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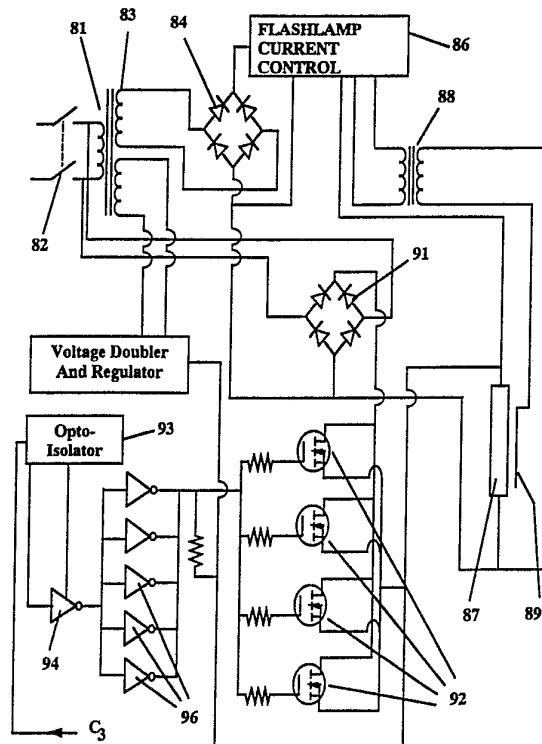
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(54) Title: LASER DRIVER AND CONTROL CIRCUIT

(57) Abstract

A control apparatus for a pumped rod-type laser includes an arc lamp (87) disposed to illuminate the lasing medium, such as an NdYAG crystalline rod. The apparatus includes a full wave rectifier (91) to power the arc lamp, and a MOSFET switching circuit (92) to turn on and off the arc lamp power at controlled times during each half cycle of the power waveform so that the laser medium is pumped and optically discharged once during each half cycle of the power supply. The laser power output is measured by a photodetector during each half cycle, and the photodetector output is integrated and compared with a manually set, variable laser output power level. When actual laser power reaches the preset power level, the comparator initiates turning off the MOSFET switching circuit power for that respective half cycle of the power waveform.



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**LASER DRIVER AND CONTROL CIRCUIT**  
Reference to Related Application

This application is a continuation-in-part of United States Patent Application Serial No. 07/019,755, filed February 27, 1987 by the present inventor and Dan Rink and Garrett Lee, for which priority is claimed.

Background of the Invention

In the field of medicine the use of laser devices for treatment purposes is becoming commonplace. Such devices are used for cauterization of wounds, excision of tissue, selective thermal absorption in tissue, welding of tissue through the formation of scar tissue, and the like. Recent developments in intravascular treatment point to recanalization of atherosclerotically occluded vessels virtually anywhere in the human body, including the relatively small vessels which supply the heart muscle itself. Such developments are described in copending United States Patent Application Serial No. 07/019,755, filed February 27, 1987 by the present inventor and Dan Rink and Garrett Lee.

Generally speaking, lasers designed for medical use should be highly controllable with respect to the power output level of the laser, and the duration of the laser illumination. Paradoxically, although the laser output

power rarely exceeds approximately 20-25 watts for medical treatment purposes, the amount of power used to generate this laser power level is extraordinarily high. In lasing medium which operates continuously, kilowatts of power are consumed, even on a standby basis, so that a few watts of light energy can be delivered briefly or sporadically to the desired application site. The heat generated in the lasing cavity and in the power supply require that an external cooling system be provided. Thus an external source of cold water is generally required, and hundreds of gallons of water are expended in relatively short procedures. External cooling systems add to the complexity and expense of a medical laser, and create further connection and maintenance problems.

In pulsed mode laser devices, there is the opportunity to save power consumption since the lasing medium is operated only sporadically. However, pulsed mediums do not react predictably when first activated, due to thermal and dimensional effects. For example, when a NdYAG laser rod is first pumped by an arc lamp, the rod experiences a rapid thermal buildup which alters the axial dimension of the rod. As the rod changes in shape, the quality of the laser output pulse is severely affected. Thus prior art devices may provide erratic power outputs in pulse or burst modes of operation.

This problem is complicated by the fact that many prior art pulsed laser systems measure the power output of each pulse (by any of several

techniques known in the art), compare that power level to a preselected level, and in response alter the intensity or period of succeeding pulses. The inherent time lag of this process, together with the averaging errors and the potential instability in such level-hunting systems, can create unacceptably erratic performance.

Prior art lasers have employed high voltage DC power supplies to pump and fire a pulsed mode laser, and pseudo-continuous operation may be added by charging capacitors with the high-voltage power and sequentially connecting the capacitors to a flash lamp or the like to fire the laser to produce a plurality of time-separated pulses. However, such power supplies are expensive and inefficient, and there is a limit to how many capacitors can be provided in a practical laser apparatus.

Another difficulty found in medical and other forms of work with lasers is that prudent safety considerations that all personnel wear laser safety goggles whenever they are in an area in which a laser is in use. Particularly in medical settings such as a surgical operating room, the surgeons and assisting staff, the anesthesiologists and the patient must be equipped with safety goggles. Often the goggles interfere with other equipment, such as sterile masks, the anesthesia mask, and the like, and are a distraction at best. There is no remedy for this problem known to the present inventors.

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### Summary of the Present Invention

The present invention generally comprises a laser driving method and system that provides a laser system with a high safety factor, low power consumption, and a compact, simplified power supply. The laser system includes a pumped rod-type laser and an arc lamp or the like disposed to illuminate the lasing medium, such as a NdYAG crystalline rod. The apparatus includes a full wave rectifier to power the arc lamp, and a MOSFET switching circuit to turn on and off the arc lamp power at controlled times during each half cycle of the power waveform so that the laser medium is pumped and optically discharged once during each half cycle of the power supply.

In order to control the power of the laser pulse, the laser power output is measured by a photodetector during each half cycle, and the photodetector output is integrated and compared with a pre-set, variable laser output power level. When the actual laser power reaches the preset power level, the comparator initiates turning off the MOSFET switching circuit power for that respective half cycle of the power waveform. At the beginning of the next half cycle the integrator is reset and the MOSFET switching circuit is turned on again. Thus the power of each pulse of the laser is measured and chopped at the appropriate instant to deliver the precise power level desired.

The full wave rectified power is used to drive the laser medium in a burst mode of several pulses, or in a repetitive pulsed mode that emulates the effects of continuous output lasers. The full wave rectified power supply also permits the use of 110 VAC utility power, and obviates the need for external cooling of the laser. The apparatus also includes safety circuits that permit laser operation only when the internal cooling system is operating, when the current to the arc lamp is below a maximum level, and when the temperature created by the laser illumination on a target or on a portion of the beam delivery system is above a variable preset level, and the like. A further safety circuit detects the presence of laser radiation in the area surrounding the laser to shut it off when laser light escapes from the system. For medical, industrial, and experimental laser uses, this feature obviates the need for laser safety goggles for operational personnel.

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Brief Description of the Drawing

Figure 1 is a schematic representation of the laser power control circuit of the present invention, and in particular the circuit that senses and controls the portion of each half cycle of the power waveform that is applied to the laser pumping light source.

Figure 2 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the temperature safety circuit that senses an overtemperature condition in the laser system and shuts off power to the laser power supply.

Figure 3 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the cooling safety circuit that shuts off the laser power supply whenever there occurs an interruption in flow of coolant to the laser cavity.

Figure 4 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the photodetector circuit that senses the laser output during each half cycle of the power waveform, and shuts off the laser whenever a desired, preset output power level is reached.

