

(19) World Intellectual Property Organization
International Bureau(43) International Publication Date
4 September 2008 (04.09.2008)

PCT

(10) International Publication Number
WO 2008/104052 A1

(51) International Patent Classification:

B22D 7/02 (2006.01) *B22D 7/08* (2006.01)
B22D 15/04 (2006.01) *B22D 7/12* (2006.01)
B22D 21/04 (2006.01) *B22D 9/00* (2006.01)

(21) International Application Number:

PCT/CA2008/000332

(22) International Filing Date:

21 February 2008 (21.02.2008)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

60/904,212 28 February 2007 (28.02.2007) US

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(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

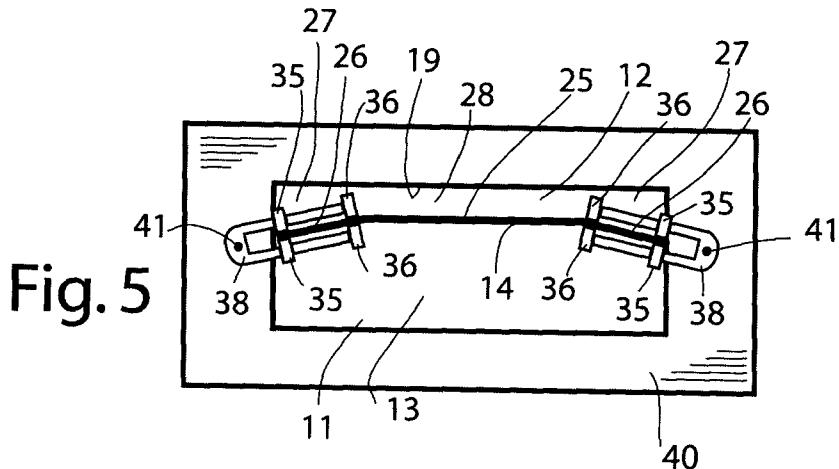
(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, NO, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Declarations under Rule 4.17:

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))
- of inventorship (Rule 4.17(iv))

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(54) Title: CO-CASTING OF METALS BY DIRECT-CHILL CASTING



WO 2008/104052 A1

(57) **Abstract:** Apparatus and method of co-casting metal ingots in direct-chill casting apparatus. The apparatus and method employs at least one divider (divider member or divider wall) that separates a casting mold into two or more chambers for receiving molten metal that is combined into a single ingot. The divider may be moved, angled and/or flexed during casting to produce ingots that are designed primarily for rolling into thin plate or sheet. The ingot has at least one outer layer that is thicker adjacent to the side (width) edges than in the center, and/or thicker adjacent to the butt or head regions. This compensates for wiping of the outer layer from the ingot core during rolling. Also, the divider may be outwardly bowed outwardly towards one of the mold walls during the casting run.



Published:

— *with international search report*

CO-CASTING OF METALS BY DIRECT-CHILL CASTING

TECHNICAL FIELD

This invention relates to the casting of metals, particularly aluminum and aluminum alloys, by direct chill casting techniques. More particularly, the invention relates to the co-casting of metal layers by direct chill casting.

BACKGROUND ART

Metal ingots are commonly produced by direct chill (DC) casting of molten metals in which a molten metal is poured into a mold having an open upper end and (after start-up) an open lower end. The metal emerges from the lower end of the mold as a metal ingot that descends as the casting operation proceeds. In other cases, the casting takes place horizontally, but the procedure is essentially the same. Such casting techniques are particularly suited for the casting of aluminum and aluminum alloys, but are suitable for the casting of other metals as well.

Casting techniques of this kind are discussed extensively in U.S. Patent No. 6,260,602 to Wagstaff, which relates exclusively to the casting of monolithic ingots, i.e. ingots made of the same material throughout cast as a single layer or ingot. Apparatus and methods for casting layered structures by DC casting are disclosed, for example, in U.S. patent 6,705,384 to Kilmer et al., issued March 16, 2004, and in U.S. Patent Publication No. 2005/0011630 A1 to Anderson et al., published on January 20, 2005. The Kilmer et al. patent makes use of a metallic divider member suspended in a direct-chill mold. The divider member separates the mold into two chambers that may be supplied with different molten metals, and the member becomes part of the ingot as the molten metal freezes. Consequently, the divider member is continuously fed into the mold through the entry end as the casting operation progresses so that part of the divider member is always present in the mold to keep the molten metal pools separated from each other. In contrast, the Anderson et al. publication employs so-called sequential solidification which requires the casting of a first layer (e.g. a core ingot) and allowing it to cool to the extent that it forms a solid (or at least

semi-solid) outer surface, and then, subsequently but in the same casting operation, casting one or more layers of other metal on the solidified surface of the first metal layer. This can be achieved by providing a cooled divider wall at the entrance of the mold to divide the mold entrance into two

5 chambers for receiving feeds of different molten metals. The divider wall remains in place during the casting operation and does not become incorporated into the solidified ingot. The length of the divider wall (in the axial direction of the mold) is long enough to permit the first layer to form its solid shell before it comes into contact with molten metal forming additional
10 layers. The disclosures of the Wagstaff, Kilmer et al. and Anderson et al. references are specifically incorporated herein by this reference.

Ingots produced by both of these co-casting techniques, i.e. the use of a continuously supplied divider member that becomes incorporated into the ingot, and the provision of a cooled divider wall, may suffer from certain
15 disadvantages, especially when intended for subsequent rolling into sheet products, such as brazing strip. One problem is that a relatively thin coating layer formed on a thicker core ingot may be "wiped off" during rolling at the leading and trailing ends of the ingot (i.e. at the ingot head and butt ends), and also at the width sides of the ingot. These phenomena are referred to,
20 respectively, as head-, butt- and edge-wiping, and involve a squeezing of the metal of the coating layer beyond the ends or sides of the ingot at the points where localized rolling pressures may be higher than those over the remainder of the ingot. Another problem is that, because the ingot is subjected to different cooling dynamics during the main stage of the casting
25 operation than at the start and end of casting, so that the cooling ingot is subjected to different rates of contraction in these stages, the interface between the layers may become non-planar in the final cast ingot. This may cause differences of thickness of the coating layer after rolling.

There is therefore a need for improvements to casting apparatus and
30 methods of this kind.

DISCLOSURE OF THE INVENTION

An exemplary embodiment of the invention provides an apparatus for casting a composite metal ingot. The apparatus comprises an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end opening and to move axially of the mold during casting. The mold cavity has opposed side walls and opposed end walls adapted to cast a generally rectangular composite ingot having opposed faces and opposed ends. A divider is positioned in the mold cavity and extends across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers. The apparatus further includes a first molten metal feed arrangement for feeding molten metal for a first layer of the composite ingot into one of the feed chambers, and a second molten metal feed arrangement for feeding molten metal for a second layer of the composite ingot into the second feed chamber. The apparatus further includes a support for the divider, the support being movable, at least in part, thereby allowing the divider to be moved and/or flexed at times during casting in directions towards or away from one of the side walls of the mold cavity.

