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Huibers et al.

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(54) **LIGHT COMBINER**

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G02B 27/10 (2006.01)
G02B 27/28 (2006.01)

(52) **U.S. Cl.** **359/618**; 359/490; 359/634

(58) **Field of Classification Search** 359/490,
359/618, 634

See application file for complete search history.

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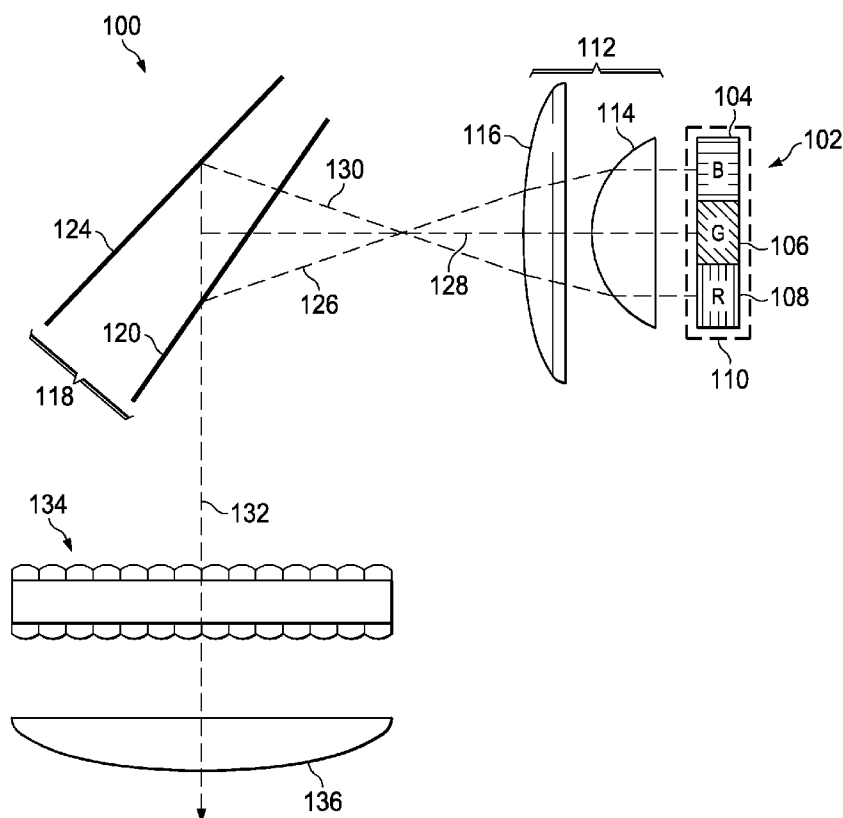
Primary Examiner — James Greece

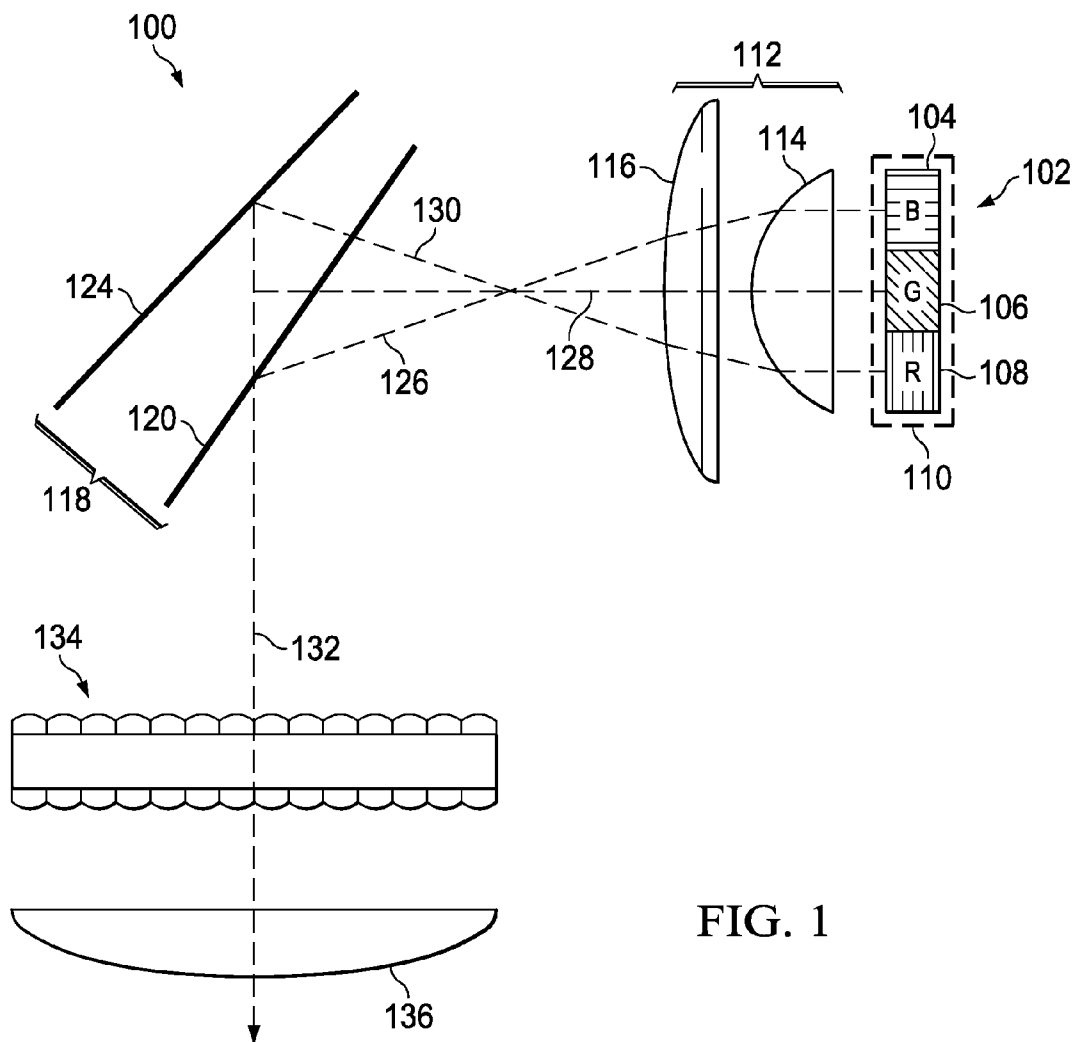
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Brady, III; Frederick J. Telecky, Jr.

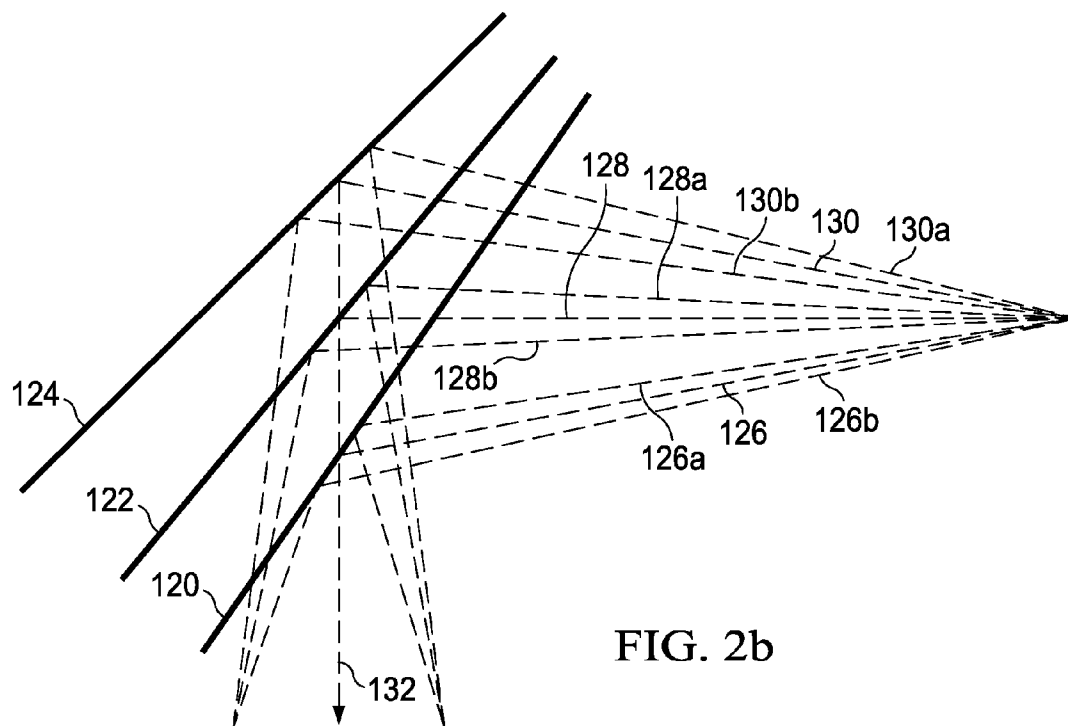
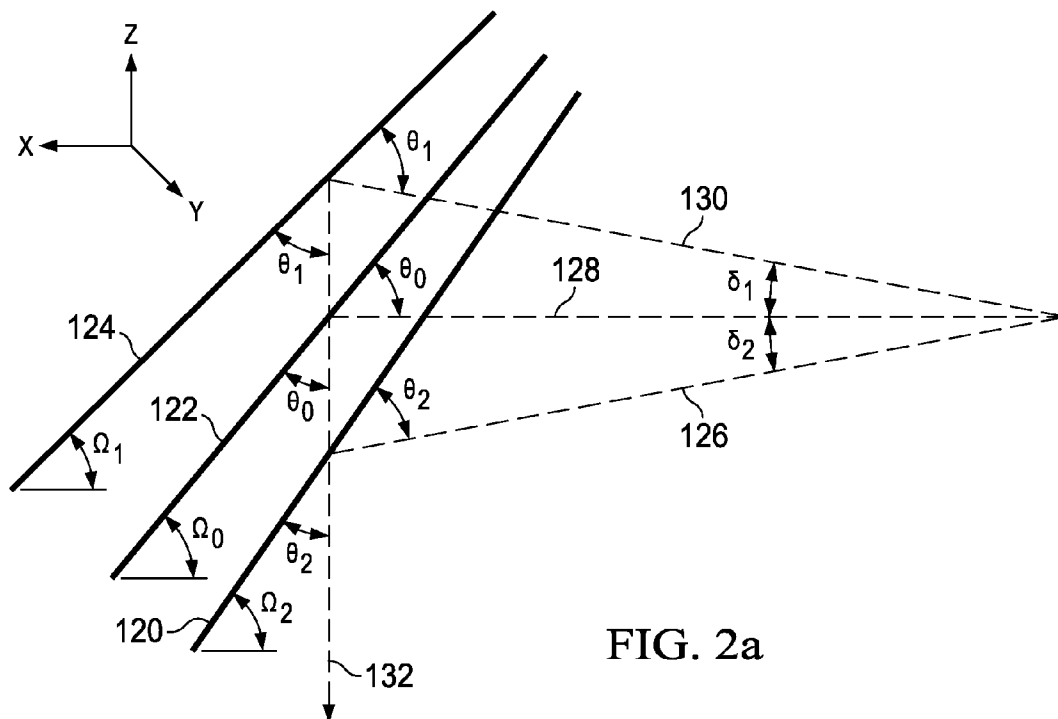
(57) **ABSTRACT**

For combining light from different light sources in a light
source, dichroic filters are displaced individually according to
the physical arrangement of the light sources such that the
reflected light from the dichroic filters is coincident in angle
and space.

