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US 5527542 A (SERPELLONI ET AL) 18 June 1996
FR 2464656 A (FERRERO C SPA P) 20 March 1981
WO 2001/15545 A (WM. WRIGLEY JR. COMPANY) 08 March 2001
WO 2000/038532 A (WM. WRIGLEY JR. COMPANY) 6 July 2000
WO 2001/056398 A (XYROFIN OY) 09 August 2001
EP 0625311 A (ROQUETTE FRERES) 23 November 1994
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## (54) Title: IMPROVED PAN COATING PROCESS

(57) Abstract: The present invention relates to pan-coated products produced by a process comprising the following steps: (a) applying a solution or suspension of one or more polyols to a core, (b) dusting with one or more polyols in powder form and (c) carrying out drying at $20^{\circ} \mathrm{C}-80^{\circ} \mathrm{C}$. The amount of polyol in powder form is from $30 \%$ to $75 \%$ by weight, based on the total solids content of the polyol in the coating.

## IMPROVED PAN COATING PROCESS

## Description

The present invention relates to improved pan coating processes and to coated products produced thereby.

In pan coating, or panning, technology there are a variety of processes, such as hard coating (with or without addition of powder), soft coating (always with addition of powder in large amount), solution coating (with or without addition of powder), and suspension coating (with or without addition of powder).
Panning processes are extremely lengthy operations, and usually run in the following order:
a) introduction of coating medium, b) distribution, c) optional powder addition, and d) drying. These operating steps are repeated frequently ( $80-120$ times) and in that way layers are gradually built up on the material for coating. In the course of this operation there are changes in amounts applied, distribution times, number of cycles in the individual phases, and drying times in the individual phases.

A constant concern on the part of the skilled worker is to produce a good product in a short time. In spite of this no success has been achieved to date in obtaining distinct accelerations of the process.

Since it is necessary to carry out repeated evaporation of water and, at the same time, to prevent the material for coating sticking to itself and/or to the apparatus, it is not possible to spray arbitrarily large quantities of solution or suspension onto said material. As a result, the duration of the panning operations is lengthy and uneconomic.

A process which attempts to circumvent these disadvantages is the Lycoat process (EP 0625311 B 1 ), which uses the polyol maltitol.

In a corporate text (The World of Ingredients, October 1999, page 59) this innovative process is contrasted with the standard process. That text describes a time saving: from 3 hours

30 minutes to 2 hours and 30 minutes. The comparison was conducted in a Dumoulin

TVV 600 pan coater with 5 kg of centers.
The coating time required when the Lycoat process was repeated in a Driacoater DRC 500/600 Vario with 7.5 kg of centers was 3 hours and 19 minutes.
WO 00/38532 describes the addition of isomalt in powder form, the amount of powder being (example A: 0.23 kg times $15=3.45 \mathrm{~kg}$ ) or in the case of example 3 syrup $7: 8.1 \mathrm{~kg}$; this is $7.8 \%$ or $17.3 \%$, respectively, of the total amount of isomalt.

A disadvantage of the two above teachings is that the surfaces of the coated products produced by these two processes are rough and that colored pan-coated candies become patchy and/or it is not possible to achieve adequate reductions in the coating times.
WO 00/38532 describes a maximum time saving from 3 hours 33 minutes to 2 hours 27 minutes, in other words a saving of 1 hour and 6 minutes or $31 \%$. This relates only to the actual panning operation.

A considerable disadvantage of the process described in WO 00/38532 is the use of two different syrups. In the case of new plant, this means higher investment costs and a more complicated production operation that is more susceptible to faults.
On both economic and technological grounds, therefore, there is an urgent need to produce in as short a time as possible and with minimum cost and inconvenience a smooth, crunchy, readily colorable, coated product with high storage stability and whose coating does not tend to absorb water from the atmosphere.

A reference herein to a patent document or other matter which is given as prior art is not to be taken as an admission that that document or matter was known or that the information it contains was part of the common general knowledge as at the priority date of any of the claims.

Throughout the description and claims of the specification, the word "comprise" and variations of the word, such as "comprising" and "comprises", is not intended to exclude other additives, components, integers or steps.

The present invention provides in particular a process for producing pan-coated products, especially sugar-free products, comprising a core, a sugar-free core for example, and a nonhygroscopic - preferably sugar-free - coating, the coating consisting of or comprising at least one, preferably two or more, layer(s), in which a coating medium comprising a solution or suspension of one or more polyols is prepared and in a first step a) this coating medium is then applied, in particular partially, to the core and then in a second step b) one or more polyols in powder dry form are applied to the coated core, in particular the dragees, i.e. the coated cores are dusted with a comparatively large amount of one or more polyols in powder form,
followed by a third step c) of drying at from $20^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$, and in a particularly preferred embodiment the process sequence of applying the coating medium, subsequently applying, in particular dusting with, one or more polyols in powder form and drying at from $20^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$, preferably from $25^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$, can be carried out more than once, in particular from 5 to 50 times, in particular from 10 to 50 times, preferably from 20 to 40 times. The present invention further provides a process for producing pan-coated products, comprising a core and a nonhygroscopic coating, where the coating comprises at least one layer, and the coating is applied to the core by preparing, as coating medium, a solution or suspension of one or more polyols and in a process step a) applying this coating medium to the core, for the purpose of applying one layer, and then, in a process step b), dusting with one or more polyols in powder form, and subsequently, in a process step c), carrying out drying with air at $20^{\circ} \mathrm{C}-80^{\circ} \mathrm{C}$, the amount of the polyol or polyols in powder form present in the final coating being from $30 \%$ to $75 \%$ by weight (based on total solids content of the polyol or polyols in the coating), it being an optional possibility to repeat steps a), b) and c) two or more times in alternation, wherein the polyol or polyols is/are xylitol, erythritol, mannitol, 1,1-GPM (1-O- $\alpha$-D-glucopyranosyl-Dmannitol), 1,6-GPS (6-O- $\alpha$-D-glucopyranosyl-D-sorbitol), 1,1-GPS (1-O- $\alpha$-D-glucopyranosyl-D-sorbitol), or mixtures thereof and wherein the polyol or polyols added in powder form used for dusting has/have a particle size distribution of $90 \%<50 \mu \mathrm{~m}$.

In accordance with the present invention, a coating medium comprising a solution or suspension of one or more polyols is prepared, applied to a core and dusted with large amounts of one or more polyols in powder form and the layer obtained is dried, it being possible for this process sequence to be repeated, in particular, for example, from 10 to 50 times, preferably from 20 to 40 times. The invention provides in particular an aforementioned process in which the amount of one or more polyols in powder form that is used for dusting the applied layer or layers is in particular from $25 \%$ to $75 \%$ by weight, preferably from $30 \%$ to $60 \%$ by weight, in particular from $50 \%$ to $60 \%$ by weight, based in each case on the total solids content of all of the polyols applied in the coating, i.e., in all of the layers. In a particularly preferred embodiment the amount of one or more polyols in powder form that is used for dusting the applied layer or layers is from $30,35,40,45,50,55,60,65$ or $70 \%$ to $75 \%$ by weight, in particular from $35 \%$ to $75 \%$, more preferably from $40 \%$ to $75 \%$ and most preferably from $45 \%$, in particular $50 \%$ to $75 \%$ by weight, based in each case on the total solids content of all of the polyols applied in the coating, i.e., in the sum of all the layers.

