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- [54] **MOTOR CONTROL CIRCUIT** 5,086,492 2/1992 Kent 388/815
5,338,977 8/1994 Carobolante 388/815
- [75] Inventor: **Seiichi Yamamoto**, Kyoto, Japan
- [73] Assignee: **Rohm Co., Ltd.**, Kyoto, Japan
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318/677; 318/632
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388/900; 318/637-638, 671, 677-682, 632

Primary Examiner—David Martin
Attorney, Agent, or Firm—Nikaido Marmelstein Murray & Oram LLP

[57] **ABSTRACT**

In an optical disc player, as signals are read from and written to an optical disc, the optical disc is rotated by a spindle motor and an optical pickup is moved by a sled motor. These motors are both direct-current motors. The motor control circuit of the invention uses a drive circuit based on the BTL method, and additionally uses a resistor that is connected in series with the direct-current motor between the output terminals of the drive circuit. The voltage drop across the resistor is fed back, as positive feedback, to the drive circuit through a feedback amplifier. Since, when the motor is started up, a high current flows through the motor and thus a large voltage drop occurs across the resistor, a high feedback voltage is obtained and thus a high drive voltage is applied to the motor.

- [56] **References Cited**
U.S. PATENT DOCUMENTS
4,350,943 8/1982 Pritchard 318/432
4,933,614 6/1990 Kawata 388/821
5,020,125 5/1991 Losic et al. 318/811