Figure 5 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the current level sensing safety circuit that detects excessive current flow in the conductor to the laser optical pumping source and shuts off the laser power system.

Figure 6 is a graphic depiction of the timing sequence of the laser power control circuit of the present invention.

Figure 7 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the FET signal control circuit that delivers power to the laser optical pumping source.

Figure 8 is a schematic representation of a portion of the laser power control circuit of the present invention, and in particular the laser radiation area detector safety circuit.

### Description of the Preferred Embodiment

The present invention generally comprises a laser driving and control system and method of operation thereof. The most salient features of the invention is that it provides a laser system which is power efficient, stable, accurately controlled and extremely safe. Although the preferred embodiment is described with respect to medical applications, it may be appreciated that the attributes of the laser system of the present invention could be directed to industrial, investigative; and other uses.

The invention is adapted to be employed with a standard-in-the-art laser generating unit, or head, which comprises a closed reflective chamber housing a lasing rod and an optical pumping source such as a flashlamp in operational relationship. One possible configuration of the laser head includes a optical enclosure having a uniform, elliptical cross-sectional configuration along a longitudinal axis, with focal lines parallel to the longitudinal axis, and the laser rod and flashlamp extending parallel along respective focal lines. The lasing rod material may be NdYAG or the equivalent. A conventional cooling system which circulates coolant in the laser head is provided to remove excess heat generated by absorption of a good portion of the flashlamp energy by the laser head.

A significant aspect of the invention is the design and operation of the power supply that controls the flashlamp and thus the laser output

power level. Unlike prior art laser systems, which use high voltage DC power supply arrangements, the present invention is designed to use 117 VAC (or 220VAC) power directly from the utility power source. With regard to Figure 1, the power control circuit includes a transformer 11 to step down the input line voltage and deliver it to a full wave rectifier 12. The result is the rectified sinusoidal power wave P, shown in Figure 6. The power wave P is fed to a Zener diode voltage regulator, which chops the peaks of the power wave P at a desirable voltage to form a low voltage analog of the power voltage signal.

The analog power signal is fed to the trigger input of a timer 16, such as the common 7555 IC timer known in the prior art. The circuit includes a trio of such timer circuits 16, 17, and 18, connected output-to-input in serial fashion. The input 19 of timer 16 is connected between a capacitor 21 leading to ground, and a resistor 22 connected to the 5 VDC power supply which also drives the timer 16. As is known in the prior art, the resistor 22 and capacitor 21 comprise an RC network which slowly charges the input 19 to 5 volts in a time period determined by the values of the resistor and capacitor. Each of the timer circuits 17 and 18 operate in a similar fashion, although the values of the respective resistors and capacitors at the input differ to determine selected time delay factors.

In addition, the power wave analog signal is connected to the input 19. Whenever this signal pulls the input low, to a range of one-third the

power supply voltage, the timer output 23 goes high, forming the signal C<sub>1</sub> depicted in Figure 6. Note that signal C<sub>1</sub> switches high as the power waveform P approaches zero, and stays high until P exceeds the threshold voltage once again. The on-off thresholds may be set to be identical so that the signal C<sub>1</sub> is symmetrical about the zero point of the power voltage P, but this is not necessary for the system to operate.

The output of timer 16 is connected to the input of timer 17, which is connected to be triggered immediately by the fall of signal C<sub>1</sub> and to remain on only a short time. The output of timer 17, signal C<sub>2</sub>, is fed to timer 18, which is connected to produce the signal C<sub>3</sub>. It is important to note that signal C<sub>3</sub> commences when C<sub>2</sub> goes low, so that C<sub>2</sub> comprises a firing signal for the system. The output of timer 18 is connected to an actuating input of a MOSFET laser power supply control 33, described in the following specification, so that the laser pumping light source is turned on whenever signal C<sub>3</sub> goes high. The operating period (on time) of timer 18 also establishes a maximum elapsed time for operation of the pumping light source during each half cycle of the power voltage waveform.

It should be pointed out that the timer 18 differs from the others in that the reset input 31 is not connected to the 5 VDC power supply for instant reset. Rather, input 31 is connected to the output of reset AND gate 32, which has a plurality of reset inputs 32R. Whenever any of the reset inputs receive a low-going input, the AND gate 32 causes the timer 18 to

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reset and the output C3 goes low. Thus the inputs to gate 32 determine that period of each pulse of signal C3 and the laser pulse itself may be terminated before the maximum elapsed time, as shown by reference numeral RC3 in Figure 6. Furthermore, a continued low input to the gate 32 will effectively block operation of the laser. Thus the inputs 32R comprise important control factors for the operation of the laser.

With regard to Figure 4, another important portion of the invention is an output power monitor circuit 36, which has an output connected to one of the reset inputs 32R. The circuit 36 includes a photosensor 37, preferably a linear response photodiode fabricated of silicon or the equivalent, and placed in the laser light path to receive a small fraction of the laser output beam. For example, the photosensor 37 may be placed behind a partially conducting mirror disposed in the laser beam path, to receive the small percentage of beam power that is passed by the mirror. The photosensor outputs are connected across the inputs of an operational amplifier 38. The output of the op amp 38 is connected to the negative input in a feedback loop by capacitor 39, so that the output current of photosensor 37 is integrated with respect to time and represented by the voltage across the capacitor 39. The integration product is an analog signal having a voltage level which varies generally linearly with the power output of each laser pulse.

Also connected in parallel with the capacitor 39 is a solid state switch 41. The switch 41 has a trigger input connected to receive the signal C<sub>2</sub>, and is actuated thereby to short out the capacitor and remove the accumulated voltage thereon. Thus the firing signal C<sub>2</sub> resets to zero the voltage signal at the op amp 38 output just prior to firing the next laser pulse.

The voltage signal output of op amp 38 is conducted to the negative input of op amp 42. The other input is connected to the wiper connection of a potentiometer 43, which may be controlled manually or by appropriate software. It may be appreciated that whenever the signal from op amp 38 exceeds the voltage set by potentiometer 43, op amp 42 will emit a low-going signal that is connected directly to one of the inputs 32R of the reset AND gate 32. Thus the power output of each pulse of the laser is monitored in real time, and the power supply is squelched when the pulse power equals the selected, desirable pulse power level. This system is extremely accurate in delivering the desired laser power to the device utilizing the laser radiation, since it eliminates pulse power averaging errors and correctional time delays which are known in prior art systems.

Another control circuit 46 connected to the safety reset switch 82, shown in Figure 3, is designed to monitor the cooling fluid flow to the laser head, and to deactivate the laser when there is insufficient coolant flow. The circuit 46 includes a bridge-type resistive fluid pressure sensor

47. The sensor 47 is connected by fluid conduits in a parallel relationship to the main coolant supply conduit 48, so that the pressure drop produced by fluid flow resistance in the conduit 48 is presented to the sensor 47. The opposed bridge outputs of the sensor 47 are connected across the inputs of op amp 49. Connected from the output to the negative input of op amp 49 is a parallel resistive network 51 which establishes a feedback loop. The output of op amp 49 is connected to the positive input of op amp 52, and the respective negative input is connected to the wiper contact of a potentiometer 53. When the voltage level of the output signal of the op amp 49 falls below a level set by potentiometer 53, indicative of a decrease in the fluid pressure on sensor 47 and a loss of coolant flow, the output of op amp 52 goes low, and the system reset switch 82 is disabled to stop all power to the laser pumping light source. Thus the laser output is stopped immediately.

