principles of the present invention. In the drawings, like reference numerals designate corresponding parts throughout the several views.

Fig. 1 is a schematic view of the construction of a first embodiment of the DC/DC converter

Fig. 2 is a schematic view of the construction of a second embodiment of the DC/DC converter having a different capacity layout from that shown in Fig. 1.

Fig. 3 shows further details of the embodiment of the DC/DC converter shown in Fig. 1.

5 **Fig. 4** shows further details of the embodiment of the DC/DC converter shown in Fig. 2.

Fig. 5 shows a possible way in which a circuit of the DC/DC converter shown in Fig. 3 or 4 which serves as a start-up circuit may be implemented.

10 **Fig. 6** shows another possible way of implementing the circuit which serves as a start-up circuit.

Fig. 7 shows yet another possible way of implementing the circuit which serves as a start-up circuit.

Fig. 8 shows yet another possible way of implementing the circuit which serves as a start-up circuit.

15 **Fig. 9** shows a modification of the DC/DC converter shown in Fig. 3.

Fig. 10 is a schematic view of a further embodiment of the novel DC/DC converter.

Fig. 11 is a schematic view of yet another embodiment of the novel DC/DC converter which has an amended capacity arrangement as compared to that shown in Fig. 10.

Fig. 12 shows an embodiment of the DC/DC converter which has a transformer.

20 **Fig. 13** shows further details of the embodiment of the DC/DC converter shown in Fig. 10.

Fig. 14 shows further details of the embodiment of the DC/DC converter shown in Fig. 11.

25 **Fig. 15** shows a first more detailed embodiment of the DC/DC converter shown in Fig. 12.

Fig. 16 shows a second more detailed embodiment of the DC/DC converter shown in Fig. 12.

Fig. 17 shows a possible way of using a signal from a differential current transformer in the circuit which acts as a start-up circuit, in a further more detailed embodiment of the DC/DC converter shown in Fig. 1.

Fig. 18 shows a further possible way of using a signal from a differential current transformer in the circuit which acts as a start-up circuit, in the DC/DC converter shown in Fig. 3.

Fig. 19 shows a control algorithm for a set of control logic controlling the circuit shown in Fig. 17 or Fig. 18 which acts as a start-up circuit.

DETAILED DESCRIPTION

Where the term inverter is used in the following description, it includes, except where otherwise specified, everything that a person skilled in the art may understand by this term. The term inverter thus covers particularly, but not exclusively, inverters which have, between two input lines, an inverter bridge which has at least one half-bridge constructed from actively switched switches.

Where the term rectifier is used in the following description, it includes, except where otherwise specified, everything that a person skilled in the art may understand by this term. The term rectifier thus covers particularly, but not exclusively, rectifiers which have, taken off from two output lines, a rectifier bridge which has at least one half-bridge constructed from rectifying diodes.

In this context, it should be noted that, within the scope of the present invention, any diode acting as a element which switches purely passively may be replaced by a switch which is actively switched in the appropriate way, or by a switch which is actively switched in

the appropriate way and which has an inherent or external anti-parallel diode, or by the inherent diode of an actively switchable semiconductor switch, as this does not cause the DC/DC converter to operate in any fundamentally different way. Equivalent circuits of this kind for a diode are familiar to those skilled in the art and are therefore covered in the following description by the term diode.

Where the term capacity is used in the following description, it includes, except where otherwise specified, everything that a person skilled in the art may recognise as providing an electric capacity. The term capacity thus covers particularly, but not exclusively, any combination of one or more capacitors.

Where the term inductance is used in the following description, it includes, except where otherwise specified, everything that a person skilled in the art may recognise as providing an electric inductance. The term inductance thus covers particularly, but not exclusively, any combination of one or more inductors.

In the DC/DC converter according to the present invention, the inverter does not convert the entire DC input voltage into the AC voltage at its output but only a partial DC voltage, i. e. a part of the DC input voltage dropping over a capacity which is operative between the second one of the two input terminals and the second one of the two output terminals, between which second terminals the DC voltage at the output end of the rectifier is not applied. In particular, this capacity is connected directly between the second one of the two input terminals and the second one of the two output terminals. Because this capacity and the inverter are connected in parallel between the second one of the two input terminals and the second one of the two output terminals, the potential at the second one of the two output terminals relative to the second one of the two input terminals is shifted towards the first one of the two input terminals. At the same time, the potential at the first one of the two output terminals relative to the first one of the two input terminals is shifted away from the

second one of the two input terminals. The output voltage is thus on both sides of the potential of the first one of the two input terminals. If, for whatever reason, this first one of the two input terminals is grounded, a unipolar DC input voltage becomes a bipolar DC output voltage. As a result, despite the different potential reference, the absolute value or
5 magnitude of the DC output voltage remains basically the same as that of the DC input voltage.

In the DC/DC converter, a further capacity may be connected in parallel with the rectifier at its output end between the first one of the two input terminals and first one of the two output terminals.

10 The further capacity which is connected between the first one of the two input terminals and the first one of the output terminals in parallel with the output of the rectifier may form part of that capacity which is operative between the output terminals of the DC/DC converter in that an even further capacity is connected between the second one of the output terminals and the first one of the input terminals in series with the further capacity. A
15 plurality of different arrangements of individual capacities is possible in the DC/DC converter.

If a capacity is connected in parallel with the rectifier at the output end between the first one of the two input terminals and the first one of the two output terminals, it may be divided into two partial capacities, in which case a center between the two partial capacities may be connected via an inductance to the input of the rectifier. This inductance may be
20 used for the purpose of switching switches of the inverter at a voltage of zero or at least close to zero (zero voltage switching (ZVS)). In the DC/DC converter, an inductance of this kind may generally be connected in series with a capacity between each one of the individual inverter output terminals or individual rectifier input terminals and one of the input terminals or output terminals.

25 The connection of the output of the inverter to the input of the rectifier preferably

takes place via a resonant circuit. This resonant circuit may comprise a capacity and an inductance. Alternatively, the coupling between the inverter and the rectifier may take place via a transformer with which a capacity may be connected in series to form a resonant circuit with the stray inductance of the transformer. To avoid the effect which high tolerances on the stray inductance may have, the capacity may be connected in series with a further inductance. If there is a resonant circuit between the inverter and the rectifier, the actuation of the switches of the inverter preferably takes place at a duty cycle of close to 50% and at a frequency close to the resonant frequency. In this case, the switched states of the DC/DC converter are independent of the switched states of any inverter which may be connected downstream of the DC/DC converter. The rectifier may have switches connected in parallel to enable a bidirectional flow of power to take place and/or to reduce the losses in the rectifier.

It is also possible for a plurality of resonant circuits to be formed between the output of the inverter and the input of the rectifier, like, for example, as one resonant circuit per each half-bridge of the inverter. Preferably, these different resonant circuits all have a same resonant frequency and are operated in an interleaved switching mode. If they are each connected to one half-bridge of the rectifier, they may be inductively coupled, for example, at the input of the rectifier.

To the end of achieving a high efficiency of the DC/DC converter, the attenuation between the inverter and the rectifier should be as low as possible. As a result, very high currents would flow when the switches of the inverter were switched for the first time, if the capacity lying parallel to the input of the inverter had already been charged whereas the capacity lying parallel to the output of the rectifier had not been charged. Further, the switches of the inverter would have to be switch a very high voltage, which is disadvantageous. To avoid both problems in the DC/DC converter, the capacity which is

connected between the second one of the two input terminals and the second one of the two output terminals is preferably connected in parallel with a circuit by which the voltage across this capacity can be reduced. In the simplest case, this circuit is a switch which short-circuits the capacity via a resistor. As a particular preference, the said switch is a switch of a normally conductive type which is not opened until the switches of the inverter are already being operated, which means that the switches of the inverter initially switch at a voltage of zero because no voltage has built up across the capacity yet. In this way, the circuit is used as a start-up circuit in the DC/DC converter. Even if the voltage across the capacity builds up slowly, the switches of the inverter may still be switched at a current of or close to zero, if the inverter feeds one or more resonant circuits.

The circuit by which the voltage across the capacity which is connected between the second one of the two input terminals and the second one of the two output terminals can be reduced may also deliberately change the voltage which drops between the first one of the two input terminals and the second one of the two output terminals and in this way may have at least some effect on the voltage division in the DC/DC converter. For this purpose, the circuit has one inductance and at least one diode in addition to the at least one switch.

Specifically, the switch in the circuit may be actuated in such a way that either the electric potentials relative to earth at the two input terminals are of a same sign, or one of these electric potentials is at least close to zero. Without the circuit, a presetting of this kind of the input potentials of the novel DC/DC converter can be achieved by connecting one of the input terminals to ground or to a neutral conductor, or to a potential which is defined with the help of, for example, a voltage divider. This connection preferably takes place via a resistor and/or an inductance, and a relay by which the connection can be disrupted if required. One reason for presetting a positive potential for both the input terminals may be to prevent negative potentials in a photovoltaic power generator which is connected to the input

end of the DC/DC converter, because negative potentials can be a disadvantage to certain solar cells. In other cases it may be preferable to avoid positive potentials at the input end of the DC/DC converter.

Alternatively, the actuation of the switches of the circuit may take place as a function
5 of a signal from a sensor which senses a current to ground like, for example, a leakage current to ground from one of the output terminals of the DC/DC converter. This sensor may be arranged directly at the output of the DC/DC converter but may equally well be arranged at the output of an inverter connected downstream of the DC/DC converter. The sensor may be a known differential current sensor which responds to the differential current over the
10 lines that are monitored. The actuation of the switches of the circuit is performed with the aim of reducing the leakage current to zero if possible. A particular preference is regulating the current to ground by varying the duty cycle of the switches in the circuit.

Referring now in greater detail to the drawings, the DC/DC converter 1 which is shown in **Fig. 1** has two input terminals 2 and 3 and two output terminals 4 and 5. The input
15 terminals 2 and 3 are provided for application of a DC input voltage U_E . In the present case, the input terminal 2 receives the positive pole at a potential $DC+$ of the input voltage U_E , and the input terminal 3 receives the negative pole at a potential $DC-$ of the input voltage U_E . At the output terminals 4 and 5, the DC/DC converter 1 provides a DC output voltage U_A . In the present case, the output terminal 4 provides the positive pole at a potential $ZK+$ of the
20 output voltage U_A , and the output terminal 5 provides the negative pole at a potential $ZK-$ of the output voltage U_A . A capacity 6 is connected between the input terminal 2 and the output terminal 4. The DC voltage drop over this capacity 6 is converted by an inverter 7 into an AC voltage. Via a coupling capacity 13, the output 8 of the inverter 7 is connected to the input 9 of a rectifier 10 which converts the AC voltage into a DC voltage which is applied between
25 the input terminal 3 and the output terminal 5. A capacity 11 is connected between the input

terminal 3 and the output terminal 5 in parallel with the rectifier 10. A further capacity 14 is connected between the input terminal and the output terminal 4. A series connection of the capacities 11 and 14 is thus operative between the output terminal 5 and the output terminal 4. The way in which the DC/DC converter 1 operates can be explained by saying that the input voltage U_E partially drops over the capacity 6 and partially drops over the capacity 14, and that the part of the voltage drop which is more distant from the potential DC- at the input terminal 3 is transmitted to the capacity 11 by means of the inverter 7 and the rectifier 10, and that the output voltage U_A across the capacities 11 and 14 is thus shifted with regard to earth potential in relation to the input voltage U_E . As a result, the potential DC- of the input voltage U_E , which is applied to the input terminal 3, can be connected to ground such that a unipolar positive DC input voltage U_E is converted into a bipolar output voltage U_A .

