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DESCRIPTION

[0001] The invention relates in general manner to vibratory machines for screening materials and/or for feeding materials, which machines include vibratory systems.

[0002] Vibratory systems are known in the state of the art that comprise two unbalanced shaft lines. Each unbalanced shaft line has a rotary shaft and an unbalance module constrained to rotate with said shaft. The shaft lines are driven in rotation so as to generate vibration for use in screening materials and/or for causing them to advance.

[0003] Nevertheless, driving rotation of unbalanced shaft lines in the systems known in the state of the art requires a large amount of energy. In addition, when stopping rotary drive, the vibration frequencies that are generated may include values that correspond to resonant frequencies of certain portions of the machine. In particular, the frequency of vibration may come close to the resonant frequency of damper elements on which the frame of the machine is mounted.

[0004] Document WO 2014/066573 A1 discloses a mechanical device such as a vibrating deliquifying screen which comprising circular force generators for creating at least one vibration profile in the mechanical device.

[0005] Document DE9416260 U1 discloses an adjustable vibrating mechanism that has a configuration in which vibrations are activated and a configuration in which vibrations are neutralised.

[0006] Document EP 0 505 976 A1 discloses a device for compensating a vibrational force F generated by a body, the device comprising four eccentric rotating weights located in a common plane containing the centre of gravity of said vibrating body.

[0007] Document WO 99/58258 A1 discloses a regulating device for an unbalanced mass vibration generator, comprising at least two pairs of partial unbalanced mass bodies that can be driven around an allocated axis whose vectorially added partial centrifugal force vectors form the resulting centrifugal force vector.

[0008] Document GB 1 301 855 A discloses a vibrator including a plurality of bobs rotatable about a common axis, in which driving means are provided for rotating said bobs in different directions, said driving means including transmission devices operable to alter the relative angular positions of the bobs while they are rotating such that a transition from substantially balanced to unbalanced rotation can be made.

[0009] Document US 2013/233101 A1 deals with an eccentric moment stepless adjustable vibrating mechanism, that enables to provide a 0 degree and a 180 degrees of phase difference between the eccentric blocks of an eccentric group of an upper layer and the

eccentric blocks of the eccentric group of a lower layer.

[0010] Document US 2007/120515 A1 discloses a vibrator comprising two pairs of unbalanced rotors driven in synchronous rotation by a first motor, and a second motor arranged to drive a phase shifter mechanism so as to adjust a phase difference between the first pair of rotors and the second pair of rotors.

[0011] US 2010/139424 A1 discloses a vibrator for a ground compaction apparatus said vibrator including two parallel shafts which are coupled to one another to be rotatable in opposite directions and on each of which is at least one unbalanced mass is disposed, and wherein a phase adjusting mechanism is used for modifying the phase angle of the two unbalanced masses relative to each other.

[0012] An object of the present invention is to propose a vibratory machine making it possible to reduce the energy needed to driving the unbalanced shaft lines and/or to reduce the risk of damage to all or part of the machine.

[0013] For this purpose, the invention provides a screening and/or feeder machine according to claim 1.

[0014] The claimed screening and/or feeder machine includes a vibratory system comprising shaft lines, each shaft line having an unbalance module, said vibratory system also having a drive device configured to drive the shaft lines in rotation in synchronous manner and in the same direction, said vibratory system being characterized in that it also comprises an angle modifier device configured to modify the angular position of the unbalance module of one shaft line relative to the angular position of the unbalance module of the other shaft line or of one of the other shaft lines.

[0015] In other words, the angle modifier device makes it possible to modify the angular position of the unbalance modules relative to each other when the vibratory system has two shaft lines, or to modify the angular positions of the unbalance modules relative to one another when the number of shaft lines is greater, e.g. three, four, or more. The shaft lines are parallel and are spaced apart from one another along a direction which is transversal, preferably orthogonal, to the longitudinal direction of said shaft lines. In other words, the shaft lines are not aligned with one another but are disposed side by side. The relative angular position of the unbalance modules is referred to as the angular configuration of the unbalance modules.

[0016] By way of example, when there are n shaft lines, a given angular configuration of the unbalance modules may be represented in the form of an $(n-1)$ -tuple of angle values, with each angle value of the $(n-1)$ -tuple corresponding to the angular phase difference, i.e. the angular position difference, between the unbalance module of a respective line and the unbalance module of a neighboring line.

[0017] The angular orientation axis of an unbalance module is defined as being the axis

intersecting and orthogonal to the axis of rotation of the unbalance module and passing through the center of gravity of the unbalance module. The angular position of an unbalance module corresponds to the angle between the angular orientation axis of the unbalance module and a reference axis that is orthogonal to and that intersects the axis of rotation of the unbalance module. Once a first reference axis has been defined for an unbalance module of a shaft line, the reference axis of the unbalance module of each other line is an axis that is orthogonal to and that intersects the axis of rotation of the unbalance module of said other line and that is parallel to said first reference axis.

[0018] The device may be configured to pivot the unbalance module of one, several, or each of the shaft lines, depending on the number of shaft lines provided, so as to modify the angular configuration of said unbalance modules of the shaft lines.

[0019] Such a design for the vibratory system of the invention in which the unbalanced shaft lines can be driven in rotation in the same direction and in which the unbalance module of at least one of the lines can be angularly adjusted, makes it possible to generate circular vibration of amplitude that is adjustable and with reduced energy consumption.

[0020] The angle modifier device serves to adjust the angular phase difference between the unbalance modules of the shaft lines during different operating sequences of the vibratory system.

