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(54) Title: APPARATUS AND METHOD FOR CHARACTERIZING STRESSES OF A FORMATION

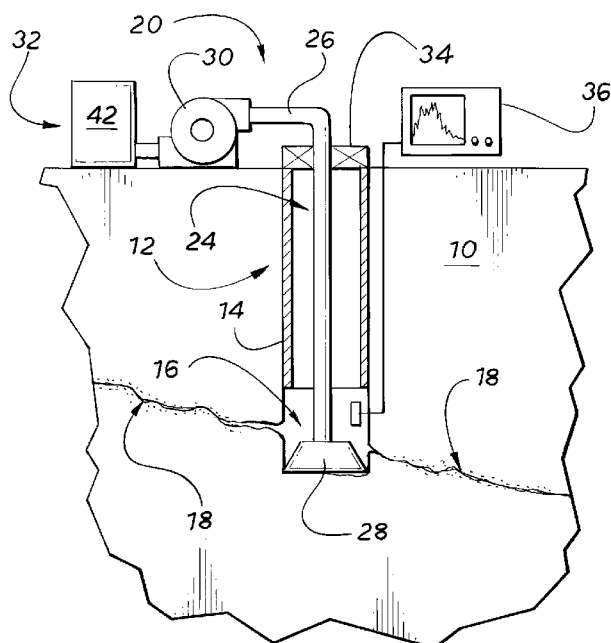


Fig. 1

(57) Abstract: An apparatus (20) and method for characterizing stresses in a formation (10) based on leakoff pressure measured in the formation (10). The method includes determining a line of shear failure (52) as a function of leakoff pressure (LOP) measured in the formation (10), determining a vertical stress (S_v), and determining each of a lower limit ($S_{h,limit}$) and an upper limit ($S_{H,limit}$) as a function of the vertical stress (S_v) and the leakoff pressure (LOP).



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APPARATUS AND METHOD FOR CHARACTERIZING STRESSES OF A FORMATION

TECHNICAL FIELD

[0001] This invention relates generally to apparatuses and methods for
5 characterizing stresses of a formation.

BACKGROUND

[0002] Stress information about a formation is collected and used to make decisions associated with exploring for hydrocarbons as well as developing and producing hydrocarbons that have been discovered. For example, stress information
10 about the formation is used in activities such as drilling margin estimation, evaluation of wellbore or borehole stability, column height estimation, determining drilling direction, determining lifespans of wells and completions, and waterflooding. If the formation is well understood, exploration, development, and production activities can be planned and executed in a cost effective and efficient manner.

[0003] The stress state and magnitudes of stresses of the formation are used in deciding how to approach exploration, development, and production activities. For example, the maximum stress magnitude is used to understand the acoustic properties of reservoirs and mudrock and to determine the porosity and volume of reservoirs. Understanding the acoustic properties of the reservoirs can facilitate
20 increasingly accurate interpretations of acoustic measurements that are used to explore the formation. If the exploration information is accurate, there is less risk in using the information to move forward with development and production activities.

[0004] In quantifying the stress state, typically, the overburden pressure is used to determine the magnitude of the vertical stress and a leakoff test is used to determine
25 the magnitude of the minimum stress. The leakoff test is analyzed to determine a leakoff pressure or other pressure that can be interpreted as the pressure when failure of the formation occurs during the leakoff test. The standard assumption is that the formation fails under a tensile mode of failure and the leakoff pressure represents either reopening of existing fractures or the initiation of a new tensile
30 fracture in non-permeable rock. Leakoff pressure is generally considered to be a reasonable estimate of the minimum principle stress of the formation.

[0005] However, in certain instances, the assumption that leakoff pressure represents the minimum principle stress of the formation has been found to be inconsistent with other evidence relating to the stress state. For example, in one instance, evidence has suggested that the stress state is a reverse-fault setting or area under compression. Here, for the leakoff pressure to be considered to be reflective of the minimum stress, leakoff pressure should be near overburden pressure. In contrast, well-understood and quality controlled leakoff pressure data was observed to be well below the overburden pressure. Accordingly, leakoff pressure does not always provide a reasonable estimate of minimum principle stress that is consistent with other evidence of the stress state and the standard assumption is not applicable in every case. What is needed is a new method of characterizing formation stresses.

SUMMARY

[0006] The various embodiments of the present disclosure overcome the shortcomings of the prior art by providing an apparatus and method for characterizing stresses in a formation where the formation is under shear failure conditions. The method is applicable where a leakoff test has induced shear failure and can be used to determine stress magnitudes as a function of leakoff pressure.

[0007] According to an exemplary embodiment, a formation under shear failure conditions includes a fracture system or weak zone that intersects an openhole or uncased portion of a borehole where a leakoff test is performed. According to an exemplary method of conducting a leakoff test, the borehole is shut in and drilling fluid is pumped into the borehole to gradually increase the pressure that the formation experiences. As the pressure of the drilling fluid in the borehole is increased, the drilling fluid penetrates the fracture system, moves through permeable paths, and interacts with the stress field of the formation. As pore pressure increases in the fracture system, the formation is induced to fail along the fracture in a shear mode. The shear failure creates mixed mode fractures, opening up the nearby rock. As the rock opens up, drilling fluid moves into the openings in the rock and the pressure of the drilling fluid in the borehole decreases. The leakoff pressure can be identified as

the pressure where the leakoff test pressure data substantially deviates from a gradual increase to reflect the pressure at which the formation fails.

[0008] Shear failure can be illustrated with the Mohr-Coulomb failure criterion envelope. A line of shear failure that defines the failure envelope can generally be determined with values for cohesion and a coefficient of friction. For example, values for these parameters can be determined through independent observation. Where shear failure is induced by the leakoff test, a new line of shear failure is established that is a function of the leakoff pressure. For example, the new line of shear failure can be established so as to be parallel to the initial line of shear failure and displaced from the initial line of shear failure by a function of the leakoff pressure.

