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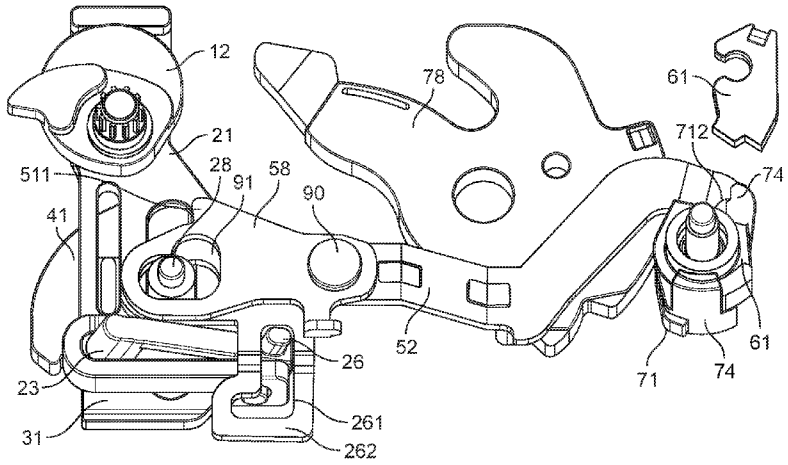


FIG. 10

(57) Abstract: A closing and latching mechanism for a closure in which further rotation of an input shaft (15) in a latching direction results in engagement of a release cam (11) with a release cam follower (511) and movement of a release slider (52) which moves a pawl (71) into a position in which a claw (78) is free to move from a latched position to an unlatched position and the claw (78) then moves towards the unlatched position under the action of a biasing spring (17).

CLOSURE AND LATCHING MECHANISMS

The present invention relates to closure and latching mechanisms, particularly for doors and most particularly for motor vehicle doors. The invention is concerned with that type of such mechanism which is moved under power between the latched and unlatched or semi-latched positions. Specifically, the invention relates to closure and latching mechanisms of the type comprising a claw for engaging a striker fixed to a door or other closure, a pawl for latching open the claw and motor drive means for moving the pawl so that it releases the claw and for moving the claw into the latched position.

WO2010/067074 discloses an automotive closure and latching mechanism including a pivotally mounted claw, a pawl and an arcuate drive lever. The claw is retained in its fully latched position by the engagement of latching shoulders on the pawl and the claw and the striker is thus retained captive within the recess defined by the claw. When the tailgate or the like is to be opened, an electric motor is operated in one direction and the drive lever is rotated in one direction. A post on the drive lever contacts the pawl and rotates it so that the latching shoulders move out of engagement. The claw is now moved by a spring acting on it into the semi-latched position. When the latch is to be re-latched, the motor is operated in the opposite direction and a cam surface causes the drive lever to rotate in the other direction. This causes the post on the drive lever to contact the claw and rotate it into the latched position. **Thus in this known mechanism** there is a **common lever** which is used to enable both release and complete the closure. When driven in one direction, this lever acts directly on the pawl to release the claw and when driven in the

opposite direction, it acts directly on the claw to drive it from an intermediate latched position to a fully latched position.

According to the present invention a closing and latching mechanism for a closure includes a claw for engaging a striker fixed to the closure, the claw being rotatable between an unlatched position and a latched position and biased by a spring towards the unlatched position, a pawl mounted to pivot between a first position, in which it can engage the claw in the latched position and prevent movement of the claw into the unlatched position, and a second position, in which the claw is free to move from the latched position to the unlatched position, a rotatable input shaft carrying a first clinch cam which is operatively coupled to the claw, whereby rotation of the input shaft in one direction results in rotation of the claw into the latched position, the input shaft also carrying a release cam which cooperates with a release cam follower forming part of a release slider, the release slider being operatively coupled to the pawl, whereby further rotation of the input shaft in the said one direction results in engagement of the release cam with the release cam follower and movement of the release slider which moves the pawl into the second position and the claw then moves towards the unlatched position under the action of the biasing spring.

Thus in the mechanism in accordance with the invention there is no common lever, as in the prior document and instead release of the mechanism is induced by a dedicated cam being driven in one direction acting on a release slider whilst latching of the mechanism is effected by a further dedicated cam carried by the same shaft and rotated in the same direction which acts on the claw to move it into the latched position.

In a preferred embodiment the first clinch cam is operatively coupled to the claw by a first clinch cam follower, which cooperates with the first clinch cam and is provided on a linearly movable clinch slider, the clinch slider being operatively coupled to a second clinch cam, which cooperates with a second clinch cam follower forming part of a pivotally mounted clinch lever, a further part of the clinch lever constituting a third clinch cam which cooperates with a third clinch cam follower constituted by a portion of the claw.

The operative connection between the first clinch cam and the claw preferably provides a mechanical advantage of at least 2, preferably at least 4. The operative connection is preferably constructed so that the mechanical advantage increases as the claw approaches the fully latched position. The clinch lever may be of generally T shape with the head of the T constituted by two limbs, a first of which constitutes the second clinch cam follower and the second of which is shorter than the first limb and constitutes the third clinch cam. The distance of the third clinch cam follower from the axis of rotation of the claw may be at least 2 and preferably 3 times greater than the distance between the said axis of rotation and the position at which, in use, the claw engages the striker. The combination of these features results in an overall mechanical advantage of at least 10 and potentially even as much as 20, e.g. 15, and this enables the electric motor to be considerably smaller, cheaper and lighter than is usual.

The mechanism preferably includes a manual release lever which is operably coupled to the pawl and the operation of which results in movement of the pawl into the second position.

The operative connection between the first clinch cam and the claw preferably includes a clutch or releasable connection which is selectively operable to sever or interrupt the operative connection. The clutch may comprise a clutch member connected to the clinch slider and movable between an engaged position in which movement of the clinch slider in the latching direction is transmitted to the claw and a disengaged position in which movement of the clinch slider is not transmitted to the claw.

The mechanism may include a release drive dog mounted to pivot about the same axis as the pawl and arranged to engage the pawl and to rotate it from the first position into the second position, the release drive dog being pivotally connected to the release slider and arranged to pivot about the said axis when the release slider is caused to move by the release cam. The manual release lever is preferably mounted to pivot about the same axis as the pawl and is arranged to engage the pawl and to rotate it from the first position into the second position when the manual release lever is operated.

In the preferred embodiment, the release slider carries a ratchet which affords the release cam follower, the ratchet being movable between a first position, in which the release cam can engage the release cam follower and move the release slider in the latching direction, and a second position in which the release cam may move past the release cam follower without contacting it, movement between the two positions being permitted when the release cam is not in contact with the release cam follower and being prevented when the release cam is in contact with the release cam follower, the mechanism carrying a third cam arranged to engage the ratchet and push it from the first position to

the second position. Thus if the clinching or closing operation of the latch mechanism should be interrupted for some reason, e.g. as a result of an obstacle preventing the door from closing fully, the closing operation is terminated and the input shaft is rotated in the reverse direction and as it moves it forces the ratchet out of the way against the force of a restoring spring and this enables the release cam to return to a position in which it may act on the release cam follower very much more rapidly than if it were to continue to rotate in the same direction.

Further features and details of the invention will be apparent from the following description of one specific embodiment of door closing and latching mechanism, which is given by way of example only with reference to the accompanying drawings, in which:

Figure 1 is a plan view of the mechanism, from which certain components have been omitted for the sake of clarity with the claw shown in the fully latched position and the striker shown in both the fully latched position and in a position before it is latched;

Figure 2 is a further plan view from which further components have been omitted, showing the claw in the intermediate latched position;

Figure 3 is yet a further plan view from which certain components have been omitted, showing the claw in the unlatched position;

Figure 4 is a scrap plan view showing the claw, pawl and release drive dog;

Figure 5 is a plan view of the first, second and third cams;

Figure 6 is a plan view of the clinch drive dog;

Figure 7 is a plan view of the clinch slider and manual clutch;

Figure 8 is a plan view of the clinch lever;

Figure 9 is an exploded perspective view of the pawl and the components associated with it;

Figure 10 is a further perspective view of the latch from which certain components have been omitted for the sake of clarity; and

Figures 11A, B, C and D show the different stages when unlatching the latch by reverse rotation of the input shaft.