Another exemplary embodiment of the invention provides a method of casting a metal ingot having an inner metal layer and at least one outer layer. The method involves providing a direct chill casting mold having a mold cavity divided into at least two chambers by at least one divider, separately introducing molten metal into the at least two chambers to produce a cast ingot including the layers and having a head region, a butt region, lateral side regions and a central region between the head, butt and side regions. The method further involves moving and/or flexing the at least one divider within the casting cavity at different times during casting. This allows the at least one outer layer of the cast ingot to be thicker in at least one of the head region, the butt region, and the end regions than in the central region, or to maintain a planar arrangement at the interface between the layers.

Another exemplary embodiment provides an apparatus for casting a composite metal ingot, comprising: an open-ended generally rectangular

mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a rectangular composite ingot having

- 5 opposed faces and opposed ends; a divider positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers; a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot to one of said feed chambers;
- 10 and a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot to said second feed chamber; wherein said divider has a central part and two opposite end parts, said end parts being oriented relative to said central part such that said second layer of said composite ingot emerging from said discharge end of said mold cavity has
- 15 end regions adjacent to said opposed ends of said ingot of greater thickness than a central region positioned between said end regions.

Another exemplary embodiment provides an apparatus for casting a composite metal ingot, comprising: an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a rectangular composite ingot having opposed faces and opposed ends; a longitudinal divider positioned in said mold cavity and extending across the cavity towards opposite end walls

- 20 thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers, said divider being flexible in directions towards and away from said opposed side walls of the mold cavity; a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot to one of said feed chambers; a second molten metal
- 25 feed arrangement for feeding molten metal for a second layer of said composite ingot to said second feed chamber; and flexing equipment acting on said divider to produce flexing of at least a central part of said divider
- 30

towards and away from one of said opposed side walls at different times during casting.

Yet another exemplary embodiment provides an apparatus for casting a composite metal ingot, comprising: an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a rectangular composite ingot having opposed faces and opposed ends; a divider positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers; a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot to one of said feed chambers; a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot to said second feed chamber; and a guide for said divider, said guide being movable, thereby allowing said divider to be moved at times during casting relative to said mold cavity in directions towards or away from one of said side walls of the mold cavity.

Other exemplary embodiments relate to methods of casting for producing ingots as indicated above.

The term "divider" as used in this specification (both in the description and claims) is intended to include any means for dividing an entry portion of a direct chill casting mold into two internal chambers (feed chambers) for continuous metal casting. If the divider is in the form of a continuous sheet or plate fed into the mold and intended to become part of the ingot (e.g. as disclosed in Kilmer et al.), it is referred to herein as a "divider member". On the other hand, a divider that is cooled and remains stationary in the mold (e.g. as disclosed in Anderson et al.) is referred to herein as a "divider wall". Of course, the divider may be rigid (as is normally the case for conventional divider walls) or fully or partially flexible (normally more suitable for divider members), at least at operational temperatures of the casting apparatus. The divider may be only movable or only flexible or both movable and flexible. By

an appropriate combination of such features, it is possible to produce an ingot having an outer layer that is thicker in any one or all of the head, butt and lateral edge regions to compensate for wiping-off of the peripheral parts of the outer layer during later rolling. It should also be appreciated that,

5 despite such differences in thickness of parts of the outer layer, the overall thickness of the cast ingot is preferably constant throughout (i.e. the thickness of the inner layer is adjusted in such parts to maintain the overall thickness the same).

It is to be noted that that the term "rectangular" as used in this
10 specification is meant to include the term "square", although ingots intended for rolling are generally not square. The term "generally rectangular" includes small variations from the rectangular outline that are common in ingot casting of this kind. For example, contraction may cause ingot walls to be slightly concave. Precise geometrical shapes are often hard to produce, or
15 unnecessary, in casting procedures of this kind, so the reference to "rectangular" or "square" should be interpreted with this in mind.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a simplified top plan view of a co-casting mold apparatus;

20 Fig. 2 is a side elevation of the apparatus of Fig. 1, showing the casting of an ingot;

Fig. 3 is a transverse cross-section of an ingot cast according to Fig. 2;

Fig. 4 is a longitudinal cross-section of an ingot cast as in Fig. 2;

25 Fig. 5 is a top plan view similar to Fig. 1, but showing end-angling of a divider member used in the casting operation;

Fig. 6 is a transverse cross-section of an ingot cast according to Fig. 5;

Fig. 7 and Fig. 8 are top plan views of a casting apparatus showing equipment that allows the divider member to be moved towards (Fig. 8) or away from (Fig. 7) a side wall of the mold;

30 Fig. 9 is a longitudinal cross-section of an ingot cast according to Figs. 7 and 8;

Fig. 10 is a transverse cross-section of an ingot of a metal having a high coefficient of contraction cast according to Fig. 1;

Fig. 11 is a top plan view of a mold apparatus (operated during the main stage of casting) with equipment to avoid the curve in the divider 5 member shown in Fig. 10;

Figs. 12 and 13 are cross-sections, partly in perspective, of apparatus similar to that of Fig. 12, showing a divider member caused to take on a curve (Fig. 12) or allowed to retain a planar arrangement (Fig. 13);

Fig. 14 is a top plan view of a casting mold apparatus showing 10 equipment to cause a divider member to have angled end portions and a central portion that may be allowed to be planar (solid lines) or caused to adopt an outward curve (broken lines); and

Fig. 15 is a view similar to that of Fig. 14 of an embodiment having a 15 divider wall for sequential co-casting rather than a divider member that becomes embedded in the ingot.

BEST MODES FOR CARRYING OUT THE INVENTION

Figures 1 and 2 of the accompanying drawings show a modification of the Kilmer et al. casting apparatus referred to above. It will of course be 20 realized by persons skilled in the art that Figures 1 and 2 are greatly simplified and that a working version of the apparatus will require additional equipment and structures, all of which will be apparent to a person skilled in the art.

