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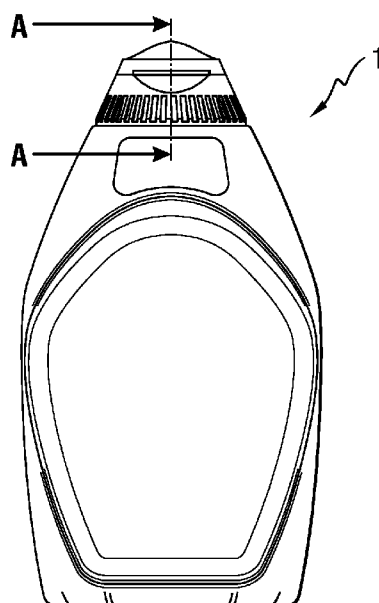


Fig. 1A

(57) Abstract: An apparatus and means of repeatedly dispensing controlled doses of liquid contained in a resiliently squeezable container, wherein the dose size can be adjusted..



LIQUID DOSING APPARATUS

FIELD OF INVENTION

The present invention relates to an apparatus and means of repeatedly dispensing controlled doses
5 of liquid, while also varying the dosage volume.

BACKGROUND OF THE INVENTION

It may be desirable to deliver a precise dose of a liquid and be able to vary and select the volume
of this dose for different applications and different needs. It may also be desirable to provide a
10 dosage system that does not rely solely on gravity or needs a bulky volumetric dosing chamber or
requires a complex and large pumping mechanism. It may be particular desirable to deliver said
benefits by simply inverting and squeezing a container whilst offering a compact, low cost and
simple constructions.

For example, a large dose is desired when dosing a hard surface cleaning composition into a bucket
15 of water for the general cleaning of floors. However, a smaller dose is desired when directly
applying the hard surface cleaning composition onto the surface for spot cleaning a stain. A large
dose would also be desired for dosing a laundry liquid composition into a washing machine, while
a smaller dose is desired for direct application onto a fabric stain.

EP2653842 relates to an apparatus and means of repeatedly dispensing controlled doses of liquid
20 comprising a resiliently squeezable container for containing a liquid detergent composition; a cap
operably connected to said container, the cap comprising a nozzle for expelling the liquid out of
the container; a dosing chamber operably connected to the cap, wherein the dosing chamber
comprises a base having a discharge opening therein, sidewalls extending upwardly along the
perimeter of said base and at least one inlet opening located proximal the sidewalls; at least one
25 timer aperture located proximal to the discharge opening; a plunger, provided in the dosing
chamber and moveable relative to the chamber so as to advance upon squeezing of the container,
up to a blocking position; a valve retaining means located below the base; a valve provided in the
valve retaining mean wherein the valve is movable from an open position, allowing liquid flow
through the discharge opening, and a closed position, where the valve blocks the discharge
30 opening; wherein the liquid is a shear thinning liquid and the shear thinning liquid has a viscosity
of greater than 150mPa.s measured at 10s⁻¹ at 20°C. EP2444782 relates to an apparatus and means
of repeatedly dispensing controlled doses of liquid.

WO 2005049477 A2 relates to liquid dosing devices of the kind in which flow to a front discharge
opening of a container is blocked after a controlled delay by a sliding piston movable in a control

chamber mounted in a container neck behind the discharge opening. Movement of the piston is governed by restricted flow through control openings at the back of the control chamber. Restoration of the piston after a dosing operation is assisted by providing a dump valve at the rear of the control chamber. For simplicity and ease of construction, as well as effective sealing operation, the dump valve member is a ball retained in a cage. Another proposal provides a one-way valve in the outlet path, obviating the dump valve and enabling rapid recovery after a dosing operation when used with a resiliently squeezable container.

SUMMARY OF THE INVENTION

The present invention relates to a dosing apparatus (1) for dispensing a dose of liquid comprising: a resiliently squeezable container (2); a cap (3) operably connected to said container (2); a dosing chamber (4) operably connected to said cap (3), wherein said dosing chamber (4) comprises a dosing chamber base (12) having a discharge opening (13) therein, dosing chamber sidewalls (14) extending upwardly along the perimeter of said dosing chamber base (12) and at least one dosing chamber inlet opening (15) located proximal said dosing chamber sidewalls (14); at least one timer aperture (16) located proximal to said discharge opening (13); a valve retaining means (6) located below said dosing chamber base (12); a valve (7, 29, 33) provided in said valve retaining means (6) wherein said valve (7, 29, 33) is movable from an open position, allowing liquid flow through said discharge opening (13), and a closed position, where the valve blocks said discharge opening; characterized in that the dosing chamber (4) comprises: a rotatable element (34), wherein the rotatable element (34) comprises: a rotatable element base (35), the rotatable element base (35) located proximal to the at least one timer aperture (16), the rotatable element base (35) comprising at least one flow restricting aperture (37) having an exposed cross-sectional area, such that the exposed cross-sectional area of the at least one timer aperture (16) is altered by rotating the rotatable element (34), in order to alter the dose, and at least one rotatable element opening (38) located proximal to the at least one dosing chamber inlet opening (15); a plunger, provided in said rotatable element (34) and moveable relative to said rotatable element (34) so as to advance upon squeezing of said container (2), up to a blocking position; and the cap (3) or rotatable element (34) comprises a nozzle (8).

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1A is a front view of the dosing apparatus (1) according to one embodiment of the present invention.

Fig. 1B is a side view of the dosing apparatus (1) according to one embodiment of the present invention.

Fig. 2 is an exploded view of the dosing apparatus (1) according to one embodiment of the present invention.

5 Fig. 3 is a cross-section taken along the line A-A of Fig. 1A of the dosing apparatus (1) according to one embodiment of the present invention.

Fig. 4 is an isometric view of a piston (5) of the dosing apparatus (1) according to a preferred embodiment of the present invention.

10 Fig. 5A is an isometric view of part of a rotatable element (34), with a cut-out showing the placement of the piston (5).

Fig. 5B is an isometric view of part of the rotatable element (34) of Fig. 5A, viewed from below in order to show the rotatable element base (35) and flow restricting aperture (37).

Fig. 5C is an isometric view of the assembly of the rotatable element (34), plunger, dosing chamber (4), valve (7), and nozzle (8), positioned in the dosing apparatus (1).

15 Fig. 6A is a bottom view of a dosing chamber base (12) comprising 3 timer apertures (16) (left) and a corresponding rotatable element base (35) comprising flow restricting apertures (37) having two different sizes (right).

Figure 6B is a view of the dosing chamber base (12) superposed under the rotatable element base (35) such that the timer apertures (16) are superposed with the largest flow restricting apertures (37).

Figure 6C is a view of the dosing chamber base (12) superposed under the rotatable element base (35) such that the timer apertures (16) are superposed with the smallest flow restricting apertures (37).

25 Fig. 7A is a view of a dosing chamber base (12) (left) having circular timer apertures (16) and a rotatable element base (35) (right) having flow restricting apertures (37) in the form of an elongated opening, such each elongated opening has a width which varies along the major axis of the elongated opening. The major axis of the elongated opening is radially offset, such that the radial distance of the center-line of the elongated opening increases from the first opening extremity to the second opening extremity.

30 Fig. 7B is a view of the dosing chamber base (12) of Fig. 7A with the rotatable element base (35) of Fig. 7A superimposed on top.

Fig. 8A is a view of a dosing chamber base (12) (left) having timer apertures (16) in the form of an elongated opening, such each elongated opening has a width which varies along the

major axis of the elongated opening, and a rotatable element base (35) (right) having circular flow restricting apertures (37).

Fig. 8B is a view of the dosing chamber base (12) of Fig. 8A with the rotatable element base (35) of Fig. 8A superimposed on top.

5 Fig. 9A to 9D shows an embodiment where the overlap of the at least one timer aperture (16) and the at least one flow restricting apertures (37) can altered by rotating the rotatable element (34) such that exposed cross-sectional area of the timer apertures (16) is altered.

Fig. 10 is an axial cross-section of an embodiment of the present invention illustrating the flow path of the liquid into the dosing chamber.

10 Fig. 11 is a cross-section taken along the line A-A of Fig. 1A of the dosing apparatus according to one embodiment of the present invention.

Fig. 12A and 12B illustrate an embodiment comprising a valve retaining means (6) formed by a projection (32) extending from the dosing chamber base (12) which engages with a flexible one-way disc valve (33) via a central snap fit.

15 Fig. 13 illustrates an embodiment having a valve (29) which is bullet shaped.

Fig. 14A to 14C are axial cross-sections of an embodiment of the present invention illustrating the positioning of the piston and valve in the various phases of dispensing.

DETAILED DESCRIPTION OF THE INVENTION

20 By the terms “a” and “an” when describing a particular element, we herein mean “at least one” of that particular element.

The term “dose” as used herein is defined as the measured amount of liquid to be delivered by the apparatus. The dose begins when the liquid first exits the nozzle and ends once the flow of said liquid stops. The volume of liquid dosed for each squeeze of the container is typically from
25 1ml to 80ml, preferably from 3ml to 40ml, more preferably 10ml to 30ml, and even more preferably 15ml to 30ml.

By “substantially independently from pressure” as used herein it is meant that pressure causes less than 10% variation from the target measured dose.

30 By “substantially constant liquid output or dosage” as used herein it is meant that variation from the target measured dose is less than 10%.

By “resiliently squeezable” as used herein it is meant that the container returns to its original shape without suffering any permanent deformation once pressure is released therefrom.

By “shear thinning” as used herein it is meant that the liquid referred to is non-Newtonian and preferably has a viscosity that changes with changes in shear rate.

By “ergonomic(s)” as used herein it is meant that the feature(s) is designed to maximize productivity by reducing operator (or user) fatigue and discomfort.

By “drip-free” as used herein it is meant that no visible residue is left proximal to the nozzle of the cap following dosing and/or that no liquid exits the resilient container when the apparatus is held top down without squeezing.

Various embodiments will now be described to provide an overall understanding of the principles of the structure, function, manufacture, and use of the apparatus and methods disclosed herein. One or more examples of these embodiments are illustrated in the accompanying drawings. Those of ordinary skill in the art will understand that features described or illustrated in connection with one example embodiment can be combined with the features of other example embodiments without generalization from the present disclosure.

A preferred field of use is that of dosage devices for domestic or household use, containing detergents such as hard surface cleaning compositions, liquid laundry detergent compositions, or other cleaning preparations, fabric conditioners and the like. Other fields of use include dosage devices for manual and automatic dishwashing liquids, hair-care products and oral care applications such as mouth washes, beverages (such as syrups, shots of liquors, alcohols, liquid coffee concentrates and the like), food applications (such as food pastes and liquid food ingredients), pesticides, and the like.

The resiliently squeezable container (2) can comprise a liquid therein, preferably a detergent composition. The liquid can be Newtonian or shear thinning. The viscosity of the liquid can be from 1 to 350mPa•s, preferably from 1 to 300mPa•s, more preferably from 1 to 250 mPa•s, even more preferably from 1 to 220 mPa•s, even more preferably 1 to 200mPa•s and most preferably from 1 to 150mPa•s (measured at 1000s⁻¹ at 20°C).

The invention is directed to an apparatus (1) for repeatedly dosing a quantity of liquid, in which the quantity of liquid dosed can be easily adjusted to suit the user’s requirement. The apparatus (1) comprises a resiliently squeezable container (2), a cap (3) operably connected to the container, a dosing chamber (4) operably connected to said cap (3), a plunger provided in said dosing chamber (4), a valve retaining means (6), and a valve (7). The apparatus (1) may have a longitudinal axis (YY) extending along/or substantially parallel to, the centerline of the apparatus (1). Said

longitudinal axis (YY) may also be parallel to the direction of a portion of the fluid flow during dispensing.

The dosing chamber comprises a rotatable element (34), as exemplified in Fig. 2, and 5A to 5C.

5 The rotatable element (34) comprises a rotatable element base (35) having a rotatable base discharge opening (39) located therein. Preferably, the rotatable base discharge opening (39) is located at the centre of the rotatable element base (35) to allow the liquid accumulated in the volume (11) of the rotatable element (34) below the plunger to be quickly flushed back into the container (2) after squeezing. At least one flow restricting aperture (37) is located proximal to the
10 rotatable base discharge opening (39). The rotatable element (34) also has rotatable element sidewalls (36) extending upwardly along the perimeter of the rotatable element base (35) and have at least one rotatable element opening (38) located proximal to said rotatable element sidewalls (36). Preferably, the rotatable element opening (38) are located proximal to the apex of the rotatable element sidewalls (36) opposite the rotatable element base (35) of the rotatable element
15 (34). The rotatable element base (35) may be chamfered to form an inclined surface extending from the rotatable element sidewalls (36) to the rotatable base discharge opening (39). Preferably, said inclined surface extends substantially linearly from said rotatable element sidewalls (36) to said rotatable base discharge opening (39). Such configuration allows the liquid to drain from the rotatable element (34) in an effective manner without leaving any left-behind residue, particularly
20 in locations proximal to the rotatable element sidewalls (36), which would otherwise cause jamming of the plunger upon drying.

