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LUBRICANT COMPOSITION FOR HOT-ROLLING OF STEEL

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(57) Claim

1. A lubricating composition for hot-rolling steel, which comprises a base oil and a heat-insulating agent incorporated therein, wherein (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7 are used as the heat insulating agent.

2. A lubricating composition for hot-rolling steel, which comprises a base grease and a heat-insulating agent incorporated therein, wherein (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and/or (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7 is used as the heat-insulating agent.

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6. A lubricating composition for hot-rolling steel (A) according to claim 1 or 2, wherein the heat-insulating agent is a member selected from the group consisting of condensed phosphoric acid salts, sodium silicate, chromic acid salts and halides.

7. A lubricating composition for hot-rolling steel according to claim 1 or 2, wherein the heat-insulating agent (B) is a member selected from the group consisting of boron nitride, silicon nitride, amorphous carbon, K_3PO_4 , $Ca_3(PO_4)_2$, bentonite, SiO_2 and ZnO .

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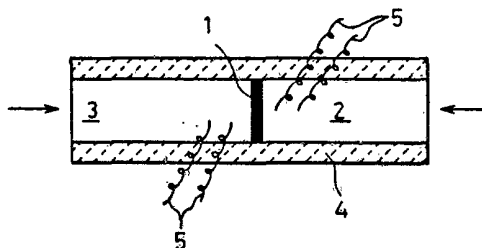
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(54) Title: LUBRICANT COMPOSITION FOR HOT-ROLLING OF STEEL

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(57) Abstract

The title lubricant composition comprises a base oil or base grease and a specified amount of a heat insulating agent comprising (A) an inorganic compound undergoing endothermic melting at temperatures of 1200°C or below and (B) an inorganic powder which neither melts nor decomposes at temperatures of 1200°C or below and which has a thermal conductivity of 0.01 cal/cm.s.°C or less and a friction coefficient of 0.7 or less at room temperature added alone or as a combination. This lubricant composition has an excellent heat-insulating effect and is effective in preventing occurrence of thermal crown of working rolls.

LUBRICATING COMPOSITION FOR HOT-ROLLING STEEL

TECHNICAL FIELD

The present invention relates to a lubricating composition for hot-rolling steel. More particularly, the present invention relates to a lubricating composition by which a transfer of heat to a work roll from a material to be rolled is prevented and the effect of reducing the thermal crown of the work roll is attained by incorporating a specific heat-insulating agent into a base oil or base grease.

BACKGROUND ART

In the conventional hot-rolling method, only roll-cooling water is used for protecting a roll, but now a rolling oil is used for reducing the rolling load and decreasing wear of the roll, and an excellent effect is attached thereby.

The main object of the conventional lubricant for hot rolling is to reduce wear of a work roll and improve the roll surface, because the requirement for the quality of a rolled product is relatively moderate and the thermal crown of the work roll is not regarded as important. Nevertheless, recently, an increased of the quality of the product has been demanded, and the effect of reducing the thermal crown of the work roll, which has an direct adverse influence on the quality of the product, has become important.

DISCLOSURE OF THE INVENTION

The present invention relates to a lubricant composition for hot-rolling steel, which is characterized in that a heat-insulating agent is incorporated into a base oil or base grease. More specifically, it was found that if two specific kinds of heat-insulating agents, i.e., (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C, and (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has



a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7, are incorporated singly or in combination in specific amounts in the composition, an excellent heat-insulating effect can be attained and the thermal crown of a work roll can be effectively prevented. The present invention was completed based on this finding.

In accordance with the first aspect of the present invention, there is provided a lubricating composition for hot-rolling steel, which comprises a base oil and a heat-insulating agent incorporated therein, wherein the above-mentioned components (A) and (B) are used as the heat-insulating agent. By incorporating the heat-insulating agents (A) and (B) having different properties in combination in the base oil, the heat-insulating effect can be increased by the synergistic effect of these heat-insulating agents.