6 Claims, 15 Drawing Sheets







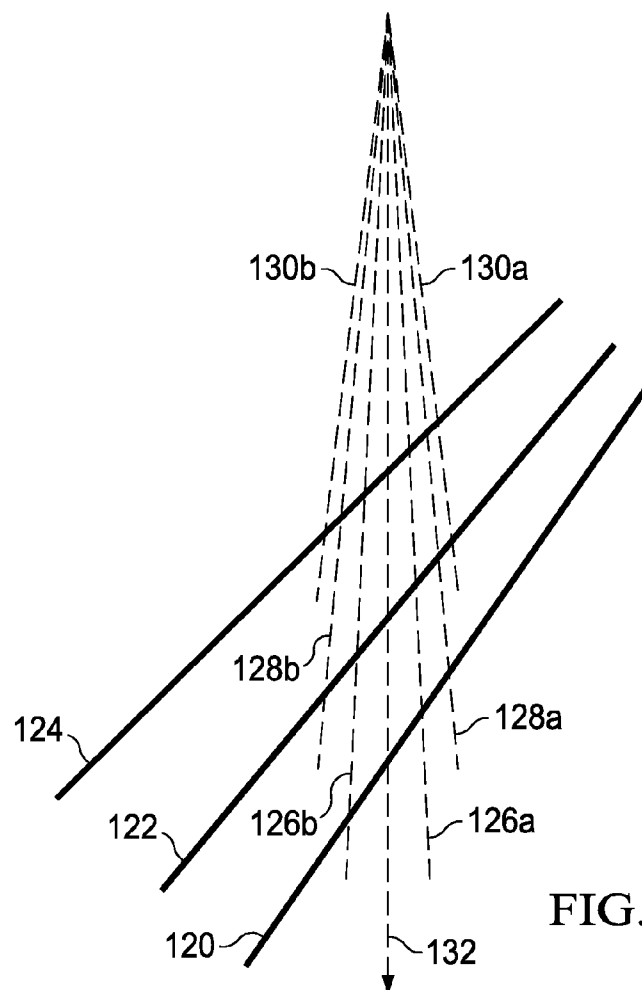


FIG. 2c

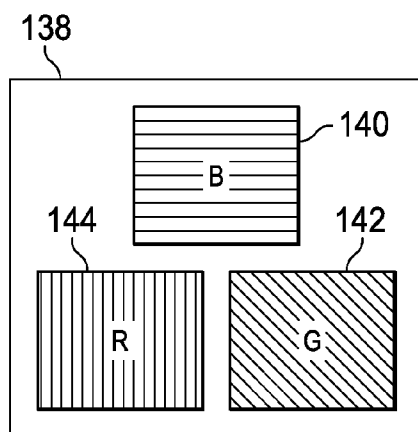


FIG. 3

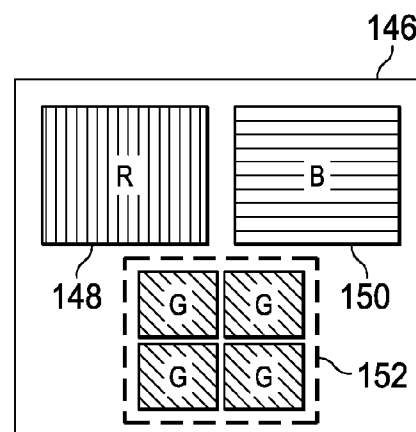


FIG. 4

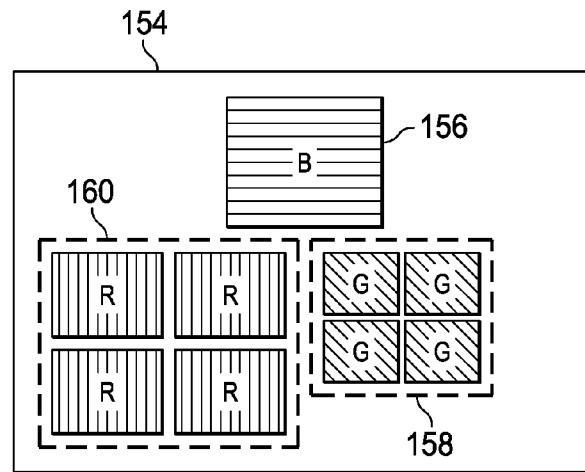


FIG. 5

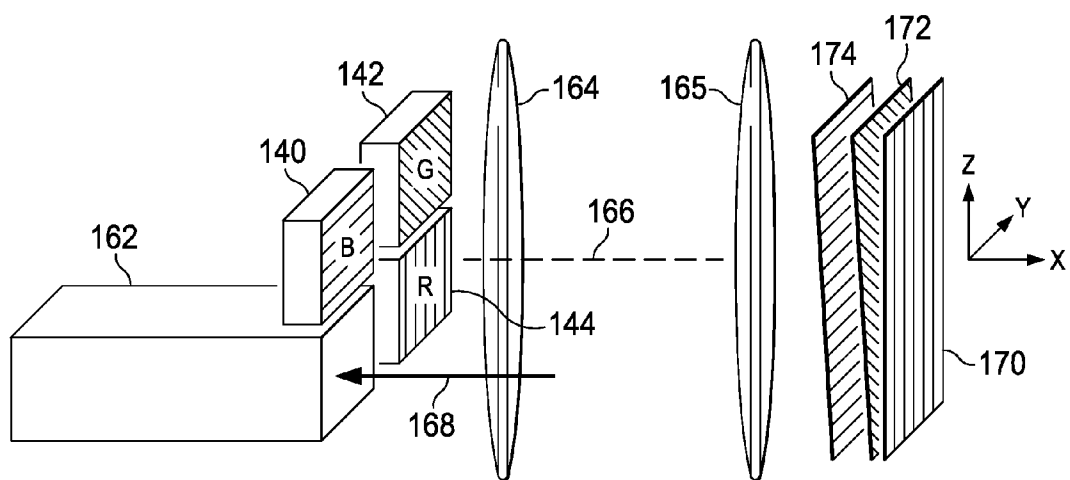


FIG. 6

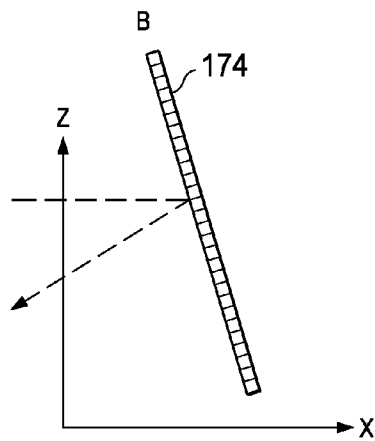


FIG. 7

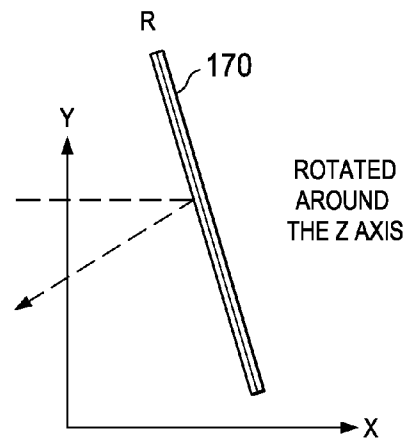


FIG. 8

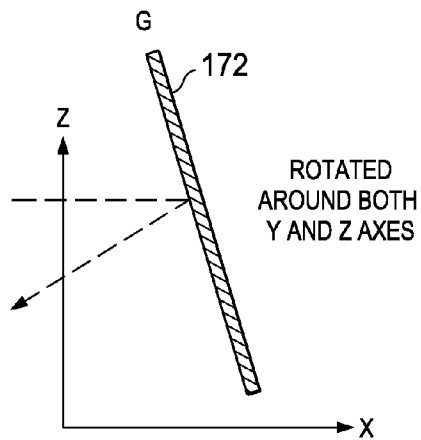


FIG. 9a

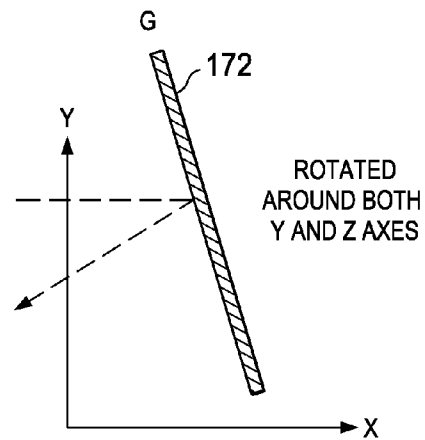


FIG. 9b

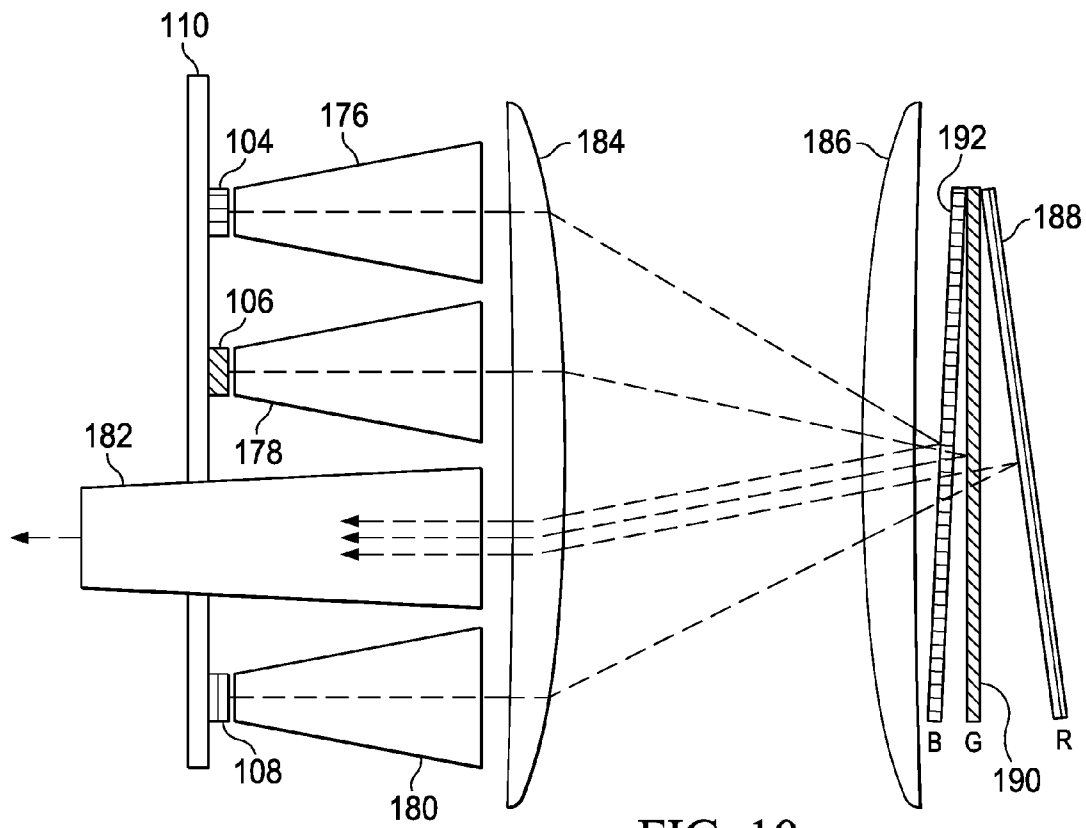


FIG. 10

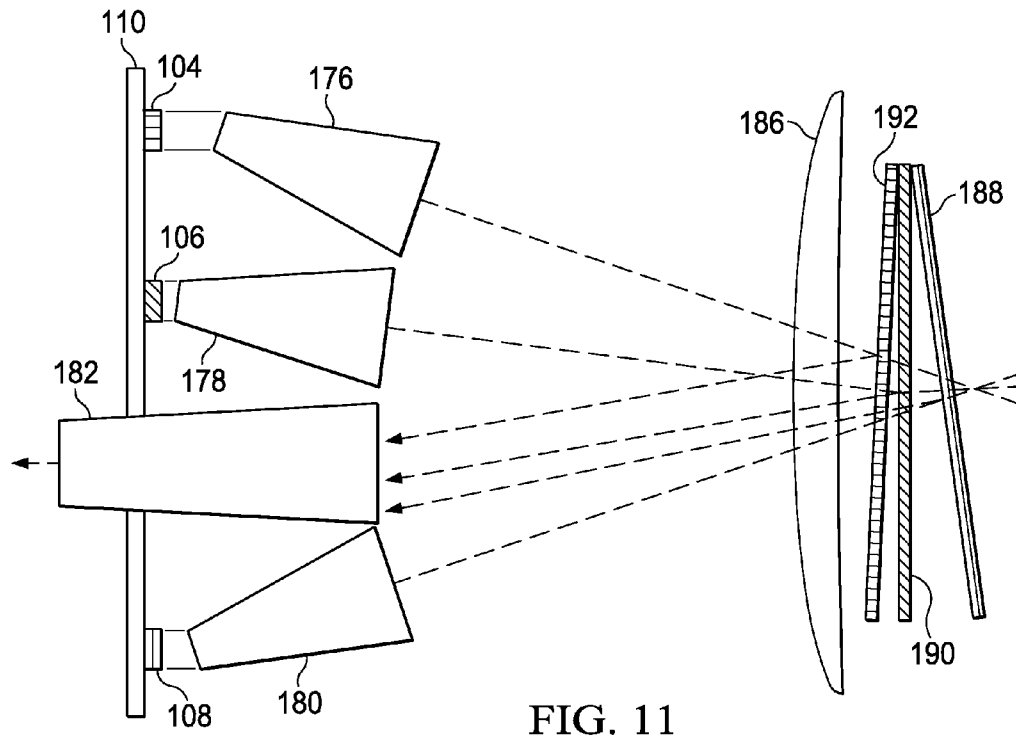


FIG. 11

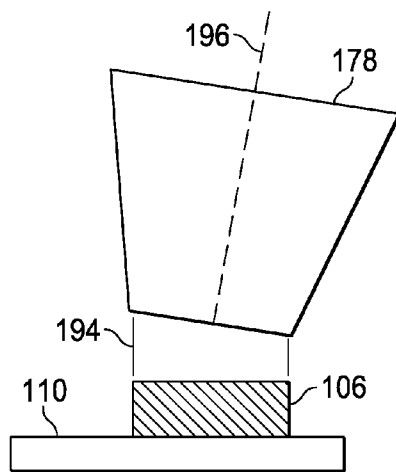


FIG. 12

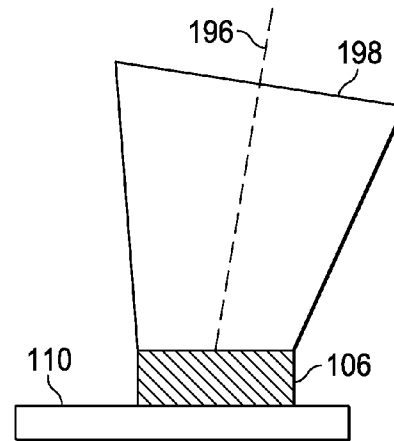
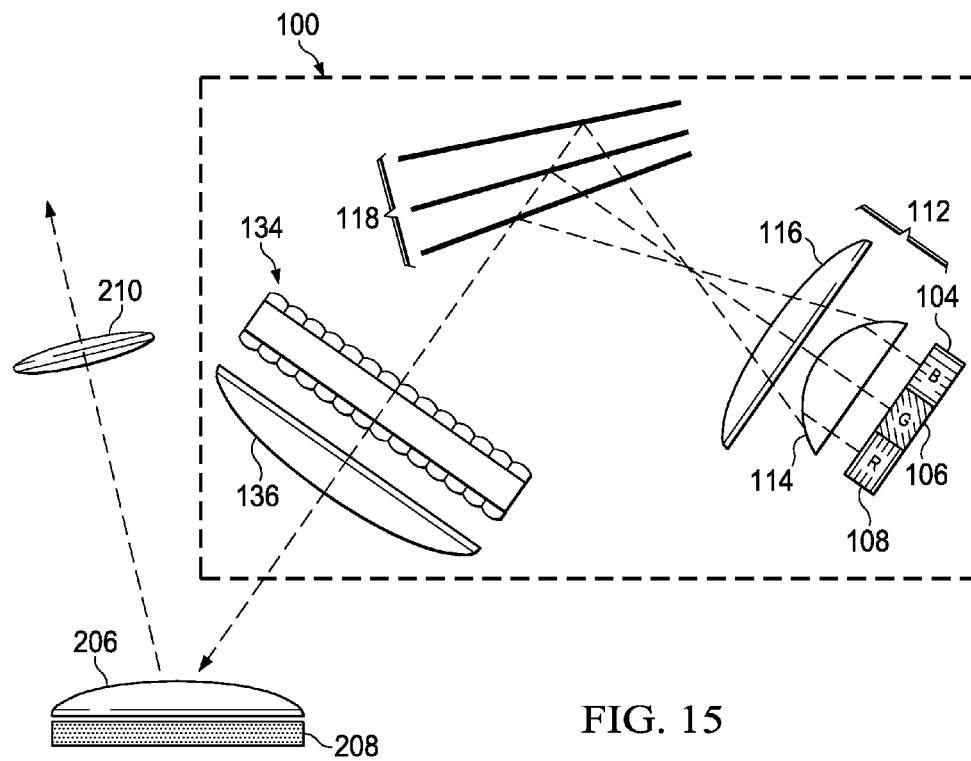
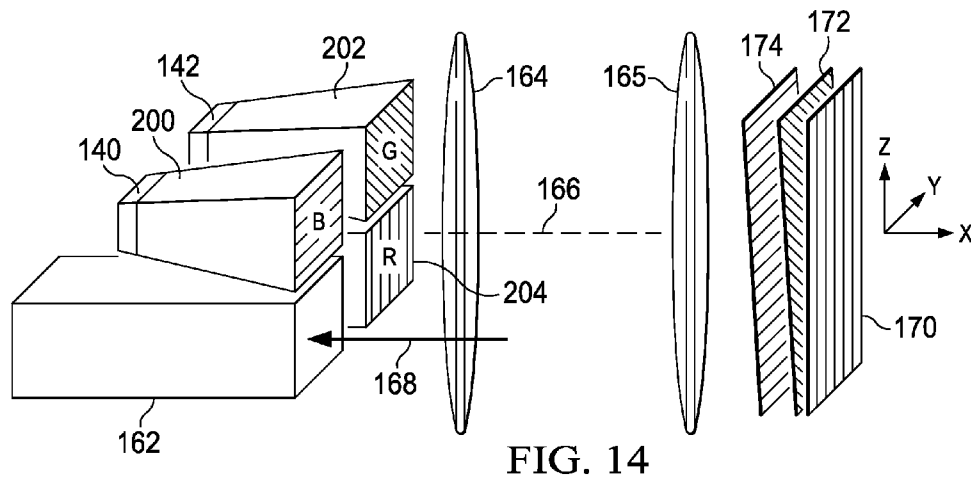


