Title: SURGICAL ROD BENDING SYSTEM AND METHOD

Abstract: A system and method for bending a surgical rod using an automated bending system includes receiving an indication of a plurality of line segments defined on the rod and an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments. Bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments are determined and operation of the automated bending system is controlled using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments.
SURGICAL ROD BENDING SYSTEM AND METHOD

CROSS-REFERENCE
[0001] This application is based on, claims priority to, and incorporates herein by reference in its entirety U.S. Provisional Application Serial No. 81/733,752, filed December 5, 2012, and entitled "SURGICAL ROD BENDING SYSTEM AND METHOD."

BACKGROUND OF THE INVENTION
[0002] The present application is directed to systems and methods for surgical rod bending. More particularly, the present invention relates to a system and method for controlling a surgical rod bending system to effectuate improved creation of surgical rods.
[0003] Surgical rods are used with bone screws in spine surgery to add stability to and/or correct curvatures of the spine. Surgical rods often have to be contoured to fit a desired curve of the spine and to intersect with sometimes irregular locations of bone screw heads.
[0004] Currently, the most common method for imparting complex bends to surgical rods is entirely manual. A surgeon must first determine the desired curvature of the rod by temporarily positioning a flexible surrogate rod in the bone screw heads and bending the surrogate rod by hand until it fits properly in each bone screw head. The surgeon must then remove the surrogate from the surgical table and take the surrogate to a side table where it is used as a visual guide to bend an actual surgical rod with a manual rod-bending tool. This procedure is subjective and can lead to metal fatigue if the surgical rod is accidentally over-bent and then re-bent in the opposite direction. In addition, this method can often subject the surgical rod to an increased risk of surface damage caused by accidental contact with sharp metal tools, resulting in local stress riser points and potential rod breakage after implantation. This method is also time-consuming, especially for inexperienced surgeons.
[0005] Attempted solutions to the above manual methods involve automated mapping and bending of surgical rods. For example, some newer systems include an input device that receives or calculates virtual coordinates of a surgical rod with a desired curvature, and a motorized rod-bending device that bends a surgical rod according to the coordinates. More specifically, the coordinates are used to produce
bend commands for controlling linear and rotational movement of a straight surgical rod as it is fed through the motorized rod-bending device. The bend commands are also used to control a force-actuating mechanism which bends the surgical rod around a post as it is fed through the motorized rod-bending device.

[0006] Common force-actuating mechanisms include bending arms which impose a radial or rotating force on the surgical rod so that the surgical rod bends around the post. These force-actuating mechanisms tend to be bulky and require substantially large systems for applying enough force to bend the surgical rods. In addition, some force-actuating mechanisms fail to provide enough support for the surgical rod to ensure that bending only occurs at the desired points. Other force-actuating mechanisms provide such support but, as a result, impose additional limitations such as restricting the degree of rotation of the surgical rod as it is fed through the rod-bending device. These restrictions limit the range of bending capabilities of the rod-bending device and therefore only permit certain combinations of rotation and bending.

[0007] Therefore, it would be desirable to provide a compact system to automatically bend a surgical rod to a desired curvature. Furthermore, it would be desirable to have such system sufficiently support the surgical rod without restricting its range of bending capabilities. Further still, it would be desirable to have methods and apparatuses for creating, detecting, and finalizing a desired curvature of a surgical rod using an automatic rod bending system.

SUMMARY OF THE INVENTION

[0008] The present invention overcomes the aforementioned drawbacks by providing an automated surgical rod bending system that permits full rotation of a surgical rod as it passes through the system, independent of previous bends performed along the length of the surgical rod. The present invention additionally incorporates methods for detecting a desired curvature of a surgical rod and outputting such detection information to the automated surgical rod bending system. Further still, the present invention provides methods for controlling an automatic rod bending system.

[0009] In accordance with one aspect of the invention, a method is disclosed for bending a rod configured to be implanted into a patient. The method includes determining a shape for the rod to be formed into to allow a rod to be implanted into
a patient, determining a plurality of pedicle points along the rod where pedicle screws will attach the rod to the patient when the rod is in the shape, and determining a plurality of intermediate points along the rod and between the plurality of pedicle points. The method also includes identifying a plurality of line segments defined by adjacent ones of at least one of the plurality of pedicle points and the plurality of intermediate points and determining an angle measurement to be formed between at least two adjacent ones of the plurality of line segments to form the rod into the shape. The method further includes determining bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments and feeding the rod into a bending system configured to bend the rod into the shape using at least one of the bending parameters and the angle measurement.

[0010] In accordance with another aspect of the invention, a system is disclosed for bending a rod into a shape designed for implantation into a patient. The system includes a plurality of guide rollers, a linear movement device configured to axially feed the rod in a first direction between the plurality of guide rollers, and a rotational movement device configured to rotate the rod as it is axially fed between the plurality of guide rollers. The system also includes a bending device configured to impose bending forces against the rod in a second direction perpendicular to the first direction after it is fed between the plurality of rollers. The bending device is positioned adjacent to the plurality of guide rollers so that the imposed bending forces against the rod causes the rod to bend along a curve of one of the plurality of guide rollers. The system further includes a controller configured to receive an indication of a plurality of line segments defined on the rod and an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments. The controller is further configured to identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments and control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments.

[0011] In accordance with another aspect of the invention, a system is disclosed for bending a rod into a shape designed for implantation into a patient. The system includes a base including a base passage extending there through, a linear
movement device configured to axially feed the rod in a first direction through the base passage, and a rotational movement device coupled to one of the base and the linear movement device, the rotational movement device configured to rotate the rod while being fed through the base passage by the linear movement device. The system also includes a bending device moveable in a second direction perpendicular to the first direction to impose bending forces against the rod and a controller. The controller is configured to receive an indication of a plurality of sine segments defined on the rod and an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments. The controller is also configured to identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments and control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments.

