Office de la Propriété Intellectuelle du Canada
Un organisme d'Industrie Canada

Canadian Intellectual Property Office
An agency of Industry Canada

CA 2804028 C 2015/05/26

(11)(21) **2 804 028**

(12) **BREVET CANADIEN**
CANADIAN PATENT

(13) **C**

(86) **Date de dépôt PCT/PCT Filing Date:** 2011/06/29
(87) **Date publication PCT/PCT Publication Date:** 2012/01/05
(45) **Date de délivrance/Issue Date:** 2015/05/26
(85) **Entrée phase nationale/National Entry:** 2012/12/28
(86) **N° demande PCT/PCT Application No.:** US 2011/042278
(87) **N° publication PCT/PCT Publication No.:** 2012/003196
(30) **Priorité/Priority:** 2010/07/02 (US12/830,039)

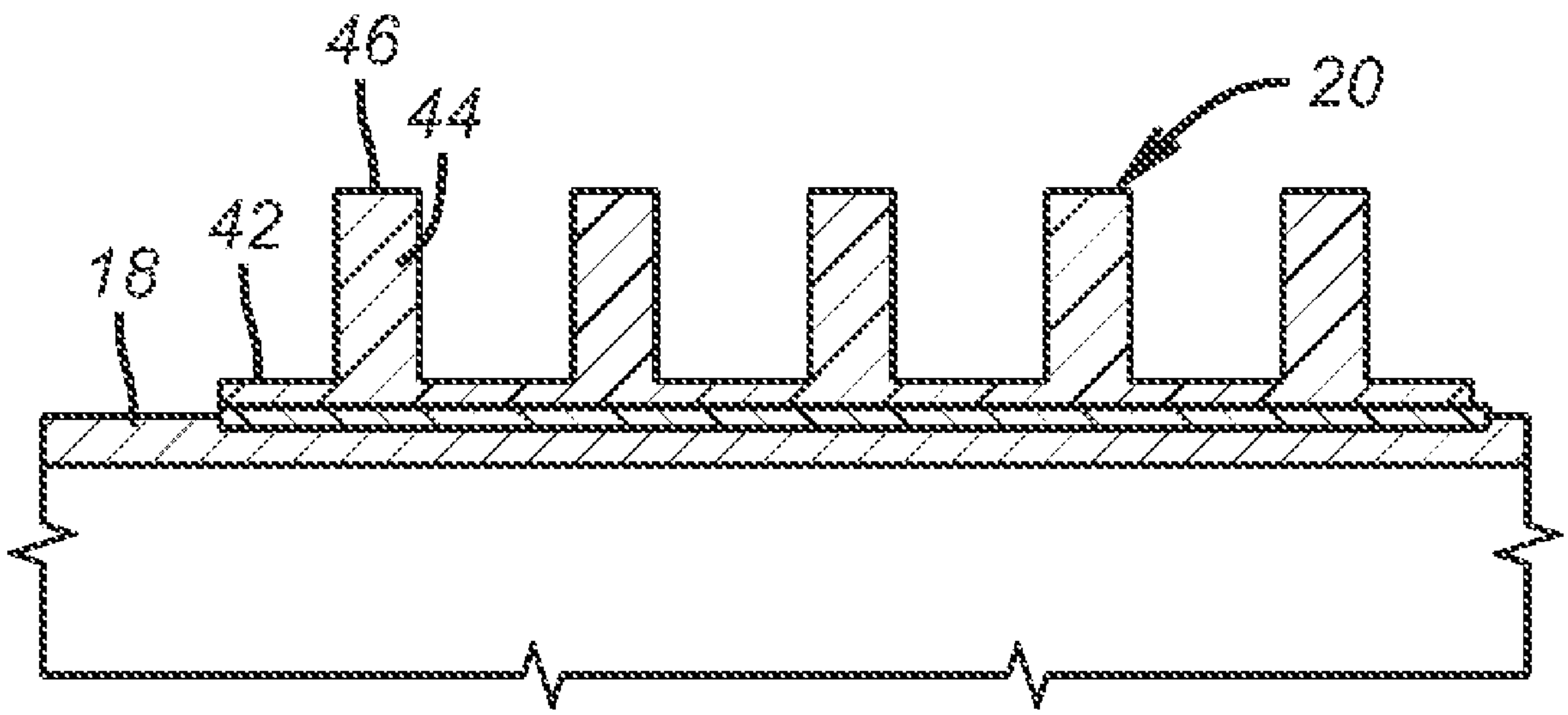
(51) **Cl.Int./Int.Cl.** *E21B 33/13* (2006.01), *E21B 33/138* (2006.01)

(72) **Inventeurs/Inventors:**
MATHEW, THOMAS, US;
JOHNSON, MICHAEL H., US;
ROSENBLATT, STEVE, US

(73) **Propriétaire/Owner:**
BAKER HUGHES INCORPORATED, US

(74) **Agent:** SIM & MCBURNEY

(54) Titre : APPAREIL DE PREVENTION DE MIGRATION DE GAZ ANNULAIRE DE CIMENT A MEMOIRE DE FORME
(54) Title: SHAPE MEMORY CEMENT ANNULUS GAS MIGRATION PREVENTION APPARATUS



(57) **Abrégé/Abstract:**
The annular space around a tubular string has a shape memory material that is in a low profile configuration for run in. After the desired position is obtained and the annulus has cement delivered to fill the annular space, the shape memory device is triggered to revert to an original shape that spans the annulus to seal the tubular and the wellbore sides of the annular space against gas migration through the cement. The structures can have varying run in shapes and can also have original shapes that when the material is triggered will act to displace cement to enhance its compaction on the tubular or the wellbore wall. Combinations of shape memory alloys and polymers are also contemplated to enhance the seal against gas migration.

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau

(43) International Publication Date
5 January 2012 (05.01.2012)

PCT

(10) International Publication Number
WO 2012/003196 A3

(51) International Patent Classification:
E21B 33/13 (2006.01) *E21B 33/138* (2006.01)

(21) International Application Number:
PCT/US2011/042278

(22) International Filing Date:
29 June 2011 (29.06.2011)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
12/830,039 2 July 2010 (02.07.2010) US

(71) Applicant *(for all designated States except US)*: **BAKER HUGHES INCORPORATED** [US/US]; P.O. Box 4740, Houston, TX 77210-4740 (US).

(72) Inventors; and
(75) Inventors/Applicants *(for US only)*: **MATHEW, Thomas** [US/US]; 11011 Pleasant Colony Drive, No. 1627, Houston, TX 77065 (US). **JOHNSON, Michael, H.** [US/US]; 6230 Clear Canyon Drive, Katy, TX 77450 (US). **ROSENBLATT, Steve** [US/US]; 3600 Montrose Boulevard, No. 502, Houston, TX 77006 (US).

(74) Agent: **PORTER, Andre, J.**; Baker Hughes Incorporated, P.O. Box 4740, Houston, TX 77210-4740 (US).

(81) Designated States *(unless otherwise indicated, for every kind of national protection available)*: AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PE, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States *(unless otherwise indicated, for every kind of regional protection available)*: ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Declarations under Rule 4.17:

— *as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))*

— *as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii))*

Published:

— *with international search report (Art. 21(3))*

— *before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments (Rule 48.2(h))*

(88) Date of publication of the international search report:
1 March 2012

(54) Title: SHAPE MEMORY CEMENT ANNULUS GAS MIGRATION PREVENTION APPARATUS

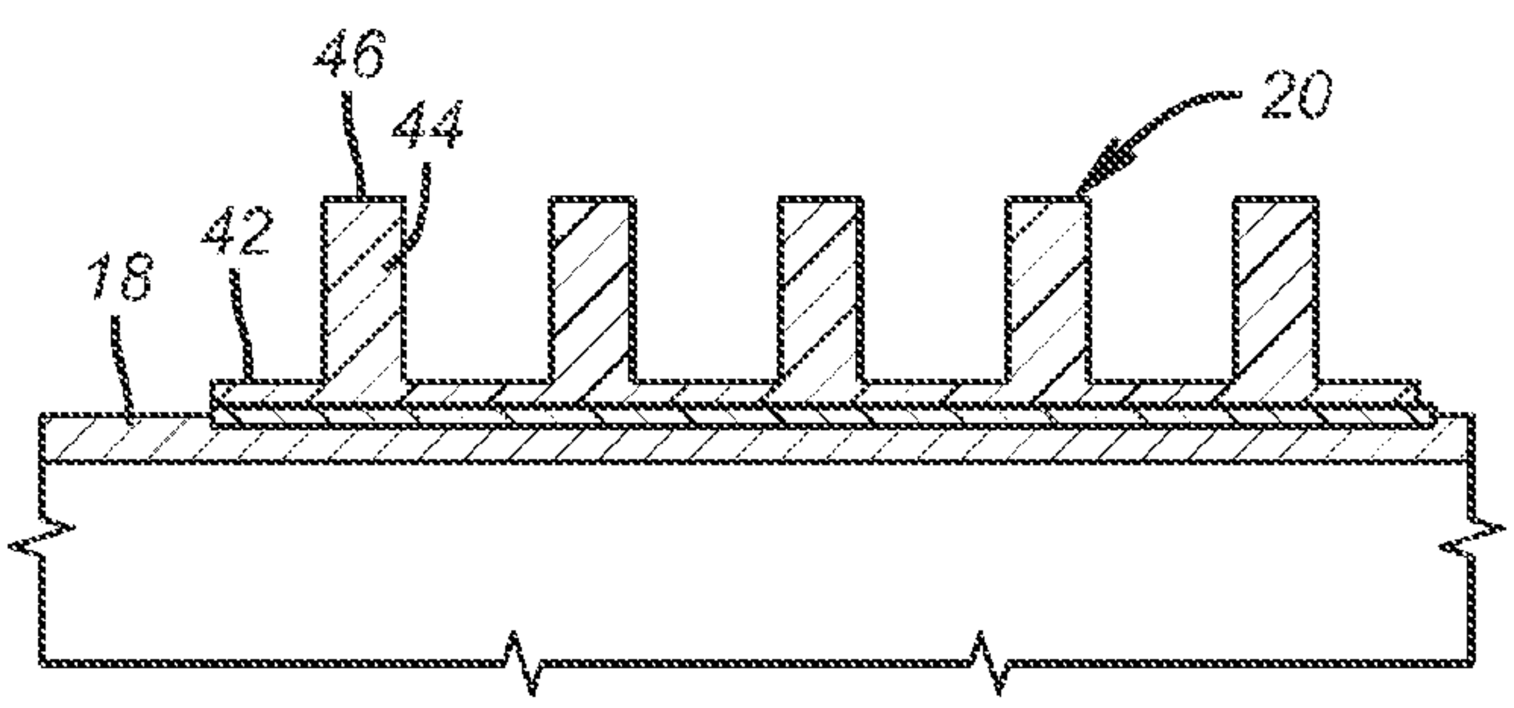


FIG. 5

(57) Abstract: The annular space around a tubular string has a shape memory material that is in a low profile configuration for run in. After the desired position is obtained and the annulus has cement delivered to fill the annular space, the shape memory device is triggered to revert to an original shape that spans the annulus to seal the tubular and the wellbore sides of the annular space against gas migration through the cement. The structures can have varying run in shapes and can also have original shapes that when the material is triggered will act to displace cement to enhance its compaction on the tubular or the wellbore wall. Combinations of shape memory alloys and polymers are also contemplated to enhance the seal against gas migration.

WO 2012/003196 A3

SHAPE MEMORY CEMENT ANNULUS GAS MIGRATION PREVENTION APPARATUS

Inventors: Thomas Mathew; Michael H. Johnson and Steve Rosenblatt

FIELD OF THE INVENTION

[0001] The field of this invention is devices that minimize or prevent gas migration through cement in an annular space around a tubular extending to a subterranean location.

BACKGROUND OF THE INVENTION

[0002] Tubular strings have been sealed in bores with cement. The setting cement can shrink and pull away from the tubular on either side of an annular space or it can pull away from a borehole wall in an open hole cementing application. There can be other causes too such as incomplete mud cake removal or incomplete drilling fluid removal prior to cementing, subsidence and compaction. Cracks can develop later on due to tectonic activities as well. The present invention focuses on gas migration through the set cement as opposed to mitigation of cracks or openings developed after the cement is set. Gas migration through cement can be a dangerous situation and is one of the discussed causes of the Deepwater Horizon accident in the Gulf of Mexico.