The rotatable element base (35) is located proximal to the at least one timer aperture (16). The rotatable element base (35) comprises at least one flow restricting aperture (37), such that the
25 exposed cross-sectional area of the at least one timer aperture (16) is altered by rotating the rotatable element (34), in order to alter the dose. The rotatable element base (35) further comprises at least one rotatable element opening (38) located proximal to the at least one dosing chamber inlet opening (15).

30 To simplify construction, the rotatable element (34) can be made in at least two parts which clip together. For instance, a first part of the rotatable element (34a) can comprise a protrusion (40a) while a second part of the rotatable element (34b) can comprise a corresponding groove (40b), as exemplified in Fig. 5A and Fig. 5B. The exterior surface of the rotatable element (34) and interior

surface of the dosing chamber (4) can also be connected by a cooperating protrusion (41a) and groove (41b), as shown in Fig. 5A and Fig. 10, such that the rotatable element can be rotated.

The rotatable element (34) contains a plunger, provided in said rotatable element (34) and moveable relative to said rotatable element (34) so as to advance upon squeezing of said container (2), up to a blocking position, as exemplified in Fig. 14A to Fig. 14C.

The rotatable element base (35) can comprise a plurality of different flow restricting apertures (37) such that a different flow restricting aperture (37) is positioned over the at least one timer aperture (16) by rotating the rotatable element (34), as exemplified in Figures 6A to 6C. In such embodiments, the liquid dose is varied by positioning a different flow restricting aperture (37) over at least one timer aperture (16). The smallest flow restricting aperture (37) can have a cross-sectional open area which is less than 90%, preferably less than 50%, more preferably less than 25% of the cross-sectional open area of the largest flow restricting aperture (37), based on the cross-sectional open area.

The number of dose settings can be defined by the ratio of the number of flow restricting apertures (37) to the number of timer apertures (16). For less than 4 dose settings, the ratio of the number of flow restricting apertures (37) to the number of timer apertures (16) is less than 4. For less than 3 dose settings, the ratio of the number of flow restricting apertures (37) to the number of timer apertures (16) is less than 3. For 2 dose settings, the ratio of the number of flow restricting apertures (37) to the number of timer apertures (16) is 2, as exemplified in Fig 6A to 6C.

Alternatively, or in addition, the flow restricting aperture (37) or timer aperture (16) can be in the form of an elongated opening, wherein the elongated opening comprises a major axis having at one end, a first opening extremity (42), and having at the second end, a second opening extremity (43), and is positioned such that the exposed cross-sectional area of the at least one timer aperture (16) is varied by rotating the rotatable element (34). Such embodiments are exemplified in figures 7A and 7B, wherein the flow restricting aperture (37) is in the form of an elongated opening. Embodiments wherein the timer aperture (16) is in the form of an elongated opening are exemplified in figures 8A and 8B. Preferably, each elongated opening has a width which varies along the major axis of the elongated opening. The major axis of the elongated opening can be radially offset, such that the radial distance of the center-line of the elongated opening increases

from the first opening extremity to the second opening extremity, as exemplified in figures 7A, 7B, 8A and 8B.

The overlap of the at least one timer aperture (16) and the at least one flow restricting apertures (37) can altered by rotating the rotatable element (34) such that exposed cross-sectional area of the timer apertures (16) is altered, as exemplified in figures 9A to 9D.

The rotatable element (34) can be rotated in an arc, wherein the arc has two arc extremities and the at least one flow restricting aperture (37) is arranged such that the largest dose setting is proximal to one extremity of the arc, and as the rotatable element (34) is rotated, the dose settings become smaller, preferably incrementally smaller. At at least one of the arc extremities, the at least one timer aperture (16) is preferably not coincident with the at least one flow restricting aperture (37). As such, the dosing chamber is closed off when the at least one timer aperture (16) is not coincident with the at least one flow restricting aperture (37) (see Fig. 9B).

In addition, or alternatively, the overlap of the at least one dosing chamber inlet opening (15) and at least one dosing chamber opening (35) can altered by rotating the rotatable element (34) such that exposed cross-sectional area of the at least one dosing chamber inlet opening (15) is altered. In such embodiments, when the at least one timer aperture (16) is fully closed, the dosing chamber opening (35) is preferably not coincident with the at least one dosing chamber inlet opening (15).

The dose volume dispensed from the smallest dose setting can be from 5% to 90%, preferably from 10% to 50%, more preferably from 15% to 30% of the volume dispensed from the largest dose setting. Preferably, said dose can be varied from 1ml to 80ml, preferably from 3ml to 40ml, more preferably 10ml to 30ml.

Accordingly, the dosing apparatus (1) can dispense a volume from the smallest dose setting which can be from 5% to 90%, or from 5% to 66%, preferably from 10% to 50%, more preferably from 15% to 30% of the volume dispensed from the largest dose setting.

For certain applications, such as dispensing liquid hard surface cleaning compositions, the “high” dose can be from 10 ml to 100 ml, preferably from 15 ml to 50 ml, more preferably from 20 ml to 30 ml. In contrast, the “low” dose can be from 0.1 ml to 5.0 ml, preferably from 0.2 ml to 2.5 ml, more preferably from 0.3 ml to 1.0 ml. For instance, it is desirable to dispense a large dose of

liquid hard surface cleaning composition for dilution into a bucket of water, for example, for mopping of floors. In contrast, a smaller dose is desired for direct application on to a stain on a hard surface, before scrubbing.

- 5 For other applications, such as dispensing liquid laundry detergent compositions, the “high” dose can be from 20 ml to 150 ml, preferably from 25 ml to 120 ml, more preferably from 30 ml to 90 ml. In contrast, the “low” dose can be from 1 ml to 17.5 ml, preferably from 2.5 ml to 15 ml, more preferably from 5.0 ml to 10 ml. For instance, it is desirable to dispense a “high” dose of liquid laundry detergent composition into a washing machine, while a “low” dose is desired for direct
10 application on to a fabric stain during pretreating.

Referring to Fig. 2, Fig 10 and Fig. 11, the cap (3) or rotatable element (34) can comprise a nozzle (8) extending substantially parallel to the longitudinal axis (YY) preferably comprising and/or defining an orifice (9) at its apex, and an entry tube (10) which extends downwardly and opposite
15 said orifice (9). Said orifice (9) can comprise a slit valve to reduce and even eliminate dripping. The entry tube (10) may extend vertically downwardly substantially parallel to the longitudinal axis (YY) so as to at least partly enter a volume formed by the dosing chamber (4). The cap (3) or rotatable element (34) may further comprise a top lid (17) capable of engaging with the nozzle (8) to provide a closing and sealing means. Preferably, the top lid (17) may be pivotable upon a pivot
20 point (18) located on a surface of the cap (3). The person skilled in the art would understand that other closing features or cap constructions could also be used, such as twist, pull, push, screw or other caps known in the art. Preferably, the rotatable element (34) comprises the nozzle (8). Preferably, the cap (3) comprises the top lid (17).

25 The dosing chamber (4) comprises a dosing chamber base (12) having a discharge opening (13) located therein. Preferably, the discharge opening (13) is located at the centre of the dosing chamber base (12) to allow the liquid accumulated in the volume (11) of the dosing chamber (4) below the plunger to be quickly flushed back into the container (2) after squeezing. At least one timer aperture (16) is located proximal to the discharge opening (13). The dosing chamber (4) also
30 has sidewalls (14) extending upwardly along the perimeter of the dosing chamber base (12) and have at least one dosing chamber inlet opening (15) located proximal to said sidewalls (14). Preferably, the dosing chamber inlet openings (15) are located proximal to the apex of the sidewalls (14) opposite the dosing chamber base (12) of the dosing chamber (4). The dosing chamber base (12) may be chamfered to form an inclined surface extending from the sidewalls

(14) to the discharge opening (13). Preferably, said inclined surface extends substantially linearly from said sidewalls (14) to said discharge opening (13). Such configuration allows the liquid to drain from the dosing chamber (4) in an effective manner without leaving any left-behind residue, particularly in locations proximal to the sidewalls (14), which would otherwise cause jamming of the plunger upon drying. Preferably, the sidewalls (14) are essentially flush with the rotatable element sidewalls (36). Preferably, the dosing chamber base (12) is essentially flush with the rotatable element base (35). Grease or other lubricants can be added between the sidewalls 14 and sidewall 36 to improve the sealing and minimize the friction to rotate.

10 The rotatable base discharge opening (39) of the rotatable element base (35) is at least partially or fully superimposed onto the discharge opening (13) of the dosing chamber base (12).

The ratio of the total cross-sectional open area of dosing chamber inlet openings (15) and the timer apertures (16) can be between 2 to 25, preferably from 2 to 24, preferably from 2 to 23, preferably from 4 to 22, preferably from 6 to 22, more preferably from 8 to 20, most preferably 10 to 18.

The plunger is preferably in the form of a piston (5) and is moveable relative to the dosing chamber (4) and rotatable element (34) so as to advance upon squeezing of the inverted container (2). The piston (5) moves from a starting position - wherein the piston (5) is at its furthest position from the entry tube (10), up to a blocking position - wherein at least part of the piston (5) contacts the entry tube (10) so as to close it and terminating the dose. Preferably the motion of the piston (5) is linear and parallel to the longitudinal axis (YY), however, it is understood that any other kind of motion such as rotation and combination of rotation and translation may be equally suitable for generating a dose.

25

The valve retaining means (6) is located below the dosing chamber base (12) and may extend vertically downward from said dosing chamber base (12) in a direction substantially parallel to the longitudinal axis (YY). Preferably, the valve retaining means (6) is one part with the dosing chamber (4). This allows to reduce the number of parts required and contributes towards introducing benefits such as reduced manufacturing complexity and cost, and ease of assembly.

30 The valve (7) is preferably uni-directional (i.e. it opens and closes in one direction only) and is provided in the retaining means (6). The valve (7) is moveable from an open position - allowing

liquid to flow through the discharge opening (13), and a closed position - wherein the valve blocks said discharge opening (13).

In a preferred embodiment, said valve (7) may be spherical in shape and may be capable of blocking the discharge opening (13) by at least partly entering the dosing chamber (4). Preferably, said valve may be capable of contacting and/or impacting and/or abutting at least part of the piston (5) when said piston (5) is in its starting position and said valve (7) is in its closed position upon squeezing of the resilient container (2). Such configuration allows easy and accurate location of the valve into the discharge opening upon squeezing of the container (2) with no need for a specific orientation to be maintained. Another advantage is that by allowing the valve (7) to at least partly enter the dosing chamber (4) and impact and/or abut at least part of the piston (5), said valve (7) acts as a precursor and pushes up the piston so as to overcome any initial jamming of said piston (5).

In a preferred embodiment, as illustrated in both Fig. 3 and Fig. 4, the piston (5) may have a substantially flat surface, preferably a flat surface, and may comprise stabilizing wings (24) extending upwardly and substantially parallel to the longitudinal axis (YY). Preferably, the root of said stabilizing wings (24) may be located along the circumference of said piston (5). Said stabilizing wings may be spaced apart so as to minimize material used and any friction with the dosing chamber sidewalls (14) and rotatable element sidewalls (36). The diameter of said piston (5) may be smaller than the diameter of said dosing chamber (4) and said rotatable element (34) to further reduce any friction effects between the surfaces thereof. Preferably, said piston (5) may further comprise protrusions (25) extending opposite and mirrored to said stabilizing wings (24) wherein said protrusions (25) are of smaller length than said stabilizing wings (24). Without being bound by theory, it is believed that an advantage of the flat configuration of the piston is that the pressure differential is minimized between the liquid flowing through the dosing chamber inlet openings (15) and the liquid flowing through the timer apertures (16), thus rendering the rate of climb of the piston (5) and consequently the dosage, dependent primarily on the ratio of the surface of the openings and the viscosity of the liquid. A further advantage is introduced by the protrusions (25), which reduce contact with the dosing chamber base (12), thus minimizing jamming of the piston (5).

Referring to Fig. 10, when a force is applied to the inverted container (2), said container (2) experiences buckling and concurrently generates a pressure within said container (2) which causes

the valve (7) to close the discharge opening (13). The liquid is consequently forced to flow into the dosing chamber (4) via the timer apertures (16), through the flow restricting apertures (37), and also the dosing chamber inlet openings (15). The flow path of the liquid is shown by arrows A and B of Fig. 10. The part of the liquid that flows through the timer apertures (16), through the flow restricting apertures (37), pushes the piston (5) towards the entry tube (10), whilst the part of the liquid that flows through the dosing chamber inlet openings (15) and the rotating element opening (38) is directly expelled from the container (5) through the entry tube (10) and out of the nozzle (8). Once the piston reaches the entry tube (10) liquid flow is stopped and the dose complete. Releasing the force from the inverted container (2) causes the resilient spring-back of the container surfaces and allows the vacuum, formed during squeezing and buckling of the container (2), to open the valve (7) and effectively drain the dosing chamber (4) while the piston returns to its starting position. At the same time the volume above the piston fills with air which is pulled in via the nozzle(8), venting the container (2) to bring the deformed container (2) back to its starting form. At this point a new dose may be dispensed by simply squeezing again said container (2) without needing to rotate the apparatus (1) back to the upright position.