[0021] Adjusting the angle of the unbalance module of at least one of the lines makes it possible in particular to reduce or even eliminate the static moment of the set of unbalance modules so that, when starting to drive rotation, the energy required for providing such drive is limited, and when stopping rotary drive, the risk of the system generating frequencies close to the resonant frequencies of certain portions of the system or of the corresponding machine is limited.

[0022] Thus, during a sequence of starting the system, the angle modifier device may be used to obtain a configuration in which the unbalance modules of the shaft lines are in phase opposition. When the vibratory system has two shaft lines, a configuration in phase opposition corresponds to an angular position difference of 180° between the two unbalance modules. In another example, when the vibratory system has three shaft lines, each having a respective unbalance module, a configuration in phase opposition corresponds to an angular position difference of 120° between the unbalance modules of the first and second lines, and to an angular position difference of 120° between the unbalance modules of the second and third lines. The static moment of the set of unbalance modules is then zero, thereby reducing the energy needed for driving the shaft lines in rotation.

[0023] During an operating sequence, also referred to as "production mode", the angle modifier device can be used to modify the angular configuration of the unbalance modules of the shaft lines so as to adapt the level of vibration to the quality and the quantity of material that is to be screened and/or caused to advance.

[0024] In order to stop the system, the angle modifier device may be used to bring the unbalance modules into phase opposition so as to limit any risk of all or part of the system or of the machine entering into resonance.

[0025] For this purpose, the vibratory system further comprises a control unit configured to control the drive device and the angle modifier device, the angle modifier device enabling the unbalance modules to take up an angular position relative to one or each of the others, according to which the unbalance modules are in phase, and another angular position relative to one or each of the others, according to which the unbalance modules are in phase opposition.

[0026] The control unit includes a processor and computer instructions which, when executed by the processor, causes the processor to:

- prior to driving the shaft lines in rotation by means of the drive device, bring the unbalance modules into phase opposition;
- drive the shaft lines in rotation by means of the drive device,
- until the unbalance modules have reached a given operating speed, keep the unbalance modules of the shaft lines in phase opposition;
- after said given speed of rotation has been reached for the shaft lines, bring the unbalance modules in phase;
- prior stopping rotary drive of the shaft lines, bring the unbalance modules into phase opposition, and stop the rotary drive of the shaft lines when said unbalance modules have been brought into phase opposition, and
- when rotation of the shaft lines is stopped, bring the unbalance modules in phase and into a low position.

[0027] According to an advantageous characteristic of the invention, the drive device comprises:

- a motor, referred to as the "main" motor, configured to drive one of the shaft lines in rotation; and
- a synchronous transmission mechanism configured to transmit rotation from the shaft line driven by the main motor to the other shaft line(s) so that said shaft lines rotate in synchronous manner and in the same direction.

[0028] According to an advantageous characteristic of the invention, the control unit is configured, while the shaft lines are being driven in rotation by the drive device, so as to modify the amplitude of the vibration by modifying the angular position of the unbalance module of one shaft line relative to the angular position of the unbalance module of the other shaft line or

of one of the other shaft lines.

[0029] According to an advantageous characteristic of the invention, the angle modifier device comprises a motor, referred to as the "adjustment" motor, and an epicyclic gear train, the epicyclic gear train comprising a sun gear connected to the outlet shaft of the adjustment motor, a toothed ring connected to one of the shaft lines, and planets mounted to mesh with the toothed ring and with the sun gear, the angle modifier device also comprising a planet carrier that carries the planets and that is coupled to rotate with the other shaft line.

[0030] According to an advantageous characteristic of the invention, the adjustment motor is configured in such a manner that its outlet shaft is suitable firstly for rotating in one direction in order to modify the angular position of an unbalance module, and secondly for preventing rotation in the opposite direction.

[0031] The invention also provides a method according to claim 6. The claimed method is a method of controlling the screening and/or feeder vibrator machine as claimed in claim 1.

[0032] According to an advantageous characteristic of the invention, while the shaft lines are being driven in rotation by the drive device, said method includes the step of modifying the amplitude of vibration by modifying the angular position of the unbalance module of one shaft line relative to the angular position of the unbalance module of the other shaft line or of one of the other shaft lines.

[0033] The invention can be well understood on reading the following description of embodiments, given with reference to the accompanying drawings, in which:

- Figure 1 is a diagrammatic side view of a machine in an embodiment of the invention;
- Figure 2 is a diagram of the vibratory system of the machine in an embodiment of the invention;
- Figure 3 is a perspective view of the vibratory system of the machine in an embodiment of the invention, the unit for controlling the motors being shown diagrammatically;
- Figure 3A is an exploded perspective view of the epicyclic gear train of the vibratory system of the machine in an embodiment of the invention;
- Figures 4 to 4E are diagrammatic end views of the unbalanced shaft lines of the vibratory system in an embodiment, shown at different instants, starting from the shaft lines being completely stopped, the shaft lines then being driven in rotation so as to reach a desired given speed;
- Figure 5 is a diagrammatic end view of the unbalanced shaft lines of the vibratory system of the machine in an embodiment, said view showing the angular phase difference introduced between the unbalance weights while they are rotating at a given speed; and

· Figures 6 to 6E are diagrammatic end views of the unbalanced shaft lines of the vibratory system of the machine in an embodiment, shown at different moments, starting with the shaft lines rotating at a desired given speed until they come to rest.

[0034] With reference to the figures and as mentioned above, the invention relates to a vibrator machine 6 for screening and/or moving materials, such as aggregates or ores.

