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HOSACK, Chad [US/US]; 12228 South West 131st Avenue, Tigard, **OR** (US).

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(74) **Agent: BELLES, Brian, L.;** Wolf, Block, Schorr and Solis-Cohe nLLP, 1650 Arch Street, 22nd Floor, Philadelphia, PA 19103 (US).

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(71) **Applicant** (for all designated States except US): **AKRION TECHNOLOGIES, INC.** [US/US]; 1105 N. Market Street, Suite 1300, Wilmi ngton, DE (US).

(72) **Inventors; and**

(75) **Inventors/Applicants** (for US only): **PEJMAN, Fani** [US/US]; P.O. Box 910252, San Diego, CA 92191 (US). **KORBLER, John** [US/US]; 211 Mine Street, Mertzow n, PA (US). **ROUILLARD, Mark** [US/US]; 26882 Peraza Lane, Missio n Viejo, CA 92691 (US). **BROWN, James** [US/US]; 923 Center Street, Jim Thorpe, PA 18229 (US).

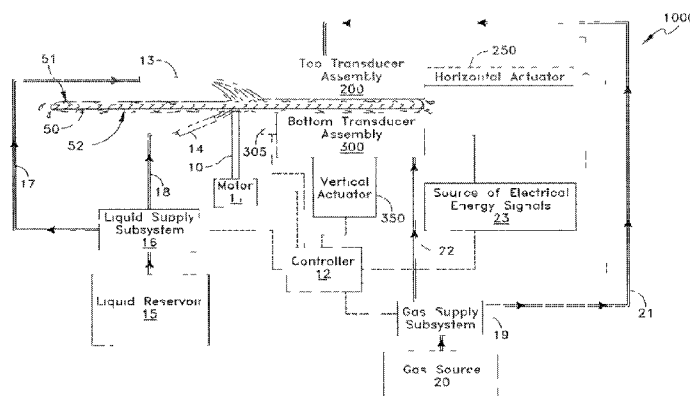
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[Continued on next page]

(54) **Title:** ACOUSTIC ENERGY SYSTEM, METHOD AND APPARATUS FOR PROCESSING FLAT ARTICLES



(57) **Abstract:** A system, apparatus and method for processi ng this flat articles, such as semico nductor wafers, with acoustical energy. In a clea ning process, the inventive system, apparatus and method can remove particles from both sides of a wafer more efficie ntly and effectively in one aspect, the invention is a system for processi ng flat articles compri ng: a rotatable support for supporti ng a flat article; a first dispe nser for applyi ng liquid to a first surface of a flat article o n the rotatable support; a second dispe nser for applyi ng liquid to a seco nd surface of a flat article o n the rotatable support; a first transducer assembly compri ng a first transducer for generating acoustic energy and a first transmitter acoustically coupled to the first transducer, the first transducer assembly positio ned so that whe n the first dispe nser applies liquid to the first surface of a flat article o n the rotatable support, a first meniscus of liquid is formed betwee n a portio n of the first transmitter and the first surface of the flat article; and a second transducer assembly compri ng a seco nd transducer for generating acoustic energy and a seco nd transmitter acoustically coupled to the seco nd transducer, the seco nd transducer assembly positio ned so that whe n the seco nd dispe nser applies liquid to the seco nd surface of the flat article o n the rotatable support, a seco nd meniscus of liquid is formed betwee n a portio n of the seco nd transmitter and the seco nd surface of the flat article.

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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

ACOUSTIC ENERGY SYSTEM, METHOD AND APPARATUS FOR PROCESSING FEAT ARTICLES-

Cross-Reference to Related Patent Applications

[0001] The present patent application claims the benefit of United States Provisional Patent Application No. (50/760,820, filed January 20, 2006; United States Provisional Patent Application No. 60/837,965, filed August 16, 2006; United States Provisional Patent Application No. 60/850,930, filed October 11, 2006; United States Provisional Patent Application No. 60/885,755, filed January 22, 2007; and United States Non-Provisional Patent Application Serial No. 11/125,550, filed January 22, 2007, the entire contents of which are hereby incorporated by reference.

Background of the Invention

[0002] The present invention relates generally to the field of processing flat plate devices using acoustic energy; specifically to systems, methods and apparatuses that utilize acoustic energy for cleaning flat articles, such as semiconductor wafers;

Summary of the Invention

[0003] In the field of semiconductor manufacturing, it has been recognized that the beginning of the semiconductor wafer cleaning process is a critical requirement to producing quality semiconductor wafers. Many different systems and methods have been developed over the years to remove particles from semiconductor wafers. These systems and methods are undesirable because they damage the wafers. Thus, the removal of particles from wafers, which is measured in terms of particle removal efficiency ("PRE"), must be balanced against the amount of damage caused to the wafer by the cleaning method used. It is therefore desirable to have a system to be able to remove particles from the surface of a semiconductor wafer without resulting in damage to the device on the wafer surface.

[0004] Existing techniques for removing particles from the surface of a semiconductor wafer utilize a combination of chemical and mechanical processes. One typical chemical process is standard clean ("SC1"), which uses a mixture of hydrogen peroxide, ammonium hydroxide, and water. SC1 oxidizes and etches the surface of the wafer. This etching process, known as undercutting, reduces the physical contact of the wafer surface to the particles. The particle removal rate of removal is a function of the process, is still required to actually remove the particles from the surface.

Abstract

The purpose of this study was to evaluate the effectiveness of a new ultrasonic cleaning method for removing particulate contamination from semiconductor wafers. The study involved comparing the results of traditional manual cleaning methods with those of the new ultrasonic method. The results showed that the ultrasonic method significantly reduced the number of particles remaining on the wafer surface, indicating improved cleaning efficiency.

Keywords: Ultrasonic cleaning, Semiconductor wafers, Particulate contamination, Cleaning efficiency.

Introduction

Semiconductor manufacturing processes are highly sensitive to particulate contamination. Even small amounts of dust or debris can lead to defects in the final product, resulting in significant financial losses. Therefore, effective cleaning methods are essential for maintaining high yields and quality in semiconductor production.

Traditional cleaning methods, such as manual brushing or rinsing, have been widely used in the industry. However, these methods often require significant labor and time, and they may not effectively remove all contaminants, especially those embedded in the wafer surface. Ultrasonic cleaning, which uses high-frequency sound waves to dislodge particles, has emerged as a promising alternative due to its potential for more thorough and efficient cleaning.

This paper presents the findings of a controlled experiment designed to compare the performance of manual cleaning versus ultrasonic cleaning. The primary objective was to quantify the reduction in particulate density achieved by the ultrasonic method. Secondary objectives included assessing the impact of cleaning parameters (e.g., frequency, power) on the overall effectiveness of the process.

The experimental setup involved measuring the particle count on a series of semiconductor wafers before and after cleaning. The results were analyzed statistically to determine if the differences between the two methods were significant. This study aims to provide valuable insights into the optimization of cleaning processes for semiconductor manufacturers.

Methodology

The study employed a randomized controlled trial design. A total of 60 semiconductor wafers were selected for testing. These wafers were divided into two groups: Group A, which underwent manual cleaning, and Group B, which underwent ultrasonic cleaning. The wafers were initially contaminated with a known quantity of standard test particles.

The manual cleaning procedure followed established industry practices, involving physical scrubbing and rinsing. The ultrasonic cleaning procedure utilized a specialized ultrasonic bath operating at a frequency of 40 kHz. The duration and power level of the ultrasonic treatment were carefully monitored and recorded.

After cleaning, each wafer was subjected to a rigorous inspection process using a scanning electron microscope (SEM) to identify and count any remaining particles. The SEM provided high-magnification images that allowed for precise measurement of particle size and location. The particle counts were then compared between the two groups to evaluate the relative effectiveness of each cleaning method.

Results and Discussion

The initial particle density across all wafers was found to be approximately 150 particles per square centimeter. Following manual cleaning (Group A), the average particle density decreased to about 80 particles per square centimeter. In contrast, the ultrasonic cleaning group (Group B) achieved a much lower average particle density of approximately 20 particles per square centimeter.

These results demonstrate that the ultrasonic method is significantly more effective than manual cleaning in removing particulate contamination from semiconductor wafers. The statistical analysis confirmed that the difference in particle density between the two groups was highly significant ($p < 0.001$). Furthermore, the ultrasonic method consistently performed well across different wafer types and contamination levels, suggesting its broad applicability in semiconductor manufacturing.

The success of the ultrasonic method can be attributed to several factors. First, the high-frequency sound waves create cavitation bubbles that implode against the wafer surface, effectively dislodging particles. Second, the ultrasonic process is non-contact, reducing the risk of damage to the delicate wafer surface. Finally, the automated nature of ultrasonic cleaning allows for more consistent and repeatable results compared to manual methods.

Conclusion

In conclusion, this study provides strong evidence that ultrasonic cleaning is a superior method for removing particulate contamination from semiconductor wafers. Its ability to achieve higher cleaning efficiency while minimizing the risk of surface damage makes it a compelling choice for modern semiconductor manufacturing facilities. Further research could explore the optimal parameters for ultrasonic cleaning and investigate its application in other areas of microelectronics fabrication.

Acknowledgments

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Appendix A: Data Summary

Parameter	Manual Cleaning (Group A)	Ultrasonic Cleaning (Group B)
Initial Particle Density (particles/cm²)	~150	~150
Final Average Particle Density (particles/cm²)	~80	~20
Standard Deviation (particles/cm²)	~25	~15
Cleaning Time (minutes)	~15	~10
Labor Intensity (Relative Units)	High	Low

Appendix B: SEM Images

Figure 1 shows a typical SEM image of a wafer surface after manual cleaning, displaying numerous small, dark spots representing residual particles. Figure 2 shows a similar SEM image after ultrasonic cleaning, where the surface appears much smoother and free of visible contaminants.

Appendix C: Statistical Analysis

T-test results comparing the mean particle densities of Groups A and B. The null hypothesis (H_0) states that there is no significant difference between the two groups. The alternative hypothesis (H_a) states that the ultrasonic group has a significantly lower mean particle density. The calculated t-value is 12.5, which is greater than the critical value of 2.0 for a significance level of 0.05. Therefore, we reject the null hypothesis and conclude that the difference is statistically significant.