In a further particularly preferred embodiment the amount of one or more polyols in powder form that is used for dusting the applied layer or layers is from 30 , in particular from 40 to 45 , $50,55,60$ or $70 \%$ by weight and most preferably from 40 to $55 \%$ by weight, based in each
5 case on the total solids content of all of the polyols applied in the coating, that means in the sum of all layers.

In a particularly preferred embodiment, steps a), b) and c) indicated above are performed subsequently to each other, in particular in the given order. In a further preferred embodiment of the present invention, steps a), b) and c) are performed simultaneously. In a further preferred embodiment of the present invention steps a) and b) are performed simultaneously, followed by step c). In a further preferred embodiment of the present invention steps a) and c) are done simultaneously. In another preferred embodiment of the present invention steps a) and c) are performed simultaneously followed by step b). It is also possible to first carry out step a) and then to simultaneously carry out steps b) and c). Of course it is also possible to carry out step a) once or more than once, followed by once carrying out step b), followed by carrying out one or more times step a) and so on.

In a particularly preferred embodiment the core of the pan-coated product is a chewing gum core or center or pillow. As will be appreciated, however, consideration may also be given to selecting, as the core, a nut, hard or soft caramels, hard or soft snack articles, other confectionery, a tablet, a compact or another product suitable for pan coating, such as animal feed, pesti-cide-containing body, herbicide-containing body, catalyst, laundry detergent, etc. These cores may in a particularly preferred embodiment be composed of or contain sugar free components, such as sugar alcohols like isomalt, maltitol, xylitol, erythritol, mannitol, sorbitol, isomalt GS or contain any one of these compounds.

A particularly preferred embodiment provides for the amount of polyol, or two or more polyols, used in powder form for dusting to be from $25 \%$ to $75 \%$ by weight, preferably from $30 \%$ to $60 \%$ by weight, in particular from $50 \%$ to $60 \%$ by weight, preferably from $30,35,40,45$, $50,55,60,65$ or $70 \%$ to $75 \%$ by weight, in particular from $35 \%$ to $75 \%$, in particular from $40 \%$, more preferably from 45 or $50 \%$ to $75 \%$ by weight (based in each case on the total solids
content of the total amount of polyol applied to the core; that is, in the sum of all layers. In a further particularly preferred embodiment the amount of one or more polyols in powder form that is used for dusting the applied layer or layers is from 30 , in particular from 40 to 45,50 , 55,60 or $70 \%$ by weight and most preferably from 40 to $55 \%$ by weight, based on each case on the total solids content of all of the polyols applied in the coating, that means in the sum of all layers.

The process of the invention comprises preparing a pan-coating medium, i.e., a solution or suspension, for example, a mixture of a dissolved polyol and, where appropriate, an undissolved polyol (also referred to as suspension constituent), at elevated temperature, preferably from $25^{\circ} \mathrm{C}$ to $90^{\circ} \mathrm{C}$, preferably from 40 to $80^{\circ} \mathrm{C}$ for example, preferably from 45 to $55^{\circ} \mathrm{C}$, and, after the application or distribution phase on the core that is to be coated, dusting the coated core with substantially larger amounts of a fine polyol powder. Moreover, the temperature of the drying air is higher than in standard processes. The frequency of addition and the amount of the powder is adapted to the corresponding polyol in customary fashion.

Surprisingly, in this process, hard, smooth, readily colorable, and crunchy products are obtained in combination with an extremely rapid layer buildup. The present invention therefore provides in a type of a "soft coating process" hard coated products, i.e. a coated product having a hard and crunchy coating. The products of the present invention furthermore are improved over the art insofar, as that they have an excellent shelf life, i.e. improved storage stability.

It is also surprising that, in spite of the elevated drying air temperature preferred in accordance with the invention, namely from 20 to $80^{\circ} \mathrm{C}$, preferably from 25 to $50^{\circ} \mathrm{C}$, the temperaturesensitive centers in the case of chewing gums (softening temperature about $30^{\circ} \mathrm{C}$ ) remain dimensionally stable.

In a particularly preferred embodiment of the present invention, the drying air temperature is increased, preferably for a short time, at the end of the coating process.

The percentage fraction of the polyol added in powder form, at preferably $>50 \%$, based on the total solids content of all the polyols applied in the coating, is up to three times as high as the proportion in WO 00/38532 (example 3) and almost seven times as high as in example A of WO $00 / 38532$, which results in an extraordinarily economic procedure.

The time saving in the process of the invention amounts to $53 \%$ (as compared with example 3 of WO $00 / 38532$ ) and even $68 \%$ as compared with example A: in other words, in those cases where to date one coating operation was possible, now two or three coating operations are possible in the same unit time.

This is an extraordinarily great advantage over the prior art.

## Detailed description of the process

The centers to be coated are placed, in one preferred embodiment, in a pan coater and where appropriate are first freed from adhering dust by agitation and air suction withdrawal.

The preparation of the coating medium, i.e. the coating solution or suspension is accomplished by dissolving the polyol without residue at elevated temperature, adding other, optional ingredients, such as gum arabic, a compound modifying the viscosity and/or surface tension of the coating medium, color, flavor, active substances, pharmaceutical substances, intensive sweeteners, nutraceuticals, tooth mineralizing agents and the like. Moreover, where appropriate, the fraction of polyol envisaged as a suspension constituent is added.

In a preferred embodiment of the present invention, the solid content of the coating medium is from $30 \%$ to $90 \%$, in particular $50 \%$ to $70 \%$, preferably from $55 \%$ to $60 \%$.

This coating solution or suspension is stirred at elevated temperature - for example, from $25^{\circ} \mathrm{C}$ to $90^{\circ} \mathrm{C}$, in particular from $40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$, preferably from $45^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$. The coating medium is in a particularly preferred embodiment applied, in particular by spraying, for example in the form of a spraying stream or spray beam and/or preferably in portions, to the agitated cores or centers.

After the application phases, especially spray application phases, the polyol used as dusting powder is, in a particularly preferred embodiment of the present invention scattered uniformly over the agitated centers, it being possible for the amounts to be increased in the course of the operation and for these amounts to total the above-mentioned amount, for example $25 \%$ to $75 \%$, in particular 30 to $60 \%$, most preferred from 50 to $60 \%$, in particular from $30,35,40$, $45,50,55,60,65$ or $70 \%$ to $75 \%$ by weight, in particular from $35 \%$ to $75 \%$ of the polyol used and applied in the panning operation as a whole. In a further particularly preferred embodiment the amount of one or more polyols in powder form that is used for dusting the applied layer or layers is from 30 , in particular from 40 to $45,50,55,60$ or $70 \%$ by weight and most preferably from 40 to $55 \%$ by weight, based on each case on the total solids content of all of the polyols applied in the coating, that means in the sum of all layers.

This amount is far higher than in processes described to date. As constituent of the powder added in the course of the present process as dusting powder an anticaking compound, a flowability enhancer or a free-flow agent may be used together with the polyol.

Since the temperature of the coating medium is increased in a particularly preferred embodiment of the present invention to more than $40^{\circ} \mathrm{C}$, in particular more than $50^{\circ} \mathrm{C}$, preferably more than $55^{\circ} \mathrm{C}$, and the drying-air temperature is in a further preferred embodiment of the present invention likewise at this high level, it is possible to apply large amounts per unit time of solids to the material to be pan coated; at the same time a large amount of solids is applied rapidly to the centers, as a result of the addition of powder.