3 Claims, 4 Drawing Sheets

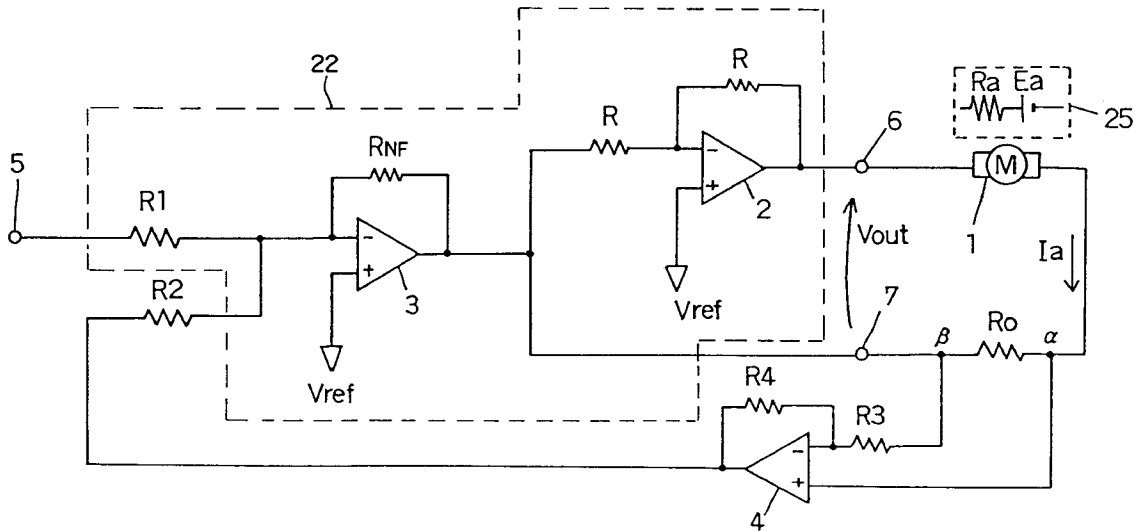


FIG. 1
PRIOR ART

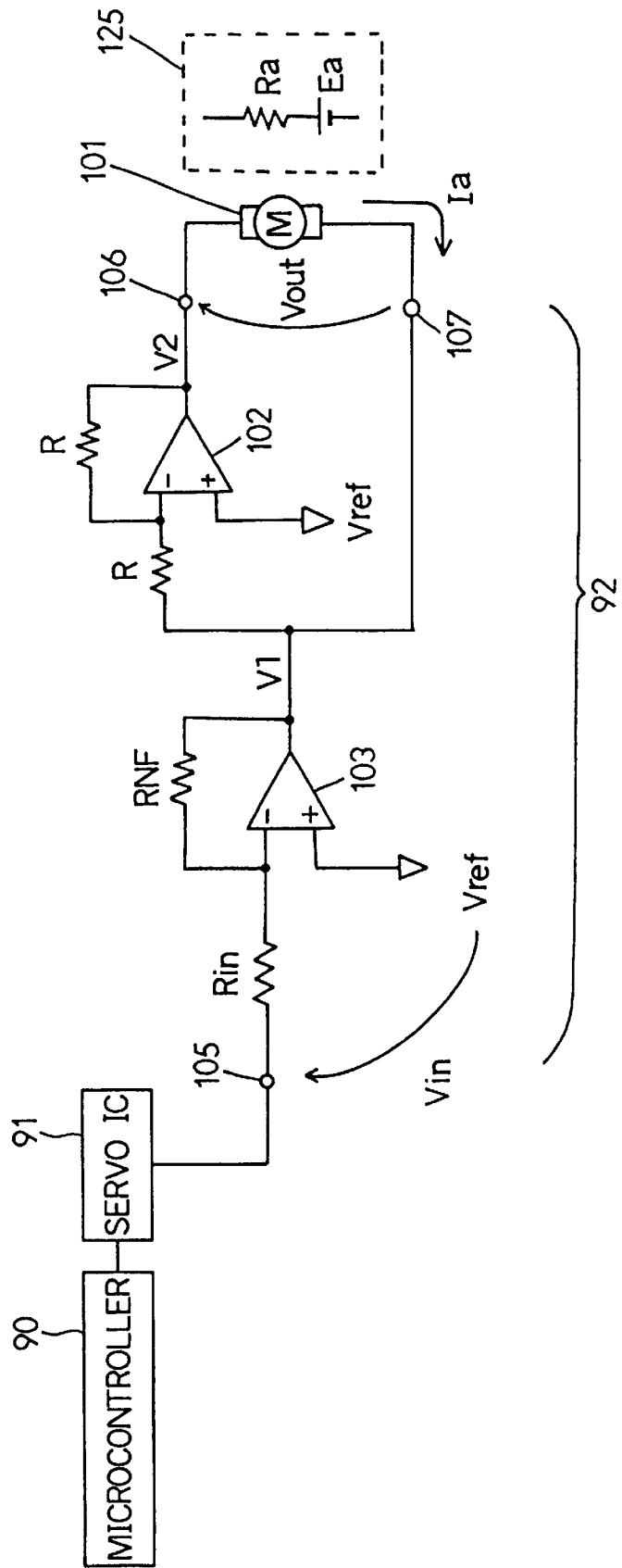
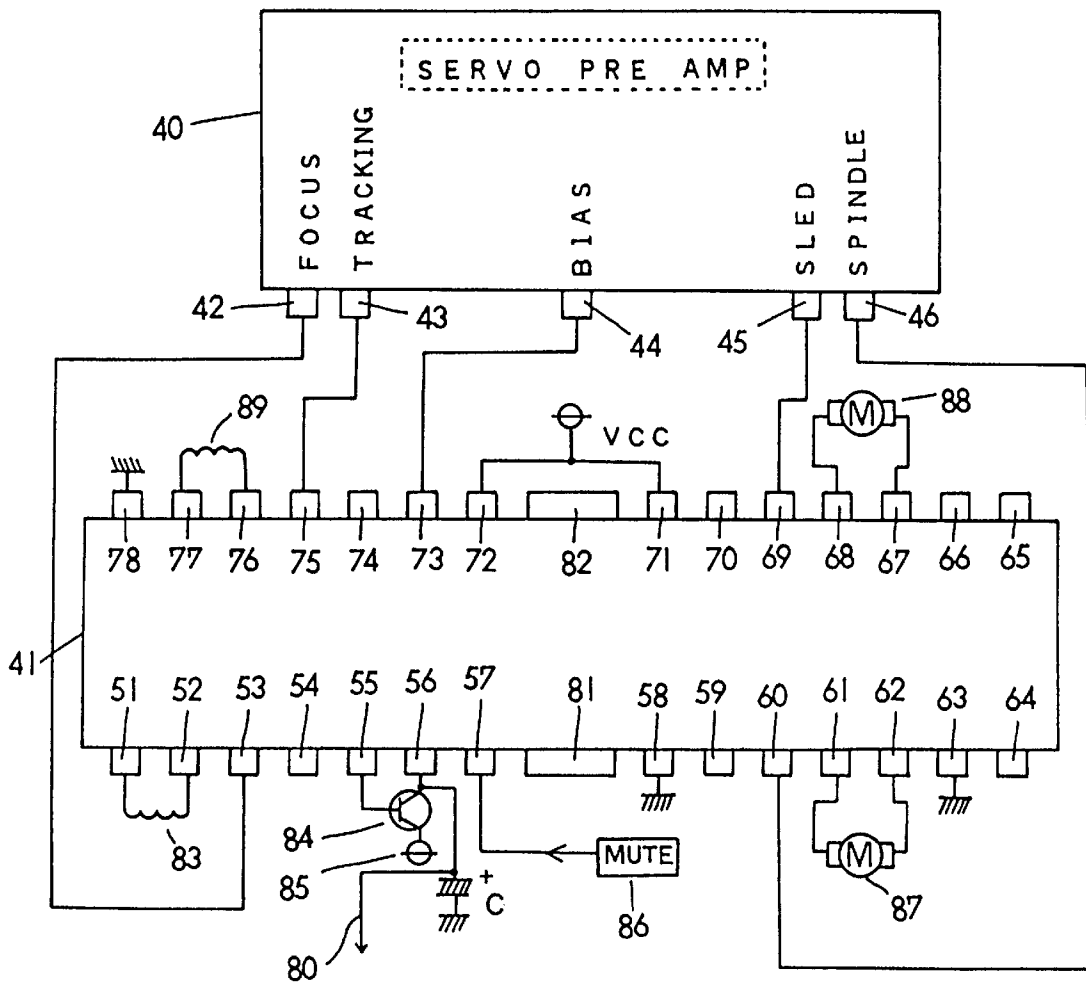


