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Intumescent electrical installation systems and processes for their production

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Abstract

Intumescent, electrical installation systems which comprise an injection molding material of polyolefins or polyimides in combination with intumescent additives, the melting points of the polyolefins and of the polyimides being lower than the intumescence temperature of the intumescent additives.

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COMPLETE SPECIFICATION
STANDARD PATENT

Applicant:

INTUMEX GMBH

Invention Title:

INTUMESCENT ELECTRICAL INSTALLATION SYSTEMS AND
PROCESSES FOR THEIR PRODUCTION

The following statement is a full description of this
invention, including the best method of performing it known to
us:

Intumescent electrical installation systems and processes for their production

Electrical installation systems, such as, for example, conduit boxes, junction boxes, switch boxes, armored boxes, conduits, etc., are produced from a very wide range of materials, depending on the intended use.

Materials used to date are steel sheet, aluminum, cast iron, (polyvinyl chloride (PVC), polyphenylene ether/polyphenylene oxide (PPE/PPO), polycarbonate (PC), polystyrene (PS), polypropylene (PP), polyethylene (PE), ABS or polyamide (PA). Depending on the field of use and national provisions, the electrical installation systems must meet certain requirements with respect to fire resistance, thermal stability, chemical stability, electrical properties, such as, for example, volume resistivity, dielectric strength or resistance to tracking, etc.

Thus, for example in Germany and Austria, the following values for flame retardance of electrical installation systems according to VDE 0471/DIN IEC 695 Part 2-1 are applicable: flame retardance for electrical installation systems for flush mounting and in concrete construction must be 650°, that for covers and lids must be 750°C, that for installation systems for mounting cavity walls must be 850°C and that for terminals and semiflush-mounted conduit boxes for riser cables having 1.5 and 2.5 mm² copper conductors must be 960°C.

The installation systems available nowadays and comprising PVC, PPE/PPO, PC, PC blend, PP blend, PA are self-extinguishing and non-flame-propagating according to ÖVE-EN 50086 or VDE 0605 in the event of a fire. Installation systems of steel sheet or aluminum must be protected with kneadable, intumescent cements or intumescent inlays to render said systems fire-retardant.

In the USA, the installation systems protected in this manner may not exceed the temperature of 181°C in a fire test according to ASTM E-119.

5 However, in the cases of fires, for example in the case of cable fires caused by short-circuits, serious consequences can nevertheless easily arise through the formation of dangerous fumes. Particularly in the case of installation systems whose flame retardance is due to a halogen, e.g. chlorine, fire results in the formation of corrosive gases
10 which can rapidly spread and cause permanent secondary fire damage. In order to avoid in particular the formation of corrosive gases, so-called HFT installation systems have been developed which are halogen-free, flame-retardant, i.e. self-extinguishing and non-dripping and
15 thermally stable from -40°C to +140°C in the event of a fire. However, these systems, too, cannot prevent the spread of fumes.

For this reason, it would be advantageous if at least
20 preferred embodiments of the invention provide electrical installation systems which prevent the spread of fumes in a simple manner.

Unexpectedly, this advantage can be achieved by
25 intumescent, electrical installation systems which are produced by the injection molding process from polyimides in combination with intumescent additives.

The invention accordingly relates to intumescent,
30 electrical installation systems which are formed solely from an injection molding material consisting of
a) 20 - 50% per weight of a polyimide
b) 50 - 80% per weight of intumescent additives,
c) 0 - 20% per weight of inorganic fillers and
35 d) 0 - 5% per weight of dispersants.

Electrical installation systems are to be understood as

meaning, surface-mounted sockets and boxes, such as, for example, conduit boxes and armored boxes, flush-mounted sockets and boxes, such as, for example, equipment boxes or switch boxes and conduit boxes, and junction boxes, 5 cavity wall sockets and boxes and installation systems for concrete construction.

The abovementioned installation systems may be in the form of conduits, angle boxes, branch-Ts, cross boxes, a 10 combination conduit box/switch box, a double conduit box/switch box, a semiflush-mounted conduit box, a ceiling light connection box, a wall light connection box, a dome box, a double equipment or switch box, a triple equipment box, an equipment conduit box, a junction box/switch box, 15 a transition box, a universal box, etc.

The intumescent, electrical installation systems according to the invention are formed solely from injection molding material of polyimides in combination with intumescent 20 additives.

Suitable polyimides are those which are present as a low-melting precursor and form highly crosslinked products, such as, for example, bismaleimides by addition reaction 25 under the action of heat.

Bismaleimides which consist of diphenylmethane 4,4'-bismaleimide and methylenedianiline or other aromatic diamines are preferably used. The bismaleimides used 30 should have a melting point below about 200°C.