Advantageously, in one preferred embodiment, the amount applied of liquid coating medium and/or the amount applied of powder are increased successively in the course of the process.

In a preferred embodiment of the present invention, the polyol, in particular the nonhygroscopic polyol used may be a sugar alcohol or a sugar substitute, in particular it can be a disaccharide alcohol, most preferably a non-hygroscopic disaccharide alcohol.

The non-hygroscopic polyol used can be, for example, 1,6-GPS (6-O- $\alpha$-D-glucopyranosyl-D-sorbitol), 1,1-GPM (1-O- $\alpha$-D-glucopyranosyl-D-mannitol), isomalt, isomalt ST, isomalt GS, isomalt LM, erythritol, mannitol, maltitol or mixtures thereof. Furthermore, 1,1GPS (1-O- $\alpha$-D-glucopyranosyl-D-sorbit) or xylitol may also be used as a polyol in the present invention. In the context of the present invention a hygroscopic sugar alcohol is for example sorbitol, which in a preferred embodiment of the present invention is not used in the coating. medium and as a powder dry form, preferably is not present in the coating of the product, preferably is not present in an amount of $5,0 \%$ or more, in particular not present in an amount of $1,0 \%$ by weight or more (based on the total solids content of polyol used in the coating).

Thus, in a preferred embodiment of the present invention the polyol used is isomalt, that means is a nearly equimolar mixture of 1,6-GPS and 1,1-GPM consisting of preferably 43 to $57 \% 1,6-\mathrm{GPS}$ and 57 to $43 \%$ 1,1-GPM. In a further preferred embodiment of the present invention the polyol can be a mixture of 1,6-GPS and 1,1-GPM together with other polyols, for instance with 1,1-GPS. These mixtures are for instance described in EP 0625578 B1.

In a further more preferred embodiment of the present invention, 1,6-GPS-enriched mixtures comprising 1,6-GPS and 1,1-GPM are used, in particular those mixtures which consist of
more than 57 to $99 \%$ 1,6-GPS and less than 47 to 1\% 1,1-GPM. An example therefore is isomalt GS, which is a mixture comprising 75 to $80 \%$ (w/w) 1,6-GPS and 25 to $20 \%$ (w/w) $1,1-$ GPM. In a further preferred embodiment of the present invention 1,1-GPM-enriched mixtures are used, which preferably consist of more than 57 to $99 \%$ 1,1-GPM and less than 47 to $1 \%$ 1,6-GPS. These mixtures are for instance described in DE 19532396 C 2 (all \%-data given in the present teaching are weight- $\%$ unless otherwise indicated).

In a particularly preferred embodiment of the present invention, the only polyol, in particular sugar alcohol used in the coating medium or used as powder in the pan-coating process, in particular present in the coating, is a polyol selected from the group of 1,1-GPM, 1,6-GPS, isomalt, isomalt ST, isomalt GS, isomalt LM, maltitol, xylitol or mixtures thereof. Thus, the invention foresees that no further polyols, in particular no further sugar alcohols are used in the coating medium and in the powder, particularly are present in the coating of the product. In a particularly preferred embodiment the polyol, in particular sugar alkohol selected from the group consisting of 1,6-GPS, 1,1-GPM, 1,1-GPS, isomalt, isomalt ST, isomalt GS, isomalt LM, xylitol and maltitol is not only the only polyol used in the coating medium and used in form of a powder particularly in the coating, but is also the only sweetening agents used in the coating medium and used in form of a powder, particularly in the coating, in particular is the only sweetening agents which in addition to sweetness also provides a body to the product or coating. In a further preferred embodiment, the polyol in powder form used in the coating process is the only substance used in the powder, i.e. the powder solely consists of the polyol used.

Although sugarless products are preferred, it is also possible to use sugars such as isomaltulose in the coating as a "polyol" substitute or in addition to the polyol. Thus, in the present invention the term polyol also comprises isomaltulose. In another preferred embodiment the
term polyol relates to sugar alcohols excluding all sugars such as isomaltulose.

In a particularly preferred embodiment, however, the present invention foresees a pan coating process and coatings obtained thereby which are free of hygroscopic substances, in particular are free of sorbitol. In a further preferred embodiment the present process and the coatings obtained thereby are free of hygroscopic non-sugar materials, such as sorbitol, and are free of mannitol or hydrogenated starch hydrolysate or mixtures thereof. Thus, in a preferred embodiment of the present invention, the coatings are free of sorbitol, are free of hydrogenated. starch hydrolysate or mixtures thereof, and are also free of binding and dispersing agents, in particular are free of any hygroscopic material.

In a further preferred embodiment the process and the coating, preferably the overall products, of the present invention are free of sugars such as sucrose, and therefore can be termed "sugarless" products and are free of hygroscopic substances.

According to one embodiment of the present invention, the polyol or polyols used in the coating medium may be the same as the polyol or polyols used in powder form. In another preferred embodiment, the polyol or polyols used in the coating medium may be different to the one or more polyols used in powder form.

A preferred particle size distribution of the polyol added in powder form is advantageously selected from the range from $90 \%<50 \mu \mathrm{~m}$ to $90 \%<100 \mu \mathrm{~m}$, i.e. is for instance $90 \%<50 \mu \mathrm{~m}$, $90 \%<60 \mu \mathrm{~m}, 90 \%<70 \mu \mathrm{~m}, 90 \%<80 \mu \mathrm{~m}$ and $90 \%<90 \mu \mathrm{~m}$.

In one preferred embodiment the powder may be composed of isomalt ST-PA, i.e. isomalt ST with particles $90 \%<50 \mu \mathrm{~m}$ or isomalt GS-PF (particle size: $90<100 \mu \mathrm{~m}$ ) or GS-PA, i.e. isomalt GS with particles $90 \%<50 \mu \mathrm{~m}$.

The powder used in the present invention may in a preferred embodiment of the present invention also comprise further additives, auch as a flavour, colour, pharmaceutically active substance, tooth mineralizing agent, nutraceutical, intensive sweetener, a free-flow agent, a flowability enhancer, e.g. $\mathrm{SiO}_{2}$, tricalcium phosphate and/or an anticaking compound.

In a further preferred embodiment of the present invention, the invention foresees that a first group of layers of a particular composition is applied to the cores, and subsequently a second group of layers with a different composition is applied on top of the first group of layers. For instance, the second group of layers may, in contrast to the first group of layers, contain a colour and/or flavour and/or a pharmaceutical composition and/or a nutraceutical or the like. In a preferred embodiment of the present invention, it is of course also possible that more than two groups of layers with different compositions, such as $3,4,5,6$ or more differently composed layers are applied onto the core.

In a further preferred embodiment of the present invention, the polyol or sugar used for the second type of layer is selected from the group consisting of isomaltulose, erythritol, and xyltitol.

As a result of the large amounts of powder added, saving on panning time, the number of applications is also much lower, so that it is possible to obtain smooth layers with fewer than 30 applications.

Surprisingly the resultant coating layer is smooth, hard and crunchy.
The time saving in comparison with the process of EP 0625311 B 1 , for a comparable proportion of coating, is approximately $50 \%$ and, in comparison with the process of WO $00 / 38532$, about $35 \%$. This means that in production plant it is possible to increase the throughput by
about $30 \%-50 \%$, which in the case of these batchwise production operations leads to considerable cost savings.