The closure and latching mechanism is accommodated in an outer housing and for the sake of clarity only the base plate or retention plate 66 of the housing is shown in Figures 1 and 3. The housing defines an elongate opening 2, into which the striker 4 of a door, which is not shown, may enter. Connected to the retention plate 66 to rotate about a shaft 79 is a latching claw 78, which includes two arms, a short arm 8 and a long arm 10, which define between them an elongate recess 6. The claw is rotatable about the shaft 79 between three positions. The first of these is the unlatched position, shown in Figure 3, in which the claw is offset about 45° in the clockwise direction from the latched position shown in Figure 1. In this unlatched position, the opening 2 in the

housing is accessible and the door striker may freely enter and leave the opening 2. The second position, shown in Figure 2, is a partially latched position, in which the claw is offset about 25° in the clockwise direction from the position shown in Figure 1. When the door is closed manually, the striker will impinge against the long arm 10 and cause the claw to rotate in the anticlockwise direction, as seen in Figure 1. In this position exit of the striker from the opening 3 is blocked by the arm 8. The third position is the fully latched position shown in Figure 1, in which the striker is forced into the opening 2 and held there and the associated door is fully closed. The claw is biased into the unlatched position by a claw spring 17. At the free end of the arm 10 is a latching cam follower surface or clinch cam follower 714 and remote from the arms 8 and 10 the claw affords a primary retaining notch 712, affording a primary retaining surface and a secondary retaining notch 711 affording a secondary retaining surface. The function of these surfaces will be described below. The claw also carries one or more position sensor magnets 713, whose function will also be described below.

Pivotally connected to the retention plate 66 by way of a pivotal support 29 is a further pivotal shaft 29, which constitutes the power input shaft and is connected, in use, to an electric drive motor. Connected to rotate with the shaft 29 is a composite actuator cam, shown in Figure 5, which includes a first cam in the form of a projecting nose 11, a second cam or first power clinch cam 12, a third cam 13, constituted by one side of the nose 11 and a substantially straight rest surface 14 afforded by the cam 12.

Situated beneath the composite actuator cam is an elongate clinch slider 21, which is guided to move only parallel to its length by virtue of the fact that the

shaft 29 passes through a first elongate slot 19 in the clinch slider and that a further shaft 28 passes through a second slot 15 (see fig. 7) 5 in the clinch slider offset from the first slot 19. At its left-hand end, as seen in Figure 7, the clinch slider carries an upstanding ledge whose side surface 22 constitutes a third cam follower, which is in contact with the rest surface 14 or the power clinch cam 12, depending on the rotary position of the composite actuator cam. At its end remote from the third cam 32 is a clutch bar 23, which is mounted at one end to rotate with respect to the clinch slider 21 by a pivotal shaft 25, which extends parallel to the slots 19 and 15 (fig 7) 5. Upstanding from the clutch bar is a boss 26, which will be described in more detail below. The clutch bar normally extends below the clinch slider and constitutes an abutment 23 (Figure 10).

Situated below the clinch slider is a clinch drive dog 31, which is constrained to be movable only linearly parallel to the direction of movement of the clinch slider 21 by the shaft 28 extending through a linear slot 17 and by a linear upstanding guide formation 33 on its upper surface extending into or through a further linear slot 18 formed in the clinch slider. Extending downwardly from the clinch drive dog 31 is a generally cylindrical projection 34, which constitutes a fourth cam.

Situated below the clinch drive dog 31 and mounted to pivot about the shaft 28 is a clinch lever 41, shown in Figure 8. The clinch lever is of generally asymmetrical T shape and the side surface 43 of one limb of the T constitutes a fourth cam follower surface, which is in engagement with the fourth cam 34. A portion of the surface of the other limb of the T constitutes a fifth cam 42, which is positioned to contact the clinch cam follower 714 constituted by a portion of the surface of the claw, referred to above. Accordingly, when the

clinch slider moves to the left, as seen in Figures 1 and 2, the engagement of the clutch bar 23 with the clinch drive dog 31 causes the clinch drive dog also to move linearly to the left. This results in the fourth cam 34 engaging the fourth cam follow surface 43 and thus in rotation in the clockwise direction of the clinch lever. This rotation results in the fifth cam 42 engaging the cam follower surface 714 and thus in the claw rotating in the anticlockwise direction in Figures 1 and 2, that is to say from the semi-latched position to the fully latched position.

As best seen in Figure 9, upstanding from the other end of the retention plate 66 is a further fixed pivotal shaft 80. Rotatably carried by the shaft 80 is a latching pawl 71, which affords an abutment surface 72. Also pivotally carried by the shaft 80 above the latching pawl 71 is a release drive dog 74 with a downwardly extending lower tab 75 affording a first abutment surface, which is arranged to contact the surface 72 on the pawl 71, and an upwardly extending upper tab 76 affording a second abutment surface. Extending downwardly from the release drive dog 74, and shown in Figure 9 only in chain lines, is a pivotal boss 77. Also pivotally carried by the shaft 80 above the release drive dog is a manual release lever 61 carrying a tab 611, which affords a third engagement surface arranged to contact the second engagement surface on the tab 76 of the release drive dog 74. The release lever 61 is in the form of an elongate arm and near its outer end affords a notch or recess 612 in which a manual release cable or the like (not shown) may be secured. The pawl 71 is biased by a spring 73 into contact with the side surface of the latching claw 78. If the claw 78 is moved into the semi-latched position, the pawl will be urged by the spring 73 into the secondary retaining notch 711 and will engage a surface of that notch and prevent the claw from returning to the unlatched position under the action of its

return spring 17. If the claw is moved into the latched position, the pawl will be urged into the primary retaining notch 712 and will engage a surface of that notch and prevent the claw from returning to the semi-latched position or the unlatched position under the action of its return spring.

In use, the input shaft 15 is generally rotated only in one direction, that is to say anti-clockwise, as seen in the drawings, to both latch and unlatch a door and its movement is transmitted through two different pathways to the claw to move it from the semi-latched to the latched position and to the pawl to move it out of engagement with the primary retaining notch 712. When the latch is in the fully latched position, rotation of the input shaft 15 is transmitted via the first cam 11 to an elongate release slider 52 which is mounted to be movable substantially only linearly parallel to its length. One end of the release slider 52 has a hole formed in it, through which the pivotal boss 77 on the release drive dog 74 passes, such that linear movement of the release slider results in rotation of the release drive dog about the shaft 80. Pivotally connected to the release slider at a position adjacent its other end by means of a pivot pin 90 is one end of an elongate release ratchet 58. Formed in the release ratchet opposite its other end is an L-shaped slot 91, through which the shaft 28 extends. When the latch is latched, the release slider is generally in the position shown in Figure 2 in which the shaft 28 is received in a first limb of the L-shaped slot which extends transversely to the length of the release slider and rotation of the ratchet 58 relative to the release slider is permitted. However, when the release slider is moved in order to rotate the pawl into the released position, as seen in Figure 10, the shaft 28 is received in the second limb of the L-shaped slot extending parallel to the length of the release slider and ratchet and limited pivotal movement of the ratchet relative to the release slider is therefore not possible.

Alternatively, the ratchet is provided with one extended arm 514 (Figure 1) which abuts against shaft 28 and held resiliently in that position by a spring 515 and provided with a shoulder on the opposing side formed as a cam follower 511 to cooperate with the release cam 11. When rotated counter clockwise, cam 11 attacks the ratchet at the shoulder 513 (Fig.1). The force applied by the release cam 11 has two coordinates; a linear force acting on the slider to move it to rotate the pawl to release the claw and a rotary force acting on the ratchet to maintain it held against the shaft 28 while moving to rotate the pawl to release the claw. Though prevented by shaft 28, the second force coordinate has the effect of rotating the ratchet clockwise. In this embodiment the ratchet is permitted within the scope allowed to rotate counter clockwise and is always prevented from rotating clockwise by shaft 28 regardless of the position of the slider. Cam 13 rotates the ratchet counter clockwise to a limited extent. This extent is represented by the angular degree defined between the rest position of the ratchet and the point whereby cam 13 rotates past the ratchet. Once disengaged from cam 13, the ratchet is returned to its rest position by spring 515.

Projecting laterally from the release slider 52 is a plate 262 in which an L-shaped slot 261 is formed. This slot has a relatively long limb extending transverse to the length and direction of movement of the release slider and a relatively short limb extending parallel to the length of the release slider. The pivot boss 26 of the clutch arm 23 projects through this slot and is normally received in the relatively short limb of the slot 261, whereby movement of the release slider parallel to its length and relative to the pivot boss 26, is possible only during the release operation, whereby the slider is moved to rotate the pawl to release the claw and not possible during the clinch operation whereby the claw is driven from the secondary latch position to the primary latch position

without breaking the dynamic link and interrupting the clinch operation to release the claw.