Figures 1 and 2 show a rectangular direct-chill casting mold 10 having 25 a mold cavity 11 which is divided into two mold chambers (i.e. metal feed chambers) 12 and 13 by a vertical divider member 14. The divider member 14 may be attached to a bottom block 15, which is positioned at a discharge end opening (or outlet) 16 of the mold cavity during start-up and is fed into the mold from above by a supporting and feed apparatus (not shown). The 30 divider member 14 may be made of a suitable metal, e.g. aluminum, an aluminum alloy, or a clad aluminum product that preferably has a solidus temperature greater than the liquidus temperature of the molten alloys fed to

the chambers via supply tubes 19 and 19', or equivalent metal supply apparatus such as launders, and cast on either side of the divider member in the chambers 12 and 13. As the bottom block 15 descends during casting, cooling water 17 is directed onto the outer surface 18 of the emerging ingot

5 20 in order to cool this surface of the ingot as quickly as possible. As noted earlier, the divider member 14 becomes incorporated into the ingot as the ingot solidifies. If desired, more than one divider member 14 may be provided within the mold cavity in order to create an ingot consisting of more than two layers. A horizontal cross-section of an ingot produced according to
10 the equipment of Figures 1 and 2 incorporating a single divider member 14 is shown in Figures 3 and 4 (Fig. 3 being a transverse cross-section and Fig. 4 being a longitudinal cross-section through the same ingot). The ingot has two distinct layers 21 and 22 of solidified metal separated by divider member 14 incorporated into the solid structure. It should be appreciated that one of
15 the layers, e.g. layer 21, is intended only as a cladding and may thus be much thinner than represented here.

It will be seen that the divider member 14 is essentially planar so that the metal layers on each side are of constant thickness at all points between the divider member 14 and the respective rolling face 23 or 24 of the metal
20 layers, both in the transverse and in the longitudinal directions. While this kind of structure is desirable in certain applications, most ingots produced in this way are intended for rolling into sheet or plate of reduced thickness compared to the ingot itself. This involves passing the ingot several times through a rolling mill and there is a tendency for a thinner surface layer 21 (cladding) to be "wiped off" an inner layer 22 (core) towards the ends and the edges of the ingot where pressures exerted by rollers may be significantly increased compared to the remaining area of the ingot structure. The resulting thinning of the cladding layer in the rolled structure can result in significant wastage because the parts of the rolled sheet or plate product not
25 having a required thickness of coating may have to be trimmed off and discarded.

The disadvantage of layer thinning at the transverse edges (width edges) of the rolled structure is addressed by the arrangement shown in Figs. 5 and 6. The embodiment illustrated in these figures makes use of the relative flexibility of the divider member 14 caused by the relative thinness of

5 this member and the fact that it becomes heated to a relatively high temperature (e.g. 500 to 600°C or more) immediately in advance of the mold cavity 11 because of heat conducted along the divider member from the part already incorporated into the hot ingot. This allows the divider member 14 to be provided with the profile as shown in the top plan view of Figure 5, i.e.

10 having a central part 25 of the member that remains essentially planar, and opposite end parts 26 that are bent or angled relative to the central part in such a manner that one of the chambers of the mold (chamber 12) has end regions 27 of increased spacing between the divider member 14 and the adjacent side wall 19, whereas the other chamber 13 has end regions of

15 reduced spacing relative to the distance between the divider member and the opposite side wall in the end regions of the mold cavity. The chamber with the increased spacing is generally intended for the overall thinner cladding layer of the resulting ingot, consequently the ingot thus formed (shown in exaggerated form in transverse cross-section in Fig. 6) has a thinner layer 21

20 with increased thickness in the region of the lateral edges (width edges) 30 of the ingot. The ingot 20 is of constant total thickness throughout, so the increase in thickness of the cladding layer 21 in the region of the lateral ends 30 of the ingot is compensated for by a reduction in thickness of the core layer 22.

25 During rolling of an ingot of this structure, the increased thickness of the cladding layer at the lateral edges of the ingot compensates for the loss of the material of this layer caused by "edge-wipe" and thereby reduces or eliminates the need for waste-causing edge-trimming of resulting sheet or plate products. The profile of the divider member is preferably kept constant

30 throughout the entire casting operation to produce a cast ingot having a cladding layer with side edges of increased thickness along the entire length of the ingot. The positions where the ends 26 of the divider member are bent

out of the plane of the central section 25, and the angle of the bend in these positions, is of course chosen to cause the thickness of the coating layer to be as uniform as possible in the direction from one lateral side edge to the other in the finished rolled plate or sheet product. Generally, the angle

5 between the ends and central part (i.e. the angle by which the end parts deviate from the planar position) is no more than 30°, and more preferably 15 to 25°. The lengths of the angled ends, in an ingot having a width of 753 mm (69 inches) may be, for example, up to 381 mm (15 inches). The length and angle may have to be varied according to the inherent properties of the
10 metals being cast (particularly the properties of the metal used for the outer layer), the pressures employed during rolling, and the ultimate thickness of the sheet or plate products as well as the cast ingot. However, the required length and thickness for each case can be obtained empirically by carrying out test casts and rollings, or theoretically based on knowledge of the
15 materials involved and the rolling pressures employed. For example, when using aluminum alloy AA4045 as the metal of the outer layer for an ingot, the ingot dimensions may be as follows:

Ingot width:	753 mm (69 inches)
Ingot thickness:	702 mm (27.63 inches)
Length of cast ingot:	4,699 mm (185 inches)
Thickness of outer layer:	77 mm (3.01 inches)
Length of each angled part of divider member:	381 mm (15 inches)
Angle of each angled part of divider member:	25°.

A shown in Figure 5, the required bending of the divider member 14
25 can be achieved by passing the divider member between two opposed sets of rollers 35, 35 and 36, 36 supported on carriages 38 attached to the top surface 40 of the mold or by other supporting structure. If desired, instead of using two sets of rollers, a single set of elongated rollers covering the entire length of end parts 26 may be used instead, or any equivalent guiding
30 means. If the carriages 38 are pivotable about pivots 41, the angle of the bend in the divider member may be changed and the carriages then clamped against further rotation, thereby making it possible to produce ingots having

different edge thicknesses. This may be suitable for casting different combinations of metals in different casting operations.

As noted above, as well as lateral edge-wiping, so-called head- and butt-wiping may also be experienced during rolling, i.e. loss of cladding metal

5 at the longitudinal ends (head and butt) of a product rolled from an ingot.

Suitable compensation for this metal loss can be provided according to the apparatus shown in Figure 7. This shows a casting mold similar to that of Figure 1, but the guiding apparatus for the divider member 14 is movable in the manner shown by the double-headed arrows 43 and 44 to slide from a

10 position more distant from side wall 19 of the mold (Figure 7), or closer to it (Figure 8). This move can be made during a casting operation, for example

so that the divider member 14 is moved further away from side wall 19 during the start phase of casting and also during the end phase of casting, and then moved towards the sidewall 19 for the remainder of the cast (referred to as

15 the "run"). During the times when the divider member is moved in this way, the part immediately above the metal is kept planar and does not change in shape or flex significantly. As the divider member is moved from one position to the other, the part entering and descending through the molten metal undertakes a smooth curve before becoming embedded in the solidified

20 metal of the cast ingot. At other times, the divider member is kept planar throughout the cast. This produces an ingot as shown in simplified form in Figure 9, which is a longitudinal cross-section of an ingot produced in this way. As shown in the figure, the cladding layer 21 is thicker at the head 45 and butt 46 of the ingot to compensate for metal loss due to wiping of the

25 cladding layer at these locations.