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Application Publication 2006702782:53 ("Verfeaverbefcs ct-a!") with the transducer assembly located adjacent the backside of the wafer.

Despite the foregoing, there still remains a need for single wafer systems that can achieve improved F31E with misfit stress, further, continued miniaturization of devices to render such systems it is achievable achieving an acceptable balance between high PRB and minimized device damage.

SUMMARY OF THE INVENTION

[0012] It is an object of the present invention to provide a system, apparatus and method for processing wafers, such as semiconductor wafers, with acoustic energy.

[0013] Another object of the present invention is to provide a system, apparatus and method for simultaneously cleaning both surface of flat articles, such as semiconductor wafers, with acoustic energy.

[0014] Still another object of the present invention is to provide a system, apparatus and method for cleaning both surface of flat articles, such as semiconductor wafers, with acoustic energy that improves the damage to the wafer.

[0015] Yet another object of the present invention is to provide a system, apparatus and method for applying acoustic energy to the bottom surface of a rotating flat article.

[0016] A further object of the present invention is to provide a system, apparatus and method for simultaneously cleaning both surface of flat articles, such as semiconductor wafers, that utilize acoustic energy.

[0017] A still further object of the present invention is to provide a system, apparatus and method that allows existing single surface cleaners to be retrofitted to achieve improved cleaning of both surfaces of a wafer.

[0018] A yet further object of the present invention is to provide a system, apparatus and method that achieves an improved coupling between a transducer assembly and the bottom surface of a flat article.

[0023] *It is to be understood that the invention can be a system for processing flat articles comprising: a rotatable support for supporting and locating a substantially*
JiorizohtaiQAWiatott transducer assembly comprising a transducer for generating acoustic
energy, a transmitter, and a receiver; the transducer assembly is positioned so that at least a portion of the perimeter of the flat article is adjacent to the transducer and the transmitter is adjacent to the bottom surface of the flat article of the flat article.
so that when a pressure is applied to the bottom surface of the flat article, a pressure is applied between the transmitter and the bottom surface of the flat article.

[0024] *It is still to be understood that the invention can be a transducer assembly for mounting*
on a bottom surface of a flat article comprising: a transducer for generating acoustic
energy; a transmitter acoustically coupled to the transducer; and a receiver coupled to the
transmitter and the receiver is positioned so that at least a portion of the perimeter of the flat article is adjacent to the transducer and the transmitter is adjacent to the bottom surface of the flat article.

[0025] *It is still to be understood that the invention can be a transducer assembly for mounting*
on a bottom surface of a flat article comprising: a transducer for generating acoustic
energy; a transmitter acoustically coupled to the transducer; and a receiver coupled to the
transmitter and the receiver is positioned so that at least a portion of the perimeter of the flat article is adjacent to the transducer and the transmitter is adjacent to the bottom surface of the flat article.

[0026] *It is still to be understood that the invention can be a method of processing a flat article comprising: a) supporting a flat article in a substantially horizontal orientation within a gaseous atmosphere, and a flat article having a bottom surface and a top surface; b) mounting a transmitter to the bottom surface of the flat article; c) applying a pressure to the bottom surface of the flat article; d) applying a pressure of liquid on the bottom surface of the flat article; e) applying acoustic energy to the top surface of the flat article via a first transducer assembly comprising a first transducer and a receiver, a portion of the first transducer is in contact with the bottom surface of the flat article; f) applying acoustic energy to the bottom surface of the flat article via a second transducer assembly comprising a second transducer and a second transmitter, a portion of the second transducer is in contact with the bottom surface of the flat article;*

[illegible]

[0039] FIG. 9 is a cross-sectional view of the schematic representation of the transducer assembly of FIG. 8 along the cross-sectional cut B-B of FIG. 8.

[0040] Figure 10 is a schematic representation of an alternative embodiment of the transducer assembly relative to the bottom-side transducer assembly for the acoustic energy system of FIG. 2.

[0041] Figure 11 is a cross-sectional view of the schematic representation of the transducer assembly arrangement of FIG. 10 along the cross-sectional cut C-C of FIG. 10.

[0042] Figure 12 is a schematic representation of the acoustic energy system utilizing a reflector sleeve according to one embodiment of the present invention.

[0043] FIG. 13 is a schematic representation of the acoustic energy system utilizing a reflector sleeve according to another embodiment of the present invention.

[0044] FIG. 14 shows various embodiments of the transducer assembly that can also act as a reflector for the acoustic energy system of FIG. 12.

DESCRIPTION OF THE INVENTION.

[0045] Referring first to FIG. 1, a schematic of an acoustic energy cleaning system 1000 (hereinafter referred to as "cleaning system 1000") is illustrated according to one embodiment of the present invention. The cleaning system 1000 includes a substrate 10 and a transducer assembly 20. The substrate 10 is a semiconductor wafer. However, the substrate 10 is not so limited and can be utilized for wet processing of any flat article.

[0046] The transducer assembly 20 comprises a top transducer assembly 200, bottom transducer assembly 300 and a rotatable support 10 for supporting a semiconductor wafer 50 in a substantially horizontal orientation. Preferably, the semiconductor wafer 50 is supported so its top surface 51 is the device side of the wafer 50 while the bottom surface 52 is the non-device side. Of course, the wafer can be supported so that its top surface 51 is the non-device side and the bottom surface 52 is the device side if desired.

[0047] The rotatable support 10 is designed to contact and engage only a perimeter of the substrate 50 in performing its support function. However, the exact details of the structure of the support 10 are not limiting of the present invention and a wide variety of other support structures can be used, such as support plates, etc., while still achieving the same result. The support 10 is a rotatable support for the semiconductor wafer 50.

coi ϕ lécito the bottom transducer &ssent% 30β. The actuators 250, 350 are operably coupled to and controlled by the control system 12. The actuators 250, 350 can be pneumatic actuators, drive-able actuators, or any other style desired to effectuate movement.

FIG. 3 The horizontal actuator 250 can horizontally translate the top transducer assembly 200 between a retracted position and a processing position. When the retracted position the top transducer assembly 200 is withdrawn away from the top surface of the wafer so that the wafer can be loaded and unloaded without obstruction on the support 10. When in the processing position, at least a portion of the top transducer assembly 200 is positioned close to the top surface of the wafer so that when liquid is supplied to the top surface of the wafer, a meniscus of liquid is formed between the top surface 51 of the wafer and the top of the top transducer assembly 200. FIG. 4, the top transducer assembly 200 is in the processing position.

FIG. 5 Similar to the vertical actuator 350, the horizontal actuator 250 can move the bottom transducer assembly 300 between a retracted position and a processing position. For the bottom transducer assembly 300, the retracted position is also a position where the wafer can be safely loaded onto the support 10 without contacting the bottom transducer assembly 300 and/or interfering with processes that may be carried out on the top surface 52 of the wafer. FIG. 6, the bottom transducer assembly 300 is in the processing position. FIG. 7, the bottom transducer assembly 300 is in the processing position. FIG. 8, the bottom transducer assembly 300 is in the processing position. FIG. 9, the bottom transducer assembly 300 is in the processing position. FIG. 10, the bottom transducer assembly 300 is in the processing position. FIG. 11, the bottom transducer assembly 300 is in the processing position. FIG. 12, the bottom transducer assembly 300 is in the processing position. 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FIG. 91, the bottom transducer assembly 300 is in the processing position. FIG. 92, the bottom transducer assembly 300 is in the processing position. FIG. 93, the bottom transducer assembly 300 is in the processing position. FIG. 94, the bottom transducer assembly 300 is in the processing position. FIG. 95, the bottom transducer assembly 300 is in the processing position. FIG. 96, the bottom transducer assembly 300 is in the processing position. FIG. 97, the bottom transducer assembly 300 is in the processing position. FIG. 98, the bottom transducer assembly 300 is in the processing position. FIG. 99, the bottom transducer assembly 300 is in the processing position. FIG. 100, the bottom transducer assembly 300 is in the processing position.

FIG. 11 White & al. (2003) are exemplified in system 100 as a dual horizontal and vertical actuators respectively, in other embodiments of the invention, either horizontal or vertical actuators can be used in place of each. For example, the actuator operably coupled to the bottom transducer assembly 300 can be a horizontal, vertical, angled, or any other suitable actuator. The same device can exist for the actuator operably coupled to the top transducer assembly 200.

(0059) In a position, sensor 305 is positioned in the feedback system so that the position of the bottom transducer assembly 300 can be determined and controlled. The position of sensor 305 is positioned between the bottom transducer assembly 300 and the

the bottom surface 52 of the wafer 50 so that the proper distance between the two can be achieved to effectuate the proper processing of the liquid interface. The position sensor 305 is operably and electrically coupled to the controller 12. Moreover, specifically, the position sensor 305 generates a signal indicative of the measured distance and transmits this signal to the controller 12 for processing. While the sensor 305 is illustrated as being connected to the bottom transducer assembly 306, it can be located almost anywhere in the cleaning system 100 so long as it can perform its position indicating function.

[0060] This system 100 comprises an electrical energy signal source 13, which is operably coupled to the top transducer assembly 20 and the bottom transducer assembly 30. The electrical energy signal source 13 creates the electrical signal that is transmitted to the transducers (discussed later) in the top transducer assembly 20 and the bottom transducer assembly 30 for conversion into compressional energy. The desired electrical signal can be sent to the top transducer assembly 20 and the bottom transducer assembly 30 concurrently, consecutively and/or in an alternating fashion, depending on the process needs. The electrical energy signal source 13 is operably coupled to and controlled by the controller 12. As a result, the controller 12 will dictate the frequency, power level and duration of the acoustic energy generated by the top transducer assembly 20 and the bottom transducer assembly 30. The electrical energy signal source 13 is configured so that the acoustic energy generated by the top transducer assembly 20 and the bottom transducer assembly 30 has a frequency in the ultrasonic range.