[0009] A solution space that includes the possible stress states that are consistent with shear failure induced by a leakoff test can be determined. Each individual solution in the solution space consists of three mutually orthogonal stresses. According to an exemplary embodiment, the orthogonal stresses are a vertical stress, a minimum horizontal stress, and a maximum horizontal stress. The solution space itself is bound by a lower limit, which is the smallest that minimum horizontal stress can be for any possible solution, and an upper limit, which is the largest that maximum horizontal stress can be for any solution in the solution space. The limits are not the minimum and maximum horizontal stresses for one solution, but the limits for any solution in the solution space. The lower and upper limits for the horizontal stresses in the solution space are a function of the vertical stress and the line of shear failure that is a function of leakoff pressure. The vertical stress itself is a function of the overburden and is most often determined from density log data.

[0010] The lower limit and upper limit can be determined from two Mohr's circles where each Mohr's circle has the vertical stress as a principal stress and each Mohr's circle is in tangential contact with the leakoff pressure line of shear failure. The lower limit will be determined as the lower principle stress on the Mohr's circle that has the vertical stress as the maximum principle stress. The upper limit will be determined as the higher principle stress on the Mohr's circle that has the vertical stress as the minimum principle stress. Each limiting Mohr's circle is a function of overburden

pressure and parameters of the line of shear failure such as cohesion and coefficient of friction.

[0011] The solution space can be broken down into three cases: a normal-fault case, a reverse-fault case, and a strike-slip fault case.

5 **[0012]** The set of stress-state solutions that represents a normal-fault setting and is consistent with shear failure includes the vertical stress and the lower limit as the principal stresses with the largest differential in magnitude. The intermediate stress, maximum horizontal stress, can vary between these two values. Here the minimum stress and intermediate stress are horizontal.

10 **[0013]** The set of stress-state solutions that represents a reverse-fault setting and is consistent with shear failure includes the vertical stress and the upper limit as the principal stresses with the largest differential in magnitude. The intermediate stress, minimum horizontal stress, can vary between these two values. Here, the maximum stress and intermediate stress are horizontal.

15 **[0014]** The set of stress-state solutions that represents a strike-slip fault setting and is consistent with shear failure includes the minimum horizontal stress and the maximum horizontal stress as the principal stresses with the largest differential in magnitude. The minimum horizontal stress value may not exceed lower limit and the maximum horizontal stress value may not exceed the upper limit. The minimum
20 horizontal stress and the maximum horizontal stress values are determined as pairs from a series of Mohr's circles that are in tangential contact with the line of shear failure that is a function of leakoff pressure. The intermediate stress in this case is vertical stress. Here the maximum stress and minimum stress are horizontal.

[0015] The foregoing has broadly outlined some of the aspects and features of the
25 present invention, which should be construed to be merely illustrative of various potential applications of the invention. Other beneficial results can be obtained by applying the disclosed information in a different manner or by combining various aspects of the disclosed embodiments. Accordingly, other aspects and a more comprehensive understanding of the invention may be obtained by referring to the
30 detailed description of the exemplary embodiments taken in conjunction with the

accompanying drawings, in addition to the scope of the invention defined by the claims.

BRIEF DESCRIPTION OF THE DRAWINGS

- 5 **[0016]** **FIG. 1** is a partial view a formation and an apparatus for conducting a leakoff test in an openhole portion of a borehole in the formation, according to an exemplary embodiment of the disclosure.
- [0017]** **FIGs. 2 and 3** are partial views of the formation of **FIG. 1**, illustrating leakoff test induced shear failure of the formation.
- 10 **[0018]** **FIG. 4** is a graphical illustration of leakoff test data.
- [0019]** **FIG. 5** is a graphical illustration of Mohr-Coulomb shear failure criteria that represents leakoff test induced shear failure of the formation.
- [0020]** **FIG. 6** is a graphical illustration corresponding to **FIG. 5** of a geometrical relationship between potential horizontal principle stresses.
- 15 **[0021]** **FIG. 7** is a graphical illustration of a stress polygon that represents the potential horizontal principle stresses of the formation.

DETAILED DESCRIPTION

- [0022]** As required, detailed embodiments are disclosed herein. It must be
20 understood that the disclosed embodiments are merely exemplary and other embodiments may be embodied in various and alternative forms, and combinations thereof, without departing from the scope of the teachings of the disclosure. As used herein, the word "exemplary" is used expansively to refer to embodiments that serve as illustrations, specimens, models, or patterns. The figures are not necessarily to
25 scale and some features may be exaggerated or minimized to show details of particular components. In other instances, well-known components, systems, materials, or methods have not been described in detail in order to avoid obscuring the disclosure. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a basis for the claims and as a

representative basis for teaching one skilled in the art.

Formation and Apparatus

[0023] Referring to **FIG. 1**, an exemplary formation **10** is illustrated. A borehole **12** is drilled in formation **10** and a casing string **14** is cemented along a portion of
5 borehole **12**. As used herein, the term “formation” generally refers to the rock around the borehole or otherwise to a body of rock. An openhole **16** or uncased portion of borehole **12** is intersected by a permeable fracture system **18** or weak zone in formation **10**.

[0024] As used herein, the term “in situ” refers to the original location or position,
10 such as a formation that has not been disturbed by faults or landslides.

[0025] An exemplary apparatus **20** for drilling borehole **12** and for collecting leakoff test data **22** (**FIG. 4**) includes a drillstring **24**, a drillpipe **26**, a drill bit **28**, a drilling fluid pump **30**, a drilling fluid reservoir **32**, a borehole seal **34**, and a data acquisition unit **36**. During the drilling operations, apparatus **20** is used to shut in
15 borehole **12** and gradually increase the pressure that formation **10** at the bottom of borehole **12** experiences. At a certain pressure, fluids will enter formation **10**, i.e., fluids will leakoff. The results of the procedure dictate the maximum pressure that may be applied to that portion of borehole **12** during drilling operations. This procedure is accomplished by pumping drilling fluid **42** into the borehole **12**. Drilling
20 fluid **42**, also known as drilling mud, refers to any number of liquid fluids and mixtures of fluids and solids used in operations to drill boreholes into the earth.