In one embodiment shown in Fig 13 the valve (30) may be an open bullet shape with a central timer aperture (16). The bullet shape closes the discharge opening (13) when the container is squeezed but a controlled stream of liquid can pass through timer aperture (16) to move the piston (5) forward ,

Referring to Fig. 3, in a preferred embodiment of the present invention the dosing chamber (4) may comprise dosing chamber sidewalls (14) extending vertically upwardly along the perimeter of dosing chamber base (12) and parallel to the longitudinal axis (YY), and at least two tabs (18) extending vertically upwardly from the apex of said dosing chamber sidewalls (14) in a direction opposite to said dosing chamber base (12). The tabs (18) may be spaced apart so as to form a castellation on the upper portion of the dosing chamber (4). Such tabs (18) may define dosing chamber inlet openings (15) formed by the open space between said tabs (18). Preferably, the perimeter of said dosing chamber base (12) may be substantially circular, however it is understood by the person skilled in the art that other shapes may also be suitable such as oval, squared, triangular and so on. This configuration allows for ease of manufacture of the dosing chamber inlet openings (15). More preferably, the dosing chamber comprises multiple tabs (18) forming multiple dosing chamber inlet openings (15).

In one embodiment the tabs (18) may further comprise a notch (19) which may follow the contour of the inside face of said tabs (18) and extend a predetermined length towards the longitudinal axis (YY), for compliance with a groove (20) located on a surface of the cap (3). Preferably, said surface of cap (3) faces opposite to said longitudinal axis (YY) and is located on a first skirt (21). Said first skirt (21) may extend downwardly and substantially parallel to said longitudinal axis (YY) from a first surface of the cap (3). The dosing chamber (4) may be connected to the cap (2) by snap fitting said tabs (18) to said first skirt (21). Such a construction allows for ease of assembly.

In a preferred embodiment the timer apertures (16) may be located in the dosing chamber base (12). Preferably, said timer apertures (16) may be proximal to the discharge opening (13) and the centre line of said timer apertures (16) may be parallel to the centre line of said discharge opening (13). An advantage of such configuration is that laminar flow is maintained which serves to apply a constant and balanced force on the piston. Without wishing to be bound by theory, it is believed that turbulent flow may destabilize the smooth movement of the piston.

In a particularly preferred embodiment (not shown), the timer apertures (16) may be in the form of multiple slots extending for a predetermined length from the discharge opening (13) towards the dosing chamber sidewalls (14) through the dosing chamber base (12). In this particular embodiment, the piston (5) comprises a ring-like protrusion extending from the base thereof in a direction substantially parallel to the longitudinal axis (YY) towards said dosing chamber base (12). The said ring-like protrusion may be capable of closing the multiple slots and the discharge opening (13) when in its starting position by being in relative contact with the corresponding surface of said dosing chamber base (12). An advantage of this configuration is that bubbling through the timer apertures is significantly reduced and even prevented when the filled container is inverted without squeezing it. Without wishing to be bound by theory, it is believed that when holding the apparatus (1) in its inverted position, particularly when at an angle or when the liquid in the container has been partly depleted, air may flow through the timer holes causing a back pressure differential that results in some of the liquid to flow in the dosing chamber (4) through the dosing chamber inlet openings (15) and leak. Consistent dosing is therefore improved over different tilt angles and also at different container fill levels.

In a preferred embodiment, the dosing chamber base (12) may be chamfered in such a way to define a first area and a second area. Preferably, said first area may be demarcated by the dosing chamber sidewalls (14), and said second area may define the circumference of the discharge

opening (13). More preferably, the said second area is located below said first area and the centerline of said first area coincides with the centerline of said second area.

Referring to Fig. 11, in an embodiment of the present invention, the cap (3) may comprise a second skirt forming a plug seal (22) extending downwardly proximal to the first skirt (21), and a v-shaped notch (23) proximal to said second skirt (22). The plug-seal (22) and the V-shaped notch (23) may be capable of at least partly engaging with the uppermost surface of the container (2) so as to provide a secure sealing means and prevent leakage during dosage. An advantage of such a configuration is the reduction in the number of parts, since an additional sealing means such as an O-ring or the like is no longer required.

In an embodiment (not shown) of the present invention, the first skirt (21) may comprise shutter tabs in the form of spaced flanges or the like to at least partly cover at least one of the dosing chamber inlet openings (15). Alternatively, the first skirt (21) may have shutter tabs formed by portions of the first skirt (21) subtending at a variable vertical distance taken from a plane substantially parallel to the longitudinal axis (YY) to form a series of preferably linear gradients along the entire circumference of said first skirt (21). In this embodiment the first skirt (21) may be rotatable with respect to the dosing chamber (4) so as to allow variation in the size of the dosing chamber inlet openings (15). This allows greater flexibility in dosage whereby the user can dispense different amounts of liquid by rotating the cap (3) which in turn changes the size of said inlet openings and thus the ratio of the surface of said dosing chamber inlet openings (15) and the timer apertures (16).

In a preferred embodiment of the present invention, as illustrated in Fig. 5C, the valve retaining means (6) may be formed by at least three flexible hook-shaped protrusions (26) extending downwardly from said dosing chamber base (12) in a direction opposite to the dosing chamber sidewalls (14) of the dosing chamber (4) and substantially parallel to the longitudinal axis (YY). An advantage of such hook shaped protrusions (26) is the simplification of the de-molding operation during manufacturing by allowing pull-off from the injection mold without complex slides in the mold. A further advantage is that said hook shaped protrusions (26) allow to assemble the valve (7) easily via push-fit, while minimizing contact between said valve (7) and said hook shaped protrusions (26) which aids in preventing blockage. Alternatively, the flexible hook-shaped protrusions (26) can be molded into the rotatable element base (35).

In a further embodiment the retaining means (6) may further comprise at least one flat panel extending downwardly from said dosing chamber base (12) and substantially parallel to the longitudinal axis (YY). Said panels are preferably located in the gaps formed between the hook-shaped protrusions (26). This configuration allows to securely locate the valve (7) inside the retaining means (6) in a child-proof manner by preventing the removal of the valve (7) once inserted.

In a preferred embodiment (not shown) the valve retaining means (6) may be formed by at least two overhangs, preferably at least three overhangs, extending downwardly from said dosing chamber base (12) in a direction opposite to the dosing chamber sidewalls (14) and substantially parallel to the longitudinal axis (YY). In this embodiment, a snap ring may join to the apex of said overhangs so as to define a valve insertion opening at the centre thereof. The snap ring may extend towards the centre of the valve insertion opening, and may be inclined at an angle from a plane perpendicular to said longitudinal axis (YY). Preferably, said angle is about 35° prior to the insertion of the valve through the valve insertion opening and deforms in a direction towards said dosing chamber base (12) when the valve is pushed through the valve insertion opening. The resulting angle of said snap ring after valve insertion is preferably -45° taken along said plane perpendicular to said longitudinal axis (YY). Preferably, said overhangs and said snap ring are one part with said dosing chamber (4). An advantage of this configuration is that potential entanglement of dosing chambers during the manufacturing procedure is avoided.

In another embodiment of the present invention, illustrated in Fig. 12A and Fig. 12B, the valve retaining means (6) may be formed by a projection (32) extending from said dosing chamber base (12) in a direction opposite to said dosing chamber sidewalls (14) and may engage with a flexible one-way disc valve (33) with a very low cracking pressure (i.e. low minimum upstream pressure at which the valve will operate). The valve (33) may be engaged to said valve retaining means (6) via a central snap fit or other means which allows movement of said valve (33) relative to said projection (32). The valve (33) may be substantially flat and circular in shape, although it is understood that other shapes may also be suitable such as dome shaped and/or umbrella shaped.

In an embodiment of the present invention, illustrated in Fig. 13, the valve (29) may be bullet shaped. Said bullet shape is defined by a substantially flat surface (30) on one end and a substantially convex surface (31) on the opposite end. The valve (29) may be inserted into the valve retaining means (6) via a snap fit or other means which allows movement of said valve (29)

relative to said valve retaining means, the valve retaining means (6) guiding the valve (29) and preventing it from changing orientation. The flat surface of said valve may have an opening subtending more than 50% of the diameter of said valve (29). The valve (29) may be oriented so that the convex surface (31) faces the discharge opening (13) and the flat surface (30) faces the inside of the container (2). An advantage of such configuration is ease of manufacture of the valve.

Referring to Fig. 1B, in a preferred embodiment the container (2) may comprise a front (27) and a back (28) surface in a facing relationship. Preferably, said front (27) and back (28) surfaces have a larger surface area compared to the other surfaces of the container (2) and are spaced apart so that the distance (d) between said front (27) and back (28) surfaces is between 30mm to 100mm. This specific range has been found to be optimal for allowing the user to correctly and comfortably grip the container and squeeze effectively.

The container (2) may be made of any flexible material, however, preferably said material is selected from the group consisting of PP, PET, PE or blends thereof. Said container (2) may be capable of displacing from 5ml to 150ml, preferably from 10ml to 80ml, of liquid without experiencing permanent deformation. Without being bound by theory it is believed that permanent deformation will create cracks in the container or cause paneling (i.e. the panels do not return to the starting position) which in turn reduce the displacement volume with each use, affecting the consistency of the dosage.

In a preferred embodiment (not shown), the container (2) may comprise an indicating means to indicate to the user the acceptable inclination angle of the apparatus (1) for effective dosage. Indeed, in some operations the user may need to angle the apparatus (1) due to space restrictions or simply comfort. However, tilting the apparatus (1) at too shallow angles may result in loss of accuracy of the dosage, particularly if air starts flowing through the dosing chamber inlet openings (15). This may be particularly true when the liquid is close to depletion. It may therefore be necessary to incline the apparatus (1) as much as possible but in such a way that the liquid still covers said dosing chamber inlet openings (15). An indicating means allowing the user to see when said liquid covers said dosing chamber inlet openings (15) may be desirable. Preferably, said indicating means is a transparent window located on said container (2) proximal to the connecting portion of the cap (3) with said container (2). Alternatively, said indicating means may be an entirely transparent container. A further advantage of such configuration is that the depletion of

the liquid may be inspected by the user and the correct functioning of the valve and piston communicated.

The container (2) can comprise a front surface (27) and a back surface (28), wherein the distance
5 between said front to said back surfaces is between 30mm to 120mm.

An advantage of the present invention is that constant dosage during use (i.e. as the liquid being dispensed is depleted from the container) is achieved whilst providing optimal ergonomics for the end user who can dispense a dose of liquid without experiencing strain during the squeeze
10 operation, and allowing the dose size to be readily altered according to need. Indeed in a preferred embodiment, the dosing apparatus of the present invention consists of an ergonomic dosing apparatus.

In an preferred embodiment, the dosing apparatus delivers a dose of liquid at a pressure of less
15 than 150kPa, preferably less than 120 kPa, preferably less than or equal to 110 kPa, more preferably from 80 kPa to 110kPa, even more preferably from 90 kPa to 100kPa, measured according to the test method described herein. Without wishing to be bound by theory it is believed that higher pressures provide detriment to the ergonomics of the apparatus since the user is otherwise required to exert large forces over an extended squeeze time.

In an embodiment of the present invention, the dosage time is typically less than or equal to 3s, preferably less than or equal to 2s, preferably less than or equal to 1.5s, preferably less than or equal to 1s and more preferably less than or equal to 0.75s but greater than 0s, most preferably from 0.4s to 0.75s. Without wishing to be bound by theory it is believed that if the time of squeeze
20 is too high, the user will apply a more variable squeezing force with the greatest force being applied towards the end of the squeeze resulting in the user experiencing an undesired fatigue especially in circumstances where multiple doses are required.

It has been found that the ratio of the total cross-sectional open area of the dosing chamber inlet
30 openings (15) and the orifice (9) may also affect the dose, in particular if the total cross-sectional open area of the orifice is smaller than the total cross-sectional open area of the inlet openings. However, if the orifice (9) is too large, dripping may occur which would require the introduction of additional features to minimize said dripping such as silicone or thermoplastic elastomers (TPE) slit-seal valves and/or cross-shaped cuts in the orifice. Preferably, the ratio of the total cross-

sectional open area of said dosing chamber inlet openings (15) and said orifice (9) may be from 4 to 0.25, preferably 1.

The ratio of the dosing chamber inlet openings (15) and the orifice (9) may be selected such that the speed of dosage is less than or equal to 1.5s, preferably less than or equal to 1s and more preferably less than or equal to 0.75s, at ratios of total surface of the dosing chamber inlet openings (15): timer apertures (16) of from 15 to 25, preferably 18 to 25, more preferably 22 to 25.