This function is also performed by the DC/DC converter 1 which is shown in **Fig. 2**, in which, rather than the capacity 14 shown in Fig. 1, a capacity 15 is provided between the input terminals 2 and 3, and a capacity 12 is provided between the output terminals 4 and 5. One of these two capacities 12 and 15 may also be omitted here, as a capacity always remains operative between the output terminals 4 and 5. If the capacity 12 is omitted, the capacity in question between the output terminals 4 and 5 is made up of contributions by the capacities 6, 11 and 15.

Further details of the DC/DC converter 1 according to Fig. 1 are shown in **Fig. 3**. Additionally, a boost converter 16 is connected upstream of the DC/DC converter 1. Besides a switch 17, an inductance 18 and a diode 19, the boost converter 16 comprises a buffer capacity 20, and it boosts, as required, an input voltage U_E' to the input voltage which is applied between the input terminals 2 and 3 of the DC/DC converter 1. The inverter 7 takes the form of a half-bridge 21 having two switches 22 and 23 which are switched in phase opposition. The rectifier 10 is constructed from two diodes 25 and 26 in the form of a half-

bridge 24. Further, the coupling capacity 13 which isolates the output 8 of the inverter 7 from the input 9 of the rectifier 10 is connected in series with an inductance 27 which, together with the coupling capacity 13, forms a resonant circuit 28 at whose resonant frequency the switches 22 and 23 are switched. The capacity 11 which is connected between the input terminal 3 and the output terminal 5 in parallel with the rectifier 10 is divided into two partial capacities 11' and 11". An inductance 29 is connected between a connecting point of these partial capacities 11' and 11" and the input 9 of the rectifier 10. In this way, the inductance 29 is connected to the output terminal 5 via the partial capacity 11' and assists in switching the switches 22 and 23 of the inverter 7 at zero crossings of the voltage in the resonant circuit 28. Further, a circuit 30 which acts as a start-up circuit and which will be explained in more detail in connection with Figs. 5 and 8, is indicated.

The circuit layout shown in **Fig. 4** differs from that one shown in Fig. 3 in that the capacity 14 is omitted and that instead the capacities 12 and 15 are connected between the output terminals 4 and 5 and the input terminals 2 and 3, respectively (cf. Fig. 3). The capacity 11 is also omitted and instead the inductance 29 is connected to the output terminal 5 via a capacity 55.

Fig. 5 shows a first embodiment of the circuit 30 according to Figs. 3 and 4. Contrary to what is shown in Fig. 3, this circuit 30 is not connected to the potential DC- of the input terminal 3. In the present case, the circuit 30 has a switch 31 of the normally on or conductive type, which, in series with a resistor 32, is connected in parallel with the capacity 6 (not shown) between the input terminal 4 and the output terminal 5. For as long as control logic 33 does not open the switch 31, the switch 31 short-circuits the capacity 6 via the resistor 32. As a result, no voltage can build up across the capacity 6. In this way, operation of the switches 22 and 23 of the inverter 7 may start with no voltage present. This is directly beneficial for the switching of the switches 22 and 23. Further, the current flowing from the

output 8 of the inverter 7 to the input 9 of the rectifier 10 can be kept to a suitable low level at the beginning of the operation of the switches 22 and 23, even if the capacities on both sides of the switches are not yet equally loaded. Further, the start-up circuit 30 prevents that the full input voltage U_E drops over the capacity 6 rather than, as desired, only a part of the input voltage U_E .

Fig. 6 shows a variant of the circuit 30 shown in Fig. 5 in which the switch 31 is of the normally off type instead of the normally on or conductive type and thus has to be actively closed at first by the control logic 33. The way in which the circuit 30 shown in Fig. 6 operates as a start-up circuit is fundamentally the same as that in which the circuit shown in Fig. 5 operates.

The circuit 30 shown in **Fig. 7** additionally has an inductance 34 and a diode 35 but no resistor 32. The inductance 34 is connected between the input terminal 2 and the output terminal 4 in series with the switch 31, whereas the diode 35 is connected between the input terminal 3 and the output terminal 4 in series with the inductance 34. In this way, a boost converter for the output potential ZK^+ is formed, by which the level of the output potential ZK^+ can be set in the range between the potentials $(DC^+ + DC^-/2)$ and DC^+ .

In the circuit 30 shown in **Fig. 8**, an additional switch 36 and an additional diode 37 are provided which, together, allows for setting the output potential ZK^+ at the output terminal 4 in the range between the input potentials DC^- and DC^+ .

Fig. 9 shows a layout which is fundamentally the same as in Fig. 3 except that in this case the polarity of the input voltage U_E is reversed, i.e. the DC^- potential is at the input terminal 2 and the DC^+ potential is at the input terminal 3. Hence the output potential ZK^- is present at the output terminal 4 and the output potential ZK^+ is present at the output terminal 5. In conjunction with grounding the input terminal 3, this prevents positive potentials relative to ground in a photovoltaic generator 38 which supplies the input voltage U_E' , whereas the

previous embodiments, if grounded in this way, prevented negative potentials relative to ground at the input side. Further, Fig. 9 shows an inverter 39 connected to the output terminals 4 and 5. This inverter 39 is connected to ground via the DC+ potential and feeds the electrical energy from the photovoltaic system 38 into a three-phase AC network 40
5 having a ground reference.

In the inverter 1 which is shown in **Fig. 10**, two lines run between the output 8 of the rectifier 7 and the input 9 of the rectifier 10. In each of these lines one of two coupling capacities 13' and 13'' is arranged which are responsible for isolation. The embodiment of DC/DC converter shown in **Fig. 11** likewise comprises this feature and differs from that one
10 shown in Fig. 10 only in that it has a capacity arrangement corresponding to Fig. 2 rather than Fig. 1.

With the basic capacity arrangement shown in Fig. 11 but with the capacity 12 omitted, **Fig. 12** shows an alternative isolation of the output 8 of the inverter 7 from the input 9 of the rectifier 10 by means of a transformer 41.

The embodiment of the basic circuit shown in Fig. 10 which is shown in **Fig. 13** comprises the inverter 7 taking the form of a full bridge comprising two half-bridges 21' and 21'' having switches 22' and 23', and 22'' and 23'', respectively. In this case, each half-bridge 21 feeds power in a one of two resonant circuits 28' and 28'' each having an inductance 27' or 27'' and a coupling capacity 13' or 13''. These resonant circuits 28 are connected to
20 corresponding half-bridges 24' and 24'' of the rectifier 10 which are constructed from diodes 25' and 26', or 25'' and 26''. The two half-bridges are coupled on the input side by an inductance 55 which basically functions in the same way as the inductance 29 shown in Fig. 3 or 4. In this way, the two resonant circuits 28' and 28'' are inductively coupled to stabilise their opposing-phase oscillations caused by the pairs of switches 22' and 23'', and 22'' and
25 23', which are switched in phase opposition.

Except for the capacity arrangement and the fact that, in place of the inductance 56, an inductance 53 is directly connected between the outputs of the inverter in series with a capacity 54, the construction of the DC/DC converter 1 shown in **Fig. 14** corresponds to that one of the DC/DC converter shown in Fig. 13. (In the DC/DC converter 1 shown in Fig 13 the coupling capacities 13' and 13'' act as capacities between the outputs of the inverter.)

In the embodiment of the DC/DC converter 1 shown in **Fig. 15**, the rectifier 7 is formed by a half-bridge 21' having two switches 22 and 23 and a half-bridge 21'' having two capacities 42 and 43. Together with the primary winding 44 of the transformer 41, these capacities 42 and 43 form a resonant circuit which is fed by the inverter 7. The secondary winding 45 of the transformer 41 feeds the rectifier 10, which in this case has a half-bridge 24 comprising the diodes 25 and 26 and a half-bridge 24'' comprising the capacities 46 and 47. In view of the capacities 46 and 47 and the capacity 15, the capacities 11 and 12 are not needed in this case. As an alternative to the capacity 12, the capacity 15 could equally well be dispensed with.

In the embodiment of the DC/DC converter 1 shown in **Fig. 16**, the two half-bridges 21'' and 24'' of the inverter 7 and the rectifier 10 are not constructed in a passive form from capacities 42 and 43, and 46 and 47, respectively but, like the half-bridges 21' and 24', are constructed from switches 22'' and 23'', and diodes 25'' and 26'', respectively. The capacity 13 is provided together with the primary winding 44 of the transformer 41 to form the resonant circuit 28 in this case.

The DC/DC converter 1 which is shown in **Fig. 17** and which is connected to a photovoltaic generator 38 at the input end and to an AC power grid 40, via an inverter 39, at the output end, is basically constructed as shown in Fig. 1. An inductance 57, which is connected at one of its ends to the centre of the sole half-bridge 21 of the inverter 7 and which, like the inductance 29 which is shown in Fig. 4 to be connected to the output terminal

5 via the capacity 55, serves for ZVS, is connected at its other end to the input terminal 2 via a capacity 58. Fig. 17 also shows how account is taken of a signal 48 from a sensor 49 by the circuit 30 of the DC/DC converter 1. As a measure of an uncompensated current to earth from the DC/DC converter 1, the sensor 49 uses a differential current transducer 50 to sense an ground leakage current flowing over the output terminals of the DC/DC converter 1. The control logic of the start-up circuit 30 processes the signal 48 as an input signal and controls the switch or switches of the circuit 30 in an appropriate way to reduce the current to ground to zero.

Whereas the differential current transducer shown in Fig. 17 senses the ground leakage current directly at the output of the DC/DC converter 1, the differential current transducer 50 shown in **Fig. 18** is provided at the output of the inverter 39 which is connected downstream of the DC/DC converter, where it likewise senses the current to ground from the DC/DC converter 1 but can, in a known manner, also be used for other monitoring tasks.

Fig. 19 shows an embodiment of the control logic 33 for the circuit 30 shown in Fig. 17 or Fig. 18 to allow the current to ground sensed by the sensor 49 to be reduced to zero. The signal 48 from the sensor 49 serves as an error signal relative to the preset value of zero. A controller 51, which may be a P+R or a PI controller or any other suitable controller, acts on the pulse width modulating means 52 in order to set the duty cycle, i.e. the proportion of time for which the switch 31 is closed per cycle, for the purpose of regulating the signal 49 to zero. In this way, the circuit 30 is used in the novel DC/DC converter 1 as an auxiliary converter for compensating for current to ground. In other words, it performs a function even during the ongoing operation of the DC/DC converter 1 and is not used only to ensure that the DC/DC converter 1 starts operating safely. In this way, it is even possible to have two different circuits 30 provided in parallel to one another. One of these two different

circuits 30 acts as a pure start-up circuit and is constructed for example as shown in Fig. 5 or 6, and the other of these two different circuits 30 is adapted for the task of acting as an auxiliary converter for compensating for current to earth and is constructed for example as shown in Fig. 5 or 6.

5 Many variations and modifications may be made to the preferred embodiments of the invention without departing substantially from the spirit and principles of the invention. All such modifications and variations are intended to be included herein within the scope of the present invention, as defined by the following claims.