Once again, the positions at which the divider member 14 is moved during casting depends on the metals being cast (particularly the metal and thickness of the cladding layer) and can be determined empirically or by calculation. The objective, of course, is to produce a rolled plate or sheet

30 product having a cladding layer with a constant thickness along the entire length the length of the ingot. For example, when using alloy AA4045 as the cladding material for an ingot dimensioned as above, the divider member

may be moved at positions approximately 508 mm (20 inches) from the head and the butt ends. The extent by which the divider member is moved again depends on the product being cast, but may represent up to 17% of the thickness of the cladding layer produced during the casting run. However, 5 increases of less than 5%, or even less than 2%, may be satisfactory, depending on the properties desired.

The desired movability of the guiding apparatus 38 can be provided by mounting the guiding apparatus 38 on rails 48 and 49 positioned at the top surface 40 of the mold and moved by a suitable motor, e.g. a linear drive or 10 worm gear (not shown). The flexibility of the divider member makes this movement possible as explained above.

In some circumstances, for example with a particular combination of metals used for the core and cladding layers, it may be desirable to provide the divider member 14 with a suitable curve or arch (as seen in a top plan 15 view), at least during a particular stage of the casting procedure, either over the entire width of the divider member or at least in the central part 25 when using the apparatus of Figure 5. This is because contraction of the core layer during solidification and cooling may cause the metal to contract more at the center of a rolling face than in a region near the lateral edges. This 20 contraction will, in turn, cause the cladding layer to follow the contraction of the core layer and may produce an ingot having a cladding layer with a greater thickness at the center of a rolling face than at the lateral edges. Indeed, the entire ingot may have a rolling face that is dished in this way. Figure 10 shows an ingot of this kind in exaggerated form (shown as a cross- 25 section at a position intermediate the head and butt) produced from a rectangular mold and provided with a divider member 14 initially introduced into the mold in planar form.

To compensate for such contraction issues, the divider member 14 may be outwardly curved as it is fed into the mold so that, upon solidification 30 of the ingot, the divider member adopts a more planar configuration. This can be achieved, for example, by employing apparatus as shown in Figures 11 and 12 wherein a pusher rod 50 is movably mounted on a cross-brace 51

and has a roller 52 at its outer end that bears against a surface 53 of the divider member 14 at the center thereof. During casting, the ingot experiences greater cooling at the start and at the end of the casting procedure and solidification of the metal is more rapid at those times.

5 Because of this, contraction forces have less distance over which to act and less time to act on the metal of the core layer, so there is less of a tendency for the core layer to be pulled in at the center during these initial and end phases. Therefore, during the start and end of casting, the divider member may be allowed to adopt a planar configuration, as shown in Fig. 13. During
10 steady state casting (the casting run) between the start and end phases, however, the divider member 14 is provided with a convex configuration by movement of the pusher rod 50 to the position shown in Figures 11 and 12. The pusher rod 50 may be driven by any suitable motor (not shown), e.g. via a pinion (not shown) acting on a rack 55 cut into the underside of the pusher
15 rod as shown in Figs. 12 and 13. As with the other embodiments referred to above, the degree to which the divider member is made convex can be determined empirically or by calculation with the goal of allowing the divider member to return to the planar configuration in the solidified ingot. Generally, however, the curved part may represent 10% or less of the total thickness of
20 the cladding layer, and generally 5-7%. It will be noticed in Figs. 11 to 13 that the sidewalls 19, 19' of the casting mold are themselves outwardly bowed to compensate for contraction of the rolling faces of the resulting ingot with a view to producing an ingot that is close to rectangular (planar rolling faces) after casting and cooling.

25 Figure 14 shows a casting mold provided with a combination of the features described earlier. This is achieved by providing both the roller arrangements 35, 36 of Figure 5, the movable carriages 38, 43, 44 of Fig. 7, and the movable pusher 50, 52 of Figures 11 to 13. An arrangement of this kind is able to compensate for all of the following deficiencies of conventional
30 co-casting of this kind, namely:

thinning of a cladding layer due to lateral edge-wipe during rolling;
thinning of a cladding layer at the head and butt of an ingot due to
head- and butt-wiping during rolling;
concavity of the interface between a core layer and a cladding layer at
5 a central part of an ingot due to metal contraction in the casting run; and
concavity of the rolling faces of the ingot due to metal contraction in
the casting run.

When employing sequential casting apparatus of the kind disclosed by Anderson et al., a fixed divider wall is used rather than an elongated flexible
10 divider member that is incorporated into the ingot. As the divider wall remains within the entry portion of the mold, there is no need for the guide rollers shown in the earlier embodiments provided to guide and support the divider member as it moves downwardly through the mold in concert with the casting of the ingot. Fig. 15 is a view equivalent to Fig. 14, but of an
15 embodiment having a cooled divider wall. The divider wall 14 itself may be flexible, but the end sections 26 are firmly held by supporting bars 58 positioned at the upper end of the divider wall. The central section 25 has no such support, and is therefore free to move between a planar shape and an arched shape (shown in broken lines) as described previously with respect to
20 Fig. 14. As is also the case for the embodiment of Fig. 14, the divider wall 14 may be mounted on rails 48, 49 or the like so that it may be moved backwards and forwards as shown by the double headed arrows 43 and 44, thereby allowing for increased thickness of the coating layer at the head and butt regions of the ingot. In this way, casting apparatus incorporating a
25 divider wall and supports 58 may be made to operate in the same way as any of the embodiments of Fig. 3 to 14 and essentially the same details apply.

CLAIMS:

1. Apparatus for casting a composite metal ingot, comprising: an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end opening and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a generally rectangular composite ingot having opposed faces and opposed ends; a divider positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers; a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot into one of said feed chambers; and a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot into said second feed chamber; characterized in that said apparatus further includes a support for said divider, said support being movable, at least in part, thereby allowing said divider to be moved and/or flexed at times during casting in directions towards or away from one of said side walls of the mold cavity.
2. Apparatus according to claim 1, characterized in that said support for said divider is movable towards or away from said one of said side walls of the mold cavity.
3. Apparatus according to claim 1, characterized in that said divider is a divider member and said support is fixed relative to said mold cavity but includes a part that is movable to cause said divider member to flex towards or away from one of said side walls of the mold cavity.
4. Apparatus according to claim 1, claim 2 or claim 3, characterized in that said apparatus includes two dividers, each provided with one said support.

5. Apparatus according to claim 2, characterized in that said divider has a central part and two opposite end parts, said end parts being oriented relative to said central part such that said second layer of said composite ingot emerging from said discharge end of said mold cavity has end regions adjacent to said opposed ends of said ingot of greater thickness than a central region positioned between said end regions.