Commercially available products are, for example, BMI B21 (DSM Fine Chemicals), Kerimide 601 (Ciba), Homide 250 (HOS Technik), etc. 35

Suitable intumescent additives are ammonium or amino compounds, such as, for example, ammonium poly-phosphate,

ammonium dihydrogen phosphate, ethylene-diamine phosphate,
ammonium pentaborate, melamine, dicyandiamide, full
phosphoric esters with polyols, dipentaerythritol,
pentaerythritol, sugar, dextran, starch, vermicular
5 graphite, waterglass, expanded mica, vermiculite, perlite
and mixtures thereof.

Preferred intumescent additives are ammonium poly-
phosphate, ethylenediamine phosphate, melamine,
10 dipentaerythritol, pentaerythritol, sodium silicate or
vermicular graphite or mixtures thereof.

Vermicular graphite is particularly preferably used as an
intumescent additive in the case of polyimides, and
15 ethylenediamine phosphate and/or ammonium polyphosphate
and/or melamine and/or dipentaerythritol and/or vermicular
graphite in the case of polyolefins.

In the case of the injection molding material according to
20 the invention, it should be noted that the melting points
of the polyimides are lower than the intumescence
temperature of the intumescent additives.

The injection molding material according to the invention
25 contains from 20 to 50% by weight, preferably from 30 to
40% by weight, of polyimide

and from 50 to 80% by weight, preferably from 60 to 70% by weight, of intumescent additives.

5 The injection molding material according to the invention can optionally also contain inorganic fillers, such as, for example, kaolin, clays, mica, wollastonite, calcium silicates, titanium dioxide, zinc borate, quartz, zinc oxide, apatite, talc, aluminum phosphates, ATH, $Mg(OH)_2$, chalk, glass fibers, mineral
10 fibers, etc. Preferred inorganic fillers are clays, mica and glass fibers.

15 If clays or mica are used as inorganic fillers, it is preferable for them to be present as nanoparticles in the mixture of polymer, intumescent additive and filler.

20 The amount of added filler may be from 0 to 20% by weight, based on the total injection molding material.

In addition, the injection molding materials according to the invention may also contain conventional dispersants, such as, for example, zinc stearate or calcium stearate, glyceryl stearate, pentaerythrityl
25 tetrastearate, cetyl palmitate, ethylenedistearoyl-diamide C_{14} - C_{18} fatty alcohols, dicarboxylic esters, fatty amines, paraffins, etc., in an amount of from 0 to 5% by weight.

30 For the preparation of the injection molding material, first a powder mixture or granules of the desired components is or are prepared by simple mixing together or by extrusion.

35 Thereafter, the intumescent electrical installation system according to the invention is shaped in only one operation in the injection molding process and optionally postcured.

The parameters, such as, for example, temperature, injection pressure and locking force, depend on the respective starting mixture.

5 In order to ensure that the installation systems according to the invention provide a fume-tight seal in the event of a fire, the material thickness is such that it corresponds to the box volume divided by the product of twice the lateral surface area and the
10 maximum expansion factor, so that the installation system is completely filled with foam by intumescence.

This condition can be represented as a formula as follows:

15

$$d_0 = V / (M_f \cdot E_f \cdot K_f)$$

d_0Material thickness

V.....Volume of the installation system (socket, distributor box, etc.)
20

M_fLateral surface area of the installation system

E_fMaximum expansion factor of the intumescent additive

25 K_fCompression factor (ratio of max. expansion factor to actual expansion factor)

A compression factor of 2 should preferably be present.

30 The intumescent electrical installation systems according to the invention have several advantages over installation systems available to date. First, the injection molding material contains no halogens, so that no corrosive gases can form in the event of a
35 fire. Furthermore, in the event of a fire, the installation systems according to the invention provide a fume-tight seal owing to the intumescent additives, so that additional fire protection measures, such as intumescent inlays or cements, are no longer required.

The advantages are furthermore achieved in a simple manner in one operation in the injection molding process. Moreover, the installation systems according to the invention have good mechanical properties.

5 Also disclosed herein are intumescent, electrical installation systems comprising an injection molding material of polyolefins in combination with intumescent additives. Polyolefins used may be thermoplastic
10 polyolefins, such as polyethylene (PE) having a low density (LDPE) to high density (HDPE), preferably HDPE, ethylene-vinyl acetate (EVA) copolymers, ethylene-butyl acrylate copolymers, polypropylene, poly-1-butene poly(methyl-pentene), copolymers of ethylene and octene,
15 ethylene/propylene-diene terpolymers (EPDM) or blends thereof.