FIG. 4



MOTOR CONTROL CIRCUIT

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a motor control circuit for controlling a direct-current motor by use of a drive circuit based on the BTL (balanced transformer less) method.

2. Description of the Prior Art

Optical disc players include players for CDs (compact discs), CD-ROMs, DVDs (digital video discs), DVD-ROMs, SD-ROMs (super-density ROMs), LDs (laser discs), MDs (minidisks), and similar optical discs. In optical disc players, as signals are read from or write to an optical disc, the optical disc is rotated by a spindle motor, and an optical pickup is moved by a sled motor.

Conventional optical disc players employ a drive circuit based on the BTL method as shown in FIG. 1. In FIG. 1, the direct-current motor **101**, which is a motor having brushes, corresponds to a spindle motor or sled motor used in an optical disc player. Typically, an optical disc player is provided with separate drive circuits to control a spindle motor and a sled motor independently.

The drive circuit **92** shown in FIG. 1 operates as follows. The drive circuit **92** receives at its input terminal **105** a control voltage from a servo IC **91**. The control voltage is fed through a resistor R_{in} to the inverting input terminal (-) of an operational amplifier **103**. The operational amplifier **103** receives at its non-inverting input terminal (+) a reference voltage (V_{ref}). The voltage difference between the control voltage and the reference voltage (V_{ref}) is represented by V_{in} . The operational amplifier **103** has a feedback resistor R_{NF} connected between its inverting input terminal (-) and output terminal, so that the output voltage of the operational amplifier **3** is

$$V_1 = -(R_{NF}/R_{in})V_{in} + V_{ref}$$

This voltage V_1 is fed through a resistor R to the inverting input terminal (-) of another operational amplifier **102**. The operational amplifier **102** receives at its non-inverting terminal (+) the reference voltage (V_{ref}). Moreover, the operational amplifier **102** has a feedback resistor R connected to its inverting input terminal (-), so that the output voltage of the operational amplifier **102** is

$$V_2 = -(V_1 - V_{ref})$$

This voltage V_2 is output via an output terminal **106**. On the other hand, the voltage V_1 is outputted via another output terminal **107**. The motor **101** is connected between these output terminals **106** and **107**. Thus, when a voltage V_{out} is applied to the motor **101**, the motor **101** rotates. Here, V_{out} is expressed as

$$\begin{aligned} V_{out} &= V_2 - V_1 \\ &= -(V_1 - V_{ref}) + (R_{NF}/R_{in})V_{in} - V_{ref} \\ &= 2(R_{NF}/R_{in})V_{in} \end{aligned}$$

Accordingly, the voltage V_{out} applied to the motor **101** varies according as the voltage V_{in} varies, and this voltage V_{in} varies according as the control voltage fed from the servo IC **91** varies. In some applications, the servo IC **91** is controlled by instructions given from software running on a microcontroller **90**.

As shown in the broken-line square **125**, the motor **101** can be regarded as equivalent to a circuit composed of

armature resistance R_a and back electromotive force (voltage) E_a connected in series. Here, the back electromotive force E_a is proportional to the rotation rate N (i.e. number of revolutions per unit time) of the motor **101**. Accordingly, the current that flows through the motor **101** is expressed as

$$I_a = (V_{out} - E_a)/R_a, \quad (1)$$

and the back electromotive force E_a , which is proportional to the rotation rate N , is expressed as

$$E_a = K \cdot \Phi \cdot N.$$

(Here, K is the constant of proportionality, and Φ is the effective magnetic flux per pole.) Hence, the rotation rate N is expressed as

$$N = E_a / (K \cdot \Phi). \quad (2)$$

Further, from expressions (1) and (2), the following expression is obtained:

$$N = (V_{out} - I_a \cdot R_a) / (K \cdot \Phi). \quad (3)$$

As described above, the voltage V_{out} applied to the motor **101** is controlled in accordance with the control voltage from the servo IC **91**. However, as expression (3) indicates, this does not mean that the rotation rate N is directly controlled in accordance with the control voltage; in reality, it is controlled as follows. Consider, for example, a transient state of the motor **101**, as when the motor has just been started up. When the motor **101**, after having been completely at rest, receives a voltage V_{out} and thus starts to rotate, the back electromotive force E_a does not appear at first. Accordingly, at this time, the current I_a is larger than predicted from expression (1), and thus the rotation rate N is lower than predicted from expression (3). Then, gradually, the rotation rate N increases, and the current I_a decreases accordingly, until the motor comes to rotate at a constant rotation rate N .