LIST OF REFERENCE NUMERALS

	1	DC/DC converter	31	Switch
	2	Input terminal	32	Resistor
5	3	Input terminal	33	Control logic
	4	Output terminal	34	Inductance
	5	Output terminal	35	Diode
	6	Capacity	36	Switch
	7	Inverter	37	Diode
10	8	Output	38	Photovoltaic generator
	9	Input	39	Inverter
	10	Rectifier	40	AC network
	11	Capacity	41	Transformer
	12	Capacity	42	Capacity
15	13	Capacity	43	Capacity
	14	Capacity	44	Primary winding
	15	Capacity	45	Secondary winding
	16	Boost converter	46	Capacity
	17	Switch	47	Capacity
20	18	Inductance	48	Signal
	19	Diode	49	Sensor
	20	Capacity	50	Differential current transducer
	21	Half-bridge	51	Controller
	22	Switch	52	Pulse width modulating means
25	23	Switch	53	Inductance
	24	Half-bridge	54	Capacity
	25	Diode	55	Capacity
	26	Diode	56	Inductance
	27	Inductance	57	Inductance
30	28	Resonant circuit	58	Capacity
	29	Inductance		
	30	Circuit		

CLAIMS

- 1 1. A DC/DC converter (1) comprising:
- 2 - two input terminals (2, 3) for receiving a DC input voltage (U_E),
- 3 - two output terminals (4, 5) for providing a DC output voltage (U_A),
- 4 - an inverter (7) converting a DC voltage into an AC voltage at its output (8), and
- 5 - a rectifier (10) connected to the output (8) of the inverter (7) at its input end and
- 6 connected between a first one of the input terminals (3) and a first one of the two output
- 7 terminals (5) at its output end, the rectifier converting an AC voltage applied to its input (9) into a
- 8 DC voltage between the first one of the two input terminals (3) and the first one of the two
- 9 output terminals (5),
- 10 - at least one galvanically isolating element being arranged between the output (8) of the
- 11 inverter (7) and the input (9) of the rectifier (10), and
- 12 - a capacity being operative between the two output terminals (4, 5),
- 13 wherein the inverter (7) converts a partial DC voltage dropping over a capacity (6) which is
- 14 operative between the second one of the two input terminals (2) and the second one of the two
- 15 output terminals (4), the partial DC Voltage being smaller than the full DC input voltage (U_E).
- 1 2. The DC/DC converter (1) of claim 1, wherein the at least one galvanically isolating
- 2 element is a capacitor (13) or a transformer (41).
- 1 3. The DC/DC converter (1) of claim 2, wherein at least one resonant circuit (28) is formed
- 2 between the output (8) of the inverter (7) and the input (9) of the rectifier (10).

1 4. The DC/DC converter (1) of claim 3, wherein one resonant circuit (28) is formed between
2 the output (8) of the inverter (7) and the input (9) of the rectifier (10) per each half-bridge (21) of
3 the inverter (7).

1 5. The DC/DC converter (1) of claim 4, wherein all resonant circuits (28) between the
2 output (8) of the inverter (7) and the input (9) of the rectifier (10) have a same resonant
3 frequency.

1 6. The DC/DC converter (1) of any of the preceding claims, wherein individual output
2 terminals of the inverter are connected to each other via at least one inductance (56, 53) and at
3 least one capacity (13, 54).

1 7. The DC/DC converter (1) of any of the preceding claims, wherein each individual output
2 terminal of the inverter and/or each individual input terminal of the rectifier is connected to one
3 of the input terminals (2, 3) or output terminals (4, 5) via an inductance (29, 57) and a capacity
4 (55, 58).

1 8. The DC/DC converter (1) of any of the preceding claims, wherein the actuation of
2 switches (22, 23) of the inverter (7) is performed at a duty cycle between 30% and 50%
3 regardless of the switched states of converters connected downstream.

1 9. The DC/DC converter (1) of any of the preceding claims, wherein the capacity (6) which
2 is operative between the second one of the two input terminals (2) and the second one of the
3 two output terminals (4) is connected in parallel with at least one circuit (30) for deliberately
4 varying the voltage drop over the capacity (6).

1 10. The DC/DC converter (1) of claim 9, wherein the voltage drop over the capacity (6)
2 which is operative between the second one of the two input terminals (2) and the second one of
3 the two output terminals (4) is reducible towards zero by the circuit (30).

1 11. The DC/DC converter (1) of claim 9 or 10, wherein the circuit (30) has at least one switch
2 (31, 36).

1 12. The DC/DC converter (1) of claim 11, wherein the circuit (30) has one inductance (34)
2 and at least one diode (35, 37).

1 13. The DC/DC converter (1) of any of the preceding claims, wherein electric potentials of
2 the two input terminals (2, 3) relative to ground have a same signs or one of these electric
3 potentials is zero.

1 14. The DC/DC converter (1) of claim 12, wherein, in one mode of operation of the circuit
2 (30), a signal (48) from a sensor (49) which senses a current to earth has an impact on a control
3 logic (33) of the circuit (30).

1 15. The DC/DC converter (1) of claim 13 and 14, wherein the sensor (49) senses the
2 current to earth, that is a leakage current from one of the output terminals (4, 5) of the
3 DC/DC converter (1), directly at the output of the DC/DC converter (1) or at the output of an
4 inverter (39) connected downstream of the DC/DC converter.

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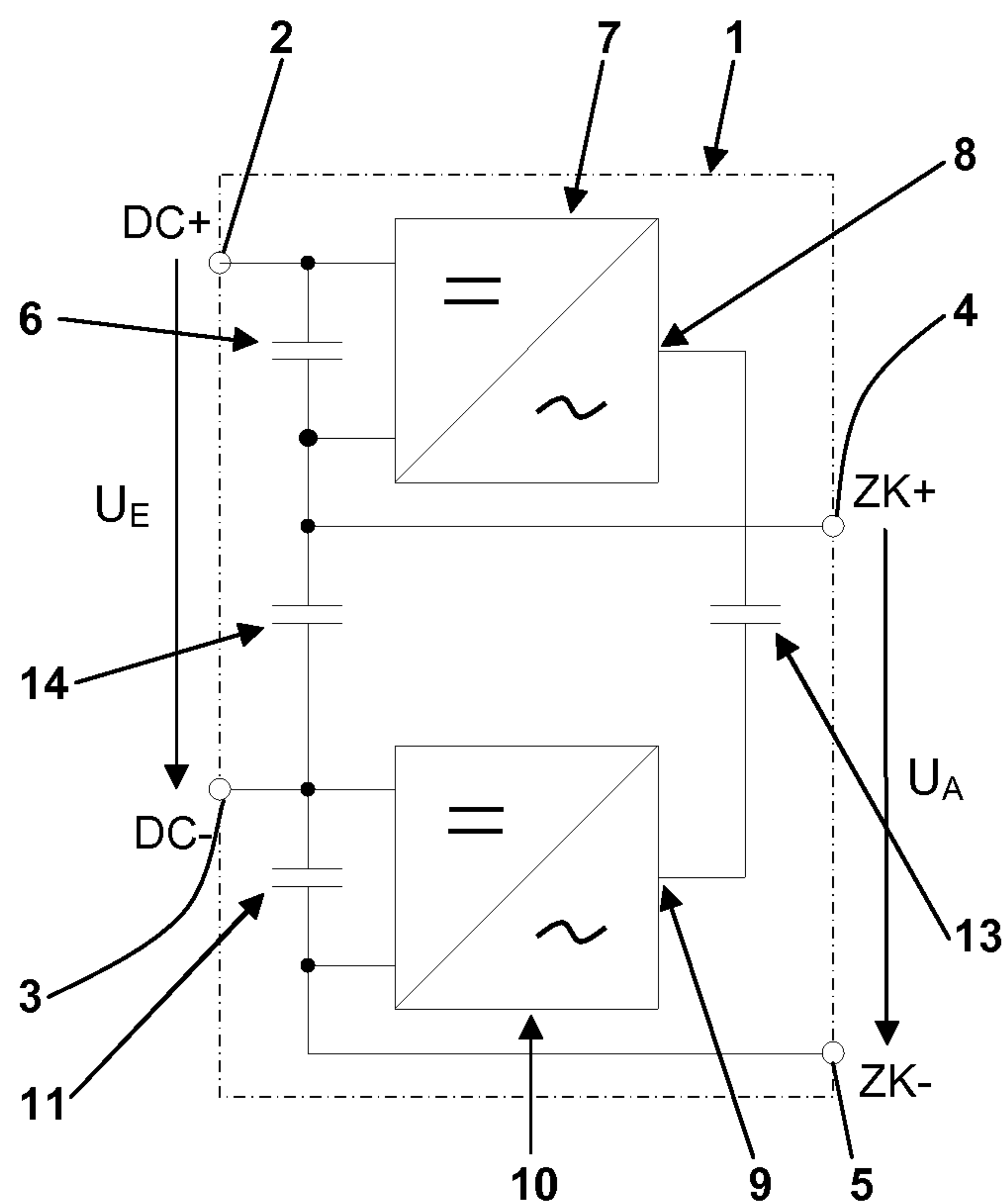