[0061] Depending on system, it may not be desirable to use a single electrical energy signal source for both the top transducer assembly 20 and the bottom transducer assembly 30. Thus, more than one source of the electrical energy signal may be used, one for each transducer assembly.

[0062] The controller 12 may be a processor, which can be a suitably microprocessor based programmable logic controller, personal computer, or the like, for process control. The controller 12 preferably includes various input/output ports used to provide control to the various components of the cleaning system 100 that is connected to the controller 12. The controller 12 also preferably comprises sufficient memory to store process recipes and other data, such as thresholds, determined by the operator, process parameters, desired temperatures, process conditions, process time, etc. The controller 12

[9075] The transmitter 362 is a generally par-cylindrical shaped plate having a convex outer surface 306 and a concave inner surface 307. The irradiating 302, however, can be on a wide variety of other shapes and sizes. The transmitter 302 can be constructed of any material that transmits or reflects energy generated by the transducer-SOTs, including quartz, sapphire, boron nitride, plastic, and metals. One suitable material is aluminum.

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(0077J) Oie -ifaaschi cšr S(B Ls a curved piate liayl iig a cp^yssi upper s«fice.3Q8 aaid concave knyer suiface.JOP: Th& constmction oftraosdueers -hattwaverf: electrical &a&gf:into :aoo«stkalcii Šrgy is vcr3f well known iirtheait. The conyεχ surface 3OS of the ttransducer hast a curvature thati.corresponds; to &e curvature. oft Üs ianer oplicave sjtfface 3li7. The transducer 305 ss acoBstically coupled to the tratsmmitter 302 so that acoustic Metrgy geneyrated by the tmisducer 3#5 propagates through thetrahsmiite 302 and to the wa&r 50. More specifically., the coiwx.ttpper-s wface 398 of the.trœcsducsr 30 is bôncicti to the concave imst siirfac e 3§7 of the itaisMittef 302. This bôitdmg CSB bs a direct bonding between ilts surface s 30^3 øis-^r ean.be m indirect fjonng udli ksglatetf βediaty transmission layers. la-other ©mbodiaients, the ttransdtucerts maybe filaf plates or other shapes *. Moreover, \iMI&the bbtftom trted pcr assembly 380 Ls illy dtrated as utii izmg & single ttransducer 30S_7 a plmr^iity of transducers .can be usecl.if desired b create the acoijsitic-energy, Freie.mb:iy,the lTajtsduc dr 305 is adapted to generate ηiegasosic. energy.

[0978J Tlietranšmitt«r 302 is connected to:thelioutsiaġ 304 sq as iŋo foit π a substantially enclosed space 310 in which tlietfaiisduçer 305- is locjtski. Any soαtφ lem.eans cm be used to coa.ftδd the housing MA tō jhe:tot msimittør.302 s including- adhesion, h\$at. welding, fnsfesn^s or-a-üght-fit ass&nbly. A plunility of :opeŋmgs3li are-provided is the bottomt pαM^π of the housing 304. Hie ŋpetnmgs 311 are provided tō aHow st.gas-.to.VeMrodtcted. úitó tsx00R out of ŵe.space 31.0 so.that.thetip^sduceit?:^ can bs. pooled *uwl/ar purged. Tli ε or>onkgs 31.1 are.o pεπu>ly€onix\$cte:t θ tli«g3tøso^oe t^as des ónbéd mF10. -1. Jhe.liQ üsifig-304 a3so comprises an dpeRMg^31.2:ibr alknvijhg the electrical cotiQectio iss (i,c...wii é s) tli&iare

[illegible]

[0084] Referring to FIGS. 8 and 9, an embodiment is illustrated wherein the transmitter 20 of the top transducer assembly 200 is aligned with the top surface 51 of the bottom transducer assembly 300. A wafer 50 is illustrated as being positioned between the assemblies 200 and 300. As liquid 70 is applied to the top surface 51 of the wafer 50, a meniscus 72 is formed between a bottom portion 206 of the transmitter 20 of the top transducer assembly 200 and the top surface 51 of the wafer 50. Similarly, as liquid 70 is applied to the bottom surface 52 of the wafer 50, a meniscus 72 is formed between the bottom surface 52 of the wafer 50 and the bottom surface 52 of the wafer 50. As can be seen, the coupled portions of the top transmitter 20 and the bottom transmitter 300 oppose each other. The aligned portions of the top transmitter 20 and the bottom transmitter 300 oppose each other. As a result, it is possible that the acoustic energy that is generated by the top transmitter 20 and the bottom transmitter 300 and transmitted to the wafer via the meniscus 72 can interfere with and/or cancel out the other.

[0085] Thus, it may be desirable, in certain instances, to operate the top and bottom transducer assemblies 200, 300 in an alternating and/or coactive manner during a wafer cleaning operation. In other embodiments, one may want to activate the top and bottom transducers separately. For example, if the wafer 50 is tilted, the top transducer 200 may be activated first, followed by the bottom transducer 300.

[0086] Referring to FIG. 10, an alternative relative arrangement of the top transducer assembly 200 and the bottom transducer assembly 300 is shown. In this embodiment, the transmitter 20 of the top transducer assembly 200 is aligned with the top surface 51 of the wafer 50, and the transmitter 30 of the bottom transducer assembly 300 is aligned with the bottom surface 52 of the wafer 50. Thus, the transmitters 20 and 30 are positioned on opposite sides of the wafer 50. The angle of separation between the top and bottom transmitters 20 and 30 is 90 degrees. In the illustration, the angle of separation between the top and bottom transmitters 20 and 30 is 90 degrees, including without limitation 45 degrees, etc.

[0087] It will be appreciated that the above-described system that includes the cleaning system 1000 and arranged as shown in FIG. 8, even when activated (i.e., passive). It was determined that the transmitter 30 of the bottom transducer assembly 300 was realigned at least a fraction of the acoustic energy that was generated by the top transducer assembly 200 back toward the bottom surface 51 of the wafer 50. Therefore, a new aspect of the invention is a novel method that includes a passive member coupled to the opposite side of the wafer than the active transducer assembly.

Material	Z_{α}
Alumina	40.6
Ah&thtmun	17.33
Araldite	3.52

Aramite 502/956 50 phe	4.14
Araldite 502/956 90 phe	12.81
Beryl! nun	24.10
Bismuth	21.5
Brass 70cu 30 In	40.6
Brick	7.4
Cadmium	24
Carbon vitreous, sigradur	7.38
Concrete	8.0
Copper rolled	44.6
Dura! utiúu«ia 17S	17.63
Epotek 301	2J5
Fused silica	12.55
GeøttanhiBi	29.6
G lass pyrex	13.1
Glass quartz	12.1
Glass siSia	13
Glucose	5.0
Gold	63.8
Granite	26.5
Induim	18.7
Iron	46.4
Iron east	33.2
Lead	24.6
LilMum	33.0
Magnesium	10.0
Marble	10i
Molybdenum	63.1
Kick el	49.5

Pamfiin	1.76
Polyseslei casting resin	2.86
Porcelain	13.5
FVDF	4.2
Quart/ x cut	15.3
Rubidium	1.93
Salt cryattaltjac x dkeefi α	10.37
Sapphire, aluminium oxide	44.3
Scotch tape 2.5 rails thick	2.08
Silicon wry anisotropic apprx	19.7
Silicon carbide	91.8
Siiicoπ nitride	36
S'her	38.0
Steel inild	46.0
Steel stainless	45.7
St)cast	2.04
Tantakmi	54.8
Teiloa	2.97
Tin	24.2
Titanium	27.3
'i racon	4.82
Tungsten	101.0
Urauium	63.0
Vanadiunt	36.2
Wood cork	0.12
Wood pine	LSI
/Mc	29.6
Zinc oxide	36.4
Zirconium	30.1

[0091] In acoustics, Impedance Z of a material is defined as the product of the density of that material ρ and the velocity of sound in that material. The units for Z are $\text{kg} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$. A coefficient of transmission is affected by the difference in Z of the material through which the acoustic energy must pass. More significant differences in Z between adjacent materials through which the acoustic energy must pass results in increased reflection of the acoustic energy.

[0092] Due to the acoustic impedance mismatch between the substrate and the film, some of the acoustic energy is effectively transmitted back toward the substrate. This reflected energy cleans the surface without having to provide additional mechanical energy. As discussed above, the selective membrane 400 is made of a material with a Z that is greater than that of the substrate, which the acoustic energy is transmitted. Preferably, the Z should be greater than $5 \text{ kg} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$, and more preferably greater than $15 \text{ kg} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$, such as quartz. The effective membrane 400 may be hollow in order to create additional free space that causes the acoustic energy to be reflected again as it passes through the reflective membrane 400. During the cleaning process, there may be continuous reflection between the wafer 50 and the reflective membrane 400 and it may continue until the acoustic energy is absorbed by the system.

[0093] FIG. 3 shows a cross-sectional view of the passive cleaning system 200 where the reflective member 400 is positioned adjacent to the top surface of the wafer 50. The bottom transducer assembly 300 is positioned below the wafer 50. A bottom transducer assembly 300 is positioned below the wafer 50. This embodiment operates in the same fashion as the embodiment shown in FIG. 12 except that the reflective member 400 and the transducer assembly 300 are reversed.

[0094] Referring to FIG. 14, it has been discovered that it may be preferable to utilize hollow tubular structures as the reflective member 400. Exemplary hollow tubular structures are shown in FIG. 14. The hollow tubular member 400 can be fitted with transducers 305A-E if desired. The tubular member can be made of quartz, plastic, metal, or other materials, and the tubular members 400 will have openings on the top surface for the transmission of the acoustic energy. The tubular members 400 may be cylindrical, conical, and frustoconical, and should be understood that

other shapes may be used and are not limited to those shown, the selection of the shape may vary depending upon the desired results,

The rounded drangleli tubular members 50A-E also may be used to direct the reflected acoustical energy at lower angles than that which is depicted at the wafer 50. Typically these angles are less than 40°. By reflecting the acoustical energy at a low angle, a majority of the acoustical energy will be focused on the bottom surface of the transducer assembly 25.