In an optical disc player, in order to improve the rate at which signals are read from or written to an optical disc, it is essential to improve the response of the motor **101**.

However, in conventional optical disc players employing the drive circuit **92**, only the voltage V_{out} to be applied across the motor **101** can be controlled. As a result, the response cannot be improved beyond limits imposed by factors such as the inertia of the motor **101**. To overcome this problem, in conventional optical disc players, it is customary to force the microcontroller **90** to vary the control voltage disproportionately when the rotation rate of the motor **101** needs to be varied greatly, as when the motor **101** has just been started up. For example, it is possible to start up the motor **101** more quickly by forcing the microcontroller **90** to demand a disproportionately high control voltage to obtain an accordingly higher output voltage V_{out} . However, such control requires the microcontroller **90** to perform complicate operations. Moreover, raising the control voltage means increasing the gain and thus tends to result in unstable operation of the drive circuit **92** due to oscillation or other undesirable condition. Accordingly, the gain cannot be increased beyond a certain limit.

Furthermore, when the load of the motor **101** as seen from the output terminals **106** and **107** varies, this drive circuit **92** cannot cope with it. To solve this problem, in conventional optical disc players, as the microcontroller **90** reads signals from the optical disc, it checks whether those signals have been read correctly, and instructs the servo IC **91** to adjust

the control voltage appropriately. However, to achieve this, the microcontroller **90**, the servo IC **92**, and the drive circuit **92** all need to be involved in the control of the motor **101**. Such control requires complicate operations, and thus the response cannot be improved beyond a certain limit.

Ideally, the motor **101** should be controlled by directly controlling its rotation rate N . In addition, the motor **101** needs to reach the desired rotation rate N as quickly as possible. However, in conventional optical disc players employing the drive circuit **92**, the rotation rate N cannot be controlled directly. As a result, the response cannot be improved beyond a certain limit. Moreover, the drive circuit **92** cannot cope with variation in the load. As a result, the microcontroller **90** and the servo IC **91** need to perform complicate operations, and thus, also for this reason, the response cannot be improved beyond a limit.

SUMMARY OF THE INVENTION

An object of the present invention is to improve the rate at which signals are read from and written to an optical disc in an optical disc player by improving the response of motors used there.

To achieve the above object, according to one aspect of the present invention, a motor control circuit for controlling a direct-current motor is provided with an input terminal for receiving a control voltage for controlling the motor; an amplifier for amplifying the control voltage received via the input terminal; a first output terminal for outputting the amplified control voltage; inverting means for inverting the amplified control voltage; a second output terminal for outputting the inverted control voltage; a resistor connected in series with the motor between the first and second output terminal; and a feedback circuit for feeding a voltage across the resistor back to an input terminal of the amplifier as positive feedback.

According to another aspect of the present invention, a motor control circuit for controlling a direct-current motor is provided with a drive circuit for driving the direct-current motor by a BTL method; a resistor connected in series with the direct-current motor; and a feedback circuit for feeding a voltage drop across the resistor back to the drive circuit as positive feedback.

According to still another aspect of the present invention, a motor control circuit for use in an optical disc player for controlling a direct-current motor is provided with a drive circuit for driving the direct-current motor by a BTL method; a resistor connected in series with the direct-current motor; and a feedback circuit for feeding a voltage drop across the resistor back to the drive circuit as positive feedback. Here, two control systems each comprising the BTL-method-based drive circuit, the resistor, and the feedback circuit are provided and are integrated together with a tracking circuit and a focusing circuit into an integrated circuit, so that one of the control systems is used to control a spindle motor and the other is used to control a sled motor.

BRIEF DESCRIPTION OF THE DRAWINGS

This and other objects and features of this invention will become clear from the following description, taken in conjunction with the preferred embodiments with reference to the accompanied drawings in which:

FIG. **1** is a circuit diagram of a conventional motor control circuit;

FIG. **2** is a circuit diagram of a motor control circuit as a first embodiment of the present invention;

FIG. **3** is a circuit diagram of another motor control circuit as a second embodiment of the present invention; and

FIG. **4** is a circuit diagram of a relevant portion of an optical disc player as a third embodiment of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, embodiments of the present invention will be described with reference to the drawings.