Fig. 1

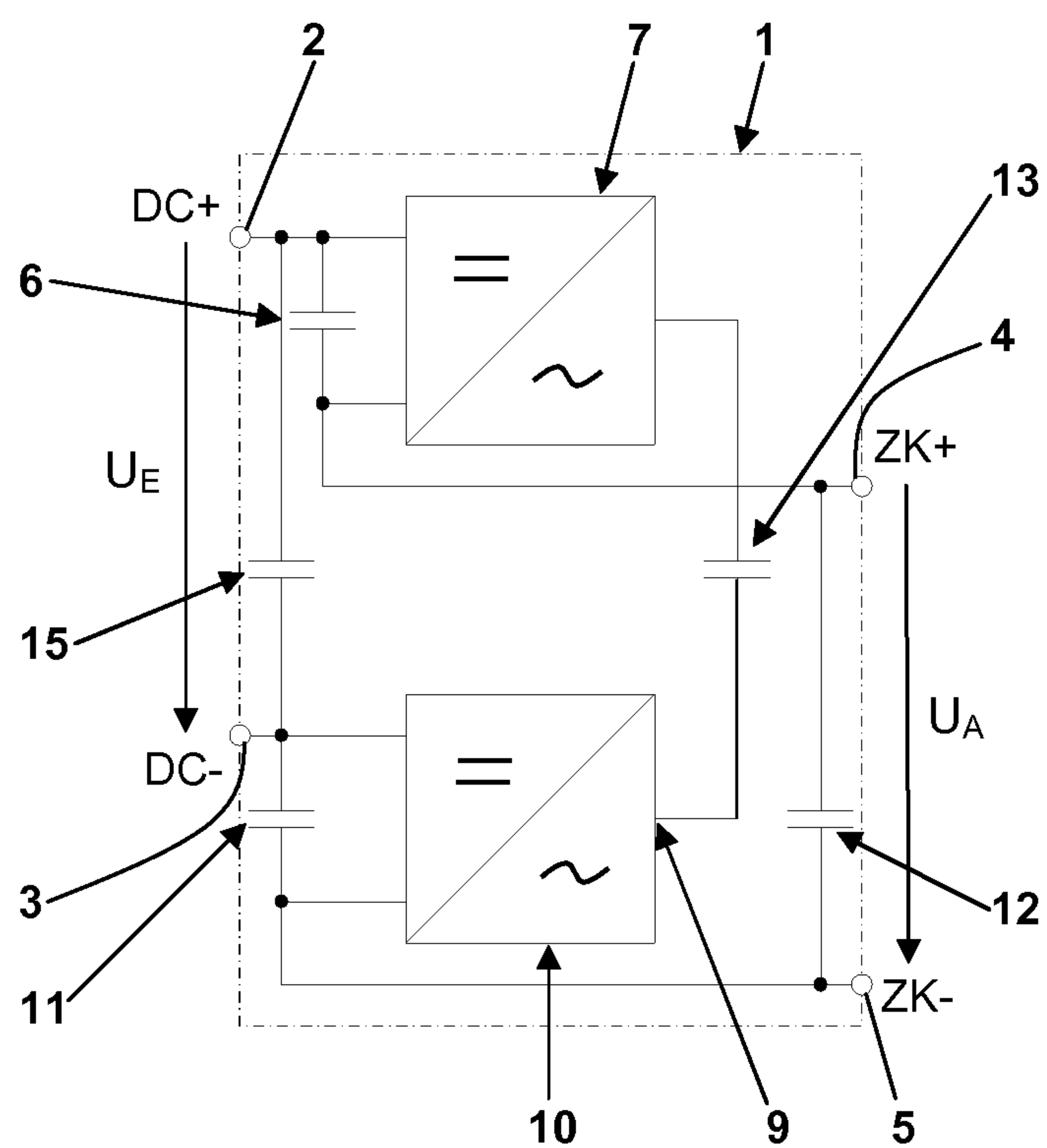
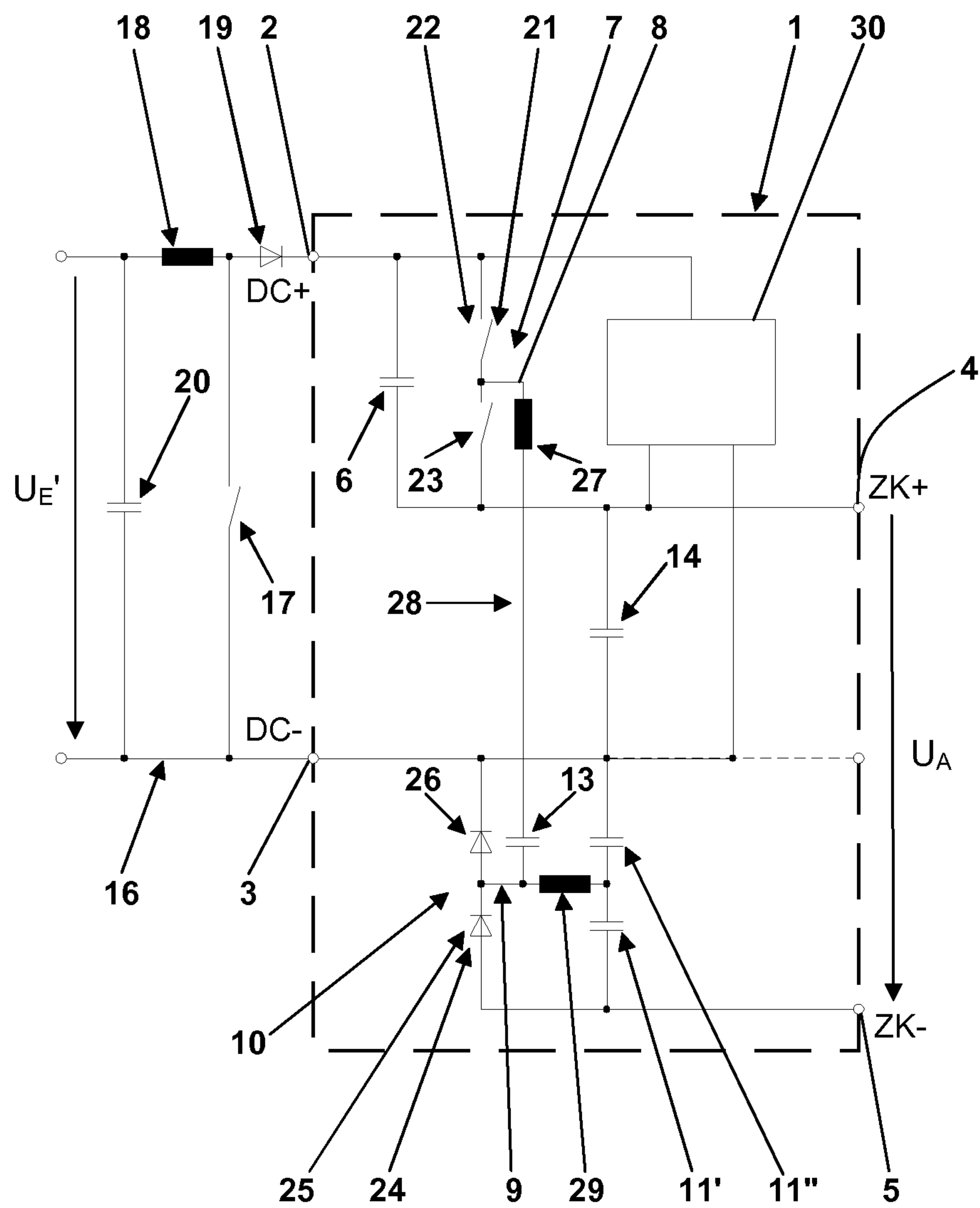
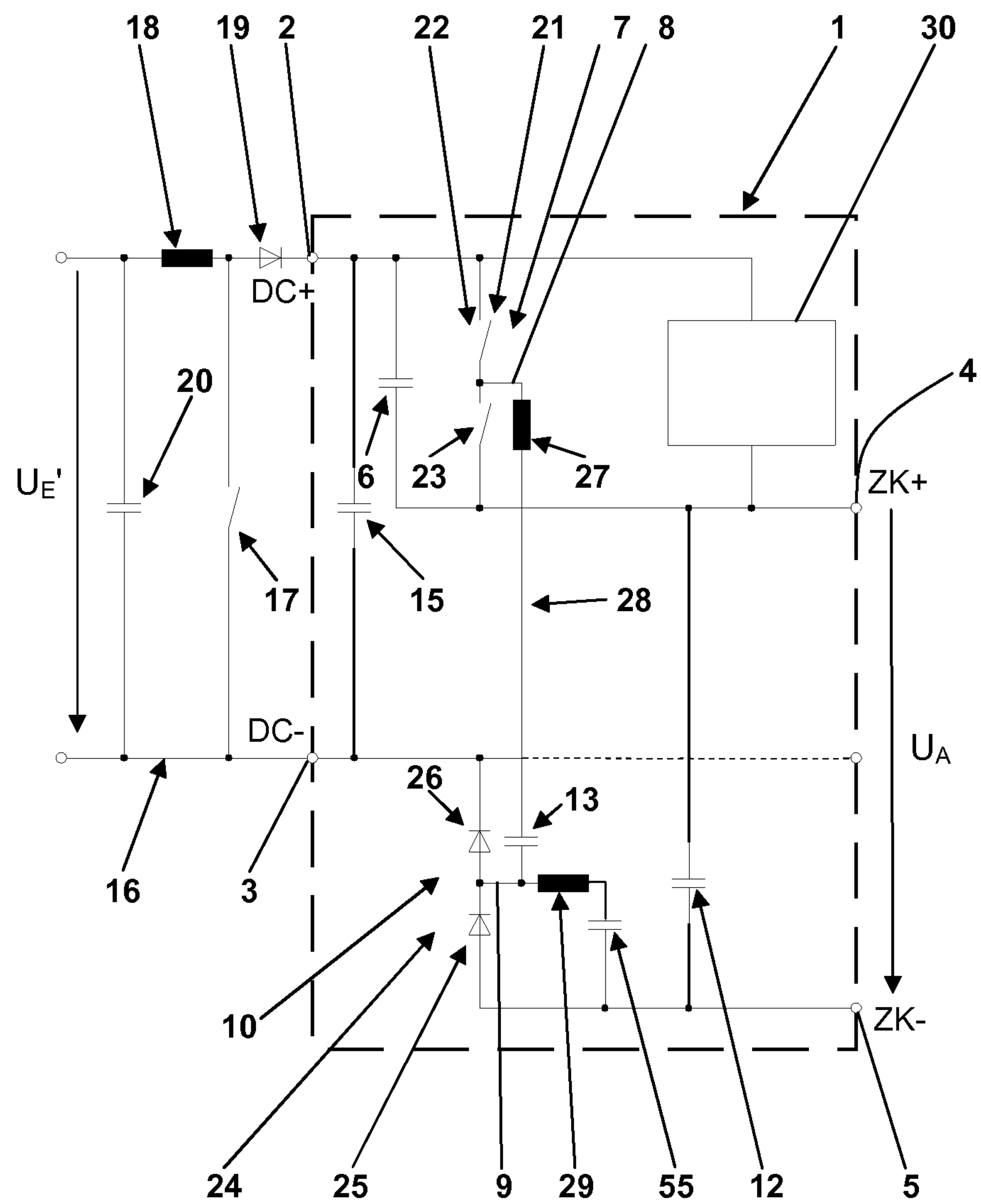