[0035] Screening is an operation of grading materials depending on their grain size. The vibrator machine can thus be used to perform grain size classification or for feeding materials in various fields such as public works, buildings, mines, or quarries.

[0036] The machine 6 comprises a frame 60 and a surface 62 for screening and/or moving materials carried by said frame 60. Said surface may be made in the form of panels or plates, e.g. made of rubber, or a taut cloth. For screening, said surface presents through gaps and/or meshes of size appropriate for the desired type of screening.

[0037] The frame 60 of the machine 6 is arranged on damper means such as springs 61. The springs 61 then act as a suspension and they serve to isolate vibration. In other words, the machine comprises a frame 60 that is resiliently mounted.

[0038] The machine 6 has a vibratory system 7 that serves to generate vibration. The vibratory system 7 is arranged to cause the surface 62 to vibrate. In particular, the vibratory system comprises support elements (not shown) that are fastened to the frame 60 of the machine 6. The support elements carry bearings 56 for passing the shafts of unbalanced shaft lines of the vibratory system 7, as described below.

[0039] In the example shown in the figures, the vibratory system 7 thus includes two unbalanced shaft lines 1 and 2. In a variant, the vibratory system may have a larger number of shaft lines, e.g. three or four shaft lines, provided with respective unbalance modules. The shaft lines are parallel and preferably horizontal. Each unbalanced shaft line 1, 2 comprises a shaft or a plurality of shafts constrained to rotate with one another, and one or more unbalance modules 12, 21 mounted so as to be constrained to rotate with the corresponding shaft (s) of the line. Said shaft may then comprise a plurality of shaft fractions connected to one another, e.g. via universal joints, as in the example shown in Figure 4.

[0040] The term "unbalance" weight is used to mean a body mounted on a shaft line and having its center of gravity off-center relative to the axis of rotation of said shaft line. In the example shown in the figures, each unbalance module comprises a plurality of unbalance weights. In particular, an unbalance module may be constituted by a single unbalance weight.

[0041] In the example shown in the figures, each unbalance module 12, 21 comprises two pairs of unbalance weights. The two pairs of each unbalance module 12, 21 are distributed

spaced apart from one another along the shaft. The two pairs of each unbalance module 12, 21 are separated from each other by a universal joint 130, 230.

[0042] The two unbalance weights of a pair are separated from each other along the shaft line by a shaft bearing 56 secured via a support element (not shown) to the frame 60 of the machine 6. In the example of Figure 3, only one bearing 56 is shown for each shaft line.

[0043] In the example shown in Figure 1, the screening and/or movement surface 62 is sloping and offset from the plane containing the axes of rotation of the unbalanced shaft lines.

[0044] Said vibratory system 7 also has a motor 3, referred to as the "main" motor, in engagement with the first shaft line 1. In a variant that is not shown in the figures, the shaft line that is engaged with the main motor 3 could be the second shaft line 2. Said system also has a synchronous transmission mechanism 30 configured so that rotation of the shaft line 1 that is driven in rotation under the control of the main motor 3 is synchronous with and in the same direction as the direction of rotation of the second shaft line 2. Thus, the first and second shafts rotate at the same speed of rotation relative to each other, possibly being in-phase or out-of-phase, as a function of steps in the operation of the machine as described below.

[0045] The synchronous transmission system 30 is thus configured so that the unbalanced shaft lines are driven in rotation by the motor 3 at the same speed and in the same direction.

[0046] The synchronous transmission system 30 comprises a wheel 31 fastened to the outlet shaft of the main motor 3, a shaft 134 constrained to rotate with the shaft line 1, a wheel 13 secured to the shaft 134, and a transmission belt 100 between the wheel 31 and the wheel 13. The synchronous transmission system 30 also has a wheel 14 fastened to the shaft 134, and a wheel 45 coupled by a belt 101 to the wheel 14. The wheel 45 is carried by, but is suitable for rotating relative to, the outlet shaft 400 of a motor 41 that is referred to as the "adjustment" motor. The transmission system also has a toothed ring 424 coupled to rotate with planet gears 423 carried by the wheel 45 that constitutes a planet carrier. The shaft 134 and the ring 424 of the synchronous transmission system are connected respectively to the shaft lines 1 and 2 by the universal joints 130 and 230.

[0047] The ring 424, the planet gears 423, and the planet carrier 45 form part of an epicyclic gear train 42 that is described below. The epicyclic gear train has a sun gear 421 connected to the outlet shaft of the adjustment motor 41, that is described below. The epicyclic gear train also has the outer toothed ring 424, which is connected to the second shaft line 2, and planets 423 mounted to mesh with the toothed ring 424 and with the sun gear 421. The epicyclic gear train 42 also has a planet carrier 45 that carries the planets 423 so that rotation of the planet carrier 45 drives the planets 423 in rotation.

[0048] The vibratory system 7 has an angle modifier device 4 configured to modify the angular position of the unbalance module 21 of the second shaft line 2 relative to the angular position of the unbalance module 12 of the first shaft line 1. In a variant not shown in the figures, the

angle modifier device may be configured to modify the angular position of the unbalance module of the first shaft line or to modify the angular positions of each of said shaft lines. More generally, when the vibratory system 7 has a number n of shaft lines provided with respective unbalance modules, where n is greater than or equal to 2, it is possible to make provision for the angle modifier device to be configured to modify the angular positions of $n-1$ shaft lines in order to be able to modify the static moment of the set of unbalance modules, as described below.

[0049] In the example shown in the figures, the angle modifier device 4 comprises the epicyclic gear train 42 and the adjustment motor 41. The motor 41 presents an outlet shaft 400 having the sun gear 421 mounted thereon to rotate therewith.