[0003] Early efforts to counteract gas migration in cement dealt with methods of delivering the cement or the addition of additives to the cement as illustrated by USP 5,327,969; 5,503,227; 5,199,489; 6,936,574; 7,060,129 and 7,373,981.

[0004] In a wholly unrelated field of artificial hip joints shape memory structures were used to retain fixation cement for the hip joint as described in USP 6,280,477.

[0005] Other applications have involved packers in the annular space that leave channels for cement and use a variety of biasing devices to get the seal material of the packer against the borehole wall. In US Publication 2010/0126735 FIGS. 2 and 3 a base pipe 56 has support members 54 that leave gaps in the annular space 38 for cement to pass. In the FIG. 2B embodiment the member 54 is a shape memory material designed to apply an incremental force to the swelling member 42 off of the tubular 56 to push against the formation 36. Even as to the borehole wall at 36 there are shortcomings of this design in preventing gas migration along the borehole wall. The swelling material can be damaged during run in to the point of openings developing in the swelling layer. The cement in the annular space can still pull away from the seal 42 even if all else functions as planned if the cement experiences shrinkage that causes it to pull away not only from the seal 42 but also from the tubular string 56.

[0006] Another attempt at dealing with cement gas migration was an effort by Halliburton to use rubber sleeves on the tubular exterior so that the sleeves are in the annular space. The idea was to pump the cement into the annulus before the rubber rings swelled to hopefully span the annulus with the hope that gas migration at the tubular could be stopped with a bonded seal of the rubber and that the sleeve would push the cement away as it swelled to the borehole wall before the cement set up. The problem with the design is that the swelling process was so slow that the cement would set ahead of the swelling sleeve so that the outer diameter of the sleeve would never reach the borehole wall and the same issues of gas migrations would still be there as the cement got to the borehole wall and the sleeve outer diameter and shrank from both on setting up, leaving open passages at both locations for gas migration.

[0007] Multistable structural members are described in US Publication 2009/0186196.

[0008] The present invention addresses the issue of gas migration in a new way. It employs shape memory material structures that are secured to the tubular at one end and that when reverting to an original shape, span the annular space by displacing the cement that has yet to set until contact with the open hole or wellbore wall is made that puts the radiating elements of the structure under a compressive load to seal or at least minimize gas migration between zones through the cement. Optionally, the shape memory or bistable structures can be covered in whole or in part with a swelling material. Those and other features of the present invention will be more readily apparent to those skilled in the art from a review of the description of the preferred embodiment and the associated drawings with an understanding that the full scope of the invention is determined from the appended claims.

SUMMARY OF THE INVENTION

[0009] The annular space around a tubular string has a shape memory material that is in a low profile configuration for run in. After the desired position is obtained and the annulus has cement delivered to fill the annular space, the shape memory device is triggered to revert to an original shape that spans the annulus to seal the tubular and the wellbore sides of the annular space against gas migration through the cement. The structures can have varying run in shapes and can also have original shapes that when the material is triggered will act to displace cement to enhance its compaction on the tubular or the wellbore wall. Combinations of shape memory alloys and polymers are also contemplated to enhance the seal against gas migration. An outer coating of a swell material can be used.

[0009a] Accordingly, in one aspect there is provided a gas migration control assembly for an annular space surrounding a tubular in a subterranean location defined by a borehole wall and further containing a sealing material, the assembly comprising: the tubular having an outer surface; the sealing material in the annular space between the tubular and the borehole wall; a gas migration control device having at least one member mounted on the outer surface of the tubular and held in alignment with the outer surface on a long dimension thereof; the gas migration control device mounted to the outer surface of the tubular, the gas migration control device having a smaller dimension for facilitating insertion to the subterranean location and a larger dimension spanning the annular space with a transition to the larger dimension selectively triggered thermally from well fluid when the annular space in the vicinity of the gas migration control device is substantially full with the sealing material so that the transition to the larger dimension selectively triggered thermally from well fluid of the gas migration control device alone displaces the sealing material in making contact with the borehole wall to at least impede gas migration through the sealing material in the annular space; and the gas migration control device comprising an annular cylindrical shape in the smaller dimension configured to extend the at least one member and, when thermally triggered, the at least one member moves away from the alignment with the outer surface and generally radially toward the borehole wall to engage the borehole wall such that a compressive stress is generated within the at least one member.

BRIEF DESCRIPTION OF THE DRAWINGS

[0010] FIG. 1 is a section view of a gas migration barrier during run in;

[0011] FIG. 2 shows the gas migration barrier deployed;

[0012] FIG. 3 shows deployment of the barrier that can start in the middle and progress to the opposed ends to displace cement;

[0013] FIG. 4 illustrates a capability of the barrier to act as a piston to displace cement into enhanced contact to the formation and the tubular that define the annular space;

[0014] FIG. 5 shows one configuration of the gas migration barrier made up of parallel discs in the initial shape before run in;

[0015] FIG. 6 is the view of FIG. 5 after application of compression above the transition temperature and removal of the heat with compaction forces still applied so that a low profile shape is maintained;

[0016] FIG. 7 shows reversion to the original shape at the formation when the temperature again crosses the transition temperature;

[0017] FIG. 8 shows the use of solid rings or a coil in an initial condition before compaction to the supporting tubular;

[0018] FIG. 9 is the view of FIG. 8 after compaction at above the transition temperature and removal of the heat while still compacting to hold the low profile shape that is depicted;

[0019] FIG. 10 shows a series of rings or a coil where shape memory polymers are backed by shape memory alloys before compaction at above the critical temperature takes place;

[0020] FIG. 11 is the view of FIG. 10 after compaction at above the transition temperature followed by removal of the heat while holding the compaction force to get a low profile for run in;

[0021] FIG. 12 is the view of FIG. 11 when the transition temperature is crossed near the formation;

[0022] FIG. 13 is an alternative embodiment in its original shape of an angular structure;

[0023] FIG. 14 is the view of FIG. 13 after crossing the transition temperature and applying a compressive force followed by heat removal while holding the compressive force to get a low profile of the gas migration barrier for run in;

[0024] FIG. 15 is the view of FIG. 14 with the transition temperature crossed at the formation and the barrier reverting to its original FIG. 13 shape;

[0025] FIG. 16 is an alternative embodiment to FIG. 5 with a swelling material around the projecting members and between the tubular and the gas migration barrier;

[0026] FIG. 17 is the view of FIG. 16 after the combined application of heat and compression followed by removal of heat while maintaining compression to retain the illustrated shape;

[0027] FIG. 18 is the view of FIG. 17 after the addition of heat at the desired location so that the shape attempts to revert to the initial FIG. 16 shape and the swelling material swells to enhance the gas migration barrier performance.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0028] FIG. 1 shows zones **10** and **12** of a formation where there is a borehole **16** that has a string **18**, in this example being casing, and a gas migration device **20** in the annular space **22** that will be filled with cement or another sealing material **24**. In the run in position the device **20** has a low profile annular shape and is preferably made of a shape memory material. Of the available shape memory materials an alloy is further preferred. Other materials that can be run in with a smaller profile and then converted to another shape or volume with a stimulus that is added to the bore **14** or uses the fluids in the bore **14** can also be deployed such as bistable materials triggered with a mechanical impact or bending force. Bistable materials can be used in isolation as a gas migration device or combined with shape memory materials to aid the transformation of the shape memory device when reverting to an original shape.

[0029] In FIG. 2 the exposure to well fluids has imparted enough heat to the device **20** to allow it to revert to an original shape that is larger than its run in shape so that contact with the borehole wall **16** is achieved while the cement **24** is pushed out of the way. In this configuration, there is a seal to the tubular **18** and the borehole wall **16** by the device **20**. The device **20** in the FIG. 2 configuration has internal compressive stress from pushing against the borehole wall **16** on one side and against the tubular **18** on the opposite side. There are no issues of cement shrinkage as the seal is made in a zone where the cement is displaced before it has had a chance to set up. As an alternative to the use of the well fluids to get the device **20** across its transition temperature so that it can revert to an original shape, auxiliary heat **H** can be added to initiate the transformation and maintain it to the end position illustrated in FIG. 2. Another available source for heat can be the heat given off by the cement as it sets or from reactions between or among ingredients or additives to the cement **24**. A shape memory alloy for the entire device **20** is preferred as alloys will create more compressive stress when abutting the wellbore wall **16** than for example a shape memory polymer. However, alloy and polymer shape memory materials can also be combined in a single device or different compositions of alloys or polymers can be used in a single device as will be discussed below.

[0030] FIG. 3 is illustrative of using a mix of materials that trigger at different temperatures to revert to an original shape so that the cement **24** can be more efficiently removed from between the growing device **20** and the wellbore wall **16**. For example FIG. 3 shows a portion of a shape memory alloy **26** triggered to revert to the original shape from the middle of the device **20** so that the cement is initially pushed toward opposed ends as indicated by arrows **28** and **30**. When the temperature is further increased to a higher level either using the well fluid or external sources such as **H**, other segments such as **32** and **34** will start in sequence to change shape and any cement **24** between those segments and the wellbore wall **16** will be pushed out beyond the opposed ends of the device **20** in the direction of arrows **28** and **30**.

[0031] FIG. 4 illustrates a different application of materials that revert to an original shape at differing transition temperatures. In this case the segment **36** moves first and acts as a piston on the cement **24** to drive it toward the wellbore wall **16**. Ultimately on reaching an even higher trigger temperature, the segment **38** will begin to revert to its original shape, which is not necessarily the same as the original shape of segment **36**. Those skilled in the art will appreciate that the shape change on reversion that is triggered by crossing the transition temperature can involve change in volume to some degree as well as a more dramatic change in shape. In this example the internal pressure in the cement **24** is raised by the device **20**. Arrow **40** indicates that there is a one way flow of cement **24** into the annulus **22** usually through a cement shoe that has check valves to prevent cement backflow. Thus the use of the device **20** as a piston is also operative to reduce gas migration through the cement **24** even without forcing out the cement from the entire length of the device **20**.

[0032] FIG. 5 illustrates a design with an annularly shaped hub **42** sealingly secured to an outer surface of a tubular string **18** with a series of discs **44** having an outer end **46**. When this shape is reverted to in the desired location it is intended that the ends **46** engage the formation such as **10** or **12** in a manner where the disc ends **46** are compressed and even slightly misshaped as shown in FIG. 7. The shapes **44** can be equally spaced or randomly spaced. The outer shape at **46** can be circular or rectangular or another shape designed to make fully circumferential contact with the wellbore **10** upon shape reversion when crossing the transition temperature. The original shape of FIG. **5** has to be reduced in profile for running in to the FIG. 7 location. This is done by applying compression while increasing the bulk temperature of the device to above the transition temperature and then holding the compressive force while reducing the temperature of the device **20**. In the FIG. 6 configuration, the extending members have been flattened into an essentially annular shape with a fairly low profile as comparing it to the original shape. Note that the extending member shapes are still discernable in FIG. 6 even though the overall profile has been greatly reduced for run in. The benefit of minimizing damage to the device **20** is clearly understood from a comparison of these FIGS. Application of heat from whatever source results in FIG. 7 of a reversion to the FIG. 5 shape. The fact that there is some distortion at the ends **46** reflects that the wellbore **16** may not let each shape fully extend to its original dimension thus forcing some of the ends and preferably all the ends **46** into some degree of deformation indicative that the annulus **22** has been spanned by a shape memory material and that a gas migration seal is in place against the tubular **18** and the borehole **16**.