[0012] The foregoing and other aspects and advantages of the invention will appear from the following description, in the description, reference is made to the accompanying drawings which form a part hereof, and in which there is shown by way of illustration a preferred embodiment of the invention. Such embodiment does not necessarily represent the full scope of the invention, however, and reference is made therefore to the claims and herein for interpreting the scope of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013] Fig. 1 is a perspective view of an automated surgical rod bending system in accordance with and/or for use with the present invention.

[0014] Figs. 2 and 3 are perspective and cross-sectional schematic views, respectively, of a rod guide for use with the system of Fig. 1.

[0015] Figs. 4A and 4B are a series of perspective views of the system of Fig. 1 in different linear positions.

[0018] Figs. 5A-5C are a series of perspective views of the system of Fig. 1 in different rotational positions.

[0017] Fig. 6 is a partial top view of the system of Fig. 1.

[0018] Fig. 7 is a partial perspective view of the system of Fig. 1.

[0019] Fig. 8 is a schematic view of an automated surgical rod bending system in accordance with and/or for use with the present invention.
[0020] Fig. 9 is a schematic view of a surrogate rod for use with the present invention.
[0021] Figs. 10A and 10B are schematic side and top views, respectively, of a surrogate rod and an optical scanner for use with the present invention.
[0022] Fig. 11 is a schematic view of a digitizing probe for use with the present invention.
[0023] Fig. 12 is a schematic illustration of a plurality of pedicle screw locations determined in accordance with the present invention.
[0024] Fig. 13 is a schematic illustration of the plurality of pedicle screw locations of Fig. 12 and a hypothetical rod shape coupled thereto in accordance with the present invention.
[0025] Fig. 14 is a schematic illustration of the plurality of pedicle screw locations of Fig. 12 and the hypothetical rod shape of Fig. 13 coupled thereto and a plurality of intermediate points selected in accordance with the present invention.
[0026] Figs. 15A through 15P are schematic diagrams illustrating a two-dimensional sequential bending process of a rod using the plurality of pedicle screw locations of Fig. 12, the hypothetical rod shape of Fig. 13 coupled thereto, and the plurality of intermediate points selected in Fig. 14.
[0027] Fig. 18 is a schematic illustration comparing the planned spline to the fitted rod after completing the bending sequence of Fig. 15.
[0028] Fig. 17 is a schematic illustration of a rod being bent in accordance with the present invention.
[0029] Fig. 18 is a schematic illustration of determining a lost path distance in accordance with the present invention.
[0030] Figs. 19A-19C are schematic illustrations of determining a recoil in accordance with the present invention.

DETAILED DESCRIPTION OF THE INVENTION

[0031] Fig. 1 illustrates an automated surgical rod bending system 10 according to the invention. The system 10 can be used to automatically bend a substantially straight rod to a desired curvature. For example, the system 10 can be used in an operating room to automatically bend an implantable surgical rod for pedicle screw surgery.
In some embodiments, as shown in Fig. 1, the system 10 can include a base 12, a linear movement device 14, a rotational movement device 16, a bending device 18, a receiving container 20, a rod guide 22 (as shown in Figs. 2 and 3), and a controller 23. The controller 23, as will be described, can be in communication with and can operate the linear movement device 14, the rotational movement device 18, and/or the bending device 18 (for example, by controlling motors for each device 14, 16, 18, as described below). Additionally or alternatively, a computer system or a separate controller 25 may be coupled to the system 10, such as through a cable 27 or wireless connection, to coordinate operation with the controller 23 or to control the system 10 without the controller 23. For example, the computer/controller 25 may include a user interface 29 configured to receive input used to automatically bend a rod. Also, as shown in Figs. 4A-5C, the system 10 can include a rod holder 24 coupled to the linear movement device 14 for holding a surgical rod 28. As will be described, the bending device 18 may be designed to also achieve cutting of the surgical rod 28 in addition to bending.

In operation, the system 10 can rigidly hold the trailing end of the surgical rod 26, feed the surgical rod 26 axially through a passage 28 of the base 12 (as best shown in Figs. 6 and 7), and rotate the surgical rod 26 so that bending can be imposed in a desired direction. More specifically, the surgical rod 26 can be coupled to or secured by the rod holder 24. The controller can operate the linear movement device 14 to vertically feed the surgical rod 26 through the base passage 28 into the receiving container 20. As the surgical rod 26 is fed through the base 12, the bending device 18 can impose bends at different points along the length of the surgical rod 26 and, in some configurations, can cut the surgical rod 26 at a desired length. Further, the rotational movement device 16 can control the rotational orientation of the surgical rod 28 with respect to the bending device 18 as the surgical rod 26 is fed through the base 12.

In some embodiments, the linear movement device 14 can be a linear actuator mounted substantially perpendicular to the base 12 and controlled by a first stepper motor 33, as shown in Fig. 5C. The linear movement device 14 can be positioned so that its movement axis is substantially vertical. For example, Figs. 4A and 4B show the linear movement device 14 in a first position and a second, vertically lower position, respectively. The first stepper motor 33 can control the
linear movement device 14 to feed the surgical rod 28 vertically down through the base passage 28 at programmed length increments. In one embodiment, as shown in Fig. 1, the linear movement device 14 can be coupled to the rotational movement device 16 by a coupling mechanism 30 and fasteners 32.