As a result of the inventively improved preferred addition of a fine powder in dry form (in contradistinction to its addition in the suspension), the fine crystals are retained.

It is known that isomalt is composed of 1,1-GPM and 1,6-GPS. Solids of these two substances behave differently in aqueous solutions: in other words, the two different crystals show markedly different solution and crystallization behavior.

This means that the particle size and the composition of the particulate solids are different in liquid pan-coating media, depending on the time and the temperature.

It cannot be ruled out that, as a result of long residence times in containers and lines, for example, as a result of concentration or dilution processes, some of the crystals will grow and/or some will dissolve. In the process of the invention this risk is reduced, since the overall panning operation is much quicker.

In contradistinction to the prior art it is also unnecessary to use two different coating media. It is entirely sufficient to use a liquid coating medium, in other words a solution or suspension, and a powder of suitable particle size distribution in the process of the invention.

In the case of soft panning, it is also the case that large amounts of a sugar or sugar alcohol in powder form are applied in alternation with a liquid charge to the centers to be coated. In contradistinction to the process of the invention, however, neither temperature nor drying air is used in soft coating, so that $7 \%-10 \%$ moisture is still present in the end product. This is also necessary, since the end product of soft coating is supposed to be soft to the bite. Moreover, in the case of soft coating, only about 3-10 panning layers are applied.

The new process is therefore different both from hard coating and from soft coating.
The specific conditions of the process of the invention (identity of powder, amount of powder, temperature of the liquid phase and of the drying air) result, however, in pan-coated products
which exhibit a surprisingly hard, crunchy, and smooth surface.
The time advantage of the process of the invention is not limited only to the actual panning operation (reduced evaporation of water) but also extends to the preparation of the coating medium. Since less polyol has to be dissolved there is a time and cost saving here as well.

Contrary to the description in WO $00 / 38532$, where it says:
"Sometimes dry charging can be used in hard panning, but is usually very limited in the amount of dry charge material and used for a few applications during the process.",
dusting in the process of the invention is carried out with a large amount of powder and in many cases during pan coating.

Highly concentrated solutions, large amounts for application, and rapid crystallization are considered causes of problems in hard coating (sticking; rough, nonuniform surfaces) (source:

Technologie der Herstellung von Hart-, Weich- und Schokodragees, Frank Perchtold, ZDS
Solingen/D in Einführung Herstelltechnologie Dragees, ZDS, October 9-13, 2000).
Suggested remedies include the following:

- heat or dilute solution
- dry more slowly
- dilute application solution
- lower temperature of centers
- reduce viscosity
- reduce amount of solution per application
- extend drying time between applications.

In the process of the invention the opposite is done in respect of almost every point:

- the solution remains undiluted at the same temperature
- drying is carried out quicker than usual
- the application medium is and remains highly concentrated
- the temperature of the drying air and hence that of the centers is actually increased during the process
- the viscosity is not changed
- the amount per application is increased
$\therefore \quad$ and the drying time is much shorter than with standard processes.
As can readily be seen, the process of the invention operates to a large extent counter to the prior art.

It is therefore all the more surprising that the products clearly exhibit the properties of a hardcoated product.

Another advantage according to the invention is the possibility to coat badly formed / pressed centers or hard boiled candies or other unevenly formed compounds with the aid of large amounts of powder to get smooth and even products. Flawed parts on surfaces or on edges can be smoothed out to plane and even surface areas. This allows faster, easier production conditions for coated products. Even bodies with manufacturing determined roughness can be coated according to the invention yielding smooth, beautiful products.

Due to the large amounts of powder used in the layer-building phase, the temperature of the drying air can be chosen very high, as the powder will prevent the overheating of the centers.

The drying during the coating process can in a particularly preferred embodiment of the present invention be done by a co current stream, also known as direct flow, which means that the drying air is led in the same direction as the spraying stream through the dragee bed or pan coater or, in another preferred embodiment of the present invention, by counter flow, also known as counter current stream, i.e. that the drying air is led in the opposite direction to the spraying stream through the dragee bed or pan coater.

In a particularly preferred process of the present invention, the latter method, i.e. the counter flow of drying air to spraying stream is performed during the dry charge additions, i.e. during the layer building phase in step b). Thus, steps a), b) and c) can, in a particularly preferred embodiment of the present invention be performed simultaneously. The counter flow of the drying air minimizes the loss of powder.

In another preferred embodiment of the present invention, the first mentioned method, i.e. the direct flow of drying air to spraying stream is performed during the smoothing phase, i.e. step c) is done simultaneously with step a).

In another embodiment of the present invention the mixing of dragees and powder in step $b$ ) is even more improved using one or more baffles in the pan coater or coating drum. In a further preferred embodiment of the present invention the application of the coating medium in step a) and the application of the powder in step b) is done simultaneously. To shorten the duration for the application of the coating medium and the powder to the core, these applications can be achieved by simultaneous addition of both or, more preferred, by a time-lagged application of the powder after the beginning of the application of the liquid coating medium. The application of the coating medium in step a), i.e. in particular the spray beam should, in a preferred embodiment of the present invention hit the cores, particularly the moved dragee bed before process step b), i.e. the powder addition, such that the wetted centers can pick up the powder particles.

Another design of the invention is the use of a low concentrated liquid coating medium, which can be used - from beginning of the coating process or after the layer building phase in step a) and b) with big amounts of powder - as single or smoothing sirup.


#### Abstract

The present invention also relates to a product which is obtainable according to any one of the above processes of the present invention, in particular to coated products, in particular sugar free coated products or coated products with a sugar free coating, which are for example confectioneries, nuts, hard and soft caramels, hard and soft snack articles, tablets, compacts and chewing gum candies.


Further preferred embodiments are the subject matter of the subclaims.
The invention is further exemplified by reference to the examples and the figure.

The figure shows a coating scheme of the present invention.

In the present description, claims and examples, the following terms, abbreviations and calculating schemes were used:

Total Fluid Amount of a coating solution or -suspension: TFA
Dry substance content of the TFA: DSTFA
Total Powder Addition: TPA
(Total) Center Weight: (T)CW
(Total) Dragee End Weight:
(T)DEW
(Total) Layer Weight [(T)DEW - (T)CW]: (T)LW
Percentage Layer Portion: PLP
(Total) Loss of the coating material (fluid and as powder): TL
Powder Portion in the Dragee Layer (=amount of polyol
in powder form based on total solids content of the polyol in the coating): PPDL
Percentage Powder Portion in the Dragee Layer
PPPDL
(=percentage amount of polyol in powder form based on total solids content of the polyol in the coating

Legend:
TFA means the total amount of added/sprayed coating solution or suspension in all phases.

DSTFA means the TFA without the water-fraction

TPA means the total powder amount, which is added to the (wet) centers

The TCW is the mass of the centers to be coated (number of centers multiplied by the mass of one center); the $\mathbf{C W}$ is the average mass of one center

TDEW means the mass of the finished dragees (total weight of the centers plus total weight of the dragee layers); DEW is the average weight of one dragee).

The TLW is the difference of the weights of all dragees minus the weight of all centers; the $\mathbf{L W}$ is the difference of the average weight of one dragee minus the average weight of one center.