[0033] FIGS. 16-18 are an alternative embodiment to FIGS. 5-7 with the difference being the addition of a cover of a swelling material **45** on the shapes **44** and their ends **46**. Another layer of a swelling material **47** can be placed between the tubular **18** and the hub **42**. Even with the addition of the swelling material **47** the hub **42** can still be affixed to the tubular **18** with fasteners or by welding. The swelling material **45** and **47** can be continuous to wholly envelop the shape illustrated or it can be segmental and applied in locations where it will have the most impact such as at the ends **46** or as one or more rings up against the tubular **18**. As before, the original position of FIG. 16 is altered with temperature above the transition point and compression followed by removal of heat while maintaining compression to hold the shape of FIG. 17 for a low profile for running in. When reaching the desired location as shown in FIG. 18 heat from well fluids or/and another stimulus such as impact or bending will cause the gas migration barrier to revert to the FIG. 16 shape with some distortion as shown in FIG. 19 against the borehole wall **16** as the shape retains compressive stress due to contact with the tubular **18** and the borehole wall **16**. The well fluids or added fluids will also cause the swelling material such as rubber to change shape or volume both at the tubular **18** and the wellbore wall **16** to compensate for any tendency of the cement to pull away as it shrinks slightly when setting up. Other swelling materials that swell in the presence of hydrocarbons or water are also contemplated.

[0034] FIG. 8 illustrates the use of a stack of rings or a coiled spring **48** in an initial configuration using a shape memory material and FIG. 9 is the lower profile configuration for run in that is obtained with compression at above the transition temperature so that an annular cylindrical shape is obtained. Removal of heat with the compression force still applied will result in retention of the FIG. 9 shape until heat is applied from whatever source and the device **20** is at the proper location. At that time the shape will revert to the FIG. 8 shape but the rings **48** will likely not fully assume the original FIG. 8 shape. It is preferred that some deformation of the rings or coil **48** take place so that the shape or shapes can be in compression to form a gas migration seal or at least an impeding structure in the cemented annulus in which the rings or coil **48** are disposed.

[0035] FIG. 10 is a variation on FIG. 8 in that the rings or coil **50** are a composite structure with a shape memory alloy internally at **52** and a shape memory polymer on the outside at **54**. As before the FIG. 11 position is the low profile position for run in and the FIG. 12 position is after heat is applied at the desired location in the borehole **16**. Note that the alloy creates the compressive strength on reversion of shape into contact with the wellbore. On the other hand the polymer is softer on reversion toward the original shape of FIG. 10 so that it acts as a sealing material that is more readily spread by the compressive stress created by the alloy core **52**. While a hollow center **56** is used to reduce the required energy to force the initial shape change and to facilitate the reversion to the original shape, a solid center **56** is also envisioned.

[0036] FIGS. 13-15 show another variation of an initial angular shape **58** that is secured at **60** to the tubular **18** and has a cantilevered free end **62** spaced from the tubular **18**. Alternatively, the free end **62** can be secured to the tubular **18.** As before the transition temperature is crossed with application of compressive force to attain the annular cylinder shape of FIG. 14 followed by heat removal while maintaining the compressive force so that the FIG. 14 shape is obtained. In the wellbore **16** where heat is added to the shape to get the shape above the transition temperature, the result is that the bent portion **64** penetrates the wellbore **16** thereby providing a gas migration seal to the cement **24** by spanning from the tubular **18** to the wellbore wall **16** while displacing the cement **24** from the contact location with the wellbore **16**.

[0037] Those skilled in the art will appreciate that the present invention in its various embodiments allows for a low profile for run in so that the gas migration device is not likely to be damaged and an ability to change shape and/or volume to span an annular cemented space before the cement sets so that it can function to slow down or eliminate gas migration. The fact that the cement shrinks when setting is not a factor in the operation of the device that spans the annular gap despite the presence of cement. While a shape memory alloy is preferred the entire device can be a composite of different alloys with stages transition temperatures so that portions of the device can deploy in a predetermined sequence so as to more effectively push the cement out of the way before contact with the formation is initiated. The device can also act as a piston to apply a compressive force to the cement to push some of the cement into the borehole wall in formations with fractures or apertures and at the same time to have the device span the annular space so that gas migration can also be retarded or halted by the device. While variations of the device are shown in the drawings in a single location, multiple locations are contemplated. At each location, the design can be a single shape initially or a plurality of adjacent shapes that can be compressed into a single shape when above the transition temperature to get the desired low profile shape. Combinations of alloys and polymers or alloys and foams are contemplated to take advantage of the compressive force that an alloy can create when transitioning back to an original shape and the polymer that gets softer on reverting to an original shape so that it can enhance the sealing capability at the borehole wall. Alternatively, sharp angles such as in FIGS. 13-15 can be used in either a cantilevered design or one supported at multiple locations to the tubular string.

[0038] The scope of the claims should not be limited by the preferred embodiments set forth above, but should be given the broadest interpretation consistent with the description as a whole.

What is claimed is:

1. A gas migration control assembly for an annular space surrounding a tubular in a subterranean location defined by a borehole wall and further containing a sealing material, the assembly comprising:

the tubular having an outer surface;

the sealing material in the annular space between the tubular and the borehole wall;

a gas migration control device having at least one member mounted on the outer surface of the tubular and held in alignment with the outer surface on a long dimension thereof;

the gas migration control device mounted to the outer surface of the tubular, the gas migration control device having a smaller dimension for facilitating insertion to the subterranean location and a larger dimension spanning the annular space with a transition to the larger dimension selectively triggered thermally from well fluid when the annular space in the vicinity of the gas migration control device is substantially full with the sealing material so that the transition to the larger dimension selectively triggered thermally from well fluid of the gas migration control device alone displaces the sealing material in making contact with the borehole wall to at least impede gas migration through the sealing material in the annular space; and

the gas migration control device comprising an annular cylindrical shape in the smaller dimension configured to extend the at least one member and, when thermally triggered, the at least one member moves away from the alignment with the outer surface and generally radially toward the borehole wall to engage the borehole wall such that a compressive stress is generated within the at least one member.

2. The assembly of claim 1, wherein:

the gas migration control device comprises at least one shape memory material.

3. The assembly of claim 1 or 2, wherein:

the selective triggering comprises using heat added to the subterranean location.

4. The assembly of claim 3, wherein:

at least some of the added heat comes from setting up of the sealing material.

5. The assembly of any one of claims 1 to 4, wherein:

portions of the gas migration control device are triggered at different temperatures than other portions of the gas migration control device.

6. The assembly of claim 2, wherein:

the gas migration control device comprises shape memory polymer mounted over shape memory alloy such that upon triggering the shape memory polymer engages the borehole wall.

7. The assembly of claim 2, wherein:

the gas migration control device is sealingly secured to the tubular in the smaller and the larger dimensions.

8. The assembly of claim 7, wherein:

the at least one member has a rounded outer periphery and substantially parallel orientation with substantially equal axial spacing.

9. The assembly of claim 7, wherein:

the gas migration control device comprises an annular cylindrical shape in the smaller dimension and an angular shape having an intermediate point in the larger dimension.

10. The assembly of claim 9, wherein:

the angular shape has opposed ends with at least one end affixed to the tubular.

11. The assembly of claim 10, wherein:

the intermediate point engages the borehole wall so that between the at least one end affixed to the tubular and the intermediate point gas migration through the sealing material is at least impeded.

12. The assembly of claim 2, wherein:

the gas migration control device in the larger dimension comprises one of a plurality of rings and a coiled shape and one of a hollow and a solid core.

13. The assembly of claim 12, wherein:

the one of the plurality of rings and the coiled shape coil further comprising a core of shape memory alloy covered by shape memory polymer with the shape memory polymer contacting and being deformed and carrying a compressive stress by the contact when the transition to the larger dimension occurs.

14. The assembly of claim 10, wherein:

the gas migration control device initially displaces the sealing material from an inner location out toward at least one of the opposed ends.

15. The assembly of claim 2, wherein:

the gas migration control device axially displaces the sealing material to increase contact pressure of the sealing material to the borehole wall past one end of the gas migration control device while at least a portion of the gas migration control device spans the annular space to engage the borehole wall.

16. The assembly of any one of claims 1 to 15, wherein:

wherein the gas migration control device is made at least in part of a bistable material.

17. The assembly of claim 16, wherein:

the gas migration control device is made at least in part of a shape memory alloy.

18. The assembly of claim 2, wherein:

the gas migration control device comprises a swelling material on an outer periphery thereof.

19. The assembly of claim 18, wherein:

the swelling material covers the gas migration control device at least in part and is positioned for contact with the borehole wall.

20. The assembly of claim 19, wherein:

the swelling material is disposed against the tubular.

21. The assembly of claim 1, wherein:

the at least one member comprise a swelling material on an outer periphery thereof.

22. The assembly of claim 21, wherein:

the swelling material covers the at least one member at least in part and is positioned for contact with the borehole wall.

23. The assembly of claim 22, wherein:

the swelling material is disposed against the tubular and the annular cylindrical shape.

