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(54) Title: STARTER SOLENOID WITH SPOOL FOR RETAINING COILS

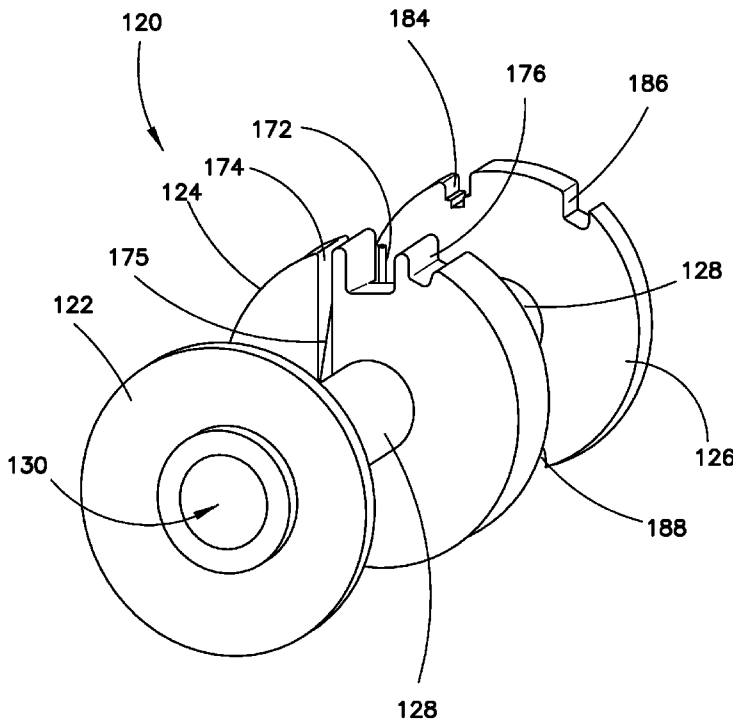


FIG. 7

(57) Abstract: A solenoid for a vehicle starter comprises a spool including a first coil bay, a second coil bay, and an interior passage defining an axial direction. A first coil is positioned in the first coil bay of the spool, and a second coil positioned in the second coil bay of the spool. A plunger is positioned within the interior passage of the spool and configured to move in the axial direction when the first coil is energized. The first coil bay is positioned adjacent to the second coil bay in the axial direction. The spool further includes two end flanges and a middle flange. The middle flange separates the first coil bay from the second coil bay.

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## STARTER SOLENOID WITH SPOOL FOR RETAINING COILS

### FIELD

[0001] This application relates to the field of vehicle starters, and more particularly, to solenoids for starter motor assemblies.

### BACKGROUND

[0002] Starter motor assemblies that assist in starting engines, such as engines in vehicles, are well known. A conventional starter motor assembly is shown in FIG. 15. The starter motor assembly 200 of FIG. 15 includes a solenoid 210, an electric motor 202, and a drive mechanism 204. The solenoid 210 includes a coil 212 that is energized by a battery upon the closing of an ignition switch. When the solenoid coil 212 is energized, a plunger 216 moves in a linear direction, causing a shift lever 205 to pivot, and forcing a pinion gear 206 into engagement with a ring gear of a vehicle engine (not shown). When the plunger 216 reaches a plunger stop, electrical contacts are closed connecting the electric motor 202 to the battery. The energized electric motor 202 then rotates and provides an output torque to the drive mechanism 204. The drive mechanism 204 transmits the torque of the electric motor through various drive components to the pinion gear 206 which is engaged with the ring gear of the vehicle engine. Accordingly, rotation of the electric motor 202 and pinion 206 results in cranking of the engine until the engine starts.

[0003] Many starter motor assemblies, such as the starter motor assembly 200 of FIG. 15 are configured with a “soft-start” starter motor engagement system. The intent of a soft start starter motor engagement system is to mesh the pinion gear of the starter into

the engine ring gear before full electrical power is applied to the starter motor. If the pinion ring gear abuts into the ring gear during this engagement, the motor provides a small torque to turn the pinion gear and allow it to properly mesh into the ring gear before high current is applied. The configuration of the solenoid, shift yoke, electrical contacts, and motor drive are such that high current is not applied to the motor before the gears are properly meshed. Accordingly, milling of the pinion gear and the ring gear is prevented in a starter motor with a soft-start engagement system.

**[0004]** Starters with a soft start engagement system, such as that of FIG. 15, typically include a solenoid with two distinct coils. The first coil is a pull-in coil 212 and the second coil is a hold in coil 214. As shown in FIG. 15, the pull-in coil 212 is wound first on the spool 220. On top of this winding the hold-in coil 214 is wound. Sometimes this order is reversed such that the hold-in coil 214 is wound first on the spool 220 followed by the pull-in coil 212.

**[0005]** During operation of the starter, the closing of the ignition switch (typically upon the operator turning a key) energizes both the pull-in coil 212 and the hold-in coil 214. Current flowing through the pull-in coil 212 at this time also reaches the electric motor 202, applying some limited power to the electric motor, and resulting in some low torque turning of the pinion. Energization of the pull-in coil 212 and hold-in coil 214 moves a solenoid shaft (also referred to herein as the “plunger”) in an axial direction. The axial movement of the solenoid plunger moves the shift lever 205 and biases the pinion gear 206 toward engagement with the engine ring gear. Once the solenoid plunger reaches the plunger stop, a set of electrical contacts is closed, thereby delivering full power to the electrical motor. Closing of the electrical contacts effectively short circuits

the pull-in coil 212, eliminating unwanted heat generated by the pull-in coil. However, with the pull-in coil is shorted, the hold-in coil 214 provides sufficient electromagnetic force to hold the plunger in place and maintain the electrical contacts in a closed position, thus allowing the delivery of full power to continue to the electric motor 202. The fully powered electric motor 202 drives the pinion gear 206, resulting in rotation of the engine ring gear, and thereby cranking the vehicle engine.

**[0006]** After the engine fires (i.e., vehicle start), the operator of the vehicle opens the ignition switch. The electrical circuit of the starter motor assembly is configured such that opening of the ignition switch causes current to flow through the hold-in coil and the pull-in coil in opposite directions. The pull-in coil 212 and the hold-in coil 214 are configured such that the electromagnetic forces of the two coils 212, 214 cancel each other upon opening of the ignition switch, and a return spring forces the plunger 216 back to its original un-energized position. As a result, the electrical contacts that connected the electric motor 202 to the source of electrical power are opened, and the electric motor is de-energized.

**[0007]** In order to produce a high performing vehicle starter with a soft start motor engagement system, such as that described above, designers are faced with numerous design challenges. First, the pull-in coil must be properly designed to avoid various issues that may arise during operation of the starter. As described above, when the pull-in coil of a soft-start starter motor engagement system is energized (i.e., when the ignition switch contacts close due to operator turning engine switch key on), the pull-in coil provides electromagnetic force to pull the plunger toward the plunger stop and to the closed position. However, the pull-in coil is connected electrically in series with the

starter motor, and should only have a low resistance. With low resistance through the pull-in coil, sufficient current flows through the pull-in coil and to the electric motor such that the electric motor can deliver a sufficient output torque to rotate the pinion gear and avoid abutment with the ring gear, as described previously. This required torque is typically 8- 12 N-m. For a 12V motor, the resistance may be on the order of 0.030 ohms so that several hundred amps flow through the motor, and also the series connected pull-in coil, during soft start. However, this low of resistance of the pull-in coil creates other design challenges. First, if the soft start period is prolonged, or repetitive starts are performed, a high amount of ohmic heat is generated in the pull-in coil because of the large amount of current flowing through the pull-in coil. For a 12V system this can be on the order of 3-4 kW, and this can lead to thermal failure of the insulation system of the wiring that forms the coils. Second, the large current through the pull-in coil creates a much stronger electromagnetic force on the plunger during closure than is needed. This may become a problem when an abutment between the pinion gear and ring gear occurs, and the impact force of the pinion gear on the ring gear can exceed 4500N. As a result, the ring gear could fracture or chip. Over time and thousands of starts, the surface of the ring gear may deteriorate and require replacement for proper starting.

**[0008]** Design challenges related to the pull-in coil, such as those discussed in the preceding paragraph result in additional design challenges with respect to other components of the starter, such as the hold-in coil. For example, as discussed in the previous paragraph, the pull-in coil has specific design limitations related to the current flowing through the pull-in coil. Since the electromagnetic excitation is the product of coil turns times current, and since current is fixed, this generally leaves the number of

turns of the pull-in coil as the primary design variable for the pull-in coil. While the number of turns of the pull-in coil can be reduced to reduce the impact abutment force issue described previously, this presents a problem with the hold-in coil. In particular, the number of turns in the hold-in coil should match the pull-in coil so that during disengagement of the pinion gear and the ring gear following vehicle start, the electromagnetic forces of the two coils will cancel each other and allow the pinion gear to pull cleanly out of the ring gear. However, before vehicle start, the hold-in coil stays energized for a much longer period of time than the pull-in coil. Therefore, the hold-in coil should not be of low resistance or it will thermally fail. Thus, the resistance of the hold-in coil generally is an order of magnitude higher than that of the pull-in coil. The high resistance of the hold-in coil means that current flow through the hold-coil before start is relatively low, resulting in a relatively low amp-turn product. If the number of turns of the hold-in coil is too low, then the hold-in coil will deliver an insufficient magnetic force to hold the plunger closed and the starter motor will disengage before vehicle start.

**[0009]** As explained in the previous paragraphs, designers of vehicle starters with soft start motor engagement systems are faced with opposing design challenges for two coils that should produce equivalent electromagnetic forces. On the one hand designers strive to limit the turns of the pull-in coil in order to reduce the impact force during engagement of the pinion gear and the ring gear. On the other hand designers strive to increase the turns of the hold-in coil such that the hold-in coil delivers sufficient electromagnetic force to maintain the plunger in a closed position during engine cranking. Accordingly, it would be desirable to provide a solenoid for a vehicle starter

with a pull-in coil that limits the impact force during engagement of the pinion gear and the ring gear. It would also be desirable to provide a hold-in coil for the solenoid that delivers sufficient electromagnetic force to maintain the plunger in a closed position during engine cranking. Additionally, it would be desirable if such a solenoid were relatively simple in design and inexpensive to implement.

#### SUMMARY

**[0010]** In accordance with one embodiment of the disclosure, there is provided a solenoid for a vehicle starter. The solenoid comprises a spool including a first coil bay, a second coil bay, and an interior passage defining an axial direction. A first coil is positioned in the first coil bay of the spool, and a second coil positioned in the second coil bay of the spool. A plunger is positioned within the interior passage of the spool and configured to move in the axial direction when the first coil is energized. In at least one embodiment of the solenoid, the first coil bay is positioned adjacent to the second coil bay in the axial direction.

**[0011]** In at least one alternative embodiment, the spool of the solenoid includes a middle flange separating the first coil bay from the second coil bay. The spool may further include two end flanges, and wherein the middle flange is not centered on the spool between the two end flanges such that the first bay and the second bay are of different lengths. Additionally the center flange of the spool may be thicker than each of the two end flanges. One or more of the flanges may include a plurality of coil mounting features positioned along the outer perimeter of the flange.

[0012] In at least one alternative embodiment, the solenoid is provided as part of a vehicle starter including an electric motor configured to be energized by a source of electric power when the solenoid is energized.

