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(54) **SYSTEMS AND METHODS FOR FLOW SENSOR BACK PRESSURE ADJUSTMENT FOR MASS FLOW CONTROLLER**

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None
See application file for complete search history.

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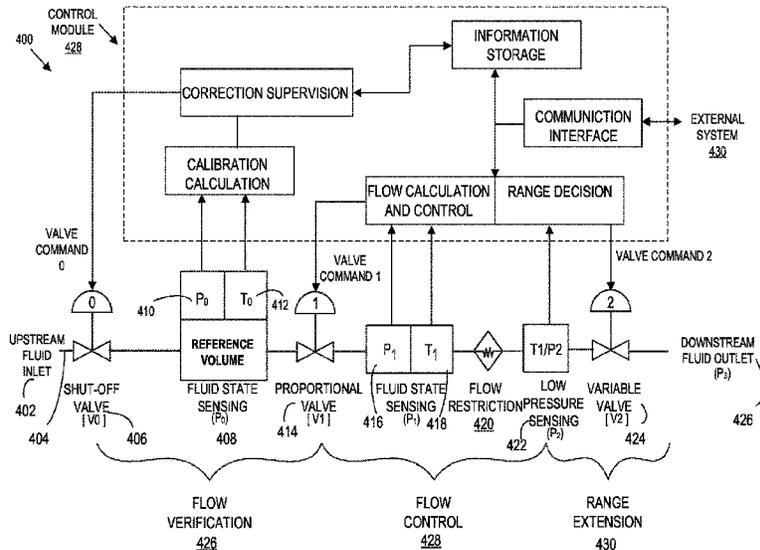
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(57) **ABSTRACT**

A mass flow control apparatus is capable of controlling a flow rate of a fluid to a tool. Pressure of the fluid is regulated by a solenoid valve, which receives signals from a control module. Various set points may be inputted to the control module, whereby control module receives pressure sensor signals from across a flow restrictor and adjusts the solenoid valve to control the fluid flow rate to equal a set point.

19 Claims, 10 Drawing Sheets



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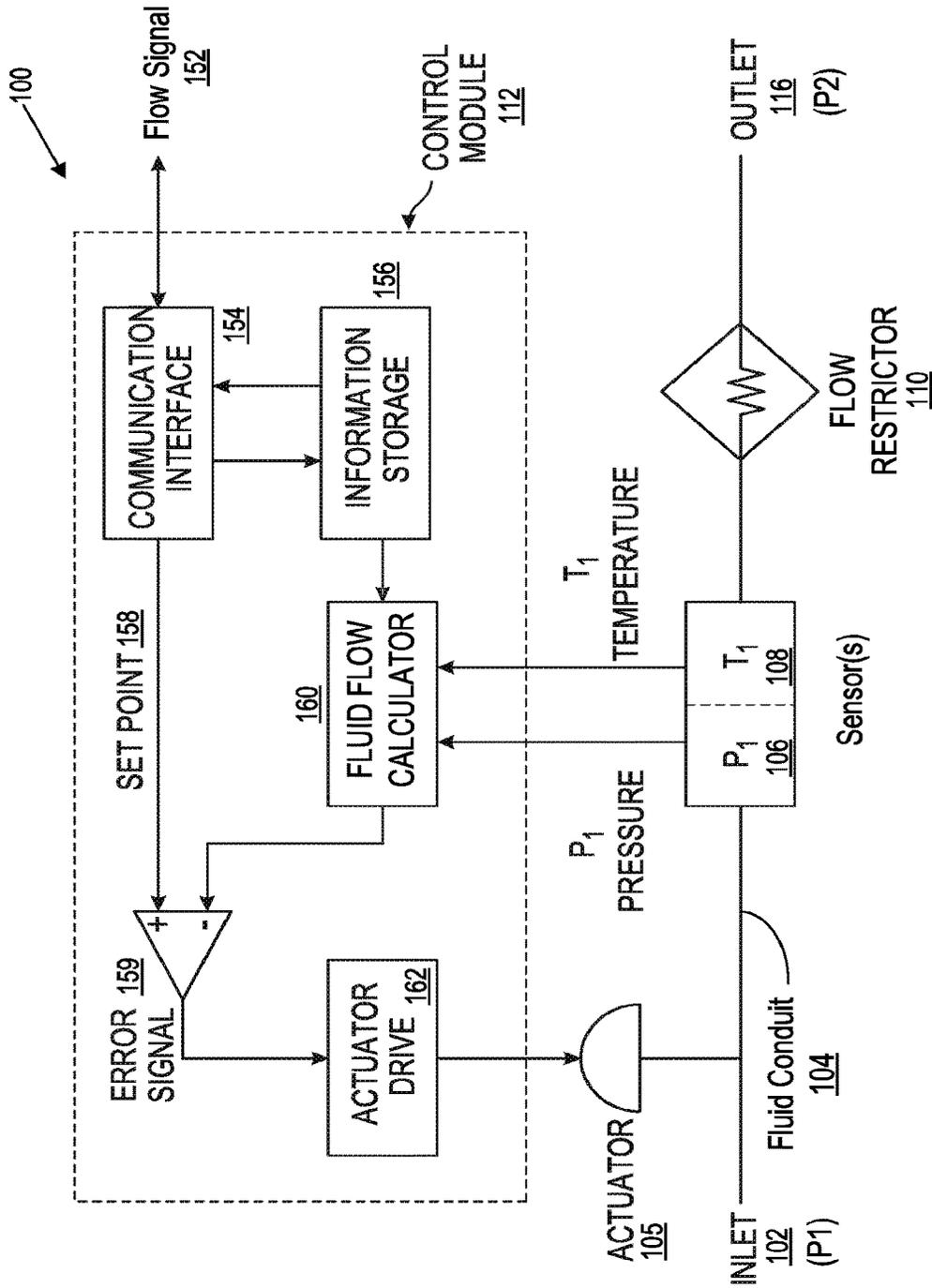


