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Description

This invention relates to glass-ceramics suitable for dielectric substrates.

Real progress in electronics has been paced by improvements in the basic active electronic device, viz., the transistor, and in the ability to pack ever-increasing numbers of them onto a single silicon or gallium arsenide wafer or chip. Performance of these active devices (or integrated circuits) requires them to be electrically connected to other devices and eventually to an operating medium. These devices must also be protected from overheating, from physical abuse, and from the environment. The necessary connections and protection are provided by encasing the active devices in a package. That package interconnects and supports the chip while providing protection thereto.

The greatest volumes of integrated circuits produced today are contained in organic plastic packages. However, for high reliability, long life applications, hermetically sealed ceramic packages are employed. Not frequently, alumina (Al_2O_3) and alumina multilayer packages have been utilized for such applications.

As the integrated circuit device grows in complexity, more and more active elements being packaged onto a chip, a higher proportion of the system signal response time is required to transmit signals between chips or to and from the operating application. The ideal unit would place the entire system on a single chip and eliminate or minimize off chip signals. That assembly has not been successfully produced.

Increased interconnected signal speed and integrity can be achieved by shortening the signal path between chips, by using a ceramic material having improved electrical properties, viz., a lower dielectric constant and a lower dissipation factor, and by lowering the resistance of the signal conductor and reducing noise. The closer spacing of chips requires very fine and closely-spaced signal lines and multi-layer packages with fine internal connections (vias). The combination of surface smoothness and flatness with close dimensional control becomes extremely critical for satisfactory fine line metallization and via registration. Whereas Al_2O_3 substrates and multilayer packages can be ground to a smooth flat surface, the high thermal shrinkage of Al_2O_3 (~18%), coupled with difficulty in machining, present problems in achieving high density via and pad registration. The relatively high dielectric constant of Al_2O_3 at ambient temperature (~9-10) restricts the ability to closely space signal lines (cross talk, noise results), and also slows the speed of the signal itself.

Another major drawback in the use of Al_2O_3 multilayer packages is the need for utilizing highly refractory metals such as molybdenum or tungsten for metallization because of the high firing temperature required for sintering Al_2O_3 ($\geq 1500^\circ\text{C}$). Whereas their electrical resistivities are relatively low, they are significantly higher than silver, copper, or gold, and, of course, molybdenum and tungsten require gold plating prior to soldering.

Accordingly, the objective of the present invention was to develop a new substrate material for a multilayer package exhibiting properties superior to those of Al_2O_3 for that application; those properties including a lower dielectric constant (<6), a sintering temperature no higher than 1000°C , a smooth flat surface without additional processing, and improved dimensional control for location of vias and pads.

Summary of the Invention

We have found that the above objective can be achieved through the use of a glass-ceramic containing willemite ($2\text{ZnO} \cdot \text{SiO}_2$) as the predominant crystal phase and cordierite as a secondary crystal phase for the substrate material.

Willemite has long been recognized as exhibiting good dielectric properties, but has not been employed in producing electronic substrates because of its high content of ZnO (73.1% by weight ZnO, 26.9% SiO_2). Such high ZnO contents are not only costly but, more importantly, volatilization of zinc becomes a very significant problem and control of crystallization can be formidable. We have found, however, a group of glass compositions containing a moderate level of ZnO which, upon heat treatment for relatively brief periods, e.g., 10 minutes to 2 hours, at temperatures 875°C - 1000°C (preferably $>900^\circ\text{C}$), will be converted into glass-ceramic bodies of high crystallinity wherein willemite constitutes the predominant, and sometimes sole, crystal phase. Such glass compositions consist essentially, expressed in terms of weight percent on the oxide basis, of 15-45% ZnO, 10-30% Al_2O_3 , 30-55% SiO_2 and 3-15% MgO. Up to 5% B_2O_3 , up to 5% CaO and/or SrO and/or BaO and/or PbO, up to 7% Cs_2O and up to 15% MnO may optionally be present; the total of all such optional ingredients not exceeding 15%. Those additions may lead to greater levels of crystallization and/or lower temperatures for sintering and/or heat treatment. The inclusion of at 3-15% MgO results in the generation of cordierite ($2\text{MgO} \cdot 2\text{Al}_2\text{O}_3 \cdot 5\text{SiO}_2$) as a secondary crystal phase. The zinc spinel, gahnite, ($\text{ZnO} \cdot \text{Al}_2\text{O}_3$) may also be developed in small amounts. The smaller alkali metal oxides Li_2O , Na_2O , and K_2O will be essentially absent from the compositions in order to avoid undue fluxing and to insure