[0050] Preferably, the adjustment motor 41 is a gear motor, i.e. a motor with a stepdown gear, thus enabling the outlet shaft of the adjustment motor 41 to rotate at a speed that is small compared with the speed of rotation of the motor 4, and with torque that is high.

[0051] As described in detail below, the adjustment motor 41 and the epicyclic gear train 42 serve to modify the angular position of the unbalance module 21 of the shaft line 2, thereby introducing an angular phase difference between the unbalance module 21 of the second shaft line 2 and the unbalance module 12 of the first shaft line 1, or enabling them to be brought into phase, i.e. into the same angular position.

[0052] Below, the orientation axis O12 or O21 of an unbalance weight of a shaft line 1, 2 is defined as being the axis perpendicular to the axis of the shaft line and passing through the center of gravity of said unbalance weight and through the axis of said shaft line.

[0053] The angular phase difference between the unbalance modules, or indeed the angular position difference between the unbalance modules, corresponds to the difference between the angular position of one unbalance module and the angular position of the other unbalance module.

[0054] The angular position of an unbalance module is defined as the angle A12, A21, referred to as the "orientation" angle, that is formed in one direction between firstly a given reference axis perpendicularly intersecting the axis of rotation of said unbalance module (i.e. the axis of the corresponding shaft) and secondly the orientation axis O12, O21 of said unbalance module, as defined above.

[0055] Said orientation angle lies in a plane perpendicular to the axes of rotation of the shaft lines. In the embodiment shown in Figure 4C, which is an end view of the shaft lines, i.e. in a plane perpendicular to their axes of rotation, the reference axis for each unbalance module 12, 21 is selected as being the portion of the vertical axis V12, V21 that intersects the axis of rotation of said unbalance module and that extends below said axis of rotation. In addition, in the embodiment shown in Figure 4C, said orientation angle is defined in the counterclockwise direction, going from the reference axis to the orientation axis of the unbalance weight.

[0056] In other words, the angular phase difference between the unbalance modules 12, 21 corresponds to the difference between their orientation angles A12 and A21.

[0057] In the embodiment shown in the figures, for a given shaft line, the unbalance weights of the line have the same angular position from one weight to another, such that the angular orientation of an unbalance weight of a shaft line corresponds to the angular orientation of the unbalance module of said line. When an unbalance module has unbalance weights that are at different angular phases relative to one another, it may be considered that the angular position of the unbalance module corresponds to the mean of the orientation angles of the unbalance weights of the unbalance module.

[0058] The angle modifier device 4 thus serves to bring the unbalance modules 21, 12 into a first angular configuration, e.g. into phase opposition, so that the set of unbalance modules presents a static moment of a first value. The angle modifier device 4 also makes it possible to bring the unbalance modules into a second angular configuration, e.g. in-phase, so that the set of unbalance modules presents a static moment of a second value that is smaller than said first value.

[0059] In order to adjust the angular position of the unbalance module 21, the motor 41 operates at low speed with high torque. The motor 41 is configured so that rotation of its output shaft 400 is irreversible, so that when the desired angular phase difference between the unbalance modules is reached, rotation of the sun gear 421 is prevented, since otherwise that would modify the angular orientation of the unbalance module 21 of the line 2 in unwanted manner.

[0060] The vibratory system 7 includes a control unit 700. The control unit is a unit of electronic and/or computer type, e.g. comprising a microcontroller or a microprocessor associated with a memory. Advantageously, the vibratory system also comprises a detector system for detecting the angular positions of the unbalance modules of the shaft lines. The detector system may comprise one or more sensors connected to the control unit in order to determine the angular phase difference between the unbalance modules of the shaft lines. The sensor(s) may be configured to detect the relative angular position between the unbalance modules or to determine the pivot angles of the or each shaft line controlled by the angle modifier device 4. Thus, in the embodiment shown in the figures, the motor 41 may be fitted with an angle measuring system for measuring the pivot angle of its outlet shaft and for deducing therefrom the angular phase difference that exists between the unbalance modules of the shaft lines.

[0061] Thus, when it is stated that the unit or means of the unit are configured to perform a given operation, it should be understood that the unit has computer instructions and corresponding execution means that enable said operation to be performed.

[0062] In particular, the control unit 700 includes instructions for controlling the speed of

rotation of the main motor 3 and the angle of rotation of the outlet shaft 400 of the motor 41.

[0063] When the vibratory system is stationary and in order to put it into operation, the control unit 700 is configured to execute the following steps. Initially, the unbalance modules 12 and 21 of the first and second shaft lines 1 and 2 are stationary and in the same angular position, i.e. in-phase, and preferably in a low position, as shown in Figure 4.

[0064] In a first step, shown in Figure 4A, the angular position of the unbalance module 21 of the second shaft line 2 is modified by using the motor 41 so that the unbalance module 21 is taken to an angular position referred to as the "starting" angular position, that is different from the angular position of the unbalance module 12 of the first shaft line 1. Relatively to a given reference axis which is parallel to the axes of rotation of the lines, in the starting position, the static moment of the set of unbalance modules, referred to as the "total" static moment, is thus less than the moment corresponding to a configuration of the unbalance modules in which they present the same angular position. In this example, the values of the total static moments are considered as absolute values. The energy needed by the motor 3 for driving rotation of the unbalanced shaft lines is thus reduced.