Fig. 1A

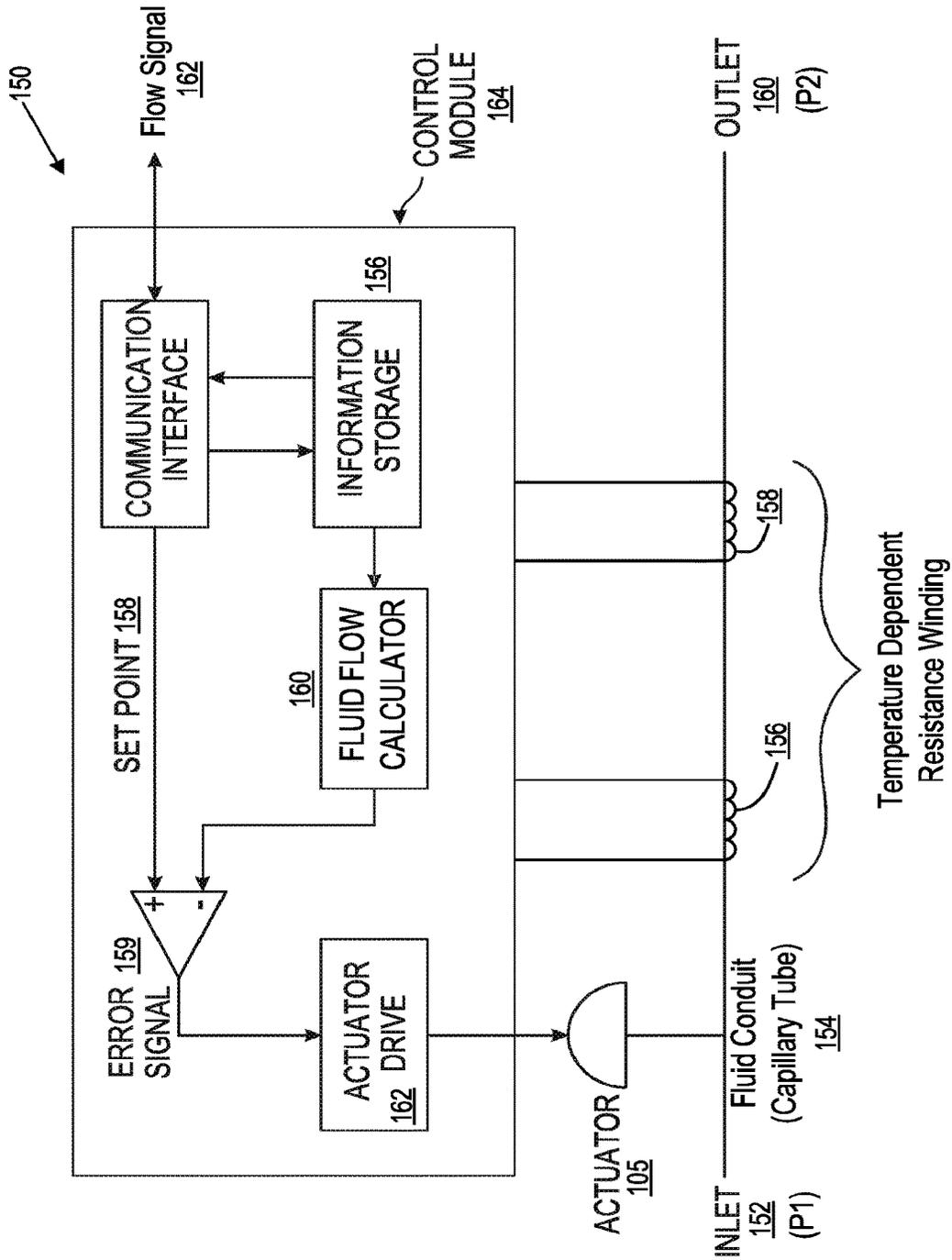


Fig. 1B

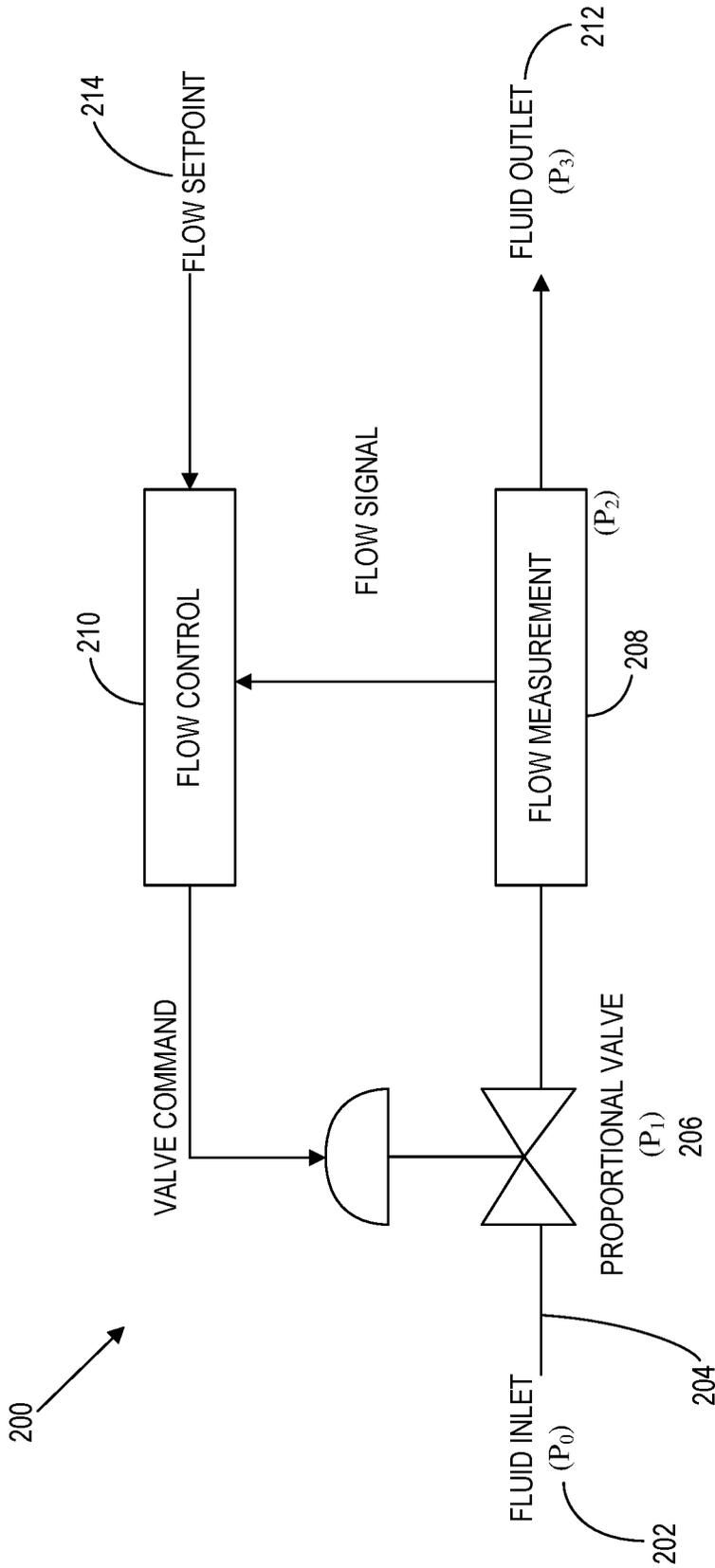


Fig. 2A

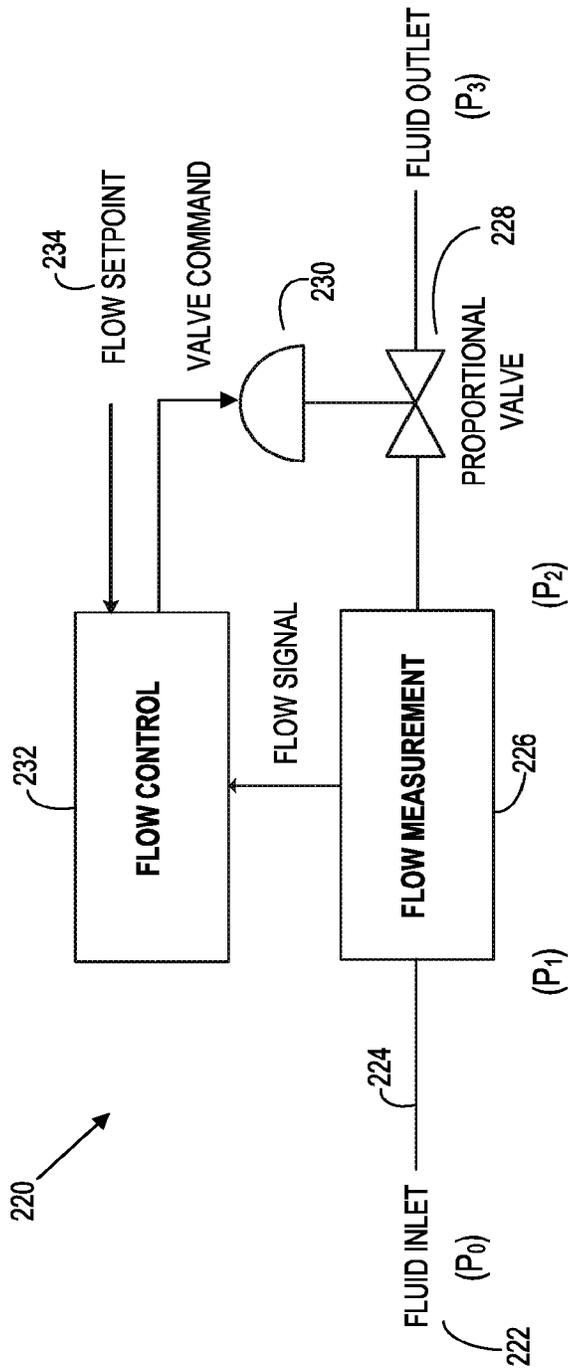


Fig. 2B

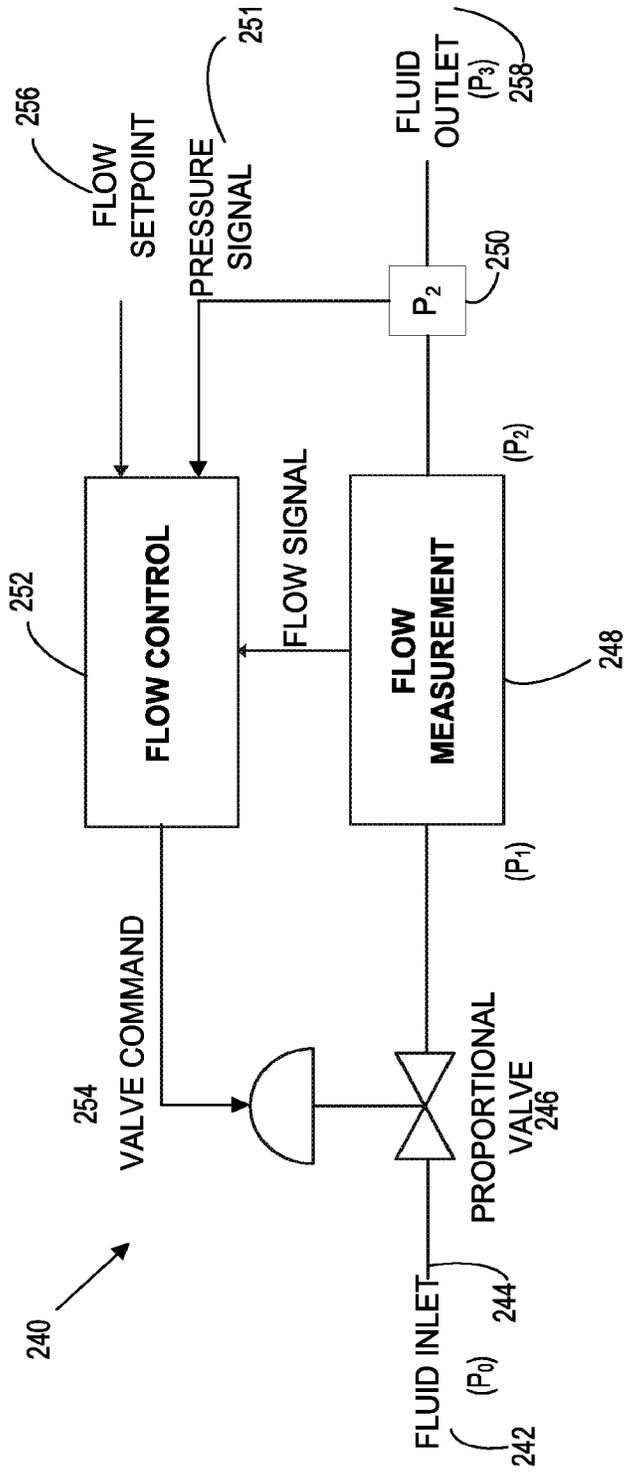


Fig. 2C

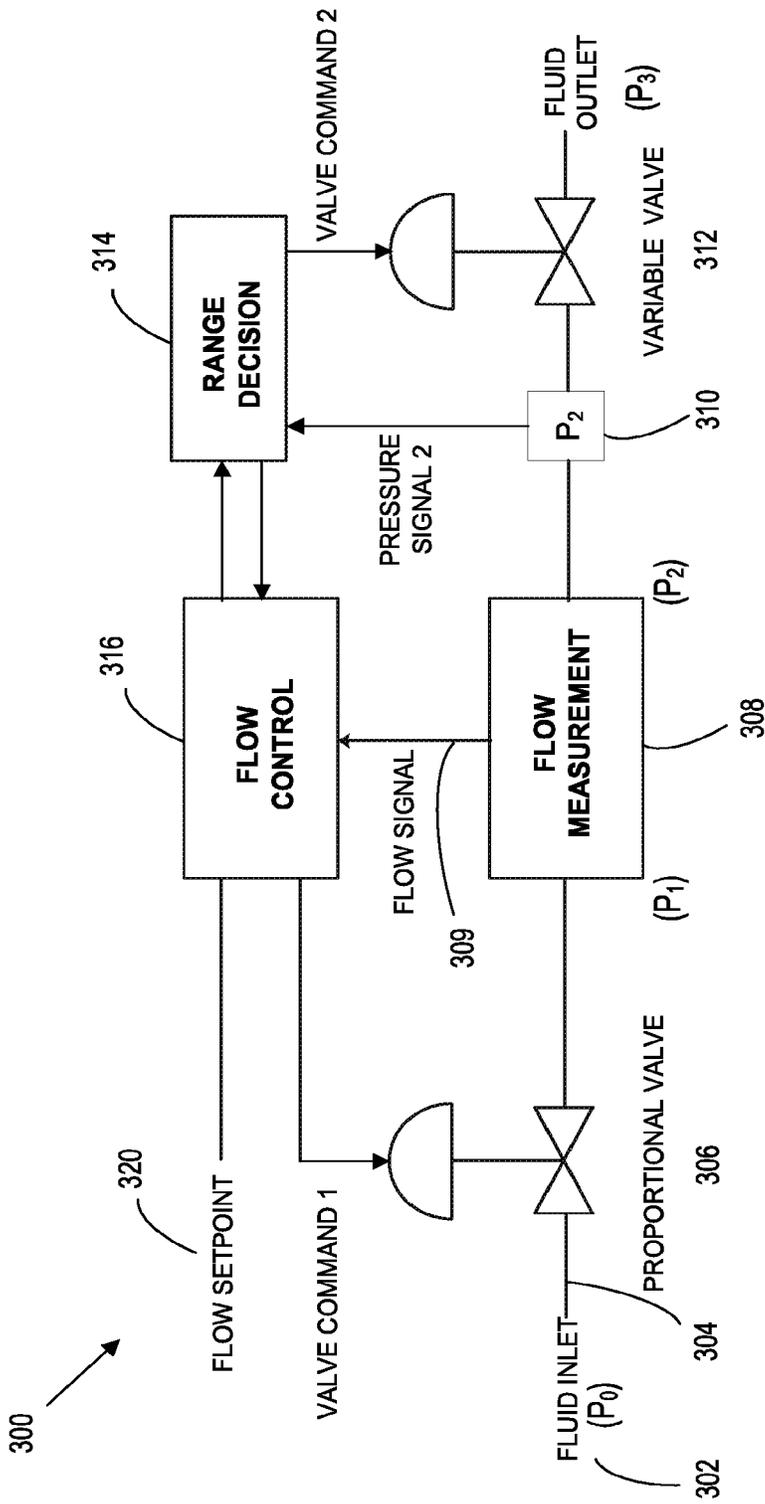


Fig. 3

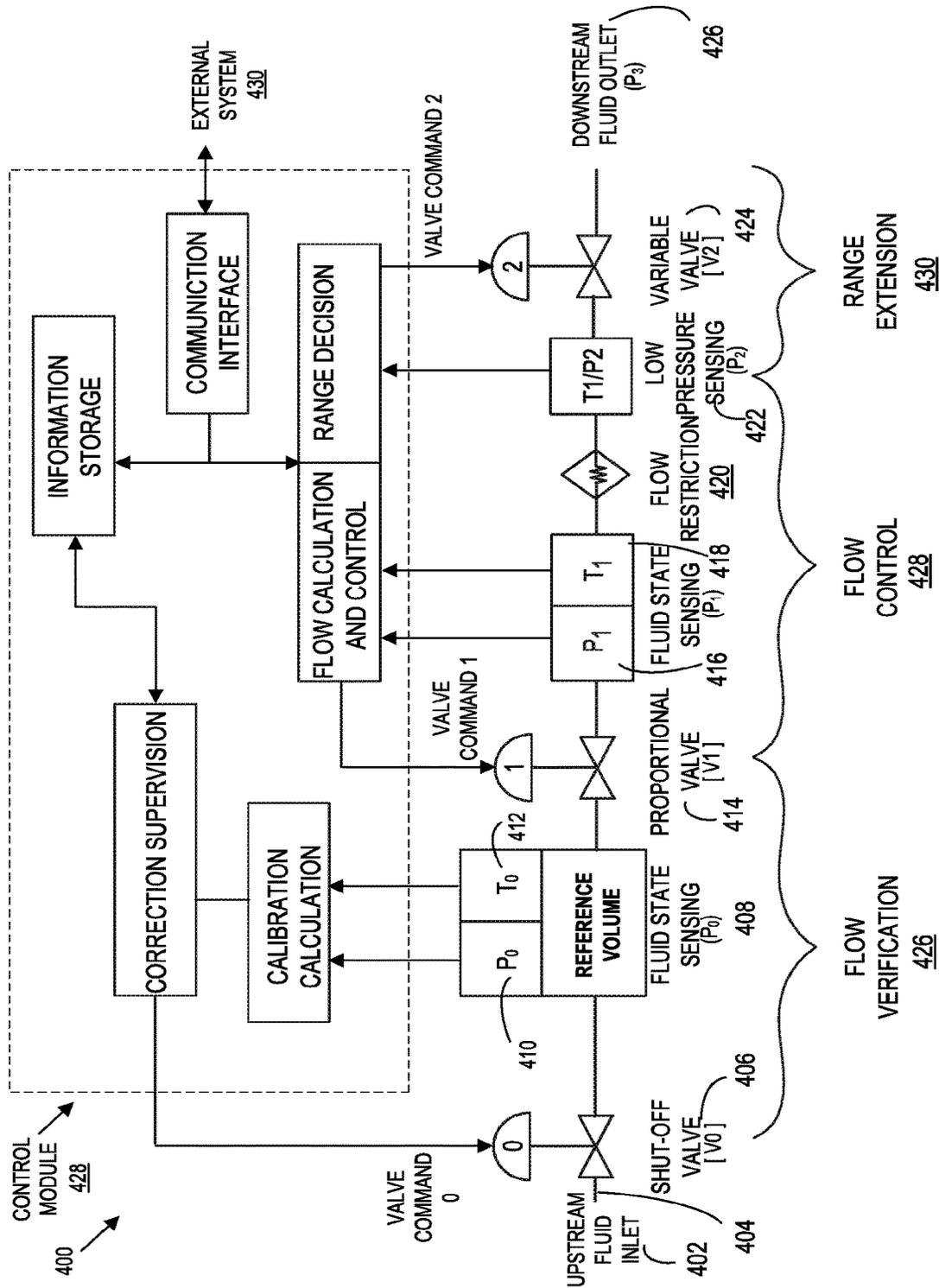


Fig. 4

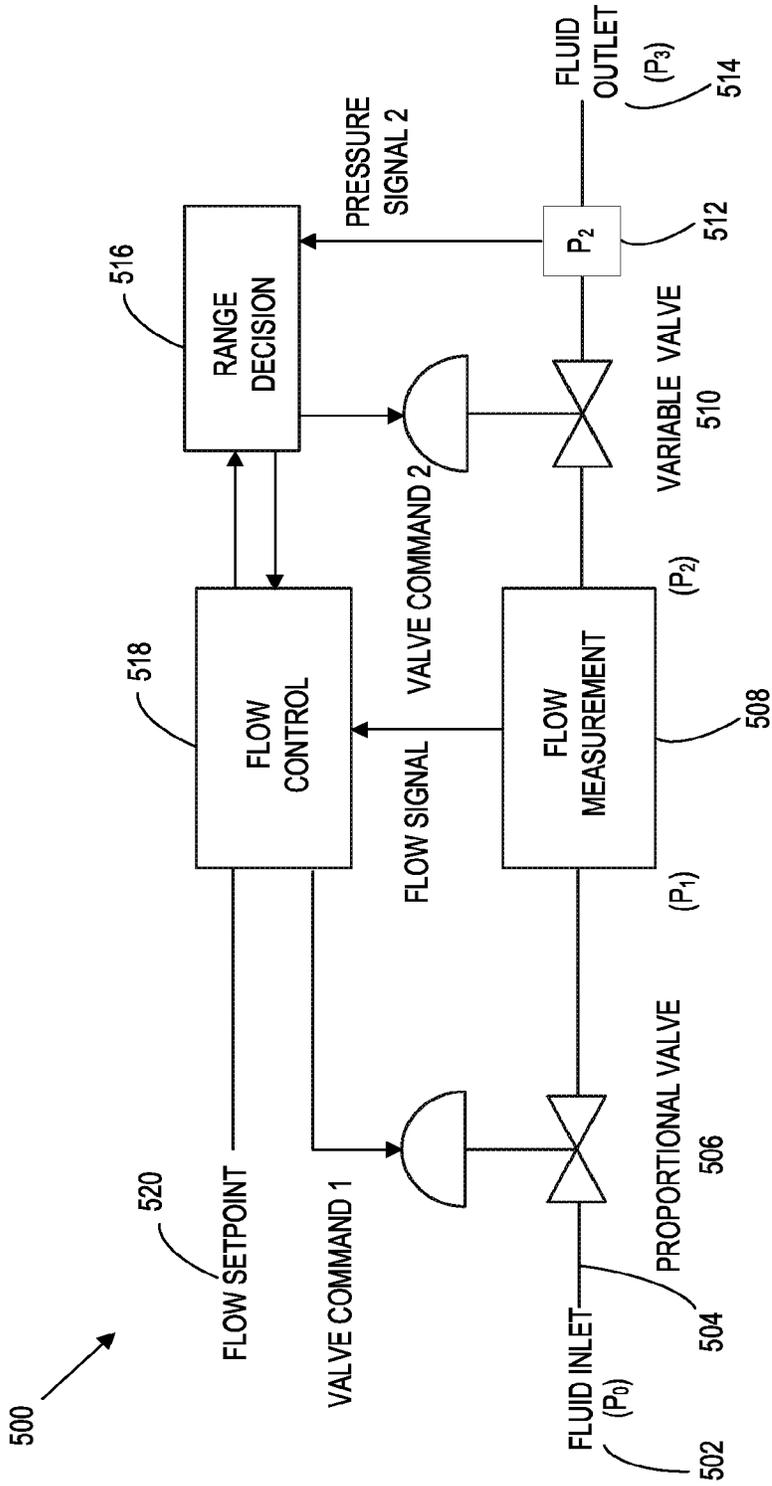