securing the desired electrical properties. It will be appreciated that certain ions such as Mg^{+2} and Mn^{+2} may enter into the willemite structure to form a solid solution. Therefore, as used herein, the term willemite includes such solid solutions. Ca^{+2} , Sr^{+2} , Pb^{+2} , Ba^{+2} , and Cs^{+1} ions are too large to enter the willemite crystal structure. Their presence may improve the sintering character of the glass by retarding early crystallization of β -quartz phases. However, in all cases the amounts included will be so small that they will be incorporated into the structure of cordierite crystals co-precipitated with the willemite. Hence, substantial concentrations thereof lead to the growth of unwanted crystal phases.

The capability of varying the identity of the crystal phases in the final product permits the close tailoring of the properties exhibited thereby. For example, the linear coefficient of thermal expansion (0° - 300° C) can be designed to be compatible with silicon ($35-45 \times 10^{-7}/^{\circ}$ C). The dielectric constants of the inventive materials at ambient temperature range between 5-6 and thermal shrinkage of the inventive materials can be better controlled from lot-to-lot, since the starting batch material therefor, i.e., a glass, provides a more homogeneous, uniform composition. And, because a glass-ceramic is formed through the heat treatment of a parent glass body which crystallizes the glass in situ, the surfaces of the glass-ceramic body can be smooth and flat as made; i.e., no subsequent machining is necessary.

The inventive glass-ceramics can be prepared in bulk form in the conventional manner, i.e., according to the following three general steps: first, a glass-forming batch, customarily containing a nucleating agent, is melted; second, that melt is cooled below the transformation range thereof and simultaneously a glass body of a desired configuration is shaped therefrom; and, third, that glass body is exposed to a predetermined heat treatment (875° - 1000° C) to cause the glass body to crystallize in situ. Operable nucleating agents include 8-12% ZrO_2 and 0.001-0.05% of a noble metal such as Au, Pd, and Pt. The use of TiO_2 as a nucleating agent leads to the growth of gahnite rather than willemite.

The inventive glass-ceramics can also be prepared without the inclusion of a nucleating agent. In this process the glass resulting from the second step of the above method is comminuted to a fine powder, and that powder fired at temperatures between 875° - 1000° C to sinter the particles into an integral body, e.g., a sheet or film, and, concurrently, to cause the glass to crystallize in situ. Nucleating is provided by the surfaces of the powdered glass particles.

This second process is of special utility with respect to forming integrated circuit packages. Thus, the finely-divided glass particles (commonly having diameters of less than $10 \mu m$) can be cast and bonded into tapes which, in turn, can be laid up and the resultant assembly fired at 875° - 1000° C to form a glass-ceramic substrate of a desired thickness.

Several mechanisms have been posited to explain the development of a willemite crystal phase in the inventive glass-ceramics even though the ZnO concentrations therein are far below 73.1%. To illustrate: First, it is known that Mg^{+2} and Mn^{+2} ions can substitute for Zn^{+2} ions in the willemite structure. Second, Al_2O_3 may replace the combination of ZnO and SiO_2 ; i.e., Al_2O_3 may substitute for $SiO_2 + ZnO$ with the same number of oxygen atoms and same charge balance. $Al_2O_3 + B_2O_3$ may react with $2SiO_2 + 2ZnO$, with B^{+3} ions replacing Si^{+4} ions and Al^{+3} ions replacing Zn^{+2} ions. The possibility of replacing $2Zn^{+2}$ ions with a Si^{+4} ion plus a cation vacancy has also been theorized. That replacement would obviously introduce a local charge imbalance, but it is believed that such condition could be tolerated to some extent.

Each of those mechanisms would give rise to willemite solid solution wherein the overall X-ray diffraction pattern displays the general character of willemite, but wherein the peaks are shifted slightly and the intensities modified somewhat. It is conjectured that some combination of those mechanisms could quite conceivably lead to greater crystallinity than would normally be anticipated. The glassy phase remaining would be in the so called cabal area of glass formation where diffusion of cations is very difficult and excellent electrical resistivity and dielectric behaviour are observed.

Prior Art

U.S. Patents 3,460,967, 3,460,987, 3,681,097, 3,681,102, 3,854,963, 3,951,669, 4,199,340, 4,256,796, 4,358,541, and 4,385,127 are presently considered to be representative of the state of the art.