FIG. 13



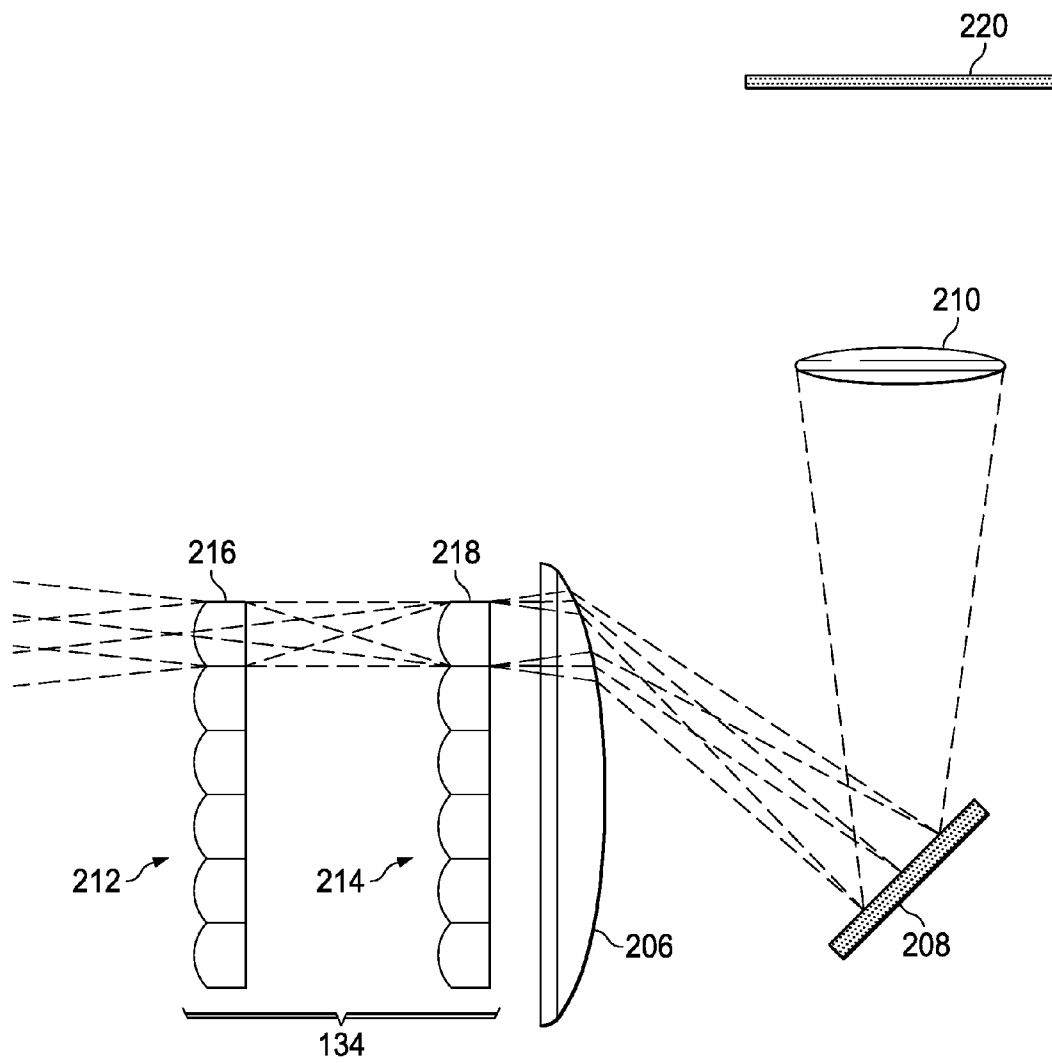


FIG. 16

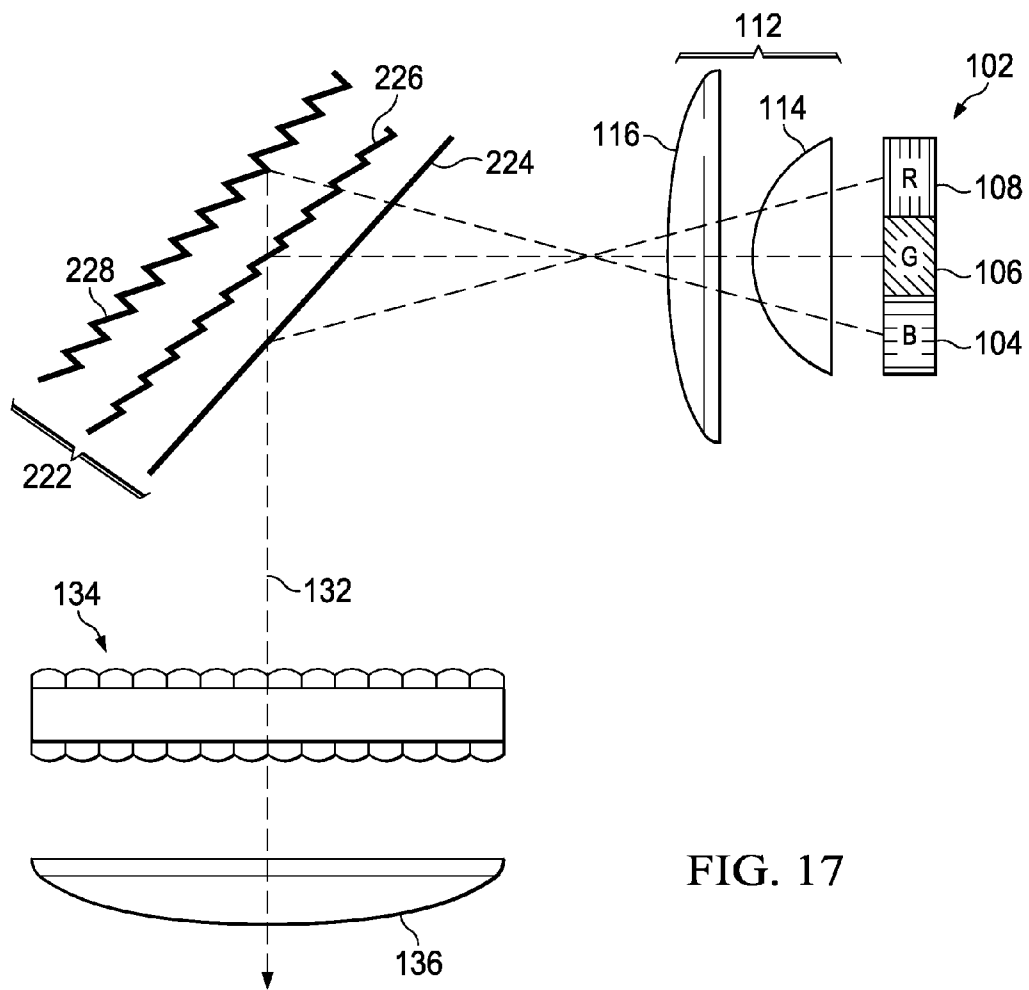


FIG. 17

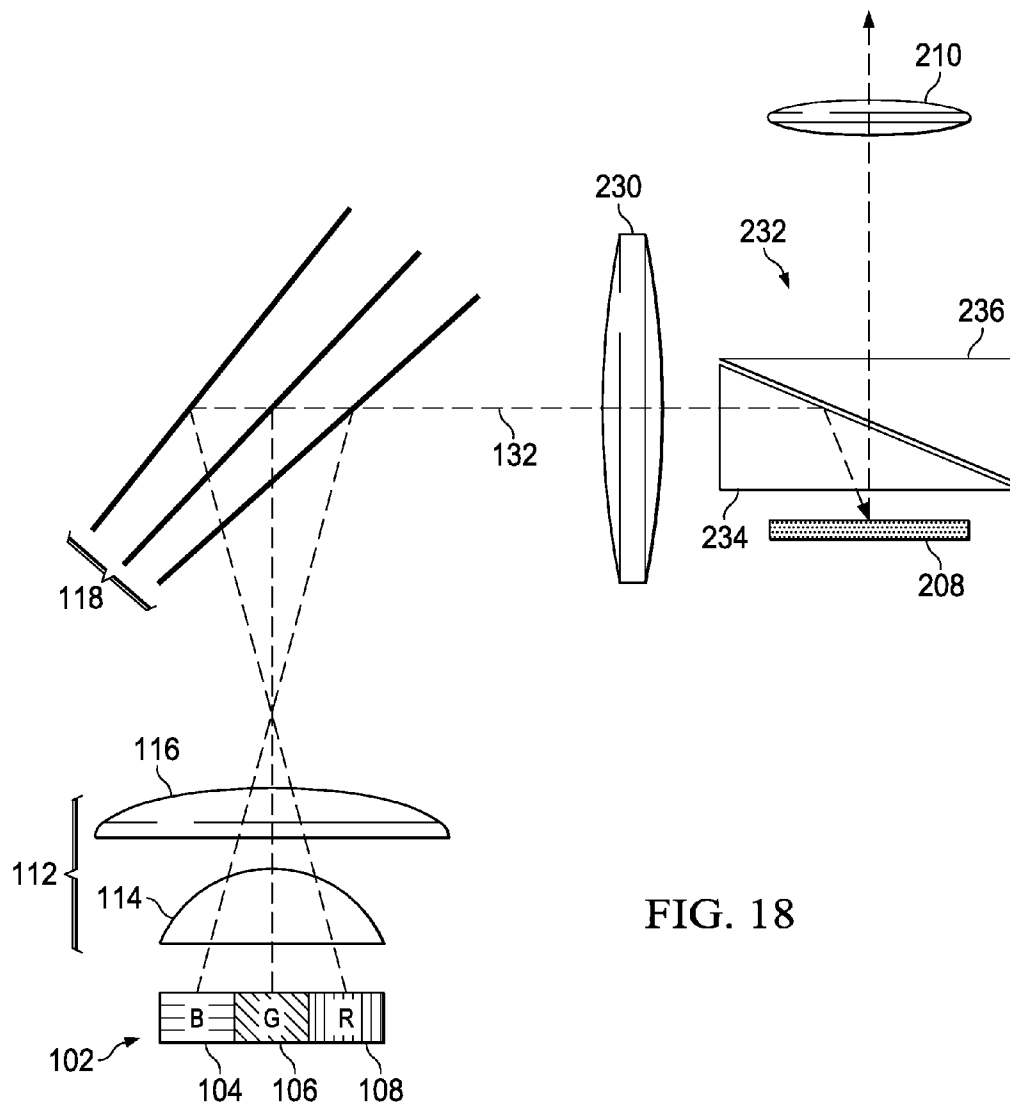


FIG. 18

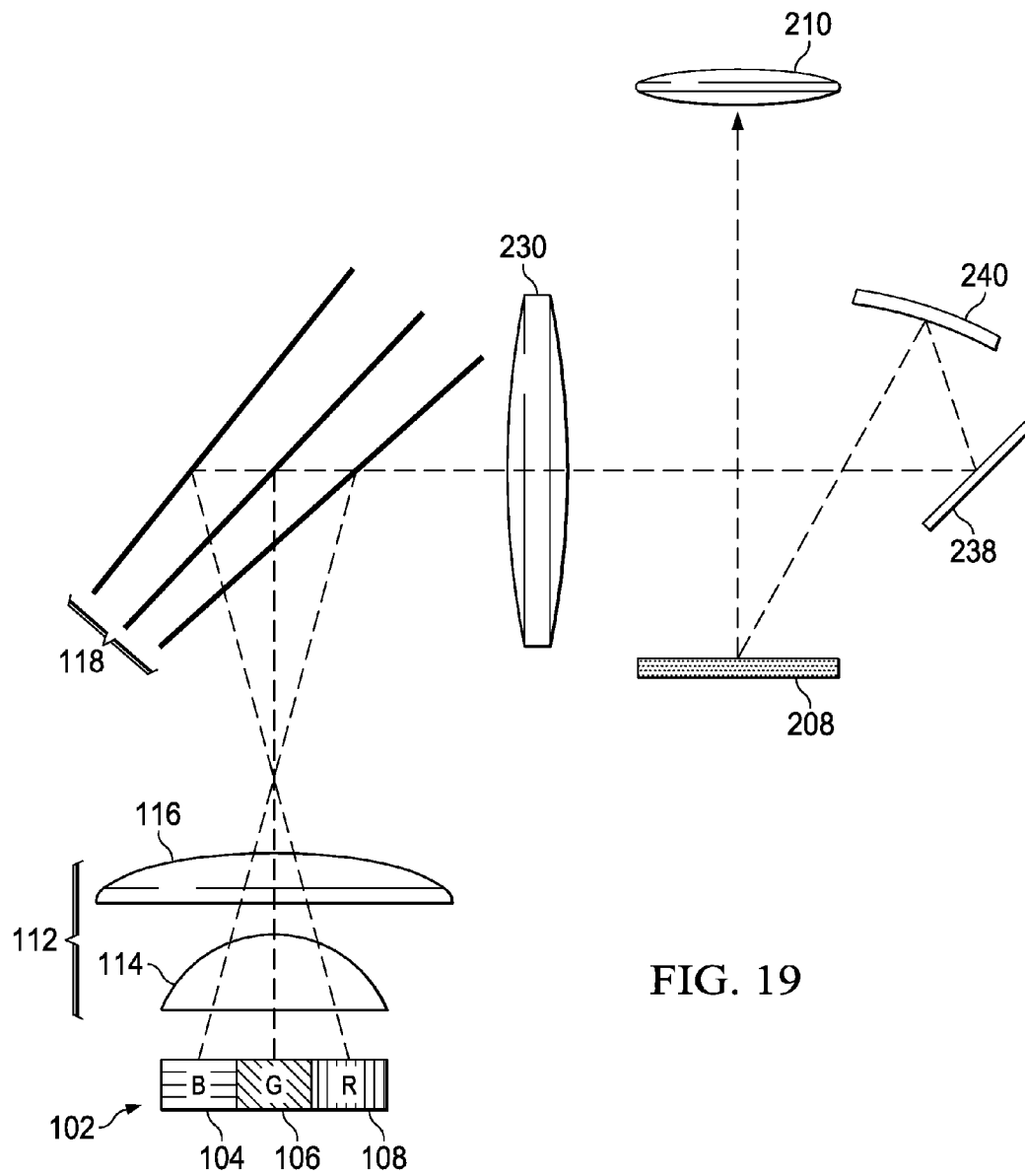


FIG. 19

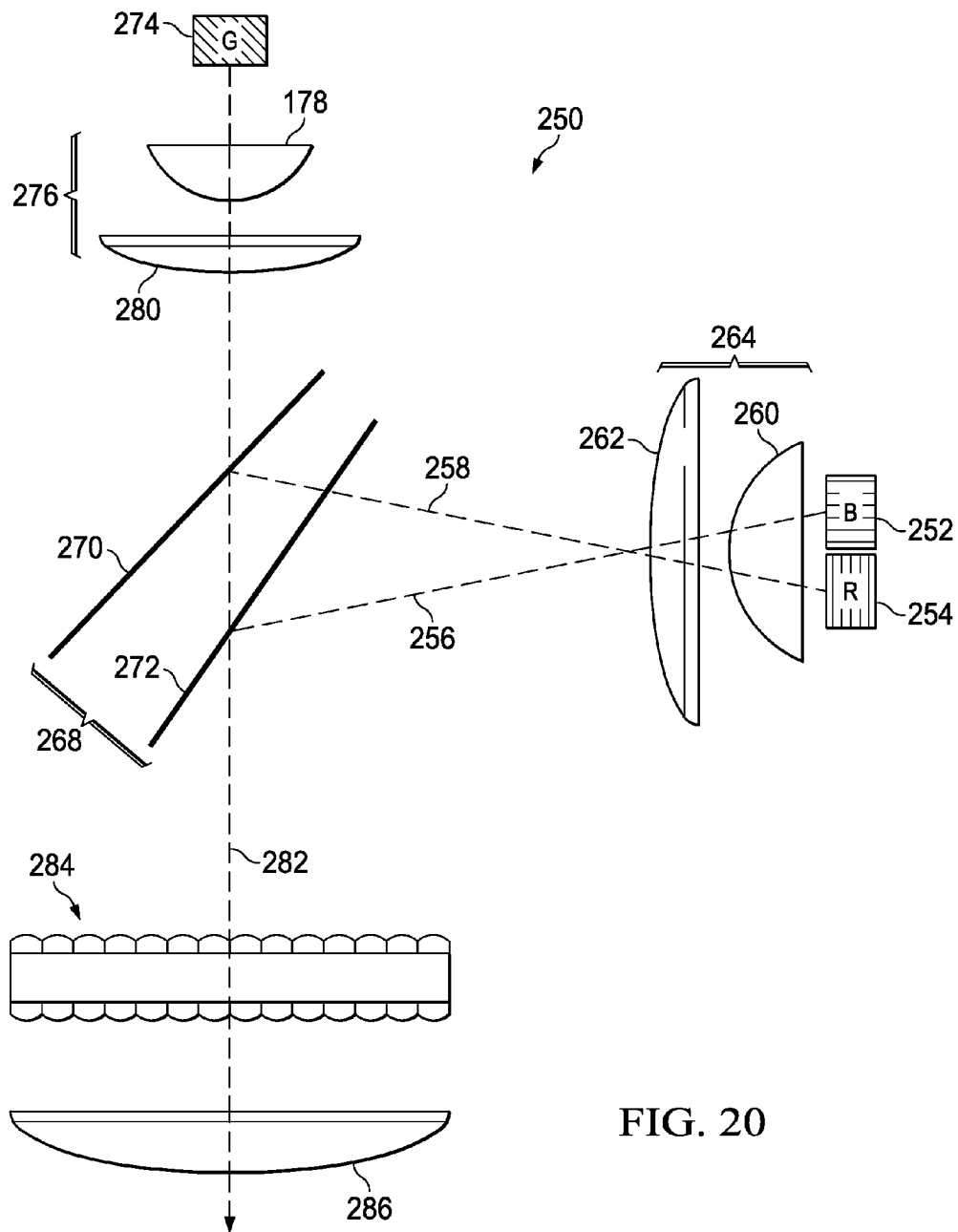


FIG. 20

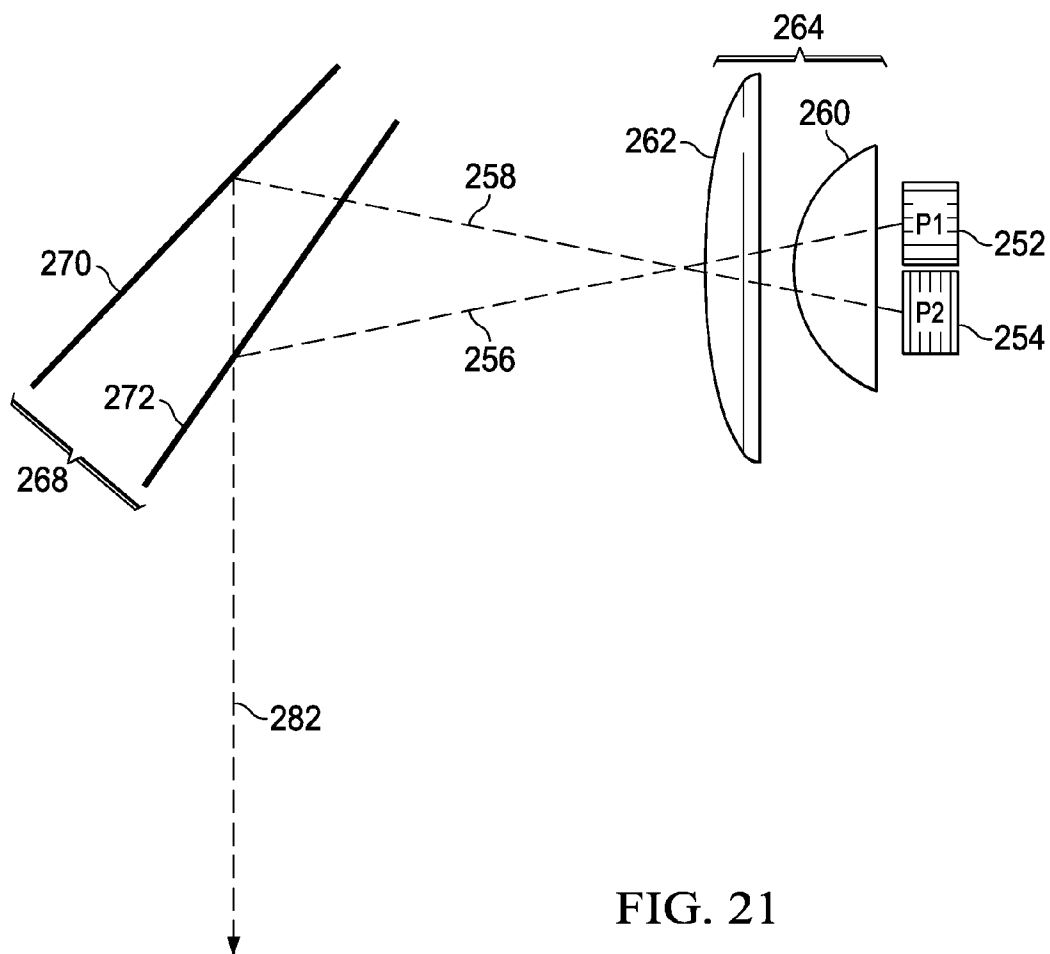
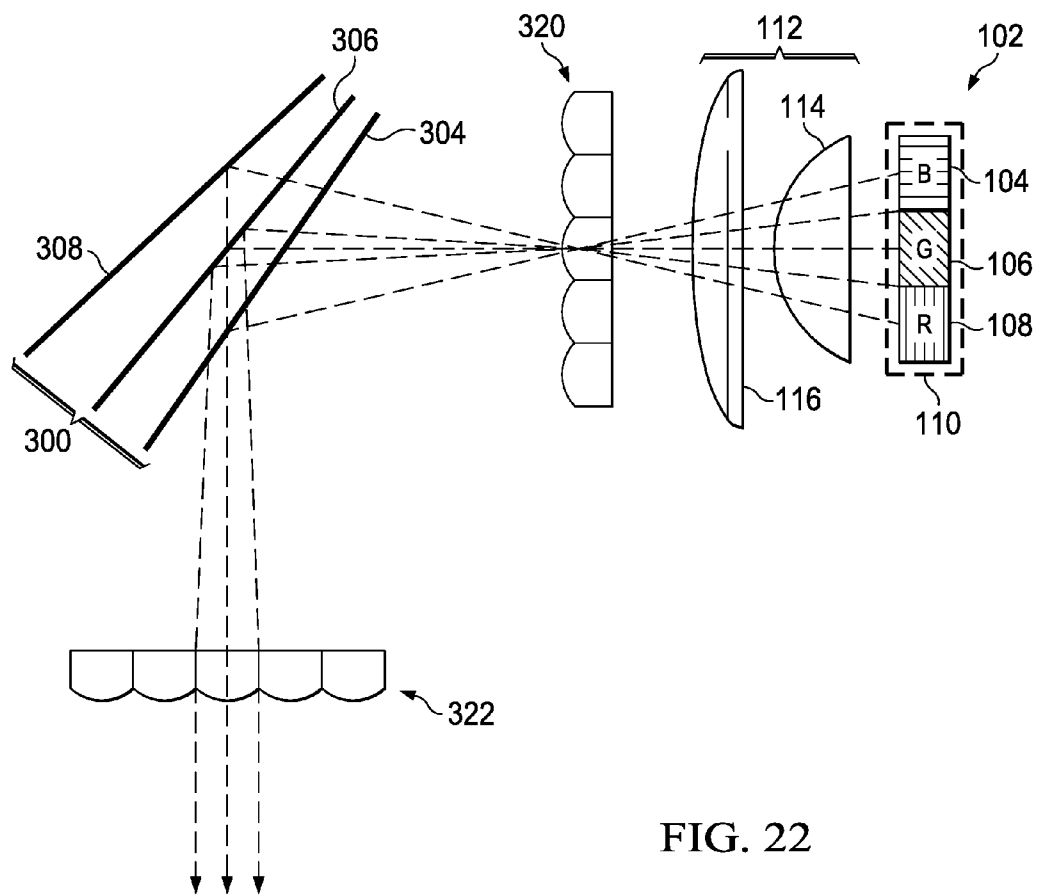


FIG. 21



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LIGHT COMBINER

TECHNICAL FIELD OF THE DISCLOSURE

The technical field of this disclosure relates to the art of optical devices; and more particularly to the art of optical systems for directing illumination light to light valves in imaging systems.

BACKGROUND OF THE DISCLOSURE

In recent years, solid-state light sources and other narrow-wavelength-band and/or polarized light sources capable of producing visible light have drawn significant attention as alternative light sources to traditional light sources for use in imaging systems (such as projection systems) due to many advantages, such as compact size, greater durability, longer operating life, and lower power consumption. For example, solid state sources such as LASERs, light-emitting-diodes (LEDs), and pumped non-linear optical crystals are increasingly used in imaging systems, especially imaging systems that employ one or more light valves each of which comprises an array of individually addressable pixels.

Despite their recognized superior properties over traditional light sources, solid-state light sources can be difficult to optically couple with light valves in imaging systems for illuminating light valves. For example, it is difficult to generate a far-field illumination area with uniform illumination intensity at a light valve location using solid-state or narrow-band light sources. This arises from a fact that the illumination light from the solid-state sources can be distributed over a large solid angle, up to a full hemisphere.

In color imaging applications using solid-state sources (or other narrow-band sources), light sources comprising one or more solid state sources emitting light of different colors or spectral profiles are provided to illuminate light valves. It is desired that the light of different colors illuminates a light valve along substantially the same optical path, for instance, with substantially the same incident angle to the pixels of the light valve. It is desirable that the multiple beams, such as colored beams, overlap to occupy the same angular and spatial optical phase space.

Because a single light source may have limited output power, which may not be sufficient to generate images with satisfactory brightness, multiple light sources for the same color light (with the same wavelength or different wavelengths, and with the same or different electromagnetic polarization state) can be employed in an imaging system. Regardless of different spatial arrangements, the light beams from separate light sources are spatially separated when exiting from the light sources. Without proper management, the spatially separated light beams may result in distorted illumination field, as well as other unwanted optical effects at the light valve, such as poor image uniformity and reduced system brightness.

Therefore, what is desired is an optical system that is capable of directing light from light sources to one or more light valves in imaging systems.

SUMMARY