A further safety circuit, shown in Figure 2, is designed to prevent excessive heat in the laser system or in a laser beam receiving target from destroying system components by shutting off the laser when an excessive temperature condition is detected. The thermal safety circuit 56 includes an infrared sensitive photosensor 57, such as an infrared diode sensor, with its terminals connected across the inputs of an op amp 58. In a preferred embodiment of the invention, the infrared sensor may be directed to the transfer system that conducts the laser beam from the laser to a delivery

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system, such as a fiberoptic beam guide that extends to a beam utilization device. An example of one such transfer system is described in copending United States Patent Application Serial No. 07/180,950 filed on April 11, 1988

by the present inventor, Dan Rink, and Garrett Lee. The disclosure of that application is incorporated herein by reference. In that apparatus there is a bushing component that supports the ends of a plurality of optical fibers while the focused laser beam is shifted among the plurality of fiber ends. Any misalignment of the focused beam can direct a focused laser pulse of extremely high power density onto the bushing component, quickly generating very high temperatures that cause the emission of infrared light. The sensor 57 picks up the infrared light, and emits a proportional voltage in response thereto. Alternatively, the sensor 57 can be directed to monitor the infrared output of a beam-receiving target member, such as a laser heated cautery cap for recanalization of atherosclerotically occluded vessels, as described in the copending United States Patent Application Serial No. 07/019,755, filed February 27, 1987 and noted above.

The output of op amp 58 is connected to a solid state switch 59, which has a trigger input connected to the firing signal C<sub>2</sub>. Switch 59 is connected in turn to the positive input of op amp 61, which is provided with a direct feedback loop 62 from output to input. The configuration of op amps 58 and 61 is such that the current level of the output of op amp 61

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is proportional to the infrared radiation received by sensor 57. This current output signal is fed through resistor 63 to one input of op amp 64, so that the current through resistor 63 is a function of the magnitude of the infrared radiation. Op amp 64 includes a feedback capacitor 66 which integrates the current input to produce an output having a voltage proportional to the total infrared power received by the sensor, which in turn is indicative of the temperature of the component being sensed. Solid state switch 67 is connected in parallel with capacitor 66, and includes a trigger input connected to C<sub>2</sub>. It should be noted that the firing signal C<sub>2</sub> causes the switch 67 to reset the integration product to zero prior to each laser pulse. Furthermore, the switch 59 connects the infrared signal to the integrator only during the brief firing signal, before the laser pulse is fired. This arrangement assures that the infrared source is monitored only when it is not being illuminated by the laser, which would overwhelm the infrared signal of interest.

The output of op amp 64, a voltage analog of the infrared power level and hence an indication of temperature level, is connected to one input of a comparator 68, and the output of comparator 68 is conducted through diode 69 to one of the reset inputs 32R. Comparator 68 includes a level-setting potentiometer 70 connected to the other input. Thus as the temperature of the monitored component increases, the voltage output of op amp 68 decreases, and when it fails to exceed the threshold of

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potentiometer 70 the output of op amp goes low and pulls the AND input 32R to a low state. This circuit effectively monitors the temperature of a component after a laser pulse, and serves to limit or chop the duration of the next successive laser pulse in response to the previous temperature level. For example, an excessive temperature condition in the component being monitored would cause the system to emit only a brief pulse in the next laser pulse cycle.

The present invention also includes a high voltage lamp driver circuit for operating the flashlamp or the like that optically pumps the laser rod to emit a coherent beam. With regard to Figure 7, the lamp driver circuit includes a transformer 81 connected through a main shutoff relay switch 82 to 117 VAC utility power. The transformer 81 includes a high voltage secondary winding 83 having an output of approximately 600 volts that is connected across a full wave bridge rectifier 84. The rectified voltage is fed to a flashlamp current control circuit 86, which includes filter capacitors that produce a smooth DC current that in turn is connected to one electrode of a flashlamp 87. The other electrode of the flashlamp is connected to one output terminal of the rectifier 84. The circuit 86 applies approximately 160 VDC to the flashlamp to maintain the lamp plasma in a conductive state, emitting light at a level well below the threshold of lasing in the NdYAG rod. The current control circuit is also connected to a spark coil 88, which has a high voltage output connected to a spark electrode 89

adjacent to the flashlamp 87. The spark coil is activated by circuit 86 to provide a high voltage pulse to initiate flashlamp conduction, after which the circuit 86 provides a steady "simmer" current to maintain conduction in anticipation of a high current pulse to dramatically increase flashlamp output and initiate lasing.

To provide the high current pulse, the driver circuit includes another full wave bridge rectifier 91 connected across the utility power supply. One output terminal of the rectifier 91 is connected to one electrode of the flashlamp, and the other output is connected to the drain terminals of a plurality of power MOSFETs 92 in a parallel configuration. The source connections of the MOSFETs 92 are connected in parallel fashion to the other flashlamp electrode. Thus switching of the MOSFET devices causes the output of the rectifier 91 to be applied directly across the flashlamp, and this branch of the circuit provides the substantial current required to sustain the output of the flashlamp at levels necessary to cause lasing.

Switching of the MOSFETs 92 is accomplished by signal C3, which is fed to an opto-isolator 93 to isolate the logic circuits for the power circuits. The output of the isolator 93 is conducted to a two stage inverter, comprising gate 94 connected in series with a parallel array of gates 96. This double inverter arrangement comprises a high current source required to overcome the intrinsic gate-to-channel capacitance and switch the MOSFETs 92 as rapidly as possible. The outputs of gates 96 are

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connected together and lead to the gate connections of the MOSFETs 92. Thus whenever signal C3 goes high, the MOSFETs 92 are switched on to provide high current to the flashlamp to sustain the lamp output as long as C3 remains high. As soon as C3 drops to zero, the MOSFETs switch off, lamp output ceases, and the maintenance voltage increases once again.

It may be appreciated that the control system of the present invention is closely tied to the utility power supply, not only in terms of voltage and current requirements, but also for timing control and repetition. Each half-cycle of the sinusoidal power wave provides a timing signal for the system, and the laser will fire repetitively, once each half cycle, as long as the system is turned on and none of the safety circuits are not activated. Each pulse will have a maximum period set by the circuit of Figure 1, and an actual period set by the laser power sensing circuit of Figure 4.

A further safety circuit, shown in Figure 5, is designed to shut off the laser system when excessive current is detected in the power circuit feeding the flashlamp. It includes a Hall effect transducer 101 which is disposed about one of the conductors connected directly to the flashlamp and adapted to sense the magnitude of the magnetic field created by the current flow in the conductor. The output of transducer 101 is conducted to op amp 102, which in turn has an output connected through a resistor to the negative input of op amp 103. Op amp 103 is provided with a parallel combination of a capacitor 104 and solid state switch 106 connected

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between the output and negative input. The capacitor integrates the current generated by the transducer to produce a voltage signal output on signal line 100 proportional to the current flow to the flashlamp. The solid state switch 106, which is triggered by signal C2, resets the integration product to zero prior to each laser pulse.

The output of op amp 103 is compared to an adjustable voltage reference 107 by comparator 108, the output of which is connected to one of the reset AND inputs 32R. Thus whenever the current to the lamp exceeds a selected maximum level, the laser is extinguished in the midst of an output pulse. The voltage produced by the potentiometer 107 sets the maximum current level permitted in the flashlamp driving circuit.

The voltage signal output on signal line 100, proportional to the current flow to the flashlamp, is also conducted to op amp 111, where it is compared with a further adjustable voltage reference 112. As before, the voltage level of reference 112 establishes a maximum current level sensing circuit. However, the output of op amp 111 is connected to the actuating input of relay switch 82, so that an excessive current condition in the flashlamp driver circuit will shut off power to the entire laser system. Thus not only is the laser pulse terminated by a high current condition (by op amp 108), but the entire laser control and driving system is disconnected from the utility power supply. This feature assures that any

malfunction or short circuit will be neutralized immediately, no shock hazard will develop, and the system components will be protected.