If it is desired to move the latch from the fully latched to the unlatched position, the input shaft 15 is rotated anti-clockwise, as seen in Figure 1, and thus brings the cam 11 into contact with the shoulder 511 on the ratchet 58. The ratchet and release slider act as a single body and the force exerted on the ratchet by the cam 11 moves the release slider to rotate the pawl to release the claw, as seen in Figure 10. This movement is transmitted to the release drive dog 74, which is caused to pivot about the shaft 80. This brings the engagement surface on the lower tab 75 into engagement with the engagement surface 72 on the pawl 71 and causes the pawl to rotate clockwise, as seen in Figure 9, and thus to move out of engagement with the primary retaining notch 712 or the secondary retaining notch 711. The claw is then moved rapidly under the action of its retaining spring to the unlatched position and the door striker 4 is released, thereby enabling the associated door to be opened.

Once the release slider has been moved to unlatch the pawl and the cam 11 has moved past the shoulder on the ratchet, the drive motor is deactivated and the cam 11 stops rotating.

If the door is now moved in a closing direction, the door striker 4 will engage the arm 10 of the claw and rotate the claw into the semi-latched, “secondary” position. Detecting the claw in this position is enabled by sensors, not shown, responsive to magnets 713 on the claw, which induce the electronic control system comprising the magnet-responsive sensors which are integrated in the latch, not shown, to drive the electric motor and rotate the input shaft 15 further in the counter clockwise direction. This actuation causes the second cam 12 on

the input shaft to act on the second cam follower 22 on the clinch slider 21 and thus to move the clinch slider to the left, as seen in Figure 1. As it does so the clutch bar 23 (Fig. 10) on the clinch slider engages the clinch drive dog 31, which is thus conjointly moved linearly to the left. As it does so, the fourth cam, i.e. the cylindrical projection 34 engages the fourth cam follower 43 on the clinch lever 43. This causes the clinch lever to rotate clockwise, which in turn causes the fifth cam 42 on the clinch lever to engage the fifth cam follower 714 on the claw 78 and thus rotate the claw 78 in the anticlockwise direction, as seen in Figure 1, into the full or primary latch position. As mentioned above, the clinch lever is of asymmetrical T shape and the arm affording the fourth cam follower 43 is significantly longer than the arm constituting the fifth cam 42. At the start of the clinch operation the projection 34 is in contact with the cam follower 43 at a point substantially closer to the pivot of the clinch lever 41, thus transmitting substantially lesser power generally below 50% of the total available and increasing closer to full power as the clinch operation progresses closer to the end of the clinch operation. This arrangement provides an important safety advantage whereby a trapped object between the striker and the latch (the door and its frame/body of the car) at the start of the clinch operation will receive substantially lesser force and therefore the mechanism is substantially likely to stall before the power reaches a higher more damaging level, thus preventing damage to the trapped object. The progressive increase in the level of power transmitted by the clinch lever is explained by the incremental increase in the mechanical advantage created by the progressive outward displacement of cam 34 against the fourth cam follower 43 relative to the centre of rotation of the clinch lever. At the start of the clinch actuation the rate of transmission is generally 0.5 to 1 whereas at the end it is substantially 1 to 1. Thus, the power being transmitted at the end is substantially more than

double that which is available at the start of the clinch actuation. Therefore a trapped object would receive a pressure force of the magnitude of 10kg to 15kg before the mechanism stalls as opposed to 30kg to 50kg towards the end of the actuation. This particular arrangement on one hand serves as a safety measure and on the other satisfies the need to provide more closing force to react to the closing force acting on the door striker, which progressively increases as the door moves into the fully latched position. This is precisely what is needed to counter the increase of the reaction force created by the door weather seal as it compresses progressively towards the end of the door closing process. This feature therefore permits the electric motor to be significantly smaller and cheaper than would otherwise be the case. This effect is further enhanced by the fact that the fifth cam follower 714 is situated 2 to 4 times, in this case 3 times, as far from the pivotal axis of the claw as the door striker 4 with respect to its contact point with the claw arm 8, thereby resulting in a yet further mechanical advantage during the latching process. A further substantial mechanical advantage is provided by the shape of the second cam 12 relative to its axis of rotation, its position in relation to the clinch slider 21 and the cam follower 22. This arrangement enables the conversion of the torque imparted by cam 12 into linear force acting on the clinch slider at a rate of 3 to 5 times, in this case substantially 4 times. In other words if the clinch slider were to be driven by a direct linear force a motor 4 times the power would have been required to achieve that compared with the current arrangement in which a smaller motor was used with the advantage of cam 12. The combined effect of these features is to provide an overall mechanical advantage of between 10 and 20, typically 15.

The door latch in accordance with the present invention is of course primarily

electrically operated and will therefore be associated with an electronic control system, though this is not illustrated. Thus it is envisaged that when it is desired to open the door, this is indicated by operating an electrical switch, e.g. of push button type. However, it is desirable that manual operation is also possible, e.g. in the event of electrical failure, and in the preferred embodiment a cable or the like is operatively connected to the manual release lever 61, as described above. If the cable is pulled by the user, this will result in the lever 61 moving in the clockwise direction, as seen in Figure 9. This will bring the third engagement surface on the tab 611 of the release lever into contact with the second engagement surface on the tab 76 of the release drive dog 74 and rotate the release drive dog in the clockwise direction also and the engagement of the engagement surfaces on the drive dog and the pawl will rotate the pawl in the clockwise direction and cause the pawl to disengage from the claw, whereby the claw will then return rapidly to the unlatched position.

As mentioned above, during normal release movement of the release slider the boss 26 of the clutch arm 23 (Fig 10) is received in a portion of the L-shaped slot 261 and has no effect on this movement. However, if the clinching process is interrupted before it is completed, e.g. by an electrical failure or an interruption of the electrical power supply, operating the manual release lever will cause the dynamic link holding together as one unit the cluster comprised of the clutch arm 23, which is pivotally carried by the clinch slider 21, the clinch drive dog 31, the cam 34 of the clinch drive dog, the cam follower 43 of the clinch lever 41, the cam 42 and the cam follower 714 of the claw 78, which is coupled to the striker 4 by means of arm 8, to break from an operatively integrated unit during the clinch operation into individual components whereby the claw is free to rotate clockwise to release the striker. By pulling on the

manual release lever 61, the release drive dog 74 is forced to rotate clockwise pulling with it by means of the engagement boss 77, in a combined linear and rotary motion the release slider 52. The release slider being operatively engaged with the clutch arm 23 by means of the projection 26, which is operatively constrained by the slot 261, thus rotates the clutch arm 23 clockwise from a position whereby it holds the entire clinch cluster together as one operative unit into a position whereby the cluster is broken up into individual components. Simultaneously, as the manual release lever is rotated clockwise to break the clinch dynamic link, the pawl is also rotated to release the claw which is now free to rotate clockwise as the clinch lever becomes free to rotate to its pre-clinch rest position by a dedicated return spring not shown. .

The various stages of movement of the release ratchet 58 and the claw 78 are shown in Figures 11A to 11D. Figure 11A shows the first cam 11 at rest, that is to say in the pre-release position, and the claw 78 in its fully latched position. The release ratchet 58 is in its rest position aligned to cooperate with the first cam 11 to release the claw 78 when the cam 11 is rotated anticlockwise. Figure 11B shows the first cam 11 in an intermediate position having already caused the release of the claw 78 when rotated anticlockwise through about 30°. The claw 78 is shown in its released position and the release slider 52 is shown moved by a short distance, e.g. 3mm, to enable the release of the claw 78 from its fully latched position. The claw 78 is shown in the position in which it is ready to receive the striker. Figure 11C shows the first cam 11 and the third cam 13 in a position past the release or pre-clinch position and ready to rotate clockwise to come into contact with the release ratchet 58 to rotate it anticlockwise to a position where it is able to engage the release ratchet 58 and the release slider 52 to enable release of the claw 78. Figure 11D shows the

third cam 13 in the course of rotating clockwise, thus causing the release ratchet 58 to rotate anticlockwise to a position such that the first cam 11 is able to move to a position in which it is able to engage the release ratchet 58 to release the claw back to the position shown in Figure 11A.

This feature is particularly valuable if the cam 12 should fail to rotate fully to complete the clinch operation or for instance to interrupt the power clinch operation. .