In accordance with the second aspect of the present invention, there is provided a lubricating composition for hot-rolling steel, which comprises a base grease and a heat-insulating agent incorporated therein, and the above-mentioned component (A) and/or the above-mentioned component (B) is used as the heat-insulating agent. In this aspect, the base grease is used instead of the base oil, and the heat-insulating property is improved by the combination of the base grease with the component (A), the component (B) or the components (A) and (B). Since a grease has a low flowability at a high temperature, compared with an oil, a remarkable effect can be attained in the grease by the addition of the component (A) or (B) alone. If the components (A) and (B) are incorporated in combination, a highest effect can be attained due to the synergistic action of the two components.

In the above-mentioned lubricating composition for hot-rolling, by incorporating an extreme pressure additive and/or a solid lubricant together with the



heat-insulating agents (A) and (B), the lubricating property of the base oil can be further improved, and the lubricating property, heat-insulating property, storage stability, working property, and water washing resistance of the base grease can be further improved.

BRIEF DESCRIPTION OF THE DRAWING

Fig. 1 is a diagram illustrating the method of measuring the contact heat transfer ratio between metals.

BEST MODE OF CARRYING OUT THE INVENTION

The surface temperature of a work roll is elevated to about 800°C by contact with a material to be rolled. Most of the conventional lubricants for hot rolling comprise a mineral oil, an oiliness agent, an extreme pressure additive, and a solid lubricating agent, in combination, and although the lubricating property is taken into consideration, an insulation of heat (prevention of transfer of heat to the work roll from the material to be rolled) is not considered.

^{It is known}
~~Japanese Unexamined Patent Publication No. 60-6211~~
~~teaches~~ that a roll can be protected by adding a fine powder of an inorganic compound having a melting point lower than 1200°C under atmospheric pressure, an average particle size smaller than 1 μ m, and no corrosive action on iron and steel including cast iron and cast steel and other metals, and acting as a substance having a poor heat conductivity to a commercially available hot-rolling oil (liquid).

The base oil disclosed in this patent publication is a commercially available hot-rolling oil (liquid) and is different from the base grease used in the second embodiment of the present invention. Furthermore, the powder used in the invention of the above-mentioned patent publication is a powder of an inorganic compound which melts at a temperature lower than 1200°C, and the heat transfer-preventing effect is drastically reduced after melting.



In the present invention, where a liquid base oil is used, an inorganic compound melting at a temperature lower than 1200°C and an inorganic powder not melting or decomposing at a temperature lower than 1200°C are used
5 in combination, and where a base grease as semi-fluid grease having a higher heat-insulating property than that of the liquid base oil is used, two kinds of the inorganic powders are added singly or in combination, whereby the heat-insulating property is further
10 increased.

Namely, the heat-insulating agent used in the present invention includes (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and (B) an inorganic
15 powder which is not melted or decomposed at a temperature lower than 1200°C, is stable against oxidation and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7. As the inorganic compound
20 (A) which is melted by an absorption of heat at a temperature lower than 1200°C, there can be mentioned solid powders of condensed phosphoric acid salts such as KPO_3 , $NaPO_3$ and $K_4P_2O_7$, sodium silicate, chromic acid salts such as $K_2Cr_2O_7$, and halides such as NaCl, KCl,
25 KF, KBr and KI. Condensed phosphoric acid salts and sodium silicate, which have no corrosive action on a rolling mill or a material to be rolled, are especially preferable.

As the inorganic powder (B) which is not melted or
30 decomposed at a temperature lower than 1200°C, is stable against oxidation and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7, there can be used boron nitride, silicon nitride, amorphous carbon, K_3PO_4 ,
35 $Ca_3(PO_4)_2$, bentonite, SiO_2 and ZnO. The friction coefficient referred to herein is determined by the pin-on-disk method (a rod having a diameter of 3 mm and



a flat top end is pressed under a load of 1 kgf against a disk having a diameter of 11 mm, and the disk is slid at a speed of 0.01 m/s).

5 A heat-insulating agent having an average particle size smaller than 50 μm can be used, but in view of the clearance between the roll and the material to be rolled, preferably the average particle size of the heat-insulating agent is smaller than 10 μm .