[0035] In some embodiments, the rotational movement device 16 can include a rotational actuator 34 mounted substantially parallel to the base 12 and controlled by a second stepper motor 38, as shown in Figs. 4A-4B. The rotational movement device 16 can also include a rotatable platform 38 coupled to the rotational actuator 34, for example via a rotational bearing (not shown) embedded in the platform 38. The platform 38 can also include a platform passage (not shown) aligned with the base passage 28. The linear movement device 14 can be coupled to the platform 38, as described above, allowing the rotational movement device 16 to control the radial orientation of the linear movement device 14, and thus, the surgical rod 26 with respect to the bending device 18. The second stepper motor 38 can operate the rotational movement device 16 to rotate in one or both directions (that is, positive or negative rotation) between zero degrees and about 360 degrees in programmed increments. For example, Fig. 5A shows the rotational movement device 16 in a first position, Fig. 5B shows the rotational movement device 16 in a second position rotated from the first position by a first degree amount, and Fig. 5C shows the rotational movement device 16 in a third position further rotated from the first position by a second, larger degree amount. In one embodiment, the rotational movement device 16 can be controlled to rotate in increments of about 0.005 degrees.

[0036] In some embodiments, the rod guide 22 can be coupled to the platform 38 so that it extends through the platform passage and terminates adjacent to the bending device 18 and/or the base passage 28. As shown in Figs. 2 and 3, the rod guide 22 can be substantially cylindrical and can include a rod passage 54 for receiving and guiding the surgical rod 26 as it is fed vertically through the platform passage. Bending can be imposed on the surgical rod 28 by the bending device 18 as it exits the rod guide 22.

[0037] In some embodiments, the rod passage 54 can terminate with a flared base 56. More specifically, one end of the rod passage 54 (that is, the end adjacent to the base passage 28) can extend radially outward so as to form a outwardly tapering surface that forms a substantial flare outward, as shown in Figs. 2 and 3. As
illustrated, this flared base 58 may advantageously be formed to present a convex surface against which the surgical rod 28 can bend or curve as bending forces are applied by a bending roller 46, as further described below. Other geometries may be used; however, the flared or convex surface provides an advantageous geometry against which to bend the surgical rod 28 without incurring sharp bends that, for example, may present an unfavorable discontinuous bend (such as those created if the rod is bent too sharply) and/or structural weakness. The cylindrical portion of the rod passage 54 can provide substantial support for the surgical rod 26 to prevent bending or increased stress at other points along the length of the surgical rod 26 as it is bent by the roller 46 and the flared base 56. In one embodiment, the rod guide 22 can rotate with the platform 38 and with the surgical rod 26, allowing bending of the surgical rod 28 to occur against any surface segment of the flared base 58. In another embodiment, the rod guide 22 can remain stationary, allowing the surgical rod 26 to rotate within the rod passage 54 so that bending can occur against the same surface segment of the base 58. In this case, the geometry of the base 58 can be made such that it is only convex on the side against which bending force from the bending device is applied. In addition, in some embodiments, the rod guide 22 can be manufactured from stainless steel or a similar material.

[0038] In some embodiments, as shown in Figs. 8 and 7, the bending device 18 can be coupled to the base 12 and can include a trolley 42 moveable along linear slides 44, a roller 46 coupled to the trolley 42, a cutting wheel 48 coupled to the trolley 42, a scissors jack 50 coupled to the trolley 42, and a third stepper motor 52. The scissors jack 50 allows the bending device 18 to exert large linear forces with a low torque requirement of a driving motor. Other mechanisms for creating linear forces can be used, such as screw drive mechanisms or electromagnetic, hydraulic, or pneumatic piston actuators. The third stepper motor 52 can be operated in forward and reverse to move the scissors jack 50 between a retracted position (as shown in Fig. 6) and an extended position. Extension and retraction of the scissors jack 50 can cause the trolley 42 to traverse across the base passage 28 in a first horizontal direction (for example, away from the third stepper motor 52) and a second horizontal direction (for example, toward the third stepper motor 52). As the surgical rod 26 is vertically fed through the base passage 28, movement of the trolley 42 in the first horizontal direction can allow the roller 46 (for example, a roller bearing) to contact the surgical rod 26, causing the surgical rod 26 to bend. In
addition, movement of the trolley 42 in the second direction can allow the cutting wheel 48 to contact and cut the surgical rod 26. In some embodiments, as shown in Fig. 1, the system 10 can include a block 31 or similar stability component coupled to the base 12 and one side of the scissors jack 50 (i.e., the side opposite the trolley 42) can be coupled to the block 51. The block 51 can provide a non-moving part for the scissors jack 50 to press against so that retraction and extension of the scissors jack 50 causes linear movement of the trolley 42.

[0039] The third stepper motor 52 and the scissors jack 50 can provide sufficient force to allow the roller 48 to exert bending forces against the surgical rod 26. The increment of distance of travel of the linear movement device 14 and the distance of travel of the bending device 18 toward the surgical rod 26 can affect the type of bend that results. For example, a gentle bend can be imposed by feeding the surgical rod 28 in small increments by advancing the linear movement device 14 and applying minimal displacement of the bending device 18 at each increment, or a sharper bend can be imposed by applying a large displacement of the bending device 18 without incrementing the linear movement device 14, forcing the surgical rod 28 to conform to the flared base 58. In one embodiment, a minimal possible bend curvature imposed on the surgical rod 26 can be dependent on the curvature of the flared base 56. As the name implies, the roller 46 can roll in order to minimize shear forces against the surgical rod 28 as it is bent against the flared base 58.