[0065] The static moment of the set of unbalance modules 12 and 21, referred to as the "total" static moment, is defined relative to an axis parallel to the axes of rotation of the lines, coplanar therewith, and situated at equal distances from these two axes of rotation. When the number n of parallel and coplanar shaft lines is greater than two, the static moment of the set of unbalance modules, referred to as the "total" static moment, can be defined relative to an axis parallel to the axes of rotation of the lines, coplanar therewith, and situated at equal distances from the two shaft lines that are furthest apart.

[0066] Preferably, the unbalance modules 12 and 21 are put into phase opposition, as shown in Figure 4B. The total static moment is then zero.

[0067] The control unit 700 then causes the first and second shaft lines 1 and 2 to be rotated by the motor 3 in order to reach a given speed, referred to as the "nominal" operating speed, as shown in Figure 4C. During this step, i.e. until they have reached the nominal operating speed, the unbalance modules of the shaft lines are kept in phase opposition.

[0068] Thereafter, the control unit controls the motor 41 so that, as shown in Figure 4D, the angular position of the unbalance module 21 of the second shaft line 2 is modified in order to bring the unbalance modules into an angular position, referred to as the "vibratory" angular position, in which the total static moment is greater than that corresponding to said starting angular position. As shown in Figure 4E, the unbalance module 21 is preferably put into the same angular position as the unbalance module 12. Thus, in the operating step shown in Figure 4E, the vibratory system is operating at the nominal speed of rotation and with an amplitude of vibration that is at a maximum since the unbalance modules of both lines are in-phase.

[0069] The control unit 700 can cause the amplitude of vibration to be modified by modifying the angular position of the unbalance module 21 of the second shaft line 2 relative to the angular position of the unbalance module 12 of the first shaft line 1.

[0070] The amplitude of vibration of the vibratory system can be reduced, as shown in Figure 5, by introducing an angular phase difference between the unbalance modules. As explained above, the angular phase difference is introduced by controlling the motor 41 in such a manner as to cause the sun gear 421 of the epicyclic gear train to turn through a desired angle. The amplitude of vibration can thus be adjusted progressively to a value lying in the range 0 to 100%.

[0071] In order to stop the vibratory system while the two shaft lines are being driven in rotation by the motor 3 at the nominal operating speed and in-phase, as shown in Figure 6, the control unit performs the following steps corresponding to steps that are the inverse of those described above with reference to Figures 4 to 4E.

[0072] In the step shown in Figure 6A, the motor 41 modifies the angular position of the unbalance module 21 of the second shaft line 2 until the angular positions of the unbalance modules 12 and 21 of the first and second lines 1 and 2 are in opposition (Figure 6B). The amplitude of vibration is then at a minimum. Thereafter, as shown in Figure 6C, the rotary drive of the shaft lines 1 and 2 is stopped so that the shaft lines cease turning without running any risk of causing some or all of the machine to enter resonance. Thereafter, as shown in Figures 6D and 6E, the unbalance module 21 is pivoted by the motor 41 so as to modify its angular position and preferably, as shown in Figure 6E, so as to bring it into the same angular position as the unbalance module 12. In particular, the unbalance modules are brought into a low position such that the potential energy of these unbalance modules is zero, thereby making it possible to act in safe manner on the system, e.g. for maintenance purposes.

[0073] The present invention can advantageously be used for screening materials in mines and quarries, and/or for feeding a machine for processing said materials.

[0074] The person skilled in the art readily understands that the various steps and functions of the embodiments described above can be performed by means of computer programs. In particular, the above-described steps may be embodied in the form of electronic and/or computer instructions that are executable by the control unit 700. In particular, the functions executed by the control unit may be embodied in the form of a set of computer instructions executed by a processor of the control unit 700.

[0075] The computer programs or computer instructions may be contained in program storage devices, for example computer readable digital data storage media, or executable programs. The programs or instructions may also be executed from program storage peripherals.

[0076] Although at least one embodiment of the invention is shown and described, it should be observed that other modifications, substitutions, and alternatives, will appear to the person

skilled in the art and can be changed without going beyond the scope of the invention, as defined by the appended claims.

REFERENCES CITED IN THE DESCRIPTION

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P A T E N T K R A V

1. En sigte- og/eller fødevibratormaskine (6), der indbefatter:

- et vibratorsystem (7) omfattende aksellinjer (1, 2), hvor hver aksellinje (1, 2) har et ubalancemodul (12, 21), hvilket vibratorsystem (7) har også en drivanordning konfigureret til at drive aksellinjerne (1, 2) i rotation på synkron måde i den samme retning, hvilket vibratorsystem (7) omfatter en vinkelmodifikationsanordning (4) konfigureret til at modificere vinkelpositionen af ubalancemodulet (21) af en aksellinje (2) relativ til vinkelpositionen af ubalancemodulet (12) af den anden aksellinje (1) eller af en af de andre aksellinjer;
- hvor vibratorsystemet (7) også omfatter en styringsenhed (700) konfigureret til at styre drivanordningen og vinkelmodifikationsanordningen (4), hvor vinkelmodifikationsanordningen (4) muliggør ubalancemodulerne (12, 21) at indtage en vinkelposition relativ til en eller hver af de andre, i hvilken ubalancemodulerne er i fase og en anden vinkelposition relativ til en eller hver af de andre, i hvilken ubalancemodulerne er i modfase; k e n d e - t e g n e t ved, at styringsenheden (700) indbefatter en processor og computerinstruktioner, hvilke, når de udføres af processoren, får processoren til:
- før aksellinjerne (1, 2) drives i rotation ved hjælp af drivanordningen, at bringe ubalancemodulerne (12, 21) i modfase;
 - at drive aksellinjerne (1, 2) i rotation ved hjælp af drivanordningen;
 - indtil ubalancemodulerne har nået en given driftshastighed, at holde ubalancemodulerne af aksellinjerne (1, 2) i modfase;
 - efter den givne driftshastighed for aksellinjerne (1, 2) er nået, at bringe ubalancemodulerne (21, 12) i fase;
 - før rotationsdrev af aksellinjerne (1, 2) stoppes, at bringe ubalancemodulerne (21, 12) i modfase og at stoppe rotationsdrevet af aksellinjerne (1, 2) når ubalancemodulerne (21, 12) er blevet bragt i modfase, og
 - når rotation af aksellinjerne (1, 2) er stoppet, at bringe ubalancemodulerne (21, 12) i fase og i en lav position.