Fig. 5

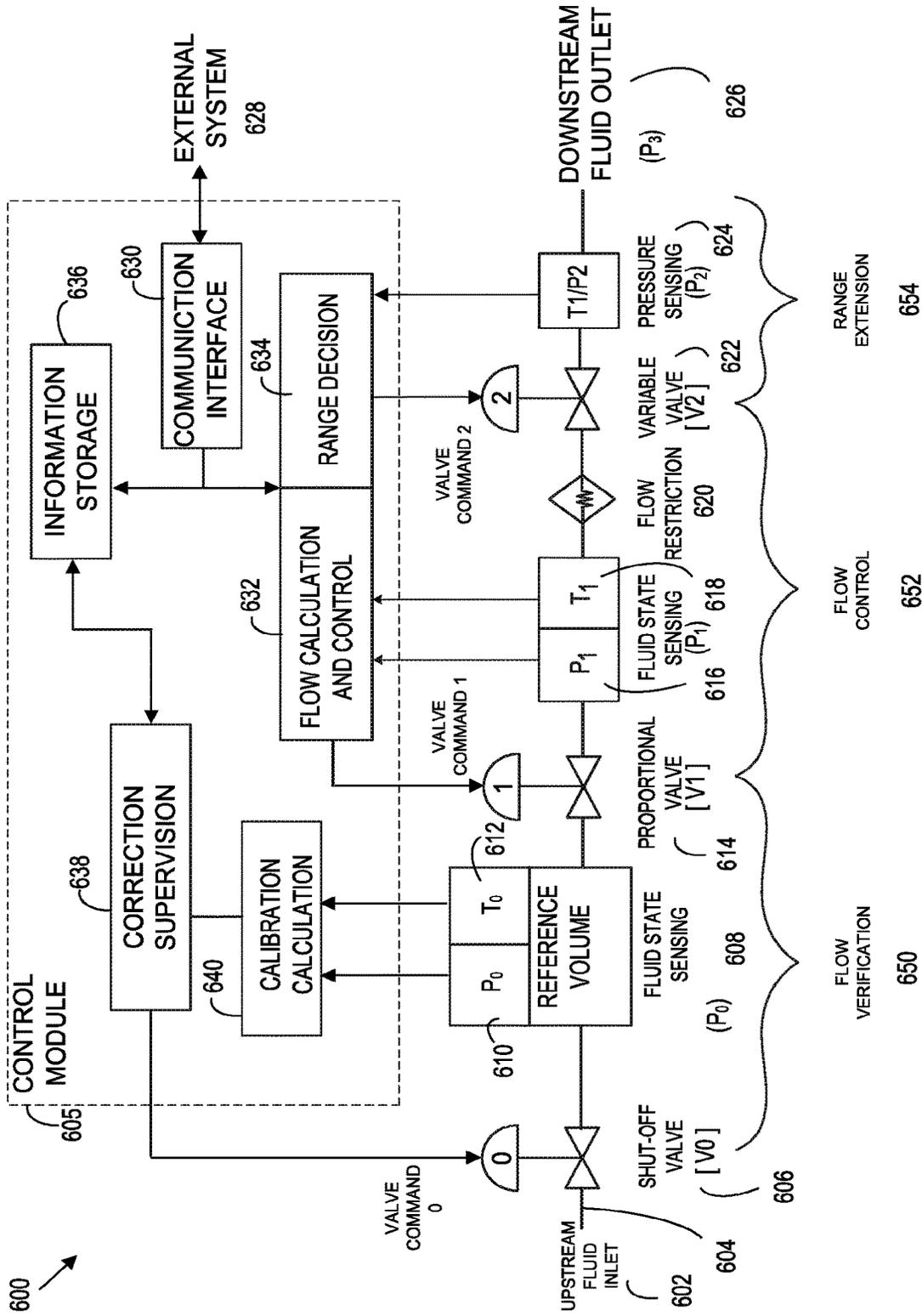


Fig. 6

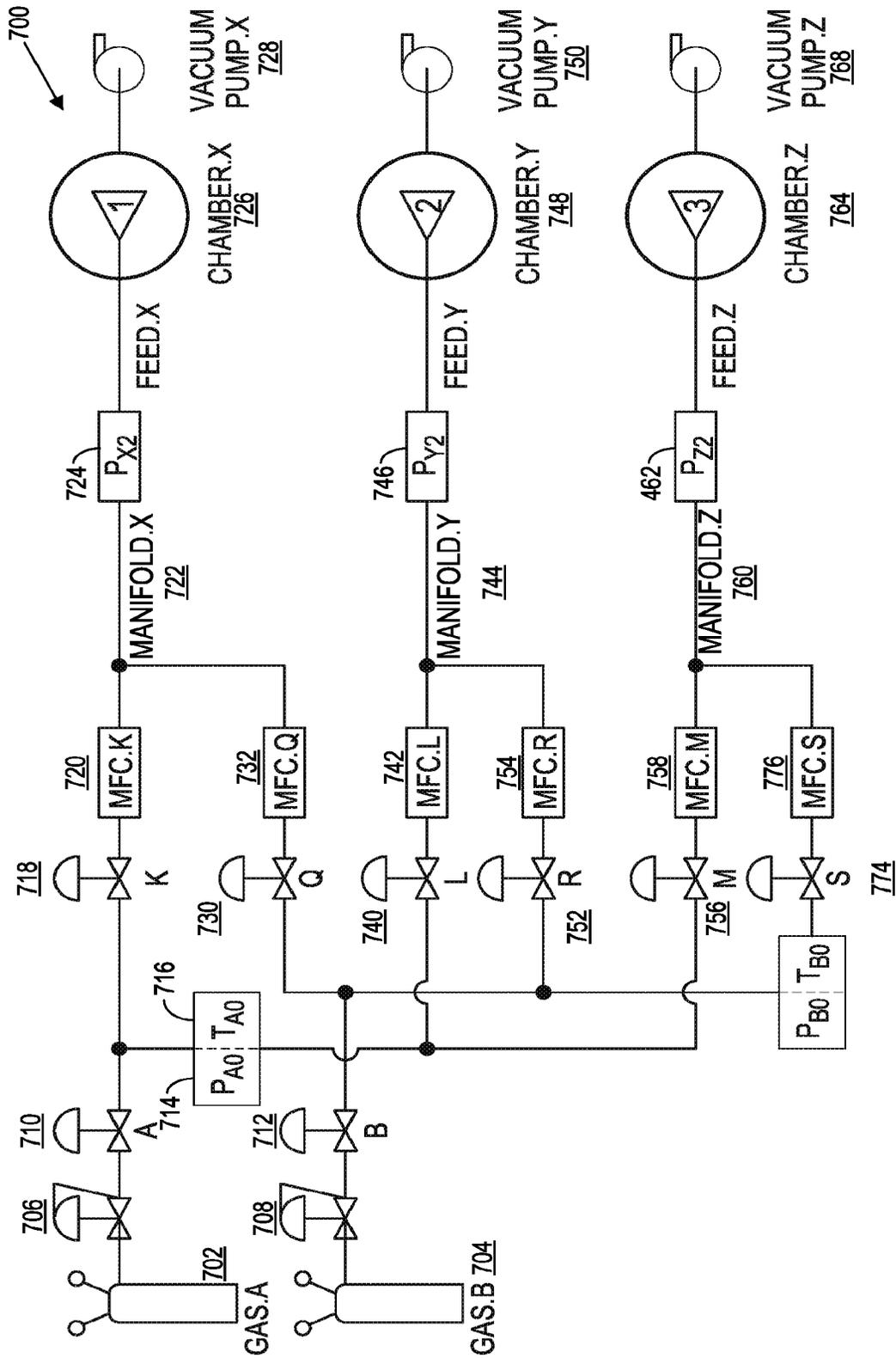


FIG. 7

**SYSTEMS AND METHODS FOR FLOW
SENSOR BACK PRESSURE ADJUSTMENT
FOR MASS FLOW CONTROLLER**

**PRIORITY CLAIM TO RELATED
APPLICATIONS**

This application is a continuation of U.S. patent application Ser. No. 15/907,138, filed Feb. 27, 2018, entitled as “SYSTEMS AND METHODS FOR FLOW SENSOR BACK PRESSURE ADJUSTMENT FOR MASS FLOW CONTROLLER”, which claimed the benefit of U.S. Provisional Patent Application No. 62/464,251, filed Feb. 27, 2017, entitled as “Systems, Apparatus and Methods for Flow Sensor Back Pressure Adjustment for Mass Flow Control”, the disclosures of which are incorporated by reference in their entirety.