In a preferred embodiment, the dose of liquid being expelled through the nozzle has a flow rate of greater than 20g/s, preferably greater than 25g/s, preferably greater or equal to 30g/s, more preferably greater or equal to 35g/s, more preferably greater or equal to 38g/s, more preferably greater or equal to 40g/s, even more preferably from 42g/s to 70g/s, even more preferably from 45g/s to 65g/s, most preferably from 50g/s to 60g/s, typically measured for the first 10 squeezes starting from a full container. By “full container” it is herein intended that the resilient container of the apparatus is filled with liquid as much as is normal in the field of detergent bottles, this is typically about 90% of the total inner volume of the container. Without wishing to be bound by theory it is believed that lower flow rates provide detriment to the ergonomic squeeze.

The viscosity and rheology profile of the liquid may impact the accuracy, speed of dosage, and comfort in the squeeze operation. It has been found that liquids having a shear thinning-type rheology profile and viscosity within the below-mentioned ranges ensure an acceptable force to be applied to the resilient container and thus permit an ergonomic squeeze of the container to provide a drip-free dose. In a preferred embodiment the liquids herein have a viscosity of from 1 to 350 mPa•s, preferably 1 to 300 mPa•s, more preferably from 1 to 250 mPa•s, even more preferably to 220 mPa•s, measured at 1000s⁻¹ at 20°C. It has further surprisingly been found that the above viscosities will deliver a constant dose of liquid whilst permitting such ergonomic squeeze. If the viscosity of the liquid is above the mentioned ranges, an unacceptable amount of force is required to be applied by the user to complete a dose.

The viscosity measurements referred to herein are taken with an AR 1000 from TA instruments with a 2° 1' 5" cone angle spindle of 40mm diameter with truncation of 57 micrometer. By “constant dose” it is herein meant that the variation in dose over multiple squeezes, typically 10 consecutive squeezes starting from a full container, does not exceed ± 3ml, preferably ± 1ml.

It has also been found that particularly shear thinning liquids provide for an optimal ergonomic squeeze of the resilient container thus providing good feel for the user upon dosing, this whilst also minimizing dripping. Without wishing to be bound by theory, it is believed that liquids having a viscosity of greater than 150 (and the below mentioned preferred ranges) at low shear (i.e. 10s^{-1} at 20°C), in combination with the apparatus according to the present invention, provides a dose of liquid substantially drip-free but also provide the necessary feel and control to the user in the squeeze operation. At the same time, ensuring that the same liquid has a high shear viscosity (i.e. 1000s^{-1} at 20°C) that is below the corresponding viscosity at low shear, preferably within the above mentioned cited ranges, ensures constant dosage with minimal effort whilst providing controlled squeezing. Therefore in a highly preferred embodiment the apparatus according to the present invention comprises a resilient container comprising a shear thinning liquid therein typically having a viscosity, at a shear rate of 10s^{-1} at 20°C , of more than 1 time, preferably at least 1.5 times, preferably 2 times, preferably from 2 to 100 times, more preferably from 3 to 50 times, even more preferably from 4 to 20 times, even more preferably from 5 to 15 times, most preferably from 6 to 10 times, greater than the viscosity at a shear rate of 1000s^{-1} at 20°C .

In a preferred embodiment, the low shear viscosity (i.e. at 10s^{-1} at 20°C) is greater than $150\text{mPa}\cdot\text{s}$, preferably greater than $200\text{mPa}\cdot\text{s}$, more preferably greater than $250\text{mPa}\cdot\text{s}$, even more preferably greater than $300\text{mPa}\cdot\text{s}$. Viscosities below the above ranges result in undesirable dripping which not only provides unsightly residues being formed on the cap proximal to the orifice and messiness but also considerably affects consistency of the dosage.

Compositions suitable for use in the apparatus of the present invention are formulated as liquid compositions, preferably liquid detergent compositions, typically comprising water, preferably in an amount from 10% to 85% by weight of the total composition. Suitable compositions may be acidic or alkaline or both, and may further comprise abrasive cleaning particles, suspending aids, chelating agents, surfactants, radical scavengers, perfumes, surface modifying polymers, solvents, builders, buffers, bactericides, hydrotropes, colorants, stabilizers, bleaches, bleach activators, suds controlling agents like fatty acids, enzymes, soil suspenders, anti dusting agents, dispersants, pigments, thickeners, and/or dyes.

In a highly preferred embodiment the liquid compositions herein consist of a compact liquid. As used herein “compact” means a composition having densities in the range of from 0.5 to 1.5 grams,

preferably from 0.8 to 1.3 grams, more preferably from 1 to 1.1 grams, per cubic centimeter, excluding any solid additives but including any bubbles, if present.

When a compact liquid is used, such has a shear thinning rheology profile to enable accurate and constant dispensing. In particular, the compact liquid typically has an undiluted viscosity “Vu” of from 1 to 350 mPa•s, preferably 1 to 300 mPa•s, more preferably from 1 to 250 mPa•s, even more preferably 1 to 220 mPa•s, at high shear (measured at 1000s^{-1} at 20°C) and of greater than 150mPa•s, preferably greater than 200 mPa•s, more preferably greater than 250mPa•s, even more preferably greater than 300 mPa•s, even more preferably from 300 mPa•s to 15000 mPa•s, even more preferably from 300 mPa•s to 10000 mPa•s, most preferably from 300 mPa•s to 5000 mPa•s at low shear (measured at 10s^{-1} at 20°C), and a diluted viscosity “Vd” that is less than or equal to 0.8Vu, more preferably less than or equal to 0.5Vu, even more preferably less than or equal to 0.3Vu at the respective shear rate, typically measured at a low shear rate of 10s^{-1} at 20°C . The water that is used to prepare the aqueous solution for determining the diluted viscosity Vd of a composition is deionized water. The dilution procedure is described below. The advantage of such embodiment is that highly concentrated compositions may be formulated in the apparatus of the present invention whilst still achieving the desired consistency in drip-free dosage. Moreover, a compact liquid composition having the above diluted viscosity “Vd” is important to ensure high dissolution. Without wishing to be bound by theory, a compact liquid composition with high undiluted viscosity “Vu”, important to ensure drip-free and constant dosing, will generally dissolve poorly, unless it is so formulated as to have a lower viscosity on dilution, as in the present highly preferred embodiment of the invention.

In a preferred embodiment, the liquid contained in the container consists of a liquid detergent composition comprising a rheology modifier comprising, preferably consisting of, polyacrylate based polymers, preferably hydrophobically modified polyacrylate polymers; hydroxyl ethyl cellulose, preferably hydrophobically modified hydroxyl ethyl cellulose, xanthan gum, hydrogenated castor oil (HCO) and mixtures thereof.

Preferred rheology modifiers are polyacrylate based polymers, preferably hydrophobically modified polyacrylate polymers. Preferably a water soluble copolymer based on main monomers acrylic acid, acrylic acid esters, vinyl acetate, methacrylic acid, acrylonitrile and mixtures thereof, more preferably copolymer is based on methacrylic acid and acrylic acid esters having appearance

of milky, low viscous dispersion. Most preferred hydrologically modified polyacrylate polymer is Rheovis® AT 120, which is commercially available from BASF.

Other suitable rheology modifiers are hydroxethylcelluloses (HM-HEC) preferably
5 hydrophobically modified hydroxyethylcellulose.

Suitable hydroxethylcelluloses (HM-HEC) are commercially available from Aqualon/Hercules under the product name Polysurf 76® and W301 from 3V Sigma.

10 Xanthan gum is one suitable rheology modifier for liquids used herein. Xanthan gum is produced by fermentation of glucose or sucrose by *xanthomonas campestris* bacterium. Suitable Xanthan gum is commercially available under trade name Kelzan T® from CP Kelco.

Hydrogenated castor oil is one suitable rheology modifier used herein. Suitable hydrogenated castor oil is available under trade name TIXCIN R from Elementis.

15 The most preferred rheology modifier used herein is hydrologically modified polyacrylate polymer Rheovis® AT 120, which is commercially available from BASF.

Typically, the thickened liquid hard surface cleaning composition herein comprises from 0.1% to 10.0% by weight of the total composition of said thickener, preferably from 0.2% to 5.0%, more
20 preferably from 0.2% to 2.5% and most preferably from 0.2% to 2.0%.

Method of use

Fig. 14A to 14C illustrate an example of the operation of apparatus (1). Fig. 14A illustrates the resting position of apparatus (1), prior to use. The user disengages the top lid (17) or opens the
25 orifice (9) and inclines the apparatus (1) top down, in a substantially inverted position. The user then squeezes the container (2) preferably with one hand to begin the dosage. The liquid flow causes the valve (7) to close the discharge opening (13) and the liquid to flow through the timer apertures (16) causes the piston (5) to move towards the entry tube (10). Concurrently the liquid forced through the dosing chamber inlet openings (15) is discharged through the entry tube (10)
30 and out of the nozzle (8). Fig. 14B shows the apparatus (1) in its dosing arrangement with the piston (5) at its mid position. The user may squeeze said container for no more than 1.5 seconds, preferably no more than one second, to complete the dose. The volume of liquid dosed for each squeeze of the container (2) may be from 1ml to 80ml, preferably from 3ml to 40ml, more

preferably 10ml to 30ml, and even more preferably 10ml to 25ml. Fig. 14C illustrates the arrangement of apparatus (1) at the end of the dosage. Once the piston (5) reaches the entry tube (10) so as to close it, the dose is complete and the user may release the force from said container (2). The valve is then opened by the pressure differential generated as the resilient container (2) deforms back to its original shape, and the liquid is discharged into the container (2) through the discharge opening (13) allowing the piston (5) to return to its starting position. The user may now re-squeeze said container (2) to dispense a new dose, without the need of re-inverting the apparatus (1). This process may be repeated for all subsequent dosages as necessary. In order to change the dosage volume, the rotatable element (34) is rotated such that exposed cross-sectional area of the timer apertures (16) is altered.

Viscosity measurements – The viscosity of liquid compositions herein, including Vu and Vd, is measured using an AR 1000 from TA Instruments with a 2° 1' 5" cone angle spindle of 40mm diameter with truncation of 57 micrometer, shear rate factor of 28.6, and shear stress factor of 0.0597. The software used is the TA Instruments software, version 3.03 or higher. The following settings are used: a pre-shear with a shear rate of 10s⁻¹ for 10 seconds with 1 minute equilibration and a shear rate continuous ramp of from 0.1s⁻¹ till 1200s⁻¹, during 3 minutes with 32 points per decade. All measurements are carried out at room temperature at 20°C.

Dilution of compact liquid composition – The compact liquid composition is diluted with deionized water according to the following protocol. 100g of composition are weighed in a plastic beaker. The beaker is stirred with a mechanical stirrer rotating at low speed 200rpm to avoid entrapment of air into the product. While stirring, 50ml of deionized water are added to the composition. The composition is stirred for 4 minutes, until the composition is fully homogeneous. The composition is allowed to rest for 15 minutes before starting the viscosity measurement. The entire procedure is carried out at room temperature at 20°C.

Pressure measurements – A pressure sensor of the type MSR145 IP67 waterproof mini data logger from MSR Electronics GmbH (frequency of 1/10s, pressure range 0-2000mBar ±2.5mBar) is inserted into a container according to the present invention filled with a liquid according to the present invention. The cap and the remaining components of the apparatus according to the present invention are then fitted to close the container. Repeated doses of liquid are prepared by repeated squeezes of the apparatus in top down vertical orientation, typically 10 consecutive squeezes starting from a full container. The squeezing is carried out by a robot with a two point squeeze and

having a Festo sfc-dc-vc-3-e-h2-co control box and Festo hgple-25-40-2.8-dc-vcsc-g85 motor, that is set to compress the container at a speed “v” of 20mm/s and acceleration “a” of 100mm/s², and using the below protocol (typically the relative distance “xt” is 32mm for containers holding 400ml, 33mm for 520ml containers, 27.5mm for 600ml containers and 21mm for 946ml containers). Pressure readings are recorded by the sensor. Such measurements are repeated for apparatuses having a wide range of inlet and timer aperture ratios and for a range of viscosities.

Determining acceptable squeeze ergonomics – Acceptable squeeze ergonomics is determined via testing a number of apparatuses according to the present invention with an expert panel. Panelists are asked to rate a number of different apparatuses in terms of comfort and easiness of squeeze to generate a complete dose of liquid. Panelists are asked to squeeze apparatuses having different inlet and timer aperture ratios and different viscosity profiles. The results are recorded.