Fig. 2

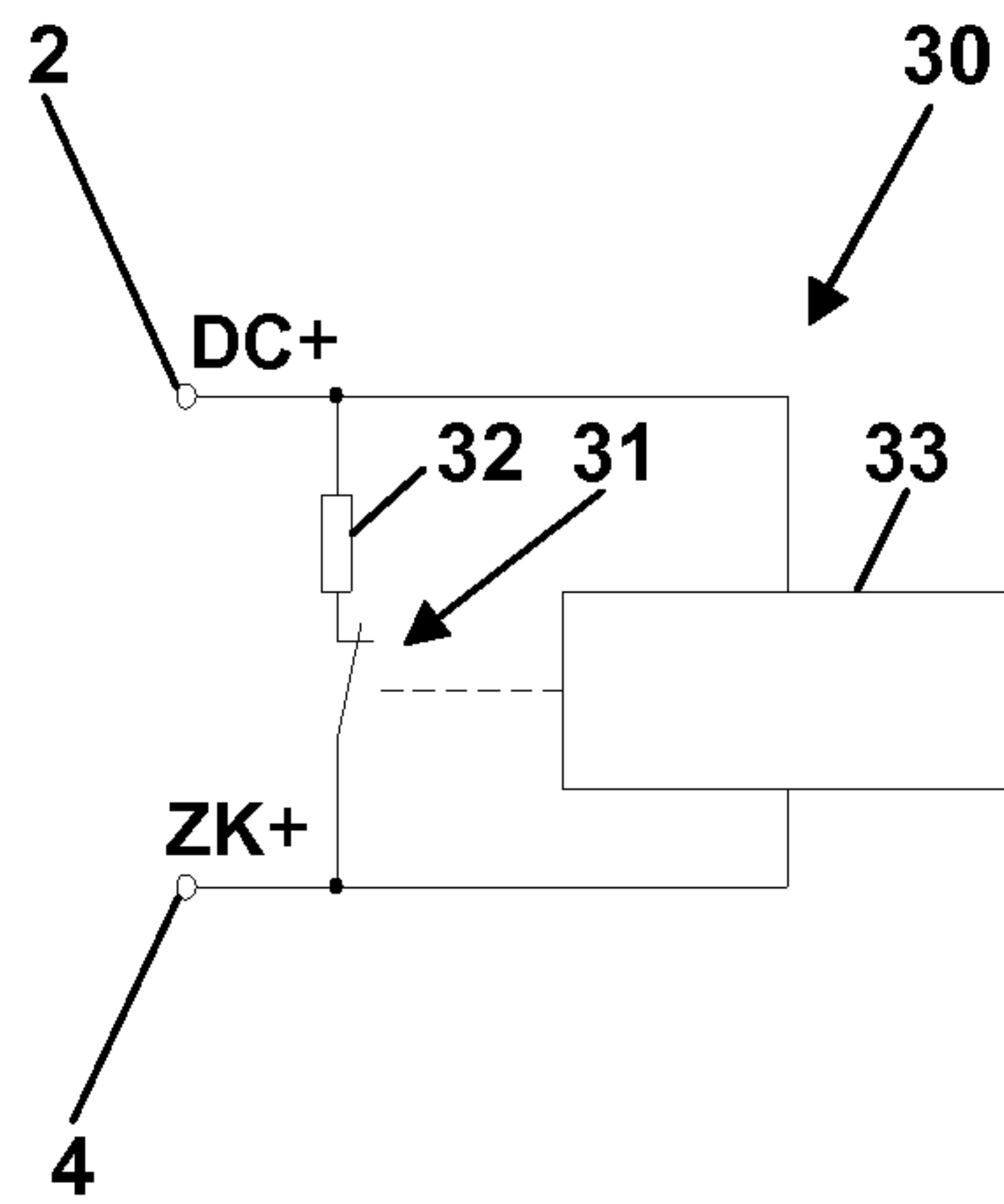
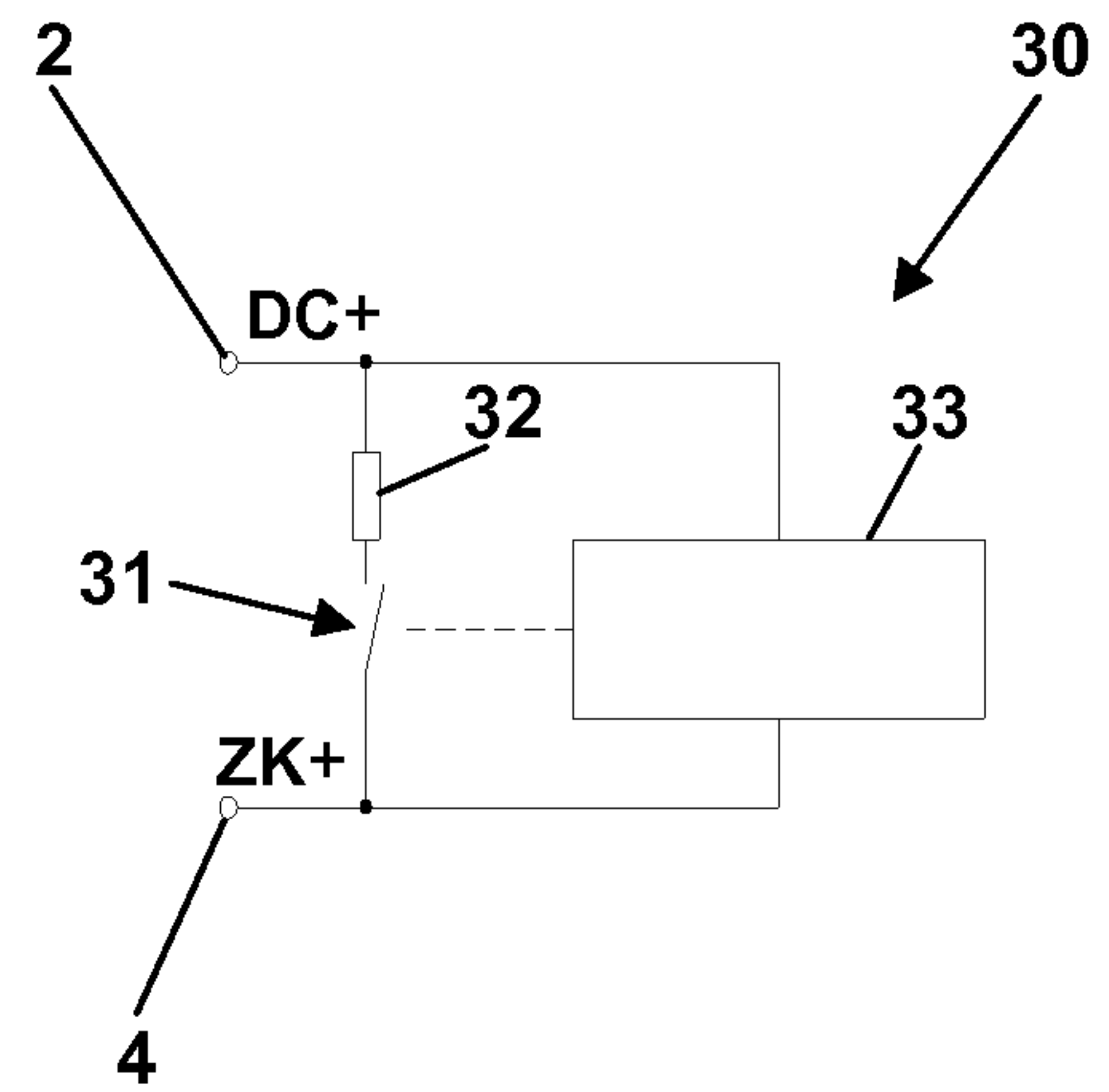
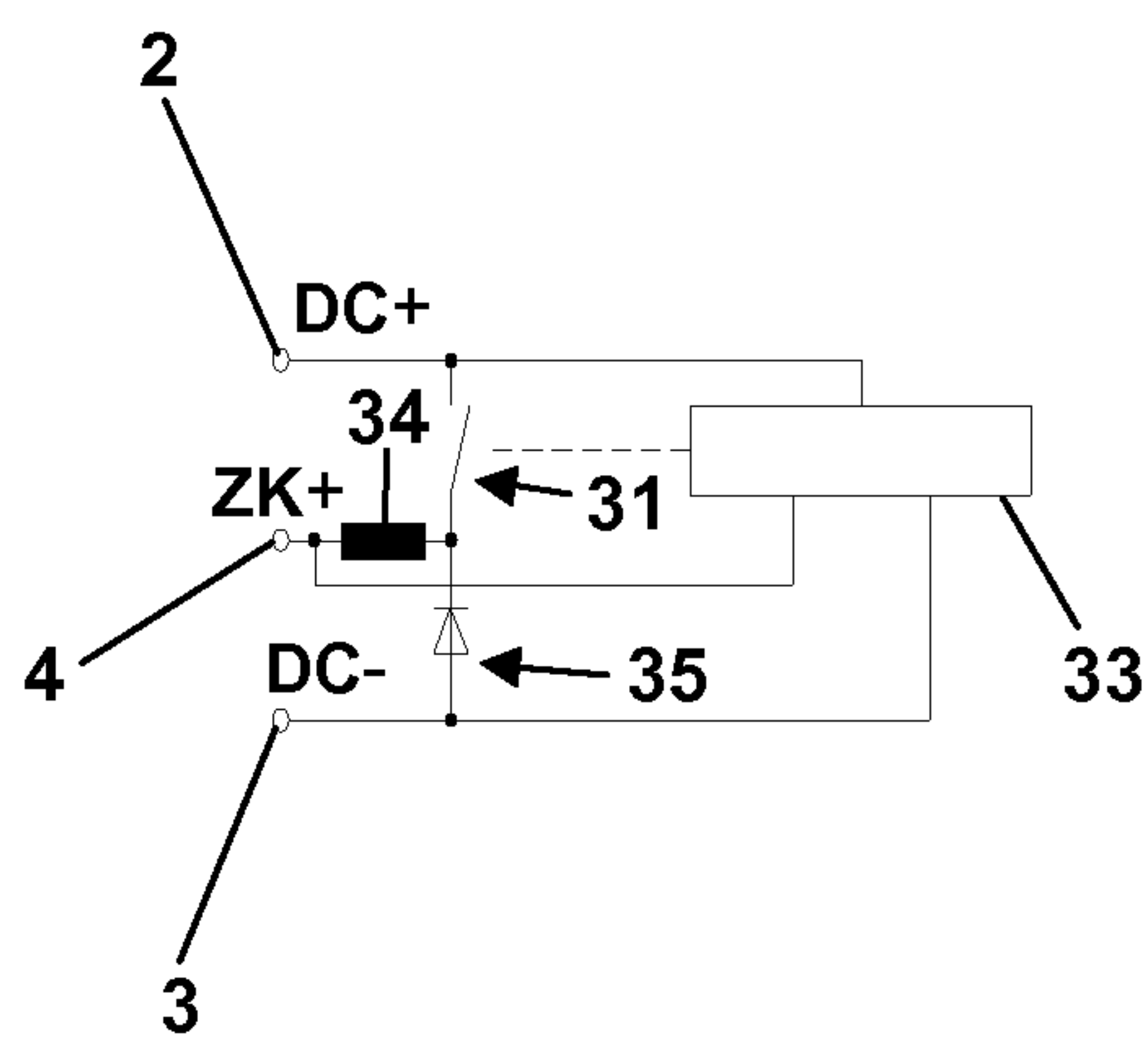
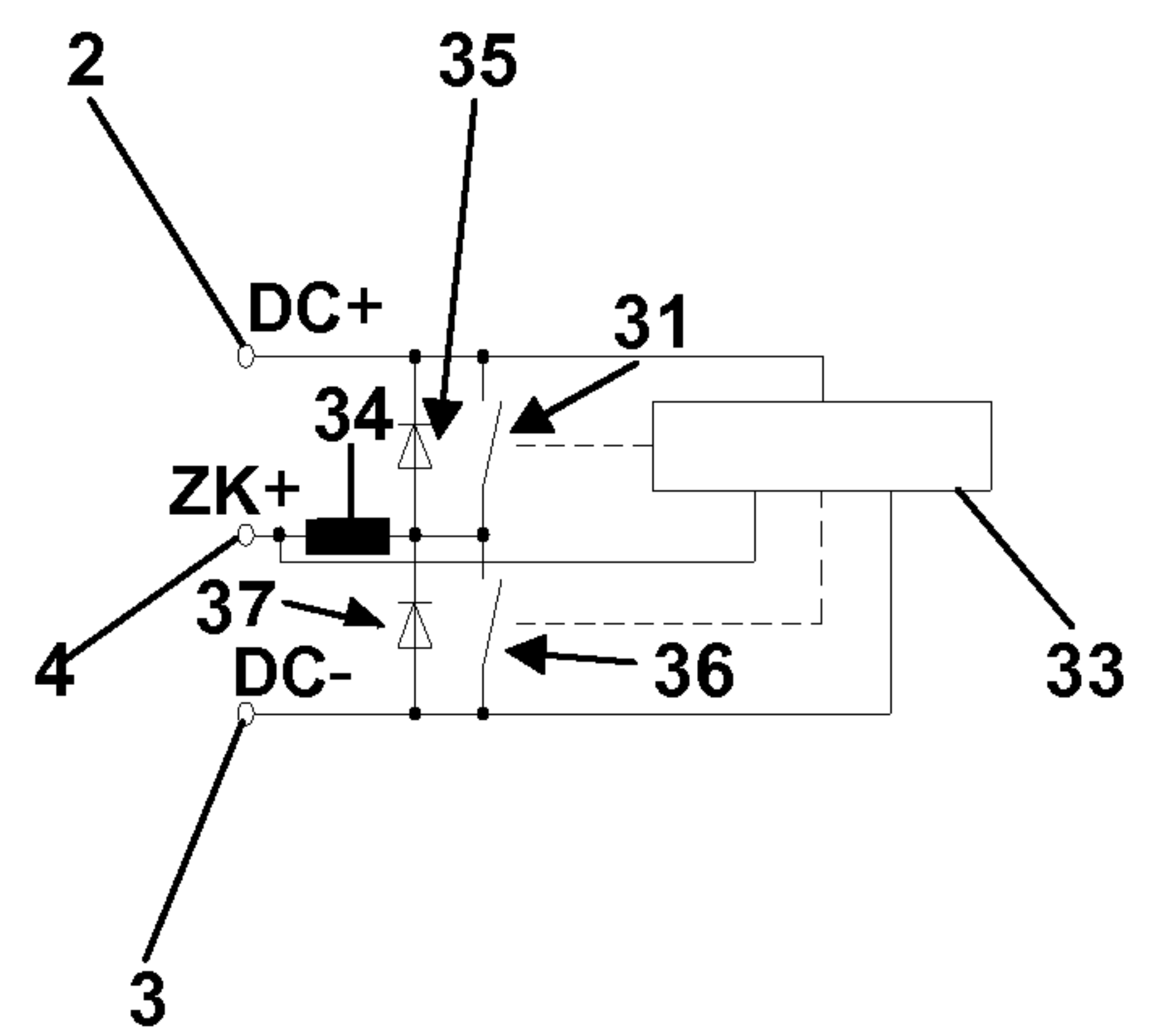
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**Fig. 3**