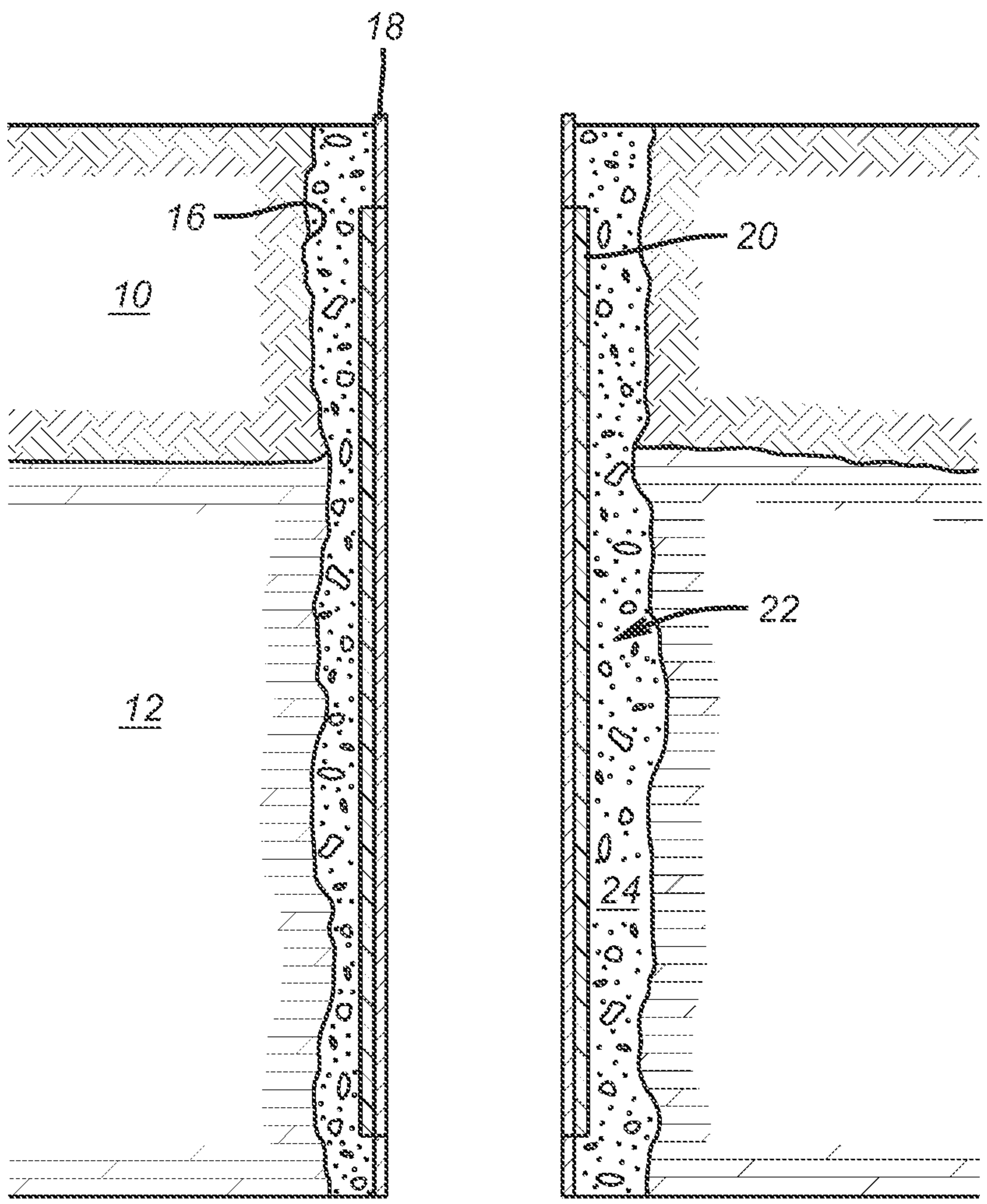


FIG. 1

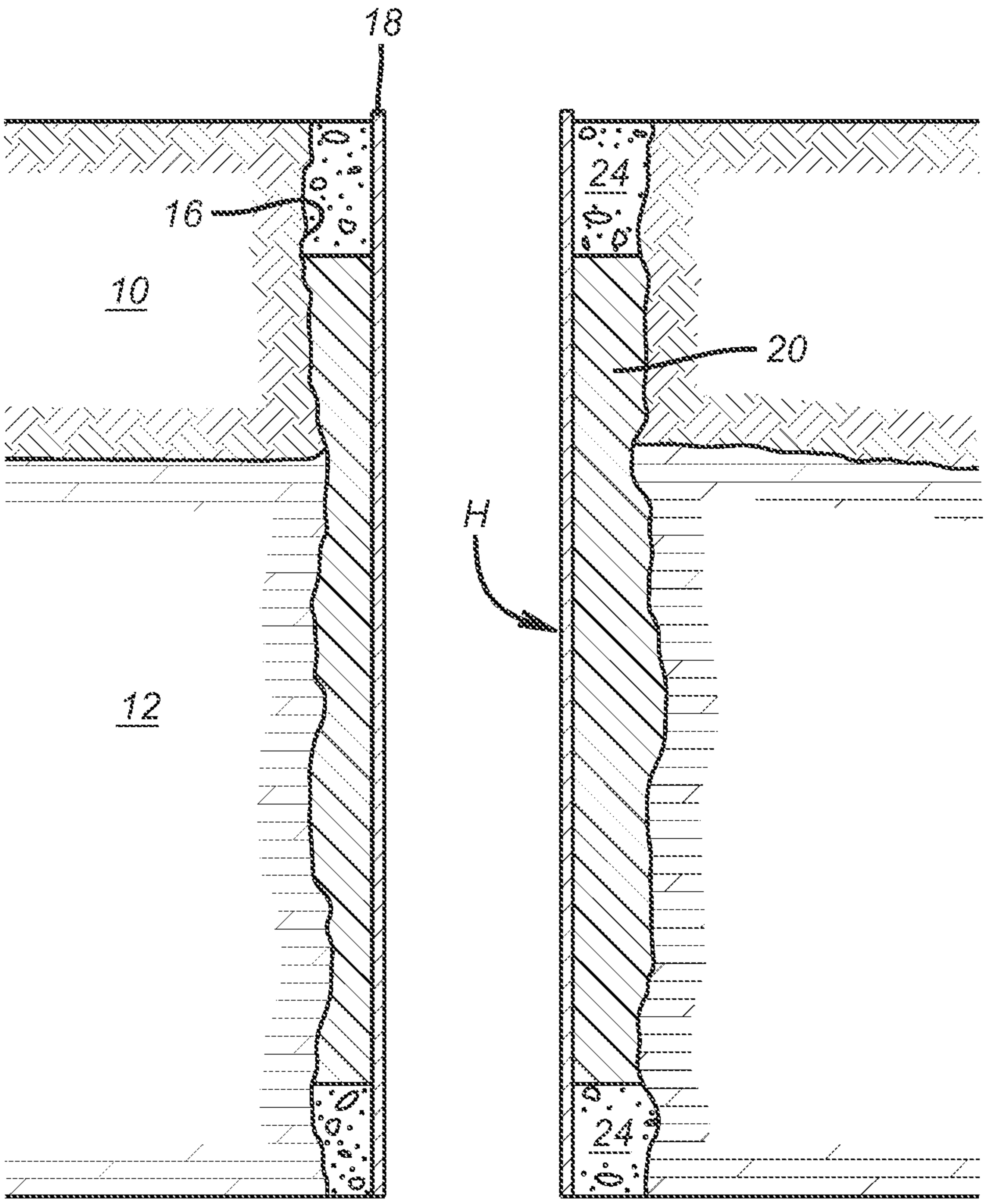


FIG. 2

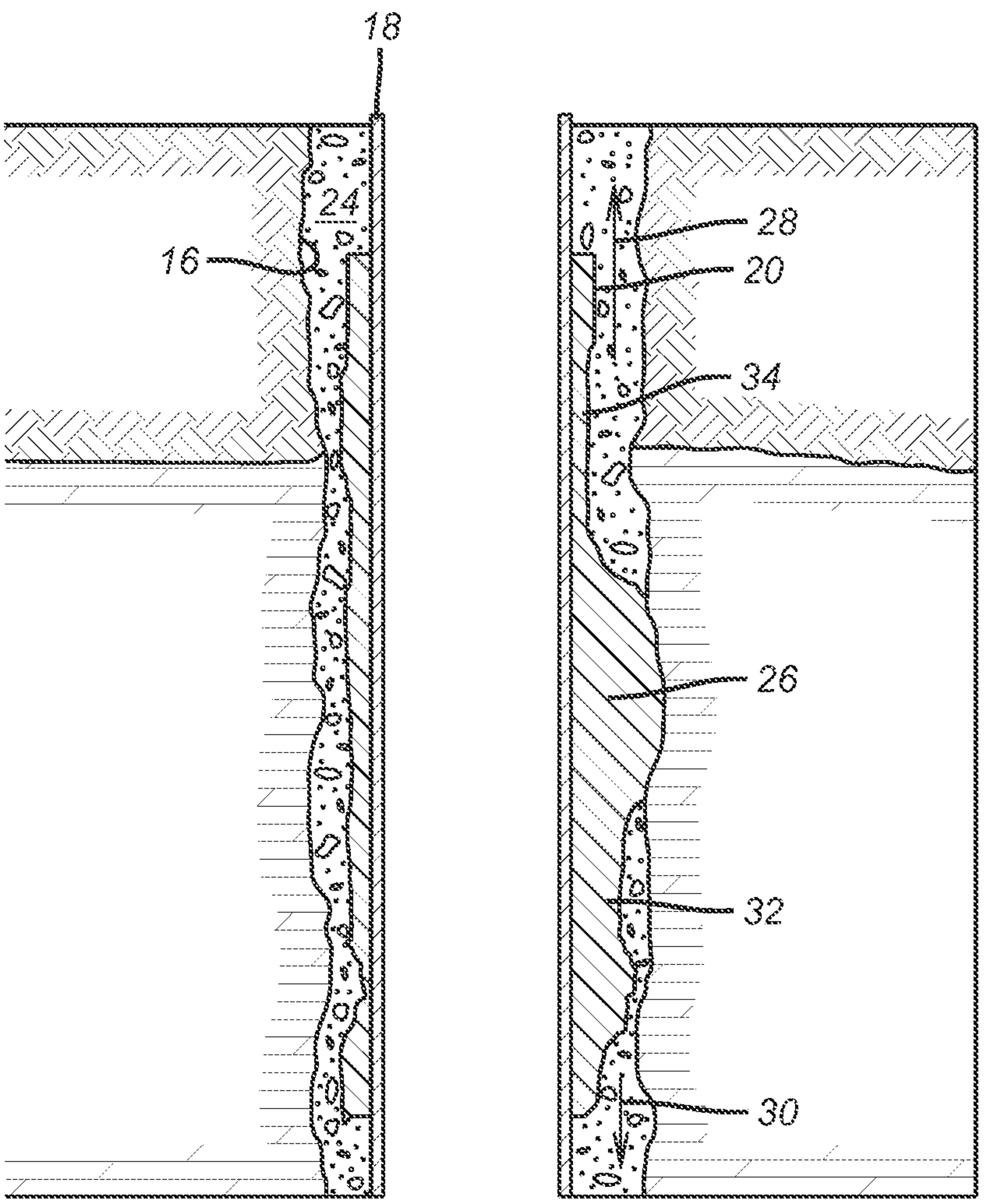


FIG. 3

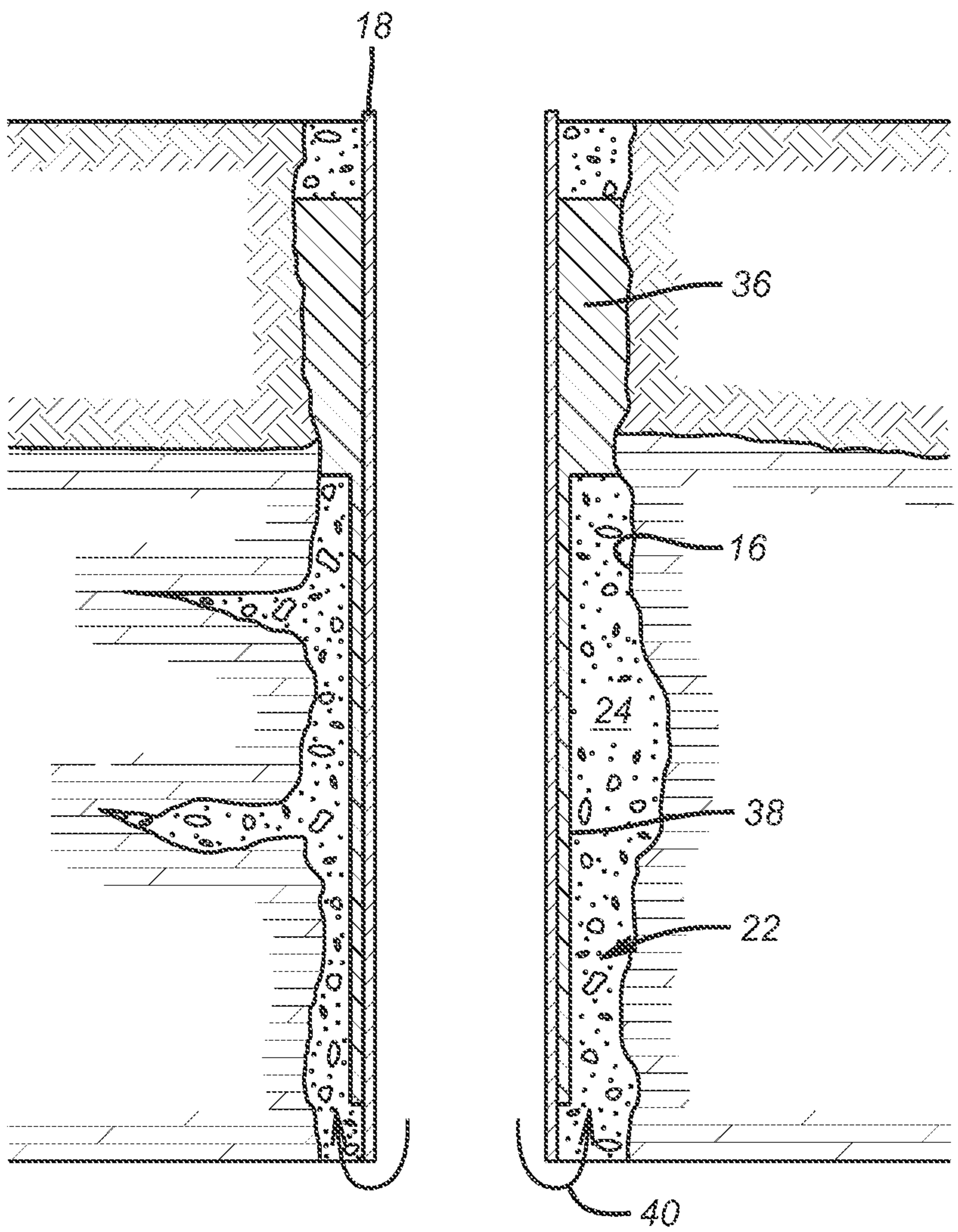