The signal line 100 is further extended through resistor 113 to one input of op amp 114. This input is also connected to an RC integrating network 116, which produces a long-term average of the power consumed in the flashlamp driving circuit. This circuit detects current flow over the average of many laser pulses, and is provided as a further safety precaution to prevent excessive current flow.

Another salient feature of the present invention comprises a novel approach to safe use of a laser in medical or industrial settings. Generally speaking, it is necessary for all personnel to wear laser safety goggles which block light radiation in a narrow range of the laser output. These goggles comprise a large expense for a group of people, such as the operating team in a surgery. Furthermore, the goggles often are distracting and annoying, especially for individuals who wear eyeglasses.

In the present invention, these problems are alleviated by the provision of a further safety circuit shown in Figure 8. This circuit, the laser radiation area detector, includes a photosensor 121 disposed adjacent to the housing in which the laser is enclosed, and directed obliquely toward a wall or ceiling surface in the room in which the laser is being used. The photosensor 121 may comprise a silicon photodiode or the equivalent, and is provided with a primary filter 122 that has a narrow optical passband in

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the range of the laser radiation. For example, commonly available filters transmit approximately 40% of light energy in the NdYAG output band, and only 1% of the remainder of the optical spectrum. The output of the photosensor, a current signal having a magnitude which is a function of the amount of laser light received by the sensor 121, is connected across the inputs of op amp 123. The output of op amp 123 is fed to differentiating capacitor 124, which in turn is connected to an input of AND gate 126.

Also connected to the same input is a parallel network comprised of a resistor and a diode extending to ground. The capacitor, in combination with this network, determines that a signal C5 will appear on the input of gate 126 only when an abrupt negative change occurs in the amplitude of light in the narrow band of the laser output. (See also Figure 6.) The component values are chosen so that the output signal C5 will comprise a brief pulse, on the order of microseconds, in response to the photosensor 121 receiving a sudden negative change in the ambient light level in the laser output band. Since virtually any broadband light source will emit some light energy in the laser output band, and this output can vary, it is important to distinguish sudden negative changes in the output band level that are indicative of laser pulse energy escaping into the area surrounding the laser itself.

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The laser radiation area detector also includes a timer 131, such as the standard 7555 timer known in the prior art, which is connected through resistor-diode network 132 and capacitor 133 to signal C3. Timer 131 is configured to produce a short output pulse C4, on the order of a few microseconds, immediately after signal C3 (actually, RC3, since the signal is modified in duration by the various inputs to reset AND gate 32) goes to zero and the laser pulse has ended for that respective cycle, as shown in Figure 6. Signal C4, which effectively comprises a time window during which the ambient light signal is sampled and detected, is also input to the AND gate 126. When signals C4 and C5 are coincident in time, as shown in Figure 6, AND gate 126 is actuated to produce an output signal during this signal convergence. Thus the gate 126 produces an output only when the photosensor 121 picks up an abruptly falling amplitude of area illumination in the laser output band, and only when this negative change occurs immediately after the cessation of a laser pumping, as the laser output is rapidly decreasing. Such convergence is a reliable indication of the escape of laser radiation into the area near the laser.

The output of gate 126 is fed through diode 136 to an integrating network 137 comprised of a resistor and diode connected in parallel to ground. It is also connected to an inverting gate 138 which has its output connected to the system reset switch 82. The integrating network 137 determines that more than one output pulse from AND gate 126 is required

to trigger a signal from gate 138 to actuate switch 82 and shut off the laser system. In the preferred embodiment the component values are chosen so that two output pulses from gate 126 are required to shut off the laser system.

Due to the fact that the safety circuit of Figure 8 reliably distinguishes laser radiation from background light and ambient light, including fluorescent lights, surgical lights, photographic flash lamps, sunlight, and the like, the use of laser safety goggles may be obviated.

The method of the present invention for controlling a laser is embodied in the functional description of the invention and in the operation of the various circuits described herein. The underlying concept in the method is the use of the AC power signal from the utility source, both as a power source and as a timing signal to drive a pulsed laser medium repetitively in synchronism with the AC power signal. The method of the present invention further includes the functional aspects of the laser safety circuits, for sensing temperature, power, and coolant flow, and in particular the laser radiation area detector that senses a decrease in area illumination in the laser output portion of the light spectrum in coincidence with termination of each laser pulse.

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## CLAIMS

1. A control and driving apparatus for a laser having an optical pumping device, comprising;

AC power supply means operatively connected to said optical pumping device, including first rectifier means for receiving an AC power signal and generating a power signal of periodic DC pulses,

switching means connected between said first rectifier means and said optical pumping device for selectively applying portions of each of said periodic DC power pulses to said optical pumping device to actuate said laser to emit laser radiation in pulses corresponding to said portions of each of said periodic DC power pulses, and

control circuit means connected to said switching means for receiving said AC power signal and generating a control signal to actuate said switching means during each of said periodic DC power pulses.

2. The laser control and driving apparatus of claim 1, wherein said control circuit means includes first photodetector means disposed to receive a portion of the laser output radiation, means connected to said first photodetector means for detecting the laser power output during each of said laser pulses, means for comparing said laser pulse power output to a selectively variable power output level, and means for shutting off said

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switching means when said laser power output attains said selectively variable power output level.

3. The laser control and driving apparatus of claim 1, wherein said control circuit means includes power detector means disposed to sense electrical power flow to said optical pumping device, means for comparing said electrical power flow to a selectively variable maximum power level, and means for shutting off said switching means when said electrical power flow exceeds said selectively variable maximum power level.

4. The laser control and driving apparatus of claim 1, wherein said control circuit means includes temperature detector means disposed to sense an excessive temperature condition in the laser beam path, including infrared detector means for generating a temperature analog signal, means for comparing said temperature analog signal to a selectively variable maximum temperature level, and means for shutting off said switching means when said temperature analog signal exceeds said selectively variable maximum temperature level.

5. The laser control and driving apparatus of claim 4, further including first sampling means interposed between said temperature detector means and said means for shutting off said switching means, said

first sampling means conducting said temperature analog signal only during periods between said laser pulses.

6. The laser control and driving apparatus of claim 1, wherein said control circuit means includes laser radiation detector means disposed to sense laser radiation in the ambient light in the area surrounding the laser, including second photodetector means directed to monitor said area surrounding the laser and adapted to generate an output signal, said second photodetector means including filter means for preferentially transmitting light in the output band of the laser, said second photodetector output signal comprising a function of the light power in said output band of the laser, means for shutting off said AC power supply means when said second photodetector output signal is received, and second sampling means for conducting said second photodetector output signal to said means for shutting off said AC power supply only during predetermined time periods.

7. The laser control and driving apparatus of claim 6, wherein said second sampling means includes means for conducting only during the time period when each of said laser pulses is ending and the laser output power is decreasing.

8. The laser control and driving apparatus of claim 7, wherein said second photodetector means includes differentiation means to emit said second photodetector output signal only when said light power in said output band of the laser is decreasing rapidly.

9. A laser radiation area safety apparatus, including laser radiation detector means disposed to sense laser radiation in the area surrounding a laser, photodetector means directed to monitor ambient light in said area surrounding the laser and adapted to generate an output signal, said photodetector means including filter means for preferentially transmitting light in the output band of the laser, said photodetector output signal comprising a function of the portion of the ambient light in said output band of the laser, means for shutting off operating power to the laser when said photodetector output signal is received, and sampling means for conducting said photodetector output signal to said means for shutting off said operating power only during predetermined time periods.