Description of Preferred Embodiments

Table I records a number of precursor glass compositions, expressed in terms of parts by weight on the oxide basis. Those compositions which contain MgO within the range of 3-15% by weight are illustrative of the invention. The other compositions are comparative. Inasmuch as the sum of the individual constituents totals or closely approximates 100, for all practical purposes the reported values can be considered to reflect weight percent. The actual batch ingredients may comprise any materials, either oxides or other

compounds, which, when melted together, will be converted into the desired oxide in the proper proportions.

5 The components for each of the exemplary compositions listed in Table I were compounded, ballmilled together to assist in obtaining a homogeneous melt, charged into platinum crucibles, and lids placed thereupon. The crucibles were introduced into a furnace operating at about 1650°C, and the batches melted for about 6 hours. The melts were poured into a steel mold to form glass slabs having dimensions of about 20x10x1.3 cm (8"x4"x0.5") and that slab was immediately moved to an annealer operating at 700°C. The casting of the melts into slabs permits the inspection of glass quality. Also, specimens can be cut therefrom with a diamond saw for use in testing for various physical properties. Where finely-divided
10 particles are desired, the molten glass can be poured as a thin stream into a bath of tap water, practice termed "d rigaging" in the glass art. The resulting glass particles are dried and comminuted to a predetermined grain size.

Whereas the following examples reflect laboratory work, it must be appreciated that the compositions recited in Table I could be scaled up to be used in commercial glassmaking facilities. Although no fining agent, such as As_2O_3 and/or Sb_2O_3 , was employed in the laboratory melts, an inclusion of a fining agent
15 may be useful to secure optimum glass quality in commercial production.

Table I

5		<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>
	ZnO	37	37	38	37	35	40	26.5
	Al ₂ O ₃	14	14	14	14	14	16.72	22.2
10	SiO ₂	49	49	47	45	47	39.28	42.4
	MnO	-	-	1	-	-	-	-
	MgO	-	-	-	2	4	4	8.8
15	B ₂ O ₃	-	-	-	2	-	-	-
	Pd	0.01	-	-	-	-	-	-
20		<u>8</u>	<u>9</u>	<u>10</u>	<u>11</u>	<u>12</u>	<u>13</u>	<u>14</u>
	ZnO	26.6	39.9	39.0	46.2	26.1	25.5	22.7
25	Al ₂ O ₃	19.4	16.7	14.3	12.9	24.5	24.7	22.7
	SiO ₂	44.1	39.2	38.5	35.9	40.8	39.3	43.4
	MgO	9.9	6.6	7.2	5.1	8.6	8.4	11.2
30		<u>15</u>	<u>16</u>	<u>17</u>	<u>18</u>	<u>19</u>	<u>20</u>	<u>21</u>
	ZnO	18.5	26.6	37.7	37.4	38.0	37.0	38.7
35	Al ₂ O ₃	23.2	23.3	17.8	17.6	17.8	17.4	18.1
	SiO ₂	44.4	42.0	37.6	34.5	35.0	34.1	35.6
	MgO	13.8	8.8	8.8	6.2	6.3	6.1	6.4
40	B ₂ O ₃	-	0.2	0.3	-	-	-	-
	PbO	-	-	-	4.3	-	-	-
	BaO	-	-	-	-	3.0	-	-
45	Cs ₂ O	-	-	-	-	-	5.3	-
	CaO	-	-	-	-	-	-	1.1

50 The glass slab of Example 1 was crystallized in situ by heat treating for two hours at 960°C. An x-ray diffraction analysis of the crystallized sample showed peaks typical of willemite. Dielectric properties at various temperatures and frequencies were measured on the crystallized product of Example 1 and the results of those measurements are recorded below in Table II. Electrical resistivity is tabulated in terms of Log ρ , dielectric constant as D.C., and dissipation factor as D.F.

Table II

	<u>32°C</u>	<u>32°C/Hz</u>	<u>32°C/1KHz</u>	<u>32°C/10KHz</u>	<u>32°C/100KHz</u>
Log ρ	0.0	-	-	-	-
D.C.	-	5.17	5.15	5.15	5.15
D.F.	-	0.0050	0.0007	0.0006	0.0009
	<u>147°C</u>	<u>147°C/Hz</u>	<u>147°C/1KHz</u>	<u>147°C/10KHz</u>	<u>147°C/100KHz</u>
Log ρ	13.48	-	-	-	-
D.C.	-	5.22	5.20	5.20	5.20
D.F.	-	0.0061	0.0010	0.0006	0.0005
	<u>197°C</u>	<u>197°C/Hz</u>	<u>197°C/1KHz</u>	<u>197°C/10KHz</u>	<u>197°C/100KHz</u>
Log ρ	12.04	-	-	-	-
D.C.	-	5.28	5.24	5.22	5.23
D.F.	-	0.0336	0.0051	0.0014	0.0007
	<u>247°C</u>	<u>247°C/Hz</u>	<u>247°C/1KHz</u>	<u>247°C/10KHz</u>	<u>247°C/100KHz</u>
Log ρ	10.90	-	-	-	-
D.C.	-	5.69	5.30	5.26	5.75
D.F.	-	0.5625	0.0343	0.0057	0.0156