Flow rate measurements – A pressure sensor of the type MSR145 IP67 waterproof mini data logger from MSR Electronics GmbH (frequency of 1/10s, pressure range 0-2000mBar ± 2.5 mBar) is inserted into a container according to the present invention filled with a liquid according to the present invention. The cap and the remaining components of the apparatus according to the present invention are then fitted to close the container. Repeated doses of liquid are prepared by repeated squeezes of the apparatus in top down vertical orientation, typically 10 consecutive squeezes starting from a full container. The squeezing is carried out by a robot with a two point squeeze and having a Festo sfc-dc-vc-3-e-h2-co control box and Festo hgple-25-40-2.8-dc-vcsc-g85 motor, that is set to compress the container at a speed “v” of 20mm/s and acceleration “a” of 100mm/s² and using the below protocol (typically the relative distance “xt” is 32mm for containers holding 400ml, 33mm for 520ml containers, 27.5mm for 600ml containers and 21mm for 946ml containers). Pressure readings are recorded by the sensor. Such measurements are repeated for apparatuses having a wide range of inlet and timer aperture ratios and for a range of viscosities. The weight of each dose and the time to deliver the dose is recorded. The time is recorded with a high speed camera at 300 frames/second. The flow rate for each dose is calculated by dividing the mass of the dose delivered by the time taken to complete the dose.

Protocol for robot squeeze – The apparatus to be tested is mounted upright in the robot arm. The settings for speed and acceleration are adjusted to the above mentioned parameters. The apparatus is turned top down and then squeezed until the dose is complete. The apparatus is turned upright and then the squeeze is released. Pressure, mass and time parameters are recorded as explained

above. The process is repeated, typically 10 times for each condition and readings recorded each time.

5 The dimensions and values disclosed herein are not to be understood as being strictly limited to the exact numerical values recited. Instead, unless otherwise specified, each such dimension is intended to mean both the recited value and a functionally equivalent range surrounding that value. For example, a dimension disclosed as “40 mm” is intended to mean “about 40 mm.”

CLAIMS

What is claimed is:

1. A dosing apparatus (1) for dispensing a dose of liquid comprising:
 - (i) a resiliently squeezable container (2);
 - (ii) a cap (3) operably connected to said container (2);
 - (iii) a dosing chamber (4) operably connected to said cap (3), wherein said dosing chamber (4) comprises a dosing chamber base (12) having a discharge opening (13) therein, dosing chamber sidewalls (14) extending upwardly along the perimeter of said dosing chamber base (12) and at least one dosing chamber inlet opening (15) located proximal said dosing chamber sidewalls (14);
 - (iv) at least one timer aperture (16) located proximal to said discharge opening (13);
 - (v) a valve retaining means (6) located below said dosing chamber base (12);
 - (vi) a valve (7, 29, 33) provided in said valve retaining means (6) wherein said valve (7, 29, 33) is movable from an open position, allowing liquid flow through said discharge opening (13), and a closed position, where the valve blocks said discharge opening;
characterized in that the dosing chamber (4) comprises:
 - (vii) a rotatable element (34), wherein the rotatable element (34) comprises:
a rotatable element base (35), the rotatable element base (35) located proximal to the at least one timer aperture (16), the rotatable element base (35) comprising at least one flow restricting aperture (37) having an exposed cross-sectional area, such that the exposed cross-sectional area of the at least one timer aperture (16) is altered by rotating the rotatable element (34), in order to alter the dose, and
at least one rotatable element opening (38) located proximal to the at least one dosing chamber inlet opening (15);
 - (vii) a plunger, provided in said rotatable element (34) and moveable relative to said rotatable element (34) so as to advance upon squeezing of said container (2), up to a blocking position; and
the cap (3) or rotatable element (34) comprises a nozzle (8).
2. The dosing apparatus (1) according to claim 1, wherein the rotatable element base (35) comprises a plurality of different flow restricting apertures (37) such that a different flow

restricting aperture (37) is positioned over at least one timer aperture (16) by rotating the rotatable element (34).

3. The dosing apparatus (1) according to claim 2, wherein rotating the rotatable element (34) provides a minimum exposed cross-sectional area and a maximum exposed cross-sectional area for the flow restricting apertures (37), wherein the minimum cross-sectional open area is less than 90%, preferably less than 50%, more preferably less than 25% of the maximum cross-sectional open area.
4. The dosing apparatus (1) according to any of claims 2 to 3, wherein the ratio of the number of flow restricting apertures (37) to the number of timer apertures (16) is less than 4, preferably less than 3, more preferably 2, such that the dosing apparatus has less than 4, preferably less than 3, more preferably 2 dose settings.
5. The dosing apparatus (1) according to any preceding claims, wherein the flow restricting aperture (37) or timer aperture (16) is in the form of an elongated opening, wherein the elongated opening comprises a major axis having at one end, a first opening extremity (42), and having at the second end, a second opening extremity (43), and is positioned such that the exposed cross-sectional area of the at least one timer aperture (16) is varied by rotating the rotatable element (34).
6. The dosing apparatus (1) according to claim 5, wherein each elongated opening has a width which varies along the major axis of the elongated opening.
7. The dosing apparatus (1) according to claim 5 or 6, wherein the major axis of the elongated opening is radially offset, such that the radial distance of the center-line of the elongated opening increases from the first opening extremity to the second opening extremity.
8. The dosing apparatus (1) according to any preceding claims, wherein the rotatable element (34) can be rotated in an arc, wherein the arc has two arc extremities and the at least one flow restricting aperture (37) is arranged such that the largest dose setting is proximal to one extremity of the arc, and as the rotatable element (34) is rotated, the dose settings become smaller, preferably incrementally smaller.
9. The dosing apparatus (1) according to claim 10, wherein at at least one of the arc extremities, the at least one timer aperture (16) is not coincident with the at least one flow restricting aperture (37).

10. The dosing apparatus (1) according to any preceding claims, wherein the overlap of the at least one dosing chamber inlet opening (15) and the at least one rotatable element opening (38) provides an exposed cross-sectional area of the at least one dosing chamber inlet opening (15), such that an exposed cross-sectional area of the at least one dosing chamber inlet opening (15) is altered by rotating the rotatable element (34).
11. The dosing apparatus (1) according to claim 12, wherein when the at least one timer aperture (16) is fully closed, the dosing chamber opening (35) is not coincident with the at least one dosing chamber inlet opening (15).
12. The dosing apparatus (1) according to any preceding claims, wherein the volume dispensed from the smallest dose setting is from 5% to 90%, preferably from 10% to 50%, more preferably from 15% to 30% of the volume dispensed from the largest dose setting.
13. The dosing apparatus (1) according to claim 8, wherein the resiliently squeezable container (2) comprises a liquid, preferably a liquid having a viscosity of from 1 to 350mPa•s, preferably from 1 to 300mPa•s, more preferably from 1 to 250 mPa•s, even more preferably from 1 to 220 mPa•s, even more preferably 1 to 200mPa•s and most preferably from 1 to 150mPa•s, when measured at 1000s⁻¹ at 20°C.
14. The dosing apparatus (1) according to any preceding claim wherein said dose can be varied from 1ml to 80ml, preferably from 3ml to 40ml, more preferably 10ml to 30ml.
15. The dosing apparatus (1) according to any preceding claim wherein said container (2) comprises a front surface (27) and a back surface (28), and wherein the distance between said front to said back surfaces is between 30mm to 120mm.

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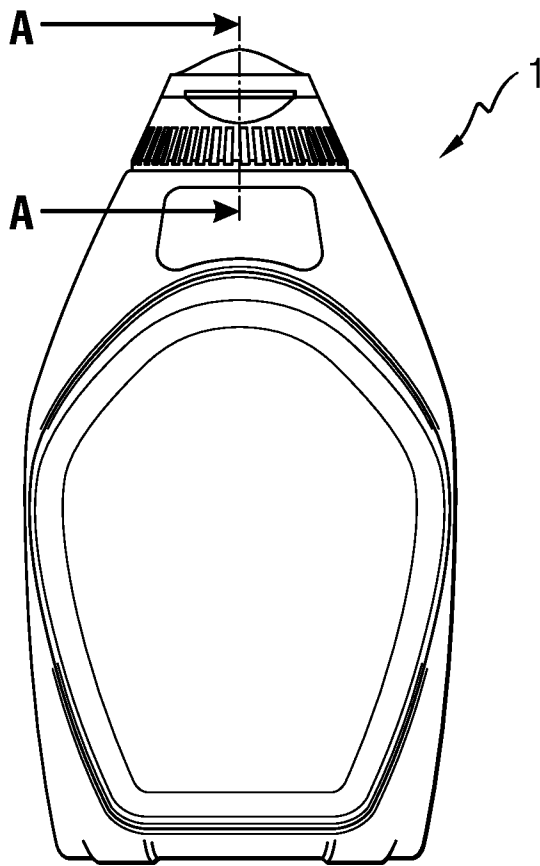