In view of the foregoing, disclosed herein is an optical system that comprises at least one optical filter, such as a dichroic filter (e.g. a thin film interference filter), and a reflective surface. In imaging systems employing one or more light valves, additional optical elements can be used for directing light from light sources to the light valves.

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In one example, an optical system is provided herein, comprising: a light source comprising first and second light sources; and first and second dichroic filters that are substantially-flat and non-parallel for directing light from the light source arrays.

In another example, a method is disclosed herein, comprising: providing light from first and second light sources; reflecting the light from the first light source by a dichroic filter that passes the light from the second light source; and reflecting the light from the second light source by a reflective surface, wherein the reflective surface has an angle to the dichroic filter with the angle being determined based upon an arrangement of the first and second light sources.

In yet another example, a method is disclosed herein, comprising: providing light from first and second light sources each comprising a principal optical axis, wherein the principal optical axes of the first and second light sources are not coincident; reflecting the light from the first light source towards a desired optical direction by a dichroic filter that passes the light from the second light source; and reflecting the light from the second light source by a reflective surface such that the reflected light from said reflective surface is substantially along the same optical path as the light reflected from said dichroic filter.

In yet another example, an optical system is disclosed herein, comprising: a light source comprising first, second, and third light sources that are arranged in a two-dimensional array; and a filter group comprising first and second dichroic filters and a reflective surface for directing the light from the first, second, and third light source towards a light valve.

In yet another example, an imaging system is disclosed herein. The system comprises: an optical system that comprises: a light source comprising first and second light sources; and first and second optical filters that are non-parallel for directing light from the light sources; and a light valve for modulating the light from the optical system, wherein the light valve comprises an array of individually addressable pixels, and wherein the optical filter could be a dichroic filter, a wire grid polarizer, or a mirror.

In yet another example, an imaging system is disclosed herein. The system comprises: an optical system that comprises a light source comprising first, second, and third light sources that are arranged in a two-dimensional array; and a filter group comprising first and second dichroic filters and a reflective surface for directing the light from the first, second, and third light source towards a light valve; and a light valve for modulating the light from the optical system, wherein the light valve comprises an array of individually addressable pixels.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a diagram of an exemplary optical system for combining light from multiple light sources in an imaging system using a set of dichroic filters;

FIG. 2a is a diagram showing the angular relationships of the dichroic filters, the light incident thereto, and the light departing therefrom in the optical system of FIG. 1;