The glass slabs of the other Examples were comminuted to pass through a No. 200 United States Sieve (74 μm), dry pressed into button-shaped specimens having a diameter of 1.3 cm (0.5") and a height of 0.64 cm (0.25"), and heat treated at various temperatures. When substantial concentrations of MgO were incorporated into the compositions, x-ray diffraction analyses indicated the development of cordierite ($2\text{MgO} \cdot 2\text{Al}_2\text{O}_3 \cdot 5\text{SiO}_2$) as a secondary crystal phase. As was explained above, it has been conjectured that the Pb^{+2} , Ba^{+2} , Ca^{+2} , and Cs^{+} ions in Examples 11-14 are incorporated into the lattice of the cordierite crystals, although that theory has not been rigorously proved. It has further been hypothesized that, because the ionic radius of the Cs^{+} ions is compatible with the large cavity in the cordierite crystal structure, the presence of Cs^{+} ions may stabilize the cordierite structure.

X-ray diffraction analysis of the button-shaped sample of Example 2 after heat treatment at 915°C for two hours evidenced a variation in the normal willemite pattern. In particular, the peak at about 0.348 nm (3.48Å) was much enhanced over the typical peaks at about 0.285 nm (2.85Å) and 0.233 nm (2.33Å). It has been posited that this shift may be due to the development of a small amount of a β -quartz phase or β -zinc silicate. β -zinc silicate has been observed on heating hemimorphite, a hydrous zinc silicate to 750°C. β -zinc silicate has a prominent X-ray peak at 0.355 nm (3.55Å). At about 960°C β -zinc silicate transforms to zinc orthosilicate, i.e., willemite.

When a button-shaped specimen of Example 3 was heat treated at 915°C for two hours, it exhibited an orange fluorescence when exposed to radiation having a wavelength of 253.7 nm (2537Å); but when a similar button-shaped sample was heat treated for two hours at 980°C, it demonstrated the green fluorescence typical of willemite when subjected to radiation of 253.7 nm (2537Å) wavelength.

The addition of B_2O_3 and/or MgO to the base $ZnO-Al_2O_3-SiO_2$ composition system results in the development of crystals displaying the typical X-ray diffraction pattern of willemite at lower temperatures and/or shorter times. Examples 4 and 5 are illustrative of that phenomenon; button-type specimens thereof exhibit the X-ray diffraction pattern typical of willemite after a heat treatment of two hours at $915^\circ C$.

As observed above, the addition of substantial amounts of MgO can lead to the generation of an additional crystal phase, cordierite, thereby resulting in an overall greater degree of crystallization. Table III records the relative peak heights observed in the X-ray diffraction patterns exhibited by button-type samples prepared from Examples 6-11 after heat treatment for two hours at $915^\circ C$ and two hours at $980^\circ C$.

Table III

Crystal Phase	X-ray Peak(m)	Example 6 Heat Treatment 915°C-2 hours	Example 7 Heat Treatment 915°C-2 hrs. 980°C-2 hrs.	
Willemite	3.48×10^{-10}	628	1083	446
	2.84×10^{-10}	626	953	834
	2.33×10^{-10}	295	412	359
Cordierite	3.14×10^{-10}	364	650	572
	3.02×10^{-10}	320	834	592
Gahnite	2.447×10^{-10}	214	119	223

Crystal Phase	X-ray Peak(m)	Example 8 Heat Treatment 915°C-2 hours 980°C-2 hours	
Willemite	3.48×10^{-10}	917	560
	2.84×10^{-10}	889	852
	2.33×10^{-10}	421	420
Cordierite	3.14×10^{-10}	660	700
	3.02×10^{-10}	642	-
Gahnite	2.447×10^{-10}	137	183