[0040] In addition, in some embodiments, the cutting wheel 48 can be diamond-tipped and/or can be rotatable (for example, by a motor 53, as shown in Fig. 6, connected to an external power source) to permit a substantially clean cut across the surgical rod 26. In other embodiments, the cutting wheel 48 can be substituted with pliers, guillotine, or other mechanical or electrical cutting devices. In some embodiments, components of the linear movement device 14, the rotational movement device 16, and/or the bending device 18 can be manufactured from aluminum and/or stainless steel.

[0041] In other embodiments, the base 12 can comprise a different orientation relative to the linear movement device 14, the rotational movement device 16, and/or the bending device 18. For example, the bending device 18 can have a supporting base mechanism that allows it to be oriented at any angle in the plane of the base 12 relative to the platform passage of the bending device 18, thereby allowing bending
to occur in more than one direction. In addition, in some embodiments, the bending device 18 may only include components for bending the surgical rod 28, while a separate, independent device includes components for cutting the surgical rod 28, and vice versa.

[0042] In conventional rod benders, previous bends may prevent a surgical rod from being rotated in a certain direction to impose subsequent bends. This limitation is often due to such conventional rod benders requiring rod guides that extend past the bending device, or requiring the bend to occur while the rod rests flat against a planar surface. in some embodiments, due to the relative orientation of the linear movement device 14, the rotational movement device 16, the rod guide 22, and the bending device 18, the system 10 may be free of barriers or other components contacting the surgical rod 26 after it passes across the bending device 18 (that is, after it is fed past the roller 46). In addition, the receiving container 20 can be substantially large enough to allow free movement of the surgical rod 28 as it is fed through the base 12 until it is cut by the bending device 18. As a result, the system 10 can allow unlimited rotation of the surgical rod 26 in either direction for subsequent bending, independent of the previous bends made. In addition, in comparison to manual rod bending, the system 10 can produce an accurately bent surgical rod 26 in minimal time.

[0043] In some embodiments, the controller can control each of the stepper motors 33 (causing linear actuation), 38 (causing rotation actuation), 52 (causing bending device actuation). In other embodiments, each of the stepper motors 33, 38, 52 can be controlled by individual controllers. Each stepper motor 33, 36, 52 can be pre-programmed to perform its respective movement operations in predetermined increments. For example, the third stepper motor 52 can control movement of the scissors jack 50 in predetermined increments in order to achieve a desired bend. Also, one or more of the stepper motors 33, 36, 52 can be programmed to operate additional components of the system 10. In one embodiment, the controller can control a relay that powers the motor 53 for rotation of the cutting wheel 48. In another embodiment, a switch can be activated to power the cutting wheel motor 53 when the trolley 48 of the bending device 18 crosses an optical sensor or touch sensor (for example, as it moves the cutting wheel 48 in proximity to the surgical rod 28).
In some embodiments, a shield or housing (not shown) can enclose some or all of the components of the system 10. For example, in one embodiment, a protective shield can substantially block access to the bending device 18 during operation of the system 10. In addition, in some embodiments, the system 10 can include a sterilization mechanism (e.g., an autoclave or another suitable sterilization mechanism) to sterilize the surgical rod 28 and/or remove metal debris at the cut locations of the surgical rod 26 after it has passed across the bending device 18.

Fig. 8 illustrates the system 10 according to another embodiment of the invention. As shown in Fig. 8, the system 10 can include the linear movement device 14 with linear bearings 58, the rotational movement device 16 including the second stepper motor 36, the rod holder 24, and the bending device or actuator 18 including the bending roller 46 and a cutting blade 60, and a controller 61 (for example, similar to the controller described above with respect to Figs. 1-7). The system 10 can also include guide rollers 62 that help guide the surgical rod 26 as well as provide a convex surface against which the rod 26 can bend when horizontal force is applied by the bending roller 46.

In the embodiment shown in Fig. 8, the linear movement device 14 can remain stationary, but move the rotational movement device 18 in a linear manner for vertically feed the surgical rod 26 past the bending roller 46. The rotational movement device 16 can cause rotation of the rod holder 24 (for example, via a rotating shaft 83 coupled to the rod holder 24) in order to rotate the surgical rod 26 as it is vertically fed past the bending roller 46. In addition, the horizontal bending forces imposed by the roller 46 against the surgical rod 28 can cause the surgical rod 28 to bend along a curve of one of the guide rollers 62. Once a desired length of the surgical rod 26 has been fed past the roller 46, the cutting blade 60 can be triggered to cut the surgical rod 26.

In some embodiments, the system 10 can be interfaced with an apparatus (not shown) that detects or calculates the desired curvature of a surgical rod and outputs bending commands to the controller 61 of the system 10. The controller 61 can manipulate the position and rotation of the straight surgical rod 26 as it is passed through the system 10 and the amount of travel of the bending roller 46 based on the bending commands.
The apparatus can apply one or more methods for determining or detecting a desired surgical rod curvature. For example, a first method can include optical digitization of a surrogate rod 84, as shown in Figs. 9-10B. The surrogate rod 64 can have mechanical properties similar to a piece of heavy electrical wire and can be bent by a surgeon by hand (that is, without tools) to align with pedicle screws implanted in a patient. Indicators 66, such as clips or markers, can be applied to the surrogate rod 84 to identify desired termini of the rod, screw head locations, possible bone collision points, etc., as shown in Fig. 9. An optical scanner 88 can then be used to scan the surrogate rod 84 and transmit optical scan information to the apparatus. In one embodiment, the surrogate rod 64 can be fed across the optical scanner 68 at a fixed rate, as shown in Figs. 10A and 10B. The optical scanner 68 can detect rod angles in two planes, or "x" and "y" location coordinates, along an array of linear "z" positions to provide a three-dimensional optical scan.