[0013] The above described features and advantages, as well as others, will become more readily apparent to those of ordinary skill in the art by reference to the following detailed description and accompanying drawings. While it would be desirable to provide a solenoid that provides one or more of these or other advantageous features, the teachings disclosed herein extend to those embodiments which fall within the scope of the appended claims, regardless of whether they accomplish one or more of the above-mentioned advantages.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0014] FIG. 1 shows a schematic diagram of a vehicle starter including a motor and solenoid;

[0015] FIG. 2 shows a perspective view of a spool, pull-in coil, and hold-in coil of the solenoid of FIG. 1;

[0016] FIG. 3 shows a diagram illustrating lines of magnetic flux through the solenoid when the pull-in coil and hold-in coil of FIG. 2 are energized and the plunger is removed from a plunger stop;

[0017] FIG. 4 shows a diagram illustrating lines of magnetic flux through the solenoid when the pull-in coil and hold-in coil of FIG. 2 are energized and the plunger is in transition toward the plunger stop;

[0018] FIG. 5 shows a diagram illustrating lines of magnetic flux through the solenoid when only the hold-in coil of FIG. 2 is energized and the plunger is engaged with the plunger stop;

[0019] FIG. 6 shows a cross-sectional view of the spool of FIG. 2 taken along a centerline of the spool;

[0020] FIG. 6A shows a cross-sectional view of the spool along line A-A of FIG. 6, illustrating one side of a middle flange of the spool;

[0021] FIG. 6B shows a cross-sectional view of the spool along line B-B of FIG. 6, illustrating another side of the middle flange of the spool;

[0022] FIG. 6C shows an side view of the spool along line C-C of FIG. 6, illustrating an end flange of the spool;

[0023] FIG. 7 shows a perspective view of an alternative embodiment of the spool of FIG. 2;

[0024] FIG. 8 shows the spool of FIG. 7 with the hold-in coil being wound in one direction on a second coil bay of the spool;

[0025] FIG. 9 shows the spool of FIG. 8 with the hold-in coil being wound in an opposite direction on the second coil bay of the spool;

[0026] FIG. 10 shows the spool of FIG. 9 with the hold-in coil completely wound on the second coil bay of the spool;

[0027] FIG. 11 shows the spool of FIG. 10 with the pull-in coil being wound on a first coil bay of the spool;

[0028] FIG. 12 shows the spool of FIG. 11 with the pull-in coil completely wound on the first coil bay of the spool;

[0029] FIG. 13 shows a cross-sectional view of the spool along line D-D of FIG. 12, including the hold-in coil and pull-in coil positioned on the spool;

[0030] FIG. 14 shows a cross-sectional view of an alternative embodiment of the spool, hold-in coil and pull-in coil of FIG. 13; and

[0031] FIG. 15 shows a cutaway view of a conventional starter motor with a soft start starter motor engagement system

## DESCRIPTION

### [0032] General Starter Arrangement

[0033] With reference to FIG. 1, in at least one embodiment a starter 100 for a vehicle comprises an electric motor 102 and a solenoid 110. Although not shown in the FIG. 1, the starter 100 also includes a drive mechanism and pinion gear, similar to the conventional starter assembly 200 described above with reference to FIG. 15. The electric motor 102 in the embodiment of FIG. 1 is positioned in a motor circuit 104 that is configured to connect the motor to the vehicle battery (not shown) via the B+ terminal. The solenoid 110 is positioned in the motor circuit 104 to facilitate connection of the motor to the vehicle battery. The solenoid includes a pull-in coil 112, a hold-in coil 114, a plunger 116, and an ignition switch 118.

[0034] The motor circuit 104 of FIG. 1 includes a first current path 106 and a second current path 108 configured to provide electrical power to the electric motor 102. The first current path 106 begins at the B+ terminal, travels across the contacts 119 of the ignition switch 118, continues to node 115, travels through the pull-in coil, and ends at

the input terminal 103 of the electric motor 102. Accordingly, this first current path 106 is only a closed path when the contacts 119 of the ignition switch 118 are closed.

**[0035]** The second current path 108 begins at the B+ terminal, travels across the motor contacts 117 associated with the plunger 116 and ends at the input terminal 103 of the electric motor 102. Accordingly, this second current path 108 is only a closed path when the plunger 116 has closed the motor contacts 117. Moreover, when the second current path 108 is closed, the first current path 106 is shorted by the second current path 108, and no current flows through the pull-in coil 112. Upon closing of the ignition switch 118, the solenoid 110 and motor 102 cooperate to provide a soft start motor engagement system for a vehicle.

**[0036]** Axially Adjacent Coils

**[0037]** FIG. 2 shows the pull-in coil 112 and the hold-in coil 114 of the solenoid 110 positioned on a spool 120 of the solenoid 110. In the embodiment of FIG. 2, the pull-in coil 112 and the hold-in coil 114 are adjacent to one another in an axial direction of the spool 120. The axial direction is represented in FIG. 2 by axis 132.

**[0038]** The pull-in coil 112 is comprised of a first length of wire wound around a first portion of the spool 120 to form a first plurality of conductor windings (i.e., turns). The wire for the pull-in coil 112 has a relatively large cross-sectional area such that the resistance of the conductor windings is relatively low. Similarly, the hold-in coil 114 is comprised of a second length of wire wound around a second portion of the spool to form a second plurality of conductor windings (i.e., turns). The wire for the hold-in coil 114 is

has a relatively small cross-sectional area such that the resistance of the conductor windings is relatively high.

**[0039]** The pull-in coil 112 and the hold-in coil 114 are retained in a side-by-side arrangement on the spool 120. In the embodiment of FIG. 2, the spool 120 is a single component comprised of a glass-filled nylon material. However, it will be recognized that the spool may alternatively be comprised of different materials. The spool 120 may be manufactured using any of various known processes, such as a straight pull mold or other molding process.

**[0040]** The spool 120 includes a first end flange 122, a middle flange 124, a second end flange 126, and a hub 128. The hub 128 of the spool 120 is generally cylindrical in shape and provides a coil retaining surface for the pull-in coil 112 and the hold-in coil 114. Although a right circular cylinder is shown in the embodiment of FIG. 1, it will be recognized that the hub 128 may take on other forms, including cylindrical and non-cylindrical forms. Furthermore, the term “spool” as used herein refers to any appropriate solenoid coil holder, regardless of whether the hub is provided as a cylinder or if flanges are included on the ends of the hub.

**[0041]** The hub 128 in the embodiment of FIG. 2 extends from the first end flange 122 to the second end flange 126. The hub 128 defines a cylindrical interior passage 130 that extends through the spool 120 from the first end flange 122 to the second end flange 126. The cylindrical hub 128 also defines a spool axis 132 that extends through the interior passage 130. The spool axis 132 defines a centerline for the spool 120 and an axial direction along the spool.

**[0042]** The first end flange 122 provides an end wall for the spool 120 that is configured to retain coil windings on the spool. The first end flange 122 is generally disc shaped and includes a circular center hole at the interior passage 130 of the spool. This end wall may be solid with a central hole for the plunger passage 130, as shown in FIG. 2, or may include a plurality of openings. Moreover, although the flange 122 is shown as a relatively thin circular disc in the embodiment of FIG. 2, it will be recognized that the end flange 122 may be provided in various different forms and shapes.

**[0043]** The middle flange 124 also provides a wall that is configured to retain coil windings on the spool. The middle flange 124 is positioned on the hub 128 between the first end flange 122 and the second end flange 126, but not necessarily centered between the first end flange 122 and the second end flange 126. Indeed, in the embodiment of FIG. 2, the middle flange 124 is positioned closer to the second end flange 126 than to the first end flange 122. The space between the first end flange 122 and the middle flange 124 provides a first coil bay 142 on the spool 120 where the pull-in coil 112 is wound around the hub 128.

**[0044]** Similar to the first end flange 122, the middle flange 124 in the embodiment of FIG. 2 is also disc shaped. The middle flange 124 is generally thicker than the first end flange and includes coil mounting features 134 such as slots 136 along the outer perimeter of the flange 124. These slots 136 provide a passage for wire leads on the pull-in coil 112. It will be recognized that additional coil mounting features 134 are also possible, and examples of such coil mounting features will be discussed in further detail below with reference to FIGs. 6-12. Although the center flange is shown in FIG. 2 as having a circular perimeter, it will be recognized that the middle flange 124 may be

provided in various different forms and shapes. For example, although the middle flange 124 is shown as being solid with a single central opening, the middle flange may also include a plurality of openings.

**[0045]** The second end flange 126 provides another end wall for the spool 120 that is configured to retain coil windings on the spool. The space between the second end flange 126 and the middle flange 124 provides a second coil bay 144 on the spool that is adjacent to the first coil bay 142 in the axial direction. The hold-in coil 112 is wound around the hub 128 at the second coil bay 144. Similar to the first end flange 122, the second end flange 126 is also generally disc shaped and includes a circular center hole at the interior passage 130 of the spool. The second end flange 126 is generally the same thickness as the first end flange 122. Similar to the middle flange 124, includes mounting features 134 such as slots 138 along the outer perimeter of the flange 126. These slots 138 provide a passage for wire leads on the pull-in coil 112 and the hold-in coil 114. The second end flange 126 may be solid, as shown in FIG. 2, or may include a plurality of openings. Moreover, although the second end flange 126 is shown as a relatively thin circular disc in the embodiment of FIG. 2, it will be recognized that the flange 126 may be provided in various different forms and shapes.

**[0046]** As described above with reference to FIG. 2, the spool 120 of the solenoid 110 is configured such that the pull-in coil 112 is positioned adjacent to the hold-in coil 114 of the solenoid in the axial direction. As a result of this adjacent coil arrangement, greatly increased flux leakage can occur around the pull-in coil, as described below with reference to FIGs. 3-5. The increased flux leakage reduces the magnetic force experienced by the plunger as a result of the pull-in coil 112, thus allowing the resistance

of the pull-in coil 112 to be low while still minimizing the abutment force issues previously described. At the same time, the adjacent coil arrangement provides for minimal flux leakage with the hold-in coil 114 when the plunger gap is zero and the contacts are closed, thus allowing the number of coil turns in the hold-in coil to be low but maximizing its hold-in force.

**[0047]** FIGs. 3-5 are diagrams illustrating lines of magnetic flux through the solenoid when the pull-in coil 112 and the hold-in coil 114 are in various energized and non-energized states. In each of FIGs. 3-5, the pull-in coil 112, hold-in coil 114, plunger 116, solenoid case 150 and plunger stop 152 are illustrated as a cross-sectional view of the solenoid taken radially outward from the solenoid centerline 132. The solenoid spool 120 of FIG. 2 is not illustrated in FIGs. 3-5 for clarity, allowing the lines of magnetic flux 170 passing through the solenoid 110 to be more clearly displayed. However, it will be recognized that the spool 120 is present in the illustrations of FIGs. 3-5 with the pull-in coil 112 and hold-in coil 114 wound around the spool, and the plunger 116 inserted in the interior passage 130 of the spool 120.

**[0048]** With particular reference to FIG. 3, the solenoid 110 is housed by the solenoid case 150. The plunger stop 152 is a generally disc shaped member that is fixed to the solenoid case 150 and extends radially inward from the solenoid case. The plunger stop 152 includes a cylindrical protrusion 154 that fits within an end of the interior passage 132 of the spool 120 (not shown in FIG. 3). This cylindrical protrusion 152 provides a stop surface 154 configured to engage the plunger 116 when the plunger is moved in the axial direction by the pull-in coil 112.

[0049] The plunger 116 is a solid component with a cylindrical shape. The cylindrical shape of the plunger 116 is provided with a first larger diameter portion 160 and a second smaller diameter portion 162. A shoulder 164 is formed between the larger diameter portion 160 and the smaller diameter portion 162. The plunger 116 is slideably positioned within the solenoid case 150. In particular, the plunger 116 is configured to slide in the axial direction along the centerline 132 to close an air gap 168 (which may also referred to herein as a “plunger gap”) between the plunger shoulder 164 and the stop surface 154 of the plunger stop 152. Each of the plunger 116, the solenoid case 150, and the plunger stop 152 are comprised of a metallic material having relatively low magnetic reluctance, such that magnetic flux lines may easily pass through the solenoid case and the plunger.

[0050] With continued reference to FIG. 3, the pull-in coil 112 of the solenoid 110 is positioned within the solenoid case 150 and encircles the larger diameter portion 160 of the plunger 116. The pull-in coil 112 is removed from the plunger stop by a distance  $d$  in an axial direction. An axial end of the pull-in coil is aligned with the shoulder 164 of the plunger 116 when the plunger is in the leftmost position of FIG. 3. As discussed previously, the pull-in coil 112 is comprised of a length of conductor including a plurality of windings that wrap around the spool 120 (not shown in FIG. 3). When the pull-in coil 112 is initially energized, the plunger 116 is urged in the axial direction to the right, as indicated by arrow 166.

[0051] The hold-in coil 114 is positioned adjacent to the pull-in coil 112 in the axial direction within the solenoid case 150. The hold-in coil 114 encircles the protrusion 154 of the plunger stop 152 and the associated stop surface 156. Accordingly, the hold-in

coil 114 also encircles the smaller diameter portion 162 of the plunger that extends through the plunger stop 152. Furthermore, the pull-in coil encircles the air gap 168 when the plunger is in the leftmost position of FIG. 3. As discussed previously, the hold-in coil 114 is comprised of a length of conductor including a plurality of windings that wrap around the spool 120 (not shown in FIG. 3). When the hold-in coil 114 is initially energized, the plunger 116 is urged in the axial direction to the right, as indicated by arrow 166.