Fig. 1A

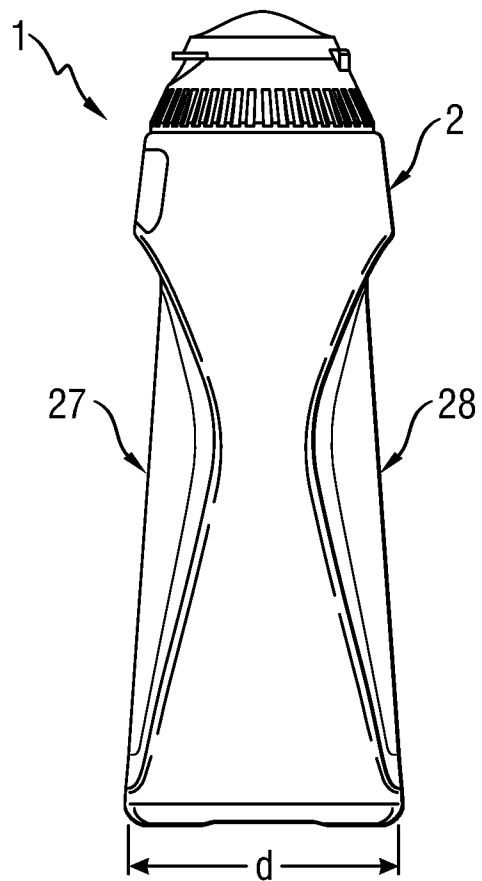


Fig. 1B

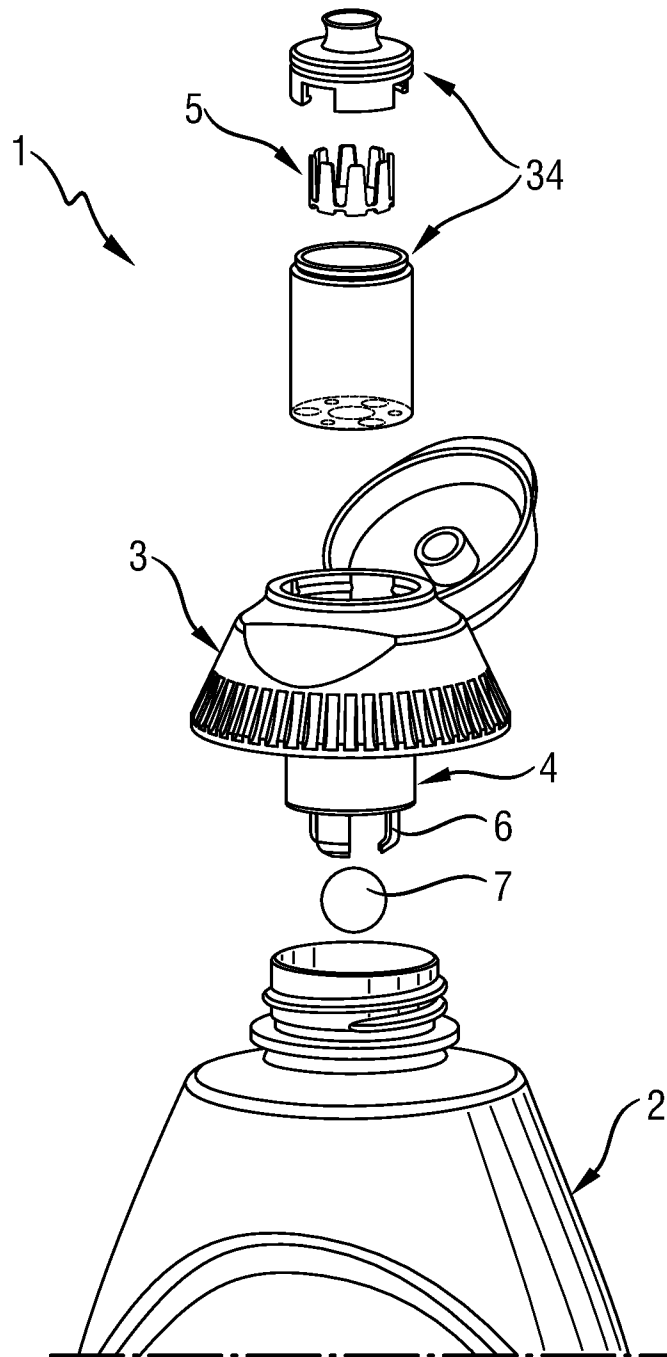


Fig. 2

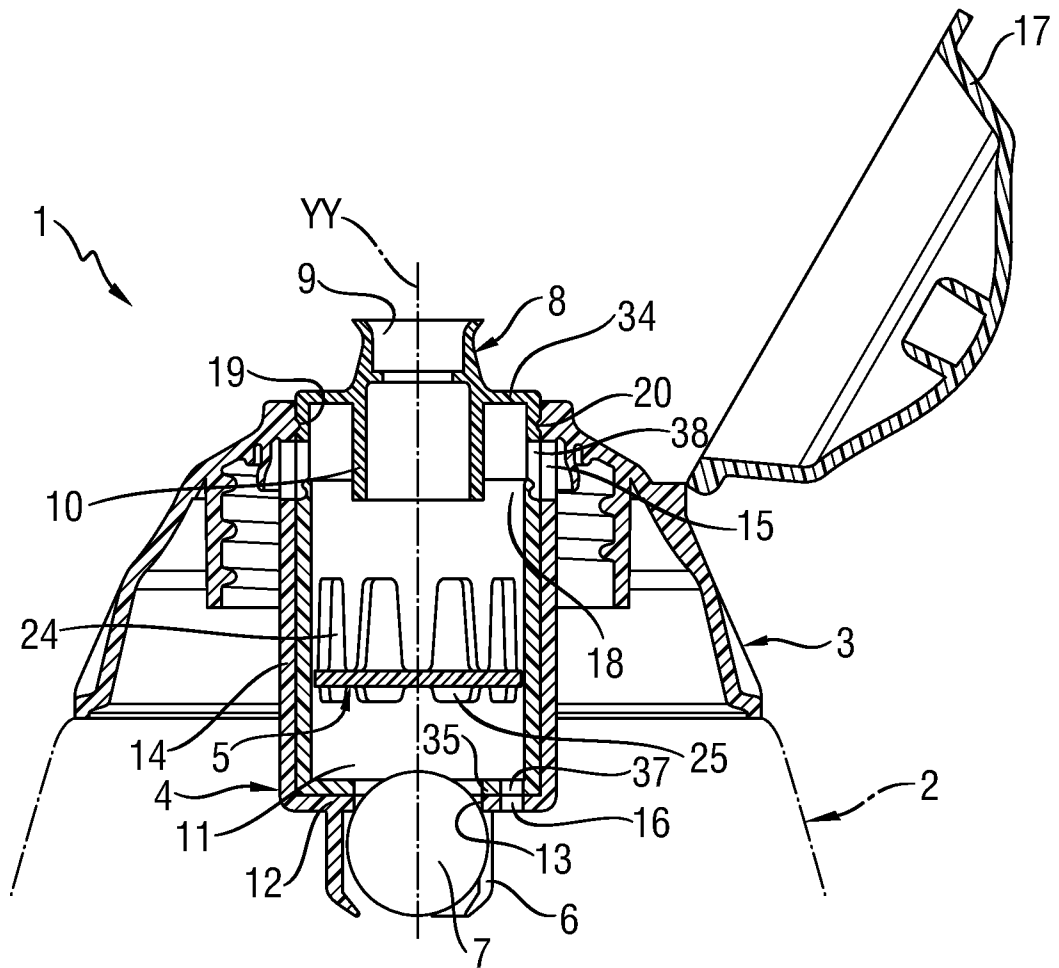


Fig. 3

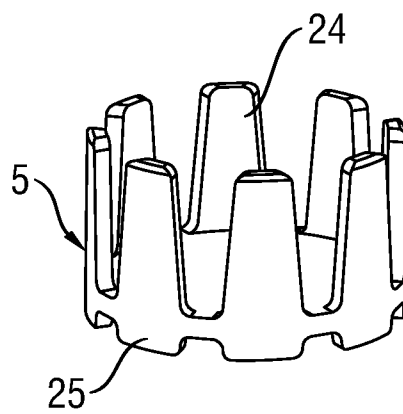
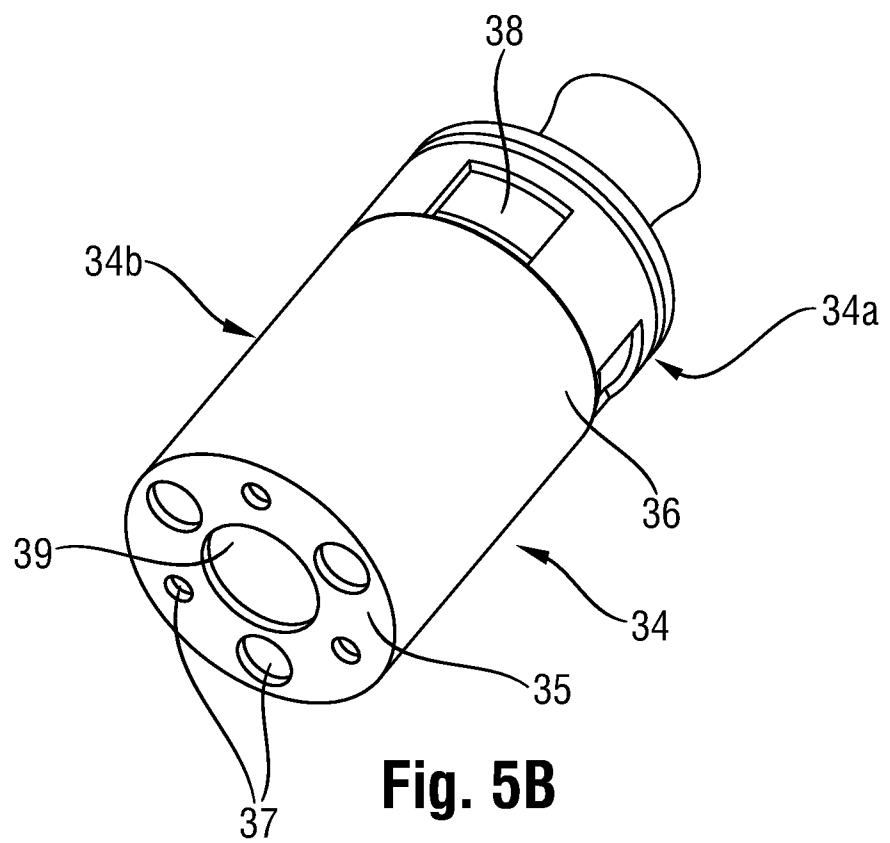
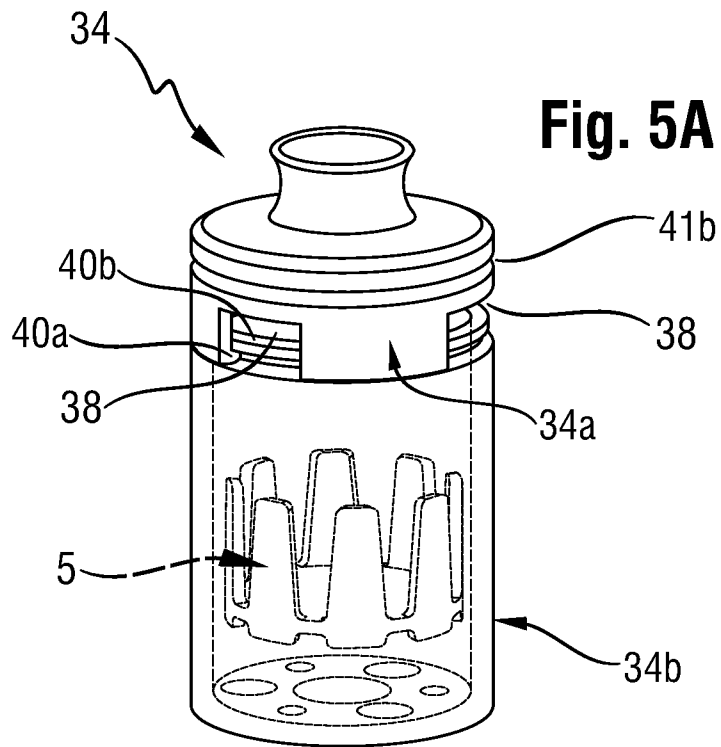


Fig. 4



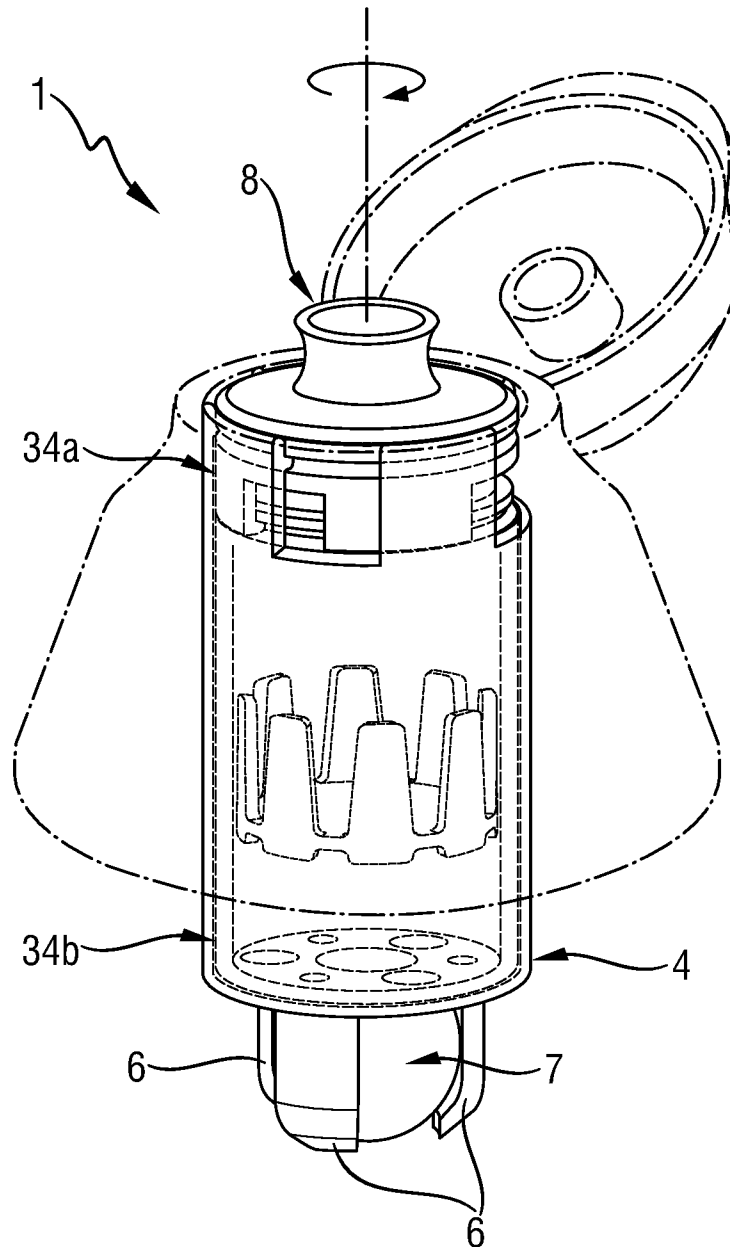


Fig. 5C

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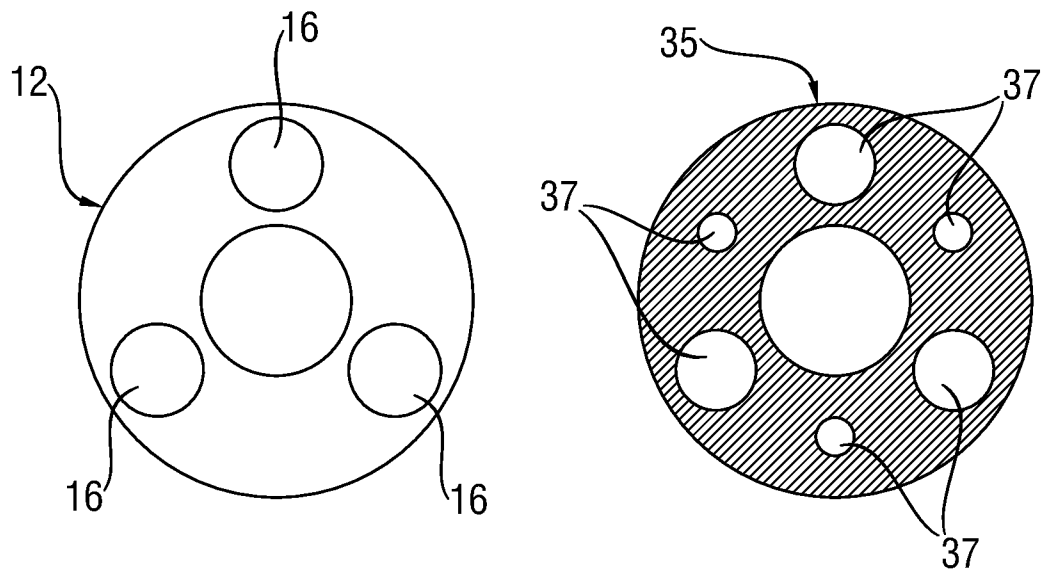