FIG. 4

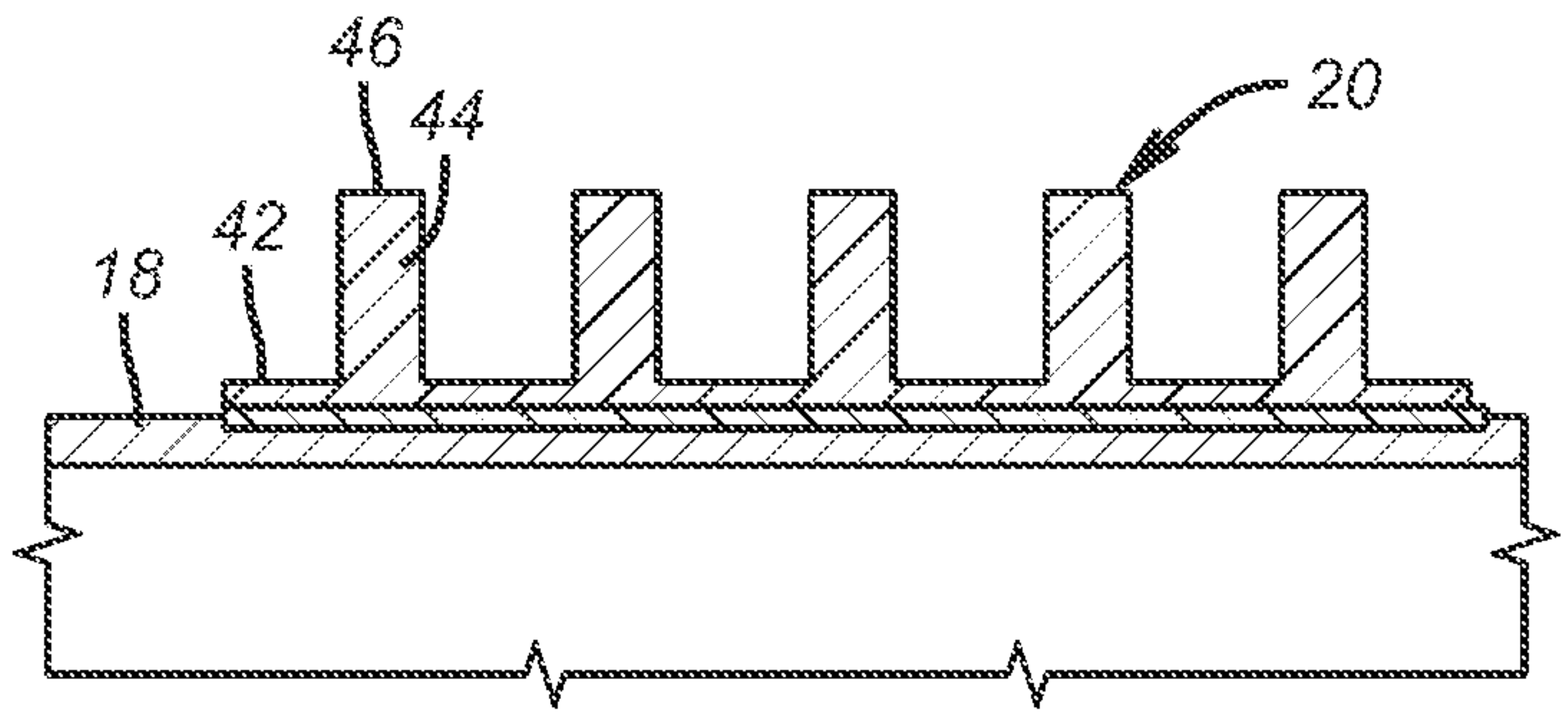


FIG. 5

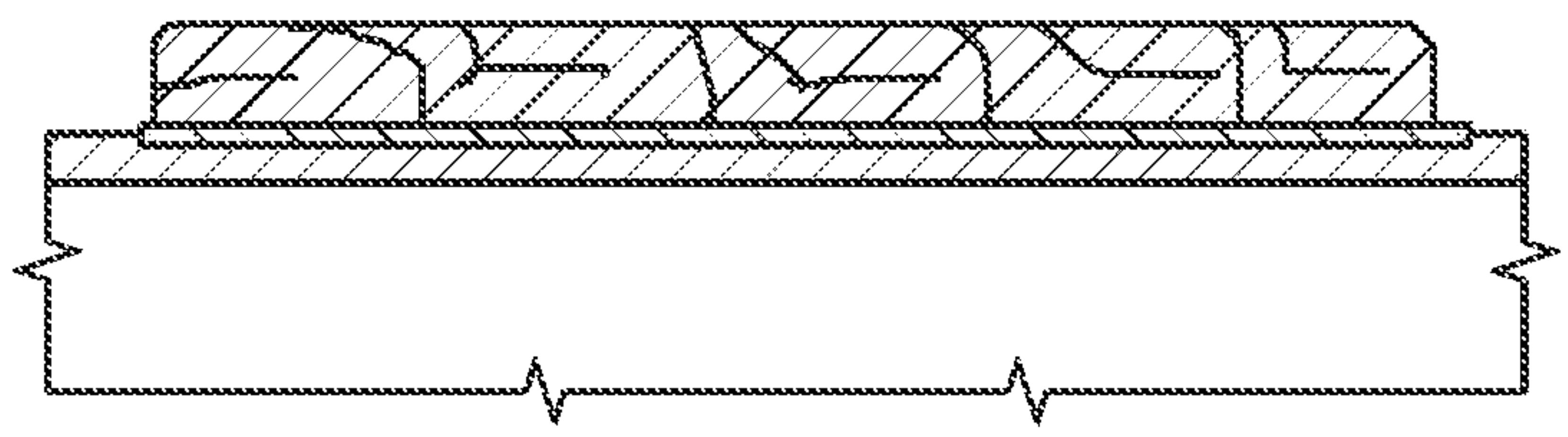


FIG. 6

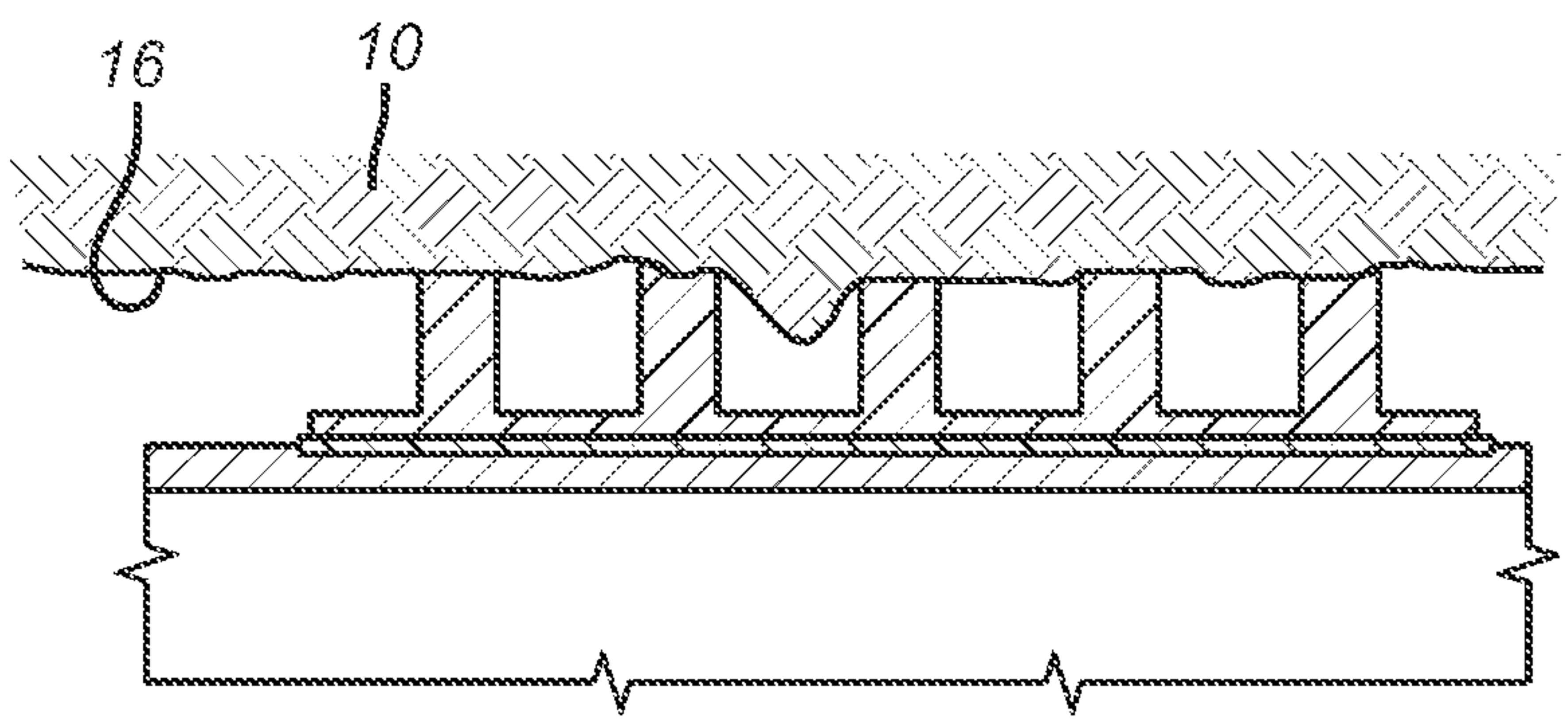


FIG. 7

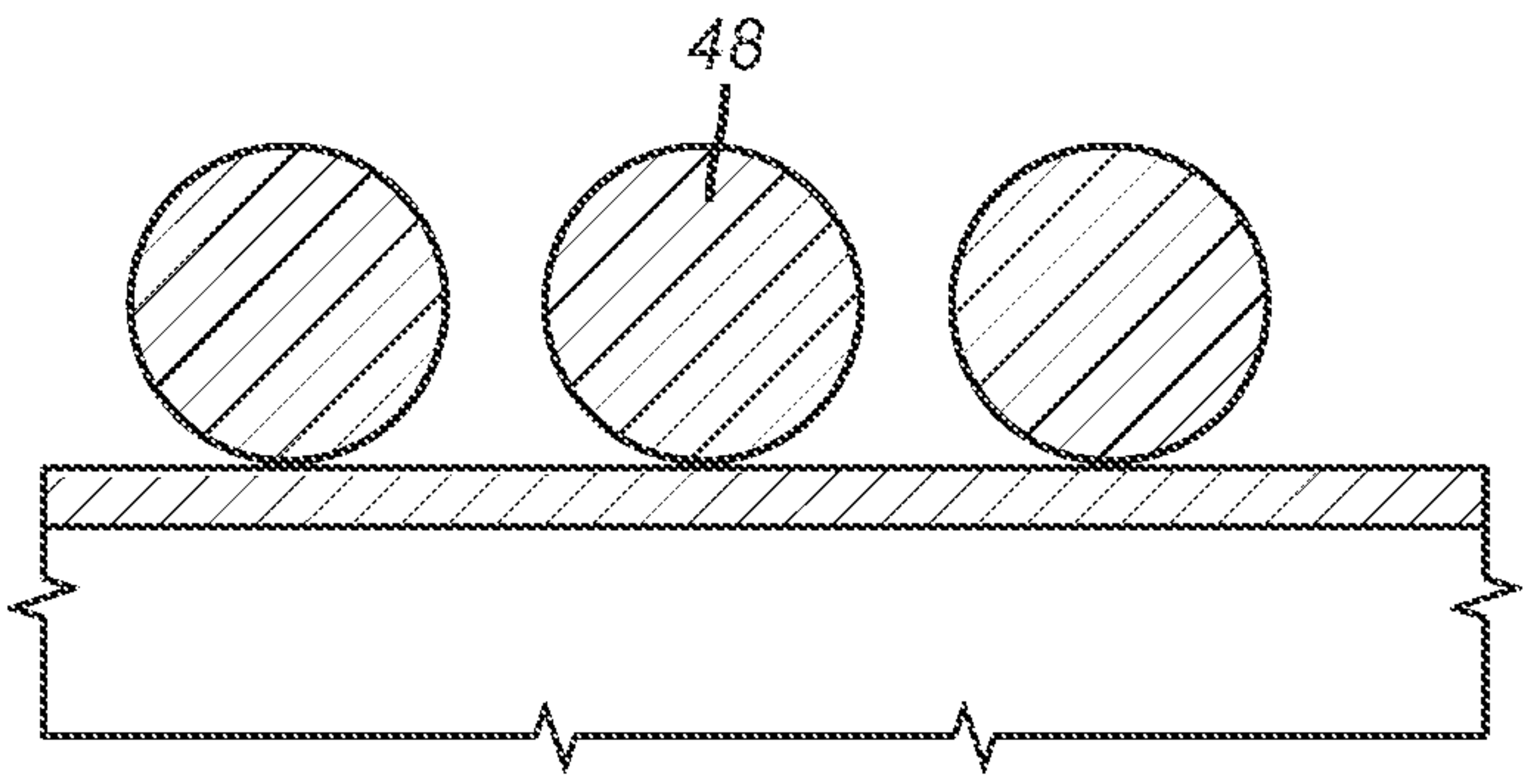