It also has been discovered that the placement of the reflective member 40 from the wafer surface effectively is controlling the distance, or gaps, between the reflective member 40, the transducer assembly 200, 201, 202 and the wafer 50 is determined so as to accommodate the frequency of the wavelength. The distance for the

$$\lambda = \frac{v}{f} \quad (1.)$$

where λ is the wavelength of an acoustical wave, v is the speed of propagation of the wave, and f is the frequency of the wave in 1/s or Hz. Odd $\lambda/4$ values (e.g., $\lambda/4$, $3\lambda/4$, $5\lambda/4$) gaps tend to act as antireflectors that permit energy to pass into the next media, as shown in FIG. 12, the gap between the reflective member 40 and the reflective member 480 tend to be the same as the gap between the media interface. For example, in FIG. 12, the gap between the top of the transducer assembly 200 and the wafer 50 may be set to be 1/4 of the wavelength of the acoustic wave. On the opposite side the gap between the reflective member 40 and the wafer 50 may be set to be 1/2 of the wavelength (i.e., even) in order to reflect the energy directed towards the surface of the wafer. In the embodiment shown, when using water and a frequency of 835 kHz, the wavelength is 0.35 m. The gap between the reflective member 40 and the wafer 50 is approximately 0.0875 m. The gap between the reflective member 480 and the wafer 50, the distance, is approximately 0.070 m.

It is to be understood, however, that even though the above characteristics of the advantages of the present invention have been set forth in the foregoing description, together with details of the structure and function of the invention, the disclosure is illustrative only, and changes may be made in the details of the invention, especially in the shape, size, and arrangement of the parts, without departing from the principles of the invention and the extent of the protection claimed in the appended claims.

Claims

What is claimed is:

1. A system for processing flat articles ϕ comprising:

a rotatable support for supporting a flat article;

a first dispenser for applying liquid to a first surface of a flat article on the support;

a second dispenser for applying liquid to a second surface of a flat article on the support;

a first transducer assembly comprising a first transducer for generating acoustic energy and a first transmitter acoustically coupled to the first transducer; and a second transducer assembly comprising a second transducer for generating acoustic energy and a second transmitter acoustically coupled to the second transducer; wherein the first transmitter applies liquid to the first surface of a flat article on the support, a first meniscus of liquid is formed between a portion of the first transmitter and the first surface of the flat article, and

a second transducer assembly comprising a second transducer for generating acoustic energy and a second transmitter acoustically coupled to the second transducer; wherein the second transmitter applies liquid to the second surface of the flat article on the support, a second meniscus of liquid is formed between a portion of the second transmitter and the second surface of the flat article.

2. The system of claim 1, wherein the rotatable support supports and rotates the flat article in a substantially horizontal plane, the first surface of the article being a top surface and the second surface of the article being a bottom surface.

3. The system of claim 1, comprising a first transducer operably connected to the second transducer for moving the second transducer assembly between a processing position and a retracted position.

Further information

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of the portion of the transmission system which is open to other persons.

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the second and first transducer

having plate
cylindrical parasy
transmission
second
wherein claim
system 22.

23. Use system of CL&3B-22 wherein the second transducer has a convex surface having a curvature that is a function of the effective area of the second transducer.

24. A system including flat articles and a support:

the support for supporting a flat article;

a first transducer assembly comprising a first transducer and a first transmitter positioned so that a first gap exists between a portion of the first transmitter and a first surface of a flat article; the support further comprising a first meniscus of liquid formed between the portion of the first transmitter and the first surface of the flat article when liquid is applied to the first surface;

a second transducer assembly comprising a second transducer and a second transmitter positioned so that a second gap exists between a portion of the second transmitter and a second surface of the flat article on the support; a second layer of liquid formed between the portion of the second transmitter and the second surface of the flat article when liquid is applied to the second surface.

25. A system for processing flat articles and a support:

the support for supporting and rotating a flat article in a horizontal orientation;

a first transducer assembly comprising a first transducer and a first transmitter positioned so that a first gap exists between a portion of the first transmitter and a first surface of a flat article; the support further comprising a first layer of liquid formed between the portion of the first transmitter and the first surface of the flat article when liquid is applied to the first surface;

a second transducer assembly positioned so that a second gap exists between a portion of the second transmitter and a second surface of a flat article; the support further comprising a second layer of liquid formed between the portion of the second transmitter and the second surface of the flat article when liquid is applied to the second surface.

26. The system of claim 25 further comprising a dispenser for applying a liquid to a bottom surface of a flat article on the rotatable support.

27. The system of claim 25 wherein the transmitter has a convex outer surface having an apex that protrudes above a top of the support.

28. The system of claim 27 wherein the transmitter is a parabolic reflector having a focal length of 5 M elongated edge.

29. The system of claim 28 wherein the transmitter is further comprised of a housing connected to the transmitter so as to form a substantially enclosed space in which the transducer is located.

30. The system of claim 29 wherein the transmitter and the housing are encapsulated in an incompressible plastic.

31. The system of claim 30 further comprising one or more openings for flowing a gas into and/or out of the space.

32. The system of claim 25 further comprising a base for supporting the transducer assembly, one or more of which are located in the base for applying a liquid to the bottom surface of a flat article on the rotatable support.

33. A transducer assembly for measuring a bottom surface of a flat article comprising:

a transducer generating an energy;

the transmitter acoustically coupled to the first transducer; and

a dam surrounding at least a portion of a perimeter of the transmitter so as to form a liquidtight seal between the first transducer and the dam.

34. The transducer assembly of claim 33 wherein the transmitter is a parabolic reflector having a concave inner surface and a convex outer surface.

35. The transducer assembly of claim 34 wherein the transmitter has a convex surface having a curvature that responds to a curvature of the surface being measured.

36. The transducer assembly of claim 33 further comprising means for mounting the transducer assembly to the bottom surface of a flat article.

37. The transducer assembly of claim 33 wherein the transducer assembly is disposed in an inner cavity of the article.

38. The transducer assembly of claim 33 further comprising a housing connected to the transducer assembly so as to form a substantially airtight space in which the transducer is located.

39. The transducer assembly of claim 38 wherein the transducer is disposed in an inner cavity of a reactive plastic.

40. The transducer assembly of claim 38 further comprising one or more openings in the housing into and/or out of the space.

41. The transducer assembly of claim 33 further comprising:

at least one transducer and a fluid inlet and outlet.

42. The transducer assembly of claim 41 further comprising a liquid dispenser located in the base and adapted to apply liquid to the bottom surface of a flat article.

43. A method of manufacturing a transducer assembly comprising:

providing a par-cylindrical transducer package;

providing one or more transducers and a coupler in the transducer package;

mounting the transducer package to the transducer to create an assembly having a substantially

airtight cavity in which the transducers are located; and

encapsulating the assembly in a non-reactive plastic.

44. The method of claim 42 further comprising connecting the transducer assembly so as to provide a liquid path of a perimeter of the assembly and liquid retaining chamber in the assembly and the dam.

45. The method of claim 42 further comprising providing one or more openings in the assembly for the gas to flow out of the cavity.

45: processing method

top surface of a portion of the first transducer assembly comprising a film of liquid on it

the horizontal surface of the first transducer assembly comprising a film of liquid on it

the top surface of the first transducer assembly comprising a film of liquid on it

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53; The junction of claim 45 wherein the portion of the first interface that contacts the S m
of liquid on the top surface of the flat article does not oppose the portion of the second
transmitter that contacts the bottom of liquid on the top surface of the flat article.

54. The method of ch0m 53 wherein step? e) aŋcTl) m perf útRied *fi mialtematmg fa shion^ concurrently s&úh f eonsee 0th?ely.

55. The method of focusing waves from a surface into at least a portion of a perimeter of the
second transducer so as to form a liquid retaining chamber between first second transmitter and
the dielectric body increases by the portion of the second time interval the amount of the
liquid on the surface of the flat surface.

56. The method of Olam 45 wherein the acoustical energy applied in steps (e), and is in the pga^cmic freq úsacy range ,

57. The method of claim 45 wherein the second transmitter has a convex outer surface having an apex that is in contact with the ISM of the liquid in the footprint of the surface of the article.

SS., The aichod pf claim 57 v^fesinlhesecondttaissmitteris apar-cyliidrical plate,. the apex'ionani^ ss.elongate edge;

59. The method of claim 57 wherein the first transmission is an elongated edge that is modified with the lift of the input of the first of the flat article,

60; The method of cblm.45 -whe-rei α the .secondtraiisducer^sseably iurther, comprises s
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which the $\wedge$ ecQnd.t δ lisducer is loeated, fce .geoottd δ transducer $\wedge$ sateialjly further compri $\wedge$ ifig
one- δ tmoxe. UifSsaings for flowing a gas ml α ajid/ox .o α of the space $\wedge$ het-method iluthet
comprising: flowing aa iilier g3S Itvto the catvity Si>d in δ onfeict i\11h the-second trfc ti δ t δ ber:

6 L The if-then of claim 50 wherein the sectcmd transmitt and line housing are encapsulated.
in a inert noii-i^active [?iasii i:]

62. The method of claim 45 wherein the second transmittance is a cylindrical package having a concave inner surface and a convex outer surface and the semiconductor has a convex surface.