The apparatus can analyze the scan information, digitally map a three-dimensional model of the surrogate rod 64, and calculate a proposed curvature of the surgical rod 28 (for example, by applying a mathematical spline fit to the three-dimensional model). The apparatus can then transmit bend commands to the system 10 based on the proposed curvature. Other commands can be determined based on the locations of the indicators. For example, the apparatus can output cutting commands where terminus indicators 66 were located on the surrogate rod 64. The apparatus can also minimize bending of the surgical rod 26 where screw head indicators 66 or possible bone collision indicators 88 were located on the surrogate rod 64. Elimination of bends at these points can permit easier insertion of the surgical rod 26 into the slots in the pedicle screw heads after the rod 26 has been bent.

A second method for defining surgical rod curvature can include a digitizing probe 70, as shown in Fig. 11, and an optical system (such as OptoTrak Certus® system or a similar system) to determine key points along a patient's spine during surgery. A surgeon can use the digitizing probe 70 to identify key points, such as screw heads 72, desired termini of the surgical rod, and/or bony structures that might interfere with the surgical rod, as shown in Fig. 11. Markers on the digitizing probe 70 can allow the optical tracking system to accurately track the location of the probe tip as the surgeon identifies the key points. The apparatus can apply a mathematical
spline fit (or another suitable curve fit) to define the desired curvature of the surgical rod based on the key points identified and transmit bend commands to the system 10 based on the defined curvature.

[0051] As described above, once curvature is defined using the optical scanning method, the digitization method, or another suitable method, the desired rod curvature can be used to create bend commands for the system 10. The apparatus and/or the controller 81 can make adjustments to the desired rod curvature to minimize bone collisions, bending at screw head locations, binding in the guide tube 54 due to bends by the system 10 that are too sharp, and/or other potential issues. These adjustments can minimize the stresses that surgical rods may experience after they are implanted.

[0052] The following paragraphs describe methods of using the system 10 for automatically creating bends in a surgical rod 28, in accordance with the present invention. As described above, the system 10 of the present invention is able to create complex bends in more than one plane. However, it is possible to conceptualize the three-dimensional (3D) bending to a two-dimensional (2D) problem to better understand the issues involved. As such, the following example will be described and illustrated in 2D, but can be extended to 3D.

[0053] Fig. 12 illustrates an example of a 2D bending problem. A series of pedicle screw heads 100 are shown, in Fig. 13, the series of pedicle screw heads 100 are illustrated as dictating the desired path of a hypothetical interconnecting rod 102, which can be automatically bent by the above-described system. Referring to Fig. 14, a spline fit 104 can be used to interconnect these screw heads 100 in a smooth, gentle curve. To do so, a plurality of points 0-9 are distributed along the spline 104. In this example, ten points 0-9 are identified along the spline path 104. As will be described, these points 0-9 can be used as the targets to which each bend aims to fit.

[0054] Referring now to Figs. 15A-15P, with the planning illustrated with respect to Figs. 12-14 in place, a rod 106 can be fed through the above-described system 10. At each increment, a bend is made by the system 10 to keep the rod 106 aligned with the spline 104 along the points 0-9 upon exit from the system 10. In this two-dimensional example, the bending roller 48 moves toward the right or the left to bend the rod in the plane drawn. In a three-dimensional implementation, the
rotational movement device 16 would orient the rod 106 to be bent in any plane. Note that each bend generally creates an angle between two line segments defined by the points 0-9. For example, angles can be measured between points 1, 2, and 3, to form 1-2-3 angle, between points 2, 3, and 4 to form 2-3-4 angle, and so on. By holding the line segment of higher numbering in the rod guide 22 of the system 10, which acts as a straight collar, and applying a bend on a given line segment of the lower numbering using the bending roller 46, each angle can be created. For example, as illustrated in Figs. 15C and 15D, the 1-2-3 angle is created by holding 2-3 straight and applying a bending force on 1-2. This same process can be applied for the 2-3-4 angle, as illustrated in Figs. 15E and 15F, and each additional angle, as illustrated in Figs. 15G through 15P, until, as illustrated in Fig. 16, the rod has been bent in a manner that matches the planned spline and layout of points 0-9 illustrated in Figs. 13 and 14.

[0055] Notably, the above-described process of bending alters the distance between points 0-9 as the rod 106 is bent and, to provide the results illustrated, these changes can be accounted for, as will be described. In particular, referring to Fig. 17, when the system applies a lateral bend along the direction indicated by arrow 110, below point 2, it changes the 1-2 segment from a straight line to a curved line. The change from straight line to curved line means path length is increased over a path in which a straight line segment connects points 1 and 2. Knowledge of the distance from point 1 to point 2 is desirable because the bend in this example is intended to position the 2-3 segment relative to what has already been bent below it. However, by the nature of the rod bending mechanism with the rod 108 gripped above and the bend occurring below point 2, the distance from point 2 to point 3 is fixed while the distance from point 1 to point 2 is not fixed. As a result, the amount of path length lost by bending must be predicted and added to an interval Y between bend points on the rod 106 considered while it is straight (i.e., the incremental rod feed distance) by taking into account a push travel distance "D-".

[0056] In particular, this concept is further illustrated with respect to Fig. 18. In Fig. 18, a bend is to be created by pushing point 1 from position 112 in the direction of arrow 110 b position 114, while holding point 2 stationary. However, when the rod 106 is bent to move point 1 to position 114, the bend in the rod 106 forms an arc instead of following a straight path between point 1 and point 2, creating a lost path of distance "D" or a $D_{lost path}$. The lost path length can be a function of the bend angle
(or pusher/roller linear travel), radius of curvature of the support (such as the flared base 58), and the composition and diameter of the rod material being bent. Therefore, an efficient way to incorporate the multiple factors into the calculation is to experimentally determine the relationship and apply it during automated bends. That is, a function “F” can be created for each type of rod being bent that satisfies:

\[ D_{\text{lost path}} = F(\text{pusher travel}) \]

[0057] For example, an operator can select the type of rod being bent and the radius of curvature of the support (if the support is interchangeable) and the controller can utilize a stored function for that material. With respect to stored functions, lost path distances may assessed experimentally at multiple pusher travels and a function can be fit to a resulting data set, which can then be stored for use by the controller. Such experiments can account for both lost path and bending recoil (discussed below) at the same time.