2. Sigte- og/eller fødevibratormaskine (6) ifølge krav 1, k e n d e t e g n e t ved, at drivanordningen omfatter:

- en motor (3), omtalt som "hovedmotoren", konfigureret til at drive en af aksellinjerne (1) i rotation; og
- en synkron transmissionsmekanisme (30) konfigureret til at transmittere rotation fra lineakslen (1), der drives af hovedmotoren (3), til den anden aksellinje / de andre aksellinjer (2) sådan at nævnte aksellinjer (1, 2) roterer synkront i den samme omdrejningsretning.

3. Sigte- og/eller fødevibratormaskine (6) ifølge et hvilket som helst af kravene 1 til 2, k e n d e t e g n e t ved, at styringsenheden (700) yderligere omfatter

computerinstruktioner, hvilke, når de udføres af processoren, får processoren til: mens aksellinjerne (1, 2) drives i rotation af drivanordningen, at modificere amplituden af vibrationen ved at modificere vinkelpositionen af ubalancemodulet (21) af en aksellinje (2) relativt til vinkelpositionen af ubalancemodulet (12) af den anden aksellinje (1) eller en af de andre aksellinjer.

4. Sigte- og/eller fødevibratormaskine (6) ifølge et hvilket som helst af kravene 1 til 3, *k e n d e t e g n e t* ved, at vinkelmodifikationsanordningen (4) omfatter en motor (41), omtalt som justeringsmotoren, og et planetgear (42), hvor planetgearet (42) omfatter et solhjul (421) forbundet med udgangsakselen af justeringsmotoren (41), et forandret ringhjul (424) forbundet med en af aksellinjerne (2), og planeter (423) monteret til at indgribe med det forandrede ringhjul (424) og med solhjulet (421), hvor vinkelmodifikationsanordningen (4) også omfatter en base (45), som bærer planeterne (423), og som er koblet til at rotere med den anden aksellinje (1).

5. Sigte- og/eller fødevibratormaskine (6) ifølge krav 4, *k e n d e t e g n e t* ved, at justeringsmotoren (41) er konfigureret på en sådan måde, at dens udgangsaksel (400) er egnet for det første til at rotere i en retning for at ændre vinkelpositionen af et ubalancemodul (21), og for det andet til at forhindre rotation i modsatte retning.

6. Fremgangsmåde for at styre en sigte- og/eller fødevibratormaskine (6) ifølge et hvilket som helst af kravene 1 til 5, hvilken fremgangsmåde er *k e n d e t e g n e t* ved, at den omfatter mindst et trin at modificere vinkelpositionen af et ubalancemodul (21) relativt til vinkelpositionen af det andet ubalancemodul / de andre ubalancemoduler (12);

hvor fremgangsmåden omfatter trinnene:

- før aksellinjerne (1, 2) drives i rotation ved hjælp af drivanordningen, at bringe ubalancemodulerne (12, 21) i modfase;
- at drive aksellinjerne (1, 2) i rotation ved hjælp af drivanordningen;
- indtil ubalancemodulerne har nået en given driftshastighed, at holde ubalancemodulerne af aksellinjerne (1, 2) i modfase;
- efter den givne driftshastighed for aksellinjerne (1, 2) er nået, at bringe ubalancemodulerne (21, 12) i fase;
- før rotationsdrev af aksellinjerne (1, 2) stoppes, at bringe ubalancemodulerne (21, 12) i modfase og at stoppe rotationsdreven af aksellinjerne (1, 2), når ubalancemodulerne (21, 12) er blevet bragt i modfase, og
- når rotation af aksellinjerne (1, 2) er stoppet, at bringe ubalancemodulerne (21, 12) i fase og i en lav position.

7. Fremgangsmåde ifølge krav 6, hvilken fremgangsmåde er *k e n d e t e g n e t* ved, at mens aksellinjerne (1, 2) drives i rotation ved hjælp af drivanordningen,

indbefatter fremgangsmåden trinene at modificere amplituden af vibration ved at modificere vinkelpositionen af ubalancemodulet (21) af en aksellinje (2) relativt til vinkelpositionen af ubalancemodulet (12) af den anden aksellinje (1) eller en af de andre aksellinjer.