<First Embodiment>

FIG. **2** is a circuit diagram of a motor control circuit as a first embodiment of the present invention. In this embodiment, the BTL-type drive circuit **92** shown in FIG. **1** as used in conventional optical disc players is further provided with a detection resistor R_O connected in series with the motor **1**, so that part of the voltage drop across this resistor R_O is fed, as positive feedback, to the inverting input terminal (-) of the operational amplifier **3** through another operational amplifier **4** serving as a feedback amplifier.

Numeral **5** represents an input terminal to which a control voltage for controlling the motor is supplied from a servo IC or the like. The control voltage supplied to the input terminal **5** is then fed through a resistor R_1 to the inverting input terminal (-) of the operational amplifier **3**. The operational amplifier **3** receives at its non-inverting input terminal (+) a reference voltage V_{ref} , has a feedback resistor R_{NF} connected between its output terminal and inverting input terminal (-), and receives at its inverting input terminal (-) the output of the operational amplifier **4** through a resistor R_2 .

The output terminal of the operational amplifier **3** is connected to the output terminal **7** of the drive circuit, and is also connected through a resistor R to the inverting input terminal (-) of still another operational amplifier **2**. The operational amplifier **2** receives at its non-inverting input terminal (+) the reference voltage V_{ref} , and has a feedback resistor R connected between its output terminal and inverting input terminal (-). This feedback resistor R has the same resistance as the resistor connected between the inverting input terminal of the operational amplifier **2** and the output terminal of the operational amplifier **3**. For this reason, these two resistors are represented by the same symbol R . Numeral **6** represents another output terminal of the drive circuit **22**. The motor **1** and the detection resistor R_O are connected between the two output terminals **6** and **7** of the drive circuit **22**. An equivalent circuit of the motor **1** is shown in the broken-line square **25**, where R_a represents the armature resistance, and E_a represents the back electromotive force (voltage). I_a represents the current that flows through the motor **1**. As this current I_a flows, a voltage is developed across the detection resistor R_O , and this voltage is fed to the operational amplifier **4**. Specifically, the node α at one end of the detection resistor R_O is connected to the non-inverting terminal (+) of the operational amplifier **4**, and the node β at the other end is connected through a resistor R_3 to the inverting terminal (-) of the operational amplifier **4**.

The operational amplifier **4** has a feedback resistor R_4 connected between its output terminal and inverting input terminal (-), so that part of the voltage drop developed across the detection resistor R_O (i.e. the voltage across the detection resistor R_O) is fed, as positive feedback, to the operational amplifier **3** through the operational amplifier **4** and the resistor R_2 . In this way, this embodiment uses positive feedback of a voltage.

In the conventional drive circuit shown in FIG. **1**, it is the voltage V_{out} between the output terminals **106** and **107** that

is controlled by the control voltage received at the input terminal 105. In this embodiment, the voltage V_{out} between the output terminals 6 and 7 is further varied in accordance with the current I_a flowing through the motor 1, so that the rotation rate of the motor 1 is controlled directly by the control voltage received at the input terminal 5. As a result, the rotation rate of the motor 1 does not vary so much even when the load as seen from the output terminals 6 and 7 varies, and thus the motor 1 can reach the desired rotation rate more quickly.

For example, consider the start-up state of the motor 1 where the motor 1 at rest has just been started so as to reach a given rotation rate. At first, only small back electromotive force E_a occurs, and accordingly the current I_a is relatively large. As a result, the voltage across the detection resistor R_o rises in proportion to the current I_a . This voltage is amplified by the operational amplifier 4, and accordingly the voltage supplied as positive feedback to the operational amplifier 3 rises in proportion to the current I_a . This rise in the voltage at the inverting input terminal (-) of the operational amplifier 3 causes the voltage V_{out} to rise, and thus the motor reaches the desired rotation rate more quickly. In addition, the microcontroller or servo IC (neither is shown) does not need to perform complicate operations, and therefore the control of the motor 1 can be realized with simple circuits.

In this way, the response of the motor 1 is improved. This contributes, with a spindle motor, to quicker start-up and reduced variation in the rotation rate, and, with a sled motor, to quicker movement of the optical pickup. As a result, the optical disc player can read signals from or write them to an optical disc at a higher rate. Note that, in this embodiment, oscillation is prevented by designing the drive circuit to have a gain lower than an amplification factor of one (i.e. 0 dB) at a phase of 180°.