[0058] For example, a user can calibrate the system using a test rod similar or identical to the rod to be bent. The test rod can be inserted in the system and a bend applied using a set pusher travel distance. The test rod is fed forward by a set distance and another bend applied is applied using another set pusher travel distance. This process is repeated until the entire length of rod is used. Before applying bends or thereafter, optical tracking markers such as reflective spheres or infrared-emitting diodes that are trackable with high precision may be affixed on the test rod. Using tracking cameras to track the 3D locations of the tracking markers, points at which markers are attached can be stored to computer memory. The stored optical marker positions can be used to measure the bends, or the bend angle. Alternately, bent rods could be analyzed using optical analysis methods, such as photographing the rod against a grid background and counting rise over run, using a compass, or using a goniometer. An experiment such as described here need only be performed in a single bending plane to create suitable functions that are applicable in controlling 3D bending.

[0059] An example of usage of lost path distance is as follows. Starting with a straight rod 106 and in creating a bend of the line segment 1-2-3 in Fig. 17 sufficient for the rod 106 to match the planned spline, the flared base is positioned such that the flare initiates adjacent to point 1 on the rod 106. The rod 106 is then advanced downward by an interval (I), such that the point of initiation of the flare is adjacent to
point 2 on the rod 108. For an applied lateral force to the rod 108 at this position, the distance (D) that the rod 108 must be pushed before point 1 intersects with the spline curve is known from the spline equation. In this position, if the rod 106 were theoretically infinitely flexible and there was zero flare at the base, the rod 106 would bend at a sharp corner adjacent to point 2 and the distance from point 1 to point 2 would be the hypotenuse of the triangle having a side of height 1 and a base of width D. Note that D and 1 are interrelated; as D increases, 1 decreases. In reality, the rod 106 is not infinitely flexible and the base has a flare; therefore the lost path for the distance D traveled by the pusher is known from the experiment. This lost path distance can be accounted for by simply advancing the rod 106 by this amount, i.e., adding D_{lost \_path} to 1. Alternately, a point on the spline can be calculated that has a path length exactly D_{lost \_path} farther up the spline toward point 2. After increasing 1 or reassessing D to account for lost path and applying a lateral force to cause displacement D, the final resting location of point 1 on the rod 106 will be at the target position. That is, the actual shape of the rod 106 at all points between points 1 and 3 will be undetermined and will be dependent on material properties of the rod 106 and geometry of the base, but the specific points 1, 2, and 3 on the rod 108 will exactly intersect with the spline.

[8060] Another variable that may be considered is bending recoil. Specifically, referring to Figs. 19A-19C, the bend achieved when the pusher/roller element 46 is in contact with the rod 106 will not be the final bend achieved when the roller 46 is removed. Specifically, as illustrated in Fig. 19A, before the roller 46 engages the rod 108, the rod 106 is straight. The roller 46, as shown in Fig. 19B, engages the rod 106 and pushes it to an extreme angle. However, as illustrated in Fig. 19C, after the roller 46 disengages and is no longer applying a bend to the rod 106, the rod 106 will recoil to some extent but will retain a permanent bend. The amount of recoil "R" will depend upon material properties of the rod 106, such as ductility, elasticity, and the like, as well as geometry of the rod 106, such as diameter, cross-section, surface pattern, and the like. Some estimates of recoil "R" may be determined theoretically from geometry and material. However, the most reliable method for assessing and accounting for recoil "R" is using an experiment, such as described above with respect to lost path distance. Such experiments can be used to establish the relationship between pusher travel and actual bend achieved for a particular rod 106.
It should be apparent to those skilled in the art that the fit between intended curve and actual curve can be improved by decreasing the incremental rod feed distance (using a greater number of discrete points). However, if the incremental rod feed distance is less than the distance from the initiation of the flare to the contact point on the lateral pusher wheel, it becomes more complicated to predict the bending because the previous residual bend may have left the rod in a position where it comes into contact with the pusher wheel at a position offset from center. By the pusher contacting the already-bent rod sooner or later than it would have contacted a straight rod, over- or underbending might occur, unless effort is made to account for the previous bend. Detecting contact of the pusher with the rod allows the contact position to be uniquely determined for every bend and overcomes this issue. Non-limiting examples of mechanisms for detecting contact of the pusher with the rod include optical sensors detecting physical gap between pusher and rod, electrical conductivity or resistivity measurement methods, detecting flow of electricity between the rod and the pusher wheel, or force sensing such as strain gauges to measure force of the pusher against the rod.

In summary, at each bend increment, the system can determine how far a previous bend point on the rod needs to be displaced laterally by the pusher, as shown in Figs. 12-16. Using functions that are experimentally determined, the system can assess the pusher travel needed and the additional incremental rod feed needed so that this point is appropriately displaced to the desired position. By performing this procedure sequentially over the rod, it is possible to fit the incremental points exactly to the plan. In some cases, portions of the bent rod corresponding to portions of the spline curve between the discrete points may not overlay exactly with the spline, but the general rod shape should be excellent for interconnecting screw heads.

This application also incorporates by references herein in its entirety, pending PCT Application No. WO 2013/085982.