FIG. 8

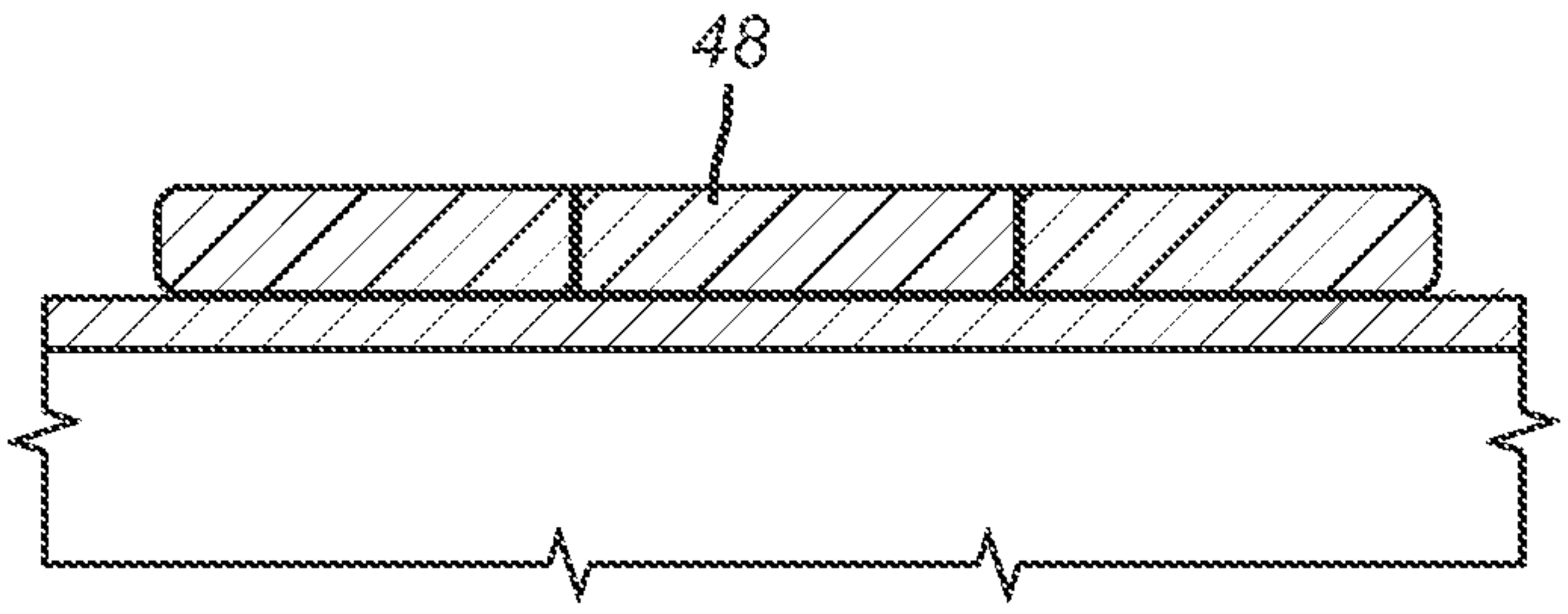


FIG. 9

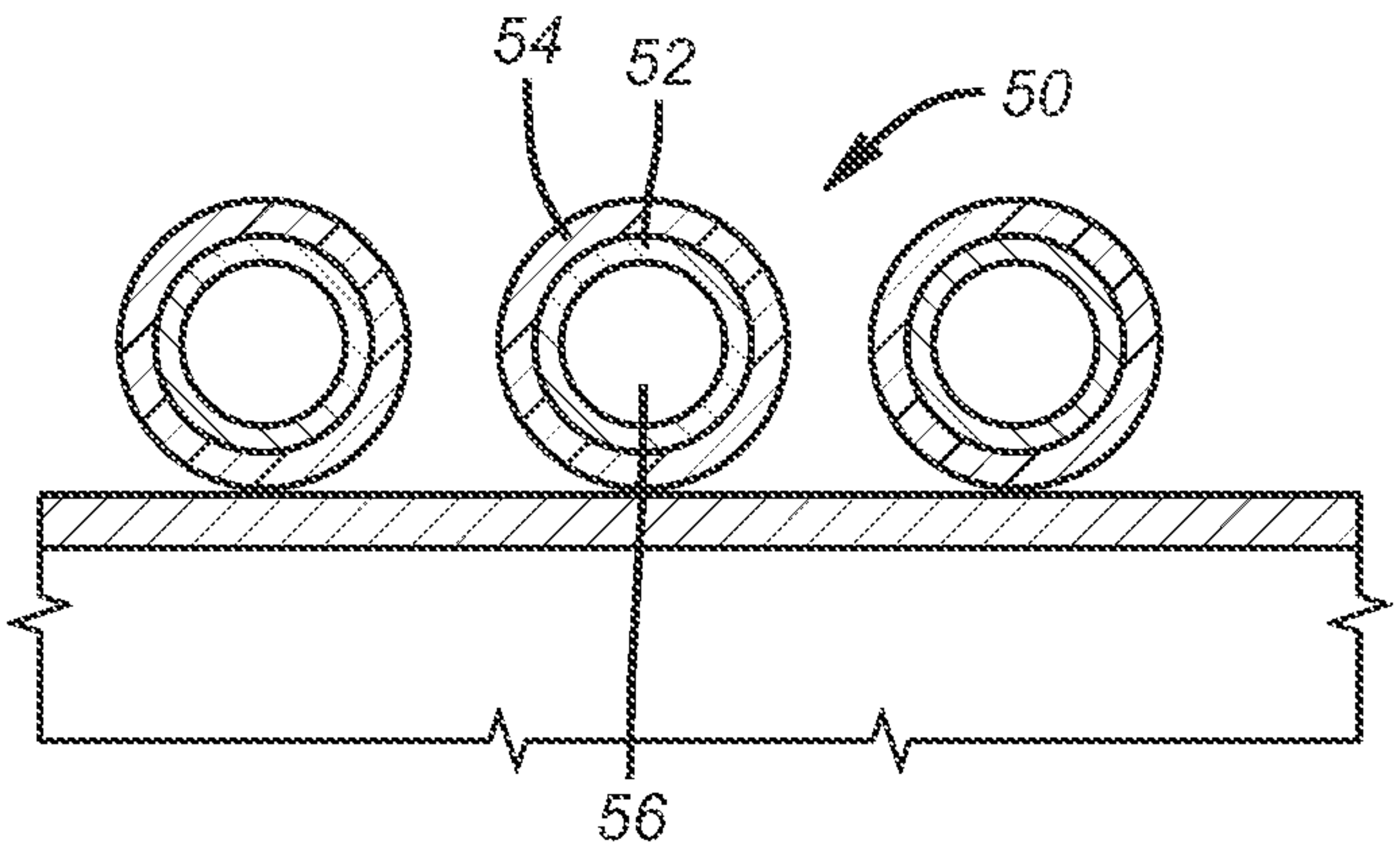


FIG. 10

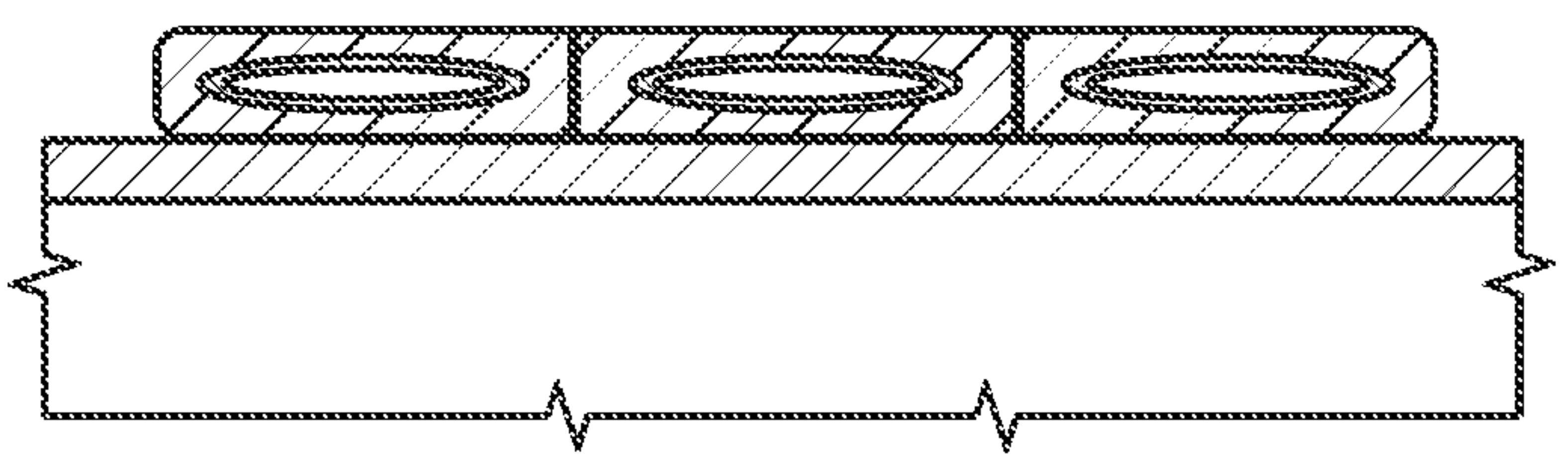


FIG. 11

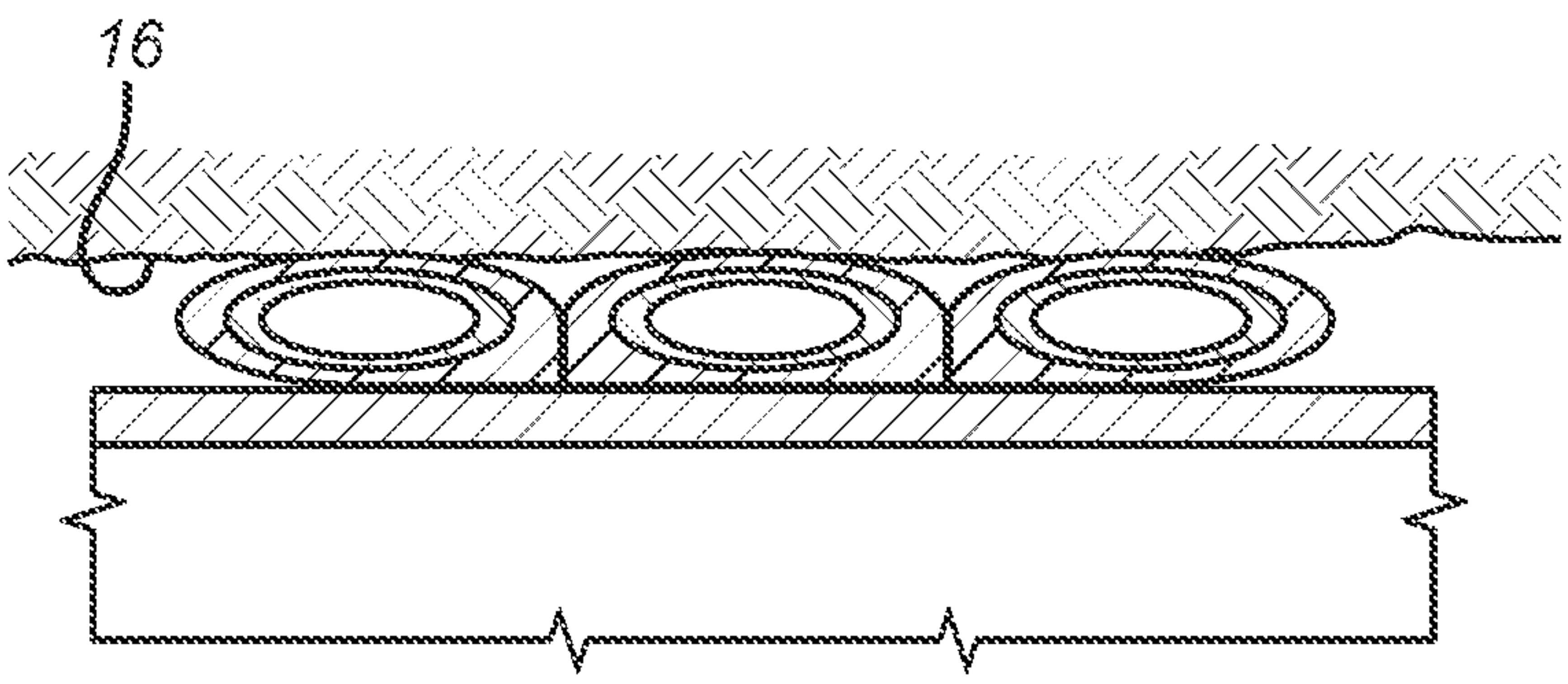