By rotating the input 15 in a direction opposite to the normal direction, i.e. clockwisecam 13 is brought into contact with the release ratchet 58, which is then pivoted about its pivot shaft 90 (fig. 10) against the force of its restoring spring until the release ratchet is able to pivot back to its original position under the force of its return spring. As soon as the cam 11 has moved back past the shoulder 511 on the ratchet 58, the direction of the motor is reversed and the cam 11 will then act on the shoulder 511 and move the release slider 52 so as to release the latch. Moving the cams 12 and 13 backwards is considerably faster than continuing to rotate them in the usual anti-clockwise direction because a smaller angular rotation is required and this enables the latching mechanism to react more rapidly to a command to unlatch the latch countermanding a previous instruction to latch it.

The latching mechanism in accordance with the invention has numerous advantages over known latching mechanisms. In particular, it has a substantially reduced weight and size and thus reduced cost and also reduced power consumption. It enables clinching or latching under a load in excess of 1000N with an electric current of only 1.5 to 1.8 amps using a 12 volt DC motor

weighing around 60 grams as compared to a weight of between 200 and 400 grams of the motor used in similar systems. This is achieved by the specific mechanical arrangement of the cam 12 and the cam follower integrated with the clinch slider, which results in a considerable mechanical advantage. As described above, overall a mechanical advantage of up to 15 or even more may be obtained, thereby permitting the use of a considerably smaller, lighter and cheaper electric motor. The latching mechanism provides an anti-trapping function with or without electronic control. This is an important advantage and enables protection against damage to articles or fingers if they should become trapped in the door during the clinching or latching operation, even without electronic control or when such electronic control fails to perform. The movement is achieved by a number of integrated cams and cam followers, thereby resulting in operation with substantially zero backlash, and this in turn means that operation is silent. Backlash is an inherent feature of gear mechanisms which need to have a certain clearance between the teeth of the meshing gearwheels. This clearance necessarily results in impact noise as each gear tooth comes into contact with a corresponding tooth. By contrast, a system operated exclusively with cams is noiseless due to the nature of the contact between the cooperating components. Movement is smooth and continuous with no impact and a substantial mechanical advantage may be obtained in a relatively small space. A further significant advantage of the latching mechanism in accordance with the invention is its exceptionally low power consumption as it enables the use of miniature motors with stall currents below 2 amps as compared to the 12 to 36 amp motors that are normally required for similar devices.

CLAIMS

1. A closing and latching mechanism for a closure including a claw for engaging a striker fixed to the closure, the claw being rotatable between an unlatched position and a latched position and biased by a spring towards the unlatched position, a pawl mounted to pivot between a first position, in which it can engage the claw in the latched position and prevent movement of the claw into the unlatched position, and a second position, in which the claw is free to move from the latched position to the unlatched position, a rotatable input shaft carrying a first clinch cam which is operatively coupled to the claw, whereby rotation of the input shaft in one direction results in rotation of the claw into the latched position, the input shaft also carrying a release cam which cooperates with a release cam follower forming part of a release slider, the release slider being operatively coupled to the pawl, whereby further rotation of the input shaft in the said one direction results in engagement of the release cam with the release cam follower and movement of the release slider which moves the pawl into the second position and the claw then moves towards the unlatched position under the action of the biasing spring.

2. A mechanism as claimed in Claim 1 in which the first clinch cam is operatively coupled to the claw by a first clinch cam follower, which cooperates with the first clinch cam and is provided on a linearly movable clinch slider, the clinch slider being operatively coupled to a second clinch cam, which cooperates with a second clinch cam follower

forming part of a pivotally mounted clinch lever, a further part of the clinch lever constituting a third clinch cam which cooperates with a third clinch cam follower constituted by a portion of the claw.

3. A mechanism as claimed in Claim 1 or 2 in which the operative connection between the first clinch cam and the claw provides a mechanical advantage of at least 2, preferably at least 4.

4. A mechanism as claimed in Claim 3 in which the operative connection is constructed so that the mechanical advantage increases as the claw approaches the fully latched position.

5. A mechanism as claimed in Claims 2 and 3 in which the clinch lever is of generally T shape with the head of the T constituted by two limbs, a first of which constitutes the second clinch cam follower and the second of which is shorter than the first limb and constitutes the third clinch cam.

6. A mechanism as claimed in any one of the preceding claims in which the distance of the third clinch cam follower from the axis of rotation of the claw is at least two and preferably three times greater than the distance between the said axis of rotation and the position at which, in use, the claw engages the striker.

7. A mechanism as claimed in any one of the preceding claims including a manual release lever which is operably coupled to the pawl and the operation of which results in movement of the pawl into the second

position.

8. A mechanism as claimed in 7 in which operating the manual release lever to release the claw also drives the release slider to a position whereby the release slider and pawl are held in the claw releasing position until the claw is rotated to its fully open position and whereby releasing the claw at a certain point past the half latch position frees the the pawl back to its ready to re-engage the claw position.

9. A mechanism as claimed in any one of the preceding claims in which the operative connection between the first clinch cam and the claw includes a clutch which is selectively operable to sever the operative connection.

10. A mechanism as claimed in Claim 9 when dependent on Claim 2 in which the clutch comprises a clutch member connected to the clinch slider and movable between an engaged position in which movement of the clinch slider in the latching direction is transmitted to the claw and a disengaged position in which movement of the clinch slider is not transmitted to the claw.

11. A mechanism as claimed in any one of the preceding claims including a release drive dog mounted to pivot about the same axis as the pawl and arranged to engage the pawl and to rotate it from the first position into the second position, the release drive dog being pivotally connected to the release drive and arranged to pivot about the said axis when the release slider is caused to move by the release cam.

12. A mechanism as claimed in Claims 7 and 11 in which the manual release lever is mounted to pivot about the same axis as the pawl and is arranged to engage the pawl and to rotate it from the first position into the second position when the manual release lever is operated.

13. A mechanism as claimed in any one of the preceding claims in which the release slider carries a ratchet which affords the release cam follower, the ratchet being movable between a first position, in which the release cam can engage the release cam follower and move the release slider in the un-latching direction, and a second position in which the release cam may move past the release cam follower without contacting it, movement between the two positions being permitted when the release cam is not in contact with the release cam follower and being prevented when the release cam is in contact with the release cam follower, the mechanism carrying a third cam arranged to engage the ratchet and push it from the first position to the second position.