DRAWINGS

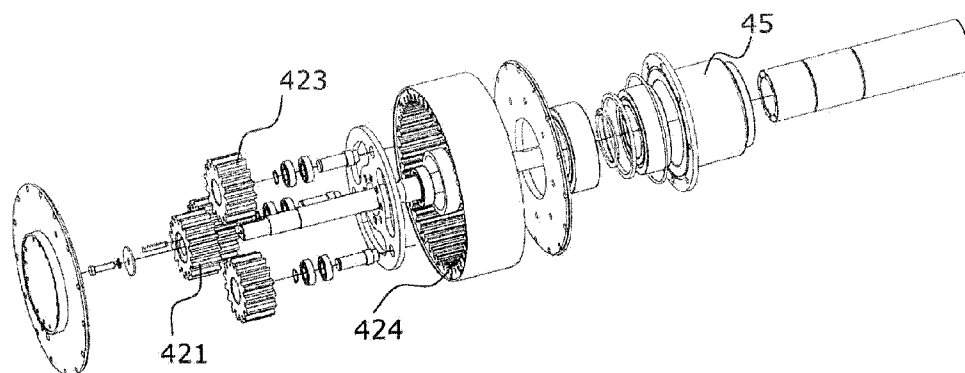
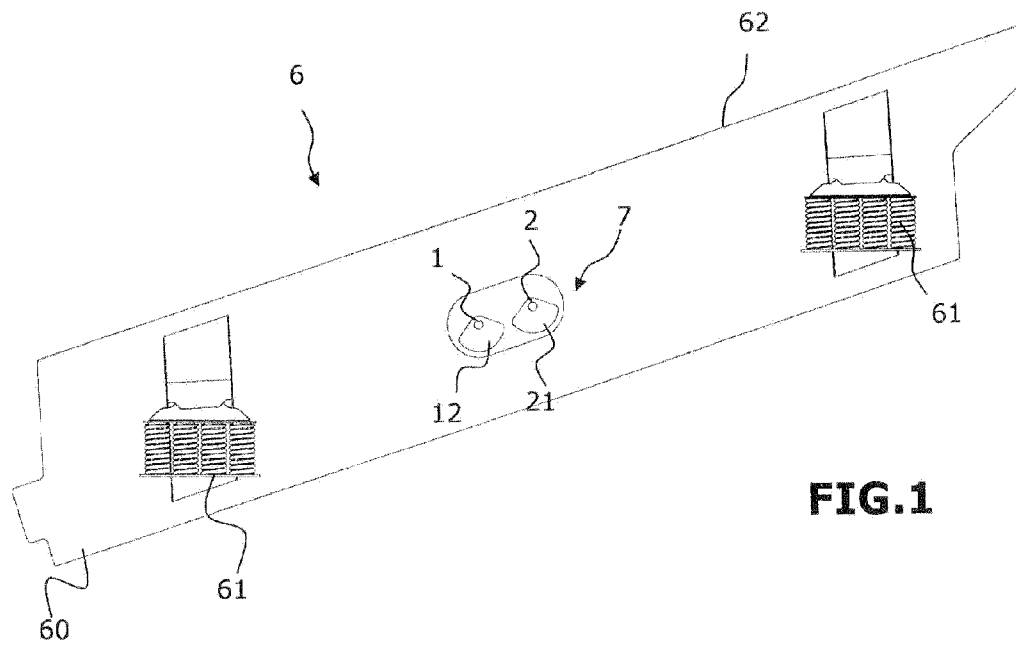