10 The reason why better results are obtained when the inorganic compound (A), which is melted by an absorption of heat at a temperature lower than 1200°C and the inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C and a friction
15 coefficient smaller than 0.7 are used in combination, has not been completely elucidated, but it is considered that the reason is probably as follows. At the rolling step, the temperature and pressure become high in a roll bite (higher than 600°C and higher than 2000 kgf/cm²).
20 At this point, the heat-insulating agent (A) is promptly melted by absorption of heat and prevents heat from being transferred to the work roll from the material to be rolled. It is known that the heat conductivity of a liquid is, in general, increased more than that of a
25 powder. Accordingly, it is considered that the heat transfer-reducing effect of the heat-insulating agent (A) is abruptly decreased by melting. On the other hand, since the heat-insulating agent (B) is not melted or decomposed even under high-temperature and high-
30 pressure conditions, the heat-insulating agent (B) is present in the form of a powder in the roll bite and prevents the work roll from falling in contact with the material to be rolled, and it is considered that since the powder per se has a lubricating property, a
35 generation of heat by friction in the roll bite is reduced by the powder of the heat-insulating agent (B).

Namely, although the heat-insulating agent (A) has



an excellent heat-insulating property, when the heat-insulating agent (A) is melted at a high temperature, the heat-insulating property is drastically reduced. On the other hand, since the heat-insulating agent (B) is not melted or decomposed at a temperature lower than 1200°C, the heat-insulating agent (B) has a heat-insulating property over a broad temperature range. Accordingly, if the heat-insulating agent (A) and the heat-insulating agent (B) are made present at a specific ratio, a lubricating agent having the excellent effects of both heat-insulating agents (A) and (B) can be obtained.

Preferably, the heat-insulating agent is added in an amount of 5 to 50% by weight, especially 10 to 40% by weight. If the amount of the heat-insulating agent is smaller than 5% by weight, the heat-insulating effect is too low, and if the amount of the heat-insulating agent is larger than 50% by weight, the viscosity of the lubricant becomes too high and the oil-supplying property is degraded. Preferably, the ^{weight} ratio of the heat-insulating agent (A) to the heat-insulating agent (B) is in the range of 49/1 to 1/49, especially 19/1 to 1/4. This is because, if the proportion of the heat-insulating agent (A) is reduced, the heat-insulating property is lowered by an absorption of heat in the roll bite, and if the proportion of the heat-insulating agent (B) is reduced, the heat-insulating property at high temperature is lowered.

As the base oil that can be used in the present invention, there can be mentioned medium and heavy mineral oils such as spindle oil, machine oil, dynamo oil, motor oil, cylinder oil and bright stock, animal and vegetable oils such as beef tallow, lard, sperm oil, palm oil, coconuts oil, linseed oil, rice bran oil and soybean oil, synthetic oils such as esters of fatty acids having 8 to 22 carbon atoms with monohydric or polyhydric alcohols, α -olefins, polybutene, silicone



oils and fluorine oils, and mixtures of these oils.

As the base grease that can be used in the present invention, there can be mentioned lithium soap grease, calcium soap grease, sodium soap grease, aluminum soap grease, calcium complex grease, polyurea grease and organo-clay grease. Lithium soap grease, calcium complex grease, polyurea grease and organo-clay grease, which have an excellent heat resistance, are preferable.

As the solid lubricant that can be used in the present invention, there can be mentioned inorganic solid lubricants such as graphite (natural graphite and artificial graphite), molybdenum disulfide, mica (natural mica and artificial mica), fluorinated graphite, boron nitride, soft metals (such as gold, silver and copper) and talc, and organic solid lubricants such as PTFE (polytetrafluoroethylene), MCA (melamine/cyanuric acid adduct) and phthalocyanine. Graphite (natural graphite and artificial graphite), mica (natural mica and artificial mica), boron nitride and talc, which have an excellent heat resistance and oxidation stability at a high temperature and have no substantial influence on a material to be rolled, are preferably. Preferably the amount added of the solid lubricant is 0 to 40% by weight, especially 5 to 15% by weight. If the amount added of the solid lubricant exceeds 40% by weight, the viscosity of the lubricant becomes too high and the oil-supplying property is reduced.