The present invention has been described in terms of one or more preferred embodiments, and it should be appreciated that many equivalents, alternatives, variations, and modifications, aside from those expressly stated, are possible and within the scope of the invention.
In the claims:

1. A system for bending a rod into a shape designed for implantation into a patient, the system comprising:
   - a base including a base passage extending there through;
   - a linear movement device configured to axially feed the rod in a first direction through the base passage;
   - a rotational movement device coupled to one of the base and the linear movement device, the rotational movement device configured to rotate the rod while being fed through the base passage by the linear movement device;
   - a bending device moveable in a second direction perpendicular to the first direction to impose bending forces against the rod; and
   - a controller configured to:
     - receive an indication of a plurality of line segments defined on the rod;
     - receive an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments;
     - identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments; and
     - control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments.

2. The system of claim 1 wherein identifying the bending parameters includes identifying at least one of a lost path distance and an amount of recoil.

3. The system of claim 2 further comprising a user interface configured to receive a user selection of the at least one of the lost path distance and the amount of recoil.

4. The system of claim 1 wherein the controller is further configured to receive an indication of at least one of a plurality of pedicle points and plurality of
intermediate points along the rod and, wherein the plurality of line segments is defined by adjacent ones of the at least one of a plurality of pedicle points and plurality of intermediate points.

5. The system of claim 1 further comprising a rod guide including a rod passage that receives the rod as it is axially fed by the linear movement device and a flared base at one end of the rod passage, wherein the rod guide is positioned adjacent to the bending device so that the rod exits the flared base prior to the bending device imposing the bending forces against the rod.

6. The system of claim 1 wherein the rotational movement device includes a rotatable platform and the linear movement device is coupled to the rotatable platform.

7. A system for bending a rod into a shape designed for implantation into a patient, the system comprising:
   a plurality of guide rollers;
   a linear movement device configured to axially feed the rod in a first direction between the plurality of guide rollers;
   a rotational movement device configured to rotate the rod as it is axially fed between the plurality of guide rollers;
   a bending device configured to impose bending forces against the rod in a second direction perpendicular to the first direction after it is fed between the plurality of rollers, the bending device positioned adjacent to the plurality of guide rollers so that the imposed bending forces against the rod causes the rod to bend along a curve of one of the plurality of guide rollers; and
   a controller configured to:
   receive an indication of a plurality of line segments defined on the rod;
   receive an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments;
   identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments; and
control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments.

8. The system of claim 7 wherein identifying the bending parameters includes identifying at least one of a lost path distance and an amount of recoil.

9. The system of claim 8 further comprising a user interface configured to receive a user selection of the at least one of the lost path distance and the amount of recoil.

10. The system of claim 7 wherein the controller is further configured to receive an indication of at least one of a plurality of pedicle points and plurality of intermediate points along the rod and, wherein the plurality of line segments is defined by adjacent ones of the at least one of a plurality of pedicle points and plurality of intermediate points.

11. A method for bending a rod configured to be implanted into a patient, the method comprising:
  determining a shape for the rod to be formed into to allow a rod to be implanted into a patient;
  determining a plurality of pedicle points along the rod where pedicle screws will attach the rod to the patient when the rod is in the shape;
  determining a plurality of intermediate points along the rod and between he plurality of pedicle points;
  identifying a plurality of line segments defined by adjacent ones of at least one of the plurality of pedicle points and the plurality of intermediate points;
  determining an angle measurement to be formed between at least two adjacent ones of the plurality of line segments to form the rod into the shape;
  determining bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments; and
  feeding the rod into a bending system configured to bend the rod into the shape using at least one of the bending parameters and the angle measurement.
12. The method of claim 11 wherein determining the bending parameters includes identifying at least one of a lost path distance and an amount of recoil.

13. The method of claim 11 wherein feeding the rod into the bending system includes rotating the surgical rod relative to a bending device.

14. The method of claim 13 wherein the rotating includes at least one of a positive rotation between about zero degrees and about 180 degrees and a negative rotation between about zero degrees and about 180 degrees.

15. The method of claim 11 wherein determining the bending parameters includes optically scanning a surrogate rod.

16. The method of claim 15 further comprising physically manipulating the surrogate rod to the shape and applying identifiers to the surrogate rod prior to optically scanning the surrogate rod.

17. The method of claim 15 wherein determining the bending parameters includes digitally mapping the plurality of pedicle points using a digitizing probe and comparing the plurality of pedicle points to the surrogate rod when the surrogate rod is formed into the shape.

18. The method of claim 17 wherein determining the bending parameters includes identifying at least one of a lost path distance and an amount of recoil based on comparing the plurality of pedicle points to the surrogate rod when the surrogate rod is formed into the shape.

19. The method of claim 15 wherein determining the bending parameters includes predicting a path length loss by bending the surrogate rod and adjusting the bending parameters using the path length loss.
20. The method of claim 11 wherein determining the bending parameters includes predicting an amount of recoil based on at least one of material properties of the rod and geometry of the rod.