FIG. 3A

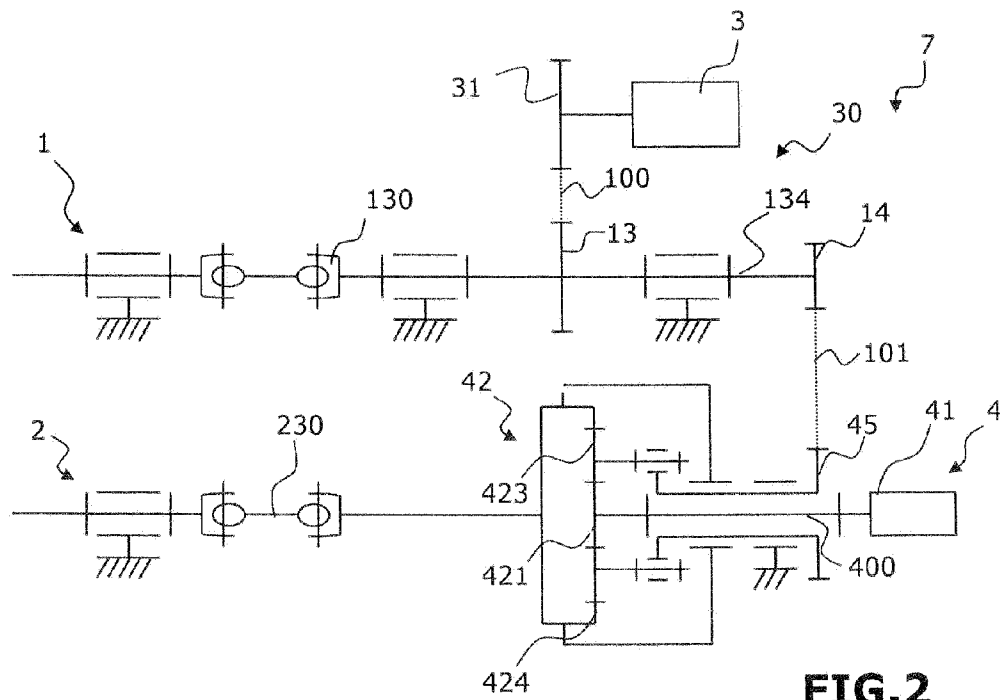


FIG. 2

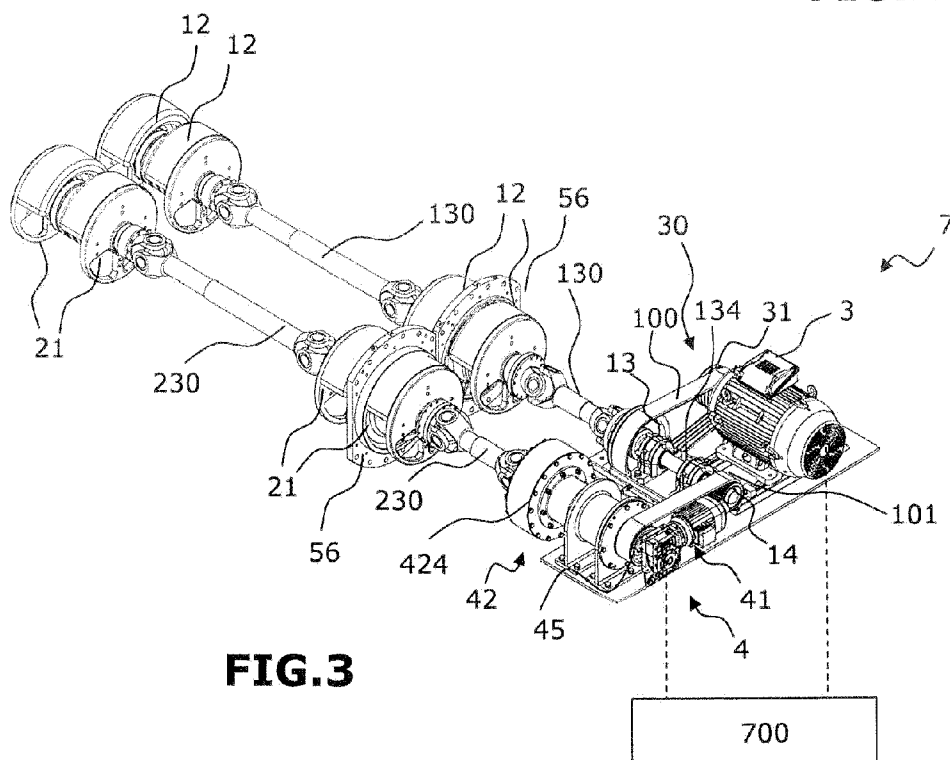


FIG. 3

700

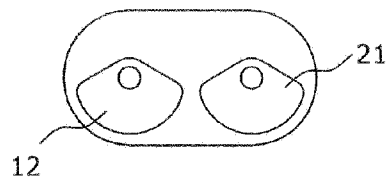


FIG. 4

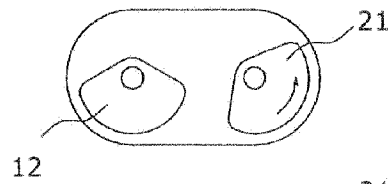


FIG. 4A

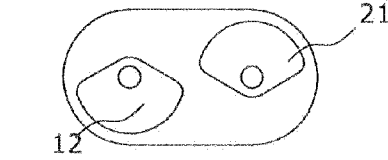


FIG. 4B

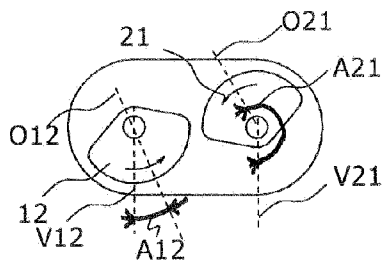


FIG. 4C

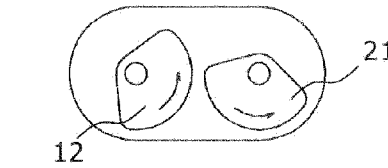


FIG. 4D

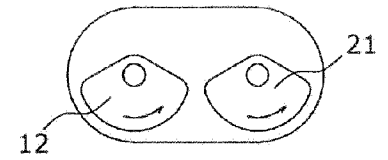


FIG. 4E

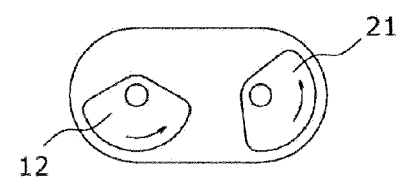


FIG. 5

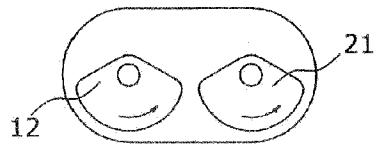


FIG. 6

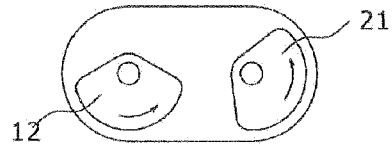


FIG. 6A

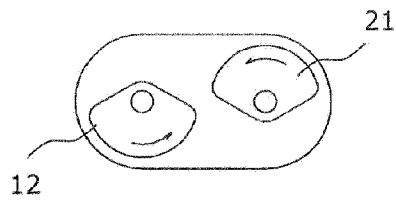


FIG. 6B

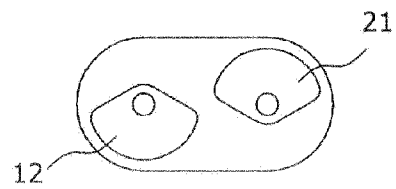


FIG. 6C

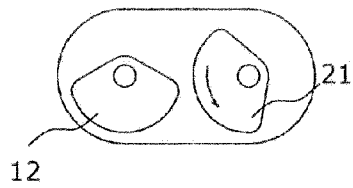


FIG. 6D

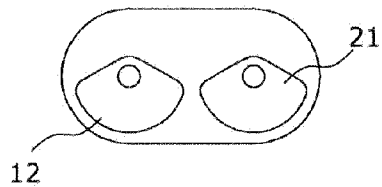


FIG. 6E