Fig. 6A

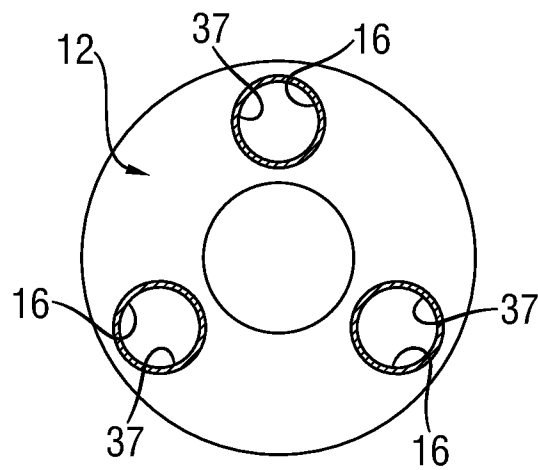


Fig. 6B

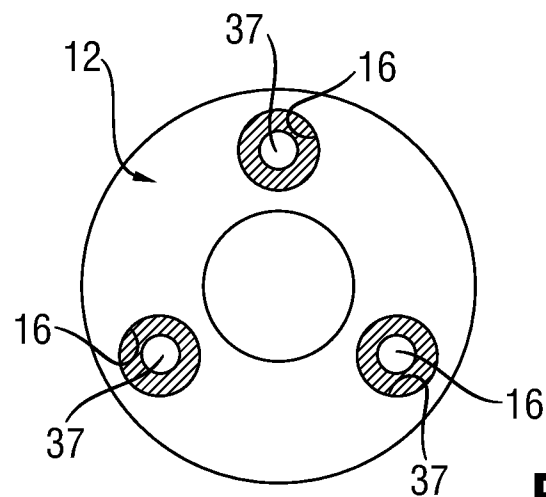


Fig. 6C

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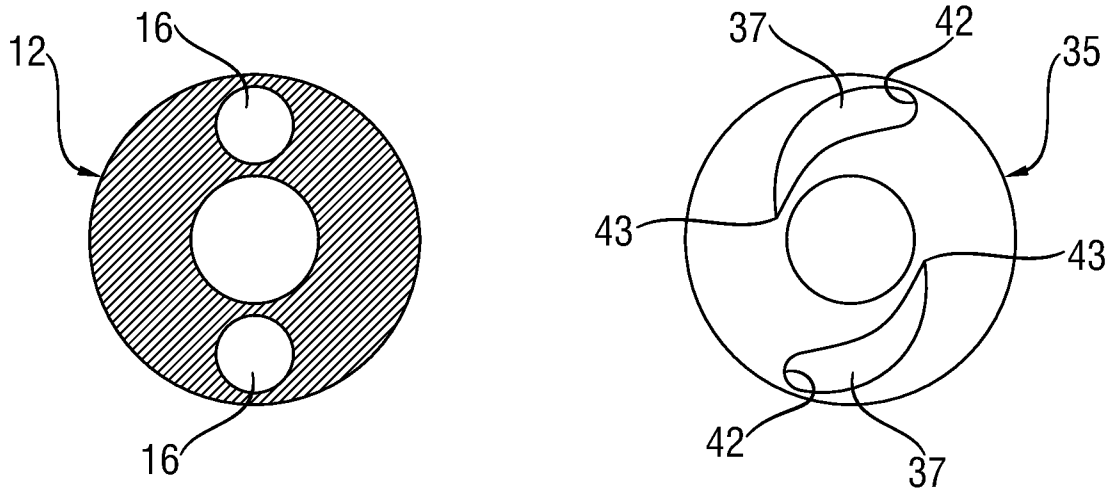


Fig. 7A

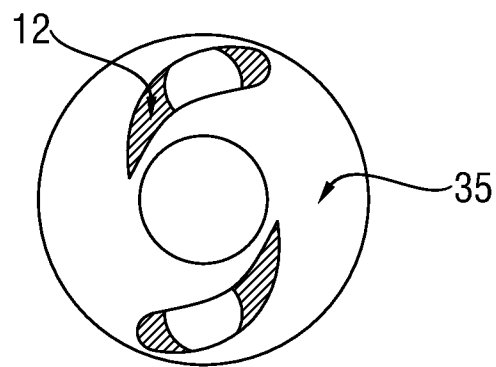


Fig. 7B

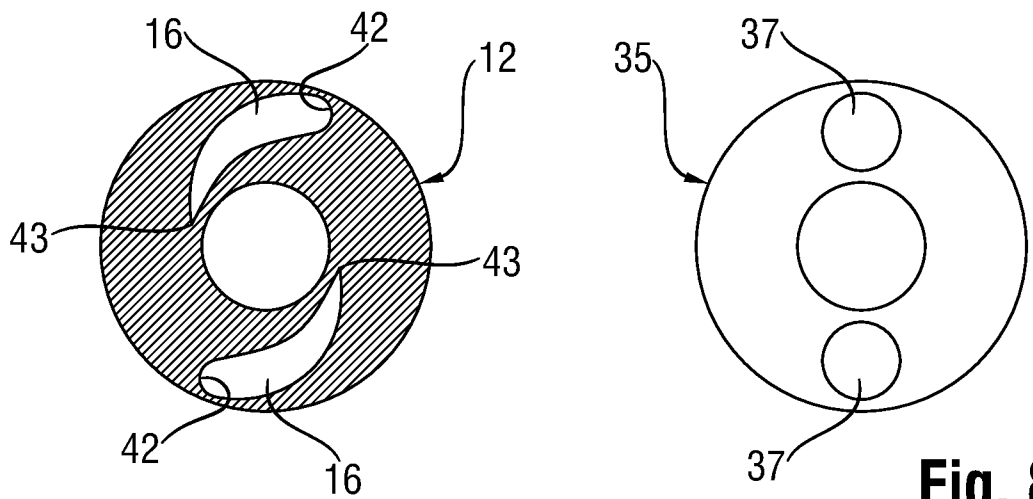


Fig. 8A

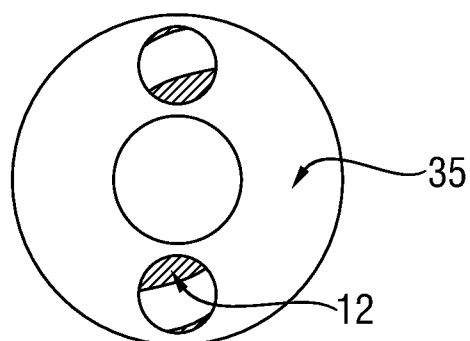


Fig. 8B

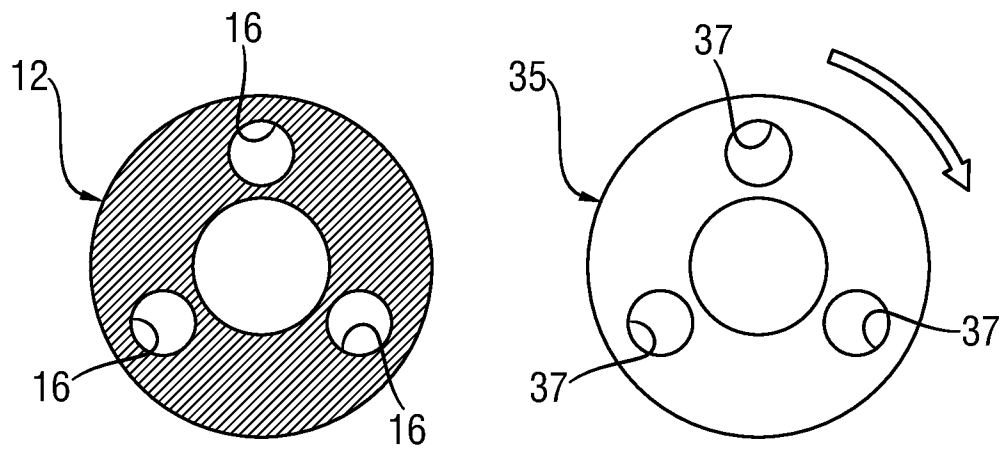


Fig. 9A

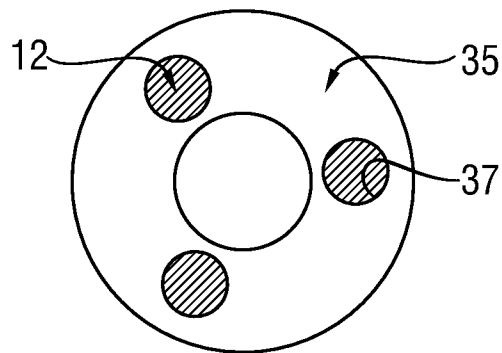


Fig. 9B

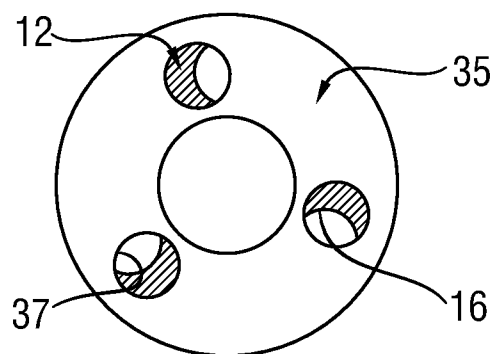


Fig. 9C

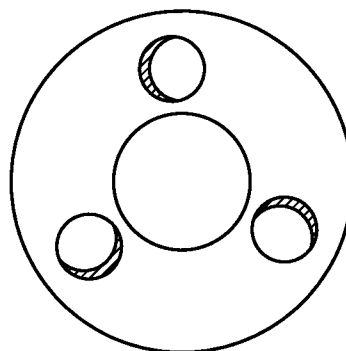


Fig. 9D

Fig. 10

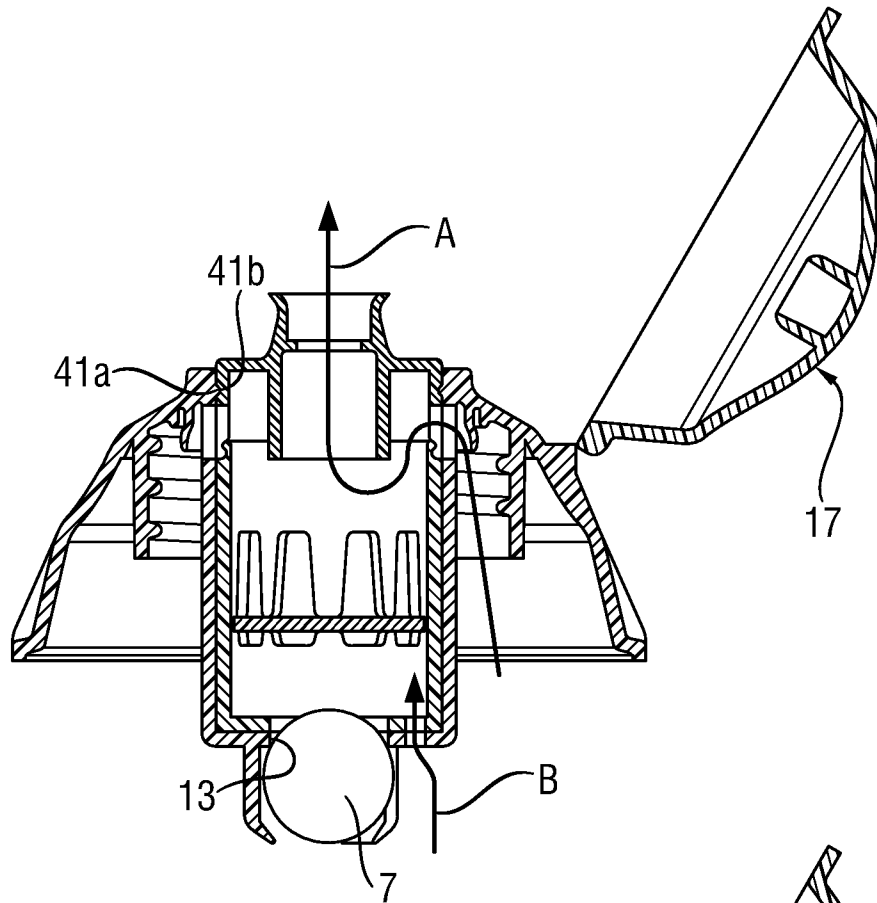
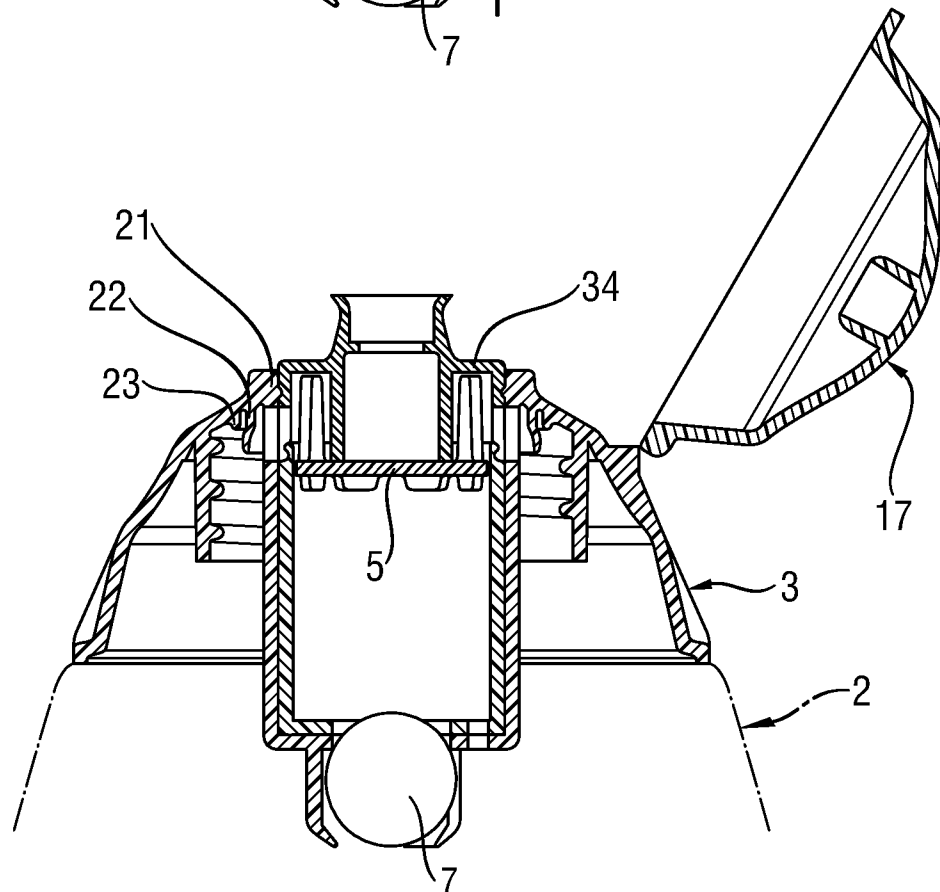