BACKGROUND

Various embodiments relate to mass flow control apparatus. Mass flow controller may operate by modulating a fluid pressure. Fluid as used herein is intended to encompass materials which are in a gaseous phase because of specific combinations of pressure and temperature despite whether such materials are gaseous under everyday circumstances. Thus, fluids may include water vapor or boron trichloride (BCl₃), for example, along with common gaseous materials such as silane (SiH₄), argon, nitrogen, etc. The embodiments described below relate to determining the present flow conditions at a flow restriction in a fluid flow pathway to ascertain whether or not a chosen flow control algorithm is valid for those present conditions. At various times, a low fluid flow rate may be required while a silicon manufacturing chamber may also provide back pressure. Providing a low fluid flow rate in a backpressure environment may be challenging. Various embodiments described below are directed to addressing issues related to low flow conditions with back pressure from the upstream direction.

SUMMARY

In consideration of the foregoing applicant has invented a fluid mass flow control apparatus comprising three valves, a flow restriction, and provisions for determining three different fluid pressures and at least one temperature.

In accordance with one embodiment, a mass flow control apparatus is provided that includes a control module configured to receive a first set point for delivering a fluid delivery to a tool, responsive to the control module receiving a second set point that is significantly lower than a first set point, a variable control valve located downstream from the flow restrictor and downstream from a first pressure sensor configured to constrict to reduce the flow of the fluid responsive to receiving the second set point. The mass flow controller apparatus further including solenoid type valve as a variable control valve. The variable control valve is configured to control the downstream pressure from the flow restrictor. A second pressure sensor located upstream from the variable control valve, the second pressure sensor configured to measure back pressure from the tool. The variable control valve constricts sufficiently to increase the pressure of the fluid from the flow restrictor to be higher than the measured back pressure from the tool and adjust the pressure to the flow restrictor such that the pressure drops across the flow restrictor to yield a flow rate that is equal to the second set point. A proportional control valve that is a solenoid

valve to control the pressure to the flow restrictor and a shutoff valve including a solenoid valve to close the inlet supply to perform a rate of decay measurement operation.

In another embodiment, a mass flow control apparatus is provided that includes a proportional valve upstream of a flow measurement portion, a pressure sensing element fluidly connected to determine a fluid pressure, downstream of the flow measurement portion and a dynamically adjustable variable valve downstream of both the flow measurement portion and the pressure sensing element connection. A solenoid valve to control pressure to a flow restrictor with a proportional control valve that is a solenoid valve to control the pressure to the flow restrictor. A shutoff valve comprises a solenoid valve to close the inlet supply to perform a rate of decay measurement operation. A pressure-based flow sensor including a fluid conduit with fluidly coupled pressure and temperature sensing provisions upstream of a known flow restriction. A thermal-based flow sensor includes fluid conduit with two spaced apart temperature responsive elements affixed to the exterior of the fluid conduit. The dynamically adjustable variable valve can be adjusted to any of at least two different amounts of openings. The dynamically adjustable variable valve can be continuously adjusted to a range of openings.

In various embodiments, a mass flow control apparatus is provided that includes an inlet to a fluid pathway, a controllable shutoff valve, the controllable shutoff valve providing provisions for measuring a reference temperature (T₀) and a reference pressure (P₀) of a fluid contained within a reference volume of the fluid pathway, a proportional control valve, the proportional control valve providing provisions for measuring a first temperature (T₁) and a first pressure (P₁) of the fluid contained within the fluid pathway upstream of a flow restriction, the flow restriction providing provision for measuring a second pressure (P₂) of the fluid contained within the fluid pathway downstream of the flow restriction, a variable valve; and an outlet from the fluid pathway. The flow restriction is chosen from group of an orifice, a nozzle, a porous sintered metal element or a laminar flow structures. A supervision function may choose an action from group of self-calibration process, change of system parameter or storage of results.

In various embodiments, a method for a mass flow control apparatus is provided, including determining a fluid pressure downstream of a flow sensor, responding to the fluid pressure downstream and adjusting dynamically a variable valve downstream of the flow sensor to maintain desired operating conditions in the flow sensor; and maintaining and extending the useful operating range of the mass flow control apparatus. The method further including a flow verification capability. The flow verification capability including the steps of closing a shutoff valve to isolate a fluid pathway from an inlet while controlled mass flow continues through an outlet; making repeated measurements of a reference volume of a fluid pathway for a period of time, opening the shutoff valve to re-establish fluid pathway connection to the inlet, calculating a verified flow signal using pressure-volume-temperature methods; and providing a verified flow signal to a supervision function. The supervision function directs that a series of flow verification measurements be performed corresponding to different values of determined fluid pressures and fluid temperatures adjacent the flow restriction and determines a calibration curve for a discrete flow restriction based on the flow signals generated by the flow verification measurements.

A mass flow control apparatus including a control module configured to receive a first set point flow rate for delivering

a fluid delivery to a tool, responsive to the control module receiving a second set point that is significantly lower than a first set point flow rate: a variable control valve located downstream from a flow restrictor and downstream from a first pressure sensor, the variable control valve configured to constrict to adjust the pressure of the fluid responsive to receiving the second set point flow rate; and a proportional control valve located upstream from the flow restrictor to adjust the pressure to the flow restrictor. In some embodiments the variable control valve is a solenoid type valve. In various embodiments, the proportional control valve is a solenoid type valve. In various embodiments, the variable control valve is configured to control the pressure downstream from the flow restrictor responsive to receiving a significantly lower second set point; and wherein significantly lower is 5% of full scale fluid flow rate. In some embodiments, significantly lower would be at least one of 60%, 65%, 70%, 75%, 80%, 85%, 90% or 95% of the previously request set point flow rate.

In various embodiments, the variable control valve constricts the fluid flow in the flow path sufficiently to increase the pressure of the fluid from the flow restrictor to be higher than a back pressure from the tool and the proportional control valve is configured to adjust the pressure to the flow restrictor such that the pressure drop across the flow restrictor yields a flow rate that is equal to the second set point. In various embodiments, a reference volume may be configured to verify the actual flow rate by closing the fluid flow using a shut off valve and measuring the pressure rate of decay in the reference volume and adjusting one or both of the variable control valve or the proportional control valve until the second set point flow rate is achieved. In some embodiments, the mass flow controller may use thermal-based flow sensor and a supervision function. The mass flow control may include a thermal-based flow sensor with a fluid conduit with two spaced apart temperature responsive elements affixed to the exterior of the fluid conduit. In some embodiments, a variable control valve can be adjusted to any of at least two different amounts of openings. In some embodiments, a variable control valve can be continuously adjusted to a range of openings. In some embodiments, a variable control valve can be adjusted to provide a complete shut-off position. In some embodiments, a shut-off valve upstream from a reference volume, wherein the reference volume is upstream from a flow restrictor, the shut-off valve configured to close the inlet supply to perform a rate of decay operation; and wherein the shut-off valve is a solenoid type valve. In some embodiments, a first pressure sensor is configured to measure fluid pressure (P0) and a first temperature sensor is configured to measure temperature (T0) of a reference volume downstream from the shutoff valve; a proportional control valve, the proportional control valve providing provisions for measuring a second temperature (T1) and a second pressure (P1) of the fluid contained within the fluid pathway upstream of a flow restriction; the flow restriction providing provision for measuring a third pressure (P2) of the fluid contained within the fluid pathway downstream of the flow restriction; and an outlet from the fluid pathway. In some embodiments, a shut-off valve upstream from a reference volume, the reference volume is upstream from a flow restrictor, the shut-off valve configured to close the inlet supply to perform a rate of decay operation; wherein the shut-off valve is a solenoid type valve, and a proportional control valve that is a solenoid valve to control the pressure to the flow restrictor. In some embodiments, the flow restrictor is chosen from group

comprising of an orifice, a nozzle, a porous sintered metal element, a laminar flow structures or tubes.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1A is a schematic of a pressure-based flow controller.

FIG. 1B is a schematic of a thermal-based flow controller.

FIG. 2A is a schematic of a mass flow controller with a proportional valve upstream of a flow measurement portion.

FIG. 2B is a schematic of a mass flow controller with a proportional valve downstream of a flow measurement portion.

FIG. 2C is a schematic of a mass flow controller that is capable of pressure monitoring downstream of a flow measurement portion.

FIG. 3 is a schematic of a mass flow controller that includes a pressure sensing element connection downstream of a flow measurement portion and a dynamically adjustable variable valve further downstream of the pressure sensing element.

FIG. 4 is a schematic of a mass flow controller that includes a flow verification capability while using a pressure-based flow sensor.

FIG. 5 is a schematic of a mass flow controller that includes a dynamically variable valve downstream of a flow measurement portion and a pressure sensing element connection further downstream of the variable valve.

FIG. 6 is a schematic of a mass flow controller that includes a flow verification capability while using a pressure-based flow sensor.

FIG. 7 is an illustration showing portions of a complex fluid delivery system within a single large apparatus for processing semiconductor devices.

DETAILED DESCRIPTION

This invention is not limited in its application to the details of construction and the arrangement of components set forth in the following description or illustrated in the drawings. The invention is capable of other embodiments and of being practiced or of being carried out in various ways. Also, the phrasing and terminology used herein is for the purpose of description and should not be regarded as limiting. The use of “including,” “comprising,” or “having,” “containing,” “involving,” and variations thereof herein, is meant to encompass the items listed thereafter and equivalents thereof as well as additional items. The use of directional adjectives “inner,” “outer,” “upper,” “lower,” “upstream,” “downstream” and like terms, are meant to assist with understanding relative relationships among design elements and should not be construed as meaning an absolute direction in space nor regarded as limiting.