10. The laser radiation area safety apparatus of claim 9, wherein said laser is operated in a pulsed mode, and said sampling means includes means for conducting only during the time period when each of said laser pulses is ending and the laser output power is decreasing.

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11. The laser radiation area safety apparatus of claim 10, wherein said photodetector means includes differentiation means to emit said photodetector output signal only when said portion of the ambient light in said output band of the laser is decreasing rapidly, whereby said means for shutting off operating power is actuated only upon coincidence of the ending of a laser pulse and an abrupt decrease in the portion of ambient light in the output band of the laser.

12. A control circuit for a laser, comprising means for receiving an AC utility power signal and generating a low voltage AC analog signal thereof, rectifier means for generating a periodic DC pulse signal from said low voltage AC analog signal, first timing means actuated by said DC pulse signal for generating a first timing signal comprising a digital pulse signal having a high absolute value when said DC pulse signal falls below a preset cutoff value, second timing means for receiving said first timing signal and generating a second timing signal in response thereto, said second timing signal comprising a digital signal of brief pulses, each occurring at the termination of each of said first timing signal pulses, and third timing means for receiving said second timing signal and generating a third timing signal in response thereto, said third timing signal comprising a digital signal of pulses each initiated by the cessation of one of said second timing signal pulses, switching means connected to deliver laser

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operating power to a laser, said switching means receiving said third timing signal and actuated to deliver laser operating power in response to receipt of each of said third timing signal pulses whereby the laser is operated in a pulsed mode with each laser pulse corresponding to one of said third timing signal pulses.

13. The control circuit for a laser of claim 12, wherein said third timing means includes a reset trigger for cutting off each of said third timing pulses upon receipt of a reset signal thereby, whereby each of said laser pulses may be foreshortened by said reset signal.

14. The control circuit for a laser of claim 13, further including optical power sensing means disposed to receive a portion of the laser output and to generate a laser power signal corresponding to the laser output power during each pulse, means for comparing said laser power signal to a selectively variable power level and generating a reset signal to said reset trigger when said laser power output attains said selectively variable power level.

15. The control circuit for a laser of claim 13, further including means for sensing the level of said laser operating power and comparing said level to a selectively variable maximum power level, and for emitting

a reset signal to said reset trigger when said laser operating power exceeds said maximum power level.

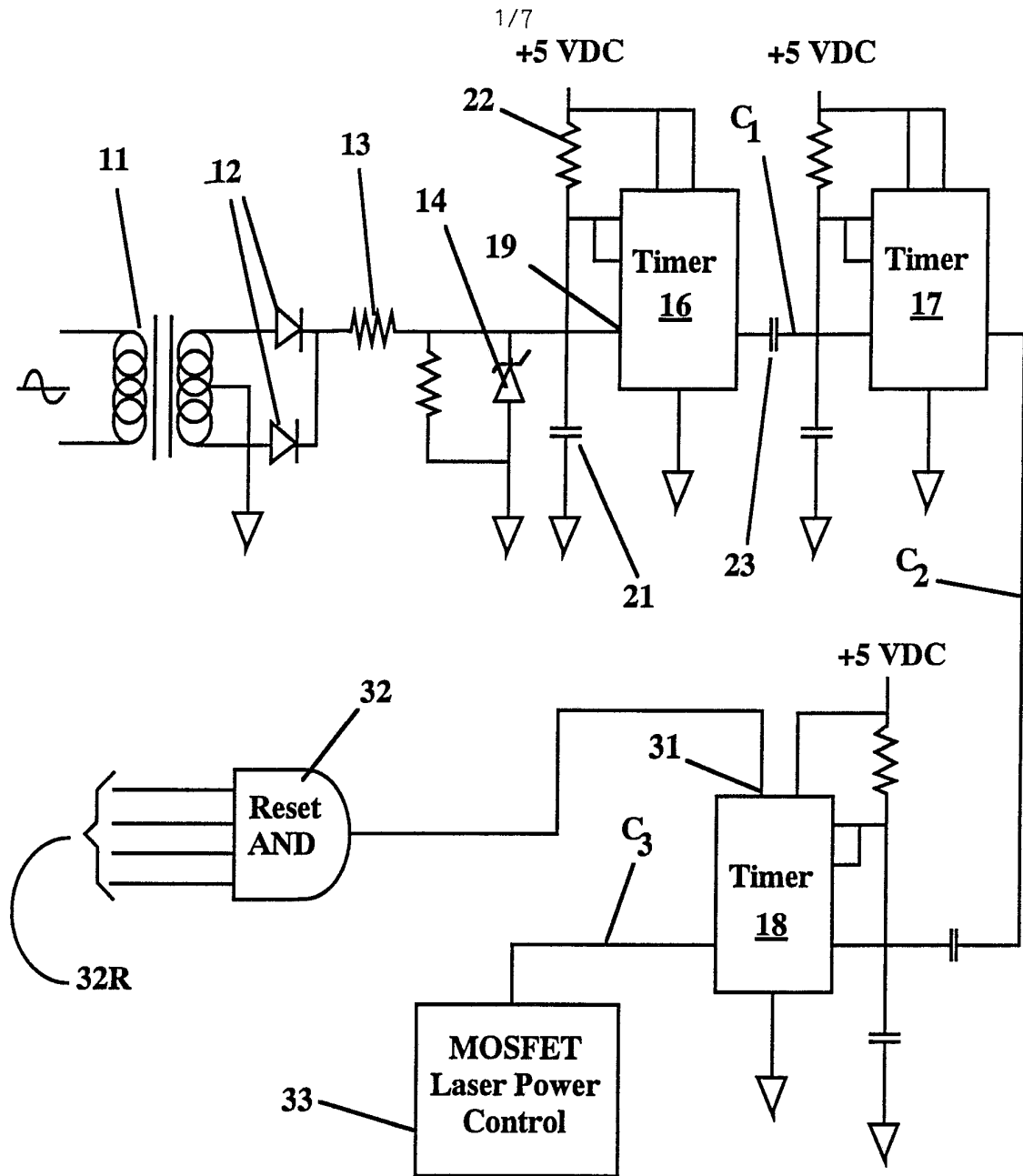
16. The control circuit for a laser of claim 13, further including temperature detector means disposed to sense an excessive temperature condition in the laser beam path, including first infrared detector means for generating a temperature analog signal, means for comparing said temperature analog signal to a selectively variable maximum temperature level, and means for sensing a reset signal to said reset trigger when said temperature analog signal exceeds said selectively variable maximum temperature level.

17. The control circuit for a laser of claim 13, further including fourth timing means for receiving said third timing signal and generating a fourth timing signal in response thereto, said fourth timing signal comprising a digital signal of extremely brief pulses, each initiated by the cessation of one of said third timing signal pulses, photodetector means for monitoring ambient light in the area external to the laser and for emitting a warning signal upon detection of an abruptly falling level of light in the output band of the laser, and means for shutting off said laser operating power upon receiving said warning signal coincident with at least one of said fourth timing signal pulses.

18. A method for driving and controlling a laser having an optical pumping device, including; rectifying and processing an AC utility power signal in full wave fashion to generate a periodic DC power pulse signal, applying the periodic DC power pulse signal to the optical pumping device so that each DC power pulse produces a laser output pulse, measuring the power output of each laser pulse and shutting off the respective DC power pulse when a selected power level for the laser pulse is attained.