**[0052]**        Coil Position Within the Solenoid Results in Leakage Flux

**[0053]**        As represented by flux lines 170 in FIGs. 3 and 4, when the pull-in coil 112 and the hold-in coil 114 are energized, magnetic flux is created within the solenoid. Leakage flux is any flux that does not contribute to the axial force acting on the plunger 116. The axial force acting to pull the plunger 116 toward the plunger stop 152 and close the plunger gap 168 is dependent upon the total flux linkage between the pull-in coil 112 and the plunger 116 and between the hold-in coil 114 and the plunger 116. When flux leakage occurs, the flux linkage is reduced and so is the resulting force on the plunger 116.

**[0054]**        By placing the pull-in coil 112 away from the plunger gap 168 and plunger stop surface 156, as shown in FIGs. 3 and 4, the flux leakage of the pull-in coil 112 is intentionally greatly increased in order to reduce the resulting force on the plunger 116. As shown in FIGs. 3 and 4, rather than traverse directly from the plunger 116 to the plunger stop 152, an increased amount of flux by-passes the plunger 116 and couples directly from one side of the case 150 to the stop 152 or even back to the case 152 outside wall 151. Examples of this leakage flux is indicated in FIG. 3 by lines 171. The leakage

flux 171 effectively lowers the magnetic force on the plunger 116 for a given amp-turn excitation of the pull-in coil 112. Since the magnetic force on the plunger 116 is reduced, and because the pinion gear is mechanically connected to the plunger via the pivoting shift lever, the impact and steady-state abutment force of the pinion gear on the ring gear is also reduced. Therefore with the embodiment of FIGs. 1-5, the resistance of the pull-in coil 112 can be made low to increase soft start current to the electric motor 102. Accordingly, the torque of the electric motor 102 is increased during soft start, without having excessive abutment force between the pinion gear and the ring gear which traditionally results from the high amp-turn excitation of the pull-in coil 112.

**[0055]** While coil arrangement in the embodiment of FIGs. 1-5 is configured to increase the leakage flux for the pull-in coil 112, the arrangement is configured to do the opposite for the hold-in coil 114. In particular, the hold-in coil 114 in FIGs. 1-5 is configured to minimize flux leakage with the plunger 116 in order to maximize the electromagnetic hold-in force on the plunger 116 for a given number of turns of the hold-in coil 114. This is accomplished by centering the hold-in coil 114 at the plunger stop surface 156 interface. In this fashion leakage flux 171 is minimized with the hold-in coil 114, and the electromagnetic force on the plunger is maximized. Accordingly, by the geometrical layout of the windings of the pull-in coil 112 and the hold-in coil 114, it is possible to reshape the force-travel curves of the plunger 116 to values more desirable for a starter with a soft start system.

**[0056]** In addition to the benefits related to flux leakage, the side-by-side arrangement for the pull-in coil 112 and the hold-in coil 114 can also have thermal benefits. In particular, with the conventional coil over coil winding such as that shown in

FIG. 15, the hold-in coil 214 suffers in strength if the abutment time between the pinion gear 206 and the ring gear is prolonged. During a prolonged abutment, the pull-in coil 212 will rapidly heat and then increase the temperature of the hold-in coil 214. When the temperature of the hold-in coil 214 increases, the electrical resistance increases and the current decreases. This decreases the resulting hold-in force provided by the hold-in coil and thus the risk of the plunger contacts opening and plunger disengagement is increased. However, with the side-by-side coil arrangement shown in the starter embodiment of FIGs. 1-5, the thermal influence of the pull-in coil 112 on the hold-in coil 114 during starting is minimal, as the thermal conductive path resistance is much higher with the two coils separated from one another in the axial direction.

**[0057]**        Spool With Additional Mounting Features

**[0058]**        With reference now to FIGs. 6-7, an alternative embodiment of the spool 120 of FIG. 2 is shown. Similar to the spool of FIG. 2, the alternative embodiment of the spool also generally includes a first end flange 122, a middle flange 124, a second end flange 126, and a hub 128. The hub 128 is generally cylindrical about an axial centerline 132, and an interior passage 130 extends through the hub from one end of the spool 120 to the other. However, as explained in further detail below, in the embodiment of FIGs. 6-7, the middle flange 124 and the second end flange 126 include a number of additional mounting features 134.

**[0059]**        FIGs. 6A and 7 show views of the side of the middle flange 124 that faces the first coil bay 142. The middle flange 124 includes various mounting features including a first winding post 172 positioned between a lead-in slot 174 and a lead-out

slot 176. The first winding post 172 extends radially outward from the centerline of the spool 120 and is configured to engage the wire from the hold-in coil. Sufficient space is provided around the first winding post 172 to allow the hold-in coil 114 to be wrapped around the winding post. Moreover, the first winding post 172 is sufficiently long to allowing wire from the hold-in coil 114 to be wrapped around the first winding post 172 several times. Accordingly, as explained in further detail below, the first winding post 172 provides a mounting feature 134 that allows the hold-in coil to be securely anchored to the spool 120 and also provides a feature for reversing the direction of the turns of the hold-in coil 114 on the spool. A reverse turn post may be advantageous in solenoids for starters with soft start systems, as described in US Patent Application No. 12/767,710, filed April 26, 2010, the content of which is incorporated herein by reference in its entirety.

**[0060]** With continued reference to FIGs. 6A and 7, the lead-in slot 174 provides an axial groove in the outer circumference of the middle flange 124 which is designed and dimensioned to receive the wire used to form the pull-in coil 112. Additionally, in the embodiment of FIGs. 6A and 7, the lead-in slot 174 includes an entry ramp 175 for the start lead of the pull-in coil 112. This entry ramp 175 extends in a substantially radial direction to the hub 128 of the spool 120. The entry ramp 175 is configured such that the depth of the slot 174 into the middle flange 124 is slightly tapered moving toward the hub 128. Accordingly, the lead-in slot 174 with entry ramp 175 allows the start lead of the pull-in coil 112 to be guided on the spool 120 from the perimeter of the middle flange 124 toward the hub 128 without consuming space in the first coil bay 142 before the start lead reaches the hub 128. Once the start lead does reach the hub 128, the first layer of

turns for the pull-in coil 112 begin. While the lead-in slot 174 has been disclosed as including the entry ramp 175, it will be recognized that in at least one alternative embodiment, the lead-in slot extends directly to the hub without the entry ramp 175 positioned in the slot 174.

**[0061]** Similar to the lead-in slot 174, the lead-out slot 176 provides another axial groove in the outer circumference of the middle flange 124 which is designed and dimensioned to receive the wire used to form the pull-in coil 112. However, unlike the lead-in slot 174 in the embodiment of FIGs. 6A-7, the lead-out slot 176 does not include a ramp portion that extends in the radial direction to the hub 128 of the spool. Instead, the lead-out slot 174 is simply provided on the perimeter of the middle flange 124 and extends radially approximately the thickness of the wire for the pull-in coil in order to allow the finish lead of the pull-in coil to cut across the middle flange 124 once the pull-in coil is completely wound in the first coil bay 142.

**[0062]** With reference now to FIG. 6B, the opposite face of the middle flange 124 is shown. The face of the middle flange 124 shown in FIG. 6B is the face presented to the second coil bay 144 of the spool 120. The first winding post 172, the lead-in slot 174, and the lead-out slot 176 are all visible on this side of the middle flange 124. In addition, this side of the middle flange 124 includes an entry ramp 182 for the start lead of the hold-in coil 114. This entry ramp 182 is similar to the entry ramp 175 for the pull-in coil, extending in a generally radial direction toward the hub 128 and gradually tapering as the ramp extends toward the hub 128. Furthermore, the side of the middle flange 124 shown in FIG. 6B includes a second winding post 178 that is only accessible on this side of the middle flange 124. Accordingly, an indentation 180 is formed in this face of the middle

flange 124, and the second winding post 178 is situated in this indentation 180. As explained in further detail below, this second winding post 178 provides a mounting feature for the hold-in coil 114 that may be used as an anchor or a reversing turn feature.

**[0063]** With reference now to FIG. 6C the second end flange 126 includes additional mounting features, including a dual start lead slot 184, a first finish lead slot 186, and a second finish lead slot 188. The dual start lead slot 184 is designed and dimensioned to allow the start leads for both the pull-in coil 112 and the hold-in coil 114 to pass through the perimeter of the second end flange 126. When both start leads are positioned in the slot 184, the start lead for the hold-in coil 114 is positioned radially inward from the start lead for the pull-in coil 112. The first finish lead slot 186 is configured to allow the finish lead for the pull-in coil 112 to pass through the perimeter of the second end flange 126. Similarly, the second finish lead slot 188 is configured to allow the finish lead for the hold-in coil 114 to pass through the perimeter of the second end flange 126.

**[0064]** It will be recognized that the middle flange 124 is thicker in the axial direction than the two end flanges 122 and 126. This increased thickness naturally follows because of the desired separation of the pull-in coil 112 and the hold-in coil 114 in the axial direction such that the coils are properly positioned on the spool 120. However, the increased thickness also provides increased space for the various coil mounting features 134 included on the middle flange 124. Without this middle flange design, the end flanges 122, 126 would need to be the thickness of the center flange to provide the same features, and this would decrease the available space for the coil bays 142, 144.

[0065] The winding of the pull-in coil 112 and the hold-in coil 114 on the spool 120 is now described with reference to FIGs. 8-12 in order to provide a better understanding of the design of the foregoing mounting features 134 of the spool 120 and arrangement of the coils 112 and 114 on the spool.

[0066] The process of winding the spool 120 begins with the hold-in coil 114. FIG. 8 shows the hold-in coil 114 being wound in the second coil bay 144 of the spool. To begin the winding process, a start lead 190 of the hold-in coil 144 is wrapped around the first winding post 172 in order to anchor the wire for the hold-in coil to the spool 120. The start lead 190 is then channeled down the entry ramp 182 (not shown in FIG. 8) on the middle flange 124 toward the hub 128. After the start lead 190 reaches the hub 128, the spool 120 is rotated in the direction of arrow 191, causing a length of wire from a reel (not shown) to be wound around the hub, and create winding turns for the hold-in coil 114. These winding turns are wound in a first turn direction in the second coil bay 144 of the spool 120.

[0067] As shown in FIG. 9, after a predetermined number of turns in the first direction are created in the second coil bay 144, the length of wire for the hold-in coil is wrapped around the first winding post, and the spool 120 is rotated in the opposite direction as indicated by arrow 192. Rotation of the spool in the direction of arrow 192 results in reverse winding turns being created in a second direction in the second coil bay 144 of the on the spool 120. Such reverse winding turns may be advantageous on the hold-in coil in a vehicle starter, as described in US Patent Application No. 12/767,710, filed April 26, 2010, the content of which is incorporated herein by reference in its entirety.

**[0068]** With reference now to FIG. 10, after the reverse winding turns are created, the wire for the hold-in coil is wrapped around the second winding post 178 on the middle flange to securely anchor the hold-in coil in the second coil bay 144. The finish lead 194 of the hold-in coil is then directed through the second finish lead slot 188 on the second end flange 126. The start lead 190 is also directed through the dual start lead slot 184 on the second end flange 126, and this completes the hold-in coil 114 on the spool 120.

**[0069]** FIG. 11 shows the pull-in coil 112 being wound in the first coil bay 142 of the spool 120 after the hold-in coil 114 is wound in the second coil bay 144. To begin winding the pull-in coil, a start lead 196 of the pull-in coil 112 is routed through the dual start lead slot 184 on the second end flange 126 and through the lead-in slot 174 on the middle flange 124. The start lead 196 is then directed down the entry ramp 175 on the middle flange 124 toward the hub 128. After the start lead 196 reaches the hub 128, the spool 120 is rotated in the direction of arrow 197, causing a length of wire from a reel (not shown) to be wound around the hub, and create winding turns for the pull-in coil 112 in the first coil bay 142 of the spool 120.

**[0070]** With reference now to FIG. 12, after the turns of the pull-in coil 112 are completely wound in the first coil bay 142, the finish lead 198 is routed through the lead out slot 176 on the middle flange 124. The finish lead 198 is then directed across the turns of the hold-in coil 114 and through the first finish lead slot 186 on the second end flange 126. This completes the winding of the pull-in coil 112 on the spool 120.