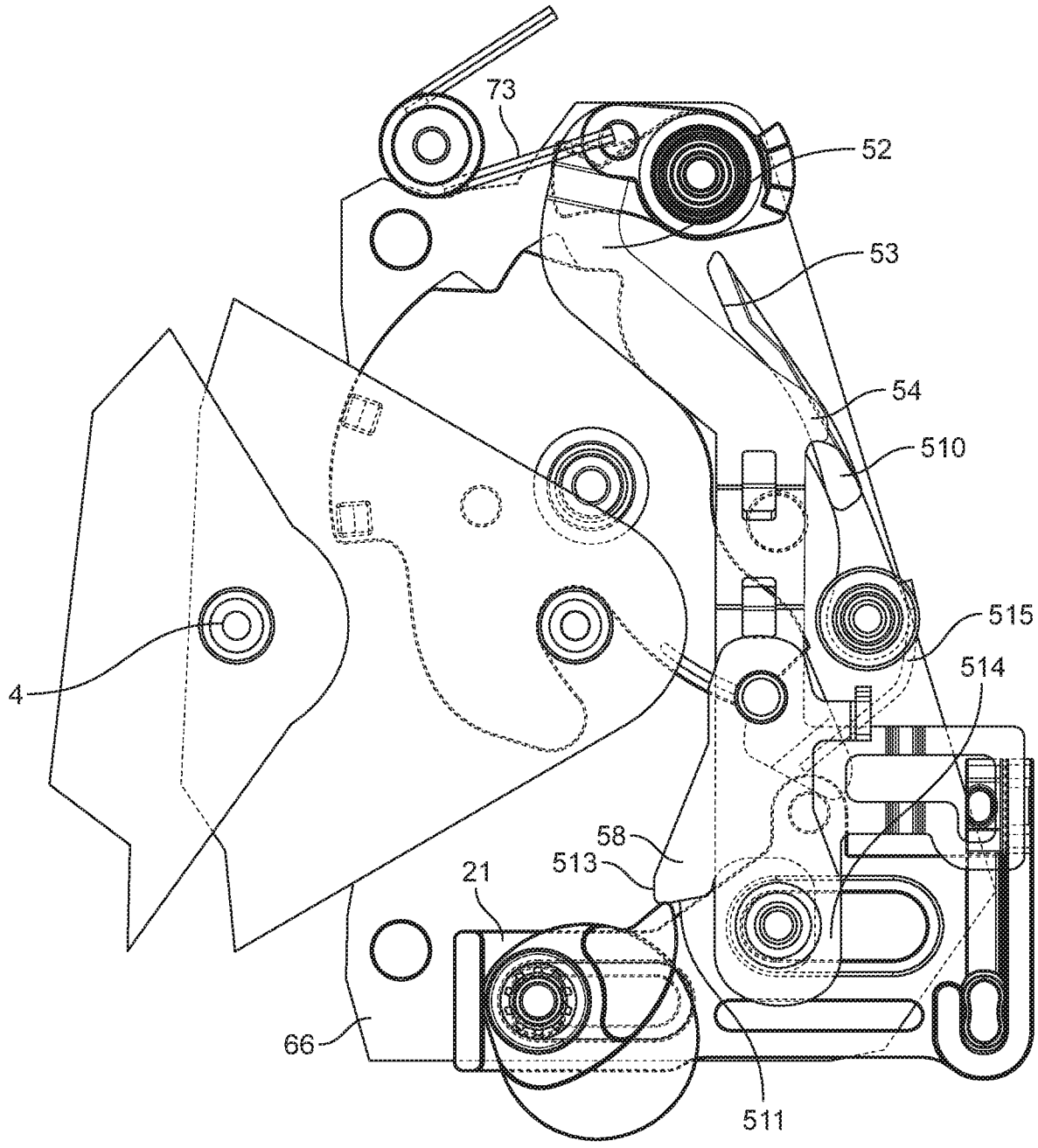


FIG. 1

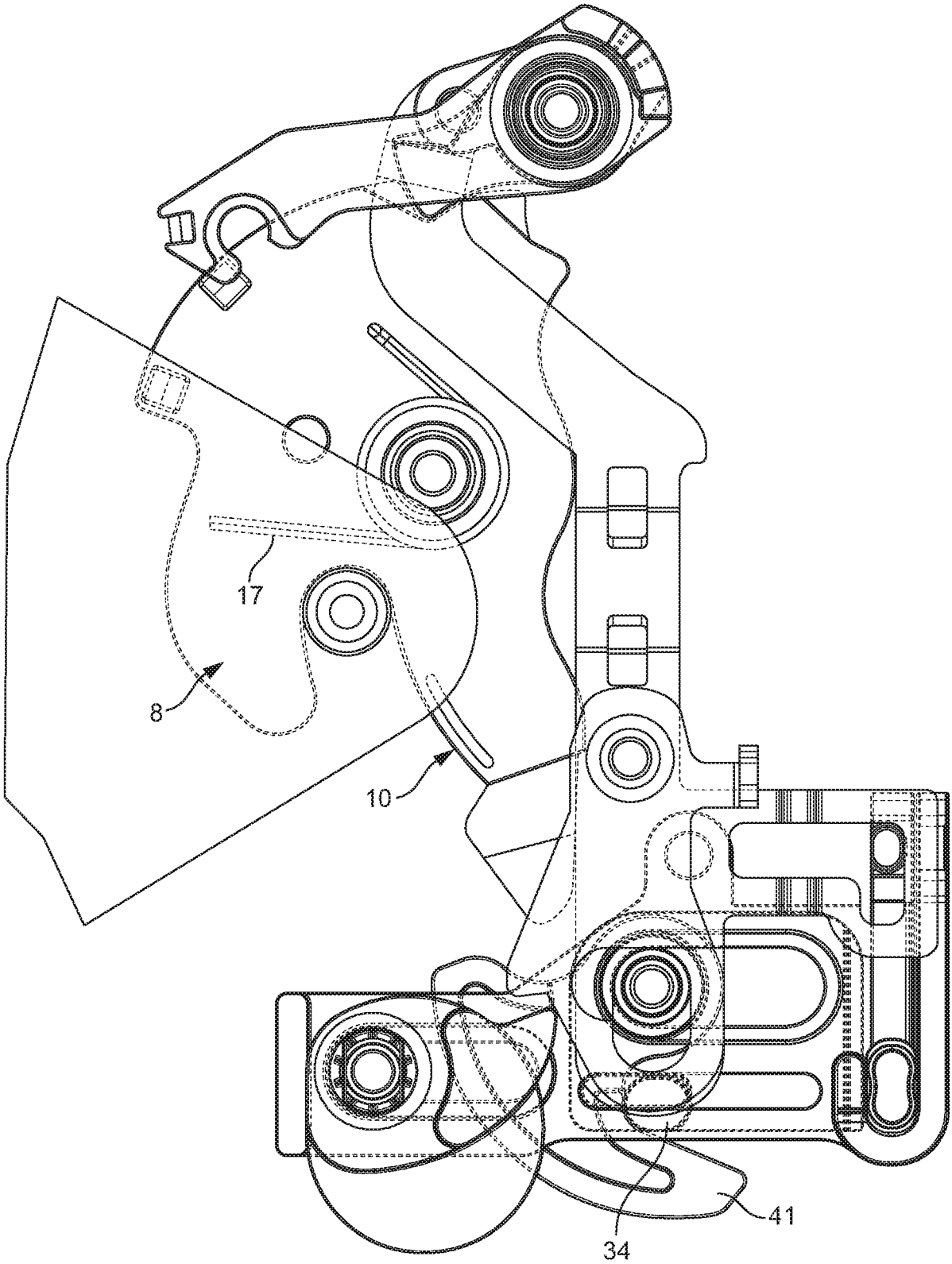


FIG. 2

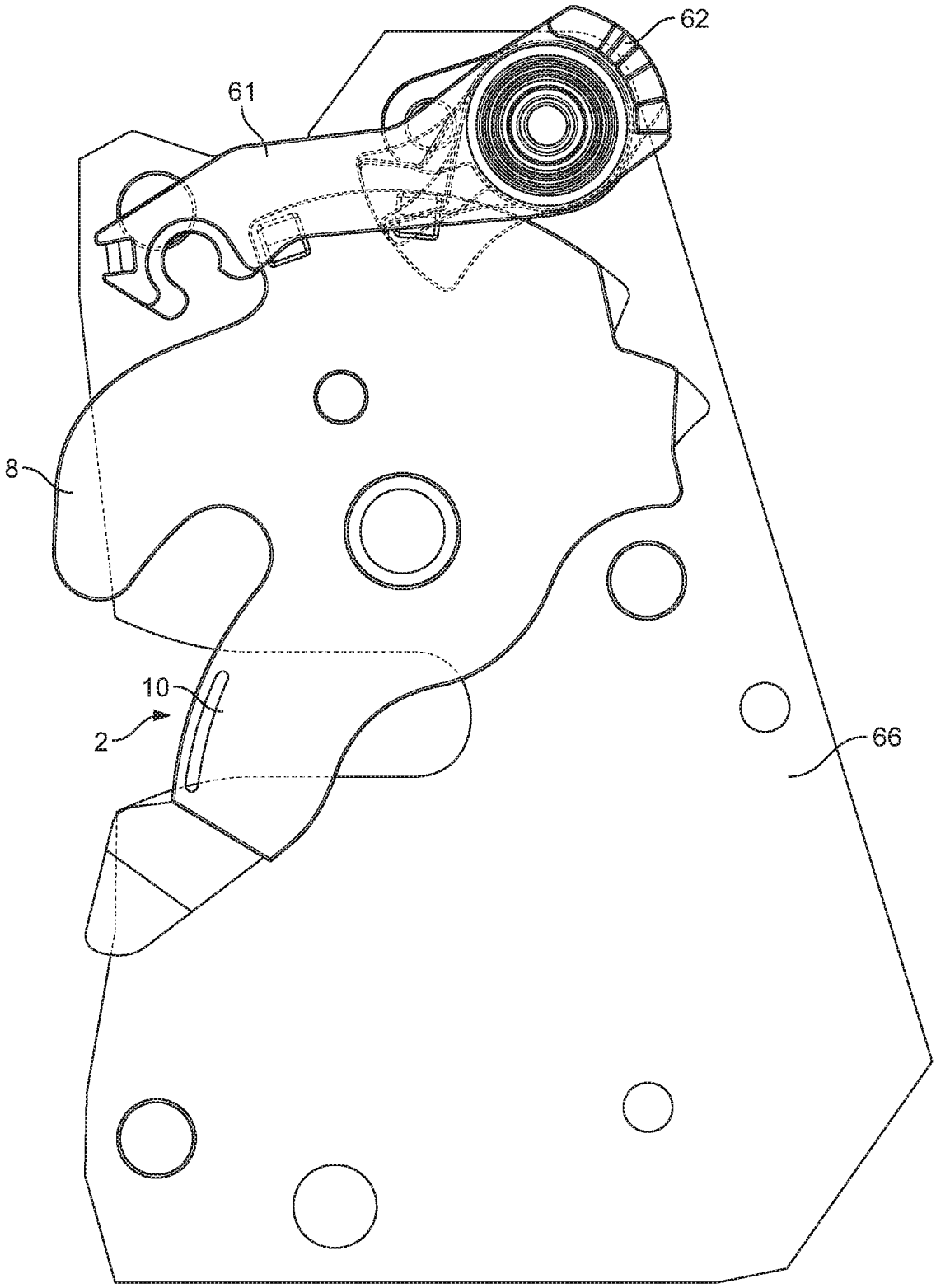


FIG. 3

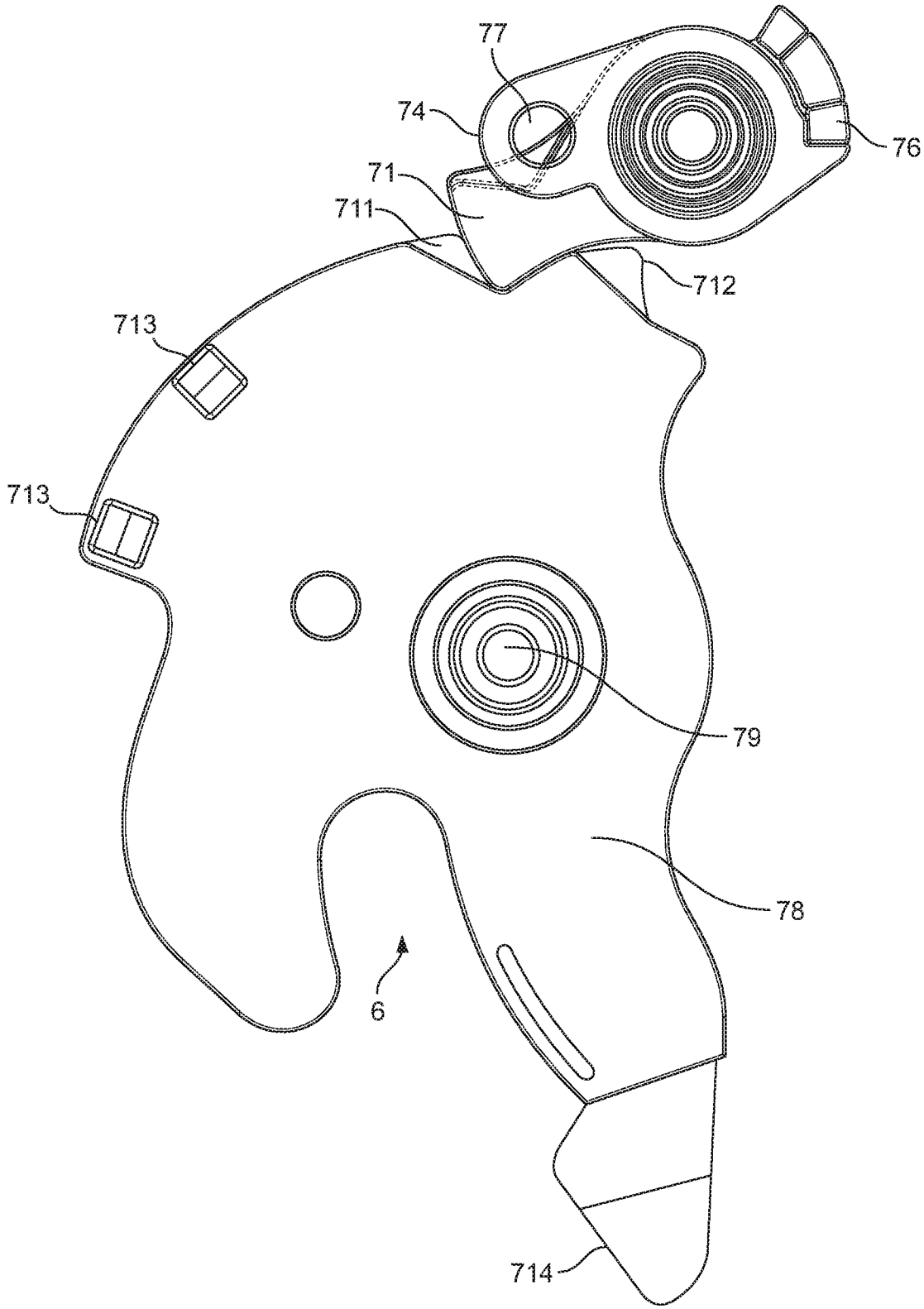


FIG. 4

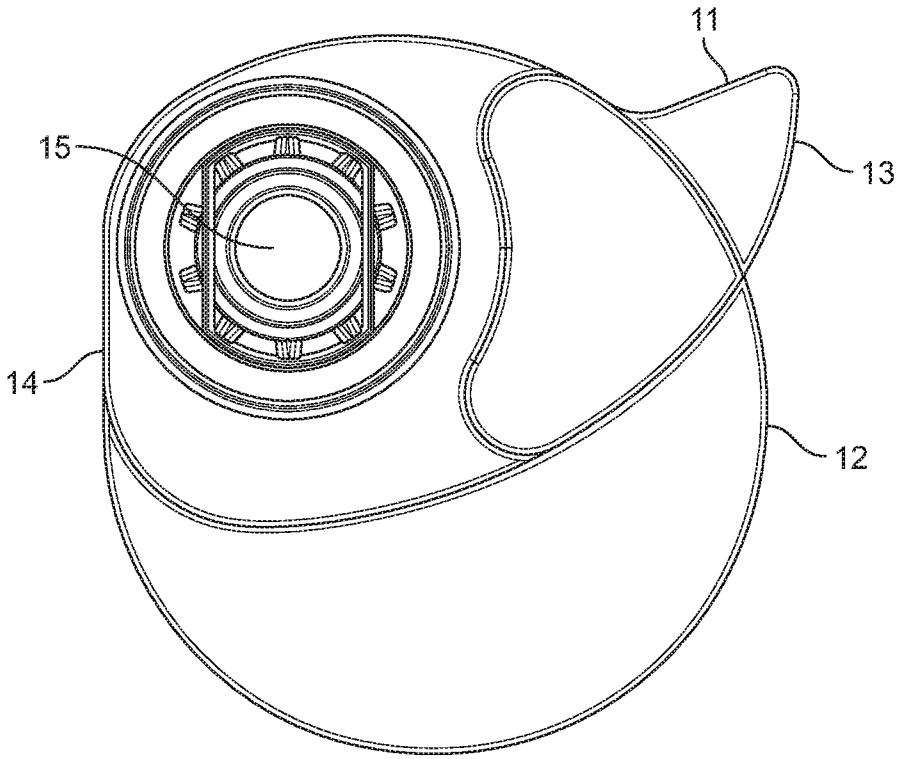


FIG. 5

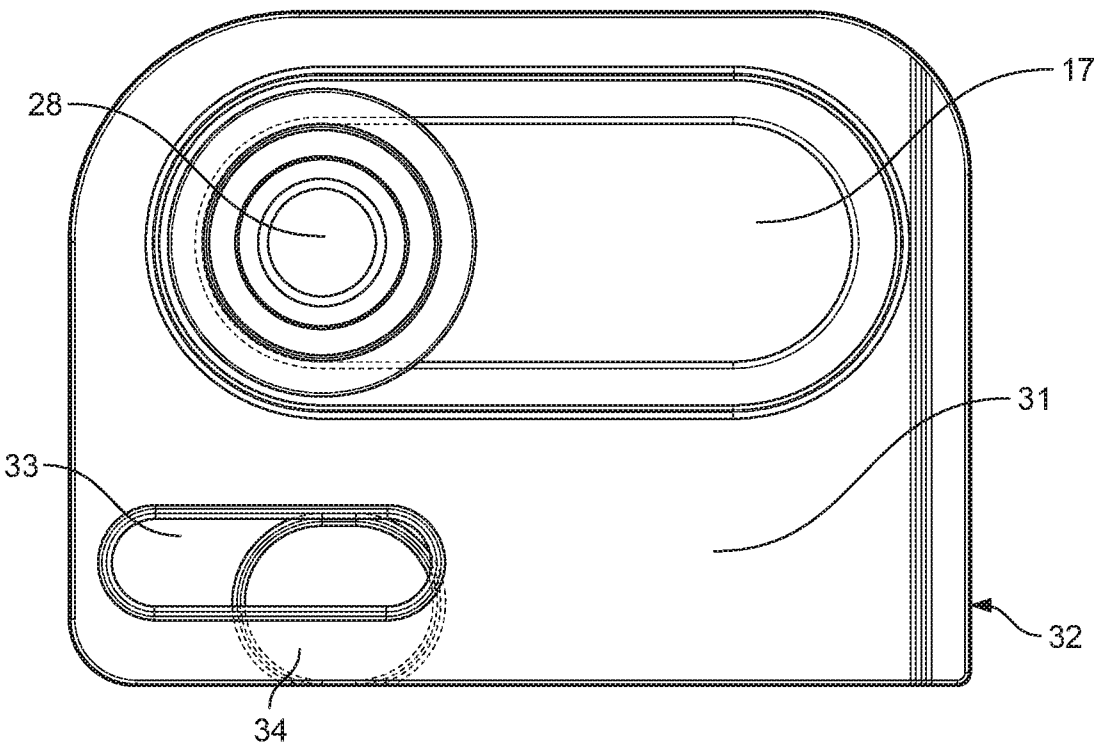


FIG. 6

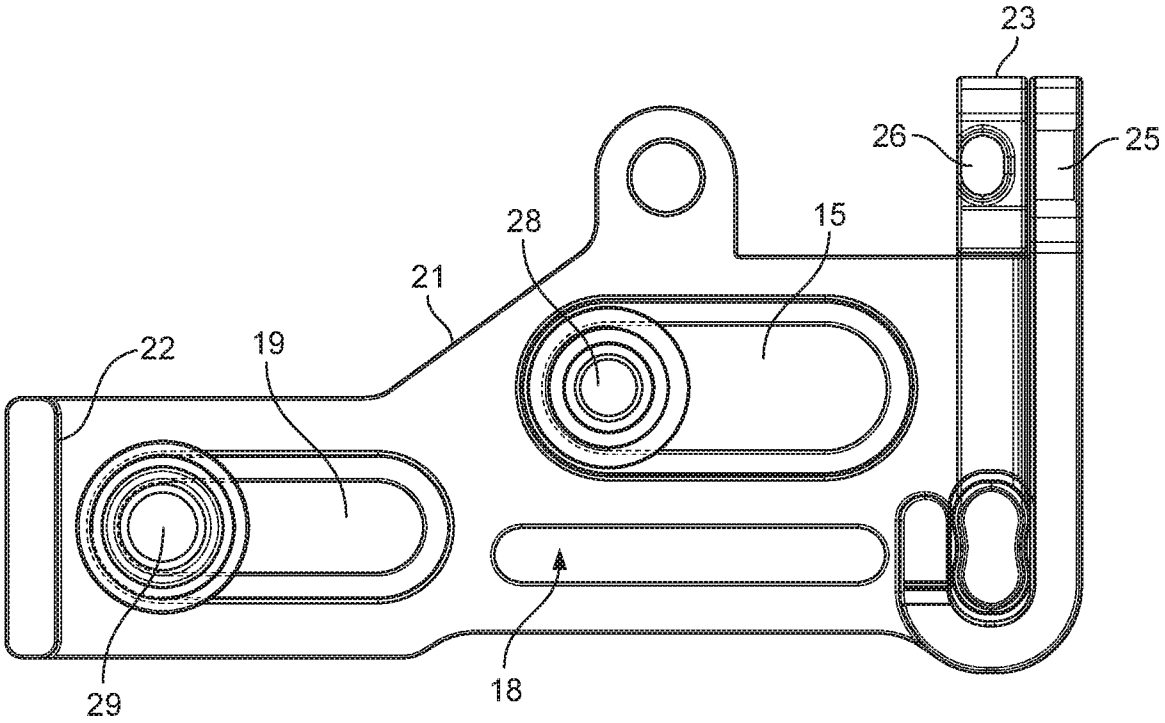


FIG. 7

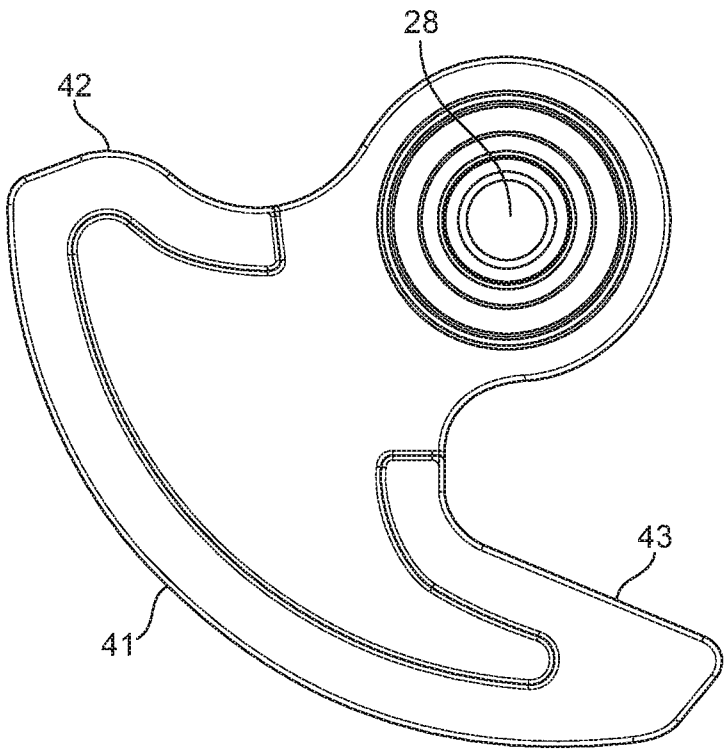


FIG. 8