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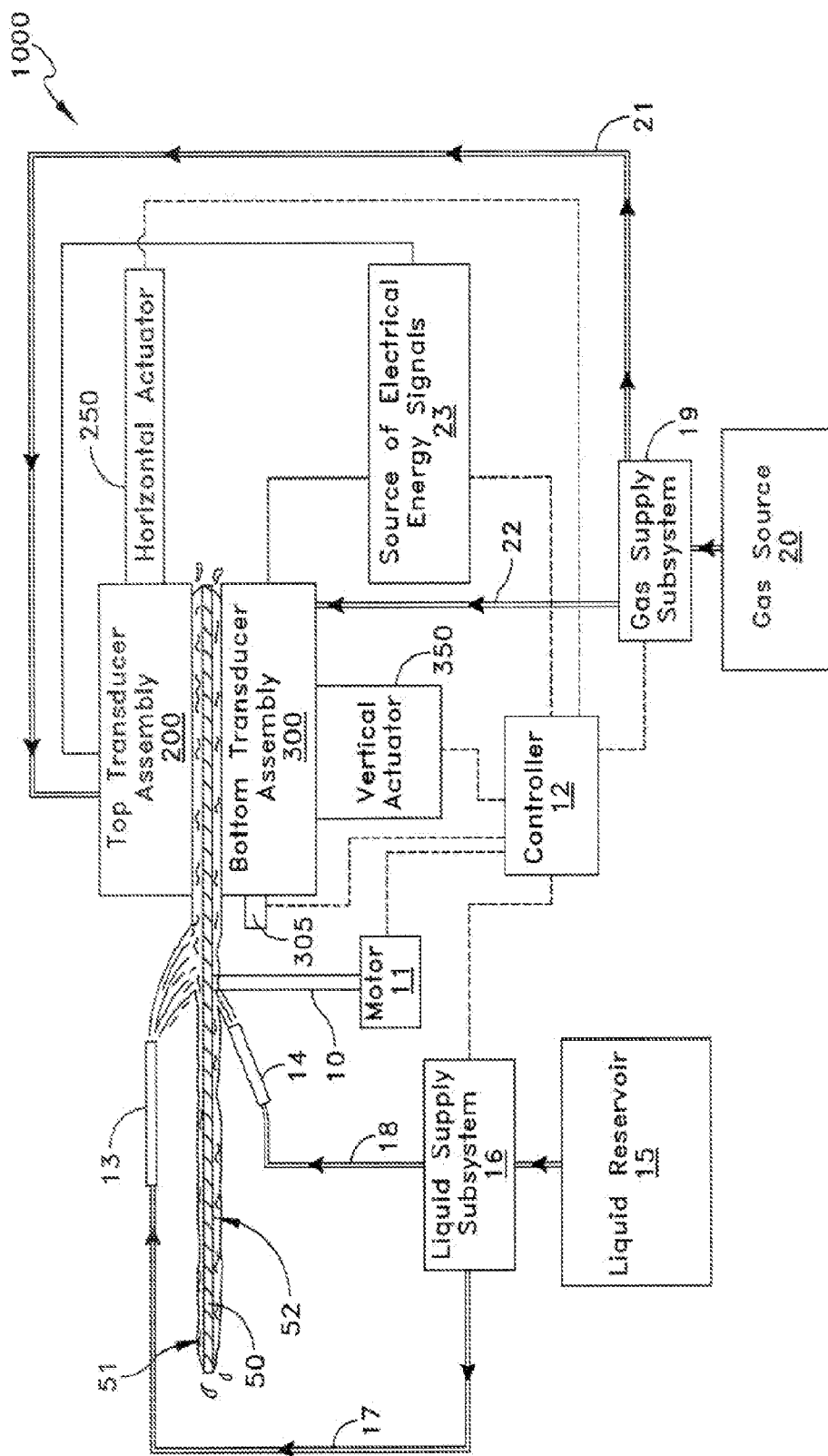


Figure 1

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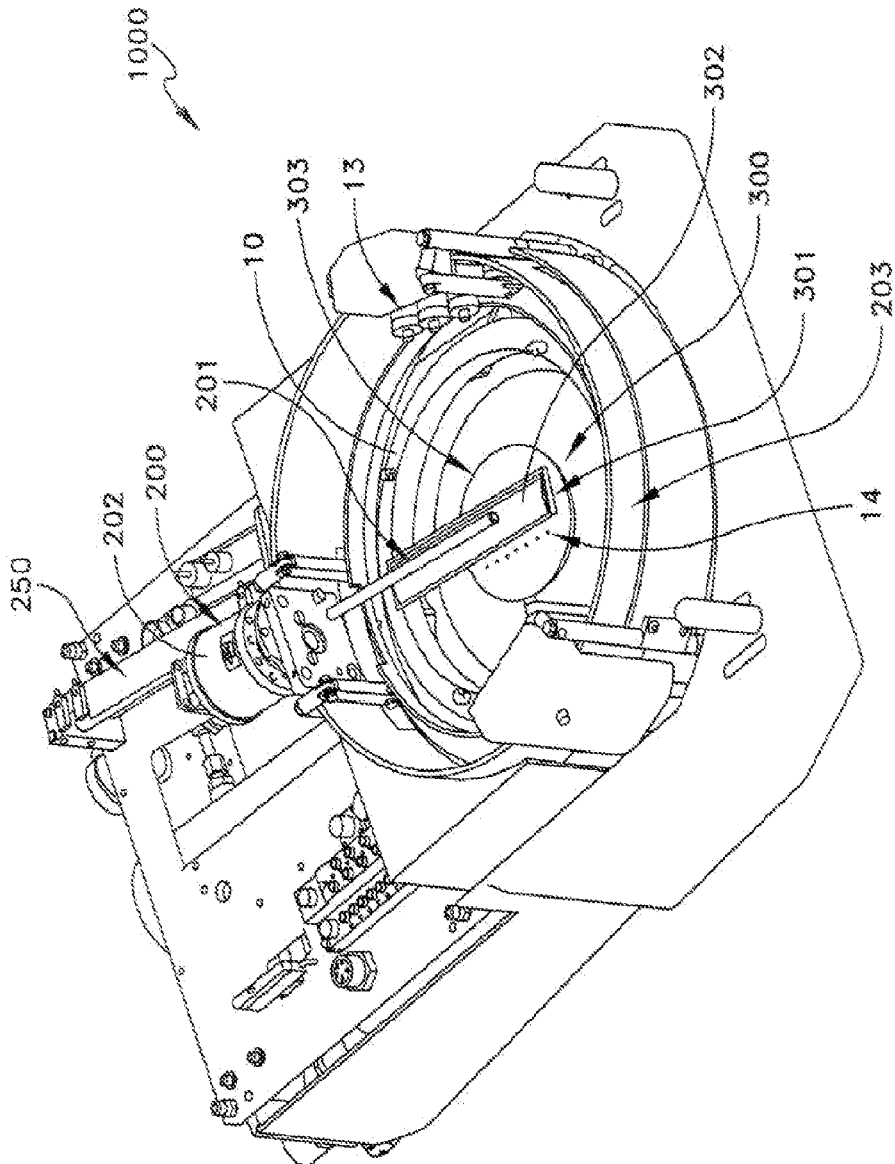


Figure 2

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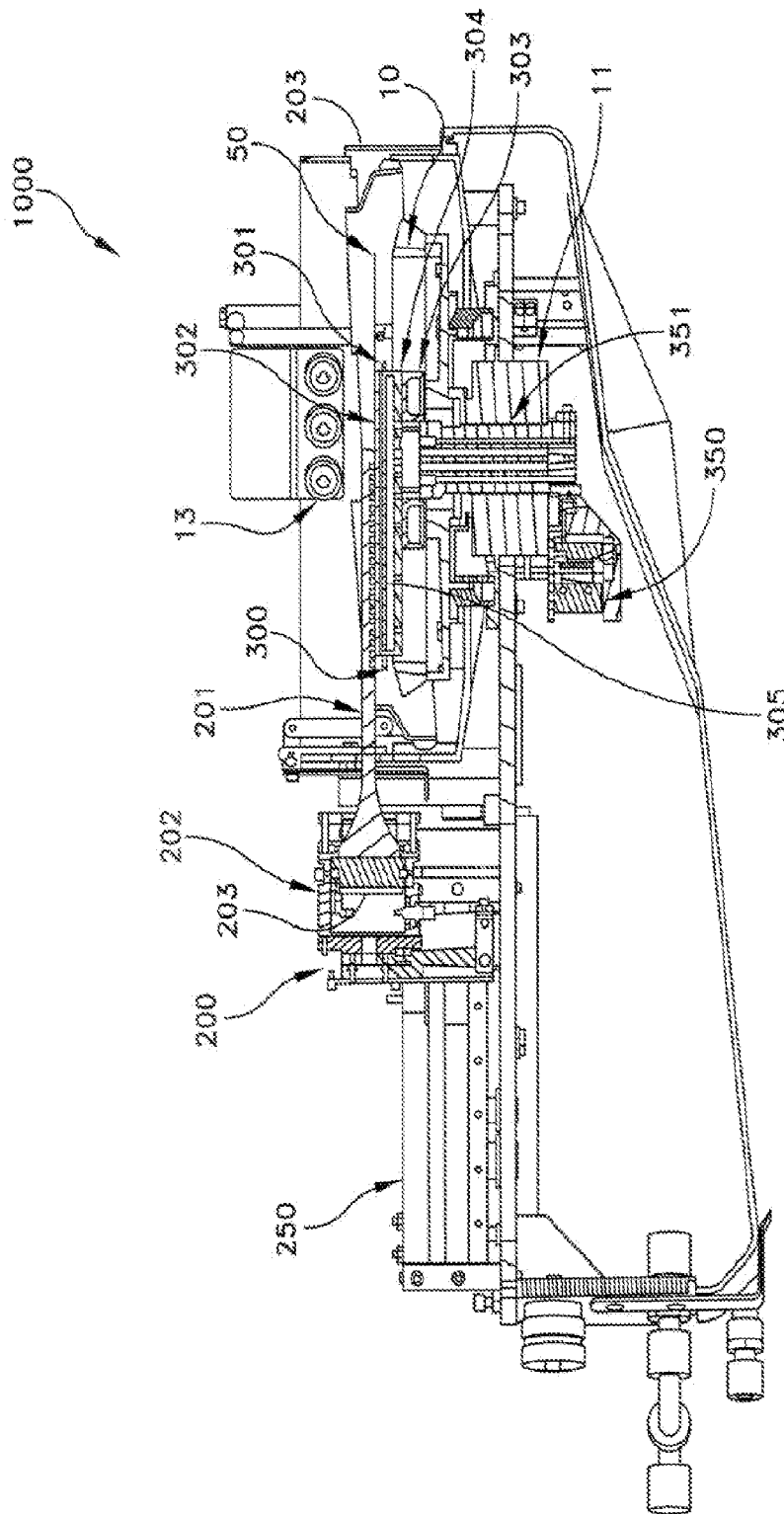