FIG. 2b and FIG. 2c are diagrams showing the spatial and angular coincidence of the light exit from the dichroic filters in the optical system of FIG. 1;

FIG. 3 schematically illustrates an exemplary arrangement of multiple light sources arranged in a two dimensional array;

FIG. 4 schematically illustrates another exemplary arrangement of multiple light sources arranged in a two dimensional array;

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FIG. 5 schematically illustrates yet another exemplary arrangement of multiple light sources arranged in a two dimensional array;

FIG. 6 is a diagram of another exemplary optical system for directing light from light sources that are arranged in a two dimensional array using a set of dichroic filters;

FIG. 7 schematically illustrates the XZ plane projection of the blue color dichroic filter in the optical system as illustrated in FIG. 6;

FIG. 8 schematically illustrates the XY plane projection of the red color dichroic filter in the optical system as illustrated in FIG. 6;

FIG. 9a schematically illustrates the XZ plane projection of the green color dichroic filter in the optical system as illustrated in FIG. 6;

FIG. 9b schematically illustrates the XY plane projection of the green color dichroic filter in the optical system as illustrated in FIG. 6;

FIG. 10 is a diagram of an exemplary optical system for directing light from light sources using a set of dichroic filters and light guides;

FIG. 11 is a diagram of another exemplary optical system for directing light from light sources using a set of dichroic filters and light guides;

FIG. 12 schematically illustrates an example of coupling a light source to a light guide using an intermediate light guide;

FIG. 13 schematically illustrates another example of coupling a solid-state light source to a light guide;

FIG. 14 is a diagram of another exemplary optical system for directing light from light sources using a set of dichroic filters and light guides, wherein the light sources are arranged in a two-dimensional array;

FIG. 15 schematically illustrates an exemplary imaging system employing the exemplary optical system as illustrated in FIG. 1 and a light valve;

FIG. 16 schematically illustrates an exemplary optical configuration for the fly's eye lens array in the imaging system in FIG. 15;

FIG. 17 schematically illustrates another exemplary optical system for directing light from a set of light sources using a set of dichroic filters, wherein the dichroic filters have saw-tooth structures;

FIG. 18 schematically illustrates another exemplary imaging system employing the exemplary optical system as illustrated in FIG. 1, a prism, and a light valve;

FIG. 19 schematically illustrates yet another exemplary imaging system employing the exemplary optical system as illustrated in FIG. 1 and a light valve; and

FIG. 20 is a diagram of an exemplary optical system for combining light from multiple light sources in an imaging system using a set of dichroic filters;

FIG. 21 is a diagram of an exemplary optical system for combining light from multiple polarized light sources in an imaging system using a set of optical filters; and

FIG. 22 is a diagram of an exemplary optical system for combining light from multiple light sources in an imaging system using a set of dichroic filters positioned between two fly's eye lens arrays.