Crystal Phase	X-ray Peak(m)	Example 9 Heat Treatment 915°C-2 hours 980°C-2 hours	
Willemite	3.48×10^{-10}	860	1191
	2.84×10^{-10}	1114	1516
	2.33×10^{-10}	519	740
Cordierite	3.14×10^{-10}	405	505
	3.02×10^{-10}	519	704
Gahnite	2.447×10^{-10}	88	162

Example 10

Crystal Phase	X-ray Peak (m)	Heat Treatment	
		915°C-2 hours	980°C-2 hours
Willemite	3.48×10^{-10}	1768	991
	2.84×10^{-10}	1361	1430
	2.33×10^{-10}	619	671
Cordierite	3.14×10^{-10}	141	357
	3.02×10^{-10}	124	471
Gahnite	2.447×10^{-10}	0	162

Example 11

Crystal Phase	X-ray Peak (m)	Heat Treatment	
		915°C-2 hours	980°C-2 hours
Willemite	3.48×10^{-10}	2011	1148
	2.84×10^{-10}	1508	1585
	2.33×10^{-10}	746	838
Cordierite	3.14×10^{-10}	120	346
	3.02×10^{-10}	100	419
Gahnite	2.447×10^{-10}	0	127

A multilayer, ceramic integrated circuit package is formed by laminating together, through sintering, a plurality of individual ceramic circuit plies, wherein each ply includes a patterned electrically conductive layer and through hole connectors, termed vias, formed in the ply for connecting the patterned electrically conductive layers of the respective plies to form a predetermined wiring circuit. In general, the individual plies have been cut from tapes prepared from very finely-divided particles of ceramic material bonded together with an organic bonding medium. Thus, in common practice, holes are punched in the tapes for the connectors, the electrically conductive layers screened onto the tapes, a predetermined number of tapes laminated together with the vias in proper registry, the laminate sintered together, and the top thereof metallized.

Table IV records a number of physical properties measured on several of the above Examples which had been fabricated into tapes in accordance with the following procedure:

Glass from each Example was ballmilled for about 24 hours utilizing Al_2O_3 balls to yield powder having diameter of less than 10 μm . That powder was then mixed with an organic vehicle to a solids:organic weight ratio of 3:2 in a ball mill for about 24 hours. The organic vehicle consisted primarily of a binder (polyvinyl butyral), a solvent (toluene), and a surfactant (phosphate ester). The resultant slurry was continuously applied at a thickness of about 127-508 μm (0.005-0.02") onto a polyester film using a doctor blade and dried in air at about 25°C to volatilize off the organic solvents. The resultant tape was cut into sheets having dimensions of about 7.6x7.6 cm (3"x3") and 8-10 of those sheets stacked up. Upon firing for 120 minutes at 940°C, an integral composite laminate was formed having a thickness of about 1.5 mm (0.06"). The firing concurrently crystallized the glass powder in situ, thereby providing a glass-ceramic body suitable for use as a substrate for integrated circuit packaging. The recited properties were determined in accordance with conventional measuring techniques.

As employed in Table IV, density in terms of g/cm^3 , modulus of rupture (MOR) in terms of MPa (psi), linear coefficient of thermal expansion (Coef. Exp.) in terms of $X10^{-7}/^\circ C$. The dielectric constant (D.C.) and

dissipation factor (D.F.) measured at ambient temperature are also tabulated.

Table IV

Property	Example 4	Example 5	Example 8
Density	3.00	3.13	2.99
MOR	177 (25,700)	122(17,700)	141(20,400)
Coef. Exp.	140.4	62.4	65.7
D.C.	5.08	5.30	5.14
D.F. (100 KHz)	0.004	0.0067	0.0031
D.F. (2.54 GHz)	<0.001	-	0.001

As has been explained above, the inventive materials can be crystallized in situ very rapidly to bodies of high crystallinity; that is, exposure times as brief as 10-15 minutes at temperatures between about 875° - 1000° C are operable, with the entire firing cycle from ambient temperature through exposure to the crystallization temperature interval and return to ambient temperature requiring about one hour. This fast firing capability is especially desirable in the fabrication of integrated circuit packages in that crystallization can be obtained utilizing a firing schedule which is also useful with thick film inks of the types used in the commercial production of integrated circuits.

In those instances where the number of layers of tape is greater than four and/or the firing of the laminate is to be conducted in a neutral atmosphere, e.g., nitrogen, or in a reducing atmosphere, e.g., hydrogen, the laminate may, desirably be initially exposed to a temperature somewhat greater than 250° C for a period of time adequate to insure complete removal of the organic components prior to the crystallization heat treatment.