Embodiments are directed to systems and methods for a mass flow controller for responding to a request for a large reduction in flow rate or a large step down in flow rate. For example, a semiconductor manufacturing recipe may require a drop from 500 cc flow rate to drop to 25 cc. The bleed down time or the amount of time a mass flow controls takes to provide the reduction should be fast. Embodiments are directed to providing a variable control valve located downstream from each of the following elements within a mass flow controller: fluid state sensing element (including reference volume, pressure sensor and temperature sensor), proportional valve, additional pressure and temperature sensors, flow restrictor and third pressure sensor. As will be discussed in greater detail below the variable control valve

may be used to achieve faster step down response times. In some embodiments, the third pressure sensor may be located downstream from the variable valve and upstream from the fluid outlet. In various embodiments, upon receiving a signal to reduce the flow rate by 80%, 85%, 90% or 95% (greater than 80% or 90%) from the previous flow rate, the variable control valve may be constricted thus increasing the pressure at the pressure sensor located closest to the variable control valve. Additionally, when the variable control valve is shutoff the inlet pressure may be increased and the pressure at other pressure sensors may show an increase.

As described herein, by constricting the variable control valve the mass flow controller may be able to change its flow rate significantly while being able to conduct a rate of decay calculation. In some embodiments, the variable control valve may be a solenoid valve to control pressure to the flow restrictor (laminar flow element, orifice, hagen pouiselle tube) that may reduce cost of manufacturing. The variable valve that may be solenoid valve may act as a shutoff valve to perform a rate of decay operation to determine the flow rate. In various embodiments, the variable control valve may be a proportional control valve that is a solenoid to control the pressure to the flow restrictor and located upstream of the flow restrictor. The solenoid type proportional control valve may be used to close the inlet supply to perform a rate of decay operation.

FIG. 1A is a schematic of a pressure-based flow controller. A representative example of a pressure-based flow controller **100** (FIG. 1A) includes fluid inlet **102**, a fluid conduit **104** (e.g., a bore in a larger body of material or the like), a pressure sensor **106**, a temperature sensor **108**, a flow restrictor **110**, a control module **112**, a flow signal (e.g., set point or flow rate indicator), a fluid outlet **116**.

The fluid conduit **104** may be fluidly coupled to the pressure sensor **106** and temperature sensor **108** upstream of a known flow restrictor **110**. The pressure sensor **106** and temperature sensor **108** may be individual elements or function as a combined single unit element. The control module **112** may receive signal from and send signals to the temperature and pressure sensors (**106** and **108**). The control module **112** may control the flow restrictor **110** to achieve desired flow rate by adjusting the pressure and/or temperature to achieve a flow rate. The control module **112** may determine corresponding pressure and temperature conditions for a fluid moving through the conduit **104** whereby the mass flow rate may be calculated based upon characteristics of the known flow restriction provided by the flow restrictor **110**. The known flow restrictor **110** may be an orifice, nozzle, porous sintered metal element, or even a laminar flow structure such as a plurality of long narrow flow passageways. Knowledge of the pressure-temperature-flow characteristics of the flow restriction is often obtained by measurements made during a flow calibration process but other methods, such as direct measurement of mechanical dimensions, may also be feasible in some designs.

The control module **112** may include circuitry to control the various elements shown in FIG. 1A. The control module **112** may generate a flow rate signal **114** and provide excitation, sense, measure and calculate based on the received signals. In some embodiments, the control module **112** may receive a pressure measurement from the pressure sensor **106** and receive a temperature from the temperature sensor **108**. The control module **112** may adjust the flow restrictor **110** based on the desired set point received from an external system. The control module **112** may be configured to use the measured pressure to determine the actual flow rate based on historical calibration information for the system

100. The pressure sensor **106** may generate a pressure P1 and generate a signal that represents a pressure to the control module **112** that controls the flow restrictor **110**. The temperature sensor **108** may generate a temperature T1 and generate a signal to the control module **112** that represents a temperature T1 to the control module **150**. Next the gas/fluid may pass through a flow restrictor **110** to the outlet **116**.

FIG. 1B is a schematic of a thermal-based flow controller **150**. A representative example of a thermal-based flow sensor (FIG. 1B) includes a fluid inlet valve **152**, a fluid conduit **154** (typically a capillary tube) with two spaced apart temperature responsive elements **156** and **158** (herein illustrated as resistance windings) affixed to the exterior of the fluid conduit. Electronic circuitry in the control module **154** provides excitation to the temperature responsive elements and senses chosen properties of the elements whereby heat transfer caused by a fluid moving through the conduit **154** may be measured and a corresponding mass flow calculated. A typical mass flow meter may additionally include a known laminar flow element (not shown) fluidly coupled in parallel with the thermal-based flow sensor whereby a proportionate fluid flow passes through the laminar flow element. The control module **164** may generate a flow signal **162** that is indicative of the flow rate of the fluid through the fluid conduit **154**.

FIG. 2A is a schematic of a mass flow controller **200** that includes a fluid inlet **202** at pressure P0, a fluid conduit **204**, a proportional valve **206**, a flow measurement module **208**, a flow control **210**, a fluid outlet **212**, and a flow set point **214**. The proportional valve **206** may be located upstream of a flow measurement module **208**. A representative mass flow controller **200** (MFC) may include a flow measurement module **208** and a proportional valve **206** upstream (FIG. 2A) of the flow measurement module **208**, the upstream valve being actively modulated by a flow control module **210** (typically electronic circuitry) to adjust the fluid flow to match a desired flow set point.

Referring to FIG. 2B, FIG. 2B illustrates a mass flow controller **220** that includes a fluid inlet **222**, a fluid conduit **224**, a flow measurement module **226**, a proportional valve **228**, a valve command **230**, a flow controller **232** and a flow set point **234**. The flow measurement module **226** may include a pressure sensor, a temperature sensor. The mass flow controller **220** may include a proportional valve **228** downstream (FIG. 2B) of the flow measurement module **210**, the downstream valve **228** being actively modulated by a flow control module **232** (typically electronic circuitry) to adjust the fluid flow to match a desired flow set point **234**. The mass flow controller **220** arrangement with an upstream proportional valve **228** (FIG. 2A) advantageously provides the flow measurement portion some isolation from deleterious effects of pressure transients at the fluid inlet **222**. In case of a thermal-based flow sensor (FIG. 1B), the upstream proportional valve MFC arrangement (FIG. 2A) may directly subject the flow sensor to very low fluid outlet pressures which may adversely change to nonlinear heat transfer caused by fluid moving through the conduit. The MFC arrangement with a downstream proportional valve **228** (FIG. 2B) advantageously provides the flow measurement portion **226** some isolation from deleterious effects of low pressure and/or pressure transients at the fluid outlet **228**. However, such arrangement directly exposes the flow measurement portion **226** to the deleterious effects of pressure transients at the fluid inlet **222**. In case of a pressure-based flow sensor (e.g. FIG. 1A), the downstream proportional valve arrangement (FIG. 2B) possibly makes the

pressure drop across the flow restriction sub-critical. The pressure at the downstream side of the flow measurement portion **248** may be monitored (FIG. 2C) to determine whether a thermal-based flow measurement portion is operating in nonlinear conditions or whether a pressure-based flow measurement portion is operating in sub-critical conditions.

FIG. 2C is a schematic of a mass flow controller **240** that is capable of pressure monitoring downstream of a flow measurement portion. The mass flow controller **240** includes a fluid inlet **242**, a fluid conduit **244**, a proportional valve **246**, a flow measurement **248**, a pressure sensor **250**, a flow control module **252**, a valve command **254**, a flow set point **256** and a fluid outlet **258**. The pressure at the downstream side of the flow measurement portion **248** may be monitored (FIG. 2C) to determine whether a thermal-based flow measurement portion is operating in nonlinear conditions or whether a pressure-based flow measurement portion **248** is operating in sub-critical conditions. The flow control module **252** may be configured to receive a flow set point **256** and send commands to the proportional valve **246**. Pressure sensor **250** generates a pressure signal **251** as an input to flow control **252**. The flow control **252** receives the pressure signal **251** and determines the flow rate and may adjust the proportional valve **246**.

FIG. 3 is a schematic of a mass flow controller **300** that includes a fluid inlet **302**, fluid conduit **304**, a proportional valve **306**, a flow measurement module **308**, a pressure sensor **310**, a variable valve **313**, a range decision module **314**, a flow control **316**, a flow set point **320** and a fluid outlet **322**. Mass flow controller **300** includes a pressure sensor **310** downstream of a flow measurement module **314** and a dynamically adjustable variable valve **312** further downstream of the pressure sensor **310**. An embodiment of the mass flow control controller **300** (FIG. 3) includes a proportional valve **306** upstream of a flow measurement module **308**, a pressure sensor **310** fluidly connected to determine a fluid pressure downstream of the flow measurement module **308**, and a dynamically adjustable variable valve **312** downstream of both the flow measurement module **308** and the pressure sensor **310**. The downstream pressure sensor **310** and variable valve **312** may be used with either a pressure-based or a thermal-based flow sensor. The variable valve **312** may be controllably adjusted (set) to any of at least two different amounts of opening (fluid conductance).

The variable valve **312** may additionally provide a complete shut-off in a third adjustment condition (setting) although this capability is optional. The variable valve **312** may be of a type with a continuously adjustable range of openings. The pressure sensor **310** may be of any convenient type and may optionally further include fluid temperature measuring provisions such as a temperature sensor.

An adjustment decision may be made, and opening of the variable valve **312** consequently adjusted, in response to a magnitude of the determined fluid pressure downstream of the flow measurement module **308** relative to a chosen threshold. The chosen threshold may be selected to ensure the flow measurement module **308** is subjected to at least a minimum (one half atmosphere, for example) determined downstream fluid pressure. Alternatively, in some embodiments, the chosen threshold may be selected to ensure the flow measurement portion is operating in a desired linear regime. The opening of the variable valve **310** may be held relatively constant, and specifically changed according to known limitations of the flow measurement module **308**, with intentional hysteresis caused by selecting a new chosen

threshold contemporaneous with each specific change of opening. Yet another control scheme may dynamically modulate the adjustment of the variable valve **312** to maintain a relatively constant determined fluid pressure downstream of the flow measurement module **308**. In yet another embodiment, the flow controller **316** may use a control scheme to select the chosen threshold based at least in part upon the pressure drop across the flow measurement module **308**. In another embodiment, the flow controller **316** may use a control method to select the chosen threshold based at least in part on the change of pressure across the flow measurement module **308**. The proportional valve **306** and the variable valve **312** control the flow of the fluid through the mass flow controller **300**. The variable valve **312** may be used to help the mass flow controller **300** have a faster step-down response when reducing the flow by more than 50%. In other embodiments, the variable valve **312** may be used to help the mass flow controller **300** have a faster step up response when increasing the flow of the fluid by more than 50%.