DETAILED DESCRIPTION OF SELECTED EXAMPLES

Disclosed herein is an optical system that comprises at least one optical filter and a reflective surface for directing light from a group of light sources. A reflective surface here can refer to a surface that reflects light of certain polarization or wavelength, such as a mirror, or a second optical filter such

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as a dichroic filter or reflective polarizer. The reflective surface and the optical filter are typically flat, but they can also be curved or have optical power. In the following, the optical system will be discussed with reference to particular examples. However, it will be appreciated by those skilled in the art that the following discussion is for demonstration purpose, and should not be interpreted as a limitation. Other variations within the scope of this disclosure are also applicable.

Referring to the drawings, FIG. 1 is a diagram showing an exemplary optical system of this disclosure. Optical system 100 in this example comprises light source 102, collimation optics 112, and optical filter group 118.

Light source 102 comprises an array of light sources for providing illumination light of desired colors. In the example as illustrated in FIG. 1, the light source array (102) comprises light sources 104, 106, and 108 for providing blue, green, and red light. By turning on and off the individual light sources at different time intervals, light of an exceedingly wide range of colors can be achieved.

The light sources can comprise solid-state devices such as lasers, LEDs, or other wavelength or polarization limited sources, or any combinations thereof. For example, the light sources can incorporate AlGaInP light emitting diodes, InGaN light emitting diodes, resonant cavity LEDs, LEDs with non-Lambertian emission profiles, LEDs producing polarized light, or other suitable LEDs. Laser light sources can be vertical cavity surface emitting lasers (VCSEL), extended cavity surface emitting lasers (NECSEL) or any other suitable lasers.

When a single light source (such as an LED die) is employed for providing light of a specific color, the light may not have sufficient intensity due to the limited output power of the light source. In this instance, multiple light sources can be arrayed for providing light of the specific color, which will be discussed in detail afterwards with reference to FIG. 3 through FIG. 5.

When the light sources (104, 106, and 108) are light sources comprising solid state devices, especially when the light sources are laser sources and/or LEDs, the light sources can be formed on the same substrate, such as substrate 110, which can be a semiconductor substrate or many other suitable substrates. The light sources can be deployed on the substrate as a one dimensional array as illustrated in FIG. 1, or can be arranged as a two-dimensional array, or any desired arrangement, as will be discussed afterwards with reference to FIG. 3 through FIG. 5.

Different applications using the optical system (100) may desire light of different colors or light of different color combinations. Accordingly, the light source array (102) may comprise any suitable combinations of solid-state light sources or combinations of any suitable light emitting devices.

In addition to solid state light sources, the light source array (102) may comprise other types of light emitting devices. For example, the light source array (102) may comprise a discharge lamp, such as a mercury lamp, a metal halide lamp, a xenon lamp, an organic or electro-luminescent light-emitting film, a phosphor, quantum dots, a non-linear optical element or other types of light emitting devices.

For combining the light from individual light sources, the light from the light sources are directed to optical filter group 118 through collimation optics 112 that comprises lenses 114 and 116 in this example. As schematically illustrated in FIG. 1, dashed line 126, dash-and-dotted line 128, and solid line 130 respectively illustrate the principal optical axes of the

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light from light sources **104**, **106**, and **108**. The collimated light **126**, **128**, and **130** are incident to the dichroic filters in the optical filter group (**118**).

The dichroic filters in the group (**118**) can be selected based upon the number of different colors of the light emitted from the light source array (**102**). In one example, the number of dichroic filters of different color filtering properties in the filter group (**118**) can be equal to the number of different colors of the light from the light source array (**101**). Given that one of the dichroic filters can be replaced by a reflective surface, the total number of dichroic filters of different color filtering properties in the filter group (**114**) can be one less than the total number of different colors of the light from the light source array (**101**). For example, a dichroic filter for the blue color is expected to have a color filtering property such that the dichroic filter is capable of reflecting the blue light and transmitting or passing light of other colors. Light of a specific color is referred to as an electromagnetic wave having a wavelength or a wavelength range that is substantially within the wavelength range of the particular color. For examples, red light is referred to as light having a wavelength within the range of 620 nm to 750 nm. Green light is referred to as light having a wavelength within the range of 495 nm to 570 nm. Blue light is referred to as light having a wavelength within the range of 420 nm to 495 nm. Accordingly, dichroic filters for the red, green, and blue light respectively reflect the light in the red, green, and blue color ranges and pass light of other colors.

In examples wherein non-visible light, such as infrared light, ultraviolet light, or other non-visible light is to be employed, the dichroic filter(s) can be selected according to the specific light. For example, when near-infrared light is employed in the optical system, a dichroic filter capable of reflecting light having a wavelength in the range of 700 nm to 1400 nm can be included in the optical filter group. When near-ultraviolet light is employed in the optical system, a dichroic filter capable of reflecting light having a wavelength in the range of 300 nm to 400 nm can be included in the optical filter group.

Because the light from the light sources are propagating along different paths with different angles relative to, for example, the principal optical axis of the optical system (**100**), the dichroic filters can be arranged according to the physical arrangement of the light sources in the light source array such that substantially all light from the light sources are spatially and angularly coincident after being reflected by the dichroic filters. For demonstration purpose, FIG. 2a illustrates the angular relationships of the dichroic filters and the light from the light sources that are arranged in a one dimensional array as illustrated in FIG. 1.

Referring to FIG. 2a, dashed line **126**, dash-and-dotted line **128**, and solid line **130** are principle optical axes of the light emitted from the light sources **104**, **106**, and **108** (as illustrated in FIG. 1) after collimation optics **112** (as illustrated in FIG. 1). By assuming that the principal optical axis **128** of the light from light source **106** (as illustrated in FIG. 1) is parallel to the X axis of the Cartesian coordinate, principal optical axes **126** and **130** have angles δ_1 and δ_2 to principal axis **128** before the dichroic filters.

Given the incident light angle and the desired propagation path (**132**) of the light departing from the dichroic filters, which can be along any desired direction, the dichroic filters can be individually tilted relative to the corresponding incident light. Specifically, dichroic filter **122** can be tilted an angle of Ω_0 from the X axis such that the light incident thereto has an incident angle θ_0 can be reflected by dichroic filter to propagate along the desired direction **132**.

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In order to reflect the light incident traveling along the principal optical axis **130** toward the desired direction **132**, dichroic filter **124** is tilted an angle of Ω_1 from the X axis such that the light incident thereto has an incident angle θ_1 . The angles of Ω_1 and θ_1 can be determined by equation 1.

$$\begin{aligned}\Omega_1 &= \Omega_0 + \delta_1/2 \\ \theta_1 &= \theta_0 + \delta_1/2\end{aligned}\quad (\text{Equation 1})$$

In order to reflect the light incident traveling along the principal optical axis **126** toward the desired direction **132**, dichroic filter **120** is tilted an angle of Ω_2 from the X axis such that the light incident thereto has an incident angle θ_2 . The angles of Ω_2 and θ_2 can be determined by equation 2.

$$\begin{aligned}\Omega_2 &= \Omega_0 + \delta_1/2 \\ \theta_2 &= \theta_0 - \delta_2/2\end{aligned}\quad (\text{Equation 2})$$

In examples when the light from each light source has angular divergence, the reflected light by the dichroic filters can be both angularly and spatially coincident as schematically illustrated in FIG. 2b and FIG. 2c.

Referring to FIG. 2b, dashed line **126**, dash-and-dotted line **128**, and solid line **130** are principle optical axes as discussed above with reference to FIG. 2a. Dichroic filters **120**, **122**, and **124** are disposed in the same way as that in FIG. 2a. Dashed lines **126a** and **126b** are the edges of the light cone having the principal optical axis **126**. Dash-and-dotted lines **128a** and **128b** are the edges of the light cone having the principal optical axis **128**. Solid lines **130a** and **130b** are the edges of the light cone having the principal optical axis **130**. It is noted that the light from the light sources (**104**, **106**, and **108**) may or may not have the same angular dispersion.

Due to the symmetry of each light cone in this example, i.e. the edges of each light cone are symmetrically located around the principal optical axis of the light cone, the spatial extension of the light cones from different light sources and reflected by different dichroic filters are spatially coincident. Specially, as schematically illustrated in FIG. 2b, the principal optical axes **126**, **128**, and **130** are substantially aligned along the desired direction **132**; and the edges (**126a**, **126b**, **128a**, **128b**, **130a**, and **130b**) of different light cones are substantially symmetrically located around the desired optical direction **132**. The angular coincident of the reflected light cones by the dichroic filters is better illustrated in FIG. 2c.

Referring to FIG. 2c, the reflected light by the dichroic filters is retro-extended to show the angles of the line cones. It can be seen that the angles of the light cones from different light sources are substantially aligned, i.e. with the common central line along the desired optical path **132**.

The arrangement of the light sources in FIG. 1, which is a one dimensional array, is only one of many possible examples. In another example, the light sources can be arranged in a two-dimensional array, as schematically illustrated in FIG. 3. Referring to FIG. 3, the light source array comprises light sources **140**, **142**, and **144**, which are solid state light sources (e.g. lasers, LEDs, or a combination thereof) for providing blue, green, and red colors in this example. In other examples, any desired combinations of light emitting devices for obtaining light of any desired color combinations can be employed. The light sources **10**, **142**, and **14** are arranged in a two-dimensional array; and can be formed on the same substrate, such as substrate **138**. In other examples, the light sources can be formed on separate substrates. It is noted that the light sources in the light source array may or may not have the same physical size.

As discussed above, the light of a specific color can be provided by multiple light sources that are capable of emitting light of substantially the same wavelength. FIG. 4 schematically illustrates such an example. Referring to FIG. 4, the light source array comprises light sources **148** and **150** for providing red and blue colors. The light source array may further comprise a light source sub-array **152** that comprises multiple light sources for providing light of substantially the same color, which is green in this example. The light sources in the light source array can be formed on the same package substrate, such as substrate **146**, or can be formed on separate substrates, which is not shown in the figure. The light sources may or may not have the same physical size. As an example as illustrated in FIG. 4, the light sources for the green color may have a smaller physical dimension than the other two light sources **148** and **150**. The sub-array **152** may have a different physical size as any one of the other two light sources **148** and **150**. In practice, a light source may have any desired number of light source sub-arrays for different purposes. For example, multiple light source sub-arrays can be provided for providing light of red and green (or light of other colors) colors, as schematically illustrated in FIG. 5.

Referring to FIG. 5, the light source array in this example comprises light source **156** for providing the blue light, light source sub-array **160** for providing the red light, and light source sub-array **158** for providing the green light. Each light source sub-array may have any desired numbers of light sources, and the light sources in the same light source sub-array may emit light of substantially the same color. The light source sub-arrays may or may not have the same physical size. All light sources in the light source array may be formed on the same substrate, such as substrate **154**, or can be formed on separate substrates.

In examples wherein the light sources of the light source array are arranged in a two-dimensional array, the dichroic filters in the optical filter group can be tilted along different directions for appropriate angles so as to combine the propagation paths of the reflected light. For demonstration purpose, FIG. 6 schematically illustrates an exemplary optical system for directing light from the light sources that are arranged in a two-dimensional array.