FIG. 12

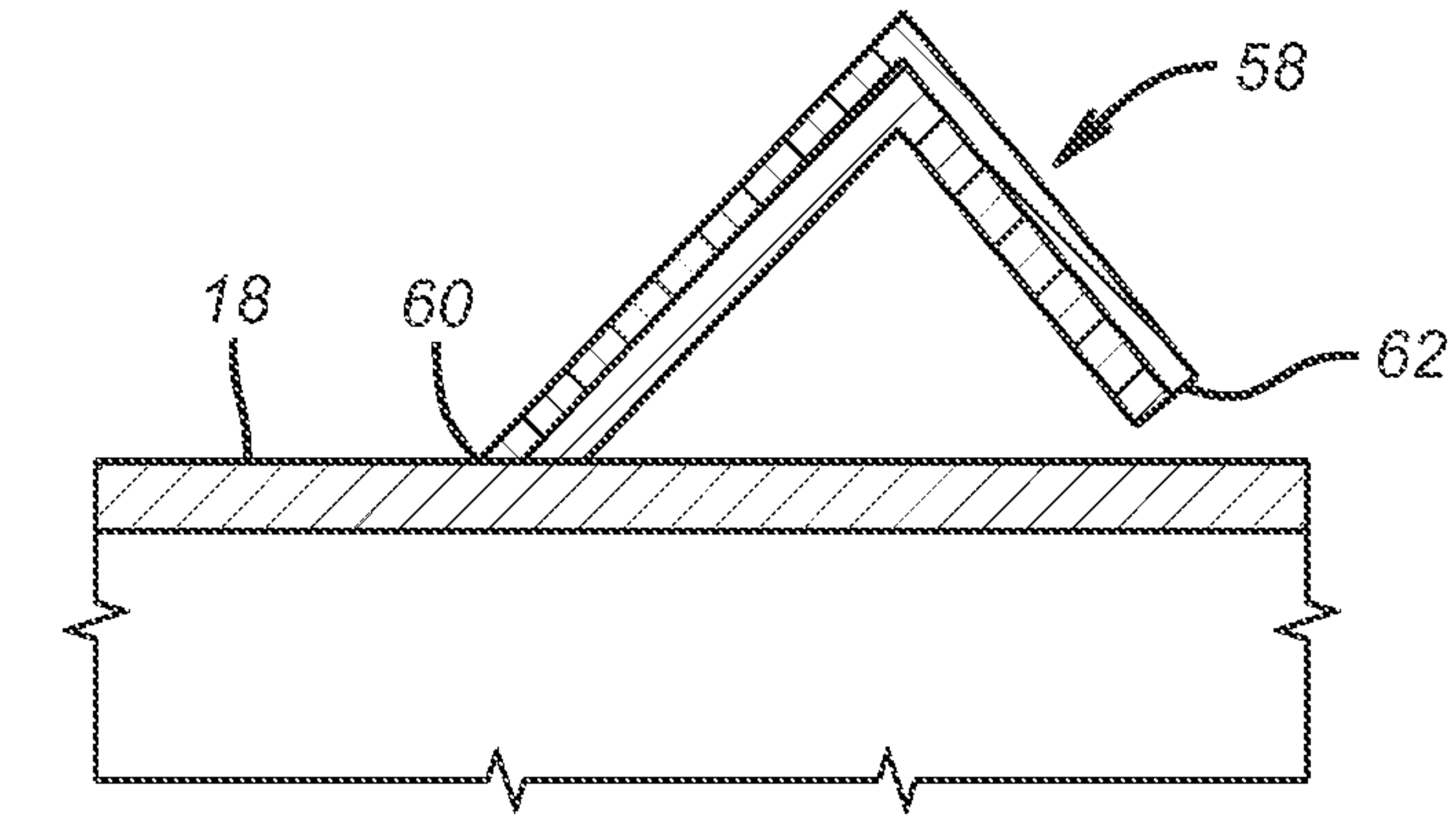


FIG. 13

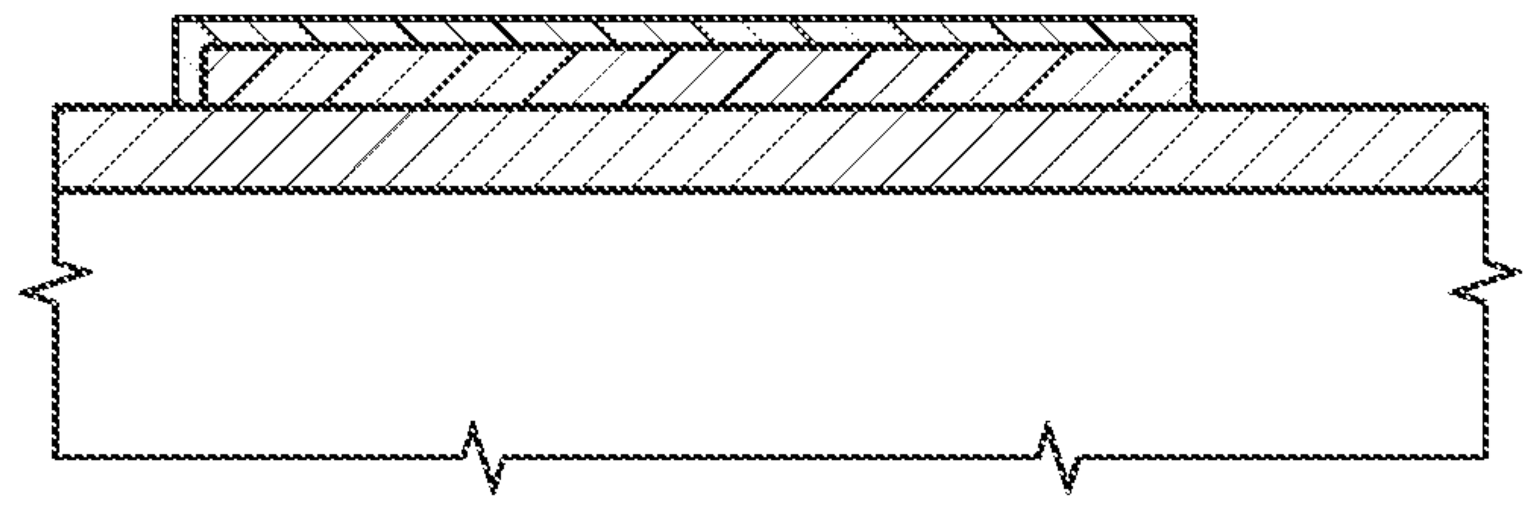


FIG. 14

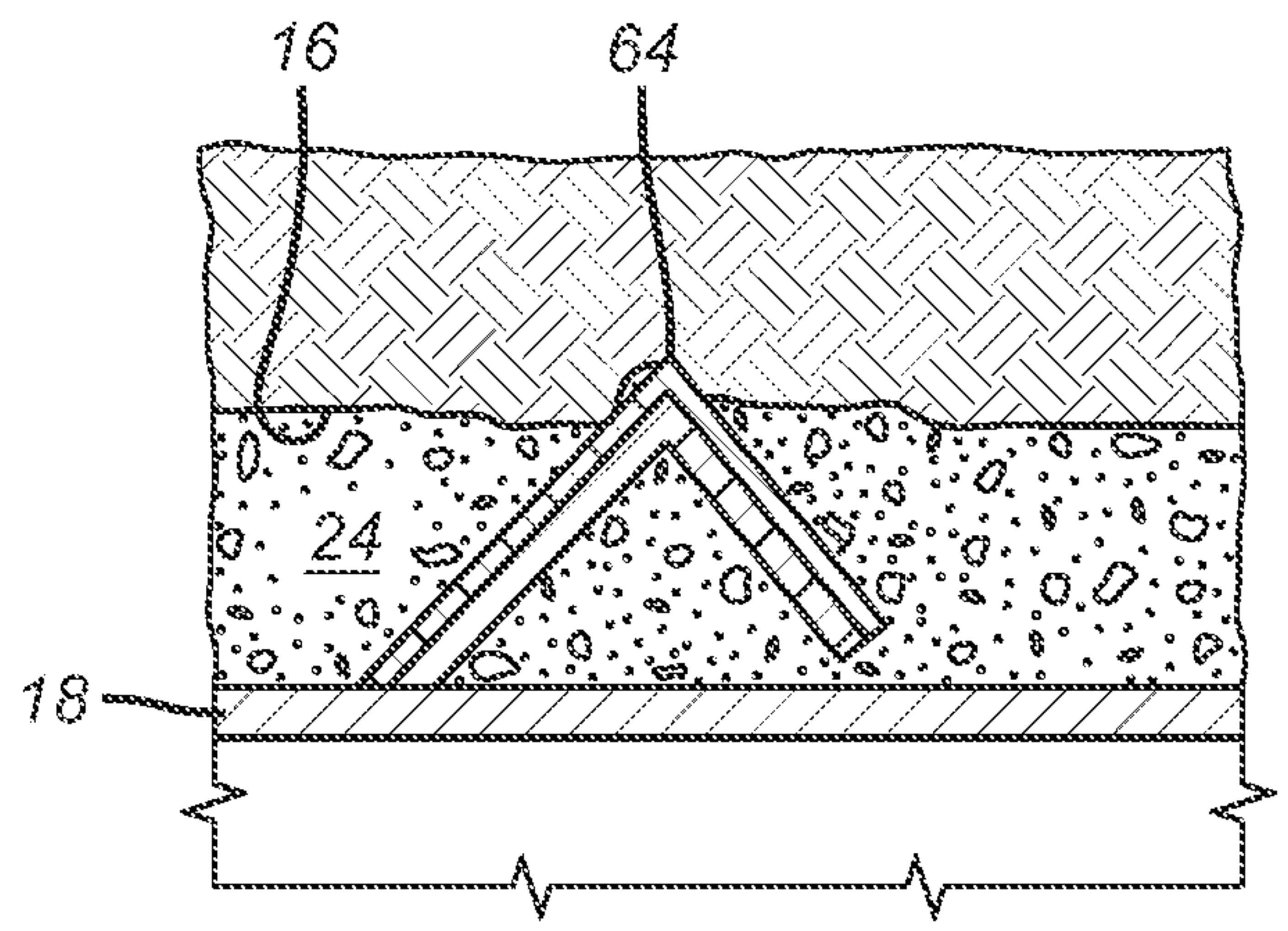


FIG. 15