Shear Failure Conditions

[0026] Formation **10** is under shear failure conditions along the permeable fracture system **18** such that, as a leakoff test is conducted, formation **10** fails in a shear
25 failure mode. Different stress states can lead to shear failure so long as the differential between principle stresses is sufficiently high. A stress state can be represented by three principle stresses that are orthogonal to one another. In the exemplary embodiment, the three principle stresses include a minimum horizontal stress **S_h**, a maximum horizontal stress **S_H**, and a vertical stress **S_v**. For purposes of
30 teaching, the minimum horizontal stress **S_h** is smaller than the maximum horizontal stress **S_H**.

[0027] For purposes of illustration, the illustrated formation is considered to be in compression with horizontal stresses S_h , S_H being greater than the vertical principle stress S_v .

[0028] Overburden pressure can be used to determine a value of the vertical principle stress S_v . Overburden pressure, also known as lithostatic pressure or geostatic pressure, is the pressure or stress imposed on a layer of soil or rock by the weight of the overlying material. A value for overburden pressure at a depth can be determined as a function of the density of the overlying rock.

Leakoff Test (LOT) and Shear Failure

[0029] Before borehole **12** is drilled to a next casing depth, a leakoff test is performed at openhole **16** to determine the maximum pressure or mudweight that can be applied when drilling to the next casing depth without failing at the current casing shoe (not shown). Casing shoe is the bottom of casing string **14** including the cement around it. It serves to isolate formation **10** from drilling fluids **42** in the casing string **14** and in openhole **16** of borehole **12**.

[0030] An exemplary method of performing a leakoff test is now described. Referring to **FIG. 1**, borehole **12** is closed with seal **34** and drilling fluid **42** is pumped into openhole **16** of borehole **12** through drill pipe **26**. Referring to **FIGs. 1** and **4**, the fluid pressure in borehole **12** gradually increases until formation **10** fails at openhole **16**. In general, formation **10** can fail in a shear mode or in a tensile mode. To illustrating a new interpretation of stress state where shear failure conditions are assumed or known (in contrast to assuming tensile failure conditions), a shear failure mode of formation **10** is described in further detail.

[0031] Referring to **FIGs. 2-4**, as the pressure of drilling fluid **42** in openhole **16** is increased, drilling fluid **42** penetrates and interacts with fracture system **18**. The pressure of drilling fluid **42** in fracture system **18** works against cohesion C_0 and friction μ in fracture system **18** until formation **10** is induced to fail in a shear mode. The failure of formation **10** creates volumes **44** into which drilling fluid **42** can move from openhole **16**. Volumes **44** can be new fractures, pores that are opened, or opening of fractures with increased displacement between the walls of fracture system **18** due to asperities along the walls of fracture system **18**. As drilling fluid **42**

moves from openhole **16** into volumes **44**, the pressure of drilling fluid **42** in borehole **12** drops.

[0032] The leakoff test measures the pressure in borehole **12** with respect to the volume of drilling fluid **42** that is pumped into borehole **12** or with respect to time.

- 5 Factors that contribute to variations in leakoff data results include different pump rates, the use of hesitation testing, and the type of drilling fluid.

Leakoff Pressure (LOP)

- [0033]** Failure of the formation can be observed in the leakoff test data **22**. For example, referring to **FIG. 4**, the leakoff test data **22** include a data point **46**, reflective
10 of a value of leakoff pressure **LOP**, where the leakoff test data **22** begins to deviate from a linear increase in pressure. Generally, the linear increase in pressure is due to pumping drilling fluid **42** into borehole **12** as the volume of borehole **12** and fracture system **18** is substantially fixed. The pressure in borehole **12** gradually builds until formation **10** fails and the volume of borehole **12** and fracture system **18** is essentially
15 increased as volumes **44** open up. By identifying leakoff pressure **LOP** where the deviation occurs, leakoff pressure **LOP** reflects the pressure at failure. It should be noted that leakoff pressure can be alternatively identified and other parameters that reflect the failure of the formation can be substituted for leakoff pressure.

- [0034]** The leakoff test data **22** can be used to determine the maximum pressure
20 limit for drilling an additional casing length, to determine casing placement for the borehole being drilled, to determine stress information in formation **10** for borehole stability analyses in future boreholes, for development issues, and for exploration of issues such as trap integrity and column height predictions in other prospects.

Method of Using Leakoff Pressure to Characterize Stress of Formation

- 25 **[0035]** Referring to **FIG. 5**, Mohr-Coulomb failure criterion can be used to quantify the magnitude of stresses of formation **10** based on leakoff pressure **LOP**. In situ or far field stresses are considered to control shear failure along fracture system **18**. Further, the pressure of drilling fluid **42** in fracture system **18** is considered to be substantially the same as the pressure of drilling fluid **42** in borehole **12**.

[0036] The Mohr-Coulomb criterion is illustrated on a graph where normal stresses are plotted along the x-axis and shear stresses are plotted along the y-axis. A notional line of shear failure **50** that defines a failure envelope is plotted on the graph. Line of shear failure **50** can be determined by selecting values for cohesion **C₀** and angle of friction **μ** and is given by $\tau_f = \mu \cdot \sigma_f + C_0$ where **τ_f** is shear stress at failure and **σ_f** is tensile stress at failure. However, notional line of shear failure **50** does not take leakoff pressure **LOP** into account.

[0037] Since the leakoff test induces shear failure, a leakoff pressure line of shear failure **52** that takes leakoff pressure **LOP** into account is established and represents that shear failure is a function of leakoff pressure **LOP**. Leakoff pressure line of shear failure **52** is parallel to notional line of shear failure **50** and is displaced from notional line of shear failure **50** along the x-axis by the magnitude of leakoff pressure **LOP**. Leakoff pressure line of shear failure **52** is given by $\tau_f = \mu \cdot (\sigma_f - LOP) + C_0$.

[0038] Leakoff pressure line of shear failure **52** can be considered to represent the failure envelope where in situ stresses on formation **10** cause shear failure on the fracture or permeable system **18** during the leakoff test. Given the vertical stress **S_v** according to the overburden pressure and the leakoff pressure line of shear failure **52**, Mohr's circles **54**, **56** can be constructed to determine a lower limit **S_{h,limit}** and an upper limit **S_{H,limit}** that are consistent with shear failure on the permeable fracture system **18**.