Referring to FIG. 6, light sources **140**, **142**, and **144** are disposed in a two-dimensional array. The light from the light sources are directed to dichroic filters **170**, **172**, and **174** through field lens **164** and imaging optic **165**. In one example, the principal optical axis **166** of the light sources **140**, **142**, and **144** can be parallel to the principal optical axis of the collimation lenses and the dichroic filters. The light from the individual light sources are reflected by the corresponding dichroic filters **170**, **172**, and **174**; and the reflected light is re-imaged at the entrance to optical integrator **162**. The imaging is accomplished with 2 passes through imaging optic **165** and filter **170**, **172** or **174** (depending on the color). The field lens **164** can have a focal length that is roughly the distance between the light sources and the filters and which causes light from the sources to overlap at optic **165** and ensures that the differently color light entering optical integrator **162** has an overlapping angular distribution. Other types of optics can be used to perform the functions of field lens **164** and imaging optic **165** such as multiple lenses, curved reflectors, Fresnel lenses, etc. The tilt angles of the individual dichroic filters **170**, **172**, and **174** relative to the incident light are better illustrated in FIG. 7 through FIG. 9b.

Referring to FIG. 7, a side view of dichroic filter **174** along the Y direction in the Cartesian coordinate that is illustrated in FIG. 6 is schematically illustrated therein. As seen in the XZ plane, dichroic filter **174** is rotated around the Y axis such that

the light from light source **140** (illustrated in FIG. 6) is reflected towards the entrance of the optical integrator (**162** as illustrated in FIG. 6).

Referring again to FIG. 6, for reflecting the light from light source **144**, dichroic filter **170** is rotated around the Z axis for an angle such that the light from light source **144** is reflected towards the entrance of optical integrator **162**, as schematically illustrated in FIG. 8, wherein a side view of dichroic filter around the Z axis of the Cartesian coordinate is schematically illustrated therein.

For reflecting the light from light source **142** by dichroic filter **172**, dichroic filter **172** is rotated around both of the Y and Z axes, as schematically illustrated in FIG. 9a and FIG. 9b. Referring to FIG. 9a, dichroic filter **172** is rotated around the Y axis for an angle such that the reflected light is substantially in the same horizontal plane as the entrance of the optical integrator (**162** as illustrated in FIG. 6). Dichroic filter **172** is further rotated around the Z axis such for an angle such that the reflected light is moved to the entrance of the optical integrator.

When multiple light sources are employed for emitting light of the same color and the light sources are arranged in a two-dimensional array, such as that illustrated in FIG. 4 and FIG. 5, a dichroic filter can be provided for each light source. The dichroic filters can be individually tilted according to the physical arrangements of the light sources so as to cause the principal optical axes of the light sources to be aligned to a substantially common optical path after the dichroic filters. Alternatively, a dichroic filter can be provided for all light sources that emit light of substantially the same color. In this instance, a dichroic filter can be tilted according to all light sources that emit light of substantially the same color. For example with reference to FIG. 5, a dichroic filter for light source sub-array **158** can be tilted for an angle according to the principal axis for substantially all light sources in light source sub-array **158**.

The light from the light sources can be directed to the dichroic filters by collimation lens as discussed above with reference to FIG. 1. Alternatively, optical integrators can be employed with the collimation lens for directing the light from the light sources. In one example, FIG. 10 schematically illustrates an optical system that employs optical integrators and collimation lens for directing light from the light sources arranged in a one-dimensional array as illustrated in FIG. 1 to dichroic filters.

Referring to FIG. 10, light sources **104**, **106**, and **108** are arranged in a one-dimensional array, and can be formed on substrate **110**. Optical integrators **176**, **178**, and **180** are provided and are disposed such that the entrances of the optical integrators are respectively aligned to the light sources **104**, **106**, and **108** for collecting the light from the light sources. The principal axes of the optical integrators are substantially parallel, for example, to the principal optical axis of the optical system. In this example the optical integrators are tapered waveguides and also serve to narrow the angular distribution of the light from the light source. Light exiting from the optical integrators are overlapped and collimated by lenses **184** and **186** as in FIG. 6; and are then directed to the dichroic filters **188**, **190**, and **192**. The dichroic filters **188**, **190**, and **192** reflect the incident light towards the entrance of optical integrator **182** that delivers the reflected light to other devices, such as a light valve of an imaging system.

The dichroic filters **188**, **190**, and **192** and lenses **184**, **186** are placed in a way such that the principal optical axes of the light from light sources **104**, **106**, and **108** can be combined along the desired direction. In particular, angular and spatial extension of the light emitted from the light sources and

reflected by the dichroic filters can be substantially coincident at the entrance of optical integrator **182**.

The optical integrators **176**, **178**, and **180** each can take any desired forms. In the example as illustrated in FIG. **10**, the optical integrators **176**, **178**, and **180** have tapered edges with the narrow entrances being coupled to the light sources and the wider exits being coupled to the collimation lens. Alternatively, a tapered optical integrator can be replaced by an optical integrator with any desired forms. For example, an optical integrator with curved edges can be used. For another example, an optical integrator can be non-tapered. In other examples, any one of the optical integrators can be replaced by or used with other optical devices, such as optical fibers and/or interference-type optical devices (e.g. interference gratings). The optical integrators (**176**, **178**, and **180**) can be formed or derived from a molded material, such as a molded plastic, which can reduce the cost of the optical system.

In another example, the optical integrators (**176**, **178**, and **180**) can be tilted such that the principal optical axes of the optical integrators are converged to substantially a single point, as schematically illustrated in FIG. **11**. In this instance, collimation lens **184** to overlap the light beams may not be necessary.

Referring to FIG. **11**, optical integrators **176**, **178**, and **180** are tilted individually such that the principal optical axes of the optical integrators are converged. The combination of lens **186** and the dichroic filters (**188**, **190**, and **192**) images the exits of the optical integrators (**176**, **178**, and **180**) onto the entrance of optical integrator **182** by which the reflected light from the dichroic filters are collected and delivered, for example to a light valve. Accordingly, the dichroic filters are tilted individually according to the directions of the principal optical axes of the optical integrators **176**, **178**, and **180**. As a consequence, the reflected light from the dichroic filters can be angularly and spatially coincident, for example, in a way as discussed above with reference to FIG. **2a** through FIG. **2c**.

The optical integrators (**176**, **178**, and **180**) can be coupled to the light sources in many ways, one of which is schematically illustrated in FIG. **12**. Referring to FIG. **12**, light source **106** is one substrate **110**. The entrance of optical integrator **178** is coupled to light source **106** through optical integrator **194**. Because the principal optical axis of optical integrator **178** is tilted, the entrance of optical integrator **178** may not be parallel to the plane of light source **106**, or may not be perpendicular to the principal optical axis of light source **106**. For this reason, the intermediate integrator **194** has an entrance this is not parallel to its exit. Instead, the entrance of the intermediate integrator **194** is substantially parallel to the plane of light source **106**; and the exit of the intermediate integrator **194** is substantially parallel to the entrance of integrator **178**. To improve the optical performance, the interfaces between the intermediate integrator **194** and the tilted integrator **178** can be filled with a suitable optical material, such as an optical film for enhancing the transmission of the interface. Instead of using an intermediate integrator, an optical integrator may be directly coupled to an light source as schematically illustrated in FIG. **13**.

Referring to FIG. **13**, optical integrator **198** in this example has an entrance that is parallel to plane of light source **106**; while the principal optical axis **196** is tilted along the desired direction. The exit of optical; integrator **198** may or may not be parallel to the entrance of the optical integrator. Alternatively, the light source **106** can be tilted so that the optical axis **196** is normal to the light source surface.

Optical integrators can also be used for directing light from light sources that are arranged in two-dimensional arrays, an example of which is schematically illustrated in FIG. **14**.

Referring to FIG. **14**, light sources **140**, **142**, and **144** (not shown, behind optical integrator **204**) are arranged in a two-dimensional array as that discussed above with reference to FIG. **6**. Optical integrators **200**, **202**, and **204** are disposed approximate to the light sources. Specifically, the narrow entrance of each one of the optical integrators (**200**, **202**, and **204**) is disposed approximately to a light source for collecting the light from the light sources. The wider exit of each optical integrator (**200**, **202**, and **204**) is opened towards collimation lenses **164** and **165** and dichroic filters **170**, **172**, and **174**. The dichroic filters **170**, **172**, and **174** can be disposed in the same way as that discussed above with reference to FIG. **7** through FIG. **9b**. The reflected light from the individual dichroic filters are collected by the entrance of optical integrator **162** that delivers the collected light to other devices, such as a light valve. At the entrance of the optical integrator **162**, the reflected light from individual dichroic filters can be spatially and angularly coincident.

The optical system as discussed above, as well as many other variations, has many applications, one of which is an imaging system. For demonstration purposes, FIG. **15** schematically illustrates a diagram of an exemplary imaging system in which an exemplary optical system is implemented therein.

Referring to FIG. **15**, optical system **100** is the same as that discussed above with reference to FIG. **1**. Specifically, optical system **100** comprises light sources **104**, **106**, and **108**, collimation optics **112** that further comprises lenses **114** and **116**, optical filter group **118**, fly's eye lens arrays **134** and **136**. The light from the optical filters is directed to light valve **208** through field lens **206** that can be disposed proximal to the light valve. The light valve modulates the incident light according to image data (e.g. bitplane data) associated with desired images. The modulated light is then directed to projection lens **210** that projects the modulated light onto a screen.

In addition to enabling the spatial and angular coincidence of the reflected light by the dichroic filters, the optical configuration of the optical system may also enables the optical length between the light sources and the light valve (**208**) to be substantially the same. As a consequence, the light sources can be directly imaged onto the light valve, which has many benefits, such as enabling the compact optical system and/or the imaging system using the optical system.

The light valve in this example comprises an array of individually addressable pixels that can be reflective or transmissive. For example, the light valve or light valves may comprise one or more reflective micromirror devices, or one or more liquid-crystal-on-silicon devices.

In the examples as illustrated above in FIG. **1** and FIG. **15**, fly's eye lens array **134** is provided for generating a uniform illumination field of the reflected light at the location of the light valve. The fly's eye lens array can be implemented in many ways, one of which is schematically illustrated in FIG. **16**.

Referring to FIG. **16**, fly's eye lens array **134** comprises front lenticular array **212** and rear lenticular array **214**. This is alternative to the one-piece design where there is an array on each side of a single optical element. The lenslets in each lenticular array can have any desired form, such as a cubical lens, a spherical lens, aspherical lens, semi-spherical lens, or other types of lenses. The lenslets in the lens arrays are individually associated with each other such that, with field lens **206** after the rear lens array **218**, the light from a lenslet (e.g. lenslet **216**) in the front lens array can be spread across substantially the entire area of light valve **208**. As a consequence, the light passed by the lenslets in the front lens array (**216**) are

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optically integrated at the location of light valve **208** after the lenslets in the rear lens array **214** and field lens **206**. The optical integration of the light results in a highly uniformed illumination field at the location of the light valve. The light valve modulates the light incident thereto based upon image data associated with desired images; and the modulated light is projected to screen **220** through projection lens **210**.

In addition to standard dichroic filters wherein the reflective surfaces of the dichroic filters are continuous, a dichroic filter can be configured to be segmented, such as in a saw-teeth arrangement, as schematically illustrated in FIG. 17. Referring to FIG. 17, optical filter group **222** in this example comprises dichroic filter **224**, dichroic filter **226**, and reflective optical element **228**. Dichroic filter **224** is a standard dichroic filter with a surface for reflecting the collimated light that is emitted from light source **108** and collimated by collimation optics **112**, which comprises lenses **114** and **116**.

Dichroic filter **226** in this example comprises a segmented saw-tooth structure that forms a reflective surface. The geometric configuration, such as the period, the angles, and the height, of the segments of dichroic filter **226** can be determined by the optical properties, such as the wavelength and the incident angle of the light from light source **106** to take into account interference effects. Alternatively, the segments can be much larger than the wavelength of light from the light source. The segments of dichroic filter **226** are rotated such that the light traveling along the principal optical axis of light source **106** can be reflected towards the desired direction **132** by dichroic filter **226**.