Table V lists physical properties measured on Examples 4, 5, 6 and 8 which had been fabricated into tapes in like manner to the description above with respect to the specimens reported in Table IV, except for the crystallization firing schedule. The stacks of sheets were placed on a lehr and subjected to the following heat treating schedule:

Ambient temperature to 800° C at about 60° C/minute
 800° C to 925° C at about 12.5° C/minute
 Hold at 925° C for about 15 minutes
 925° C to 800° C at about 25° C/minute
 800° C to ambient temperature at about 70° C/minute

The total time from entry of the specimens into the lehr to removal of the specimens from the lehr was somewhat less than about one hour.

Table V

Property	Example 4	Example 5	Example 6	Example 8
Density	3.05	3.04	3.14	2.96
MOR	122 (17,700)	106 (15,400)	108 (15,600)	121 (17,600)
Coef. Exp.	52.2	26.3	28.2	21.9
D.C.	5.21	5.54	5.74	5.37
D.F. (100 KHz)	0.0007	0.0016	0.0011	0.0013
D.F. (2.54 GHz)	-	-	-	0.0015

Table IV reports crystal phases identified through x-ray diffractometry in Examples 4, 5, and 8. In each instance the "major" phase constituted greater than 50% by volume of the article.

Table VII

	Example 4	Example 5	Example 8
Major Phase	Willemite	Willemite	Willemite
Intermediate Phase	Gahnite	-	Cordierite
Minor Phase	$\text{MgAl}_2\text{Si}_3\text{O}_{10}$	-	-
Trace	$\alpha\text{-Al}_2\text{O}_3$	$\text{Mg}_2\text{B}_2\text{O}_5$	$\alpha\text{-Al}_2\text{O}_3$

A comparison of the property values set out in Table IV and V clearly illustrates the rather broad ranges that are possible, most notably with respect to the linear coefficients of thermal expansion exhibited. These variations result from differences in composition and/or heat treatment which lead to different phase assemblages; e.g., the development of cordierite or gahnite crystals in addition to willemite. Hence, the generation of gahnite crystals strongly raises the overall linear coefficient of thermal expansion of the products; contrariwise, the presence of cordierite can reduce the expansion. Accordingly, by careful control of composition and heat treatment, the linear coefficient of thermal expansion can be tailored to be compatible with rather broad spectrum of materials.

Claims

1. A glass-ceramic body exhibiting a dielectric constant less than 6 and containing willemite as the predominant crystal phase and cordierite as a secondary crystal phase, said body having a composition essentially free from Li_2O , Na_2O , and K_2O and consisting essentially, expressed in terms of weight percent on the oxide basis, of 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 and 3-15% MgO .
2. A glass-ceramic body as claimed in claim 1 also containing a nucleating agent selected from the group consisting of 8-12% ZrO_2 and 0.001-0.05% of a noble metal selected from the group consisting of Au, Pd, and Pt.
3. A glass-ceramic body as claimed in claim 1 or claim 2 also containing up to 15% total of at least one metal oxide in the indicated proportion selected from the group consisting of up to 5% B_2O_3 , up to 5% CaO and/or SrO and/or BaO and/or PbO , up to 7% Cs_2O , and up to 15% MnO .
4. The use of a thermally crystallizable glass, said glass being essentially free from Li_2O , Na_2O , and K_2O and consisting essentially, expressed in terms of weight percent on the oxide basis, of 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 and 3-15% MgO for the production of a glass-ceramic body as claimed in claim 1 by sintering at a temperature within the range of 875-1000°C.
5. The use as claimed in claim 4, for the production of a glass-ceramic body as claimed in claim 2 characterized in that the thermally crystallizable glass also contains a nucleating agent selected from the group consisting of 8-12% ZrO_2 and 0.001-0.05% of a noble metal selected from the group consisting of Au, Pd, and Pt.
6. The use as claimed in claim 4 or claim 5, for the production of a glass-ceramic body as claimed in claim 3 characterized in that the thermally crystallizable glass also contains up to 15% total of at least one metal oxide in the indicated proportion selected from the group consisting of up to 5% B_2O_3 , up to 5% CaO and/or SrO and/or BaO and/or PbO , up to 7% Cs_2O and up to 15% MnO .
7. A substrate for integrated circuit packaging consisting of a glass-ceramic material exhibiting a dielectric constant less than 6 and containing willemite as the predominant crystal phase and cordierite as a secondary crystal phase, said glass-ceramic material having a composition essentially free from Li_2O , Na_2O , and K_2O and consisting essentially, expressed in terms of weight percent on the oxide basis, of 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 and 3-15% MgO .
8. A substrate as claimed in claim 7 characterized in that said glass-ceramic also contains a nucleating agent selected from the group consisting of 8-12% ZrO_2 and 0.001-0.05% of a noble metal selected from the group consisting of Au, Pd, and Pt.