As the extreme pressure additive that can be used in the present invention there can be mentioned sulfur compounds, phosphorus compounds, chlorine compounds and organic metal compounds. Preferably the amount added of the extreme pressure additive is 0 to 20% by weight, especially 0.5 to 10% by weight. If the amount added of the extreme pressure additive exceeds 20% by weight, undesired side effects such as an appearance of a corrosive action and reduction of the stability of the



micell structure of the grease occur.

The present invention will now be described in detail with reference to the following examples and comparative examples.

5 Examples 1 through 26 and Comparative Examples 1 through 5

 A base oil, a base grease, a heat-insulating agent, an extreme pressure additive, and a solid lubricant were mixed at a mixing ratio shown in Table 1, whereby
10 lubricating agents of Examples 1 through 26 and Comparative Examples 1 through 5 were prepared. With respect to each of the so-obtained compositions, the performances were evaluated according to the test methods described below. The results are shown in
15 Table 1.

 A) Lubricating Property Test by Hot Lubricating Property Tester Model E-12

 According to the principle of the hot lubricating property tester Model E-12, both ends of a
20 test piece were fixed and the test piece induction-heated gripped between rolls while supplying an oil to the test piece, and a slip lubrication effected. The friction coefficient and seizure resistance of each lubricant were examined to evaluate the lubricating
25 property.

$$\text{Friction coefficient } \mu = T/R \cdot W$$

 in which T represents a shaft torque, R represents a roll radius, and W represents a load. The outlines of the tester and the test conditions are as
30 follows.

 a) Type: lubricity tester of two-high type for slip lubricating

 b) Roll dimension: 124 mm (diameter) x 80 mm (length)

35 c) Roll material: high chromium roll (Hs = 70 - 75)

 d) Test piece material: SS-41 [20 mm



(height) x 20 mm (width) x 580 mm (length)]

e) Test piece temperature: 400°C, 600°C and 800°C (automatically adjusted)

f) Revolution: 200 rpm

5 g) Rolling load: 500 to 3000 kgf (the load is increased by 500 kgf at every time)

h) Method of supplying lubricant: applying

B) Rust Prevention Test

10 a) The test piece used at the test (A) was cut to a size of 20 mm x 20 mm x 100 mm.

b) The test piece prepared at a) above has hung under the eaves and allowed to stand for 2 weeks, and the state of rusting was checked.

o: no rusting

15 x: extreme rusting

C) Water Washing Resistance Test

a) A defatted and weighed steel sheet (SPCC-SD 100 mm x 100 mm x 0.8 mm) was uniformly coated with 30 ± 3 mg of the lubricant.

20 b) The steel sheet prepared at a) above was washed with water under the following conditions, and the weight was measured after the water washing and the residual oil ratio is determined.

a) Nozzle model number: 1/4 KBF 0865

25 b) Extrusion rate: 6.4 l/min
(extrusion pressure = 2.0 kgf/cm^2)

c) Water washing time: 5 seconds
(water temperature = 25°C)

30 d) Distance between steel sheet and nozzle: 200 mm

Residual oil or grease ratio (%) =
[(amount of residual oil or grease)/(amount coated of oil or grease)] x 100

35 D) Measurement of Contact Heat Transfer Ratio between Metals

a) Material of test piece: WT-60 [25 mm (diameter) x 50 mm (length)]



b) Temperature: 780°C (high-temperature material), 22 to 30°C (low-temperature material)

c) Thermocouple: CA (0.5 mm) sheath (attachment position = 1.5 mm, 3.0 mm)

5 d) Heat-insulating material: kao wool

e) Compressive force: 500 kgf/cm²

f) Method of filling sample and thickness:

As shown in Fig. 1, a high-temperature material 3 was pressed against a low-temperature material 2 coated with a sample 1, and the contact interface temperature of each sample and the heat flow flux were reckoned backward from the change of the temperatures of both materials with a lapse of time after the contact. The cooling law of Newton was applied in an extended manner to determine the heat transfer coefficient between the metals. The obtained coefficient was compared with the coefficient obtained when the sample is not coated, and the heat transfer ratio determined.

Note, in Fig. 1, reference numeral 4 represents a heat-insulating material and reference numeral 5 represents a thermocouple.