Similarly, reflective optical element **228** in this example comprises saw-tooth fine structures that form a reflective surface. The geometric configuration of the saw-teeth of reflective optical element **228** can be determined by the optical properties of the light from light source **104**. Reflective optical element **228** is rotated such that the light traveling along the principal optical axis of light source **104** can be reflected towards the desired direction **132**.

With the optical structure as illustrated in FIG. 17, the light from light sources **104**, **106**, and **108** can be directed to propagate along the desired direction **132**. The reflected light can be spatially and angularly coincident, as schematically illustrated in FIG. 2a through FIG. 2c. Using the segmented approach, the optical designer has an extra degree of freedom with which to combine the light beams to be more spatially and angularly coincident.

The dichroic filters with segmented structures can also be employed for directing light from light sources that are arranged in two-dimensional arrays, such as an array illustrated in FIG. 3 through FIG. 5. In particular, the dichroic filter segments can be rotated individually based upon the physical arrangements of the light sources in the two-dimensional light source array as discussed above with reference to FIG. 7 through FIG. 9b, which will not be repeated herein.

For demonstration purposes, another exemplary imaging system that employs an exemplary optical system is schematically illustrated in FIG. 18. Referring to FIG. 18, light source **102** comprising light sources **104**, **106**, and **108** are arranged in a one-dimensional array for providing light. The light from the light source array is directed optical filter group **118** through collimation optics **112** that comprises lenses **114** and **116**. The optical filter group (**118**) comprises a set of dichroic filters for individually reflecting the light from the light sources toward the desired direction **132**. The placements of the dichroic filters can be the same as that discussed above with reference to FIG. 1. The reflected light traveling along the desired direction **132** is directed toward prism assembly **232** through lens **230**.

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The prism assembly (**232**) comprises prisms **234** and **236** that form a totally-internally-reflective interface (TIR) that reflects the incident light onto light valve **208**. The light valve (**208**) comprises an array of individually addressable pixels for modulating the incident light. The modulated light passes through prism **236**; and is projected by projection optic **210** that images the modulated light onto a screen. In this example no light integrator such as a fly eye lens or light tunnel is shown, although one could be added. In this example the light sources **104**, **106**, **108** can be directly imaged onto the light valve **208**.

Another exemplary imaging system employing an optical system of this disclosure is schematically illustrated in FIG. 19. Referring to FIG. 19, light source **102** (which further comprises light sources **104**, **106**, and **108**), collimation optics **112** (which further comprises lenses **114** and **116**), optical filter group **118**, and lens **230** can be the same as that discussed above with reference to FIG. 18. The light after the dichroic filters and lens **230** is directed to mirror **238** that reflects the incident light onto a curved reflective surface of mirror **240**. The curved reflective mirror condenses the incident light onto light valve **208** that modulates the incident light using an array of individually addressable pixels. The modulated light is then collected and projected by projection optics **210**.

It is noted that the imaging system as discussed above with reference to FIG. 18 and FIG. 19 are only two of many possible examples. Other variations are also applicable. For example, the light source array in each one of the imaging systems can comprise light sources that are arranged in two-dimensional arrays. In these examples, the dichroic filters can be arranged accordingly, such as that discussed above with reference to FIG. 7 through FIG. 9b.

Another exemplary imaging system employing an optical system of this disclosure is schematically illustrated in FIG. 20. Referring to FIG. 20, light sources **252**, **254**, and **274** provide light of different colors, such as colors selected from red, green, blue, yellow, cyan, magenta, or any combinations thereof. In this example, light sources **252**, **254**, and **274** provide blue, red, and green light, respectively.

Light from light sources **252** and **254** is directed to filter group **268** that comprises dichroic filters **270** and **272**. The dichroic filters **270** and **272** have different filter properties. Examples of dichroic filters can be thin film interference filters.

Dichroic filter **270** reflects red light and transmits green light, whereas dichroic filter **272** reflects blue light and transmits red and green light. The dichroic filters **270** and **272** are placed in a way such that the principal optical axes of the light from light sources **252** and **254** can be combined into the desired direction **282**, as discussed above with reference to FIG. 1 through FIG. 2c, which will not be repeated herein.

Light source **274** can be disposed such that the principal optical axis of the light from light source **274** is substantially aligned to the desired direction **282**. As a consequence, the light from light source **274** can propagate along the desired direction after the collimation lens group **276** that further comprises lenses **178** and **280**, dichroic filters **270** and **282**.

The light after the dichroic filters **270** and **272** can be directed to other optical elements, such as fly's eye lens array **284** and field lens **286**; and the light after the optical elements can be directed to a light valve for illuminating the light valve. In another example, the light after the dichroic filters **270** and **272** can be directed to optical elements, such as the optical elements **230** and **232** as illustrated in FIG. 18, or can be directed to mirror **238** and curved mirror **240** as illustrated in FIG. 19 before being directed to a light valve.

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The optical systems as discussed above are also used for direction polarized light from light sources by replacing the dichroic filters of the optical systems as discussed above with reflective polarizing filters, and example of which is schematically illustrated in FIG. 21. Referring to FIG. 21, light sources 252 and 254 provide polarized light of different polarization states.

Polarized light from light sources 252 and 254 is directed to polarize filter group 268 that comprises reflective polarizing filters 270 and 272. In this example the sources can have linear or circular polarization states. The reflective polarizing filters 270 and 272 have different polarization transmission and reflection properties. Examples of reflective polarizing filters are wire grid polarizers. Specifically, the polarized light from light source 252 is reflected by filter 272, and the polarized light from light source 254 is transmitted by filter 272.

When a wire-grid polarizer is employed as reflective polarizing filters 272, the polarization direction of the polarized light from light source 252 can be parallel to the direction of the grids in the wire-grid polarizer. In another example, polarizing optics can be placed between filter 272 and the light emitting device in light source 252 for adjusting the polarization state of the polarized light from light source 252.

For passing the polarized light from light source 254, reflective polarizer filter 272 can have a polarization transmission characteristics that transmits polarized light from light source 254. In examples wherein the polarization transmission characteristic of the filter 272 and the polarized light from light source 254 do not match, polarization-modifying optics such as optical retarders or polarization rotation optics can be placed between filter 272 and the light emitting device of light source 254 for adjusting the polarization state of the polarized light from light source 254.

For reflecting the polarized light from light source 254, reflecting polarizing filter 270 can be a simple mirror in this example. Polarization-modifying optics such as optical retarders or polarization rotation optics can be placed between filters 270 and 272, or between filters 270 and the light emitting devices in light sources 252 and 254 as stated above.

The reflective polarizing filters 270 and 272 are placed in a way such that the principal optical axes of the polarized light from light sources 252 and 254 can be combined into the desired direction 282, as discussed above with reference to FIG. 1 through FIG. 2c, which will not be repeated herein.

The polarized light after the reflective polarizing filters 270 and 272 can be directed to other optical elements, such as a set of dichroic filters to combine light of different colors, fly's eye lens arrays, and other optical elements as shown in the previous figures.

FIG. 22 shows an optical system for combining light from multiple light sources in an imaging system using a set of dichroic filters positioned between two fly's eye lens arrays. Light from sources 104, 106, 108 is collimated by lens group 112 and enters fly's eye lens array 320 with a light distribution from each source uniform in angle. Light entering a single lenslet in entrance array 320 reflects from optical filter group 300 as in FIG. 1 and exits a corresponding lenslet in exit array 322. Each source can be imaged at an exit lenslet through a corresponding entrance lenslet in an efficient illumination system. Light of different colors entering one lenses can exit the same lenslet, as shown, or different (e.g. adjacent in X or Y) lenslets, depending on the angle and position and nature (segmented and flat) of the optical filters 304 and 305 and reflective optical element 308. After the optical system of FIG. 22, the light can be directed toward a light valve or through further optics as shown in the previous examples.

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The optical system as discussed above has many advantages. For example, the optical system can be configured to be very compact, such as 100 cm or less, 50 cm or less, 20 cm or less, or 1 cm or less. When the light sources are solid-state light sources, such as lasers and LEDs, the solid state light sources can be on the same substrate, such as a semiconductor substrate or packaging substrate. Moreover, the substrate can be integrated with other system components. When used in imaging systems that employ light valves, the light sources can be directly imaged onto the light valves because the optical length between the light sources and the light valve is substantially constant, which also helps to reduce the size of the optical system.

In examples wherein the dichroic filters are interference filters, the dichroic filters can be operated such that the corresponding light is incident substantially perpendicularly or close to perpendicular incidence (e.g. 10° or less, 5° or less, 2° or less). As a benefit, each dichroic filter may have fewer interference layers than dichroic filters used in larger incident angles. The dichroic filter for the green color can be a short/long pass filter especially when it is the second dichroic filter in the optical filter group (e.g. between the dichroic filters for the red and blue colors). The dichroic filters in the optical system as discussed above may have smaller sizes as compared to those used in existing optical system and/or imaging systems, which of course, reduces the cost of the system.

When a fly's eye lens array is used with the dichroic filters and integrators (e.g. integrators 176, 178, and 180 in FIG. 10 and FIG. 11, and integrators 200, 202, and 204 in FIG. 14), the fly's eye lens array can be closer to the collimation optics (e.g. collimation optics 112 in FIG. 15) than those in prior art.

It will be appreciated by those of skill in the art that a new and useful optical system comprising optical filters, including dichroic and polarization filters, for directing light from multiple light emitting devices has been described herein. In view of the many possible embodiments, however, it should be recognized that the embodiments described herein with respect to the drawing figures are meant to be illustrative only and should not be taken as limiting the scope of what is claimed. For example, a dichroic filter in any of the preceding examples could be replaced by another type of filter, such as a polarization filter. Those of skill in the art will recognize that the illustrated embodiments can be modified in arrangement and detail. Therefore, the devices and methods as described herein contemplate all such embodiments as may come within the scope of the following claims and equivalents thereof.

We claim:

1. A method, comprising:

providing light from first and second light sources each producing light having a substantially separate spectrum;

reflecting the light from the first light source by a dichroic filter that passes the light from the second light source; and

reflecting the light from the second light source by a reflective surface, wherein the reflective surface has a non-zero angle to the dichroic filter, the angle between the reflective surface and the dichroic filter causing the reflected light from the first light source and the reflected light from the second light source to be combined along a common light path;

wherein the first and second light sources are adjacent first and second LED light sources, laterally spaced in a linear array along a Cartesian Z-axis direction and producing light of respective different colors; and

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wherein light from the first LED light source is incident on the dichroic filter along a first optical axis aligned with a Cartesian coordinate X-axis, light from the second LED light source is incident on the reflective surface along a second optical axis offset by an angle δ_1 from the X-axis, the dichroic filter is tilted about a Cartesian coordinate Y-axis by an angle Ω_0 from the X-axis, and the reflective surface is tilted about the Y-axis by an angle $\Omega_1 = \Omega_0 - \delta_1/2$ from the X-axis, such that substantially all light from the first and second LED light sources is spatially and angularly coincident after being reflected off the dichroic filter and the reflective surface.

2. The method of claim 1, wherein the reflective surface is a reflective surface of another dichroic filter or a reflective surface of a mirror.

3. The method of claim 2, wherein the reflective surface comprises a series of segments.

4. The method of claim 1, further comprising:

providing light from a third LED light source adjacent to and laterally spaced along the Z-axis direction from the first and second LED light sources in the linear array and having a different color than the light from the first and second LED light sources; and

reflecting the light from the third LED light source by another dichroic filter that passes light from the first and second LED light sources;

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wherein light from the third LED light source is incident on the another dichroic filter along a third optical axis offset by an angle δ_2 from the X-axis, the another dichroic filter is tilted about the Y-axis by an angle Ω_2 from the X-axis, and the another dichroic filter is tilted about the Y-axis by an angle $\Omega_2 = \Omega_0 + \delta_2/2$ from the X-axis, the angle between the reflective surface and the another dichroic filter causing the reflected light from the first and second light sources and the reflected light from the third light source to be combined along the common light path such that substantially all light from the first, second and third LED light sources is spatially and angularly coincident after being reflected off the dichroic filter, the reflective surface and the another dichroic filter.

5. The method of claim 4, wherein the light from the first, second and third LED light sources is directed to the dichroic filter, the reflective surface and the another dichroic filter through collimation optics.

6. The method of claim 5, wherein a uniform illumination field of the reflected light is generated by passing the reflected light combined along the common light path passes through a fly's eye lens array.

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