Figure 3

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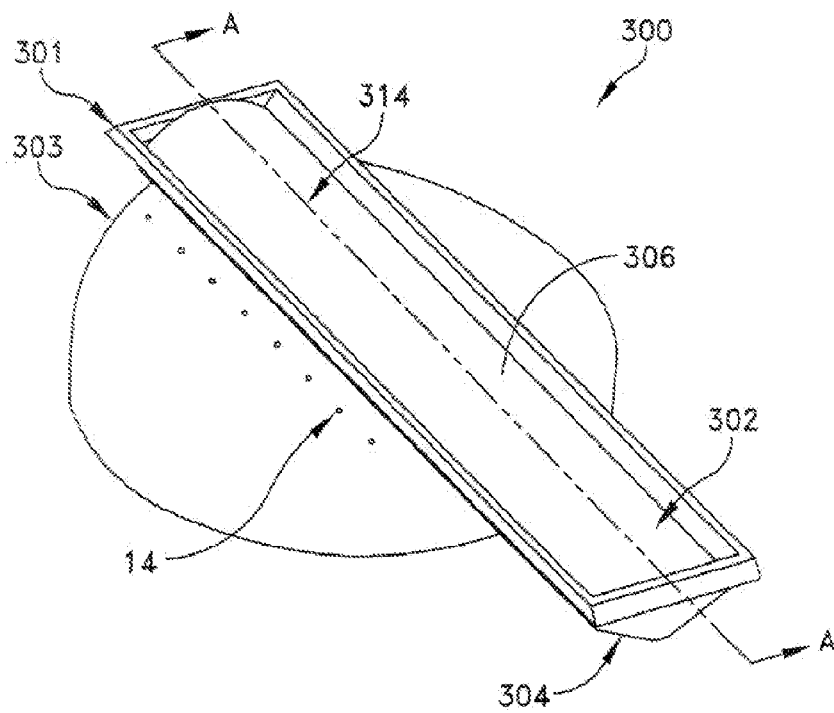


Figure 4

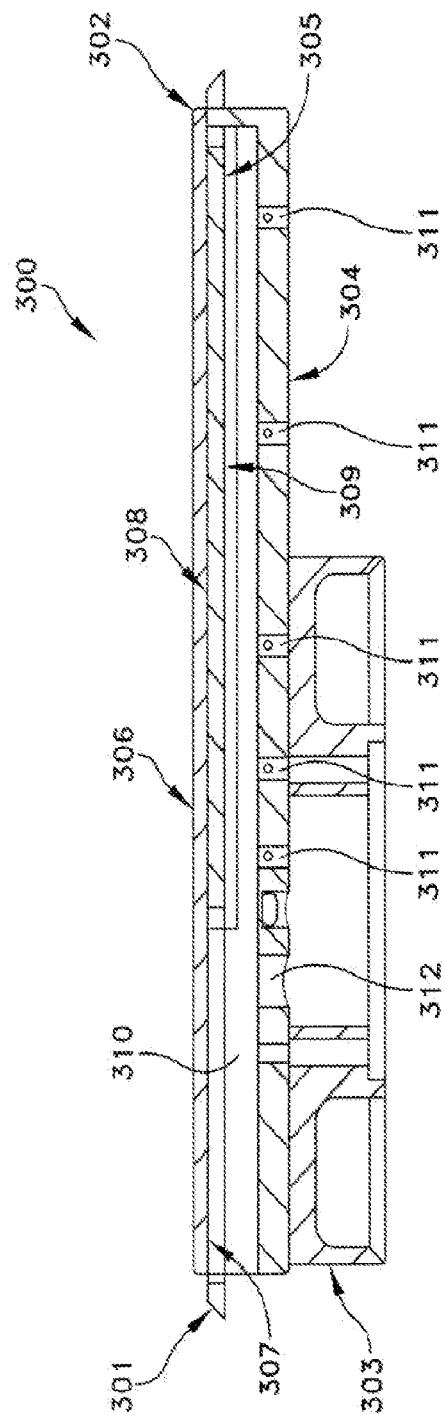


Figure 5

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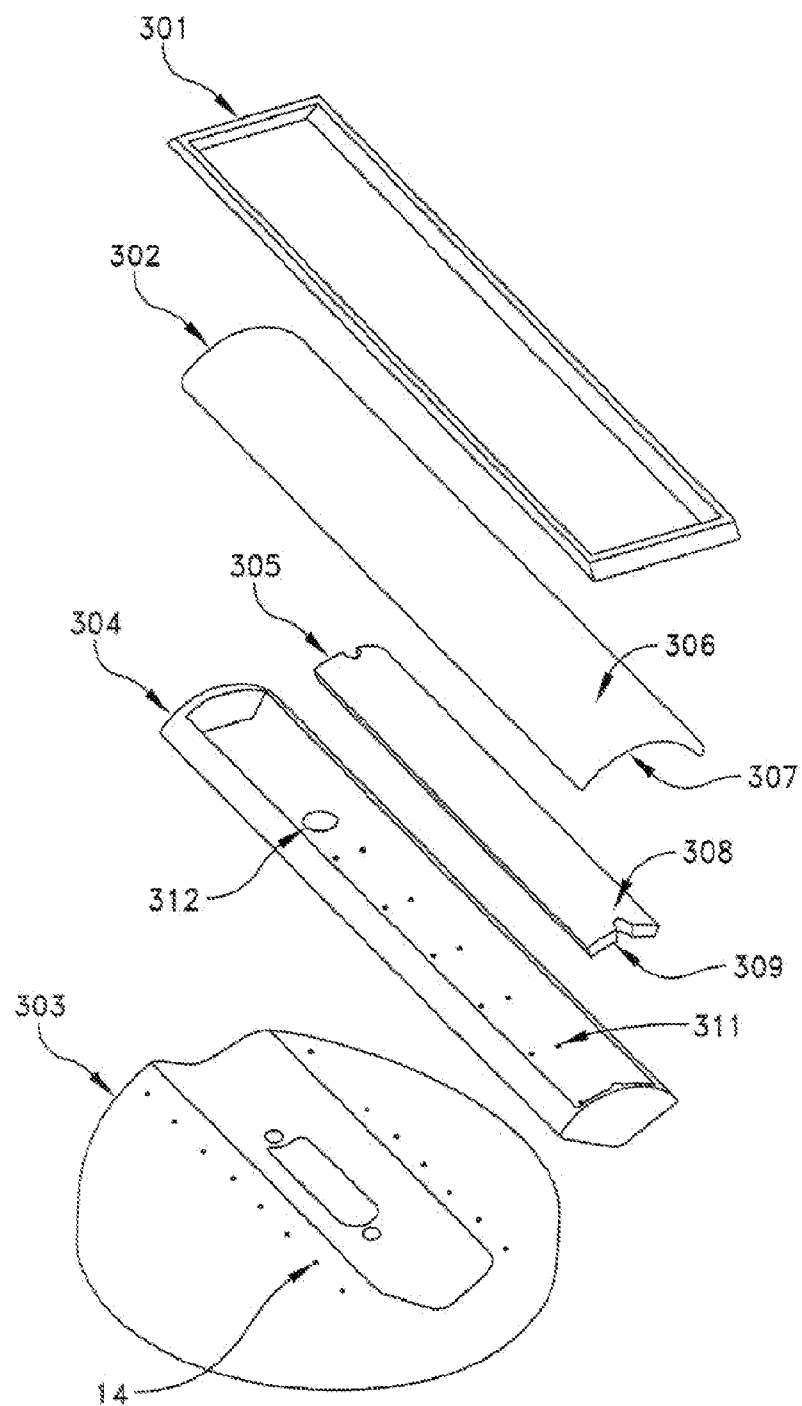


Figure 6

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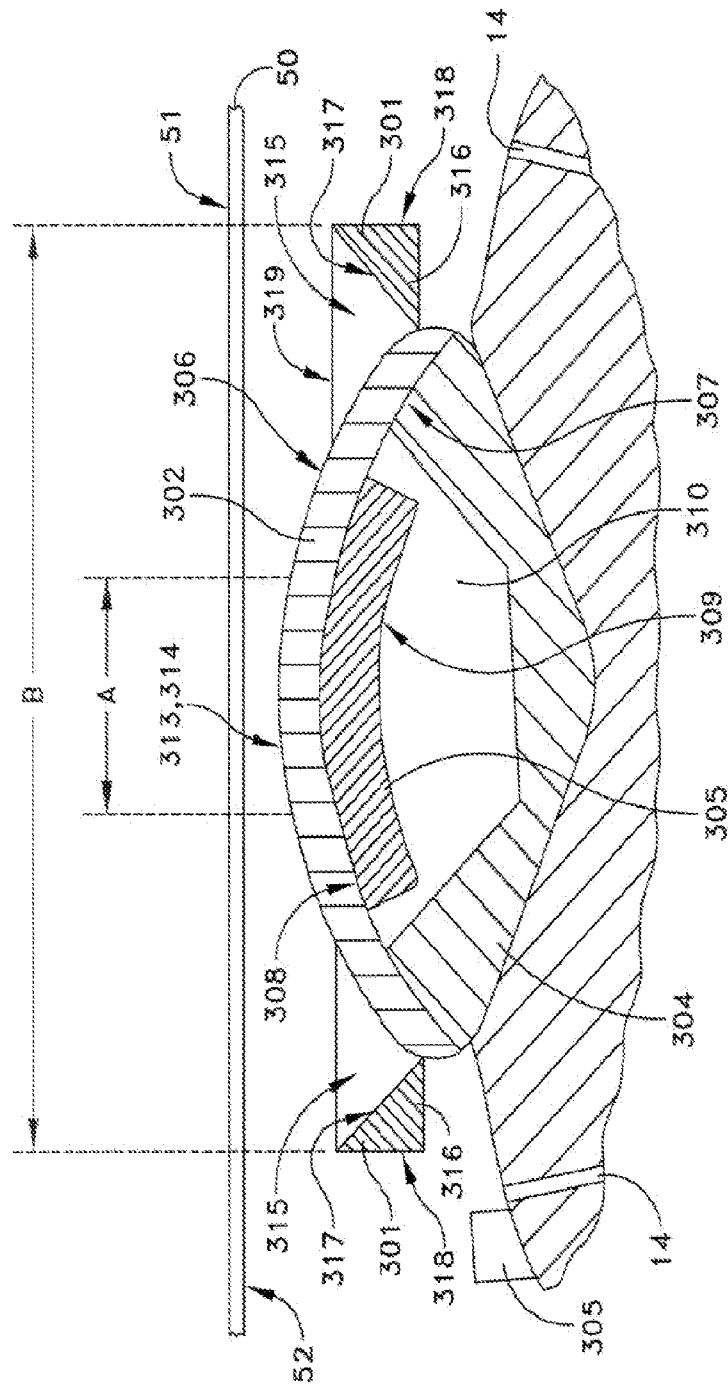