FIG. 4 is a schematic of a mass flow controller **400** that includes a flow verification capability while using a pressure-based flow sensor. The mass flow controller **400** may comprise (in upstream to downstream flow sequence) a fluid inlet **402**, to a fluid pathway **404**, a controllable shutoff valve **406**, provisions for measuring a reference temperature **412** (T₀) and a reference pressure **410** (P₀) of a fluid contained within a reference volume **408** of the fluid conduit **404**, a proportional control valve **414**, provisions for measuring a first temperature **418** (T₁) and a first pressure **416** (P₁) of the fluid contained within the fluid pathway upstream of a flow restriction **420**, provisions for measuring a second pressure **422** (P₂) of the fluid contained within the fluid pathway downstream of the flow restriction **420**, a variable valve **424**, and an outlet **426** from the fluid pathway **404**. Knowing the aggregate volume of fluid contained within the reference volume **408**, plus any directly connected fluid conduit **404** between the shutoff valve **406** and the proportional valve **414**, enables flow verification (self-calibration) of the embodiment mass flow controller **400**. Flow verification method includes closing the shutoff valve **406** to isolate the fluid conduit **404** from the inlet **402** while controlled mass flow continues through the outlet, making repeated measurements of the reference temperature **410** (T₀) and the reference pressure **412** (P₀) of the fluid contained within the reference volume **408** of the fluid conduit **404** for a period of time, opening the shutoff valve **406** to re-establish fluid pathway connection to the fluid inlet **402**, calculating a verified flow signal using pressure-volume-temperature (PVT, also known as Rate Of Fall, RoF) methods related to the aggregate volume of fluid, and providing the verified flow signal to a supervision function (control module **428**). The control module **428** may subsequently choose whether to enable additional self-calibration processes, change a system parameter, merely store the results, or take other actions. For example, the control module **428** may direct that a series of flow verification measurements be performed corresponding to different values of determined fluid pressures (P₁, P₂) and fluid temperature (T₁) adjacent the flow restriction **420**. This series of flow verification measurements readily determines a calibration curve, for a discrete flow restriction, based at least in part upon the verified flow signals. It should be noted the control module **428** does not require any particular critical ratio (P₁/P₂) be maintained between the determined upstream (P₁) and downstream (P₂)

pressures when a known calibration curve is obtained. The known calibration curve may be entirely empirical or conform to a theoretical model.

FIG. 5 is a schematic of a mass flow controller 500 that includes a dynamically variable valve downstream of a flow measurement module 508 and a pressure sensing element 512 further downstream of the variable valve 510. Another embodiment of a mass flow controller 500 (FIG. 5) includes a proportional valve 506 upstream of a flow measurement portion 508, a dynamically adjustable variable valve 510 downstream of the flow measurement portion, and a pressure sensing element fluidly connected to determine a fluid pressure downstream of the flow measurement portion and the adjustable variable valve. The downstream pressure sensing element 512 and variable valve 510 combination may be used with either a pressure-based or a thermal-based flow sensor. The variable valve 510 may be controllably adjusted (set) to any of at least two different amounts of opening (fluid conductance). The variable valve 510 may additionally provide complete shut-off in a third adjustment condition (setting) although this capability is optional. The variable valve 510 may be of a type with a continuously adjustable range of openings. The pressure sensing element 512 may be of any convenient type and may optionally further include fluid temperature measuring provisions. An adjustment decision may be made by the range decision 516, and opening of the variable valve 510 consequently adjusted, in response to operating conditions of the apparatus as further explained below.

FIG. 6 is a schematic of a mass flow controller 600 that includes a flow verification capability while using a pressure-based flow sensor. In various embodiments, of a mass flow controller 600 may additionally include a flow verification capability (FIG. 6). The mass flow controller 600 includes (in upstream to downstream flow sequence) an inlet 602, a fluid pathway 604, a controllable shutoff valve 606, provisions for measuring a reference temperature 612 (T0) and a reference pressure 610 (P0) of a fluid contained within a reference volume portion 608 of the fluid pathway 604, a proportional control valve 614, provisions for measuring a first temperature 618 (T1) and a first pressure 616 (P1) of the fluid contained within the fluid pathway upstream of a flow restriction 620, the flow restriction 620, a variable valve 622, provisions for measuring a second pressure (second pressure sensor 624) (P2). In various embodiments the second pressure sensor 624 may measure the fluid contained within the fluid pathway 604 downstream of the flow restriction 620 and the variable valve 622, and an outlet from the fluid pathway 604. Knowing the aggregate volume of fluid contained within the reference volume 608, plus any directly connected fluid pathway portions between the shutoff valve 606 and the proportional valve 614, enables flow verification (self-calibration) of another embodiment of the mass flow control apparatus. Flow verification involves closing the shutoff valve 606 to isolate the fluid pathway 604 from the inlet 602 while controlled mass flow continues through the outlet 626, making repeated measurements of the reference temperature 612 (T0) and the reference pressure 610 (P0) of the fluid contained within the reference volume 608 of the fluid pathway 604 for a period of time, opening the shutoff valve 606 to re-establish fluid pathway connection to the inlet 602, calculating a verified flow signal using pressure-volume-temperature (PVT, also known as Rate Of Fall, RoF) methods related to the aggregate volume of fluid, and providing the verified flow signal to a control module 605. The control module 605 may subsequently choose whether to enable additional self-calibration processes, change a

system parameter, merely store the results, or take other actions. For example, the control module 605 may direct that a specific valve command be presented to the variable valve 622 and a series of flow verification measurements performed corresponding to different values of determined fluid pressures (P1, P2) and fluid temperature (T1) adjacent the flow restriction 620 and variable valve 622. This series of flow verification measurements readily determines a calibration curve, for a composite flow restriction comprising the original discrete flow restriction plus the partially open variable valve 622, based at least in part upon the verified flow signals.

In various embodiments, the control module 605 may relate to making an adjustment decision using a range decision 634, and adjusting an opening of the variable valve 622 downstream of the flow measurement portion (reference volume 608), in response to a magnitude of one or more determined fluid pressures relative to a chosen threshold. In particular, if the flowing fluid pressure drop across the flow restriction 620 and variable valve 622 (P1-P2) is less than a chosen threshold, then a revised valve command may be presented to the variable valve 622 causing the variable valve 622 to assume a less open more flow restricting condition. A flow verification measurement may then provide a verified flow signal for comparison with calculated mass flow (using P1, T1, P2) through the composite flow restriction (which is comprised of the discrete flow restriction 620 and the variable valve 622) obtained by using a previously obtained calibration curve associated with the particular composite flow restriction 620. If the verified flow signal and calculated mass flow are suitably close to identical (for example, 0.5%), then the variable valve may be considered as having returned to a known condition and the supervision function may affirm use of the previously obtained calibration curve with the particular composite flow restriction. It should be noted the control module does not require any particular critical ratio (P1/P2) be maintained between the determined upstream first (P1) and downstream second (P2) pressures when a known calibration curve has been obtained. The known calibration curve may be entirely empirical or conform to a theoretical model.

In low flow and low set point applications additional advantages may be obtained from a variable valve 622 that is additionally able to provide complete shut-off in a third adjustment condition (setting). In any of the previously described embodiments a lower auto-shutoff threshold (for example, 0.25% of full-scale) may be provided to the flow control portion of a mass flow controller such that a set point request less than the auto-shutoff threshold causes the flow control portion to immediately command the proportional valve to its most flow restricting condition without need to obtain a calculated mass flow. Similarly, a variable valve capable of shutoff may be simultaneously commanded to close completely and thereby bring fluid flow to a very rapid halt. In the situation of embodiments (FIG. 3 & FIG. 4) wherein the downstream second pressure (P2) is determined immediately adjacent to the discrete flow restriction, and upstream of the variable valve (described above), then a variable valve having a continuously adjustable range of openings may be advantageously used to control the pressure drop (P1-P2) across the flow restriction while the proportional valve is commanded into its most flow restricting or other convenient condition.

FIG. 7 is an illustration showing portions of a complex fluid delivery system within a single large apparatus for processing semiconductor devices. Illustrated in FIG. 7 is an abbreviated schematic illustrating portions of a complex

fluid delivery system within a single large apparatus for processing semiconductor devices. A plurality of new embodiment mass flow controllers (of the type illustrated in FIG. 5 & FIG. 6) may be used with a plurality of process gas species to feed reactants into a plurality of vacuum chambers. Such an apparatus is often referred to as a "tool." As shown in the abbreviated schematic, a group ("pallet") of mass flow controllers (MFC.K, MFC.L) enable the simultaneous combination of several different process gases (GAS.A, GAS.B) into a single manifold (MANIFOLD.X) which feeds a gas distribution structure ("showerhead"-1) inside a vacuum chamber (CHAMBER.X). Insufficient conductance in some manifold plumbing (FEED.X) may result in the downstream pressure (Px2), of a particular group of mass flow controllers, becoming too high to maintain choked flow conditions within one or more mass flow controllers within the group. In an alternative scenario, the downstream pressure (Px2) within the manifold (MANIFOLD.X) may be so low the requisite operating conditions internal to a specific new embodiment mass flow controller (e.g. MFC.K) cannot be maintained as desired and the corresponding variable valve within the MFC adjusted as previously discussed. The pressure within the manifold may be monitored (Px2) and a corresponding signal provided to all mass flow controllers within the group (MFC.K, MFC.Q) as an alternative to each mass flow controller having a separate third pressure sensor. Individual mass flow controller adjustment decisions may then proceed based upon the shared third pressure sensor signal. Each individual new embodiment mass flow controller may contain a dedicated supervision function which determines a course of action or a supervision function may be associated with and shared among all new embodiment mass flow controllers comprising a specific pallet group of MFCs.