**[0071]**        Coil Comprised of Rectangular Wire

**[0072]**        FIG. 13 shows a cross-sectional view of the spool 120 along line D-D of FIG. 12. In this embodiment of the solenoid 110, the pull-in coil 112 is comprised of rectangular wire 146 (i.e. wire having a substantially rectangular cross-section), and the hold-in coil 114 is comprised of traditional round wire 147. In particular, the rectangular wire 146 used for the pull-in coil 112 is square wire in the embodiments of FIGs. 12 and 13. The rectangular wire 146 is jacketed with a layer of insulation on the outer perimeter. The wire 146 also includes slightly radiused corners 148 that are provided for manufacturing concerns and to avoid any sharp edges on the wire which might cut into the insulation layer on neighboring wires. As explained below, the rectangular wire 146 is advantageous for use in the pull-in coil 112, as it provides an increased stacking factor for the coil while also providing thermal benefits for the coil.

**[0073]**        The stacking factor for a coil is the ratio of the total volume consumed by conductors only (i.e., not including air voids between conductors) to the total volume consumed by the complete coil (i.e., including all conductors and air gaps between conductors). Traditional round wire has an effective stacking factor of about 78%. In contrast, the square wire disclosed herein has an effective stacking factor of 90% or more. In particular, the square wire 146 used in the embodiment of FIGs. 12 and 13 has a stacking factor of 92%. As a result, when comparing square wire and round wire, square wire will require less space to provide the same electromagnetic force (i.e., less space to provide the same amp-turns). This space savings is particularly useful for vehicle starters where the starter is often situated in a crowded engine compartment.

[0074] Another benefit of the rectangular wire 146 of FIGs. 12 and 13 is that it provides a better thermal conduction path than round wire for transporting the ohmic heat of the coil 112 to the edges of the coil, where the heat may be removed by conduction or convection. With a round wire coil, there is only point contact between adjacent windings, as the conductors layers are wound on top of each other (i.e., two adjacent circles will only touch in a single point). In contrast, as shown in FIG. 13, with square wire 146 the interface between conductors on adjacent windings is much larger since there is contact between adjacent conductors along the entire flat portion of the sides of the conductors. Therefore, the heat being transmitted from coil wire to coil wire is transported via the copper wire rather than the air between the wires, and this copper-to-copper conduction provides a significant thermal advantage. For example, the improved conduction reduces the delta temperature difference between the outside edges of the coil and the typical center hot spot of the coil.

[0075] With reference now to FIG. 14, yet another alternative embodiment of the solenoid spool 120 and coils 112, 114 is shown. In this embodiment, the pull-in coil 112 is comprised of rectangular wire 146, and the hold-in coil 114 is also comprised of rectangular wire 149. The rectangular wire 146 of the pull-in coil 112 is essentially the same as the rectangular wire 149 of the hold-in coil, but the width of the pull-in coil wire 146 is greater than the width of the hold-in coil wire 149. Accordingly, the hold-in coil wire is square wire with radiused corners. Additionally, the rectangular wire 149 is jacketed with a layer of insulation on the outer perimeter. The rectangular wire 149 of the hold-in coil 114 also provides similar advantages to those described above for the

pull-in coil 112. For example, the rectangular wire 149 provides an increased stacking factor for the hold-in coil 114 while also providing thermal benefits for the coil.

**[0076]** The foregoing detailed description of one or more embodiments of the starter solenoid with spool for retaining coils been presented herein by way of example only and not limitation. It will be recognized that there are advantages to certain individual features and functions described herein that may be obtained without incorporating other features and functions described herein. Moreover, it will be recognized that various alternatives, modifications, variations, or improvements of the above-disclosed embodiments and other features and functions, or alternatives thereof, may be desirably combined into many other different embodiments, systems or applications. Presently unforeseen or unanticipated alternatives, modifications, variations, or improvements therein may be subsequently made by those skilled in the art which are also intended to be encompassed by the appended claims. Therefore, the spirit and scope of any appended claims should not be limited to the description of the embodiments contained herein.

## CLAIMS

What is claimed is

1. A solenoid for a vehicle starter, the solenoid comprising:
  - a spool including a first coil bay, a second coil bay, and an interior passage defining an axial direction;
  - a first coil positioned in the first coil bay;
  - a second coil positioned in the second coil bay; and
  - a plunger positioned within the interior passage of the spool and configured to move in the axial direction when the first coil is energized.
2. The solenoid of claim 1 wherein first coil bay is positioned adjacent to the second coil bay in the axial direction.
3. The solenoid of claim 2 wherein the first coil bay is coaxial with the second coil bay along an axial centerline of the spool.
4. The solenoid of claim 3 wherein the spool further comprises a middle flange separating the first coil bay from the second coil bay.
5. The solenoid of claim 4 wherein the spool further comprises two end flanges, and wherein the middle flange is not centered on the spool between the two end flanges such that the first bay and the second bay are of different lengths.
6. The solenoid of claim 4 wherein the center flange is thicker than each of the two end flanges.

7. The solenoid of claim 4 wherein the middle flange includes a first winding protrusion with the second coil engaging the first winding protrusion.
8. The solenoid of claim 7 wherein the first winding protrusion is a first post extending radially outward on the flange.
9. The solenoid of claim 7 wherein the middle flange includes a second winding protrusion with the second coil engaging the second winding protrusion.
10. The solenoid of claim 4 wherein the middle flange includes a first slot and a second slot, wherein a start lead for the first coil extends through the first slot and a finish lead for the first coil extends through the second slot.
11. The solenoid of claim 10 wherein the first slot is tapered in a radial direction toward the axial centerline.
12. The solenoid of claim 10 wherein the spool further comprises an end flange including a first slot, a second slot, and a third slot, wherein the start lead for the first coil extends through the first slot and the finish lead for the first coil extends through the second slot, and wherein a start lead for the second coil extends through the first slot and a finish lead for the second coil extends through the third slot.
13. The solenoid of claim 1 wherein the first coil is a pull-in coil and the second coil is a hold-in coil.
14. The solenoid of claim 13 wherein the solenoid includes a plunger stop positioned in an end of the interior passage of the spool, wherein the pull-in coil is distanced from the plunger stop in the axial direction, and wherein the hold-in coil encircles the plunger stop.

15. The solenoid of claim 1 wherein the spool is a single molded component comprised of a glass filled nylon material.
16. A solenoid for a vehicle starter, the solenoid comprising:
  - a spool including a first end flange, a second end flange, and a middle flange;
  - a first coil positioned between the first end flange and the middle flange;
  - a second coil positioned between the middle flange and the second end flange; and
  - a plunger positioned within the spool and configured to move in an axial direction when the first coil is energized.
17. The solenoid of claim 16 wherein the middle flange is thicker than the first end flange or the second end flange.
18. The solenoid of claim 16 wherein the middle flange includes a plurality of coil mounting features positioned along the outer perimeter of the flange, and wherein the first coil and the second coil engage the coil mounting features.
19. A vehicle starter comprising:
  - an electric motor; and
  - a solenoid comprising:
    - a spool including a first coil bay, a second coil bay adjacent to the first coil bay;
    - a first coil positioned in the first coil bay;
    - a second coil positioned in the second coil bay such that the second coil is adjacent to the first coil in an axial direction; and

a plunger positioned within the spool and configured to move in the axial direction when the first coil is energized.

20. The vehicle starter of claim 19 wherein the first coil bay is positioned between a first end flange and a middle flange, and wherein the second coil bay is positioned between a second end flange and the middle flange.