<Second Embodiment>

FIG. 3 is a circuit diagram of another motor control circuit as a second embodiment of the present invention. In this embodiment, the drive circuit 32 is formed in an integrated circuit 10. A motor 1 and a detection resistor R_o are connected in series between output terminals 19 and 20 of the drive circuit 32, and a control voltage 24 is supplied to an input terminal 11 of the drive circuit. The rotation rate of the motor 1 is controlled by varying the control voltage 24, which is fed from a servo IC or microcontroller (neither is shown).

The drive circuit also receives a bias voltage V_{bias} at another input terminal 12. The bias voltage V_{bias} is set, for example, to 2.5 V. Thus, a voltage difference V_{in} occurs between the two input terminals 11 and 12. The control voltage 24 received at the input terminal 11 is fed through a resistor R_{in} to the inverting input terminal (-) of an operational amplifier 13, and the bias voltage V_{bias} is fed to the non-inverting input terminal (+) of the operational amplifier 13. As a result, a current I_{in} flows through the resistor R_{in} . The current I_{in} is expressed as

$$I_{in} = V_{in} / R_{in}. \quad (4)$$

This current I_{in} is fed to a current switching circuit 14. The current switching circuit 14 outputs a current I_{in} via its plus terminal (+), and receives a current I_{in} via its minus terminal (-). Here, the combination of the operational amplifier 13 and the current switching circuit 14 serves as a kind of voltage-controlled current source circuit that outputs a current $\pm I_{in}$ in proportion to the voltage V_{in} it receives; or it may be regarded as a voltage-to-current conversion circuit.

The plus terminal (+) of the current switching circuit 14 is connected, via a line L1, to a drive buffer 17, which is a

buffer circuit having an amplification factor of approximately one and having a sufficiently high impedance. Accordingly, as indicated by arrow A, the current I_{in} output from the current switching circuit 14 via its plus terminal (+) flows, together with a current I_{NF} (described later) added thereto at a node 36, through a resistor R_{ref} into the source of a reference voltage V_{ref} . Therefore, the voltage V_{o1} appearing at one output terminal 19 is expressed as

$$V_{o1} = (I_{in} + I_{NF}) R_{ref} + V_{ref}. \quad (5)$$

On the other hand, the minus terminal (-) of the current switching circuit 14 is connected, via a line L2, to another drive buffer 18, which is a buffer circuit of the same type as the drive buffer 17. Accordingly, as indicated by arrow B, the current I_{in} flowing into the current switching circuit 14 via its minus terminal (-) is a current fed through a resistor R_{ref} from the source of the reference voltage V_{ref} less a current I_{NF} (described later) that is diverted therefrom at a node 37. Therefore, the voltage V_{o2} appearing at the other output terminal 20 is expressed as

$$V_{o2} = V_{ref} - (I_{in} + I_{NF}) R_{ref}.$$

Hence, the voltage V_o between the output terminals 19 and 20 is expressed as

$$V_o = V_{o1} - V_{o2} = 2(I_{in} + I_{NF}) R_{ref}. \quad (5)$$

That is, the voltage V_o is applied across the serially connected motor 1 and detection resistor R_o . This voltage V_o is proportional to the current $I_{in} + I_{NF}$. Here, the drive buffers 17 and 18, together with their respective resistors R_{ref} , each serve as a kind of current-controlled voltage source circuit; or they may be regarded as current-to-voltage conversion circuits. Moreover, the nodes 36 and 37 each serve as a kind of current synthesizer for performing a given operation between the currents I_{in} and I_{NF} . At the node 36, the line L1 is connected to a line L3; at the node 37, the line L2 is connected to a line L4. A node 38 at one end of the detection resistor R_o is connected to the non-inverting input terminal (+) of another operational amplifier 15, and a node 39 at the other end of the detection resistor R_o is connected, via a terminal 21 and then through a resistor R_{NF} , to the inverting input terminal (-) of this operational amplifier 15. This resistor R_{NF} is formed within the integrated circuit 10. Now, suppose that a current I_a flows through the motor 1. Then, the current I_{NF} that flows through the resistor R_{NF} is expressed as

$$I_{NF} = (I_a R_o) / R_{NF}. \quad (6)$$

Here, the current I_{NF} is assumed to be substantially smaller than the current I_a . A simple way to achieve this is to make the resistance of the detection resistor R_o as small as practicable.