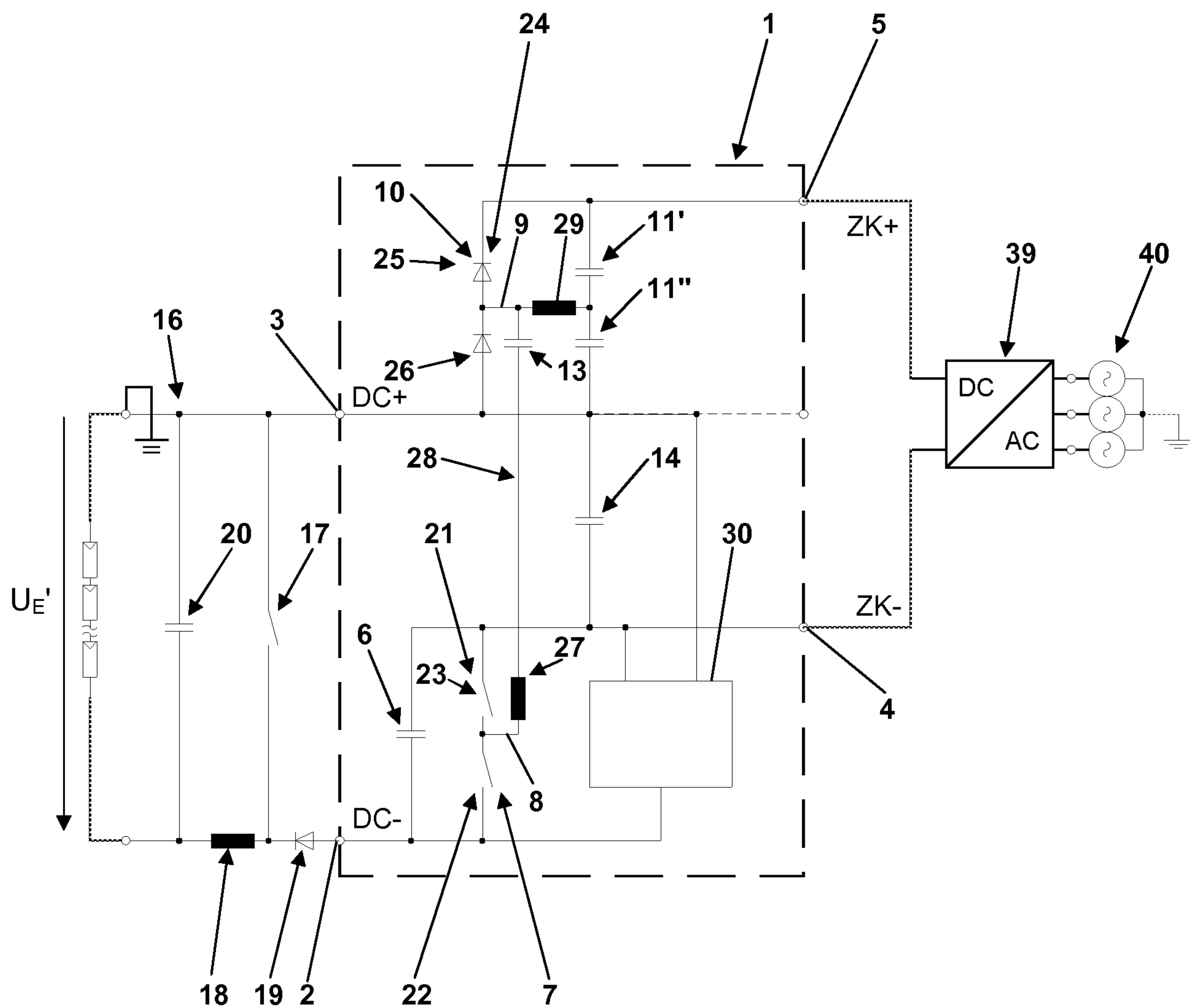
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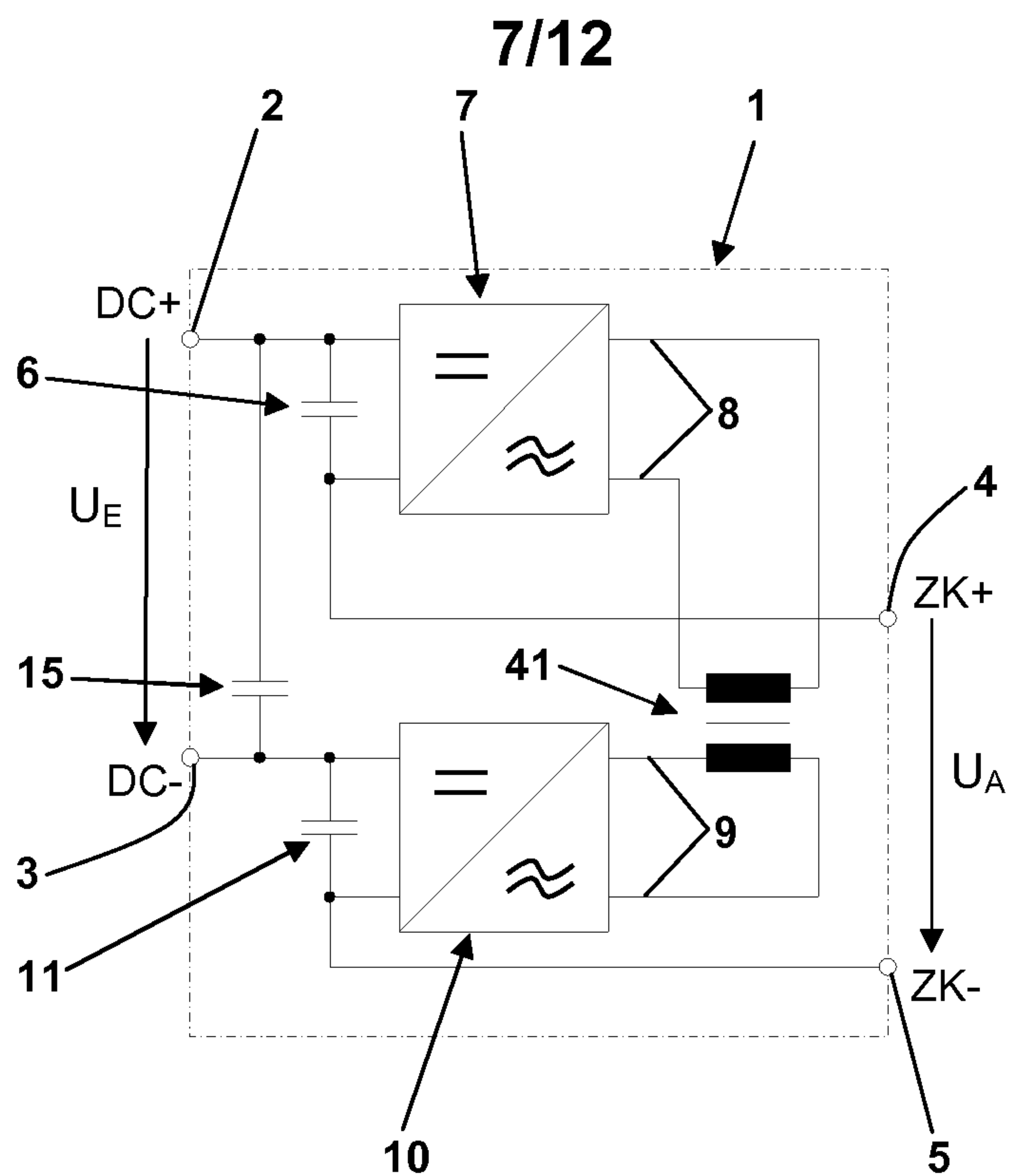
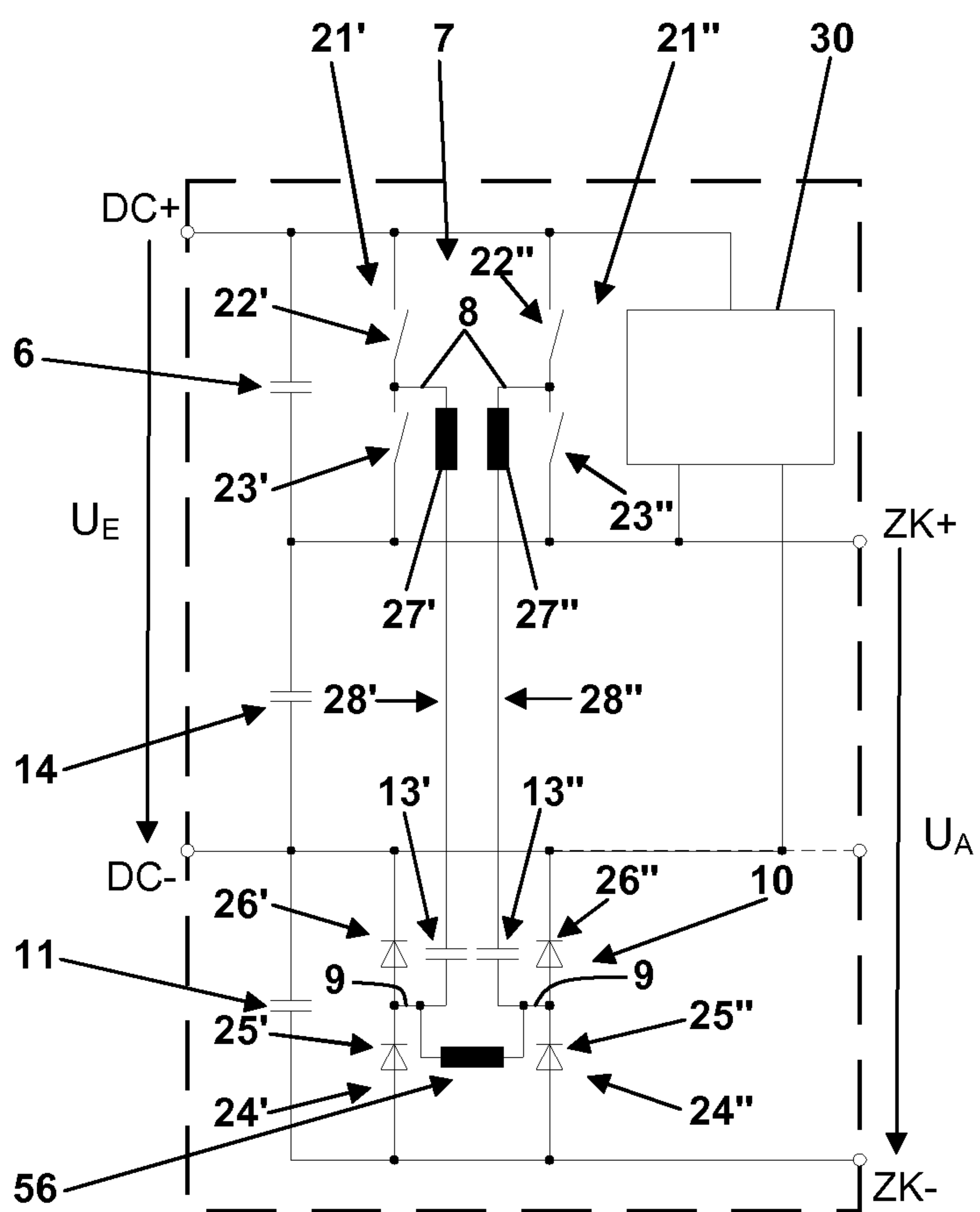
**Fig. 4**