[0039] Vertical stress **S_v** is determined at a depth where the leakoff test is performed and plotted as a point on the x-axis. Mohr's circles **54**, **56** are constructed such that each one has vertical stress **S_v** as a principle stress and each is in tangential contact with leakoff pressure line of shear failure **52**.

[0040] The two Mohr's circles **54**, **56** represent solutions in the normal-fault and reverse-fault stress states respectively. The other principle stress determined by Mohr's circle **54** is the lower limit **S_{h,limit}**, which is the smallest that the minimum horizontal stress **S_h** can be for any possible solution in the solution space. The lower limit **S_{h,limit}** corresponds to the normal-fault stress state solutions. The other principle stress determined by Mohr's circle **56** is the upper limit **S_{H,limit}**, which is the largest that the maximum horizontal stress **S_H** can be for any possible solution in the solution

space. The upper limit $\mathbf{S}_{H,limit}$ corresponds to the reverse-stress state solutions. Any number of Mohr's circles, such as Mohr's circle **58**, can be drawn in tangential contact with the leakoff pressure line of shear failure **52** where the principle stresses are between the lower limit $\mathbf{S}_{h,limit}$ and the upper limit $\mathbf{S}_{H,limit}$ in magnitude. Such

5 Mohr's circles correspond to strike-slip stress state solutions where vertical stress $\mathbf{S}_v$ is the intermediate stress.

[0041] Lower limit $\mathbf{S}_{h,limit}$ and upper limit $\mathbf{S}_{H,limit}$ can be determined as a function of vertical stress $\mathbf{S}_v$, leakoff pressure $\mathbf{LOP}$, cohesion $\mathbf{C}_0$, and coefficient of friction μ . Exemplary equations for determining lower limit $\mathbf{S}_{h,limit}$ and upper limit $\mathbf{S}_{H,limit}$ are now

10 described. Referring to **FIGs. 5** and **6**, since the leakoff pressure line of shear failure **52** is tangent to each of Mohr's circles **54**, **56**, a radial line $\mathbf{R}_1$, $\mathbf{R}_2$ extends from the center point $\mathbf{S}_1$, $\mathbf{S}_2$ of each of Mohr's circles **54**, **56** to perpendicularly intersect the leakoff pressure line of shear failure **52**. Similarly, a radial line $\mathbf{R}_v$ extends from the point of vertical stress $\mathbf{S}_v$ to perpendicularly intersect leakoff pressure line of shear

15 failure **52**. The radial lines $\mathbf{R}_1$, $\mathbf{R}_2$, $\mathbf{R}_v$ are parallel to one another and the lengths of the radial lines $\mathbf{R}_1$, $\mathbf{R}_2$, $\mathbf{R}_v$ are geometrically related to one another. The geometrical relationships can be given as

$$\frac{R_1}{S_1 - (LOP - C_0/\mu)} = \frac{R_v}{S_v - (LOP - C_0/\mu)} = \frac{R_2}{S_2 - (LOP - C_0/\mu)}.$$

The radii $\mathbf{R}_1$, $\mathbf{R}_2$ relate the center points $\mathbf{S}_1$, $\mathbf{S}_2$ to the vertical stress $\mathbf{S}_v$ according to $S_1 = S_v - R_1$ and $S_2 = S_v + R_2$

20 and relate the lower and upper limits $\mathbf{S}_{h,limit}$, $\mathbf{S}_{H,limit}$ to the vertical stress $\mathbf{S}_v$ according to $S_{h,limit} = S_v - 2R_1$ and $S_{H,limit} = S_v + 2R_2$. Also, an angle Φ is given as $\phi = \tan^{-1}(\mu)$ and the radial line $\mathbf{R}_v$ is given by $R_v = (S_v - (LOP - C_0/\mu))\sin \phi$.

[0042] These relationships can be used to determine the lower and upper limits $\mathbf{S}_{h,limit}$, $\mathbf{S}_{H,limit}$. For example, the lower and upper limits $\mathbf{S}_{h,limit}$, $\mathbf{S}_{H,limit}$ can be given as

25 $S_{h,limit} = S_v - \frac{2(S_v - (LOP - C_0/\mu))\sin \phi}{(1 + \sin \phi)}$ and $S_{H,limit} = S_v + \frac{2(S_v - (LOP - C_0/\mu))\sin \phi}{(1 - \sin \phi)}$. The magnitudes of the lower and upper limits $\mathbf{S}_{h,limit}$, $\mathbf{S}_{H,limit}$ can then be determined.

[0043] A stress state solution space that includes stress states that are consistent with shear failure induced by a leakoff test can be determined. Each stress state solution of the exemplary stress state solution space includes three mutually

orthogonal stresses: the vertical stress S_v , the minimum horizontal stress S_h , and the maximum horizontal stress S_H . The solution space itself is bound by the lower limit $S_{h,limit}$, which is the smallest the minimum horizontal stress S_h can be, and the upper limit $S_{H,limit}$, which is the largest the maximum horizontal stress S_H can be for any solution in the solution space. As described above, the limits $S_{h,limit}$, $S_{H,limit}$ are a function of the vertical stress S_v and the leakoff pressure LOP .

[0044] The solution space can be broken down into three cases: a normal-fault case where $S_v \geq S_H \geq S_h$, a reverse-fault case where $S_H \geq S_h \geq S_v$, and a strike-slip fault case where $S_H \geq S_v \geq S_h$.

[0045] The set of stress state solutions that represents a normal-fault setting and is consistent with shear failure includes vertical stress S_v and lower limit $S_{h,limit}$ as the principal stresses with the largest differential in magnitude. The intermediate stress, maximum horizontal stress S_H , can vary between these two values. Here the minimum stress and intermediate stress are horizontal.

[0046] The set of stress state solutions that represents a reverse-fault setting and is consistent with shear failure includes vertical stress S_v and upper limit $S_{H,limit}$ as the principal stresses with the largest differential in magnitude. The intermediate stress, minimum horizontal stress S_h , can vary between these two values. Here the maximum stress and intermediate stress are horizontal.