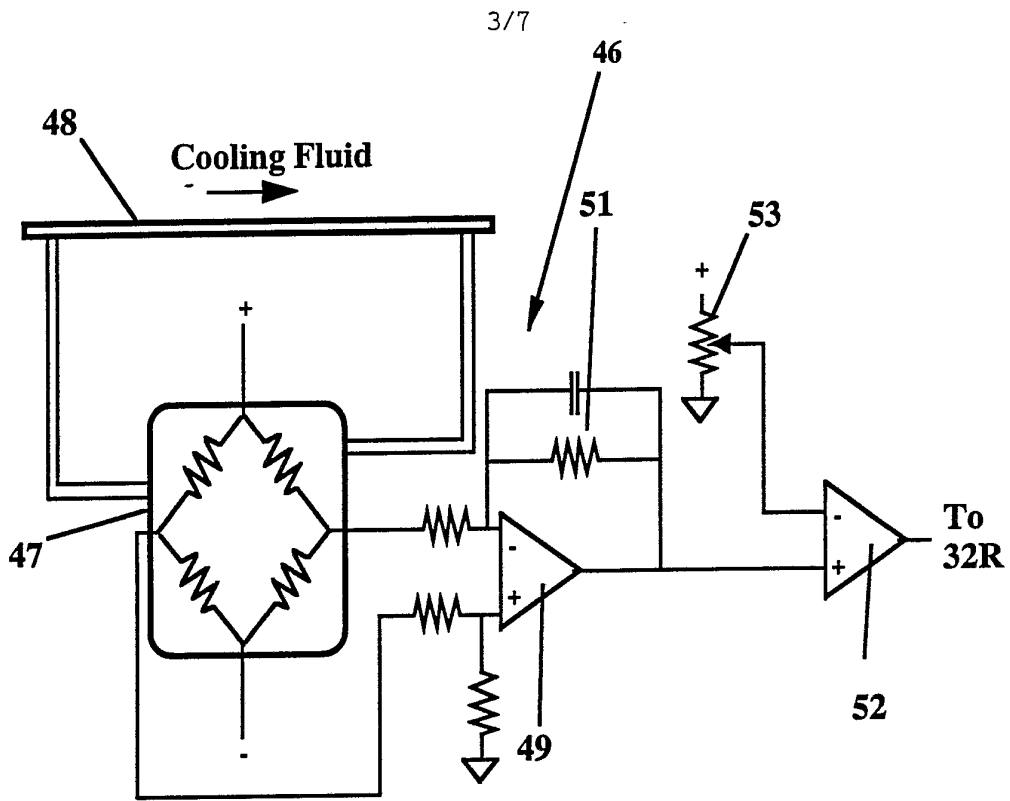
19. The method for driving and controlling a laser of claim 18, further including the step of measuring the temperature of a target receiving the laser output, prior to each laser pulse, and adjusting the duration of the next successive DC power pulse to correspondingly vary the power output of the next successive laser pulse.

20. The method for driving and controlling a laser of claim 18, further including the step of monitoring ambient light in the area external to the laser and generating a warning signal upon detection of an abruptly falling level of light in the output band of the laser, and shutting off all power to the laser when said warning signal is coincident with the cessation of a laser pulse.