E) Roll Wearing Quantity Ratio in Actual Rolling Mill

Eight air spray nozzles (20 ml/min·nozzle) were attached to a work roll on the inlet side of F5 stand (6-stand mill), and about 300 tons of an ordinary material rolled by using nickel grain rolls. The wear quantity was measured and compared with the wear quantity observed when an oiling agent now available was used.





Table 1-1

		Example 1	Example 2	Example 3	Example 4	Example 5
Base Oil	mineral oil (ISO VG 430)	85		85	85	85
	synthetic oil (hydrocarbon type)		85			
Base Grease	lithium soap grease (mineral oil type)					
	lithium soap grease (synthetic oil type)					
	polyurea grease (mineral oil type)					
	calcium complex grease (mineral oil type)					
Heat-Insulating Agent	melting type (A)					
	(KPO ₃) _n	10	10	10	10	
	Na ₂ SiO ₄					10
	NaCl					
	non-melting type (B)					
	silicon nitride	5	5			5
	amorphous carbon			5		
	silicon dioxide				5	



Table 1-1 (Continued)

			Example 1	Example 2	Example 3	Example 4	Example 5
Extreme Pressure Additive	zinc dialkyl dithiophosphate						
	tricresyl phosphate						
	sulfurized lard						
Solid Lubricant	graphite (artificial)						
	mica (natural)						
	boron nitride						
	MCA						
Consistency Number (JIS K 2220)			-	-	-	-	-
E-12 Model Hot Lubricating Per- formance Test	400°C	load resistance (kgf)	2000	2000	2000	2000	2000
		μ under above load	0.18	0.18	0.18	0.18	0.18
	600°C	load resistance (kgf)	1000	1000	1000	1000	1000
		μ under above load	0.18	0.18	0.18	0.18	0.18
	800°C	load resistance (kgf)	500	500	500	500	500
		μ under above load	0.18	0.18	0.18	0.18	0.18



Table 1-1 (Continued)

	Example 1	Example 2	Example 3	Example 4	Example 5
Rust Prevention Test	0	0	0	0	0
Water Washing Resistance Test (residual oil or grease ratio; %)	45	46	45	44	46
Contact Heat Transfer Ratio between Metals	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8
Roll Wearing Ratio in Actual Rolling Mill	0.8 - 0.9	0.8 - 0.9	0.8 - 0.9	0.8 - 0.9	0.8 - 0.9



Table 1-2

		Example 6	Example 7	Example 8	Example 9	Example 10
Base Oil	mineral oil (ISO VG 430)	85	82	80	77	
	synthetic oil (hydrocarbon type)					
Base Grease	lithium soap grease (mineral oil type)					90
	lithium soap grease (synthetic oil type)					
	polyurea grease (mineral oil type)					
	calcium complex grease (mineral oil type)					
Heat- Insulating Agent	melting type (A)		10	10	10	10
	(KPO ₃) _n					
	Na ₂ SiO ₄					
	NaCl	10				
	non-melting type (B)	5	5	5	5	
	silicon nitride					
	amorphous carbon					
	silicon dioxide					



Table 1-2 (Continued)

			Example 6	Example 7	Example 8	Example 9	Example 10
Extreme Pressure Additive	zinc dialkyl dithiophosphate			3		3	
	tricresyl phosphate						
	sulfurized lard						
Solid Lubricant	graphite (artificial)				5	5	
	mica (natural)						
	boron nitride						
	MCA						
Consistency Number (JIS K 2220)			-	-	-	-	1
E-12 Model Hot Lubricating Per- formance Test	400°C	load resistance (kgf)	2000	2500	2500	3000	2000
		μ under above load	0.18	0.17	0.17	0.15	0.18
	600°C	load resistance (kgf)	1000	1500	2000	2000	1000
		μ under above load	0.18	0.16	0.16	0.15	0.18
	800°C	load resistance (kgf)	500	1000	1000	1500	500
		μ under above load	0.18	0.16	0.18	0.16	0.18



Table 1-2 (Continued)