[0047] The set of stress state solutions that represents a strike-slip fault setting and is consistent with shear failure includes minimum horizontal stress S_h and maximum horizontal stress S_H as the principal stresses with the largest differential in magnitude where $S_h < S_v$ and $S_H > S_v$. These values may not exceed or fall outside of lower limit $S_{h,limit}$ or upper limit $S_{H,limit}$ and they are determined as pairs from a series of Mohr's circles that are in tangential contact with the leakoff pressure line of shear failure 52. The intermediate stress in this case is vertical stress S_v . Here the maximum stress and minimum stress are horizontal.

Stress Polygon

[0048] Referring to **FIG. 7**, once values of lower and upper limits $S_{h,limit}$, $S_{H,limit}$ have been determined, a stress polygon can be used to illustrate the potential range of the horizontal stresses S_h , S_H and the possible stress regimes. Minimum

horizontal stress S_h is plotted along the x-axis and maximum horizontal stress S_H is plotted along the y-axis.

[0049] The stress polygon line produced by the method described herein allows stress magnitude estimation for all three stress regimes. For purposes of illustration, a stress polygon line **60** is plotted. Stress polygon line **60** includes a vertical segment that represents the set of stress states solutions corresponding to a normal-fault setting **70**, a horizontal segment that represents the set of stress state solutions corresponding to a reverse-fault setting **72**, and a diagonal segment that represents the set of stress state solutions corresponding to a strike-slip fault setting **74**. The diagonal segment connects the vertical segment and the horizontal segment.

[0050] Where cohesion C_0 and/or coefficient of friction μ include a range of possible values, stress polygon lines can define an area of the stress polygon where possible stress magnitudes are located. For example, a stress polygon line corresponding to a first coefficient of friction and a stress polygon line corresponding to a second coefficient of friction can define a stress polygon area there between.

[0051] It should be noted that the shear failure method of determining stress is not necessarily intended to replace the prior assumption of tensile failure during a leakoff test. Rather, it can be regarded as an alternative interpretation. Determining when to use the shear failure assumption is dependent on the interpreter's understanding of the subsurface geology. It is appropriate to consider using the shear failure method of determining stress when leakoff tests are lower than expected as well as other explanations for a lower than expected leakoff which include but are not limited to stopping the test before failure, poor shoe integrity, poor control on volumes and rates, and the like.

[0052] The disclosure has been illustrated in relation to particular embodiments, which are intended in all respects to be illustrative rather than restrictive. Those skilled in the art will recognize that the disclosure is capable of many modifications and variations without departing from the scope of the disclosure.

[0053] The above-described embodiments are merely exemplary illustrations of implementations set forth for a clear understanding of the principles of the disclosure. Variations, modifications, and combinations may be made to the above-described

embodiments without departing from the scope of the claims. All such variations, modifications, and combinations are included herein by the scope of this disclosure and the following claims. For example, we have discussed the method mainly in the context of compressive, reverse-fault stress settings, but it may be applied to normal-
5 fault and strike-slip stress settings. Similarly, we have discussed the method in terms of leakoff tests, but it may also be applied to other operations or drilling events that provide information on stress conditions, such as, but not limited to, lost circulation events or production tests.

CLAIMS

1. A method for determining a stress state solution space for a formation, comprising:

- 5 a) determining a line of shear failure as a function of leakoff pressure measured in the formation;
- b) determining a vertical stress; and
- c) determining each of a lower limit and an upper limit as a function of the vertical stress and the leakoff pressure.

10

2. The method of claim 1, each of the lower limit and the upper limit being a principle stress of a respective Mohr's circle that is in tangential contact with the line of shear failure, the vertical stress being the other principle stress of the Mohr's circles.

15

3. The method of claim 1, each stress state solution in the stress state solution space comprising three principle stresses, each principle stress being within a range defined by the lower limit and the upper limit.

20

4. The method of claim 1, the vertical stress being a principal stress of each stress state solution in the stress state solution space.

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5. The method of claim 1, each stress state solution in the stress state solution space comprising minimum and maximum principle stresses defining a Mohr's circle that is in tangential contact with the line of shear failure.

6. The method of claim 1, the stress state solution space comprising stress state solutions for each of normal-fault, reverse-fault, and strike-slip conditions.

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7. The method of claim 1, further comprising generating an output representing the stress state solution space.

8. The method of claim 7 wherein the output consists entirely or in part of a stress polygon, a visual representation, or machine readable instructions.
9. The method of claim 7, the output comprising a stress polygon representing the stress state solution space in reverse-fault, normal-fault, and strike-slip conditions.
10. The method of claim 1, the line of shear failure further being a function of one of: cohesion and the coefficient of friction.
11. A method for determining a stress state of a formation, comprising:
- a) determining a line of shear failure as a function of leakoff pressure measured in the formation;
 - b) determining at least one principle stress of a Mohr's circle that is in tangential contact with the line of shear failure.
12. The method of claim 11, further comprising determining one principle stresses of the Mohr's circle as a function of overburden pressure.