Example 1: Null experiment

20 A commercial flush-mounted connection box 100 having the dimensions 107 x 107 x 57 mm and comprising high-impact polystyrene was mounted in a corresponding recess in a 100 mm Ytong wall so that the cover of the connection box is flush with the Ytong surface. A thermocouple was fastened
25 centrally on the back. The box had melted after 30 minutes and a temperature of 700°C was measured at the thermocouple after 2 hours.

Example 2:

30 Cylindrical granules of a mixture of
31.8% of ethylene-vinyl acetate copolymer: Evathane 2825 EVA (Elf Atochem)
35 21.2% of high-density polyethylene: PE FT 7245 HDPE (Borealis)
40.0% of vermicular graphite (Kaisersberg)

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7.0% of ethylenediamine phosphate

having the dimensions of 4 mm diameter and 4 mm length
were produced on a K 30 twin-screw extruder from Werner &
5 Pfleiderer. The extrusion temperature was 150°C and the
throughput was 10 kg/h.

In a second processing step, a connection box 100 having
the dimensions 107 x 107 x 57 mm was injection molded on
an FM 60 injection molding machine from Klöckner
10 Ferromatik. The temperature in the heating zone was 150 -
160°C and that in the mold was 40-60°C. The injection
pressure was 10 bar.

The connection box having a mean material thickness of 2.5 mm was closed by means of a steel sheet cover. This arrangement was mounted in a corresponding Ytong wall recess. The side with the steel sheet cover was installed facing the fire in the furnace.

5 A thermocouple for temperature measurement was mounted on the back of the connection box. In the course of the fire test, the connection box became completely filled with foam. The temperature on the back panel after 10 2 hours was 300°C.

Test specimens were produced from another connection box and the mechanical properties in the tensile strength test according to DIN 53 455 and the expansion factor at 300°C and in the course of 30 minutes were 15 determined. The values are shown in table 1.

A round connection socket having the dimensions 70 mm diameter and 36 mm height were injection molded from the same granules and likewise mounted in a 100 mm thick Ytong wall in a corresponding circular recess, 20 closed with a steel sheet cover and tested in the furnace. After 2 hours, the back panel reached a temperature of 320°C.

Example 3:

25 A powder mixture comprising

- 45% of BMI B21 bismaleimide (DSM Fine Chemicals)
- 40% of vermicular graphite (Kaisersberg)
- 30 15% of clay 610 (Bischitzky)

and having a bulk density of 35 g/l was prepared.

A connection box was injection molded on a conventional injection molding machine for heat-curable plastics, 35 having an L/D ratio of 15 and a compressionless screw with a pitch of 0.8, at a screw speed of 40 rpm.

The temperatures were 50-60°C in the feed zone, 50-60°C in the compression zone, 100-110°C in the discharge

zone and 230°C in the mold. The injection pressure was 600 bar.

The postcuring was effected in 8 h at 200°C.

The mechanical properties are shown in tab. 1 and the fire behavior and the back panel temperature of 280°C are shown in tab. 2.

A US distributor box having the dimensions 100 x 100 x 50 mm was likewise injection molded in order to be able to subject it to the UL test according to the setup of fig. 1 and 2. 180°C was not exceeded in the course of 2 hours. To ensure that the material intumesces only in an inward direction, a glass fabric tape is placed around the box.

15

Example 4

A powder mixture comprising

20 50% of BMI B 21

35% of vermicular graphite (Kaisersberg)

15% of 3 mm Vetrotex 355 glass fibers (Vetrotex) was prepared.

Round connection sockets and polygonal US distributor boxes were produced on the injection molding machine of example 3 under the same processing conditions. The corresponding data are shown in tab. 1 and 2.

30 **Example 5**

A powder mixture comprising

45% of BMI B 21

40% of vermicular graphite

35 15% of nanodisperse clay EXM 784 from SÜD-Chemie AG and having a bulk density of 0.4 g/cm³ was prepared and was processed on an injection molding machine from Klöckner Ferromatik to give moldings. The screw speed was 45 rpm and the temperatures for the injection unit

were 55°C in the feed zone, 55°C in the compression zone and 110°C in the discharge zone. The mold temperature was 250°C. An injection pressure of 500 bar and an after-pressure of 500 bar were applied. The postcuring was effected at 200°C in the course of 8 h. The fire behavior and the mechanical properties of round and rectangular connection boxes are shown in tables 1 and 2.