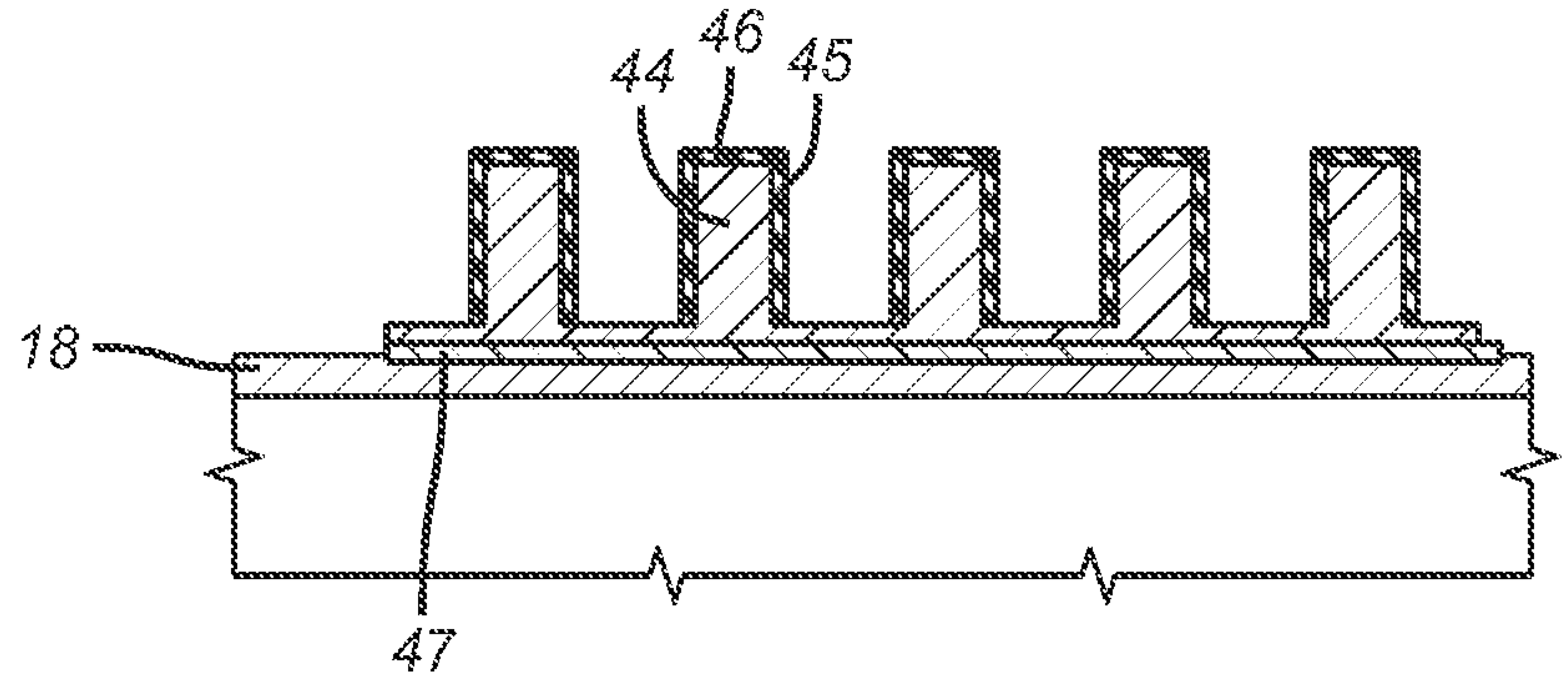


FIG. 16

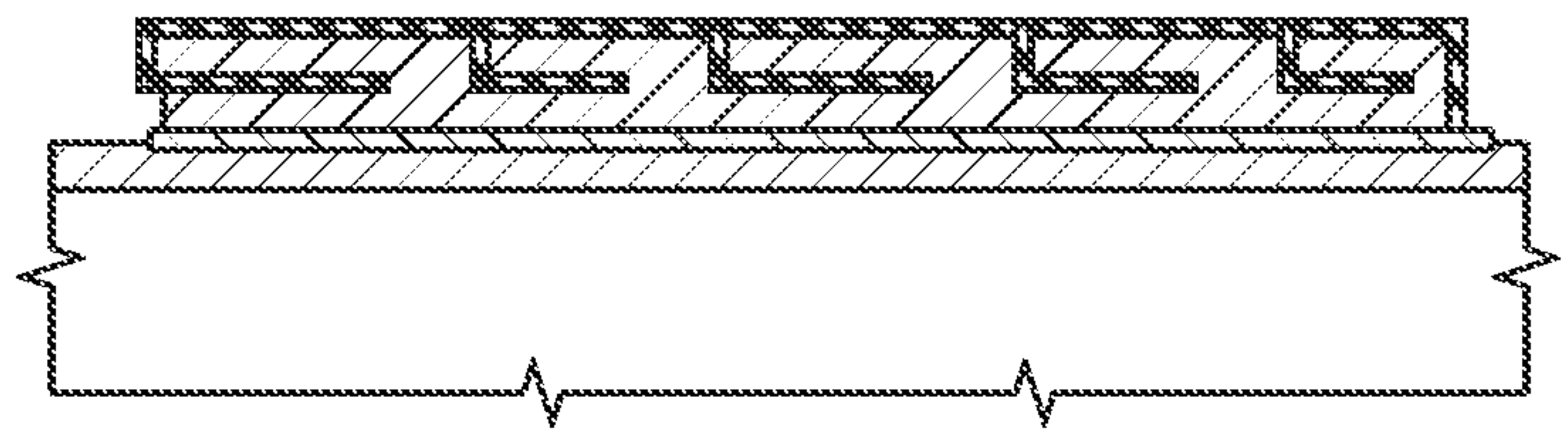


FIG. 17

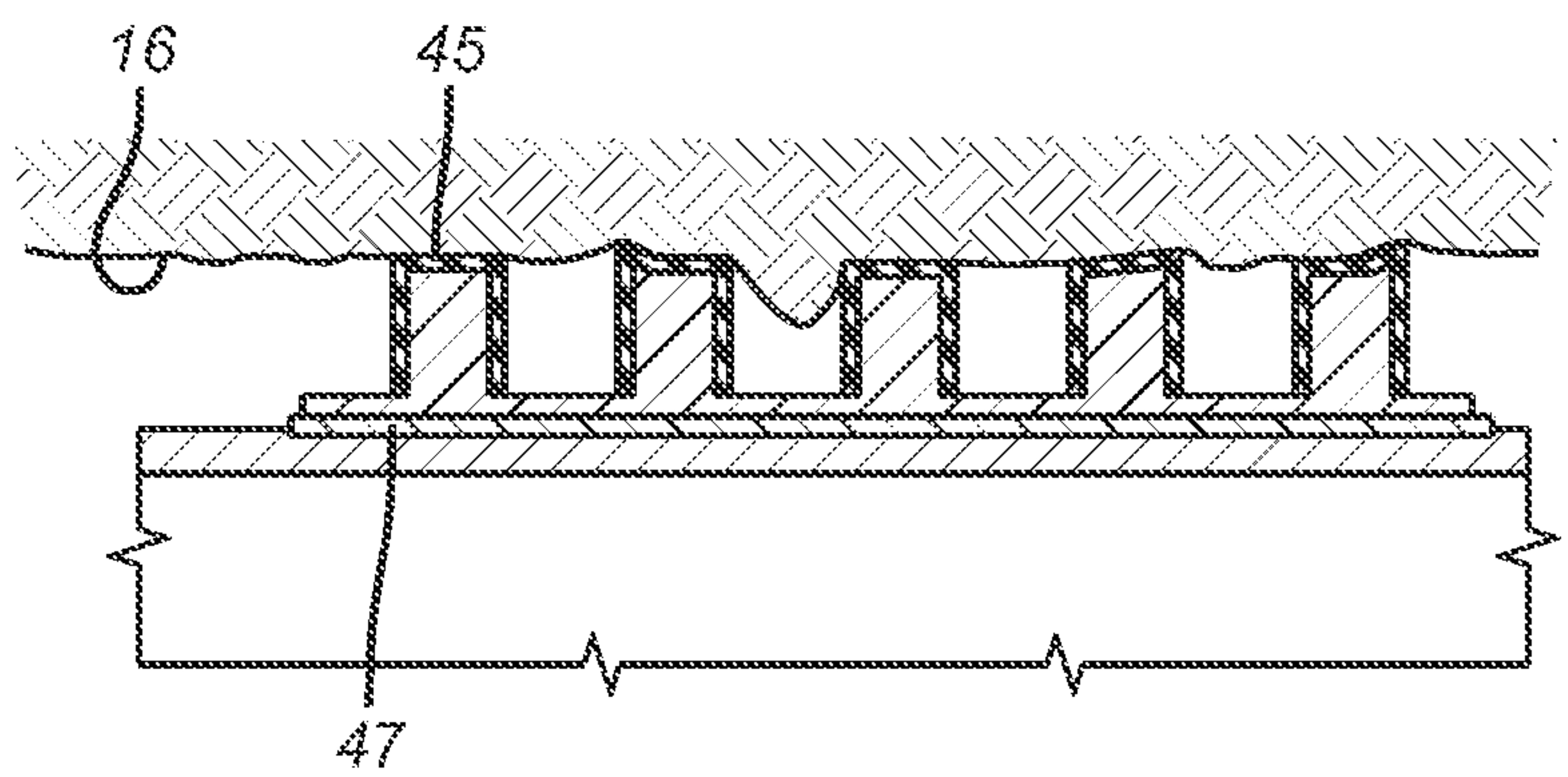


FIG. 18

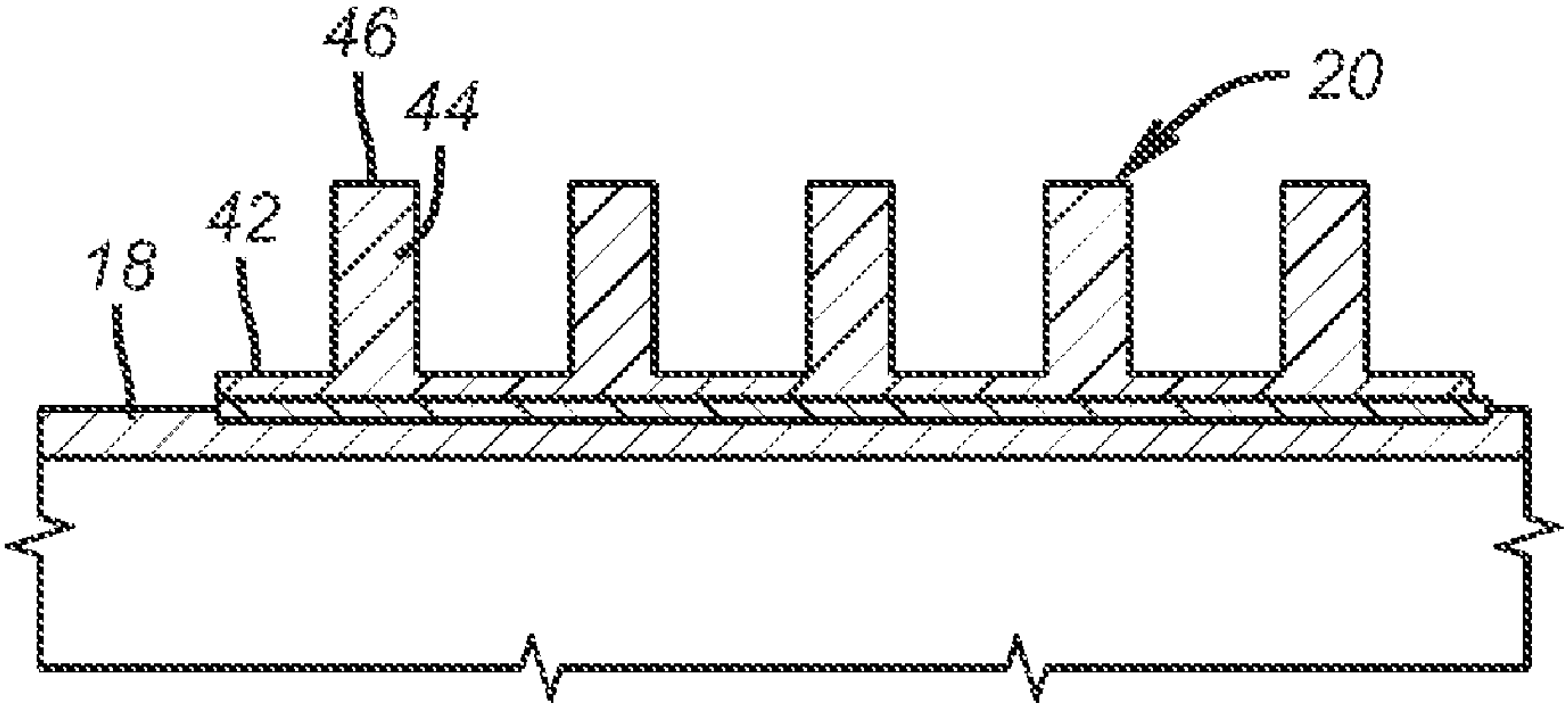


FIG. 5