6. Apparatus according to claim 5, characterized in that said divider is flexible in directions towards and away from said opposed side walls of the mold cavity; and wherein said support includes flexing equipment acting on said divider to produce flexing of at least a central part of said divider towards and away from one of said opposed side walls at different times during casting.

7. Apparatus according to claim 6, characterized in that guides for said divider are positioned at locations where said end parts meet said central part, said guides being adapted to prevent flexing of said central part from causing flexing of said end parts.

8. Apparatus according to claim 3, characterized in that said divider has a central part and two opposite end parts, said end parts being oriented relative to said central part such that said second layer of said composite ingot emerging from said discharge end of said mold cavity has end regions adjacent to said opposed ends of said ingot of greater thickness than a central region positioned between said end regions, and wherein said central part of said divider is flexible in directions towards and away from said opposed side walls of the mold cavity, and said support includes flexing equipment acting on said central part of said divider to allow flexing of at least a central part of said divider towards and away from one of said opposed side walls of said mold cavity.

9. A method of casting a metal ingot having an inner metal layer and at least one outer layer, comprising providing a direct chill casting mold having a mold cavity divided into at least two chambers by at least one divider,

separately introducing molten metal into the at least two chambers to produce a cast ingot including said layers and having a head region, a butt region, lateral side regions and a central region between said head, butt and end regions, characterized in that said at least one divider is moved and/or flexed within said casting cavity at different times during casting.

10. Apparatus for casting a composite metal ingot, comprising:

an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end opening and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a generally rectangular composite ingot having opposed faces and opposed ends;

a divider positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers;

a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot into one of said feed chambers;

a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot into said second feed chamber; and

a support for said divider, said support being movable, thereby allowing said divider to be moved at times during casting relative to said mold cavity in directions towards or away from one of said side walls of the mold cavity.

11. Apparatus for casting a composite metal ingot, comprising:

an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end opening and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a generally rectangular composite ingot having opposed faces and opposed ends;

a divider positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second feed chambers;

a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot to one of said feed chambers; and

a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot to said second feed chamber;

wherein said divider has a central part and two opposite end parts, said end parts being oriented relative to said central part such that said second layer of said composite ingot emerging from said discharge end of said mold cavity has end regions adjacent to said opposed ends of said ingot of greater thickness than a central region positioned between said end regions.

12. The apparatus of claim 11, wherein said divider is flexible, at least in said central part, and said apparatus includes movable positioning elements acting on said divider member to cause said central part to change between planar and curved orientations.

13. The apparatus of claim 11, including a movable support for said divider, said support being adapted to move said divider between different positions within said entry end portion of said mold cavity.

14. Apparatus for casting a composite metal ingot, comprising:

an open-ended generally rectangular mold cavity having an entry end portion, a discharge end opening, and a movable bottom block adapted to fit within the discharge end opening and to move axially of the mold during casting, said mold cavity having opposed side walls and opposed end walls adapted to cast a generally rectangular composite ingot having opposed faces and opposed ends;

a longitudinal divider member positioned in said mold cavity and extending across the cavity towards opposite end walls thereof, thereby dividing at least the entry end portion of the mold cavity into first and second

feed chambers, said divider member being flexible in directions towards and away from said opposed side walls of the mold cavity;

a first molten metal feed arrangement for feeding molten metal for a first layer of said composite ingot to one of said feed chambers;

a second molten metal feed arrangement for feeding molten metal for a second layer of said composite ingot to said second feed chamber; and

flexing equipment acting on said divider member to produce flexing of at least a central part of said divider member towards and away from one of said opposed side walls.

15. The apparatus of claim 14, wherein said divider member has opposite end parts, one on each side of said central part, said end parts being oriented relative to said central part such that said second layer of said composite ingot emerging from said discharge end of said mold cavity has end regions adjacent to said opposed ends of said ingot of greater thickness than a central region positioned between said end regions.

16. The apparatus of claim 15, wherein said flexing equipment acts only on said central part of said divider, said end parts remaining unflexed during casting.

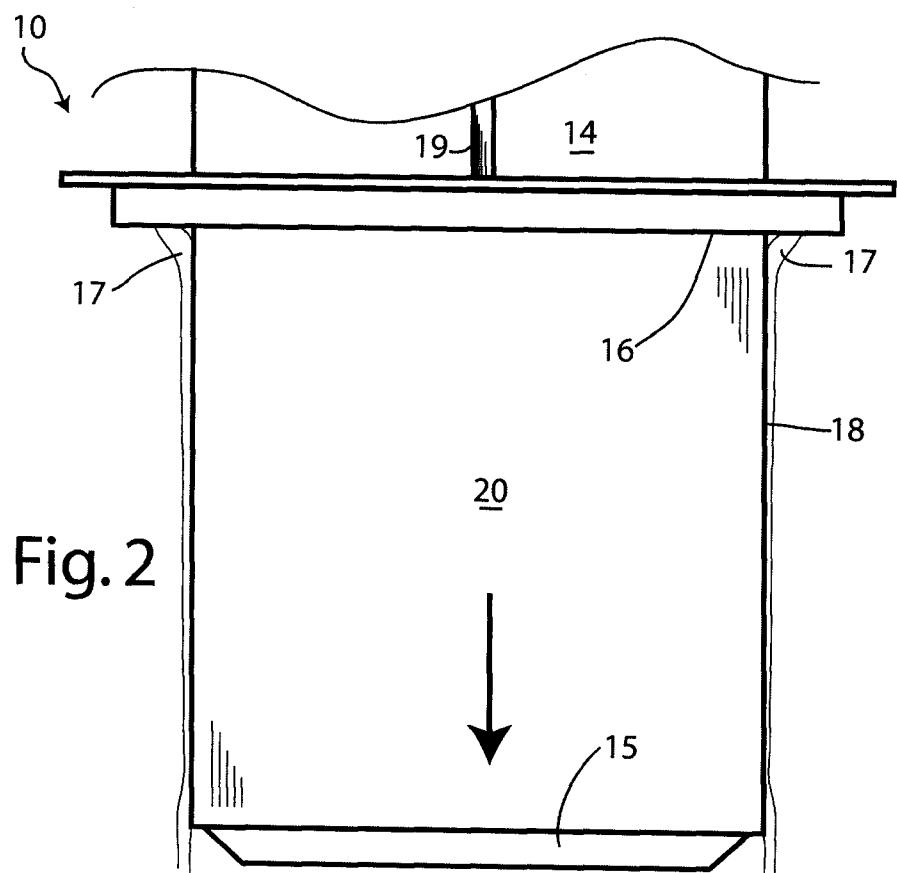
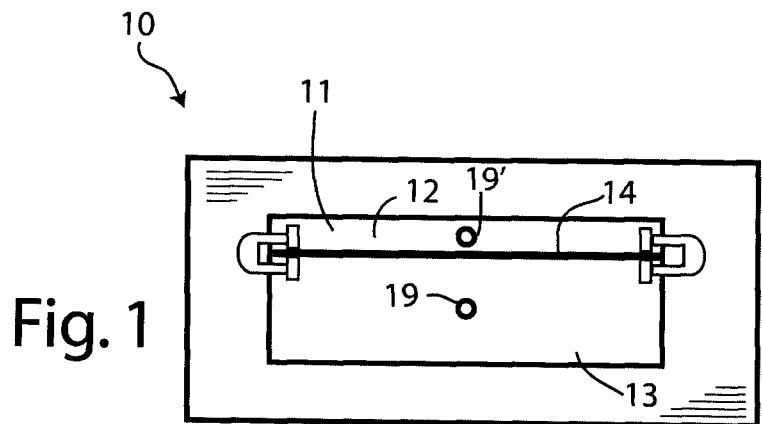
17. The apparatus of claim 15, wherein guides for said divider member are positioned at locations where said end parts meet said central part, said guides being adapted to prevent flexing of said central part from causing flexing of said end parts.