10 **Example 6**

42.1% of a copolymer of ethylene and octene: Exact Dextra 2M003 Elastomer (DSM)

42.1% of vermicular graphite (Kaisersberg)

15 10.5% of clay 610 (Bischitzky)

5.3% of Exolit 422 ammonium polyphosphate (Clariant)

were processed on a ZSK 30 to give granules. Rectangular connection boxes were then injection molded on an injection molding machine at 15 bar and at a feed zone temperature of 150°C and a mold temperature of 40°C.

20 The wall thickness was once again 2.5 mm. In the fire test of tab. 2, once again complete foam-filling of the box was observed. The back panel temperature after 25 2 hours was 280°C.

Example 7

Granules were produced from a mixture of

30 40% of a copolymer of ethylene and octene: Exact Dextra 0203 Elastomer (DSM)

40% of vermicular graphite

10% of china clay

35 10% of Amgard NK ethylenediamine phosphate (Albright and Wilson)

on a ZSK 30 and were then injection molded to give round and polygonal distributor boxes.

Example 8:

Granules having the following composition were produced by means of extrusion:

5

40% of ethylene-polyvinyl acetate Mowilith D 200 EVA (Clariant)

30% of Exolit 422 ammonium polyphosphate (Clariant)

15% of melamine (BASF)

10

15% of dipentaerythritol (Perstorp)

The extrusion temperature was 200°C. In a second operation, round connection sockets having a diameter of 70 mm and a height of 35 mm were injection molded at 90°C.

15

These were closed with a steel sheet cover and tested in a 100 mm thick Ytong wall in a furnace. The steel sheet cover was on the cold side. A thermocouple indicated the temperature of the cover. After 2 hours, 350°C was reached.

20

Table 1: Mechanical properties

Example	Tensile strength MPa	Elongation %	Modulus of elasticity MPa	Expansion under load 550°C/30 min (5g/cm ²)
2	4.5	8.0	200	16
3	50	0.5	6 000	14
4	30	0.4	7 000	15
5	40	0.3	6 500	15
6	3	12.0	175	15
7	5	5.5	450	16
8	4	10.0	200	17

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Tab. 2 Fire behavior of connection boxes and connection sockets

Example	Connection box/socket Back panel temperature (°C)	Connection box/socket Degree of foam-filling (%)	UL test (min)
1	600/ -	0/ -	
2	300/320	100/100	
3	280/ -	100/ -	> 120
4	- /300	100/100	> 120
5	290/ -	100/ -	> 120
6	280/ -	100/ -	
7	270/ -	100/ -	
8	320/ -	100/ -	

5

In the claims which follow and in the preceding description of the invention, except where the context requires otherwise due to express language or necessary implication, the word "comprise" or variations such as "comprises" or "comprising" is used in an inclusive sense, i.e. to specify the presence of the stated features but not to preclude the presence or addition of further features in various embodiments of the invention.

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

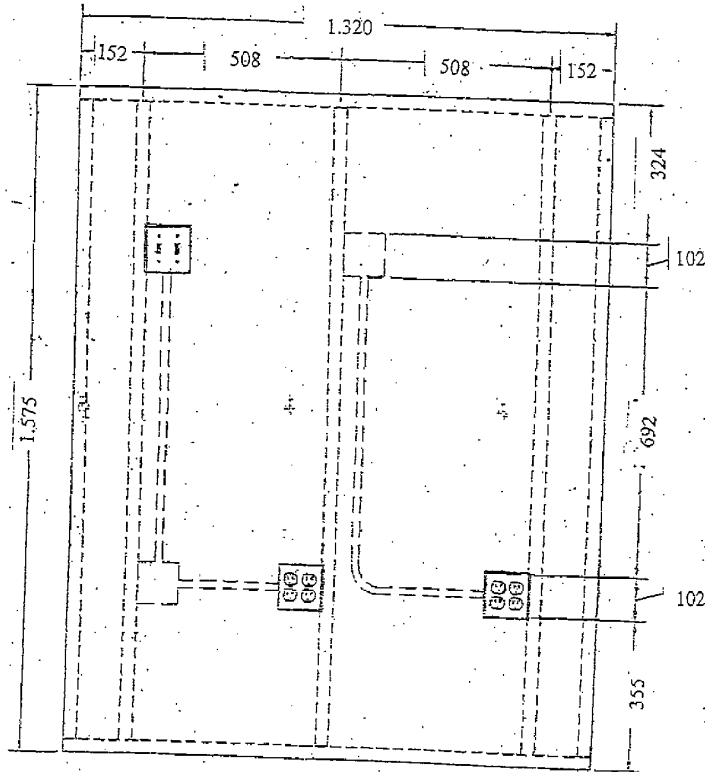
1. An intumescent, electrical installation system, which is formed solely from an injection molding material consisting of
 - a) 20 - 50% per weight of a polyimide
 - b) 50 - 80% per weight of intumescent additives,
 - c) 0 - 20% per weight of inorganic fillers and
 - d) 0 - 5% per weight of dispersants.
2. The intumescent, electrical installation system as claimed in claim 1, wherein the polyimides used are those which are present as a low-melting precursor and form highly crosslinked products by addition reactions under the action of heat.
3. The intumescent, electrical installation system as claimed in claim 1 or claim 2, wherein ammonium polyphosphate, ammonium dihydrogen phosphate, ethylenediamine phosphate, ammonium pentaborate, melamine, dicyandiamide, full phosphoric esters with polyols, dipentaerythritol, pentaerythritol, sugar, dextran, starch, vermicular graphite, waterglass, expanded mica, vermiculite, perlite and mixtures thereof are used as intumescent additives.
4. The intumescent, electrical installation system as claimed in any one of claims 1 to 3, wherein the injection molding material contains inorganic fillers from the group consisting of kaolin, clays, mica, wollastonite, calcium silicates, titanium dioxide, zinc borate, quartz, zinc oxide, apatite, talc, aluminum phosphates, ATH, $Mg(OH)_2$, chalk, glass fibers or mineral fibers.
5. The intumescent, electrical installation system as claimed in claim 4, wherein clays or micas which are