Figure 7

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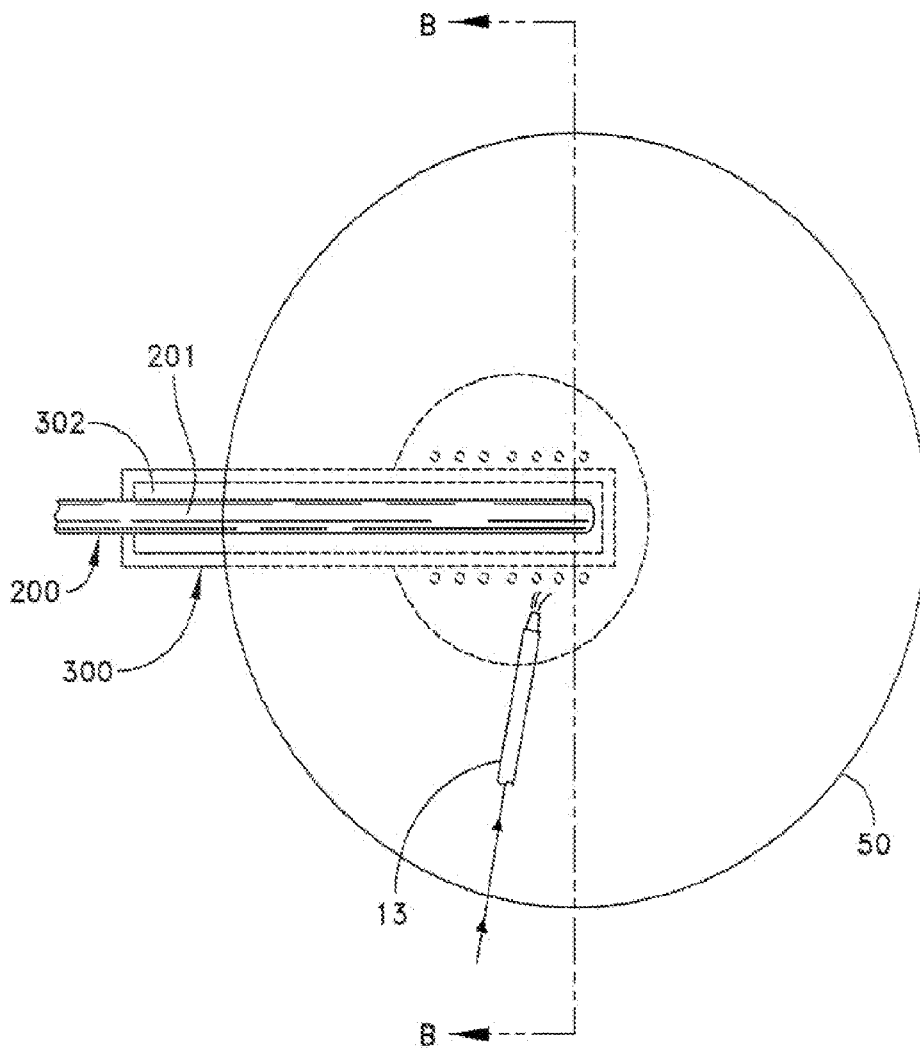


Figure 8

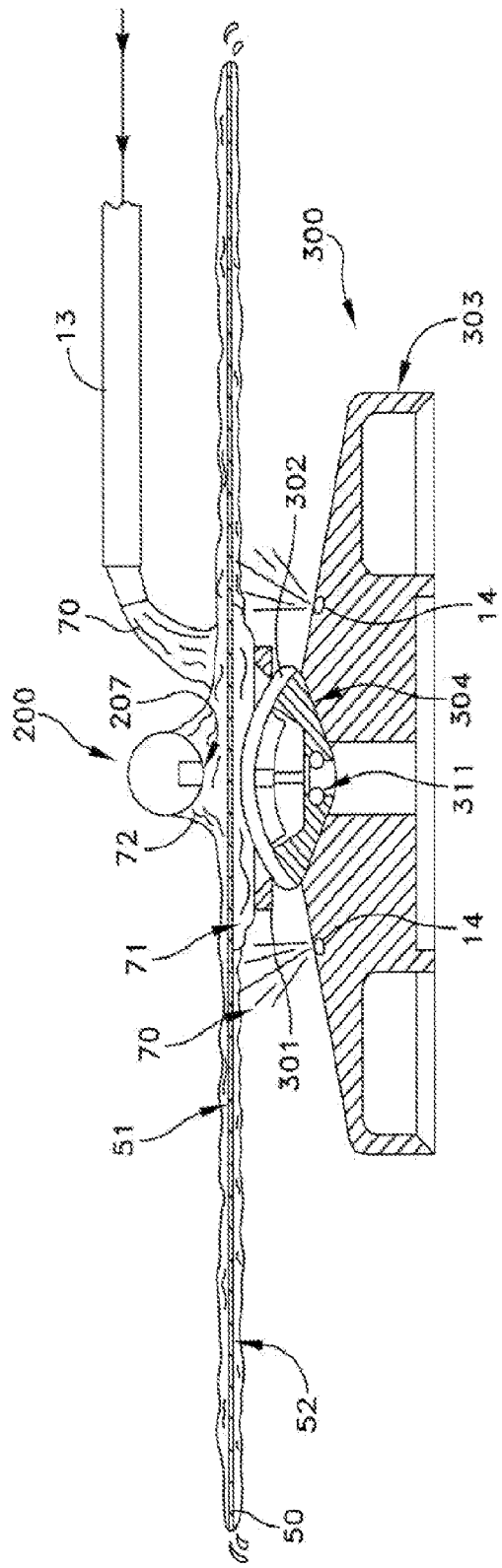


Figure 9

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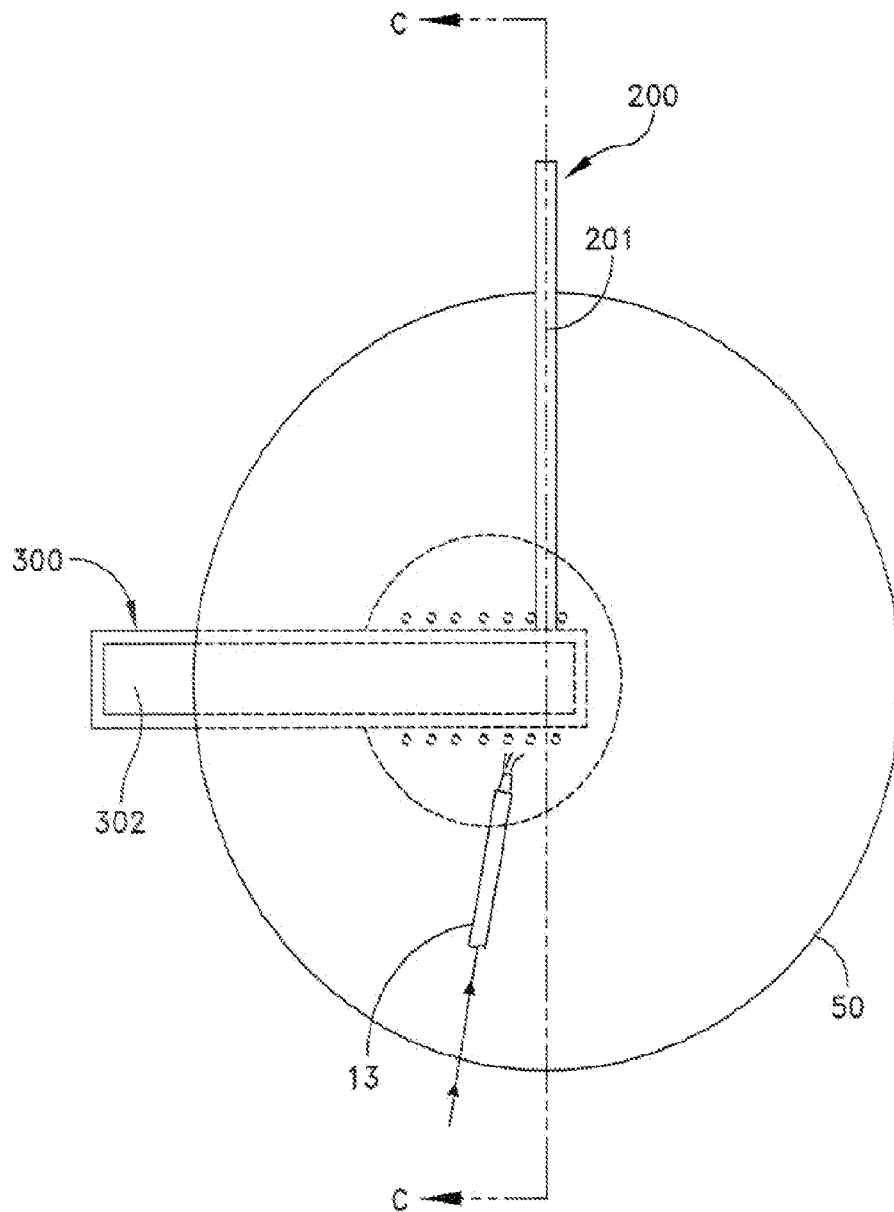