18. A method of casting a metal ingot having an inner metal layer and at least one outer layer, comprising providing a direct chill casting mold having a mold cavity divided into at least two chambers by at least one divider member, and separately introducing molten metal into the at least two chambers to produce an ingot having said layers, wherein said at least one divider member has a central part and two opposite end parts, and wherein said end parts are angled with respect to said central part during casting to

cause said at least one outer layer to be thicker adjacent to side edges of the ingot than in a center thereof.

19. A method of casting a metal ingot having an inner metal layer and at least one outer layer, comprising providing a direct chill casting mold having a mold cavity divided into at least two chambers by at least one divider member, separately introducing molten metal into the at least two chambers to produce an ingot including said layers and having a head region, a butt region and a central region between the head and butt regions, wherein said at least one divider is kept substantially planar during casting of said head and butt regions, but is moved within said casting cavity at different times during casting to cause said at least one outer layer to be thicker in said head and butt regions than in said central region.

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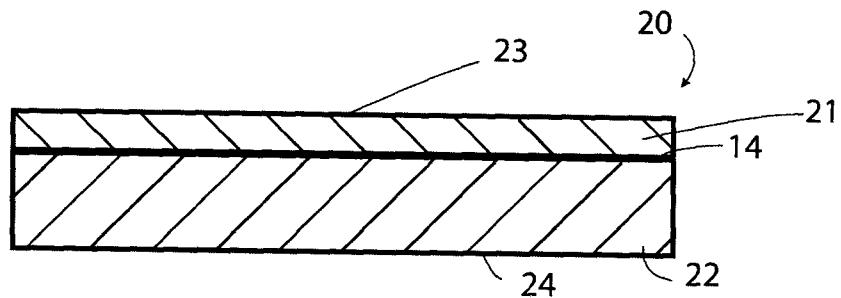


Fig. 3

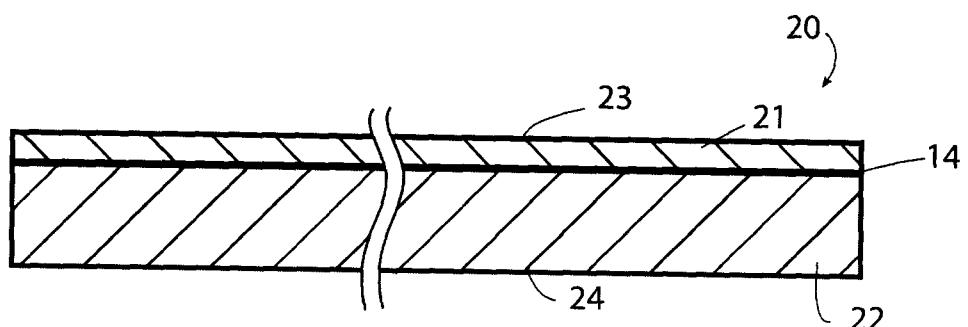


Fig. 4

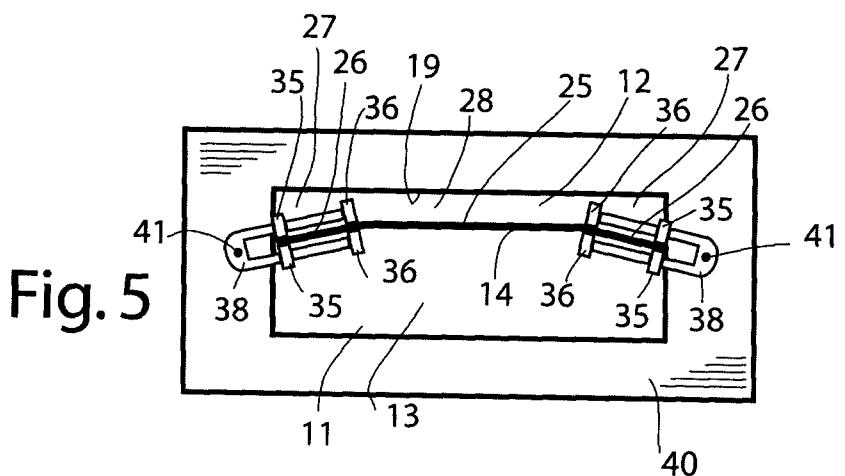


Fig. 5

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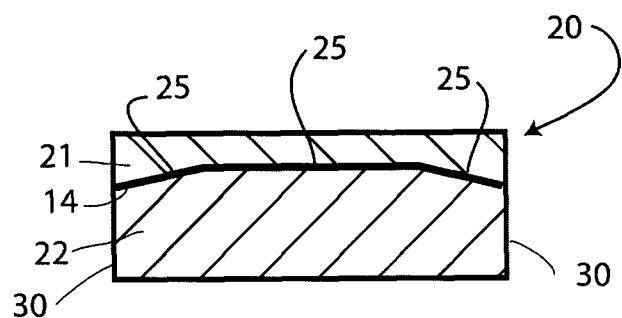