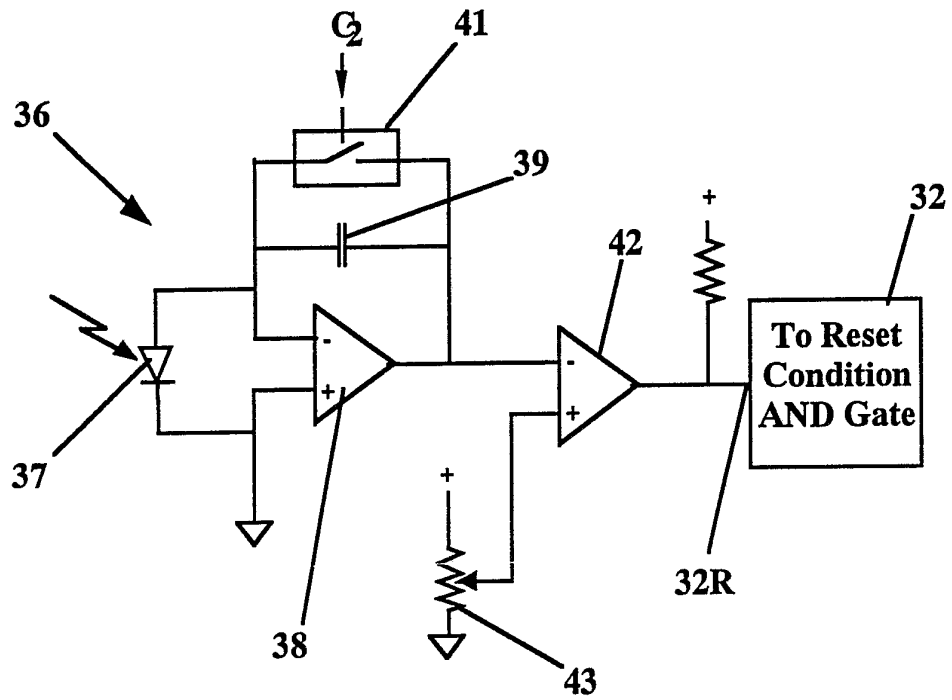


Figure\_1



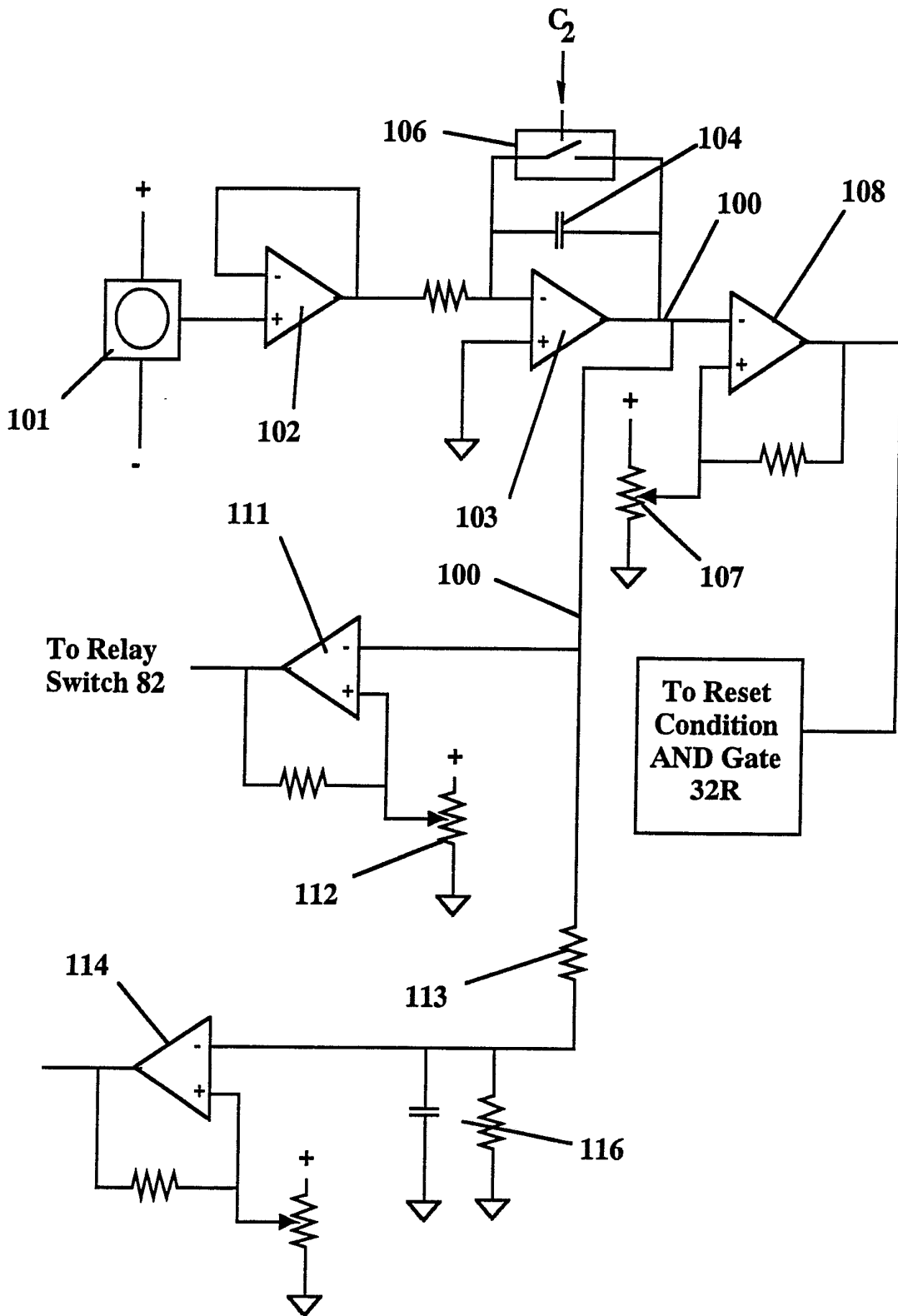


Figure\_3



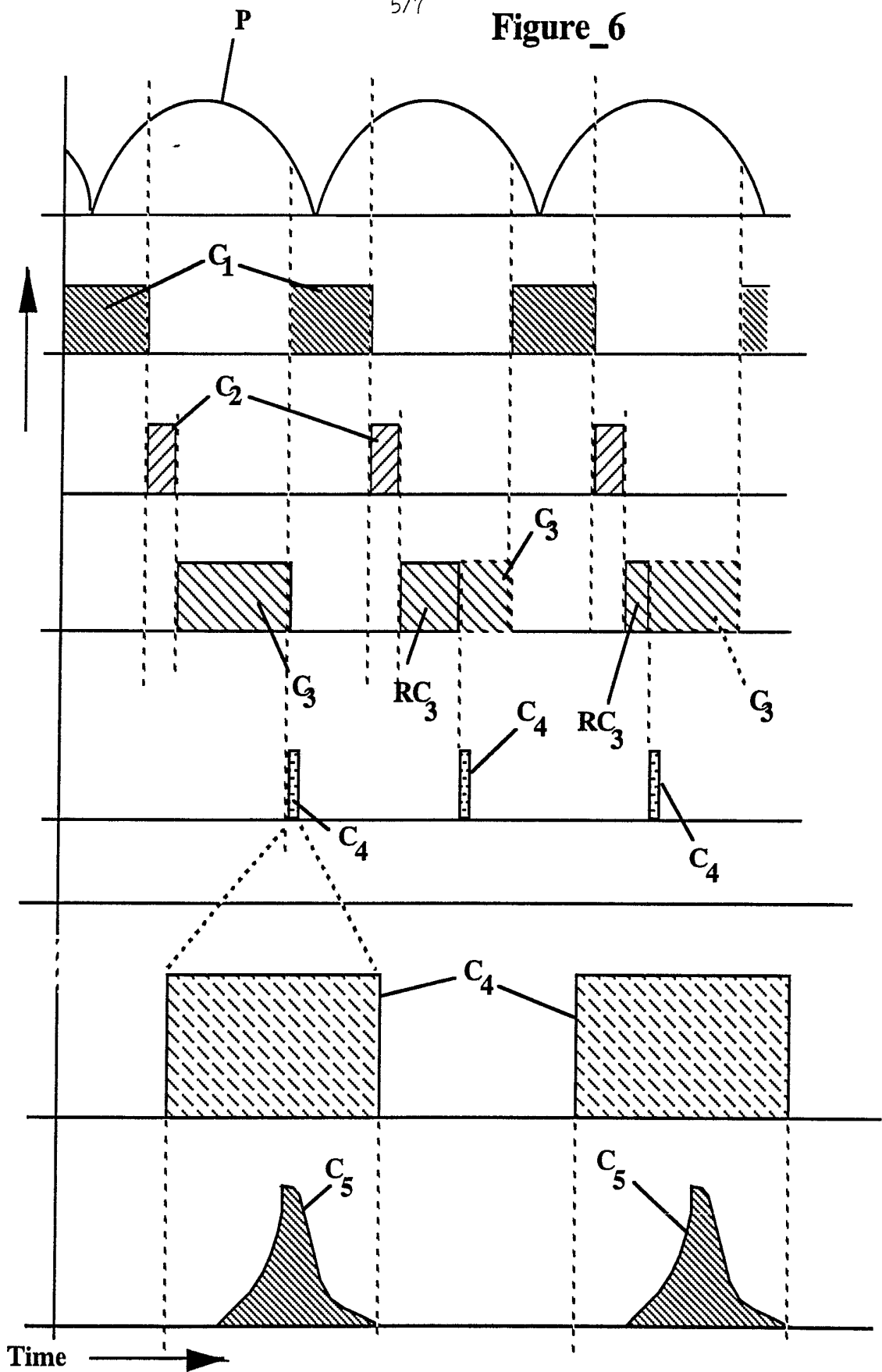
Figure\_4

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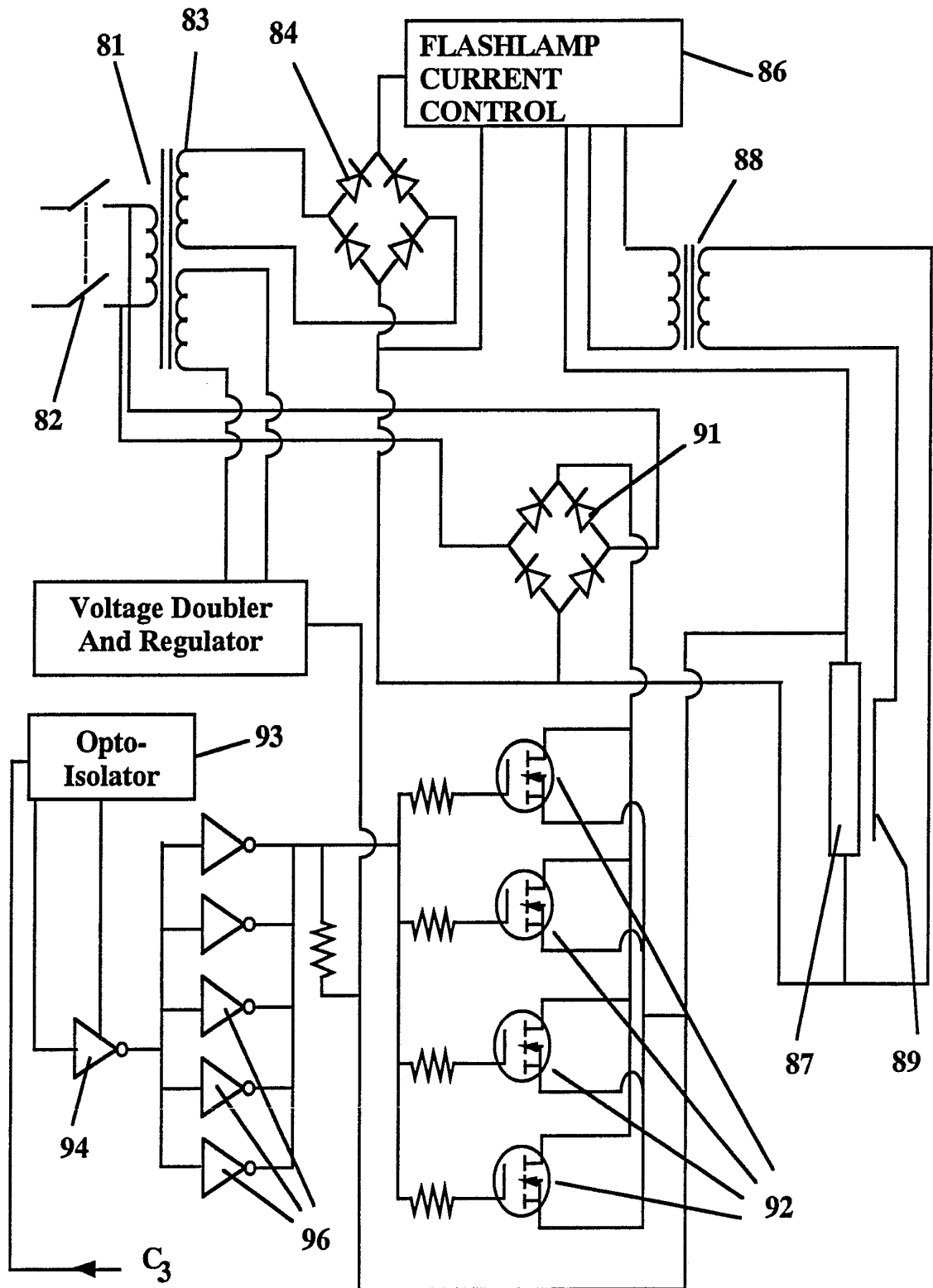
Figure\_5