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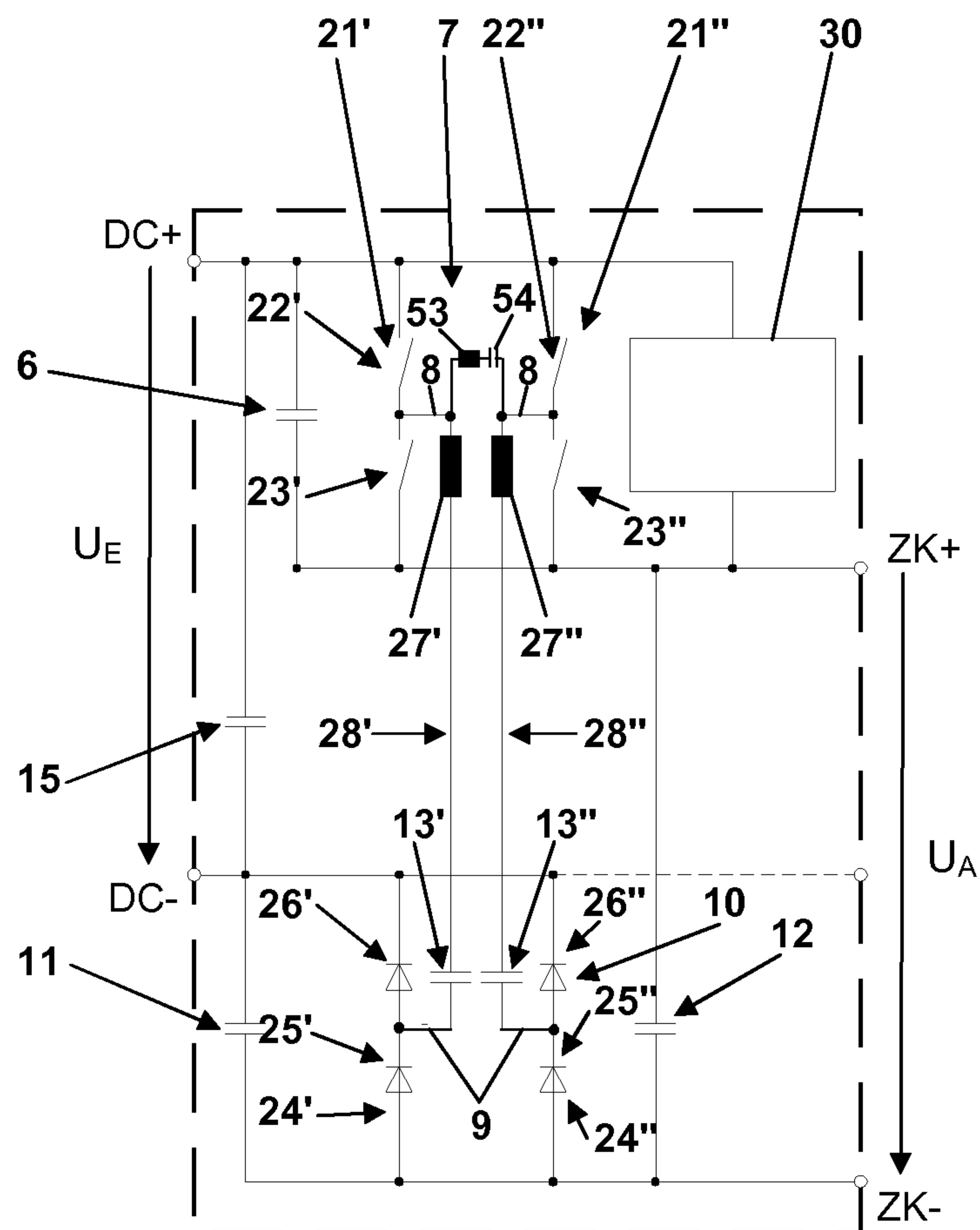
**Fig. 5****Fig. 6****Fig. 7****Fig. 8**