The current I_{NF} is fed to a current switching circuit 16. The current switching circuit 16 outputs a current I_{NF} via its plus (+) terminal, and receives a current I_{NF} via its minus (-) terminal. Also here, the combination of the operational amplifier 15 and the current switching circuit 16 serves as a kind of voltage-controlled current source circuit. As mentioned previously, the current I_{NF} from the plus terminal (+) of the current switching circuit 16 is fed via line L3 to the node 36, and the current I_{NF} from the node 37 is fed via line L4 to the minus (-) terminal of the current switching circuit 16. In this way, positive feedback of the current I_{NF} is achieved. From expressions (4) to (6) above, the voltage V_o is expressed as

$$V_o = 2(V_{in} / R_{in} + I_a R_o / R_{NF}) R_{ref}. \quad (7)$$

As described earlier, the motor **1** can be regarded as equivalent to a circuit **25** composed of armature resistance R_a and back electromotive force E_a connected in series. Accordingly, with respect to the motor **1**, the voltage V_o is expressed as

$$V_o = E_a + (R_a + R_o)I_a \quad (8)$$

From expressions (7) and (8), the back electromotive force E_a is expressed as

$$E_a = 2(R_{ref} / R_{in})V_{in} + \{(2R_{ref} / R_{NF} - 1)R_o - R_a\}I_a$$

As expression (2) indicates, the electromotive force E_a is proportional to the rotation rate N . Accordingly, in order to control the electromotive force E_a by varying the voltage V_{in} , the following condition needs to be satisfied:

$$(2R_{ref} / R_{NF} - 1)R_o - R_a = 0$$

In this way, the rotation rate N is controlled directly by varying the voltage V_{in} . This makes it easy to determine the voltage V_{in} corresponding to a given rotation rate N and thus helps simplify the control of the motor **1**. Moreover, simply by keeping the voltage V_{in} constant, the back electromotive force E_a is kept constant by feedback. This helps reduce variation in the rotation rate N that occurs when the load as seen from the output terminals **19** and **20** varies. Furthermore, the voltage V_o is controlled in such a way that its change is directly reflected in the rotation rate N . This enables the motor **1** to reach the desired rotation rate more quickly. Moreover, only a control voltage **24** corresponding to the desired rotation rate N needs to be fed from an external circuit such as a microcontroller or servo IC (neither is shown). This eliminates the need for the microcontroller or servo IC (neither is shown) to perform special operations, and thus allows the motor **1** to be controlled with simple circuits. This embodiment uses positive feedback of a current.

The integrated circuit **10** is, via its terminal **22**, connected to a power source voltage V_{CC} on which it operates, and, via a terminal **23**, connected to ground (GND). In cases where the motor **1** is a sled motor, the control voltage **24** is switched between positive and negative voltages to control the rotation direction of the motor **1**. The present invention ensures quicker movement of the optical pickup (not shown) and thus faster writing and reading of signals.

<Third Embodiment>

FIG. 4 is a circuit diagram of a relevant portion of an optical disc player as a third embodiment of the present invention. In this embodiment, the motor control circuit of the first or second embodiment is incorporated in a semiconductor device **41**. More specifically, as described later, the semiconductor device **41** incorporates two motor control circuits, a focusing circuit, and a tracking circuit formed as an integrated circuit. Of the two motor control circuits incorporated in the semiconductor device **41**, one is for driving a spindle motor **87**, which is connected to the terminals **61** and **62** of the semiconductor device **41**, and the other is for driving a sled motor **88**, which is connected to the terminals **67** and **68** of the semiconductor device **41**. The drive circuits used here are both of the type that performs positive feedback control by use of a detection resistor as described earlier. Note, however, that the detection resistors for detecting the currents flowing through the motors **87** and **88** are incorporated in the semiconductor device **41**.

A bias voltage (BIAS) is obtained from a servo preamplifier **40** via its terminal **44**, and is fed to the terminal **73** of the semiconductor device **41**. This bias voltage (BIAS) is used by both of the motor control circuits for the motors **87** and **88**. A control voltage (SPINDLE) for controlling the rotation rate of the spindle motor **87** is obtained from the servo preamplifier **40** via its terminal **46**, and is fed to the terminal **60** of the semiconductor device **41**. A control voltage (SLED) for controlling the rotation rate of the sled motor **88** is obtained from the servo preamplifier **40** via its terminal **45**, and is fed to the terminal **69** of the semiconductor device **41**.

In an optical disc player, a laser beam needs to be kept focused on the surface of an optical disc (not shown). To control such focusing, the servo preamplifier **40** monitors the vibration of the optical disc, and outputs a focusing control signal (FOCUS) via its terminal **42**. The focusing control signal (FOCUS) is fed to the terminal **53** of the semiconductor device **41**. In accordance with the focusing control signal (FOCUS), the focusing circuit incorporated in the semiconductor device **41** controls focusing by supplying an appropriate current to a focus coil **83**, which is connected to the terminals **51** and **52**.