21. The method of claim 20 wherein the material properties includes at least one of ductility and elasticity and the geometry includes at least one of diameter, cross-section, and surface pattern.
FIG. 12
INTERNATIONAL SEARCH REPORT

PCT/US 13/70773

A. CLASSIFICATION OF SUBJECT MATTER
IPC(8) - B21D 9/08 (2013.01)
USPC - 72/213

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
USPC: 72/213

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
USPC: 72/389.1, 390.4, 31.04, 31.05, 31.07, 31.08, 31.09 (keyword limited; terms below)

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
PatBase: Google Patents; Google
Search Terms Used: automatic, rod, pip, tub, bend, form, roller, flar, angl, bend, recoil, lost, path, pedicle, computer, controller, microprocessor

C. DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
<thead>
<tr>
<th>Category</th>
<th>Citation of document, with indication, where appropriate, of the relevant passages</th>
<th>Relevant to claim No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Y</td>
<td>US 2007/0227216 A1 (SCHALLIOL) 04 October 2007 (04.10.2007) fig 9, 10, para [0047][0050],[[0055]]</td>
<td>1-5</td>
</tr>
<tr>
<td>Y</td>
<td>US 3,661,002 A (PEDDINGHAUS JR.) 09 May 1972 (09.05.1972) fig 3, col 1, In 32-43, col 1, In 66-COL 2, In 19</td>
<td>2-3</td>
</tr>
<tr>
<td>Y</td>
<td>US 2009/0249851 A1 (ISAACS) 08 October 2009 (08.10.2009) para [0097]-[0098], [0102]</td>
<td>4</td>
</tr>
<tr>
<td>Y</td>
<td>US 4,785,650 A (LUSTY) 22 November 1988 (22.11.1988) entire document</td>
<td>1-6</td>
</tr>
</tbody>
</table>

Further documents are listed in the continuation of Box C.

* Special categories of cited documents:
  *A* document defining the general state of the art which is not considered to be of particular relevance
  *E* earlier application or patent but published on or after the international filing date
  *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
  *O* document referring to an oral disclosure, use, exhibition or other means
  *P* document published prior to the international filing date but later than the priority date claimed

* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

*E* document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

*F* document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

*G* document member of the same patent family

Date of the actual completion of the international search
11 March 2014 (11.03.2014)

Date of mailing of the international search report
27 MAR 2014

Name and mailing address of the ISA/US
Mail Stop PCT, Attn: ISA/US, Commissioner for Patents
P.O. Box 1450, Alexandria, Virginia 22313-1450
Facsimile No. 571-273-3301

Authorized officer: Lee W. Young

PCT Helpdesk: 571-272-4360
PCT OSP: 571-272-7774
INTERNATIONAL SEARCH REPORT

Form PCT/ISA/2 10 (continuation of first sheet (2)) (July 2009)

Box No. II  Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. [ ] Claims Nos.:
   because they relate to subject matter not required to be searched by this Authority, namely:

2. [ ] Claims Nos.:
   because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:

3. [ ] Claims Nos.:
   because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box No. III  Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:
This application contains the following inventions or groups of inventions which are not so linked as to form a single general inventive concept under PCT Rule 13.1. In order for all inventions to be examined, the appropriate additional examination fees must be paid.

Group I: Claims 1-6, directed to a system for bending a rod into a shape designed for implantation into a patient.

Group II: Claims 7-10 directed to a system for bending a rod into a shape designed for implantation into a patient.

Group III: Claims 11-21 directed to a method for bending a rod configured to be implanted into a patient.

--- See Continuation Sheet ---

1. [ ] As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.

2. [ ] As all searchable claims could be searched without effort justifying additional fees, this Authority did not invite payment of additional fees.

3. [ ] As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:

4. [x] No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:
   1-6

Remark on Protest

[ ] The additional search fees were accompanied by the applicant’s protest and, where applicable, the payment of a protest fee.

[ ] The additional search fees were accompanied by the applicant’s protest but the applicable protest fee was not paid within the time limit specified in the invitation.

[ ] No protest accompanied the payment of additional search fees.
Continuation of Box III: Observations where unity of invention is lacking

The inventions listed as Groups I-III do not relate to a single general inventive concept under PCT Rule 13.1 because, under PCT Rule 13.2, they lack the same or corresponding special technical features for the following reasons:

Groups I-III are related to an apparatus (Groups I and II) and a method of using the apparatus (Group III), and share the technical features of an automated rod bending system comprising: a linear movement device configured to axially feed the rod in a first direction; a rotational movement device, the rotational movement device configured to rotate the rod; a bending device to impose bending forces against the rod; and a controller configured to: receive an indication of a plurality of line segments defined on the rod; receive an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments; identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments; and control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments. However, these technical features fail to provide a contribution over the prior art of US 2007/0227216 A1 to Shalliol, which discloses an automated rod bending system (abstract) comprising: a linear movement device configured to axially feed the rod (105) in a first direction (fig 9, 10, para [0047]-[0050]); a rotational movement device (112), the rotational movement device configured to rotate the rod (fig 9, 10, para [0047]-[0050]); a bending device (106, 108, 110) to impose bending forces against the rod (fig 9, 10, para [0048]); and a controller (servo controller plus computer) configured to: receive an indication of a plurality of line segments defined on the rod (para [0053]-[0055]); receive an indication of an angle measurement to be formed between at least two adjacent ones of the plurality of line segments (para [0053]-[0055]); identify bending parameters to perform on the rod to form the angle measurement between the at least two adjacent ones of the plurality of line segments (para [0053]-[0055]); and control operation of at least the bending device using the bending parameters to create an angle having the angle measurement between the at least two adjacent ones of the plurality of line segments (para [0053]-[0055]).

The inventions of Group I-III each recite a special technical feature above and beyond the shared technical feature and device. In particular:

The special technical feature of Group I is a base include a base passage extending there through; not required by the inventions of Groups II and III.

The special technical feature of Group II is a plurality of guide rollers; not required by the inventions of Groups I and III.

The special technical feature of Group III is method of bending a surgical rod; not required by the inventions of Groups I and II.

As the common features were known in the art at the time of the invention, they cannot be considered special technical features that would otherwise unify the groups.

Therefore, Groups I-III lack unity under PCT Rule 13 because they do not share a same or corresponding special technical feature.