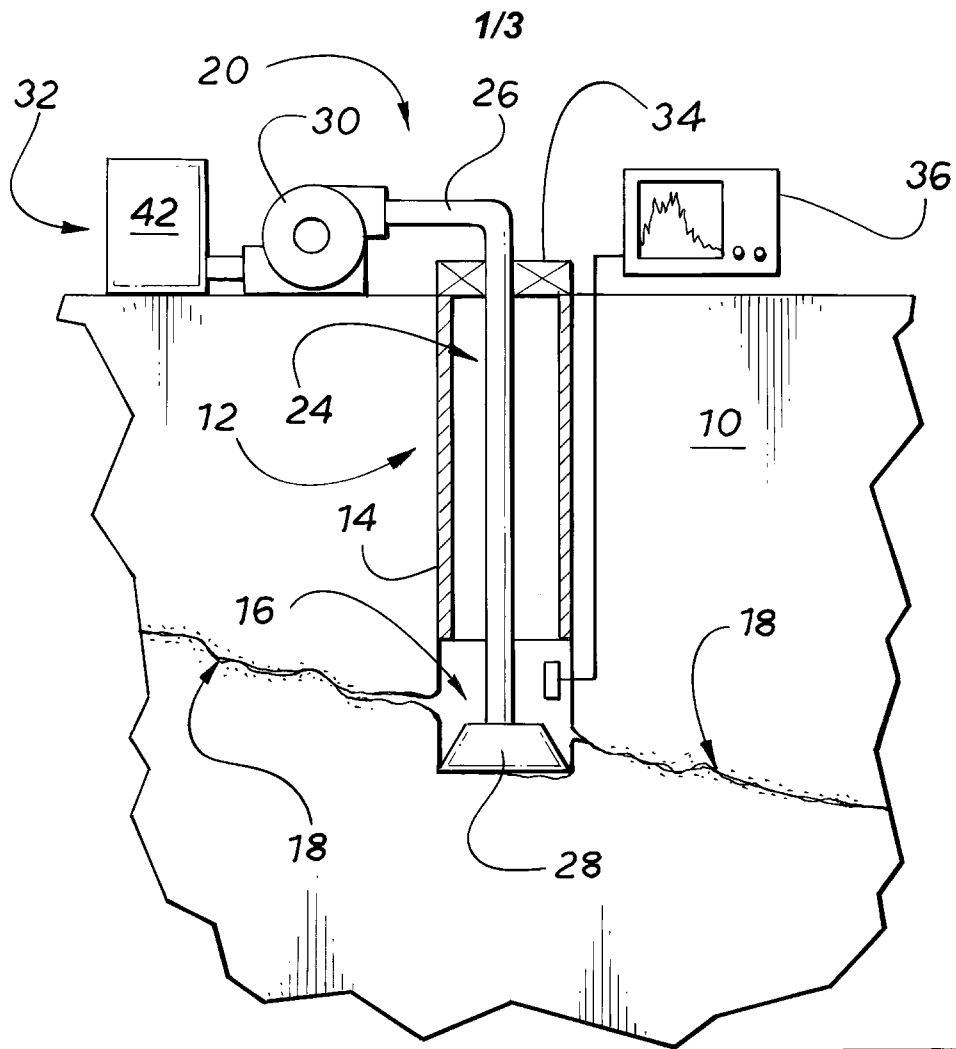


Fig. 1

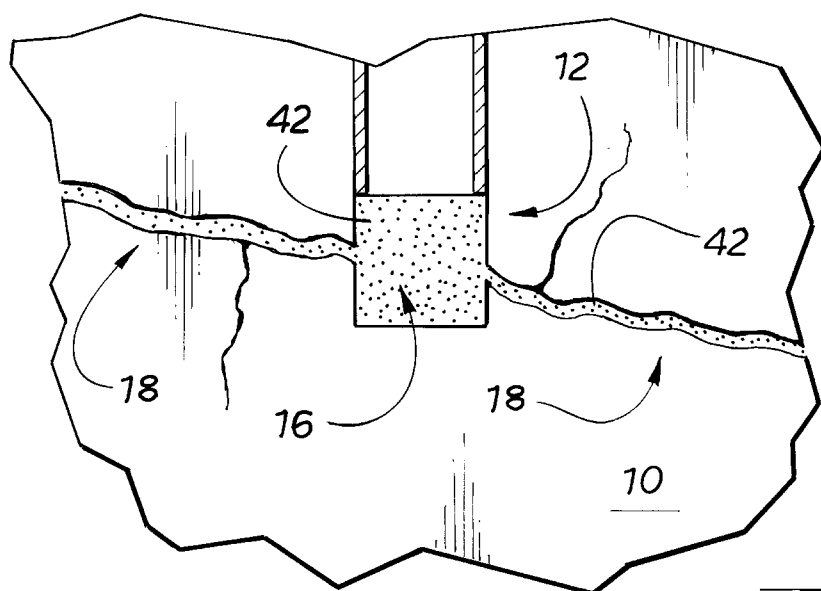


Fig. 2

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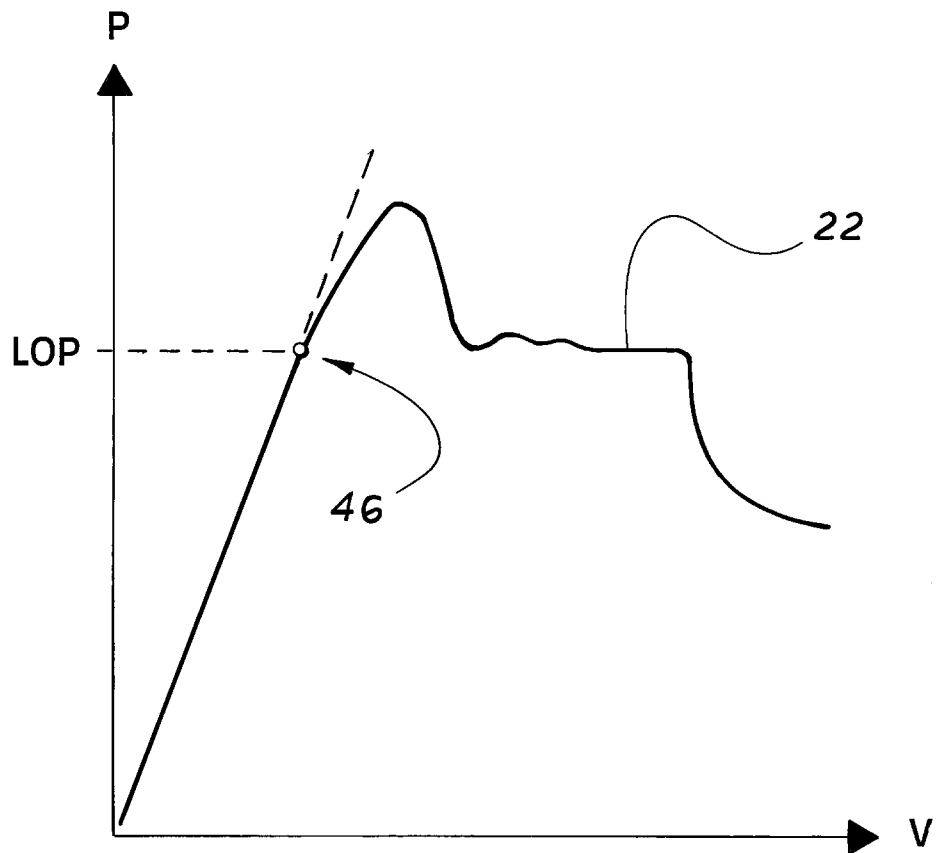