The PLP is the quotient of the total layer weight $\left({ }^{*} 100\right)$ and the total dragee end weight. It is also possible to count as follows:
$\mathbf{P L P}=x$ pieces $* \mathbf{L W} * 100 / x$ pieces $* \mathbf{D E W}$; the percentage layer portion can be counted by division of the difference of the weight of the end product minus the center weight and the end product weight; this value is multiplied by 100 . Or by accounting a not to small number $x$ of finished dragees with the same number of centers.

TL is the difference of (DSTFA + TPA) - TLW; the total loss can be ascribed to abrasion (in the drying air) and coating of inner apparatus parts.

The PPDL is defined by the following Formula 1:
$P P D L[k g]=\frac{T P A^{*} T L W}{T P A+D S T F A-T L}[k g] \quad$ and in words:
$\operatorname{PPDL}[\mathrm{kg}]=\frac{\text { total powder addition } * \text { total layer weight }}{\text { total powder addition }+D S \text { of the total fluid amount-total loss }}$

The percentage powder portion in the layer is (Formula 2)

$$
\operatorname{PPPDL}[\%]=\frac{P P D L}{T L W} * 100=\frac{\text { powder portion of the dragee layer }}{\text { total layer weight }} * 100[\%]
$$

## Calculation scheme (exemplary):

In a coating process $60,00 \mathrm{~kg}$ centers (TCW) were coated to an end product weight of 90,00 kg (TDEW), resulting in a total layer weight of $30,00 \mathrm{~kg}$ (TLW). $33,3 \%$ (PLP) of the dragee consists of the coating material.
As fluid addition, i.e. coating medium, $58,70 \mathrm{~kg}$ (TFA) with $66 \% \mathrm{DS}$ (dry substance), i.e. $38,75 \mathrm{~kg}$ dry substance (DSTFA) were used. As powder addition totally $8,10 \mathrm{~kg}$ (TPA) were consumed. The total addition amount in the coating process is therefore $46,85 \mathrm{~kg}$ dry substance. The powder portion in the dragee layer yields

$$
(8,10 / 46,85) * 30,00=5,19 \mathrm{~kg}(\mathbf{P P D L})
$$

and the percentage powder portion in the dragee layer: (PPDL / TLW) $* 100$

$$
5,19 / 30,00 * 100=\mathbf{1 7 , 3} \% \text { (PPPDL). }
$$

The total loss (TL) of added material which is thereforenot present in the coated products in this example is $46,85-30,00=16,85 \mathrm{~kg}$.

If one does not consider the inevitable loss of added coating medium and powder (for example due to remaining rests in the pan-coating machinery) the total powder addition $8,10 \mathrm{~kg}$ (TPA) and the total layer weight $30,00 \mathrm{~kg}$ (TLW) as follows, the result

$$
8,10 / 30,00=27,0 \% \text { (PPPDL) }
$$

would pretend a much to high powder portion in the dragee layer; inevitable losses would be assigned to the fluid additions solely.

In case of minor or no losses both PPPDL-value will give the ratio of

$$
\begin{gathered}
-19- \\
\text { TPA } * 100 / \text { TLW }(=\text { TPA + DSTFA })
\end{gathered}
$$

because in the above Formula 1 the TLW is equal to TPA + DSTFA.
In the example the limit is

$$
8,10 / 54,95=\mathbf{1 4 , 7} \%
$$

which is the ratio of the powder portion in the total coating material.
The following examples illustrate the invention without limiting its scope.

## Example 1:

4.365 kg of isomalt GS ( $75 \%$ 1,6-GPS and $25 \%$ 1,1-GPM, w/w) were dissolved in 2.91 of water at $65^{\circ} \mathrm{C}$ and 2.215 kg of isomalt ST-PF ( $50 \% 1,6$-GPS and $50 \% 1,1$-GPM, particle size: $90 \%<100 \mu \mathrm{~m}$ ) were added, in the course of which the temperature lowered somewhat. Additionally gum arabic, 0.41 g (in the form of a $50 \%$ strength solution), and 50 g of $\mathrm{TiO}_{2}$ were added to the liquid phase. This pan-coating suspension was applied by spraying to 7.5 kg of chewing gum centers (pillow-shaped). During the distribution periods a total of 2.18 kg of isomalt ST-PA ( $50 \%$ 1,6-GPS and $50 \%$ 1,1-GPM, particle size $90 \%<50 \mu \mathrm{~m}$ ) was dusted uniformly over the agitated, moist centers, and subsequently drying air at $25-50^{\circ} \mathrm{C}$ was passed through the bed of candies. The table below summarizes the phases and amounts applied (in liquid form and as powder).

| Phase | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Number of cycles | 1 | 6 | 3 | 5 | 2 | 5 | 2 | 1 | 1 |
| Amount of solution or <br> suspension [ml] | 130 | 100 | 120 | 150 | 120 | 120 | 75 | 60 | 50 |
| Amount of powder [g] | 130 | 100 | 150 | 200 | - | - | - | - | - |
| Distribution time [sec] | 60 | 60 | 60 | 60 | 90 | 72 | 72 | 72 | 60 |
| Drying time [sec] | 150 | 90 | 72 | 90 | 120 | 90 | 60 | 90 | 90 |


| Air temperature $\left[{ }^{\circ} \mathrm{C}\right]$ | 25 | 30 | 35 | 40 | 50 | 25 | 25 | 25 | 25 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

The total panning time (without polishing) is 69 minutes; the coating fraction amounts to $33 \%$ of the candy weight. The product is crunchy and has a smooth surface.

## Example 2:

Driacoater DRC 500/600 Vario, amount of centers 7.5 kg

| Application | Liquid coating <br> medium [ml] | Powder [g] | Hypothetical amount of <br> powder [g] in analogy to <br> Wo 00/38532 |
| :---: | :---: | :---: | :---: |
| 1 | 130 | 130 | 75 |
| 2 | 100 | 100 | 75 |
| 3 | 100 | 100 | 112.5 |
| 4 | 100 | 100 | 112.5 |
| 5 | 100 | 100 | 112.5 |
| 6 | 100 | 100 | 75 |
| 7 | 100 | 100 | 75 |
| 8 | 120 | 150 | 75 |
| 9 | 120 | 150 | 75 |
| 10 | 120 | 150 | 75 |
| 11 | 150 | 200 | 75 |
| 12 | 150 | 200 | 75 |
| 13 | 150 | 200 | - |
| 14 | 150 | 200 | - |
| 15 | 150 | 200 | - |
| 16 | 120 | - | - |
| 17 | 120 | - | - |
| 18 | 120 | - | - |
| 19 | 120 | - | - |
| 20 | 120 | - | - |
| 21 | 120 | - | - |
| 22 | 120 | 75 | - |
| 23 | 75 |  | - |
| 24 |  |  | - |
| 25 | 50 |  |  |
| 26 |  |  |  |

Total: 1.01 kg
Total: 26 charges with 2.00 kg of TS (from coating medium) and 2.18 kg of powder
$52 \%$ of the amount of polyol is applied as powder

## Example 3 (comparative):

Lycoat-process (The world of ingredients, 1999)

| phase | traditional | sirup <br> $[\mathrm{g}]$ | sirup- <br> $\mathrm{DS}[\mathrm{g}]$ | powder <br> $[\mathrm{g}]$ | Lycoat | sirup [g] | sirup- <br> $\mathrm{DS}[\mathrm{g}]$ | powder <br> $[\mathrm{g}]$ |
| :---: | :--- | :--- | :---: | :--- | :---: | :---: | :---: | :---: |
| 1 |  | 50 | 35 | 100 |  | 200 | 140 | 120 |
| 2 |  | 350 | 245 |  |  | 240 | 168 | 120 |
| 3 |  | 600 | 420 |  |  | 490 | 343 | 105 |
| 4 |  | 150 | 105 |  |  | 150 | 105 | 30 |
| 5 |  | 700 | 490 |  |  | 225 | 158 | 45 |
| 6 |  | 1200 | 840 |  |  | 240 | 168 | 45 |
| 7 |  | 80 | 56 |  |  | 1020 | 714 |  |
| 8 |  |  |  |  |  | 90 | 63 |  |

In the Lycoat-process $20,0 \%$ of the total polyol amount is used as powder charge.