Fig. 11



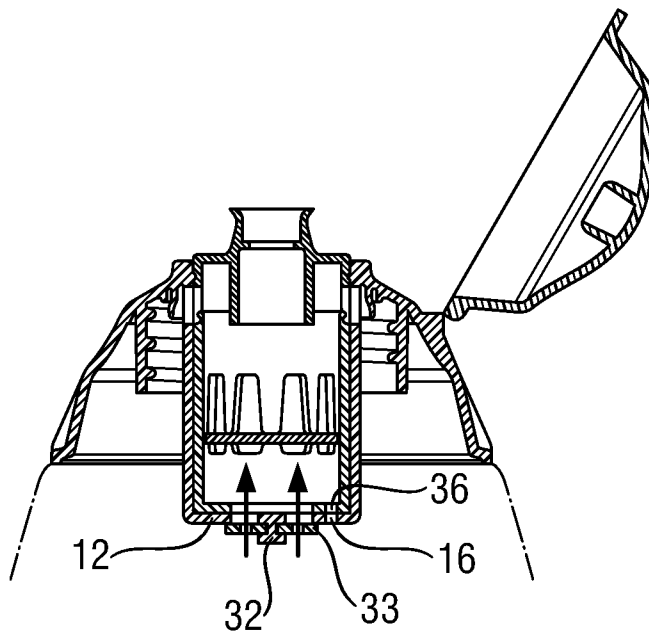


Fig. 12A

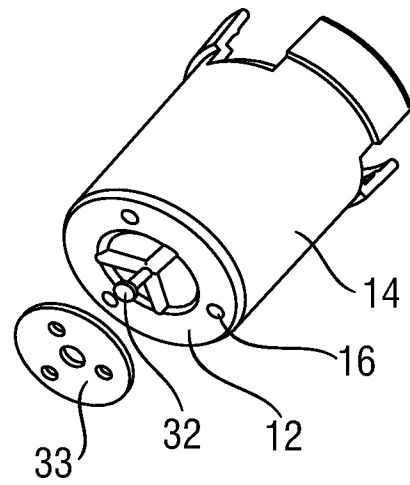


Fig. 12B

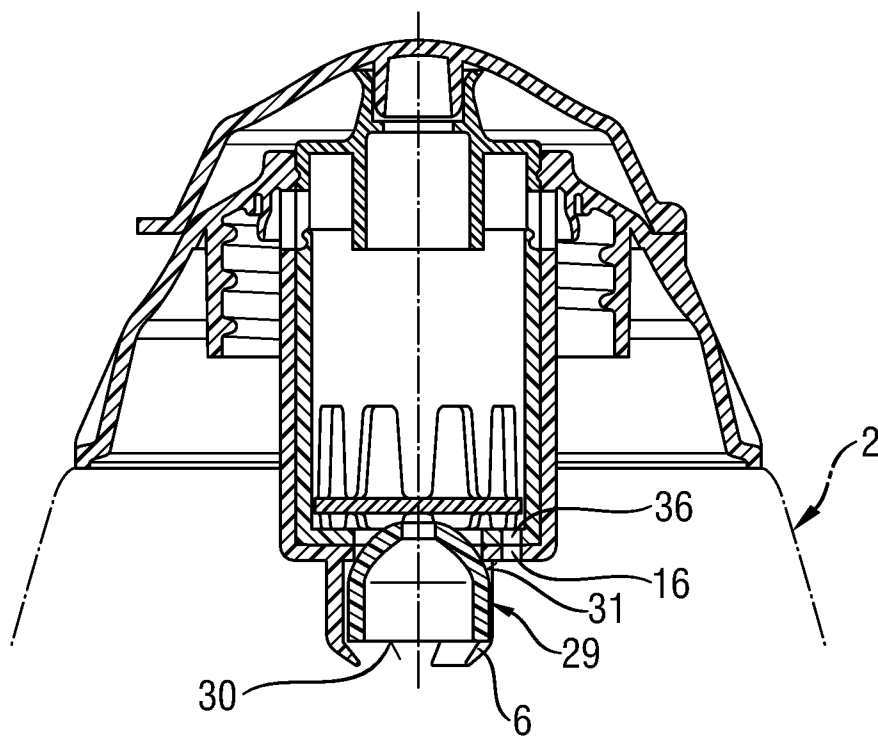


Fig. 13

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Fig. 14A

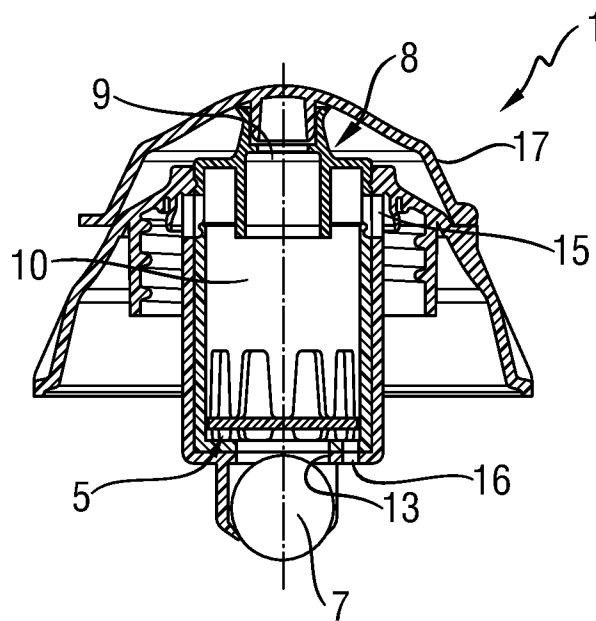


Fig. 14B

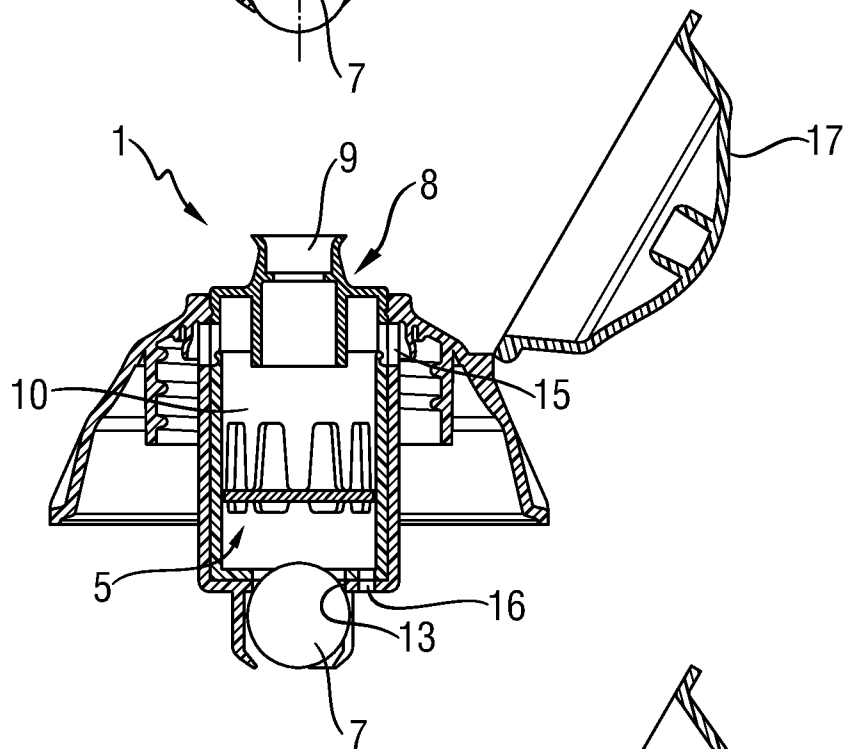
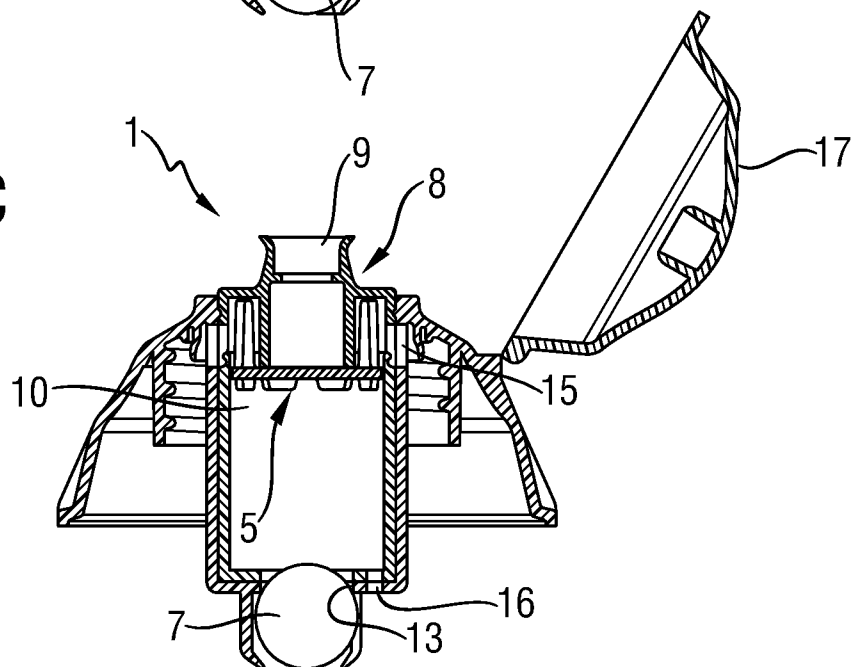


Fig. 14C



INTERNATIONAL SEARCH REPORT

International application No
PCT/US2017/057812

A. CLASSIFICATION OF SUBJECT MATTER

INV. G01F11/06 B65D47/30 G01F11/26 G01F11/28
ADD. G01F11/22

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G01F B65D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	EP 2 444 782 A1 (PROCTER & GAMBLE [US]) 25 April 2012 (2012-04-25) cited in the application figures 2, 3 paragraphs [0025], [0046] -----	1-15
Y	EP 0 446 805 A1 (CAPSULIT SRL [IT]) 18 September 1991 (1991-09-18) figures 1, 2 column 3, line 19 - column 4, line 12 -----	1-15
A	GB 1 224 927 A (BLUMEN MARJORIE ADELLE KIRKWOOD [US]) 10 March 1971 (1971-03-10) figure 1 ----- -/-	1-15



Further documents are listed in the continuation of Box C.



See patent family annex.

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"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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Date of the actual completion of the international search

18 January 2018

Date of mailing of the international search report

30/01/2018

Name and mailing address of the ISA/

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Authorized officer

Nierhaus, Thomas

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2017/057812

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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A	DE 195 00 830 C1 (HENKEL KGAA [DE]) 11 April 1996 (1996-04-11) figure 1 -----	1-15
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Information on patent family members

International application No

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