	Example 6	Example 7	Example 8	Example 9	Example 10
Rust Prevention Test	x	o	o	o	o
Water Washing Resistance Test (residual oil or grease ratio; %)	46	47	60	60	80
Contact Heat Transfer Ratio between Metals	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8
Roll Wearing Ratio in Actual Rolling Mill	0.8 - 0.9	0.5 - 0.6	0.6 - 0.7	0.5 - 0.6	0.8 - 0.9



Table 1-3

		Example 11	Example 12	Example 13	Example 14	Example 15
Base Oil	mineral oil (ISO VG 430)					
	synthetic oil (hydrocarbon type)					
Base Grease	lithium soap grease (mineral oil type)	90	80	87	87	87
	lithium soap grease (synthetic oil type)					
	polyurea grease (mineral oil type)					
	calcium complex grease (mineral oil type)					
Heat- Insulating Agent	melting type (A)					
	(KPO ₃) _n		10	10	10	10
	Na ₂ SiO ₄					
	NaCl					
	non-melting type (B)					
	silicon nitride	10	10			
	amorphous carbon					
	silicon dioxide					



Table 1-3 (Continued)

		Example 11	Example 12	Example 13	Example 14	Example 15
Extreme Pressure Additive	zinc dialkyl dithiophosphate			3		
	tricresyl phosphate				3	
	sulfurized lard					3
Solid Lubricant	graphite (artificial)					
	mica (natural)					
	boron nitride					
MCA						
Consistency Number (JIS K 2220)		1	1	1	1	1
E-12 Model Hot Lubricating Per- formance Test	400°C load resistance (kgf)	2000	2500	3000	3000	3000
	μ under above load	0.18	0.18	0.14	0.14	0.14
	600°C load resistance (kgf)	1000	1500	2000	2000	2000
	μ under above load	0.18	0.17	0.17	0.17	0.17
	800°C load resistance (kgf)	500	1000	1500	1500	1500
	μ under above load	0.18	0.17	0.16	0.16	0.16



Table 1-3 (Continued)

	Example 11	Example 12	Example 13	Example 14	Example 15
Rust Prevention Test	0	0	0	0	0
Water Washing Resistance Test (residual oil or grease ratio; %)	80	85	81	81	81
Contact Heat Transfer Ratio between Metals	0.7 - 0.8	0.6 - 0.7	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8
Roll Wearing Ratio in Actual Rolling Mill	0.8 - 0.9	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8	0.7 - 0.8



Table 1-4

		Example 16	Example 17	Example 18	Example 19	Example 20
Base Oil	mineral oil (ISO VG 430)					
	synthetic oil (hydrocarbon type)					
Base Grease	lithium soap grease (mineral oil type)	85	85	85	85	77
	lithium soap grease (synthetic oil type)					
	polyurea grease (mineral oil type)					
	calcium complex grease (mineral oil type)					
Heat-Insulating Agent	melting type (A)	10	10	10	10	10
	(KPO ₃) _n					
	Na ₂ SiO ₄					
	NaCl					
	non-melting type (B)					10
	silicon nitride					
	amorphous carbon					
	silicon dioxide					



Table 1-4 (Continued)

		Example 16	Example 17	Example 18	Example 19	Example 20
Extreme Pressure Additive	zinc dialkyl dithiophosphate					
	tricresyl phosphate					
	sulfurized lard					
Solid Lubricant	graphite (artificial)	5				
	mica (natural)		5			
	boron nitride			5		
	MCA				5	
Consistency Number (JIS K 2220)		1	1	1	1	1
E-12 Model Hot Lubricating Performance Test	400°C load resistance (kgf)	3000	3000	3000	2500	3000
	μ under above load	0.15	0.14	0.14	0.18	0.15
	600°C load resistance (kgf)	2000	2000	2000	1500	3000
	μ under above load	0.18	0.18	0.18	0.18	0.15
	800°C load resistance (kgf)	1500	1500	1500	1000	2000
	μ under above load	0.17	0.17	0.17	0.17	0.17



Table 1-4 (Continued)