Figure 10

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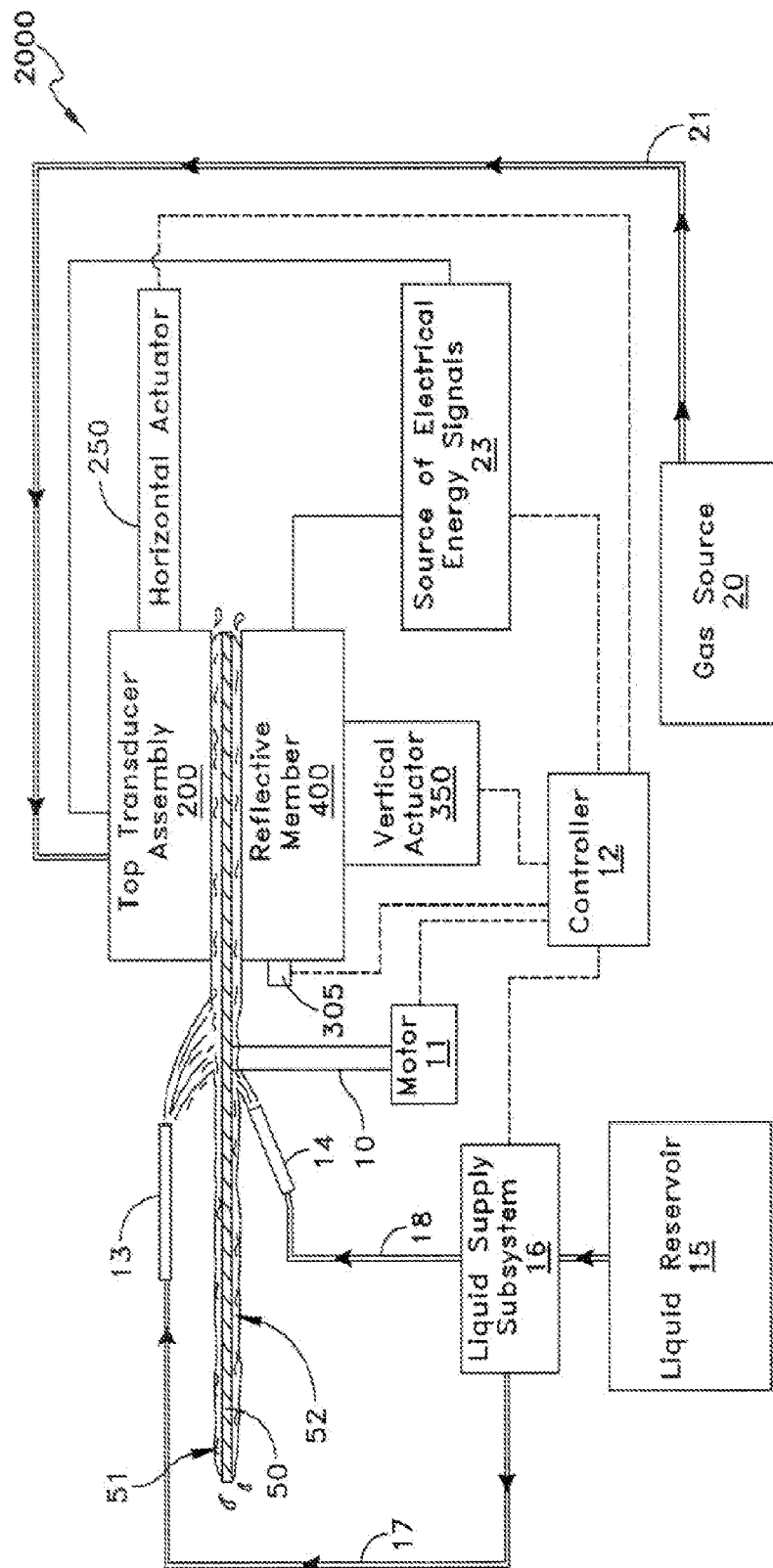


Figure 12

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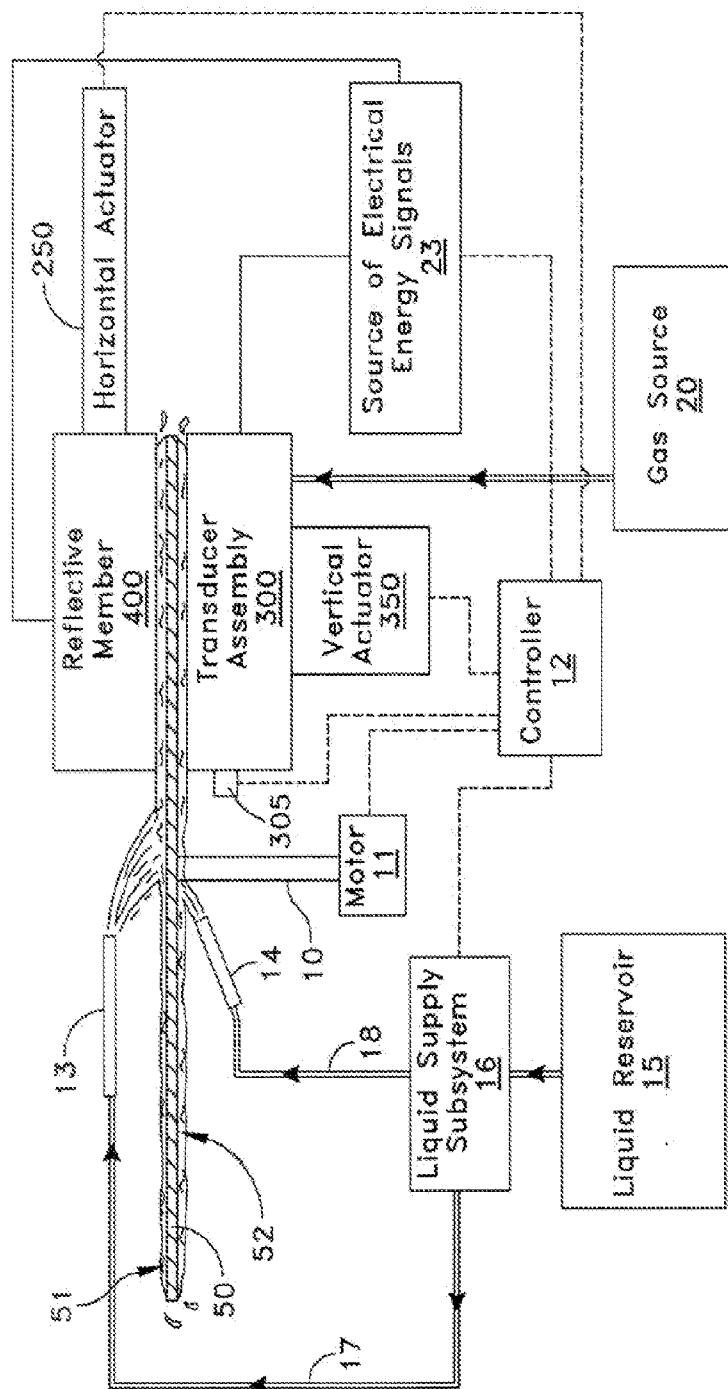


Figure 13

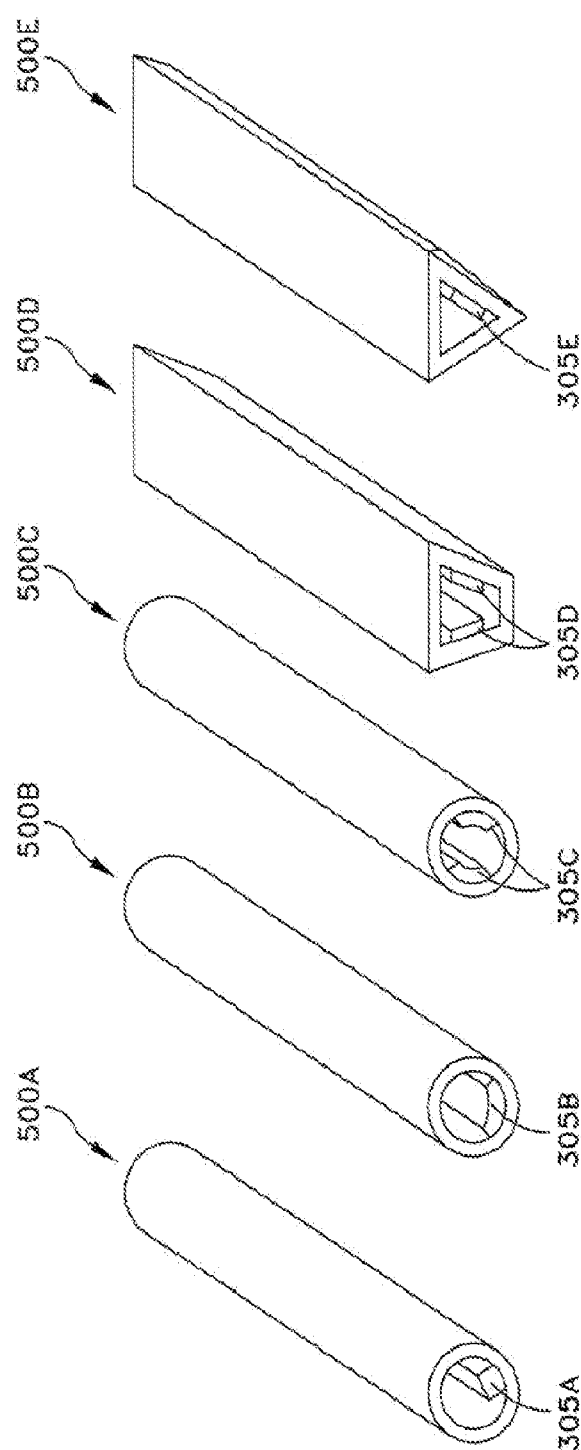


Figure 14