Fig. 6

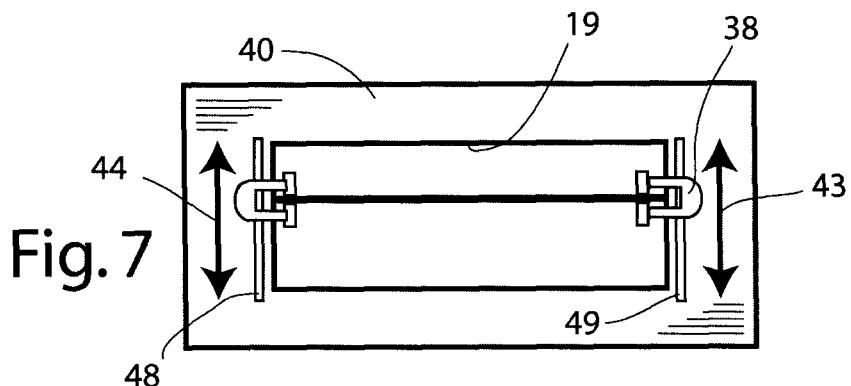


Fig. 7

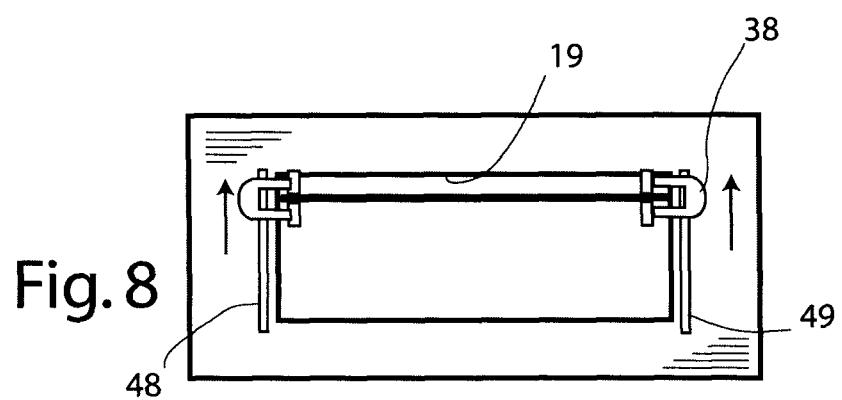


Fig. 8

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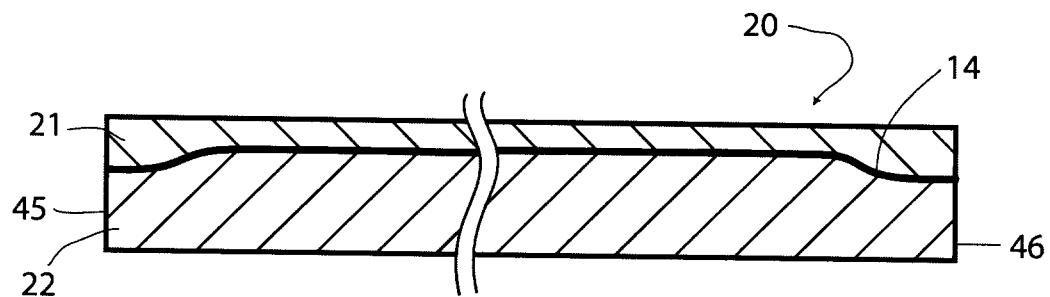


Fig. 9

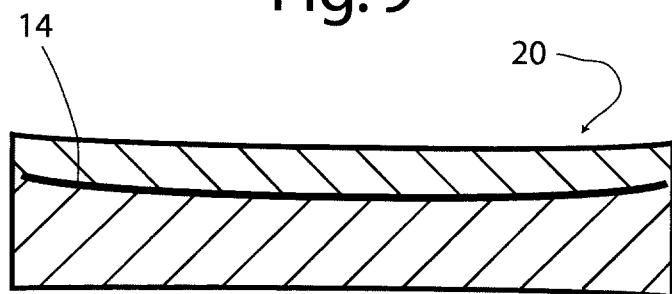


Fig. 10

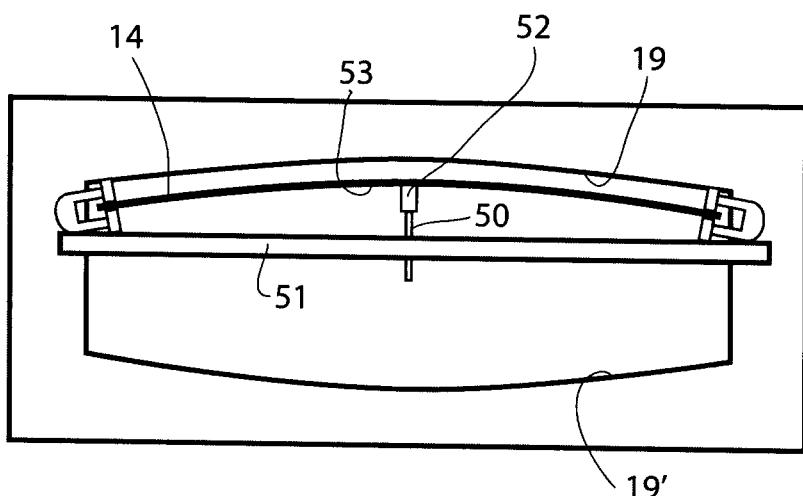


Fig. 11

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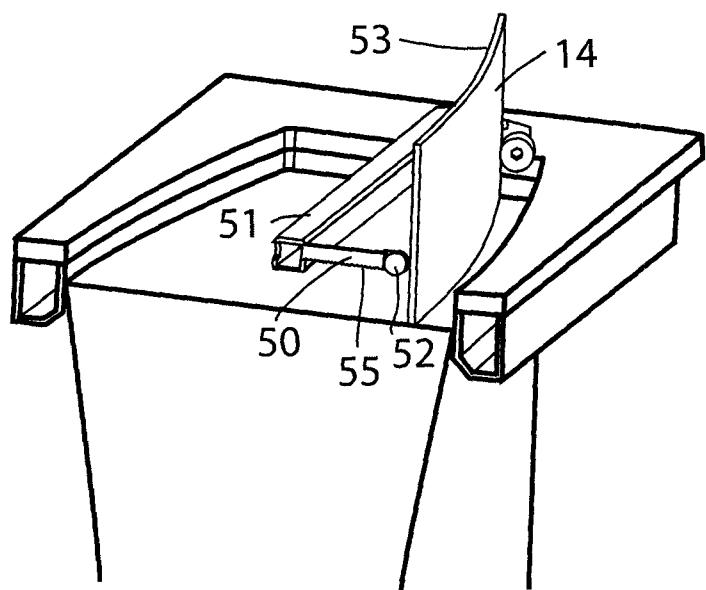