Moreover, in an optical disc player, the focus of the laser beam needs to be kept on a track formed on the optical disc. To control such tracking, the servo preamplifier **40** monitors the deviation of the laser beam, and outputs a tracking control signal (TRACKING) via its terminal **43**. The tracking control signal (TRACKING) is fed to the terminal **75** of the semiconductor device **41**. In accordance with the tracking control signal (TRACKING), the tracking circuit incorporated in the semiconductor device **41** controls tracking by supplying an appropriate current to a tracking coil **89**, which is connected to the terminals **76** and **77**.

Moreover, the semiconductor device **41** is, via its terminals **71** and **72**, connected to a power source voltage V_{CC} on which it operates, and, via its terminals **58**, **63**, and **78**, connected to ground; the terminals **54**, **59**, **64**, **65**, **66**, **70**, **74** are unused. Further, the semiconductor device **41** has its terminals **55** and **56** connected to the base and collector, respectively, of a transistor **84**, whose emitter is connected to a reference voltage **85**. From the collector of this transistor **84**, an adjustment signal **80** is extracted. For phase compensation, a capacitor C is connected between the collector of the transistor **84** and ground. This capacitor C has a capacitance of, for example, $22 \mu\text{F}$.

In some applications, the semiconductor device **41** receives, via its terminal **57**, a stop signal that is fed from a MUTE switch **86**. The stop signal is a signal that is either in a high-level or low-level state at a time. When the stop signal becomes low, reading or writing of signals from or to the optical disc is halted temporarily, and, when the stop signal becomes high, reading or writing of signals is resumed.

As described above, by additionally providing a detection resistor and a feedback amplifier to a BTL-type drive circuit so that it can perform positive feedback control, the rotation rate of a direct-current motor can be controlled directly. This not only enables the motor to reach the desired rotation rate more quickly, but also reduces variation in the rotation rate due to variation in the load. Moreover, the drive circuit then requires only a control voltage from an external control circuit such as a microcontroller or servo IC, and therefore such an external circuit does not need to be designed for special control. This makes it easy to control the rotation rate of the motor. In an optical disc player, such improvement in the response of motors leads to quicker start-up of disc rotation and to quicker movement of the optical pickup, and

thus helps achieve faster reading and writing of signals from and to the optical disc. In addition, reduction in variation of the rotation rate of motors contributes to stable operation of the motors.

In particular, according to the third embodiment of the present invention, all the circuits necessary for the rotation of the optical disc and for the movement and adjustment of the optical pickup are integrated into one integrated circuit, so that related signals can be processed at one place. Since various control signals often work in interrelated ways, processing them in one integrated circuit helps simplify the internal construction and wiring of the optical disc player. In addition, improved response of the spindle motor and the sled motor ensures faster reading and writing of signals.

What is claimed is:

1. A motor control circuit for controlling a direct-current motor, comprising:

- an input terminal for receiving a control voltage for controlling the motor;
- a first amplifier, connected to said input terminal, for amplifying the control voltage received via the input terminal;
- a first output terminal, connected to said first amplifier, for outputting the amplified control voltage;
- second amplifier, connected to said first amplifier, for inverting the amplified control voltage;
- a second output terminal, connected to said second amplifier, for outputting the output of the second amplifier;
- a resistor connected in series with the motor, said resistor and motor connected between the first and second output terminals; and
- a positive feedback circuit for feeding a voltage across the resistor back to an input terminal of the first amplifier as positive feedback.

2. A motor control circuit as claimed in claim 1, wherein the feedback circuit comprises an operational amplifier having two input terminals, one of which

being a non-inverting terminal and the other being an inverting terminal, and the resistor is connected between input terminals of the feedback circuit.

3. A motor control circuit for controlling a direct-current motor, comprising:

- a first voltage-to-current conversion circuit that receives a control voltage and a bias voltage and outputs to first and second paths two control currents whose magnitudes are both in proportion to a voltage difference between the control voltage and the bias voltage but whose phases are opposite to each other;
 - first and second buffers connected to the first and second paths, respectively;
 - a first resistor connected in series with the direct-current motor, said first resistor and direct-current motor connected between output terminals of the first and second buffers;
 - a second voltage-to-current conversion circuit, connected to first and second ends of said first resistor, said second voltage-to-current conversion circuit outputs to third and fourth paths two feedback currents whose magnitudes are both in proportion to a voltage drop across the first resistor but whose phases are opposite to each other, the third path being connected to the first path, the fourth path being connected to the second path;
 - a second resistor whose one end is connected to a reference voltage and whose other end is connected to the first path; and
 - a third resistor whose one end is connected to the reference voltage and whose other end is connected to the second path,
- wherein currents obtained by synthesizing the currents output from the first and second voltage-to-current conversion circuits flow through the second and third resistors, and voltages produced across the second and third resistors are applied to the first and second buffers.

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