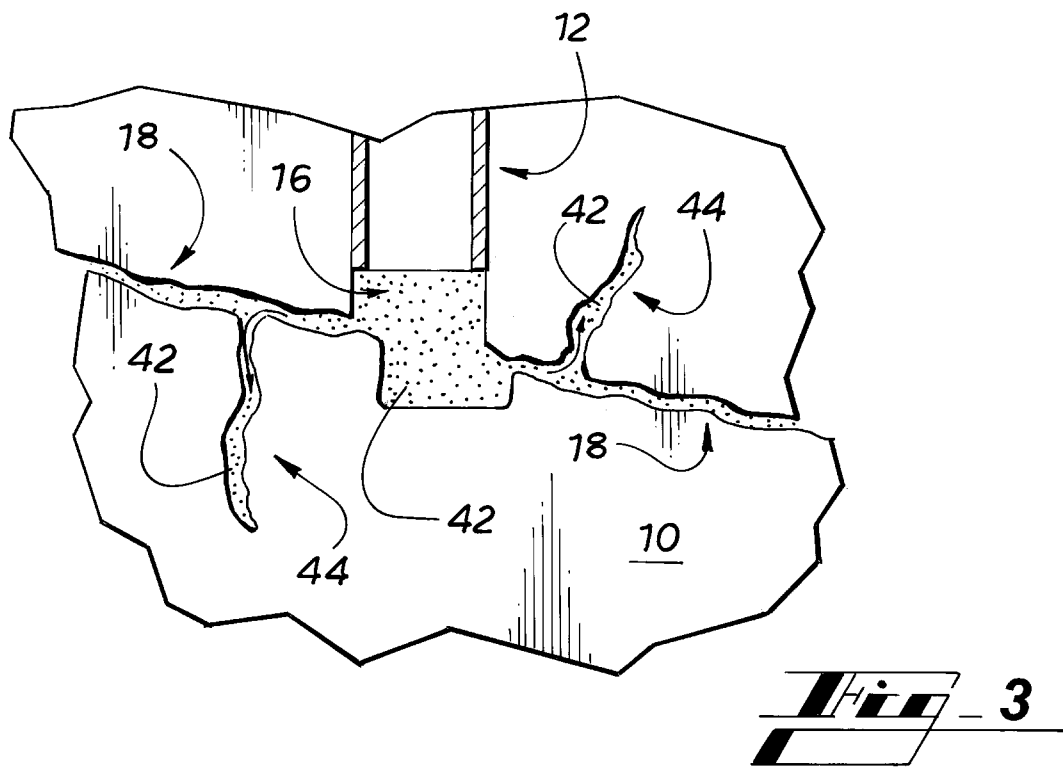
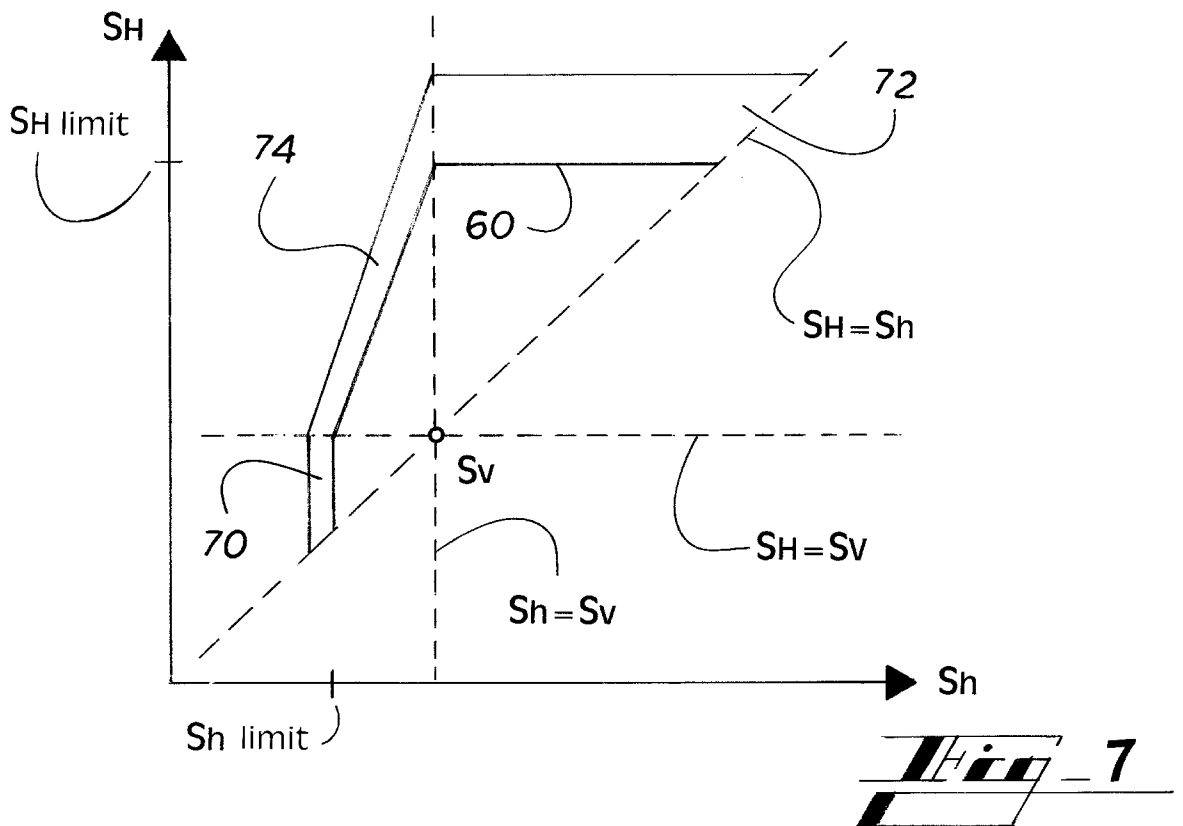
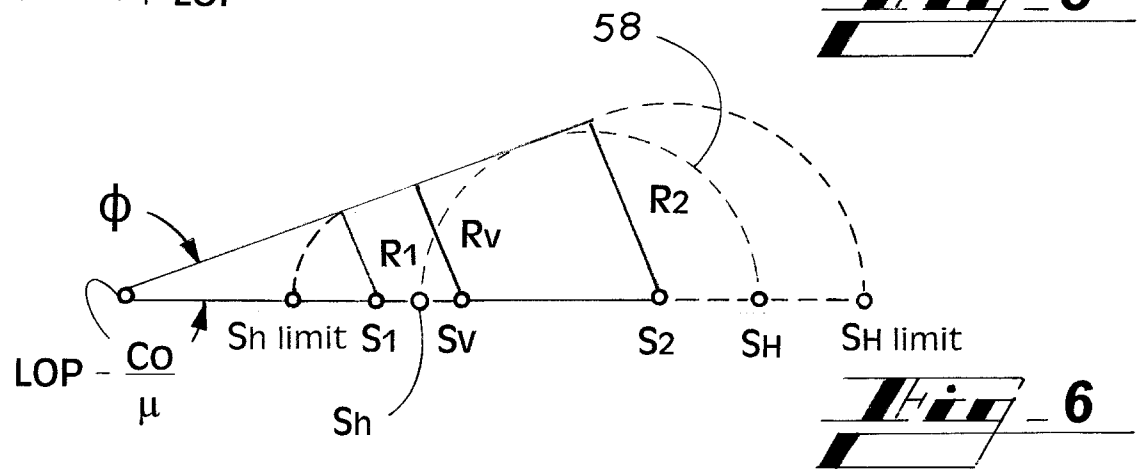
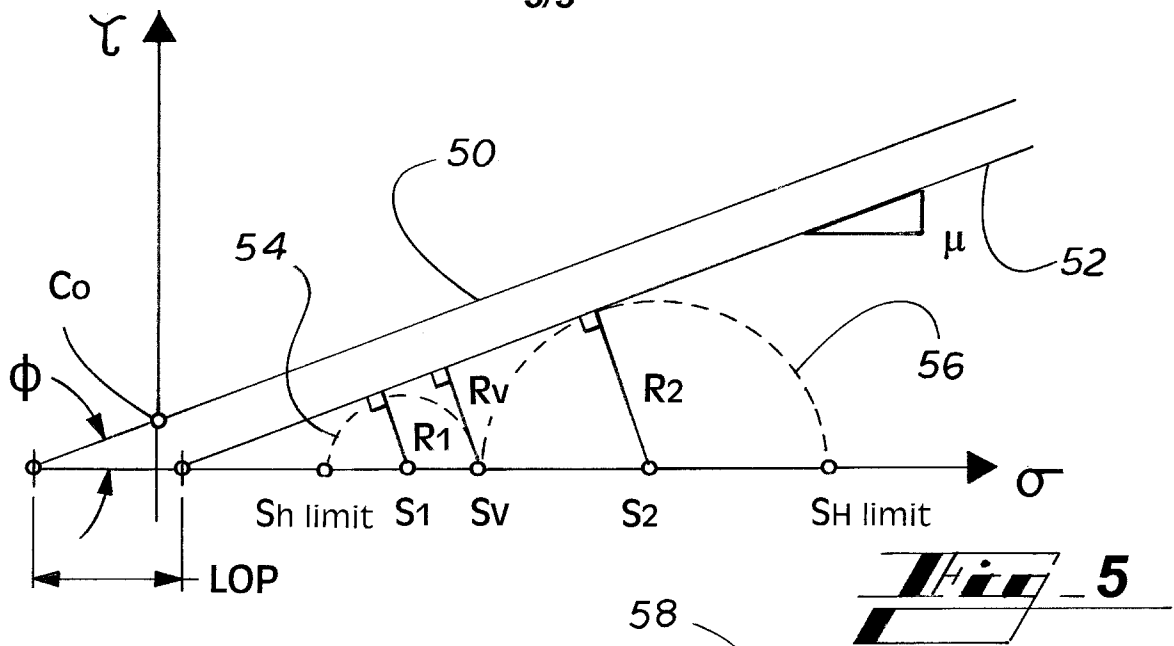