Fig. 12

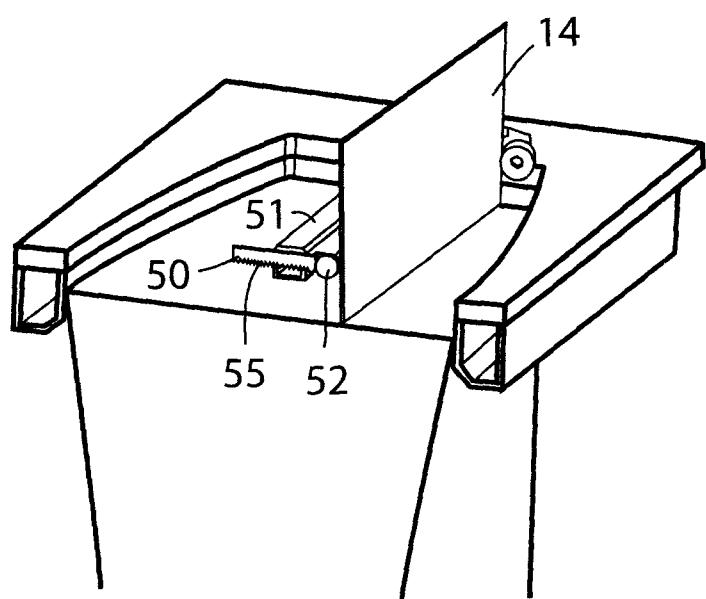


Fig. 13

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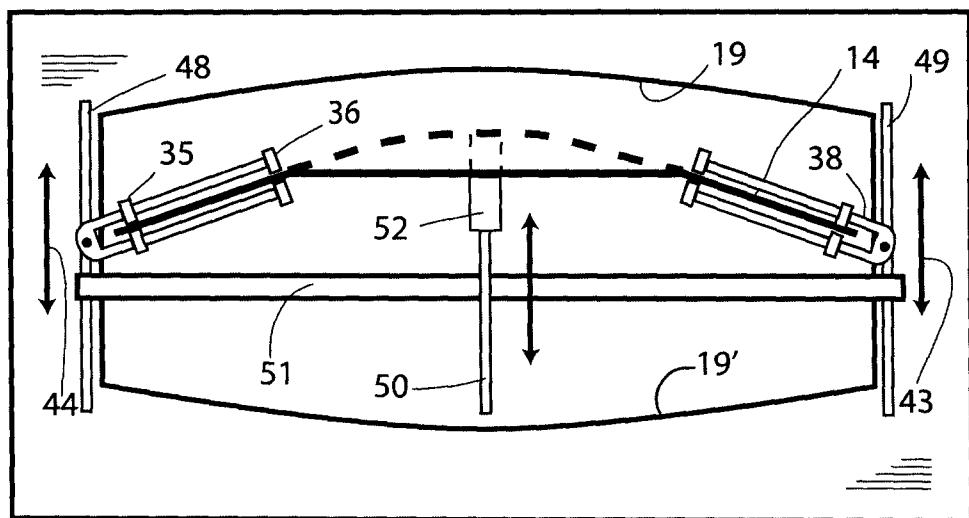


Fig. 14

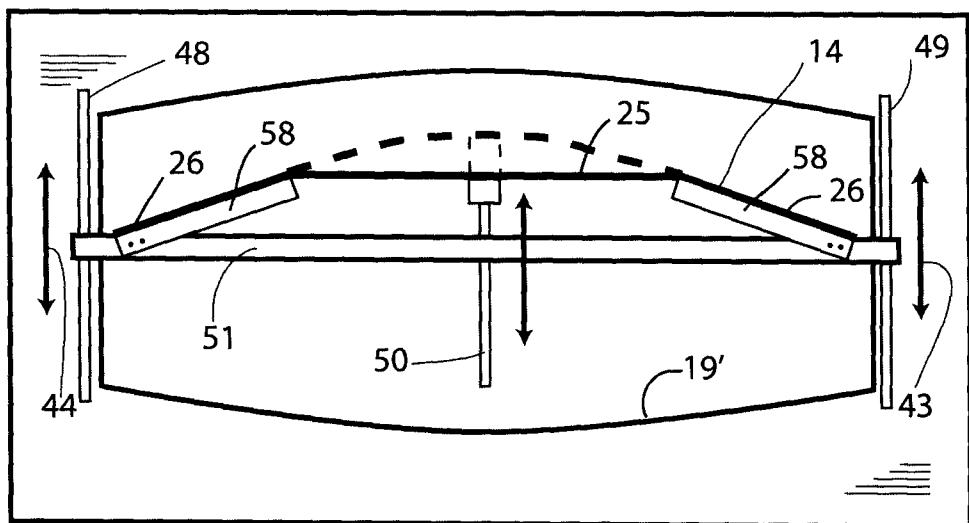


Fig. 15

INTERNATIONAL SEARCH REPORT

International application No.
PCT/CA2008/000332

A. CLASSIFICATION OF SUBJECT MATTER

IPC: **B22D 7/02** (2006.01), **B22D 15/04** (2006.01), **B22D 21/04** (2006.01), **B22D 7/08** (2006.01),
B22D 7/12 (2006.01), **B22D 9/00** (2006.01)

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: **B22D 7/02** (2006.01), **B22D 15/04** (2006.01), **B22D 21/04** (2006.01), **B22D 7/08** (2006.01), **B22D 7/12** (2006.01),
B22D 9/00 (2006.01), **B22D 11/00** (2006.01). USPC: 164/461, 164/424, 164/427, 164/429, 164/487, 164/418, 164/420.

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database(s) consulted during the international search (name of database(s) and, where practicable, search terms used)

Esp@cenet, Delphion, Canadian Patent Database.

Keywords: casting, direct chill, co-casting, composite, compound, divider, plate, barrier, coil, strip, wall, flexible.

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2006/0185816 A1 (ANDERSON, M. et al.) 24 August 2006 (24-08-2006)	1-4, 9, 10, 14
Y	* figures 6 and 7, paragraph [0107] *	5, 6, 8, 12, 13, 15, 16, 18
X	US 6,705,384 B2 (KILMER, R. et al.) 16 March 2004 (16-03-2004)	11
Y	* figure 9, column 8, lines 37-60 *	5, 6, 8, 12, 13, 15, 16, 18
A	DE 44 20 697 A1 (INST VERFORMUNGSKUNDE UND HUET) 21 December 1995 (21-12-1995) * the whole document *	1-19
A	JP 6297092 A (NIPPON STEEL CORP) 25 October 1994 (25-10-1994) * the whole document *	1-19
A	JP 61276746 A (SUMITOMO METAL IND) 6 December 1986 (06-12-1986) * the whole document *	1-19
A	JP 55068156 A (SUMITOMO METAL IND) 22 May 1980 (22-05-1980) * the whole document *	1-19

[] Further documents are listed in the continuation of Box C.

[X] See patent family annex.

* Special categories of cited documents :	
“A” document defining the general state of the art which is not considered to be of particular relevance	“T” later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
“E” earlier application or patent but published on or after the international filing date	“X” document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
“L” document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	“Y” document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
“O” document referring to an oral disclosure, use, exhibition or other means	“&” document member of the same patent family
“P” document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

4 June 2008 (04-06-2008)

Date of mailing of the international search report

6 June 2008 (06-06-2008)

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Authorized officer
Jeremy Garnet 819- 956-8721

INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.
PCT/CA2008/000332

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