present as nanoparticles in the mixture of polymer, intumescent additive and filler are used as the inorganic filler.

- 5 6. The intumescent, electrical installation system as claimed in any one of claims 1 to 5, wherein the injection molding material contains dispersants from the group consisting of zinc stearate or calcium stearate, glyceryl stearate, pentaerythrityl
- 10 tetrastearate, cetyl palmitate, ethylenedistearoyldiamide C₁₄-C₁₈ fatty alcohols, dicarboxylic esters, fatty amines or paraffins.
- 15 7. The intumescent, electrical installation system as claimed in any one of claims 1 to 6, wherein the material thickness is such that it corresponds to the volume of the installation system divided by the product of twice the lateral surface area and the maximum expansion factor, so that the installation
- 20 system is completely filled with foam by intumescence and a compression factor of 2 is present.
- 25 8. An intumescent, electrical installation system substantially as herein described with reference to any one of Examples 3 to 5.

Fig. 1

Construction Details in mm

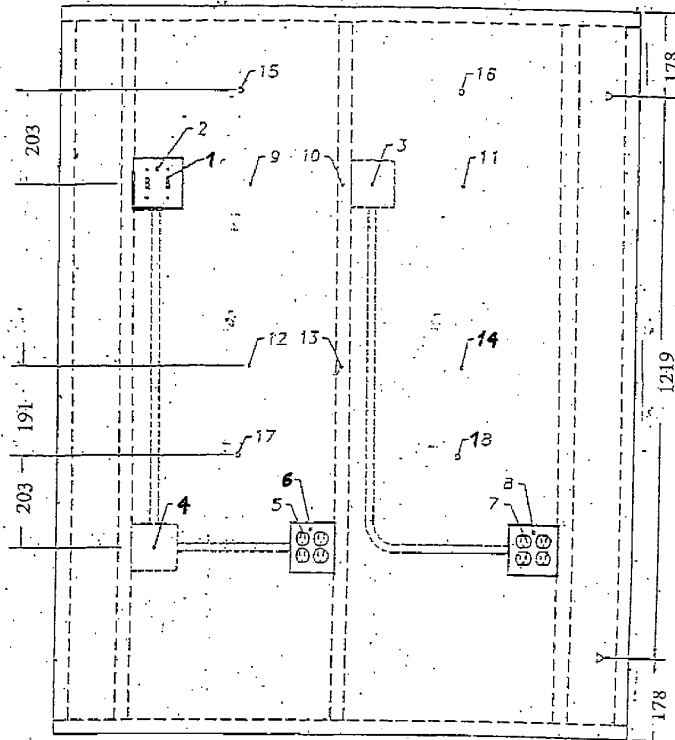


Unexposed Surface

Steel studs 1.575mm x 1.320mm; 9mm deep
On both sides faced with two layers of
gypsum wallboards 2 x 16mm = 32mm

Fig. 2

Thermocouple Locations



Thermocouple No:

- 1
- 2
- 3,4
- 5,7
- 6,8
- 9,11,12,14
- 10,13
- 15-18

Location

- On the box
- On the switch face plate
- On gypsum wall board over outlet boxes
- On top of duplex plug
- On the face plate
- On gypsum wall board away from boxes
- On gypsum wall board over steel stud
- Inside stud cavity at middepth of wall