Fig. 4

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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US2009/069626**A. CLASSIFICATION OF SUBJECT MATTER*****E21B 49/00(2006.01)i, G01N 3/10(2006.01)i, G01N 3/00(2006.01)i, G01M 3/26(2006.01)i***

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: E21B 49/00; E21B 12/02; E21B 43/00; E21B 43/25; G01R 31/08; G01V 1/00; G06F 19/00

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Korean utility models and applications for utility models

Japanese utility models and applications for utility models

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

eKOMPASS(KIPO internal) & Keywords: stress, mohr, failure, leakoff pressure

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5415030 A (PUSHKAR N. JOGI et al.) 16 May 1995 See the abstract; figures 1-16; and claims 1-43	1-12
A	US 5494108 A (IAN D. PALMER et al.) 27 February 1996 See the abstract; figures 1-9; and claims 1-13	1-12
A	US 2007-0118292 A1 (DANIEL MOOS) 24 May 2007 See the abstract; figures 1-8; and claims 1-11	1-12
A	US 3907034 A (GEORGE O. SUMAN, JR.) 23 September 1975 See the abstract; figures 1-2; and claims 1-9	1-12
A	WO 2007-056278 A2 (SAUDI ARABIAN OIL COMPANY) 18 May 2007 See the abstract; figures 1-14; and claims 1-20	1-12
A	US 6386297 B1 (CRAIG HODGES COOLEY et al.) 14 May 2002 See the abstract; figures 1-14; and claims 1-46	1-12

☐ Further documents are listed in the continuation of Box C.☒ See patent family annex.

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"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

25 MAY 2010 (25.05.2010)

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/US2009/069626

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US 6386297 B1	14.05.2002	None	