9. A substrate as claimed in claim 7 or claim 8 characterized in that the composition of said glass-ceramic also contains up to 15% total of at least one metal oxide in the indicated proportion consisting of up to 5% B_2O_3 , up to 5% CaO and/or SrO and/or BaO and/or PbO, up to 7% Cs_2O and up to 15% MnO.

5 Revendications

1. Un corps vitrocéramique présentant une constante diélectrique inférieure à 6 et contenant de la willémitte comme phase cristalline prédominante et de la cordiérite comme phase cristalline secondaire, ledit corps ayant une composition essentiellement exempte de Li_2O , Na_2O et K_2O et étant constitué essentiellement, comme exprimé en pour cent en poids sur la base des oxydes, de 15 à 45 % de ZnO, 10 à 30 % de Al_2O_3 , 30 à 55 % de SiO_2 et 3 à 15 % de MgO.
2. Un corps vitrocéramique tel que revendiqué dans la revendication 1, contenant également un agent de nucléation choisi dans le groupe formé par 8 à 12 % de ZrO_2 et 0,001 à 0,05 % d'un métal noble choisi dans le groupe formé par Au, Pd et Pt.
3. Un corps vitrocéramique tel que revendiqué dans la revendication 1 ou la revendication 2, contenant également jusqu'à 15 % au total d'au moins un oxyde de métal, dans la proportion indiquée, choisi dans le groupe formé par jusqu'à 5 % de B_2O_3 , jusqu'à 5 % de CaO et/ou SrO et/ou BaO et/ou PbO, jusqu'à 7 % de Cs_2O et jusqu'à 15 %M de MnO.
4. L'utilisation d'un verre thermiquement cristallisable, ledit verre étant essentiellement exempt de Li_2O , Na_2O et K_2O et étant constitué essentiellement, comme exprimé en pour cent en poids sur la base des oxydes, de 15 à 45 % de ZnO, 10 à 30 % de Al_2O_3 , 30 à 55 % de SiO_2 et 3 à 15 % de MgO, pour la production d'un corps vitrocéramique tel que revendiqué dans la revendication 1 par frittage à une température comprise dans l'intervalle de 875 à 1000 °C.
5. L'utilisation telle que revendiquée dans la revendication 4, pour la production d'un corps vitrocéramique tel que revendiqué dans la revendication 2, caractérisée en ce que le verre thermiquement cristallisable contient également un agent de nucléation choisi dans le groupe formé par 8 à 12 % de ZrO_2 et 0,001 à 0,05 % d'un métal noble choisi dans le groupe formé par Au, Pd et Pt.
6. L'utilisation telle que revendiquée dans la revendication 4 ou la revendication 5, pour la production d'un corps vitrocéramique tel que revendiqué dans la revendication 3, caractérisée en ce que le verre thermiquement cristallisable contient également jusqu'à 15 % au total d'au moins un oxyde de métal, dans la proportion indiquée, choisi dans le groupe formé par jusqu'à 5 % de B_2O_3 , jusqu'à 5 % de CaO et/ou SrO et/ou BaO et/ou PbO, jusqu'à 7 % de Cs_2O et jusqu'à 15 % de MnO.
7. Un substrat pour la mise en boîtier de circuit intégré, constitué d'un matériau vitrocéramique présentant une constante diélectrique inférieure à 6 et contenant de la willémitte comme phase cristalline prédominante et de la cordiérite comme phase cristalline secondaire, ledit matériau vitrocéramique ayant une composition essentiellement exempte de Li_2O , Na_2O et K_2O et étant constitué essentiellement, comme exprimé en pour cent en poids sur la base des oxydes, de 15 à 45 % de ZnO, 10 à 30 % de Al_2O_3 , 30 à 55 % de SiO_2 et 3 à 15 % de MgO.
8. Un substrat tel que revendiqué dans la revendication 7, caractérisé en ce que ledit matériau vitrocéramique contient également un agent de nucléation choisi dans le groupe formé par 8 à 12 % de ZrO_2 et 0,001 à 0,05 % d'un métal noble choisi dans le groupe formé par Au, Pd et Pt.
9. Un substrat tel que revendiqué dans la revendication 7 ou la revendication 8, caractérisé en ce que la composition dudit matériau vitrocéramique contient également jusqu'à 15 % au total d'au moins un oxyde de métal, dans la proportion indiquée, consistant en jusqu'à 5 % de B_2O_3 , jusqu'à 5 % de CaO et/ou SrO et/ou BaO et/ou PbO, jusqu'à 7 % de Cs_2O et jusqu'à 15 % de MnO.