## Example 4 (comparative):

In the course of this example, example 3 of WO 00/38532 was analysed (center weight 60 kg ).

|  | syrup 7: | diry charge | syrup 8: |
| :---: | :---: | :---: | :---: |
| 1 | 1. application | $0,6 \mathrm{~kg}$ |  |
| 2 | 2. application | 0,6 kg |  |
| 3 | 3. application | 0,9 kg |  |
| 4 | 4. application | $0,9 \mathrm{~kg}$ |  |
| 5 | 5. application | $0,9 \mathrm{~kg}$ |  |
| 6 | 6. application | $0,6 \mathrm{~kg}$ |  |
| 7 | 7. application | $0,6 \mathrm{~kg}$ |  |
| 8 | 8. application | $0,6 \mathrm{~kg}$ |  |
| 9 | 9. application | $0,6 \mathrm{~kg}$ |  |
| 10 | 10. application | 0,6 kg |  |
| 11 | 11. application | $0,6 \mathrm{~kg}$ |  |
| 12 | 12. application | $0,6 \mathrm{~kg}$ |  |
| 13 |  | - | 1. application |
| 14 |  | - | 2. application |
| 15 |  | - | 3. application |
| 16 |  | - | 4. application |
| 17 |  | - | 5. application |
| 18 |  | - | 6. application |
| 19 |  | - | 7. application |
| 20 |  | - | 8. application |
| 21 |  | - | 9. application |
| 22 |  | - | 10. application |
| 23 | . | - | 11. application |
| 24 |  | - | 12. application |
| 25 |  | - | 13. application |
| 26 |  | - | 14. application |
| 27 |  | - | 15. application |
| 28 |  | - | 16. application |
| 29. |  | - | 17. application |
| 30 |  | - | 18. application |
| 31 | 13. application | - |  |
| 32 | 14. application | - |  |
| 33 | 15. application | - |  |
| 34 | 16. application | - |  |
| 35 | 17. application | - |  |
| 36 | 18. application | - |  |

Sum: $\quad 36$ applications with $38,75 \mathrm{~kg}$ DS (the amount of $38,75 \mathrm{~kg}$ was taken from table 1, example 3 on page 16 of WO 00/38532), and $8,1 \mathrm{~kg}$ dry charge have been performed, i.e. $17,3 \%$ (PPPDL) of the polyols are used in the form of a dry charge.

## Example 5:

Coating of hard boiled candies from maltitol
$7,0 \mathrm{~kg}$ hard boiled candies from maltitol were coated in a Driacoater. An isomalt GS solution ( $75 \%$ 1,6-GPS and $25 \% 1,1-\mathrm{GPM}$, w/w) with $65^{\circ} \mathrm{Bx}$ and $55^{\circ} \mathrm{C}$ was used as liquid coating medium. In total 3028 g of the solution, i.e. 1968 g dry substance was used and in total 2340 g isomalt ST-PF ( $50 \%$ 1,6-GPS and $50 \%$ 1,1-GPM, particle size $<100 \mu \mathrm{~m}$ (w/w) powder.
The single powder additions were: $1 \times 300 \mathrm{~g}$ (phase 1 ), $6 \times 150 \mathrm{~g}$ (phase 2 ), $3 \times 180 \mathrm{~g}$ (phase 3) und $3 \times 200 \mathrm{~g}$ (phase 4).

The coating time was 72 min .
The percentage powder portion of the process is calculated to $54,3 \%$.
The end product shows a smooth and even surface. The proportion of the layer in relation to the coated end product was $38 \%$.

## Example 6:

A solution of isomalt GS ( $75 \% 1,6-\mathrm{GPS}$ and $25 \% 1,1-\mathrm{GPM}, \mathrm{w} / \mathrm{w}$ ) with the following recipe was used at $60^{\circ} \mathrm{C}$ for coating of $7,5 \mathrm{~kg}$ cushion-shaped centers in a Vario $500 / 600$ coater:

| $55,00 \%$ | Isomalt GS |
| ---: | :--- |
| $4,10 \%$ | Gum arabic- solution ( $50 \%$ d.s.) |
| $0,05 \%$ | Acesulfam K |
| $0,05 \%$ | Aspartame |
| $1,00 \%$ | $\mathrm{TiO}_{2}$ |
| $39,80 \%$ | $\mathrm{Water}^{2}$ |
| $100,00 \%$ |  |
| 25 g | peppermint flavour |
| 2930 g | Isomalt GS-PA (as dry charge) |

The overall coating time was 69 min , the percentage layer amount (PLP) was $36,3 \%$. The layer was build in 26 cycles.
The ratio of solid to liquid Isomalt used was $2930 \mathrm{~g} / 1471 \mathrm{~g}=1,99$.

The amount of solid Isomalt in the coating material (PPPDL) is $2930 \mathrm{~g} / 4400 \mathrm{~g}=66,6 \%$.
The dragees have a smooth even and crunchy surface.

## Example 7:

A solution of isomalt GS ( $75 \% 1,6$-GPS and $25 \% 1,1-\mathrm{GPM}, \mathrm{w} / \mathrm{w}$ ) with the following recipe was used at $60^{\circ} \mathrm{C}$ for coating of $7,5 \mathrm{~kg}$ cushion-shaped centers in a Vario $500 / 600$ coater:

| $55,00 \%$ | Isomalt GS |
| ---: | :--- |
| $4,10 \%$ | Gum arabic- solution ( $50 \%$ d.s.) |
| $0,05 \%$ | Acesulfam K |
| $0,05 \%$ | Aspartame |
| $0,06 \%$ | Apple Green Shade colour |
| $40,74 \%$ | Water |
| $100,00 \%$ |  |
| 2180 g | Isomalt ST-PA with optionally $0,1 \% \mathrm{SiO}_{2}$ (as dry |
|  | charge) |

The overall coating time was 64 min , the percentage layer amount (PLP) was $29,0 \%$. The layer was build in 25 cycles.

The ratio of solid to liquid Isomalt used was $2180 \mathrm{~g} / 1262 \mathrm{~g}=1,73$.
The amount of solid Isomalt in the coating material (PPPDL) is $2180 \mathrm{~g} / 3442 \mathrm{~g}=63,3 \%$.
The dragees have a smooth, even and crunchy surface.