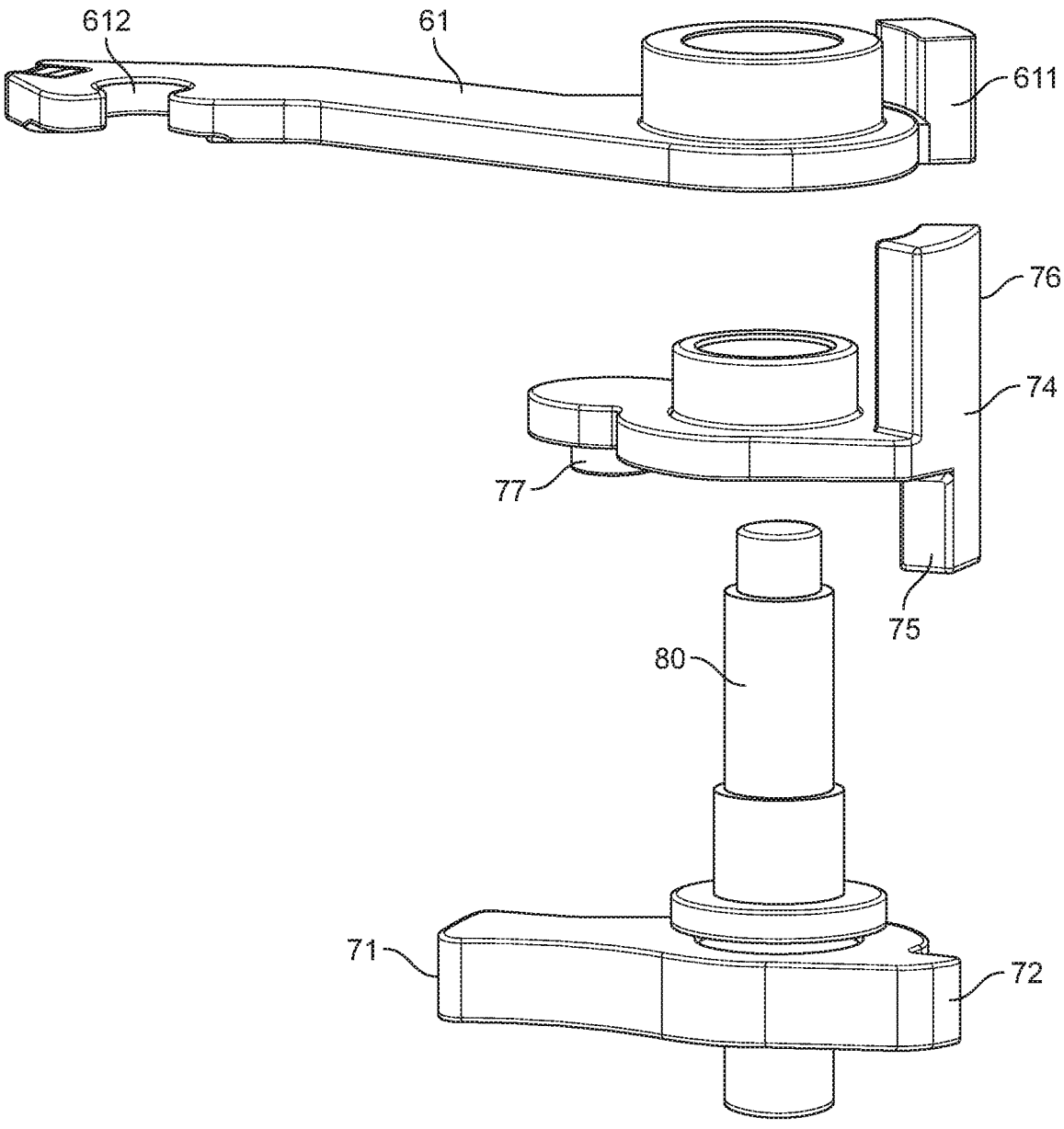


FIG. 9

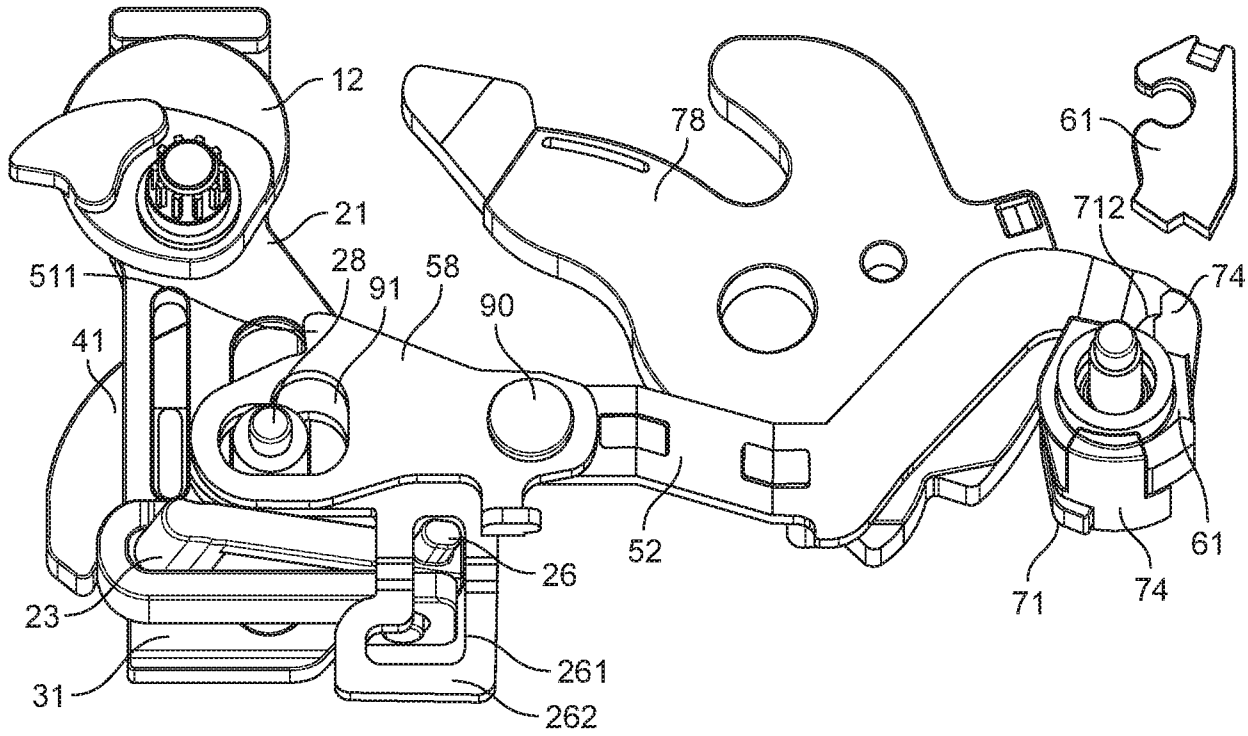


FIG. 10

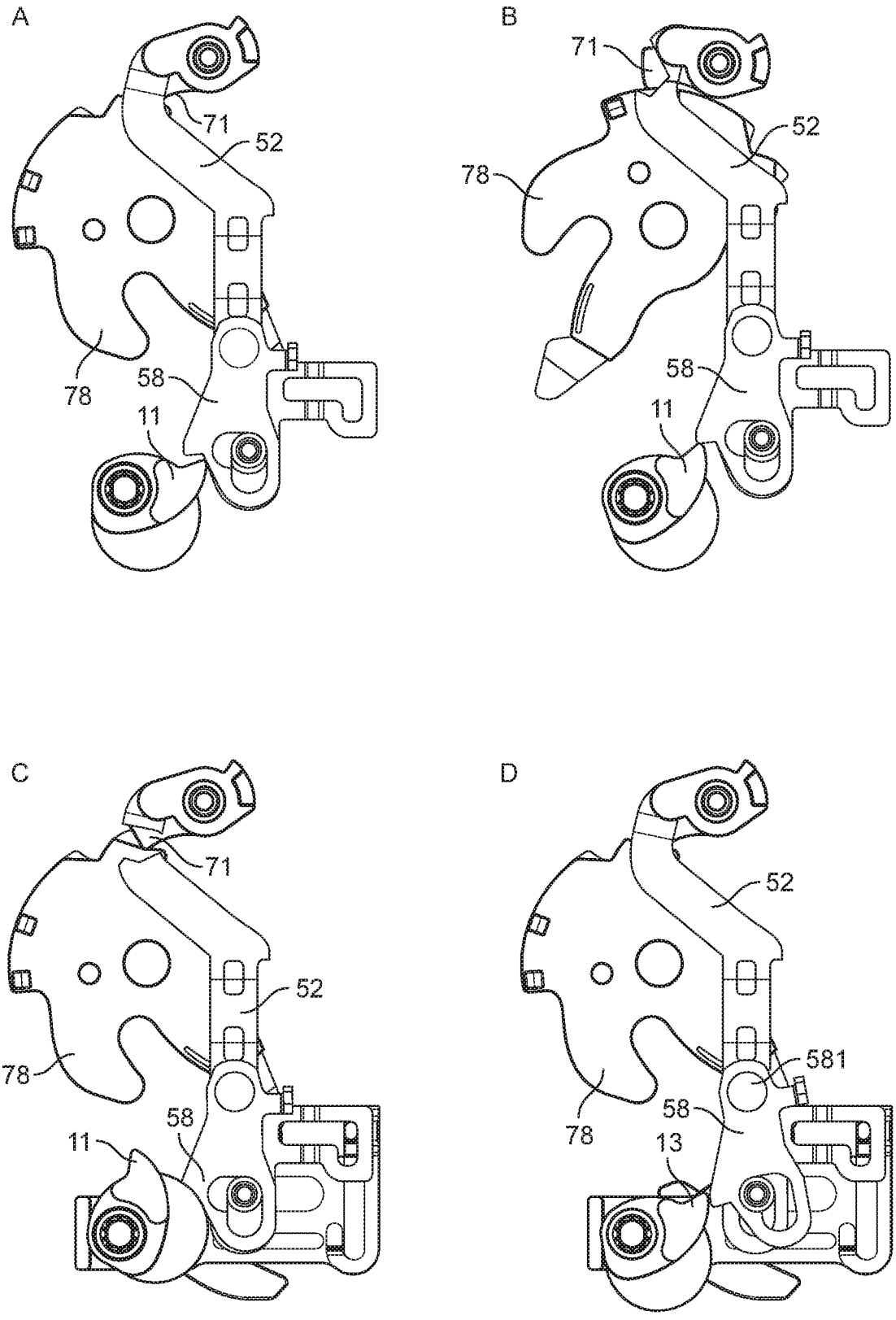


FIG. 11

INTERNATIONAL SEARCH REPORT

International application No
PCT/GB2015/051330

A. CLASSIFICATION OF SUBJECT MATTER
INV. E05B81/14 E05B81/20
ADD. E05B81/66 E05B81/90

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
E05B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 038 226 A1 (RENAULT [FR]) 21 October 1981 (1981-10-21) the whole document -----	1,9,10, 13
X	DE 10 2010 024295 A1 (BOECO BOEDDECKER & CO GMBH [DE]) 22 December 2011 (2011-12-22) paragraphs [0012] - [0014]; figures 2-5 paragraphs [0056] - [0069] -----	1-6
X	EP 1 746 230 A1 (ARVINMERITOR LIGHT VEHICLE SYS [GB]) 24 January 2007 (2007-01-24) paragraphs [0011] - [0023]; figures 6A-6D -----	1,7,8, 11,12

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

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"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
13 July 2015	20/07/2015

Name and mailing address of the ISA/	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Koster, Michael

5

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No
PCT/GB2015/051330

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