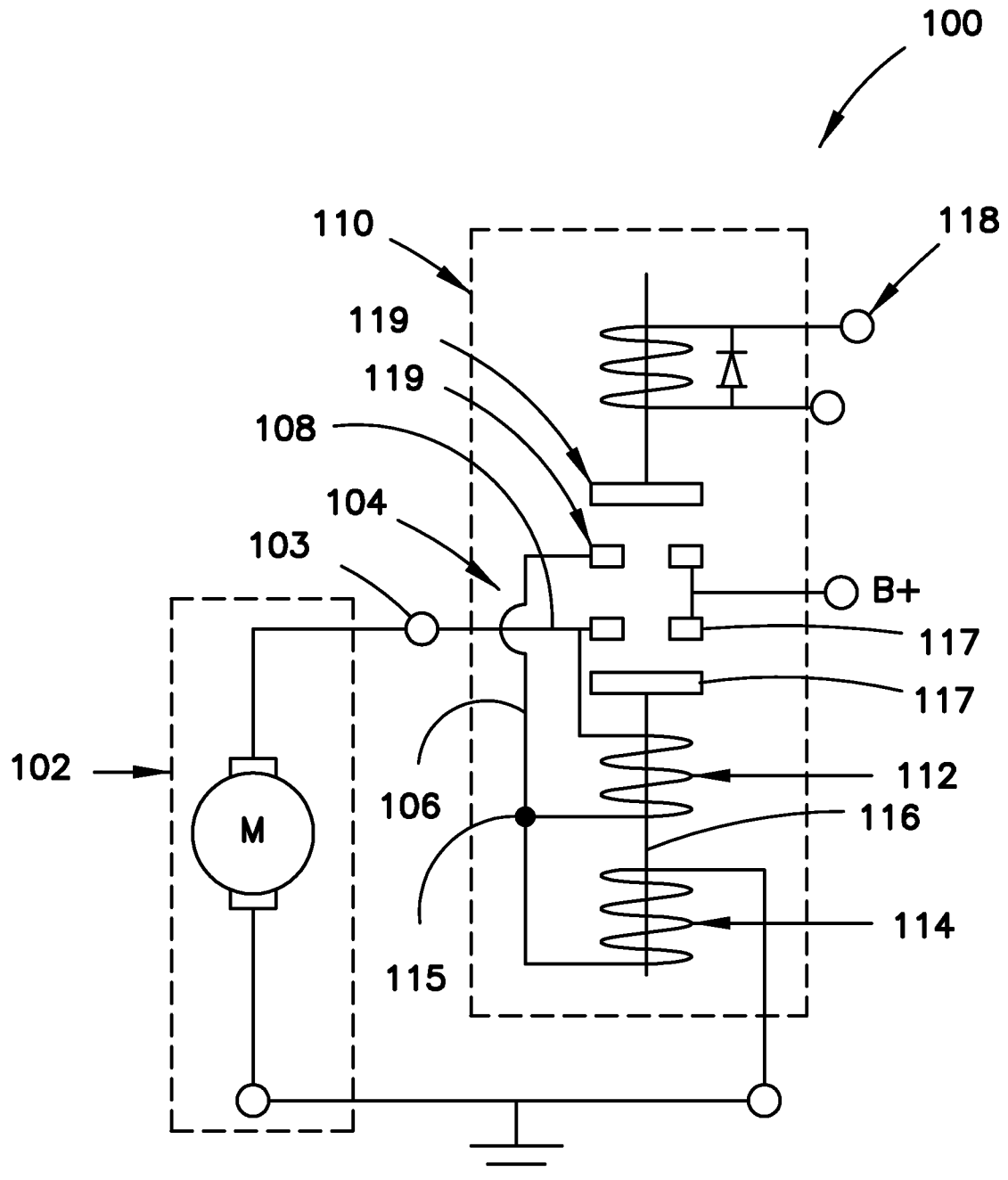


FIG. 1

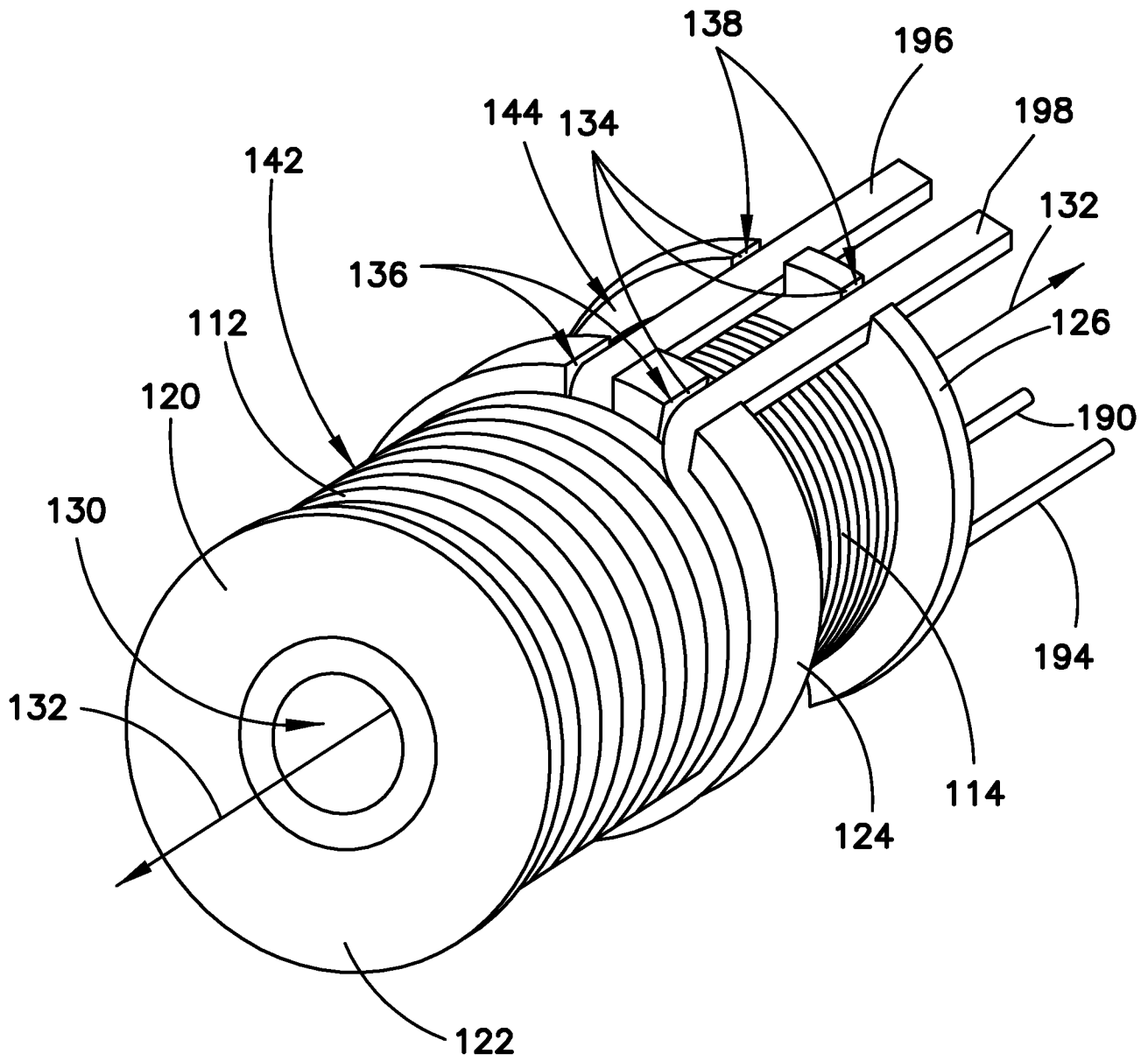


FIG. 2

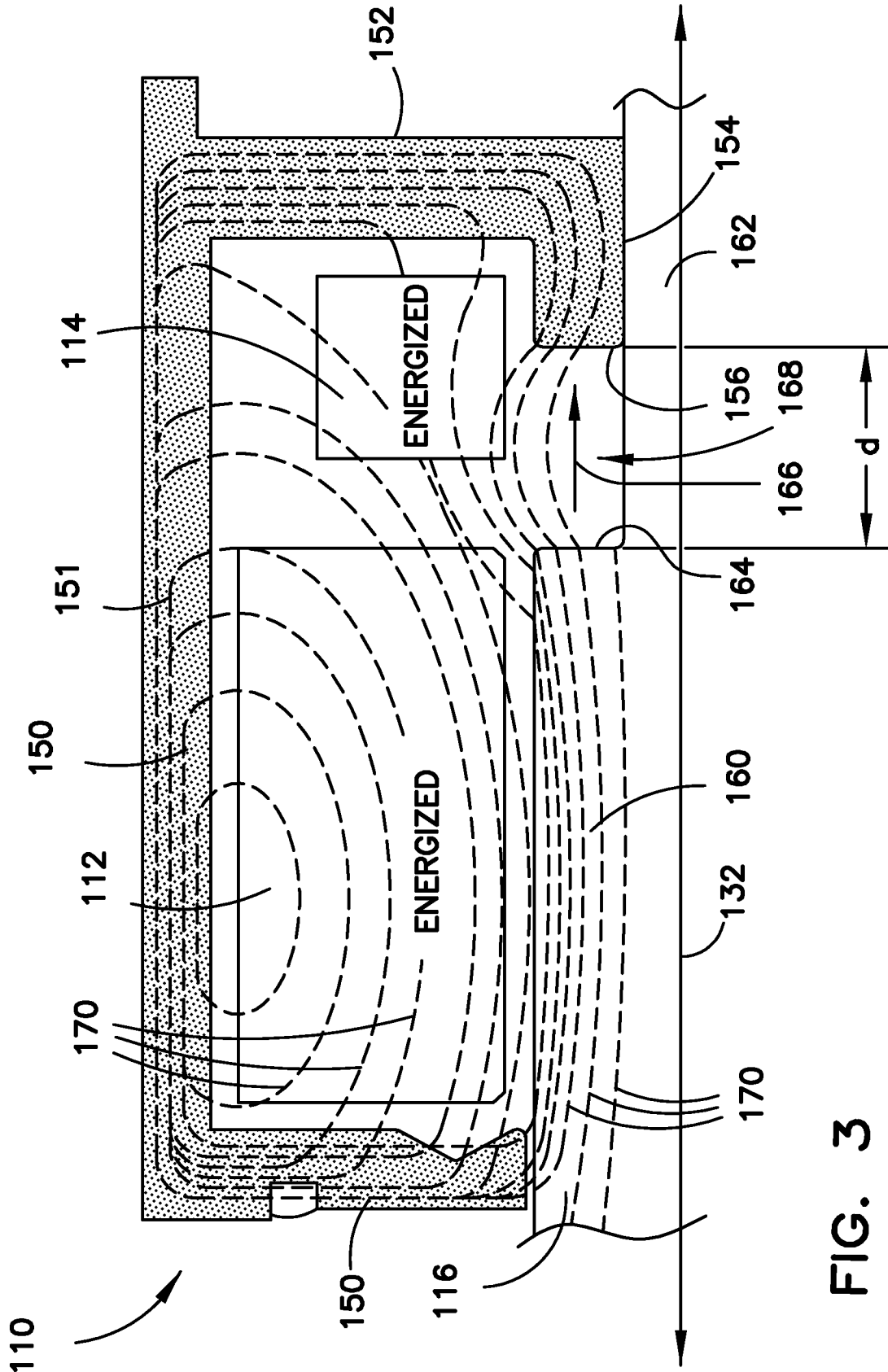


FIG. 3

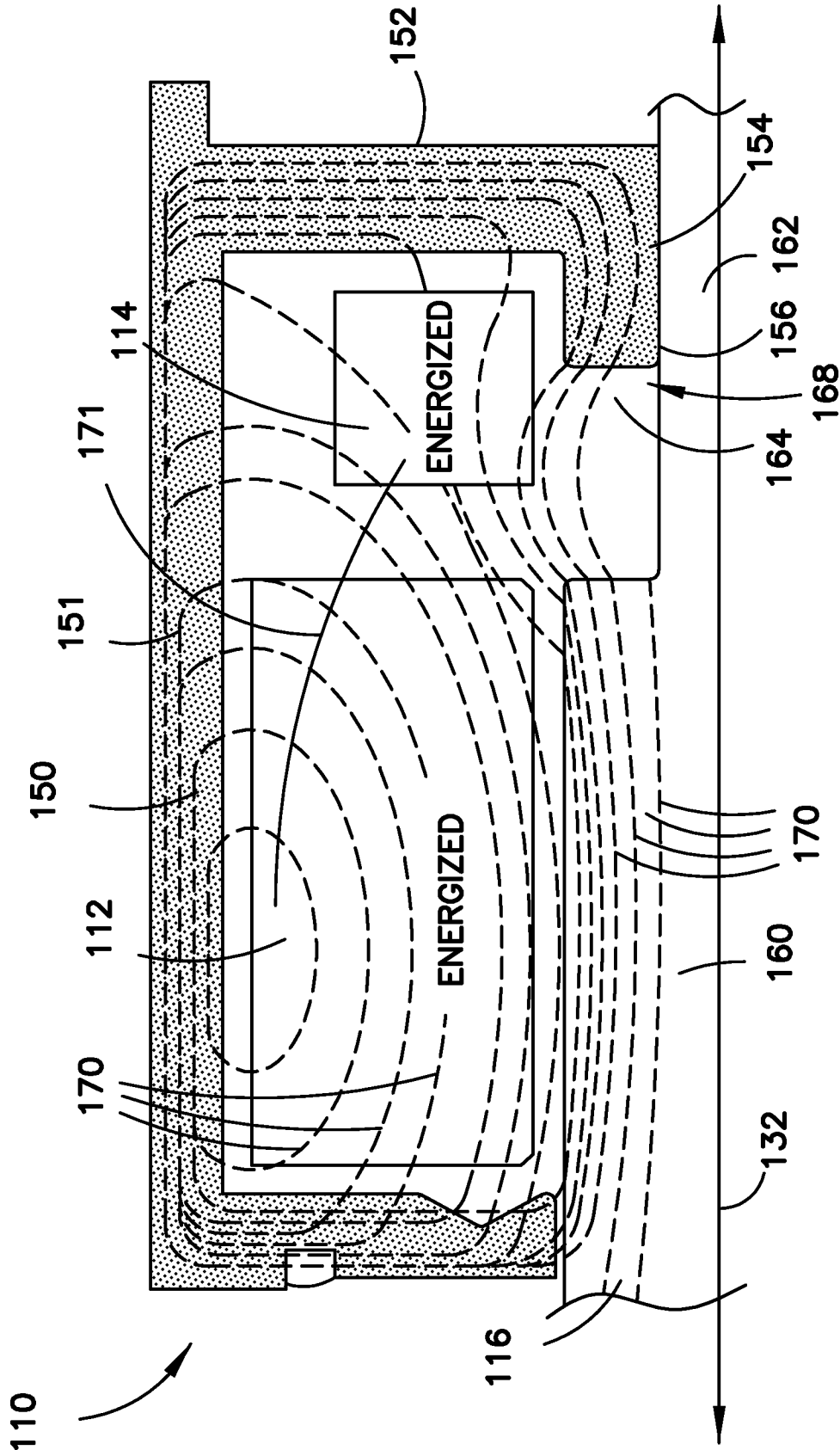


FIG. 4

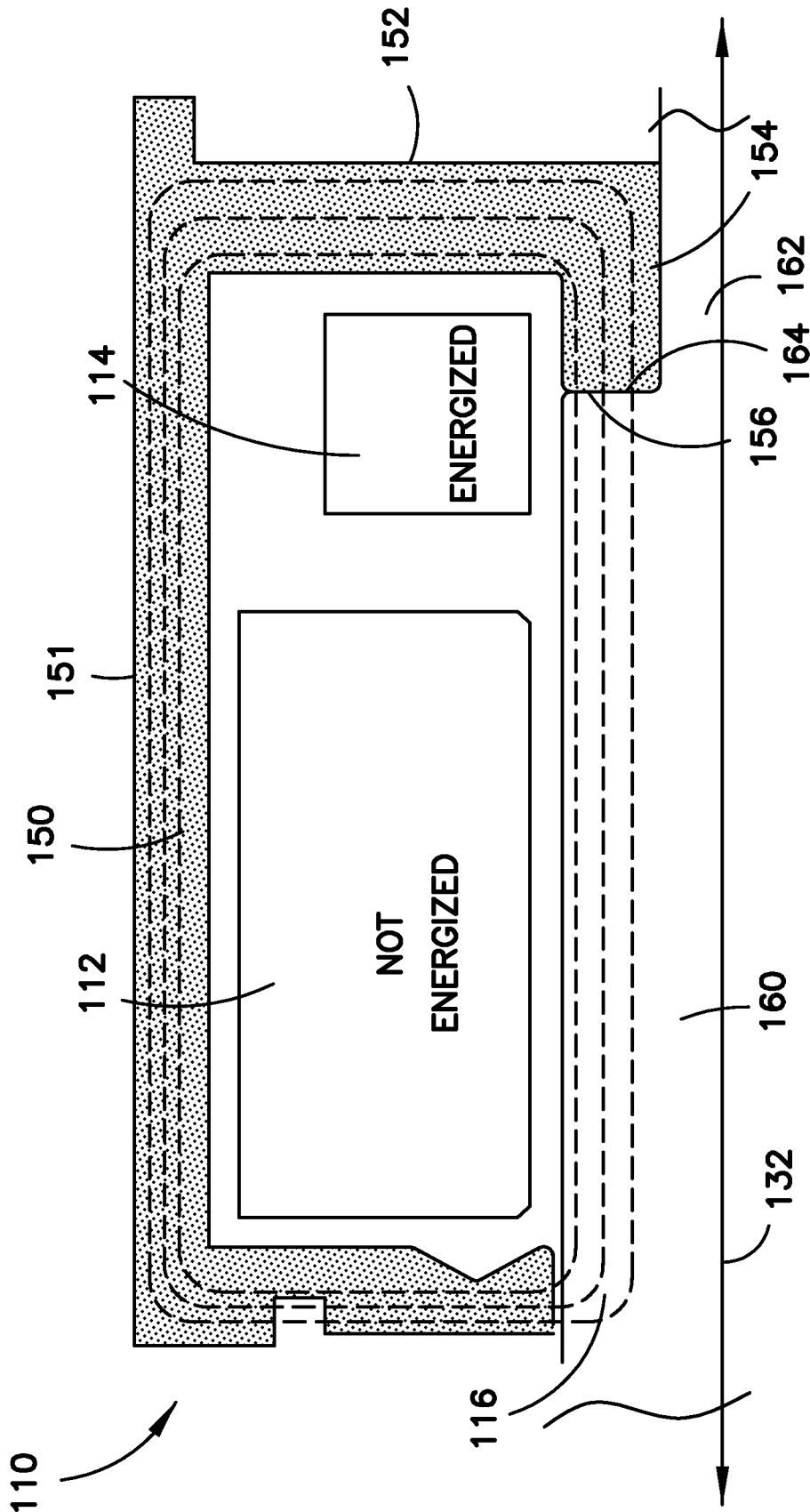


FIG. 5



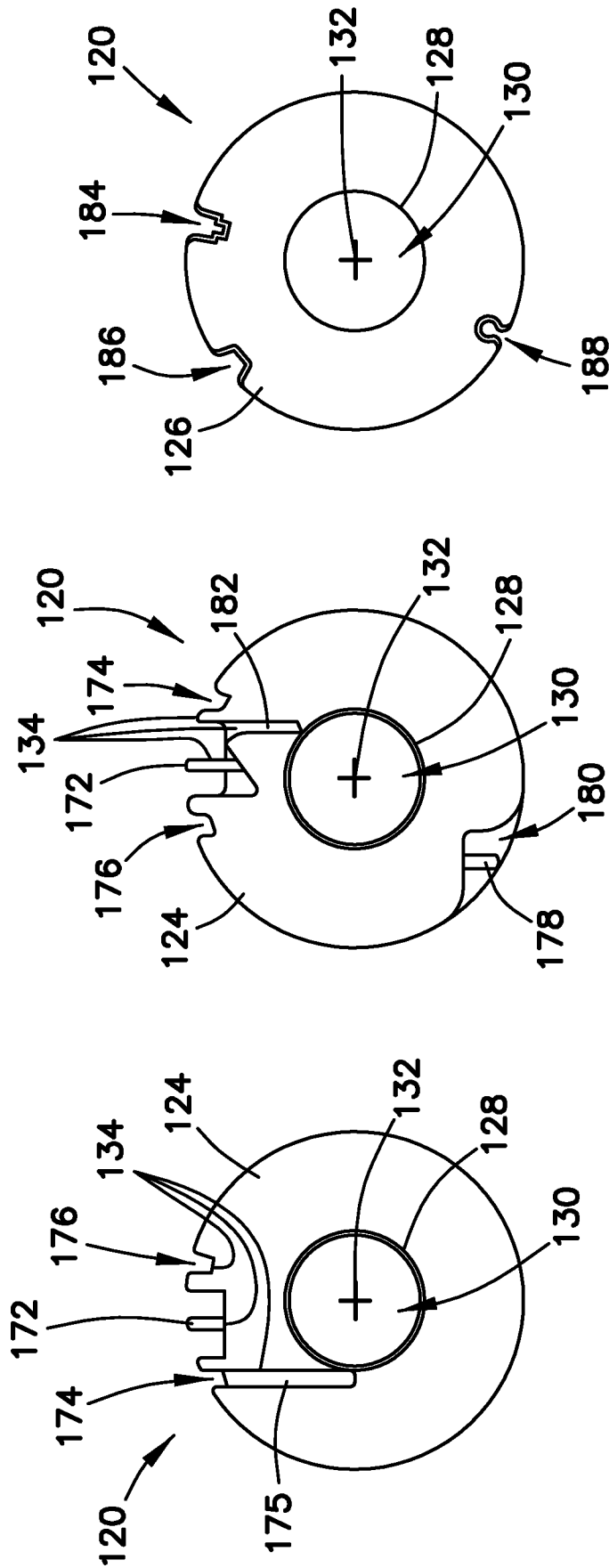


FIG. 6C

FIG. 6B

FIG. 6A

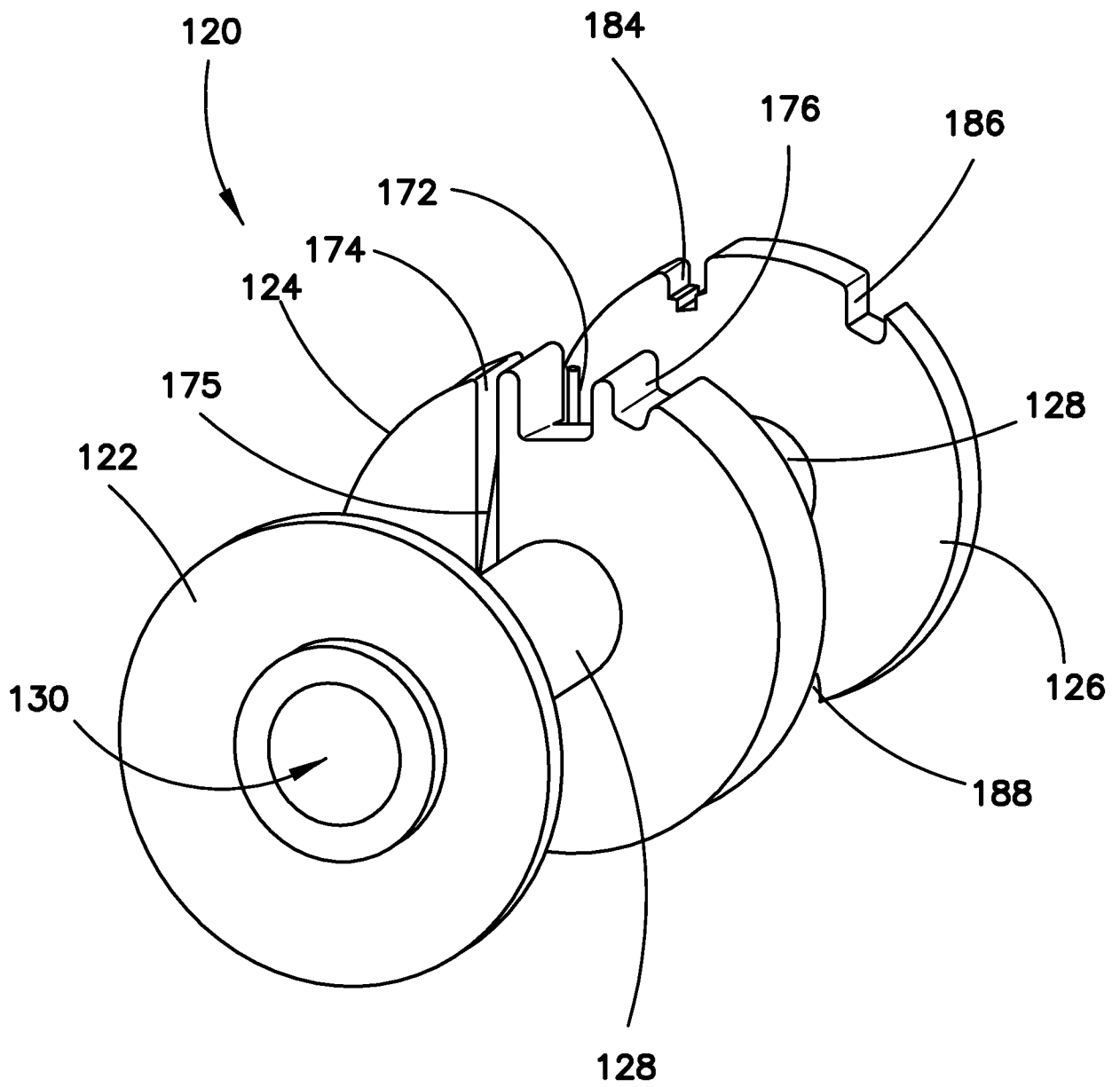


FIG. 7

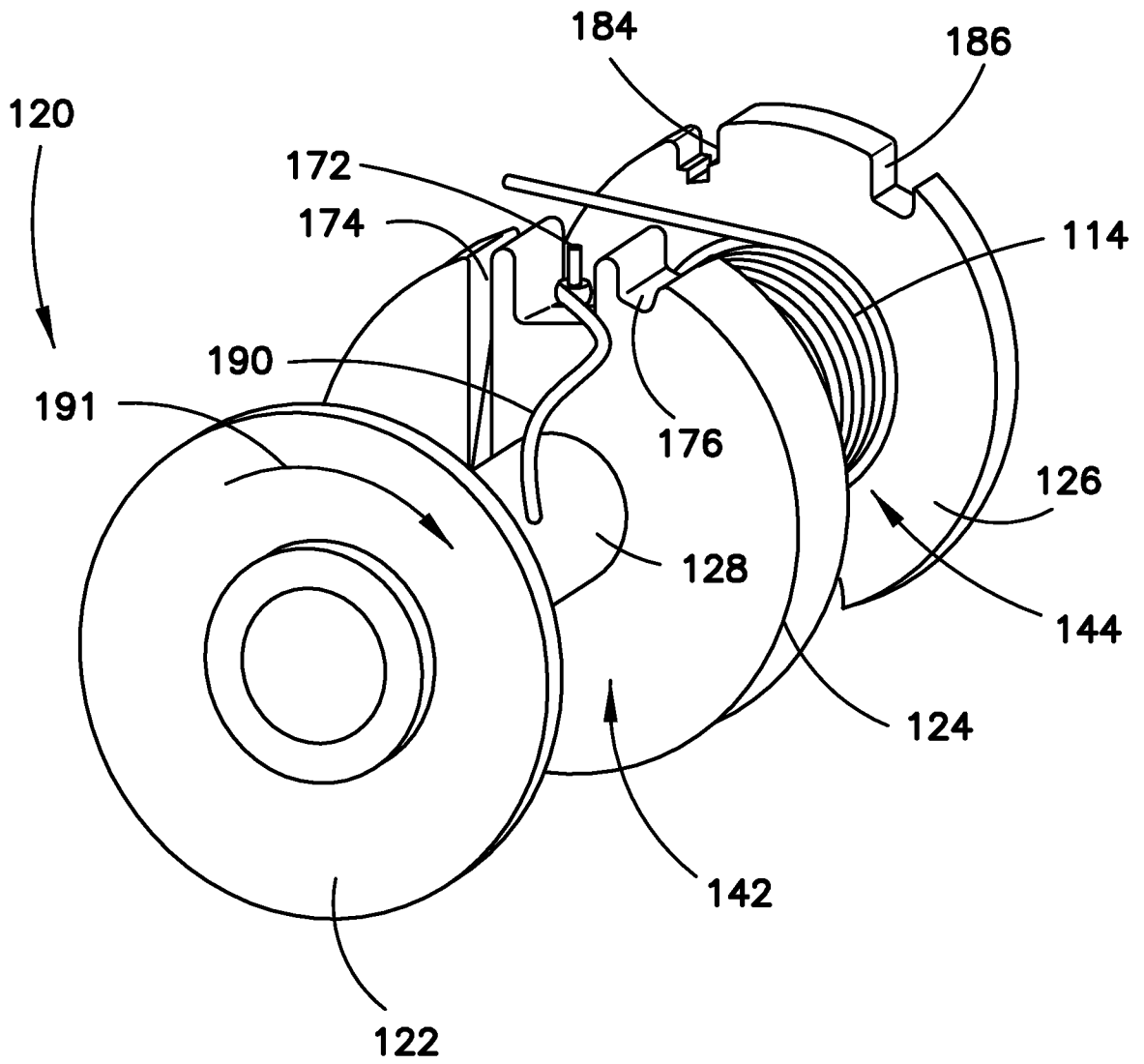


FIG. 8

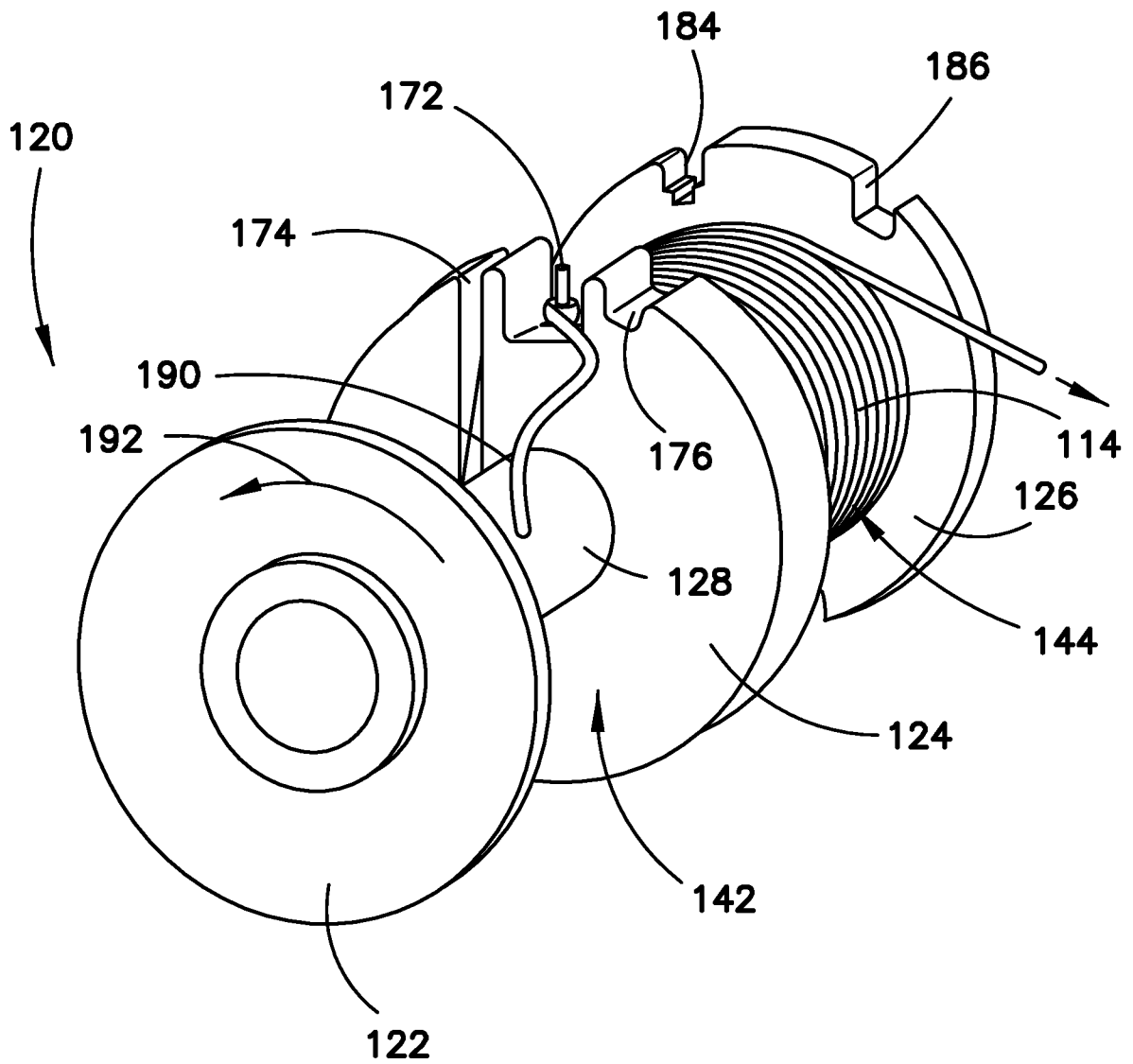


FIG. 9

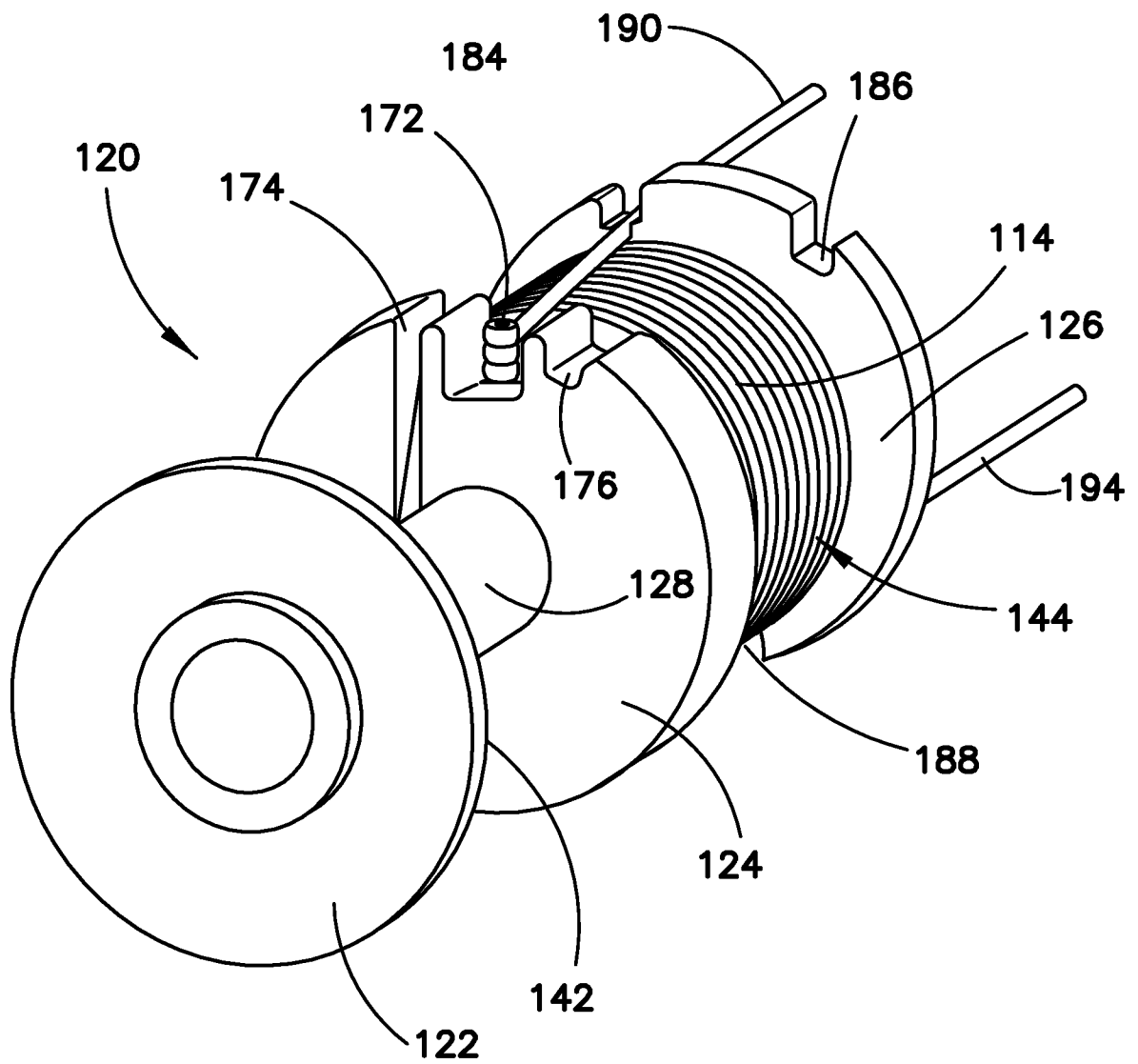


FIG. 10

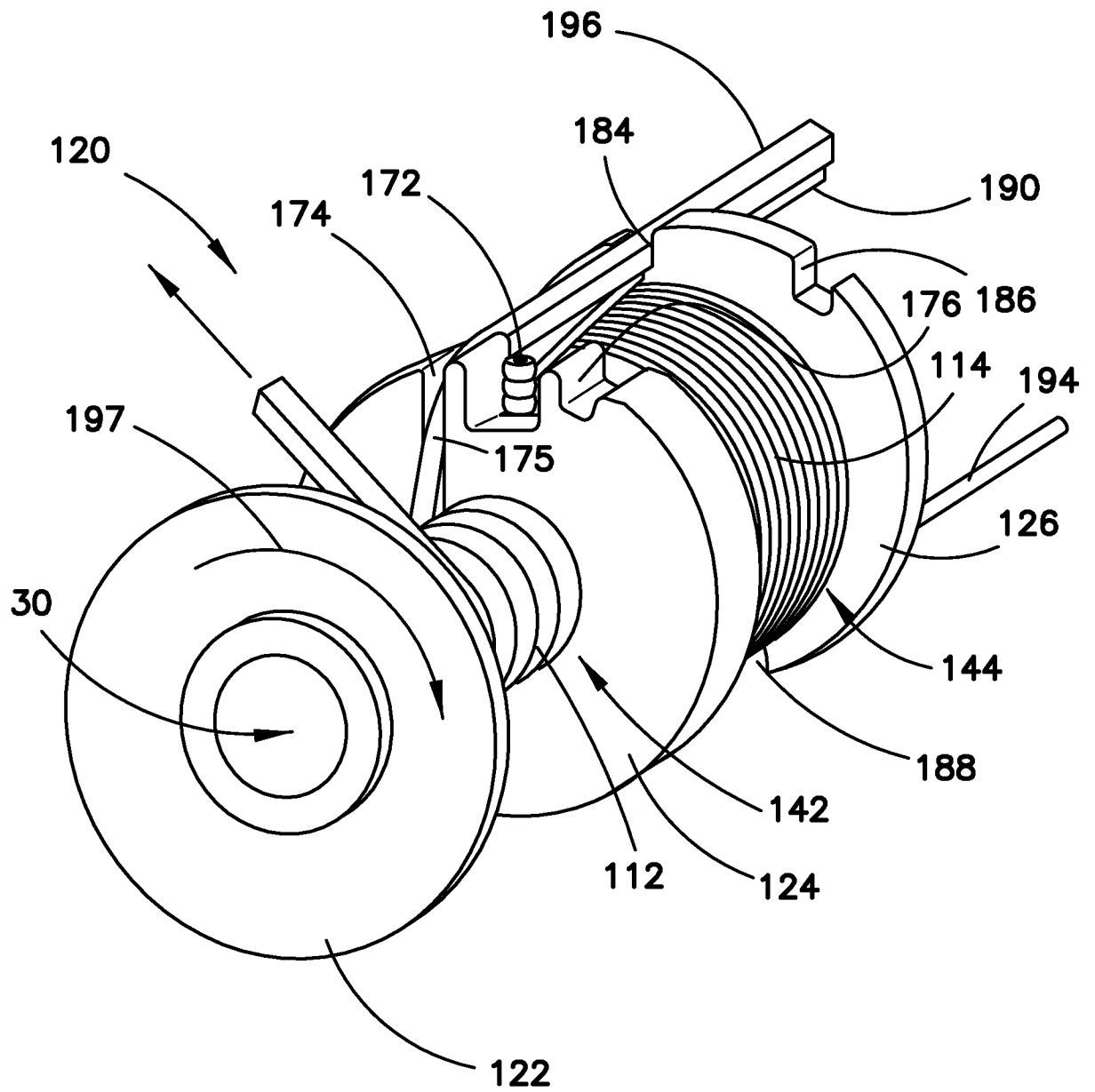


FIG. 11

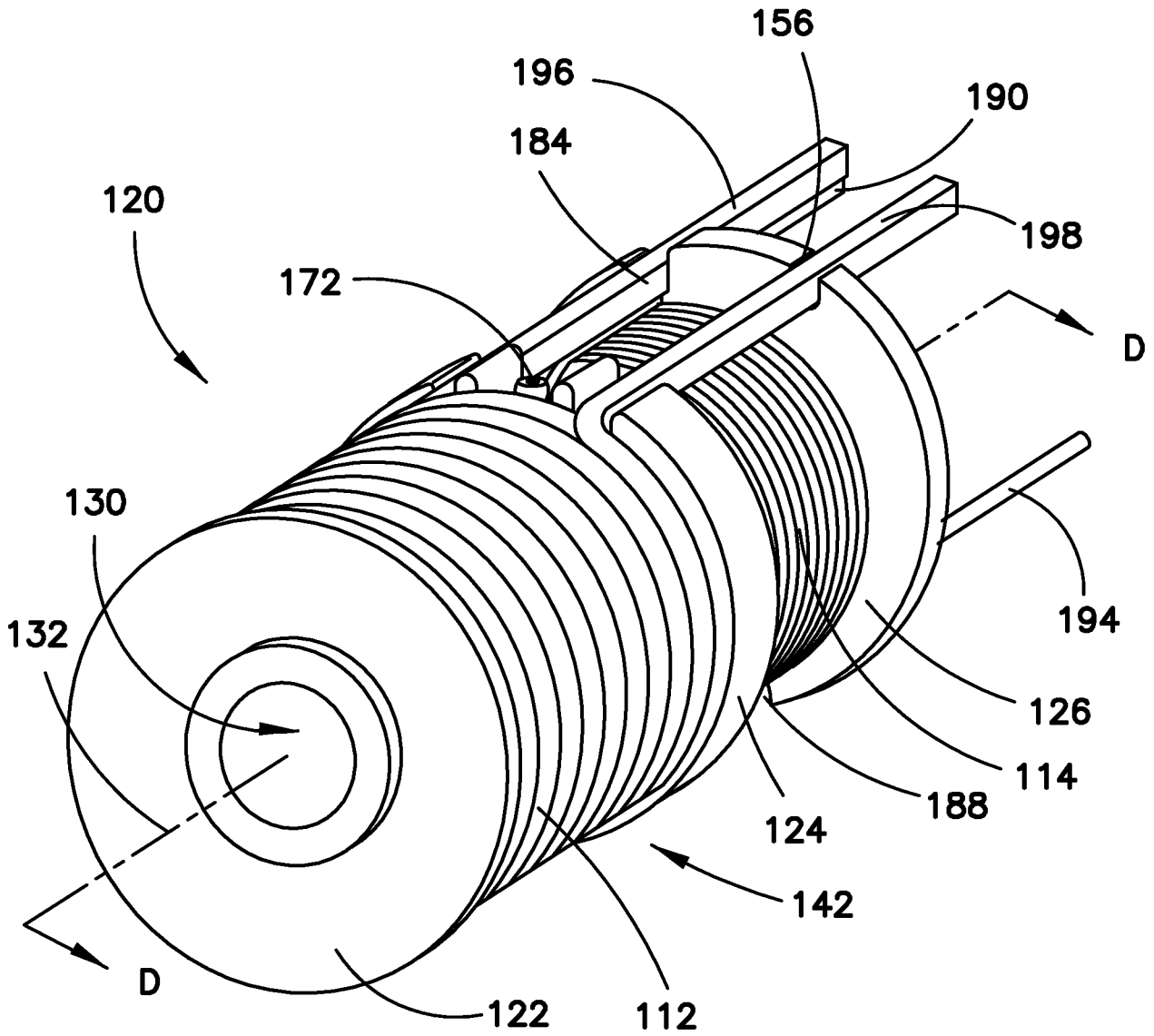


FIG. 12

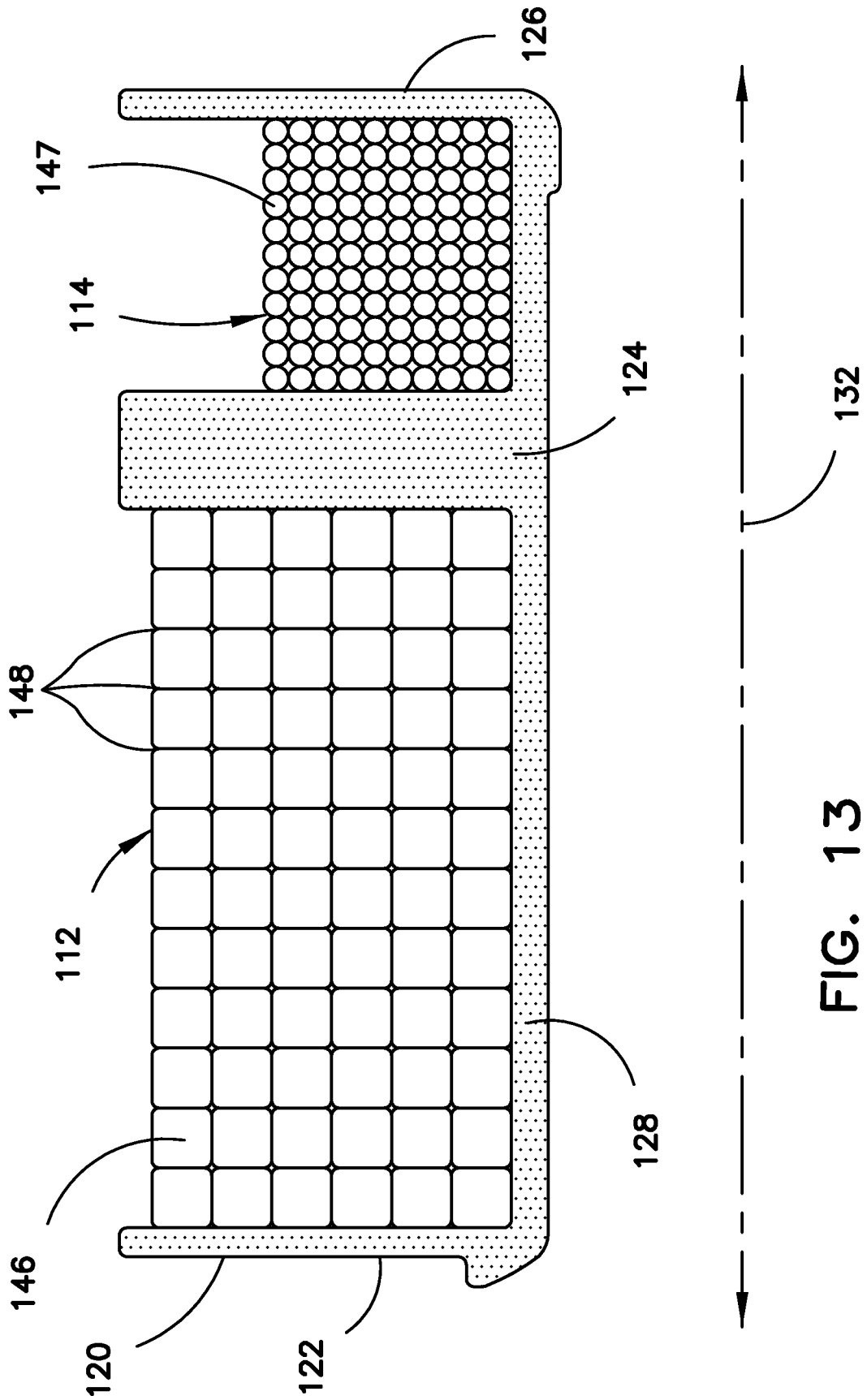


FIG. 13



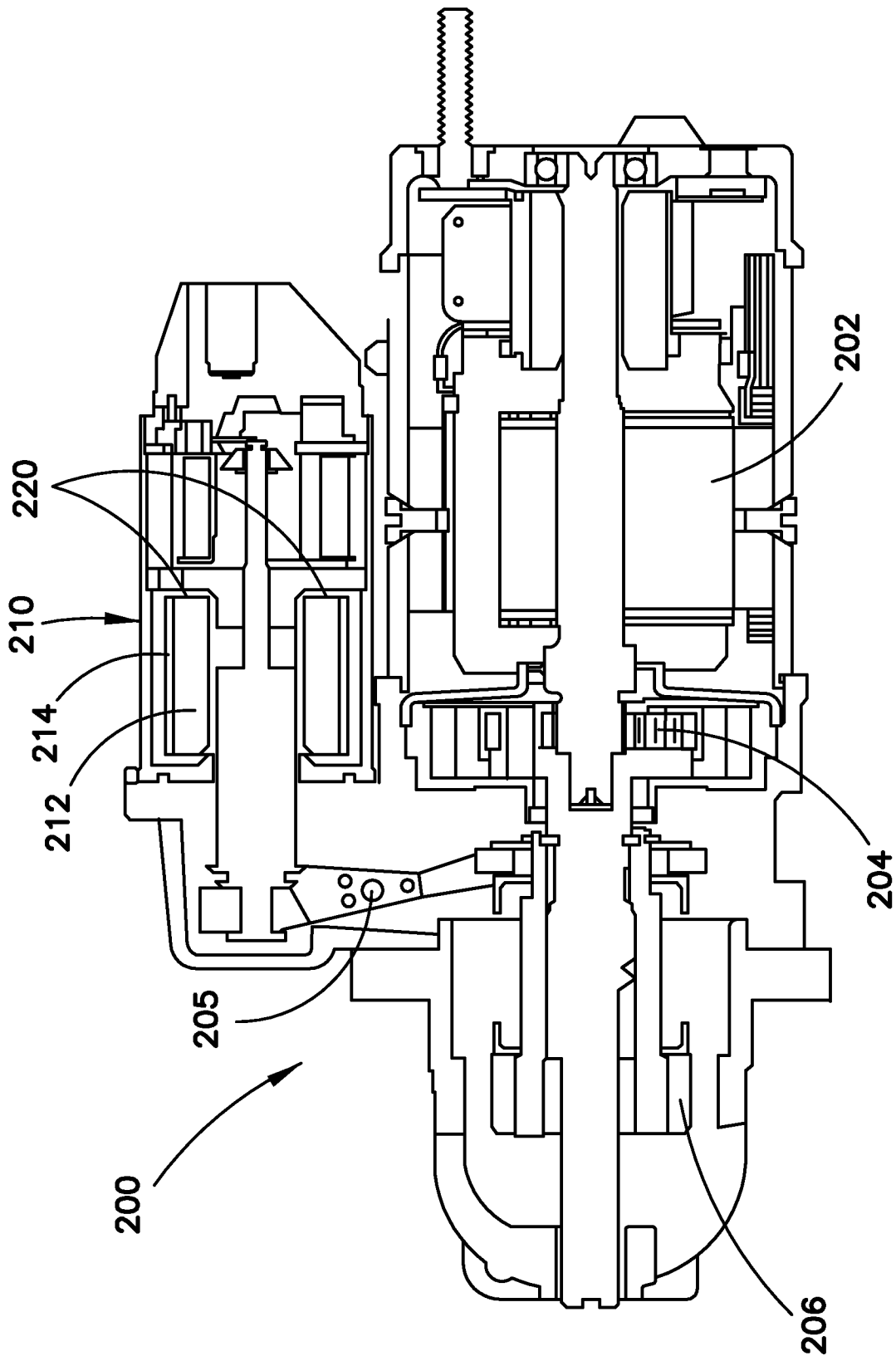