A mass flow control apparatus comprising: a proportional valve upstream of a flow measurement portion, a pressure sensing element fluidly connected to determine a fluid pressure downstream of the flow measurement portion and a dynamically adjustable variable valve downstream of both the flow measurement portion and the pressure sensing element connection. Further the mass flow control apparatus comprising of a pressure-based flow sensor including a fluid conduit with fluidly coupled pressure and temperature sensing provisions upstream of a known flow restriction. Alternatively, the mass flow control apparatus includes a thermal-based flow sensor, which has fluid conduit with two spaced apart temperature responsive elements affixed to the exterior of the fluid conduit. Further the dynamically adjustable variable valve can be adjusted to any of at least two different amounts of openings, or continuously adjusted to a range of openings or adjusted to a provide a complete shut-off position.

A mass flow control apparatus includes, an inlet to a fluid pathway; a controllable shutoff valve, the controllable shutoff valve providing provisions for measuring a reference temperature (T0) and a reference pressure (P0) of a fluid contained within a reference volume of the fluid pathway; a proportional control valve, the proportional control valve providing provisions for measuring a first temperature (T1) and a first pressure (P1) of the fluid contained within the fluid pathway upstream of a flow restriction; the flow restriction providing provision for measuring a second pressure (P2) of the fluid contained within the fluid pathway downstream of the flow restriction; a variable valve; and an outlet from the fluid pathway. The flow restriction is chosen from group comprising of an orifice, a nozzle, a porous sintered metal element or a laminar flow structures. Further

the mass flow control apparatus includes a supervision function. The supervision function may choose an action from group comprising of self-calibration process, change of system parameter or storage of results.

A mass flow control apparatus including a mass flow controller further which includes a proportional valve upstream of a flow measurement portion; a dynamically adjustable variable valve downstream of the flow measurement portion a pressure sensing element fluidly connected to determine a fluid pressure downstream of the flow measurement portion and downstream of the variable valve. The mass flow control apparatus including the plurality of mass flow controllers; a plurality of gas species to feed reactants into a plurality of vacuum chambers.

A mass flow control apparatus including an inlet to a fluid pathway; a controllable shutoff valve, the controllable shutoff valve providing provisions for measuring a reference temperature (T0) and a reference pressure (P0) of a fluid contained within a reference volume of the fluid pathway; a proportional control valve, the proportional control valve providing provisions for measuring a first temperature (T1) and a first pressure (P1) of the fluid contained within the fluid pathway upstream of a flow restriction; the flow restriction, a variable valve providing provision for measuring a second pressure (P2) of the fluid contained within the fluid pathway downstream of the flow restriction and downstream of the variable valve; and an outlet from the fluid pathway.

A method for a mass flow control apparatus including determining a fluid pressure downstream of a flow sensor; responding to the fluid pressure downstream; and adjusting dynamically a variable valve downstream of the flow sensor to maintain desired operating conditions in the flow sensor; and maintaining and extending the useful operating range of the mass flow control apparatus. The method further includes a flow verification capability. The method further wherein the flow verification capability comprises the steps of: closing a shutoff valve to isolate a fluid pathway from an inlet while controlled mass flow continues through an outlet; making repeated measurements of a reference volume of a fluid pathway for a period of time; opening the shutoff valve to re-establish fluid pathway connection to the inlet; calculating a verified flow signal using pressure-volume-temperature methods; and providing a verified flow signal to a supervision function. Wherein the supervision function directs that a series of flow verification measurements be performed corresponding to different values of determined fluid pressures and fluid temperatures adjacent the flow restriction. Wherein the supervision function determines a calibration curve for a discrete flow restriction based on the flow signals generated by the flow verification measurements.

Referring to FIG. 7, FIG. 7 shows an apparatus 700 having a plurality of self-correcting mass flow controllers may be used with a plurality of gas species fed to a plurality of vacuum chambers 726, 748, and 764 for processing semiconductor devices within a single large apparatus often referred to as a "tool." A group ("pallet") of mass flow controllers (720, 732, 742, 754, 758, and 776) allow the simultaneous combination of several different gases into a single manifold (742, 744, and 760) which feeds a gas distribution structure ("showerhead") inside a vacuum chamber (726, 748 and 764). Insufficient conductance in the manifold plumbing may result in the downstream pressure, of a particular group of mass flow controllers, becoming too high to maintain choked flow conditions within one or more mass flow controllers within the group. The pressure within

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the manifold may be monitored using pressure sensor 724, pressure sensor 746 and pressure sensor 762 and a corresponding signal provided to all mass flow controllers within the group as an alternative to each mass flow controller having a separate third pressure sensor. Individual mass flow controller self-correction may then proceed based upon the shared third pressure sensor signal or according to commands emanating from the tool master control (a control system external to the control module of each mass flow controller).

FIG. 7 illustrates an apparatus 700 that includes various system including, a gas provider 702 and a gas provider 704. The apparatus 700 has a plurality of valves. 706, 708, 710, 712, 718, 730, 740, 752, 756, and 774. The apparatus 700 includes one or more pressure sensors to determine the flow rate of the gases. The pressure sensors 714, 716, 724, 746, 762, 770, and 772 may be used to determine the pressure outside of the MFCs 720, 732, 742, 754, 758, and 776.

Having thus described several aspects of at least one embodiment of this invention, it is to be appreciated various alterations, modifications, and improvements will readily occur to those skilled in the art. Such alterations, modifications, and improvements are intended to be part of this disclosure, and are intended to be within the scope of the invention. Accordingly, the foregoing description and drawings are by way of example only.

The invention claimed is:

1. A mass flow control apparatus comprising:
 - a control module configured to receive a first set point flow rate for delivering a fluid delivery to a tool;
 - a sensing element of the mass flow control apparatus to measure pressure of the fluid across a flow restrictor;
 - a solenoid valve to control the pressure such that a pressure drop across the flow restrictor yields a flow rate that is equal to the first set point flow rate; and
 - wherein the sensing apparatus is configured to measure the pressure of the fluid in a reference volume portion while the solenoid valve is closed.
2. The mass flow control apparatus of claim 1, further comprising a reference volume configured to verify an actual flow rate by closing a fluid flow and measuring a pressure in the reference volume.
3. The mass flow control apparatus of claim 1, wherein the solenoid valve is a proportional control valve.
4. The mass flow control apparatus of claim 1, wherein the solenoid valve is configured to adjust the pressure to the flow restrictor such that the pressure drop across the flow restrictor yields a flow rate that is equal to a second set point flow rate.
5. The mass flow control apparatus of claim 1, wherein solenoid valve is adjusted until the second set point flow rate is achieved.
6. The mass flow control apparatus of claim 1, wherein the solenoid valve can be adjusted to any of at least two different amounts of openings.
7. The mass flow control apparatus of claim 1, wherein the solenoid valve is a proportional control valve that can be continuously adjusted to a range of openings.

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8. The mass flow control apparatus of claim 1, wherein the flow restrictor is chosen from a group consisting of an orifice, a nozzle, a porous sintered metal element, laminar flow structures and tubes.

9. The mass flow control apparatus of claim 1, further comprising an additional pressure sensing element to measure supply pressure to the mass flow control apparatus.

10. The mass flow control apparatus of claim 1, wherein the control module determines that a pressure drop across the flow restrictor is sub-critical based on the measurement.

11. The mass flow control apparatus of claim 1, wherein the solenoid valve is upstream from the flow restrictor.

12. The mass flow control apparatus of claim 1, wherein the solenoid valve is a single valve that comprises both a proportional valve and a shut-off valve; and

wherein the solenoid valve is configured to close an inlet supply to perform a rate of decay measurement.

13. A mass flow control apparatus comprising:

a control module configured to receive a first set point flow rate for delivering a fluid delivery to a tool;

a sensing apparatus to measure a pressure of the fluid across a flow restrictor of the mass flow control apparatus;

a solenoid valve to control the pressure such that a pressure drop across the flow restrictor yields a flow rate that is equal to the first set point flow rate; and

wherein the sensing apparatus is configured to measure the pressure of the fluid in a reference volume portion while the solenoid valve is closed.

14. The mass flow control apparatus of claim 13, further comprising a reference volume portion for verifying an actual flow rate, wherein the sensing apparatus measures a pressure of a fluid in the reference volume portion.

15. The mass flow control apparatus of claim 13, wherein a reference volume portion is located upstream from the solenoid valve.

16. The mass flow control apparatus of claim 13, further comprising a shut-off valve, wherein the sensing apparatus is configured to measure the pressure of the fluid in a reference volume portion while the shut-off valve is closed.

17. A mass flow control apparatus comprising:

a control module configured to receive a first set point flow rate for delivering a fluid delivery to a tool;

a sensing element of the mass flow control apparatus to measure pressure of the fluid across a flow restrictor;

a solenoid valve to control the pressure to the flow restrictor such that a pressure drop across the flow restrictor yields a flow rate that is equal to the first set point flow rate; and

a shut-off valve to close an inlet supply,

wherein the sensing element is configured to measure the pressure of the fluid in a reference volume portion while the shut-off valve is closed.

18. The mass flow control apparatus of claim 17, further comprising a temperature sensor for measuring a temperature of a fluid.

19. The mass flow control apparatus of claim 17, wherein the control module is configured to enable additional self-calibration processes, change a system parameter, and store results.

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