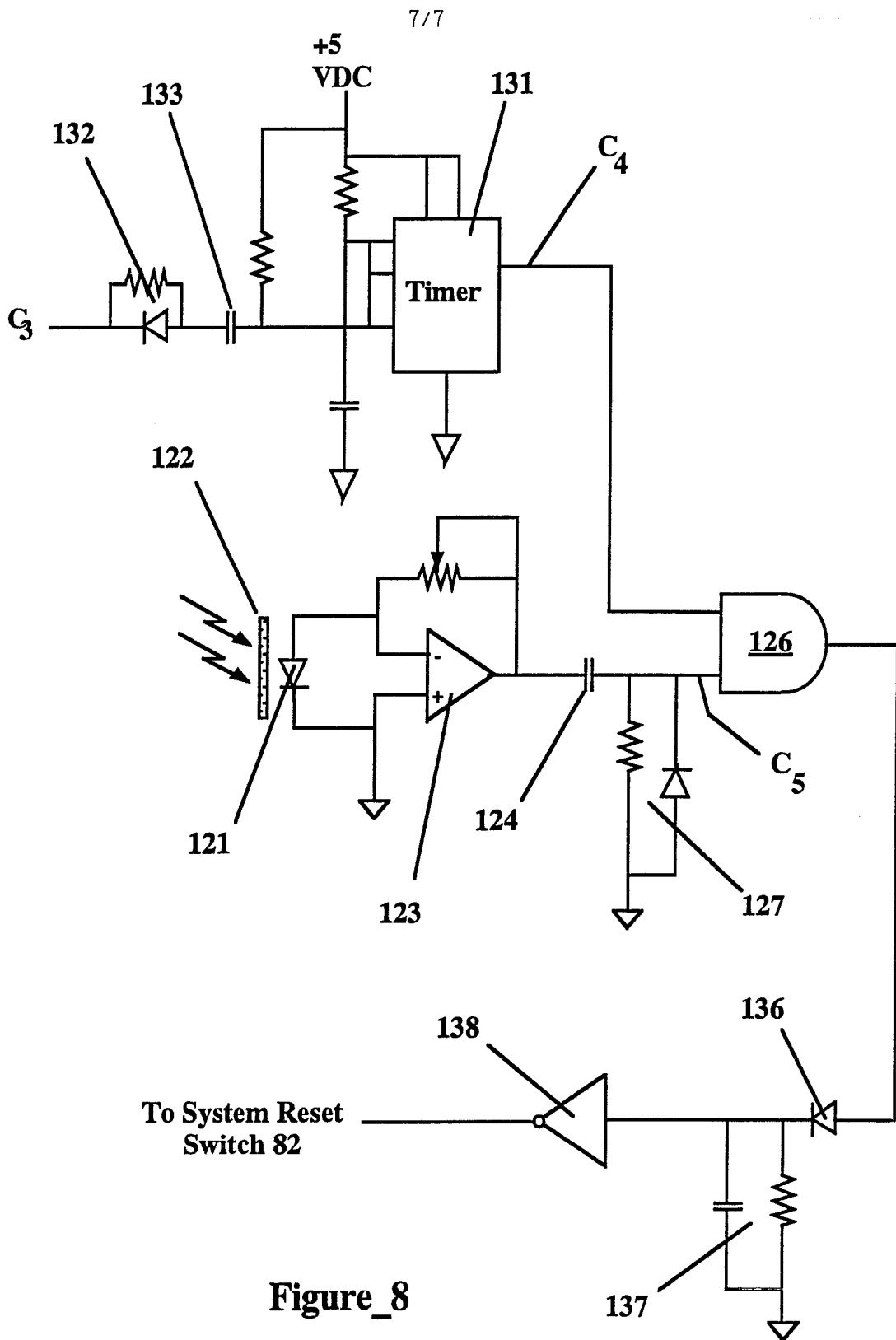
Figure\_6



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Figure 7

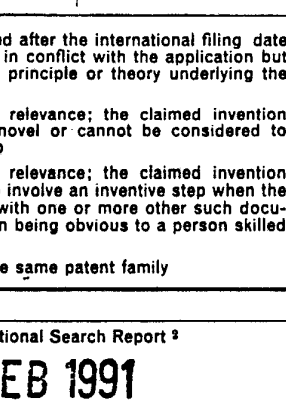




Figure\_8

# INTERNATIONAL SEARCH REPORT

International Application No **PCT/US90/04504**

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (if several classification symbols apply, indicate all) <sup>3</sup>		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC (5): A61 N 5/06 U.S. CL: 606/12		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched <sup>4</sup>		
Classification System	Classification Symbols	
U.S.	606/7,10-12; 128/303.1, 395-398, 362; 372/25, 29-31, 33-35, 82,83,87,93; 219/121.6, 121.61, 121.62, 121,84	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched <sup>5</sup>		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT</b> <sup>14</sup>		
Category *	Citation of Document, <sup>16</sup> with indication, where appropriate, of the relevant passages <sup>17</sup>	Relevant to Claim No. <sup>18</sup>
<u>X</u> Y	US,A 3,896,396 (WHITEHOUSE) 22 July 1975 See the entire document.	1 2-4, 18, 19
Y	US,A 3,806,829 (DUSTON) 23 April 1974 See entire document.	4, 19
Y	US,A 4,504,951 (McMAHAN) 12 March 1985 See entire document.	2, 3, 18, 19
<p>* Special categories of cited documents: <sup>15</sup></p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&amp;" document member of the same patent family</p>		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search <sup>2</sup>	Date of Mailing of this International Search Report <sup>3</sup>	
28 September 1990	<b>15 FEB 1991</b>	
International Searching Authority <sup>1</sup>	Signature of Authorized Officer <sup>19</sup>	
ISA/US	 NGUYEN HEOC-HO INTERNATIONAL DIVISION	