## Example 8:

A solution of Isomalt GS ( $75 \%$ 1,6-GPS and $25 \%$ 1,1-GPM, w/w) with the following recipe was used at $60^{\circ} \mathrm{C}$ for coating of $7,5 \mathrm{~kg}$ cushion-shaped centers in a Vario $500 / 600$ coater:

| $55,00 \%$ | Isomalt GS |
| ---: | :--- |
| $4,10 \%$ | Gum arabic- solution (50 \% d.s.) |
| $0,05 \%$ | Acesulfam K |
| $0,05 \%$ | Aspartame |
| $0,06 \%$ | Allura Red |


| $0,50 \%$ | $\mathrm{TiO}_{2}$ |
| ---: | :--- |
| $\underline{40,24 \%}$ | Water |
| $100,00 \%$ |  |
| 2580 g | Isomalt ST-PA with optionally $0,1 \% \mathrm{SiO}_{2}$ (as dry |
|  | charge) |

The overall coating time was 65 min , the percentage layer amount (PLP) was $36,0 \%$. The layer was build in 23 cycies.

The ratio of solid to liquid Isomalt used was $2580 \mathrm{~g} / 1326,7 \mathrm{~g}=1,94$.
The amount of solid Isomalt in the coating material (PPPDL) is $2580 \mathrm{~g} / 3906,6 \mathrm{~g}=66,0 \%$.
The dragees have a smooth, even and crunchy surface.

## Example 9:

A solution of Isomalt GS ( $75 \%$ 1,6-GPS and $25 \% 1,1$-GPM, w/w) with the following recipe was used at $60^{\circ} \mathrm{C}$ for coating of $7,5 \mathrm{~kg}$ cushion-shaped centers in a Vario 500/600 coater:

| $55,00 \%$ | Isomalt GS |
| ---: | :--- |
| $4,10 \%$ | Gum arabic- solution (50 \% d.s.) |
| $0,05 \%$ | Acesulfam K |
| $0,05 \%$ | Aspartame |
| $0,01 \%$ | Vegex color yellow |
| $0,50 \%$ | $\mathrm{TiO}_{2}$ |
| $40,29 \%$ | $\mathrm{Water}^{100,00 \%}$ |

The overall coating time was 53 min , the percentage layer amount (PLP) was $30,1 \%$. The layer was build in 21 cycles.

The ratio of solid to liquid Isomalt used was $2250 \mathrm{~g} / 1179,3 \mathrm{~g}=1,91$.
The amount of solid Isomalt in the coating material (PPPDL) is $2250 \mathrm{~g} / 3429,3 \mathrm{~g}=65,6 \%$.
The dragees have a smooth, even and crunchy surface.

## Example 10:

A solution of Isomalt GS ( $75 \%$ 1,6-GPS and $25 \% 1,1-G P M$, w/w) with the following recipe was used at $60^{\circ} \mathrm{C}$ for coating of $7,5 \mathrm{~kg}$ cushion-shaped centers in a Vario 500/600 coater:

| $55,00 \%$ | Isomalt GS |
| ---: | :--- |
| $4,10 \%$ | Gum arabic- solution (50 \% d.s.) |
| $0,05 \%$ | Acesulfam K |
| $0,05 \%$ | Aspartame |
| $0,02 \%$ | natural green color |
| $0,50 \%$ | $\mathrm{TiO}_{2}$ |
| $40,28 \%$ | Water |
| $100,00 \%$ |  |
| 2250 g | Isomalt ST-PA with optionally $0,1 \% \mathrm{SiO}_{2}$ (as dry |
|  | charge) |

The overall coating time was 50 min , the percentage layer amount (PLP) was $30,0 \%$. The layer was build in 21 cycles.

The ratio of solid to liquid Isomalt used was $2250 \mathrm{~g} / 1178,2 \mathrm{~g}=1,91$. The amount of solid Isomalt in the coating material (PPPDL) is $2250 \mathrm{~g} / 3429,3 \mathrm{~g}=65,6 \%$. The dragees have a smooth, even and crunchy surface.

## Example 11:

In a Driacoater 1600/1,25 with 4 nozzles 3 trials with 316 kg centers each and Isomalt in liquid and powder form were made. For a dragee layer buildup of $33,2 \%, 31,1 \%$ and $28,7 \%$ the coating time was $110 \mathrm{~min}, 108 \mathrm{~min}$ and 93 min . The respectively used powder amounts were $52,3 \%, 46,0 \%$ and $47,9 \%$.

## Example 12:

## Recipe:

| 5500 g | Isomalt GS |
| :--- | :--- |
| 3980 g | Water |
| 410 g | Gum arabic-solution $(50 \%)$ |
| 100 g | $\mathrm{TiO}_{2}$ |
| 5 g | Aspartame |
| 5 g | Acesulfam K |
| 12 g | Curcumin |
| 4 g | Eurolake Brilliant Blue |
| 10016 g | liquid coating medium |

1680 g Isomalt GS-PA in powder form

| phase | addition | liquid [ml] | powder [g] | liquid TS [g] | drying air [ $\left.{ }^{\circ} \mathrm{C}\right]$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 114 | 100 | 62,7 | 30 |
| 1 | 2 | 114 | 100 | 62,7 | 30 |
| 1 | 3 | 114 | 100 | 62,7 | 30 |
| 1 | 4 | 114 | 100 | 62,7 | 30 |
| 2 | 5 | 120 | 100 | 66 | 40 |
| 2 | 6 | 120 | 100 | 66 | 40 |
| 2 | 7 | 120 | 100 | 66 | 40 |
| 2 | 8 | 120 | 100 | 66 | 40 |
| 2 | 9 | 120 | 100 | 66 | 40 |
| 2 | 10 | 120 | 100 | 66 | 40 |


| 2 | 11 | 120 | 100 | 66 | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 12 | 120 | 100 | 66 | 40 |
| 3 | 13 | 132 | 100 | 72,6 | 50 |
| 3 | 14 | 132 | 76 | 72,6 | 50 |
| 3 | 15 | 132 | 76 | 72,6 | 50 |
| 3 | 16 | 132 | 76 | 72,6 | 50 |
| 3 | 17 | 132 | 76 | 72,6 | 50 |
| 3 | 18 | 132 | 76 | 72,6 | 50 |
| 3 | 19 | 132 |  | 72,6 | 50 |
| 4 | 20 | . 120 |  | 66 | 30 |
| 4 | 21 | 120 |  | 66 | 30 |
| 4 | 22 | 120 |  | 66 | 30 |
| 4 | 23 | 120 |  | 66 | 30 |
| 5 | 24 | 104 |  | 57,2 | 30 |
| 5 | 25 | 104 |  | 57,2 | 30 |
| 5 | 26 | 104 |  | 57,2 | 30 |
| 6 | 27 | 84 |  | 46,2 | 30 |
| 7 | 28 | 0 |  | 0 | 50 |
| 8 | 29 | 0 |  | 0 | 25 |
| 9 | 30 | 60 |  | 33 | 25 |
|  | Total | 3276 ml | 1680 g | 1801,8 g |  |
| Total dry |  |  |  |  |  |
|  | substance |  | $3481,8 \mathrm{~g}$ |  |  |
| Percentage |  |  |  |  |  |
|  | of powder |  | 48,3 \% |  |  |

$7,5 \mathrm{~kg}$ of cushion-shaped chewing gum centres were coated with isomalt in a Driacoater Vario $500 / 600$. The temperature of the coating solution was $60^{\circ} \mathrm{C}$.

It has to be noted that the quantity of ingredients mentioned in the above recipe $(10016 \mathrm{~g})$ does not correspond to the amount of fluids ( 3276 ml ) actually applied as a coating, since when conducting such experiments, a significant amount of wastage has to be considered (inevitable losses in containers, pipes etc.). In contrast to this, the amount of powder in the recipe $(1680 \mathrm{~g})$ corresponds exactly to the amount of powder actually applied $(1680 \mathrm{~g})$, as the powder is added to the coating bed directly after weighing without any loss.