FIG. 15  
PRIOR ART

**INTERNATIONAL SEARCH REPORT**

International application No.  
PCT/US2011/052140

**A. CLASSIFICATION OF SUBJECT MATTER**  
 IPC(8) - F02N 15/06 (2011.01)  
 USPC - 74/6  
 According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**  
 Minimum documentation searched (classification system followed by classification symbols)  
 IPC(8) - F02N 15/06; H02K 7/10; H02N 15/02; H02P 9/94 (2011.01)  
 USPC - 74/6, 7A; 123/339.27, 499; 180/270; 290/38R; 310/75R; 361/160

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)  
 MicroPatent, Google Patents, Google Scholar

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 6,930,409 B1 (SMITH) 16 August 2005 (16.08.2005) entire document	1-5, 16, 19, 20
---		-----
Y		6-15, 17, 18
Y	US 6,598,824 B2 (SCHMIDT) 29 July 2003 (29.07.2003) entire document	6-9, 12, 17, 18
Y	US 4,174,815 A (DAMMAR) 20 November 1979 (20.11.1979) entire document	8-12
Y	US 6,633,099 B2 (FULTON et al) 14 October 2003 (14.10.2003) entire document	13, 14
Y	US 4,178,332 A (HOGEMAN et al) 11 December 1979 (11.12.1979) entire document	15

Further documents are listed in the continuation of Box C.

- |   |  |
|---|--|
| * Special categories of cited documents:  | "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention  |
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| "E" earlier application or patent but published on or after the international filing date   | "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art |
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| "O" document referring to an oral disclosure, use, exhibition or other means  |  |
| "P" document published prior to the international filing date but later than the priority date claimed  |  |

Date of the actual completion of the international search 21 December 2011	Date of mailing of the international search report <b>17 JAN 2012</b>
Name and mailing address of the ISA/US Mail Stop PCT, Attn: ISA/US, Commissioner for Patents P.O. Box 1450, Alexandria, Virginia 22313-1450 Facsimile No. 571-273-3201	Authorized officer: Blaine R. Copenheaver  PCT Helpdesk: 571-272-4300 PCT OSP: 571-272-7774