55 Patentansprüche

1. Glaskeramischer Körper mit einer Dielektrizitätskonstante von weniger als 6 und enthaltend Willemite als vorherrschende Kristallphase und Cordierit als zweite Kristallphase mit einer Zusammensetzung, die im

wesentlichen frei ist von Li_2O , Na_2O und K_2O und im wesentlichen - ausgedrückt in Gewichtsprozent auf Oxidbasis - besteht aus 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 und 3-15% MgO .

2. Glaskeramischer Körper nach Anspruch 1 auch enthaltend einen Keimbildner, ausgewählt aus der Gruppe bestehend aus 8-12% ZrO_2 und 0.001-0.05% eines Edelmetalls, ausgewählt aus der Gruppe bestehend aus Au, Pd und Pt.
3. Glaskeramischer Körper nach Anspruch 1 oder 2, auch enthaltend bis zu 15% total wenigstens eines Metalloxids in dem angegebenen Verhältnis, ausgewählt aus der Gruppe bestehend aus bis zu 5% B_2O_3 , bis zu 5% CaO und/oder SrO und/oder BaO und/oder PbO , bis zu 7% Cs_2O und bis zu 15% MnO .
4. Verwendung eines thermisch kristallisierbaren Glases, das im wesentlichen frei ist von Li_2O , Na_2O und K_2O und im wesentlichen - ausgedrückt in Gewichtsprozent auf Oxidbasis - besteht aus 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 und 3-15% MgO zur Herstellung eines glaskeramischen Körpers gemäß Anspruch 1 durch Sintern bei einer Temperatur innerhalb des Bereichs von 875-1000 °C.
5. Verwendung nach Anspruch 4 für die Herstellung eines glaskeramischen Körpers gemäß Anspruch 2, dadurch gekennzeichnet, daß das thermisch kristallisierbare Glas auch einen Keimbildner enthält, ausgewählt aus der Gruppe bestehend aus 8-12% ZrO_2 und 0,001-0,05% eines Edelmetalls, ausgewählt aus der Gruppe bestehend aus Au, Pd und Pt.
6. Verwendung nach Anspruch 4 oder 5 für die Herstellung eines glaskeramischen Körpers gemäß Anspruch 3, dadurch gekennzeichnet, daß das thermisch kristallisierbare Glas auch bis zu 15% total wenigstens eines Metalloxids in dem angegebenen Verhältnis enthält, ausgewählt aus der Gruppe bestehend aus bis zu 5% B_2O_3 , bis zu 5% CaO und/oder SrO und/oder BaO und/oder PbO , bis zu 7% Cs_2O und bis zu 15% MnO .
7. Substrat für ein Einbettmaterial für integrierte Schaltungen, bestehend aus einem glaskeramischen Material mit einer Dielektrizitätskonstante von weniger als 6 und enthaltend Willemitt als vorherrschende Kristallphase und Cordierit als zweite Kristallphase, wobei das glaskeramische Material eine Zusammensetzung besitzt, die im wesentlichen frei ist von Li_2O , Na_2O und K_2O und im wesentlichen - ausgedrückt in Gewichtsprozent auf Oxidbasis - besteht aus 15-45% ZnO , 10-30% Al_2O_3 , 30-55% SiO_2 und 3-15% MgO .
8. Substrat nach Anspruch 7, dadurch gekennzeichnet, daß die Glaskeramik auch einen Keimbildner enthält, ausgewählt aus der Gruppe bestehend aus 8-12% ZrO_2 und 0,001-0,05% eines Edelmetalls, ausgewählt aus der Gruppe bestehend aus Au, Pd und Pt.
9. Substrat nach Anspruch 7 oder 8, dadurch gekennzeichnet, daß die Zusammensetzung der Glaskeramik auch bis zu 15% total wenigstens eines Metalloxids in dem angegebenen Verhältnis enthält, bestehend aus bis zu 5% B_2O_3 , bis zu 5% CaO und/oder SrO und/oder BaO und /oder PbO , bis zu 7% Cs_2O und bis zu 15% MnO .

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