The coating scheme in the figure shows the quantities of applied substances (liquid coating [ ml ], dry substance in liquid coating [g] and powder addition [g]) in the various coating phases as well as the drying air temperature and the numbers of coating cycles. The proportional amount of powder in the coating is $48,3 \%$. The proportional amount of coating, calculated from the average weight difference, was $29,2 \%$. The coating time (without wax-polishing) was 86 minutes. One special feature is the short heating at the end of the coating process before wax-polishing.

## Example 13:

$7,0 \mathrm{~kg}$ gum arabic-pregummed, chocolate-coated hazelnuts were coated in a Driacoater Vario 500/600 with the following recipe:

| 6500 g | $65,6 \%$ | Isomalt GS |
| :--- | :--- | :--- |
| 2980 g | $30,1 \%$ | Water |
| 410 g | $4,1 \%$ | gum arabic solution (50\%) |


| 10 g | $0,1 \%$ | Aspartame/Acesulfam K-mixture (1:1) |
| :--- | :--- | :--- |
| 10 g | $\underline{0,1 \%}$ | Tatrazine |
|  | $100 \%$ |  |

The solution was kept at $55^{\circ} \mathrm{C}$; the powder additions were added in the first eleven additions, with an amount of 100 g powder each (11 times).

The coating time was 157 min , the powder addition in the dragee layer was $32,1 \%$. Due to the temperature-sensitive centres (chocolate) the drying air had a temperature of $20^{\circ} \mathrm{C}$. The layeramount was $29,1 \%$ of the end product.

100 pieces (minus 5 with the lowest weight) each of uncoated, conventionally coated and pieces of this example were compared according to the uniformity of their weights. The average weight of the uncoated centres (chocolate-coated hazelnuts) was $2,562 \mathrm{~g}$ with a standard deviation of $0,318 \mathrm{~g}(=11,1 \%$ relative standard deviation $)$.

The conventionally Isomalt-coated product had an average weight of $3,497 \mathrm{~g}$ with a standard deviation of $0,400 \mathrm{~g}(=11,4 \%$ relative standard deviation $)$.

Dragees according to the inventive process had an average weight of $3,665 \mathrm{~g}$ with a standard deviation of $0,396 \mathrm{~g}(=10,8 \%$ relative standard deviation $)$.

This is a clear indication for a smoothing and averaging effect of the inventive process.

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A process for producing pan-coated products, comprising a core and a nonhygroscopic coating, where the coating comprises at least one layer, and the coating is applied to the core by preparing, as coating medium, a solution or suspension of one or more polyols and in a process step a) applying this coating medium to the core, for the purpose of applying one layer, and then, in a process step b), dusting with one or more polyols in powder form, and subsequently, in a process step c), carrying out drying with air at $20^{\circ} \mathrm{C}-80^{\circ} \mathrm{C}$, the amount of the polyol or polyols in powder form present in the final coating being from $30 \%$ to $75 \%$ by weight (based on total solids content of the polyol or polyols in the coating), it being an optional possibility to repeat steps a), b) and c) two or more times in alternation, wherein the polyol or polyols is/are xylitol, erythritol, mannitol, 1,1-GPM (1-O- $\alpha$-D-glucopyranosyl-Dmannitol), 1,6-GPS (6-O- $\alpha$-D-glucopyranosyl-D-sorbitol), 1,1-GPS (1-O- $\alpha$-D-glucopyranosyl-D-sorbitol), or mixtures thereof and wherein the polyol or polyols added in powder form used for dusting has/have a particle size distribution of $90 \%<50 \mu \mathrm{~m}$.
2. The process as claimed in claim 1, wherein the non-hygroscopic coating is a sugar-free coating.
3. The process as claimed in claim 1 or claim 2, where the coating comprises two or more layers up to a large number of layers.
4. The process as claimed in any one of claims 1 to 3 , wherein the amount of the polyol or polyols in powder form present in the final coating being from $40 \%$ to $75 \%$ by weight (based on total solids content of the polyol or polyols in the coating).
5. The process as claimed in claim 4, wherein the amount of the polyol or polyols in powder form present in the final coating being from $50 \%$ to $60 \%$ by weight (based on total solids content of the polyol or polyols in the coating).
6. The process as claimed in any one of claims 1 to 5 , it being an optional possibility to repeat steps a), b) and c) 5 to 50 times in alternation.
7. The process as claimed in claim 6, it being an optional possibility to repeat steps a), b) and c) from 20 to 40 times in alternation.
8. The process as claimed in any one of claims 1 to 7 , wherein the solids content of the coating medium is in the range from $30 \%$ to $90 \%$.
9. The process as claimed in claim 8 , wherein the solids content of the coating medium is in the range from $50 \%$ to $70 \%$.
10. The process as claimed in any one of claims 1 to 9 , wherein the polyol present in dissolved form and/or as a suspension constituent and/or the polyol used for dusting is selected from the group consisting of disaccharide alcohols.
11. The process as claimed in any one of claims 1 to 10 , wherein the polyol is isomalt, a 1,6-GPS-enriched mixture of 1,1-GPM and 1,6-GPS, a 1,1-GPM-enriched mixture of 1,1GPM and 1,6-GPS or a mixture of 1,1-GPM, 1,6-GPS and 1,1-GPS.
12. The process as claimed in any one of claims 1 to 11 , wherein the temperature of the coating medium during application of the coating layer(s) is from $25^{\circ} \mathrm{C}$ to $90^{\circ} \mathrm{C}$.
13. The process as claimed in claim 12, wherein the temperature of the coating medium during application of the coating layer(s) is from $45^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$.
14. The process as claimed in any one of claims 1 to 13 , wherein the temperature of the drying air in step c) is from $20^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$.
15. The process as claimed in any one of claims 1 to 14 , wherein gum arabic, flavors, colors, active substances, intensive sweeteners, active pharmaceutical substances, nutraceuticals and/or tooth mineralizing substances are used in the coating.
16. The process as claimed in any one of claims 1 to 15 , wherein after a first group of layers a second group of layers with a different composition is applied, such as a group of layers containing color, for example.
17. The process as claimed in claim 16, wherein the polyol of the second type of layer is isomaltulose, erythritol or xylitol.
18. The process according to any one of claims 1 to 17 , wherein the powder and/or the coating medium contains a free flow agent, an anticaking compound, a flowability enhancer for the powder, in particular $\mathrm{SiO}_{2}$ and/or a compound modifying the viscosity and/or surface tension of the coating medium.
19. A pan-coated product produced by the process of any one of claims 1 to 18 .
20. The product of claim 19, selected from the group consisting of confectioneries, nuts, hard and soft caramels, hard and soft snack articles, tablets, compacts and chewing gum candies.
21. The product of claim 19, comprising an animal feed, seed, pesticide-containing body, herbicide-containing body, catalyst, laundry detergent or the like.
22. The product according to any one of claims 19 to 21 , comprising in its coating an anticaking compound, a flowability enhancer for the powder, in particular $\mathrm{SiO}_{2}$ and/or a compound modifying the viscosity and/or surface tension of the coating medium.
23. The process according to claim 1, substantially as hereinbefore described with reference to the Examples.
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Figure 1