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**Fig. 9**

**Fig. 12****Fig. 13**

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**Fig. 14**

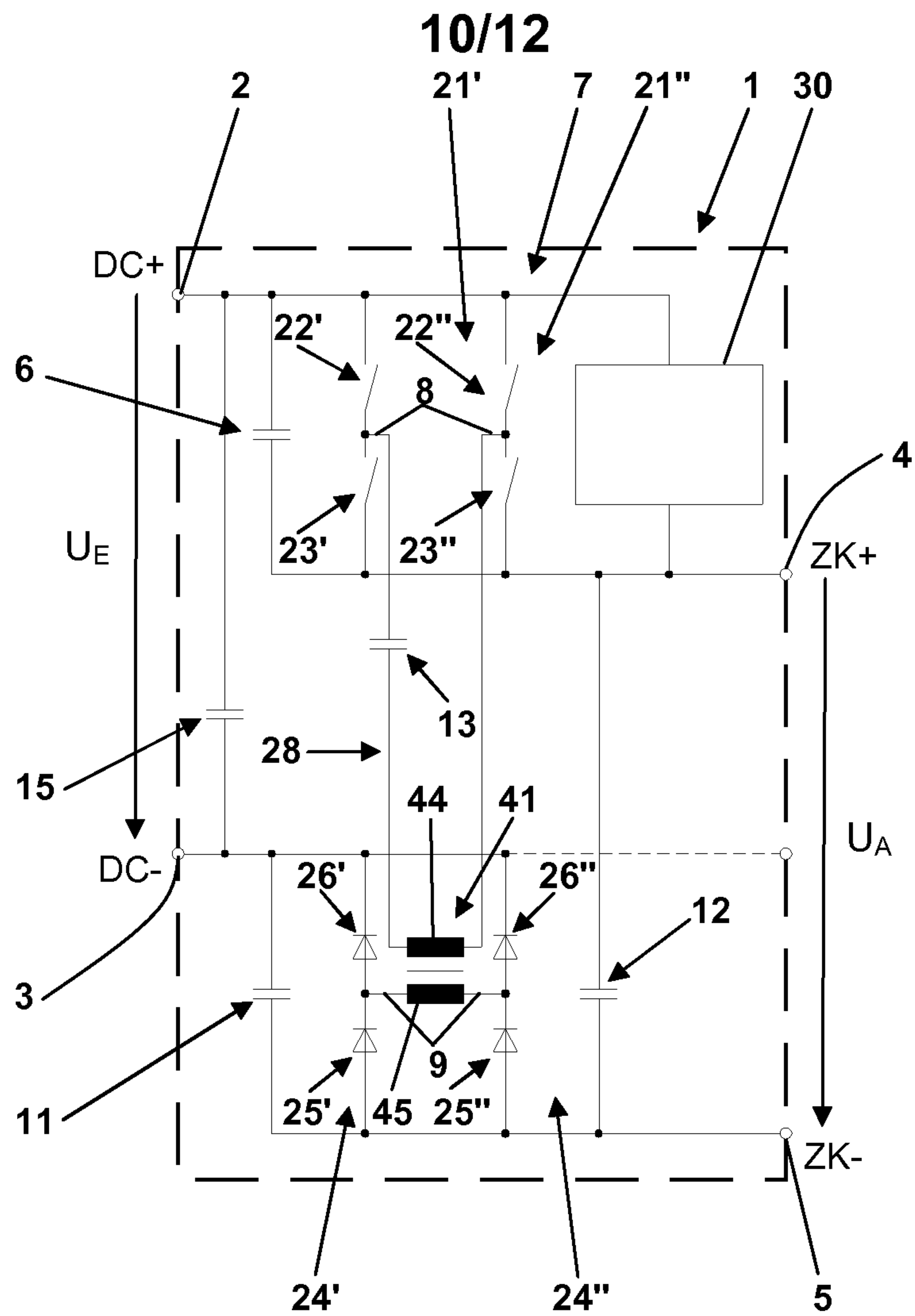


Fig. 16

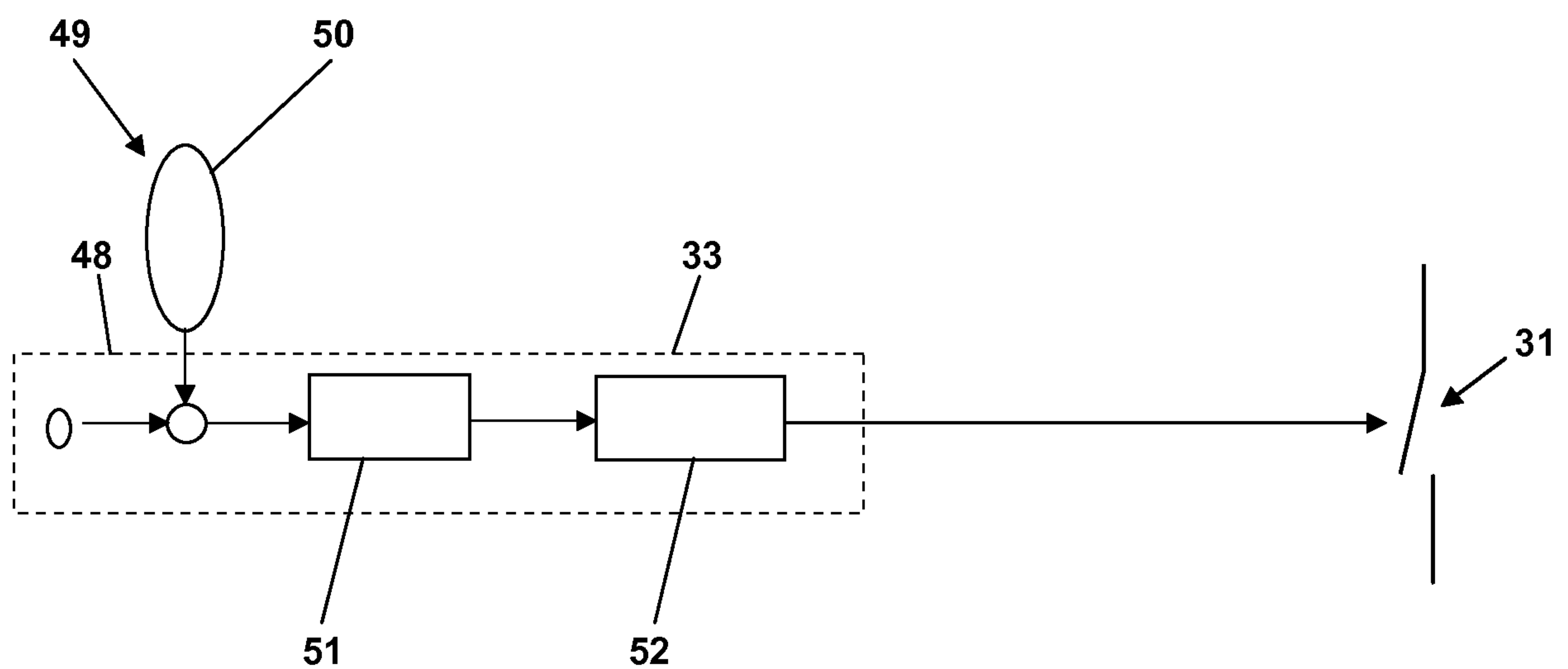
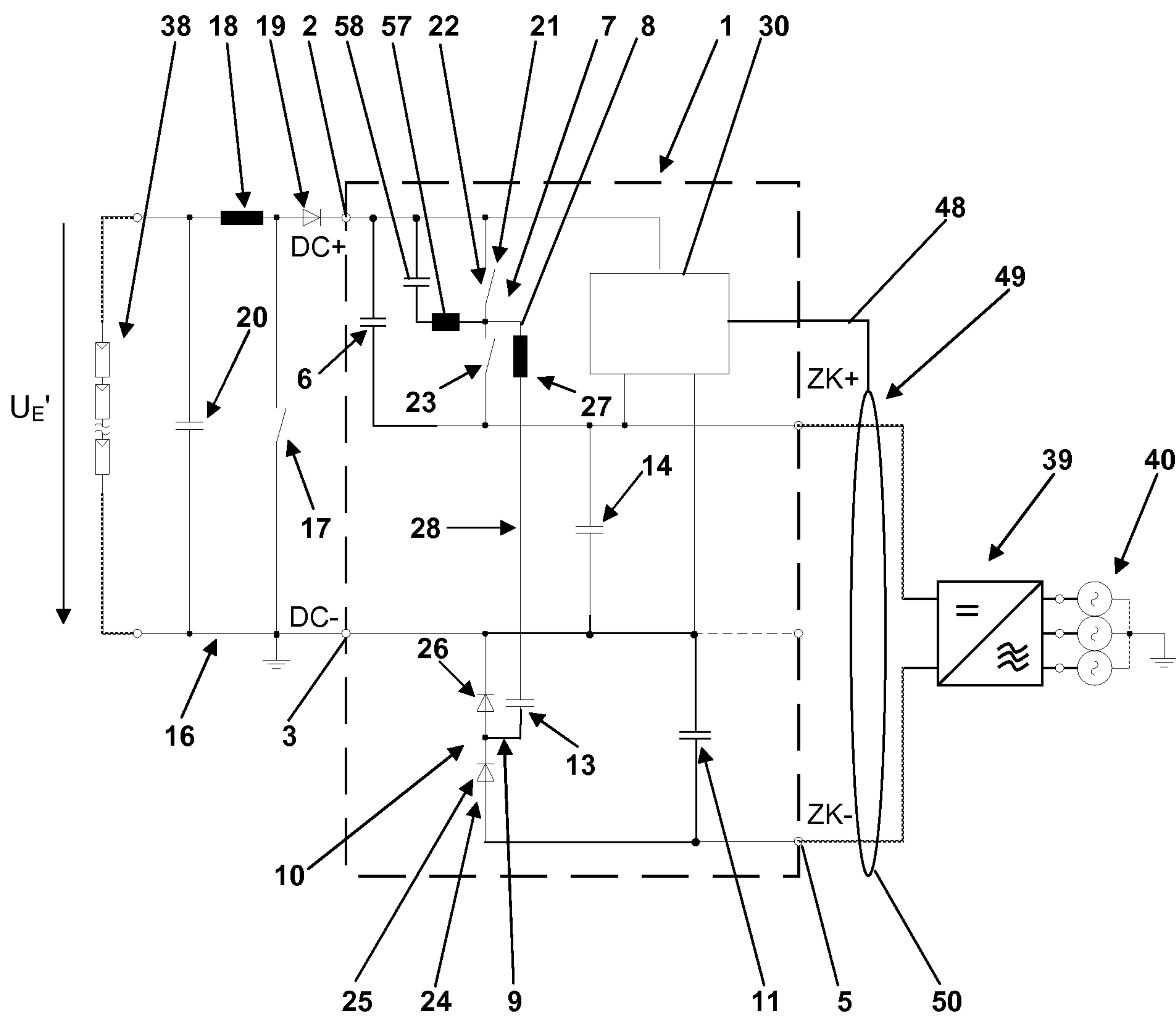


Fig. 19

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**Fig. 17**

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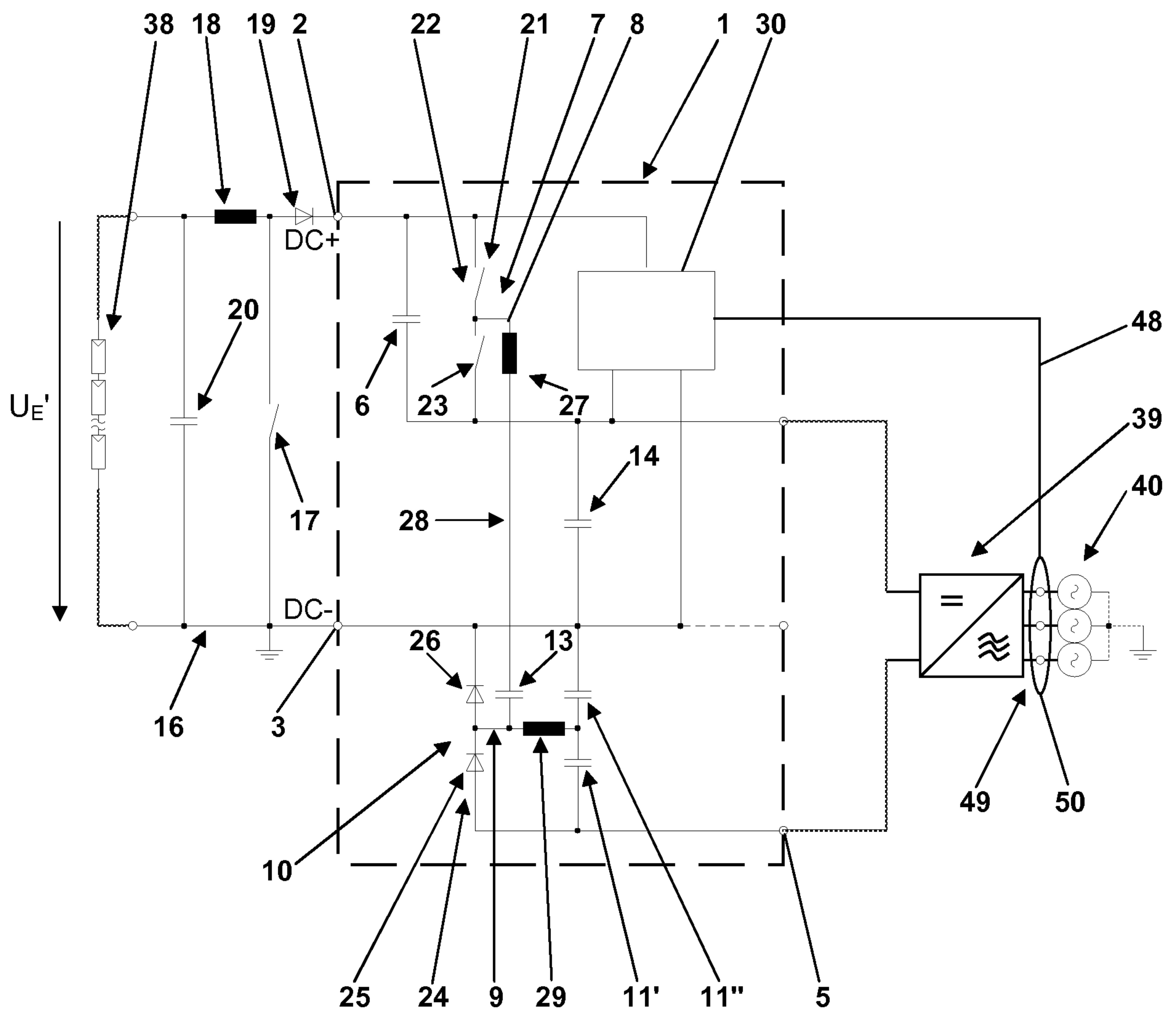


Fig. 18

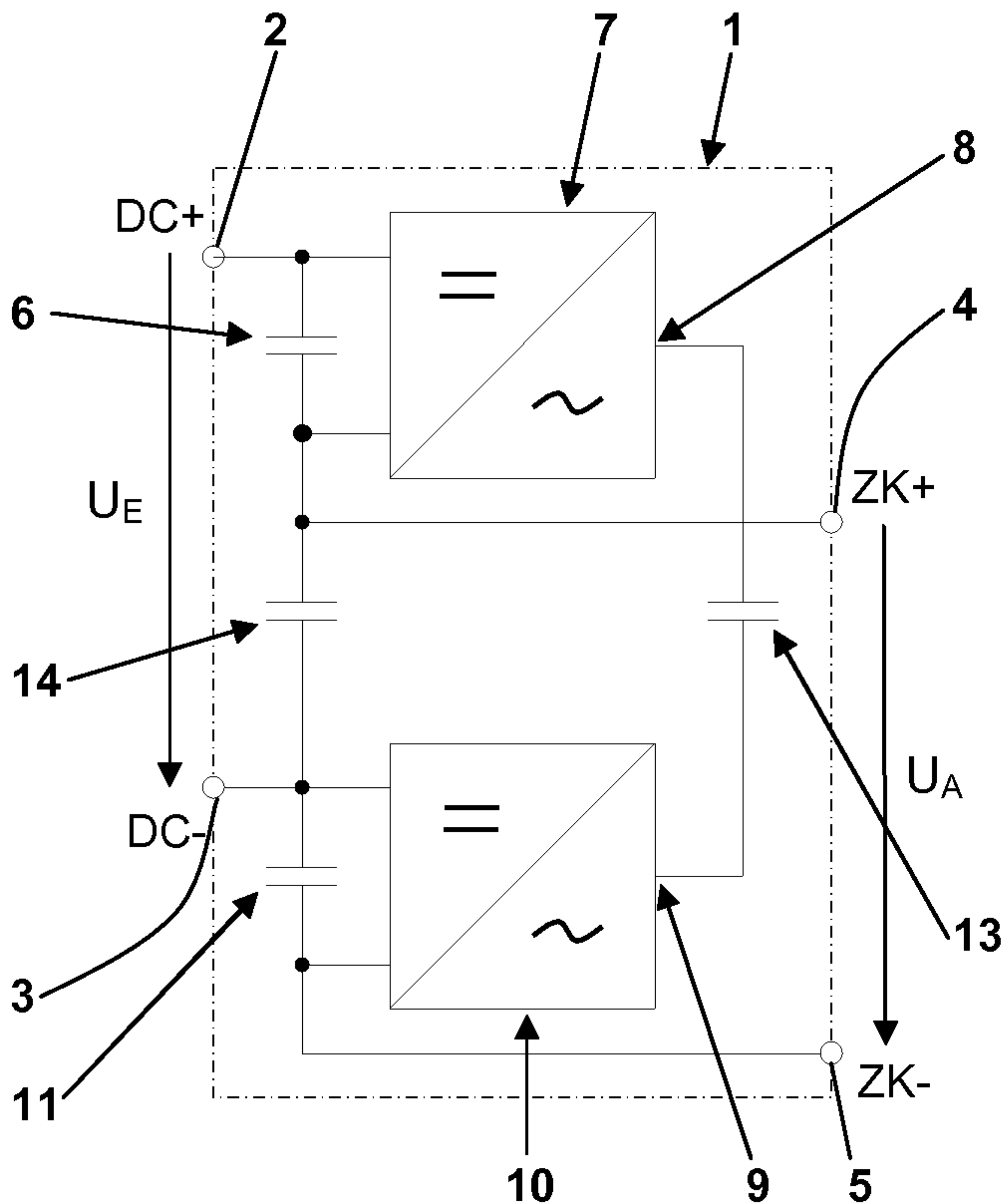


Fig. 1