	Example 16	Example 17	Example 18	Example 19	Example 20
Rust Prevention Test	0	0	0	0	0
Water Washing Resistance Test (residual oil or grease ratio; %)	86	86	87	86	86
Contact Heat Transfer Ratio between Metals	0.6 - 0.7	0.6 - 0.7	0.6 - 0.7	0.7 - 0.8	0.6 - 0.7
Roll Wearing Ratio in Actual Rolling Mill	0.6 - 0.7	0.6 - 0.7	0.6 - 0.7	0.7 - 0.8	0.5 - 0.6



Table 1-5

		Example 21	Example 22	Example 23	Example 24	Example 25
Base Oil	mineral oil (ISO VG 430)					
	synthetic oil (hydrocarbon type)					
Base Grease	lithium soap grease (mineral oil type)	72	47			
	lithium soap grease (synthetic oil type)			72		
	polyurea grease (mineral oil type)				72	
	calcium complex grease (mineral oil type)					72
Heat- Insulating Agent	melting type (A)					
	(KPO ₃) _n	10	25	10	10	10
	Na ₂ SiO ₄					
	NaCl					
	non-melting type (B)					
	silicon nitride	10	10	5	5	5
	amorphous carbon					
	silicon dioxide					



Table 1-5 (Continued)

		Example 21	Example 22	Example 23	Example 24	Example 25
Extreme Pressure Additive	zinc dialkyl dithiophosphate	3	3	3	3	3
	tricresyl phosphate					
	sulfurized lard					
Solid Lubricant	graphite (artificial)	5	15	10	10	10
	mica (natural)					
	boron nitride					
	MCA					
Consistency Number (JIS K 2220)		1	2	1	1	1
E-12 Model Hot Lubricating Per- formance Test	400°C load resistance (kgf)	3000	3000	3000	3000	3000
	μ under above load	0.14	0.06	0.14	0.14	0.14
	600°C load resistance (kgf)	3000	3000	3000	3000	3000
	μ under above load	0.15	0.08	0.15	0.15	0.15
	800°C load resistance (kgf)	2500	3000	2000	2000	2500
	μ under above load	0.16	0.10	0.16	0.16	0.14



Table 1-5 (Continued)

	Example 21	Example 22	Example 23	Example 24	Example 25
Rust Prevention Test	0	0	0	0	0
Water Washing Resistance Test (residual oil or grease ratio; %)	87	93	87	89	87
Contact Heat Transfer Ratio between Metals	0.6 - 0.7	0.5 - 0.6	0.6 - 0.7	0.6 - 0.7	0.6 - 0.7
Roll Wearing Ratio in Actual Rolling Mill	0.5 - 0.6	0.2 - 0.3	0.3 - 0.4	0.3 - 0.4	0.3 - 0.4



Table 1-6

		Example 26	Compara- tive Example 1	Compara- tive Example 2	Compara- tive Example 3
Base Oil	mineral oil (ISO VG 430)		90		
	synthetic oil (hydrocarbon type)				
Base Grease	lithium soap grease (mineral oil type)			87	72
	lithium soap grease (synthetic oil type)				
	polyurea grease (mineral oil type)	90			
	calcium complex grease (mineral oil type)				
Heat- Insulating Agent	melting type (A)	(KPO ₃) _n	10	10	10
		Na ₂ SiO ₄			
		NaCl			
	non-melting type (B)	silicon nitride			
		amorphous carbon			
		silicon dioxide			nickel powder 10 (note 1)



Table 1-6 (Continued)

		Example 26	Compara- tive Example 1	Compara- tive Example 2	Compara- tive Example 3
Extreme Pressure Additive	zinc dialkyl dithiophosphate			3	3
	tricresyl phosphate				
	sulfurized lard				
Solid Lubricant	graphite (artificial)			10	5
	mica (natural)				
	boron nitride				
	MCA				
Consistency Number (JIS K 2220)			-	-	-
E-12 Model Hot Lubricating Per- formance Test	400°C load resistance (kgf)	2500	1500	2500	3000
	μ under above load	0.18	0.18	0.16	0.14
	600°C load resistance (kgf)	1500	500	1500	3000
	μ under above load	0.17	0.17	0.16	0.16
	800°C load resistance (kgf)	1000	500 >	1000	2500
	μ under above load	0.18	-	0.17	0.17



Table 1-6 (Continued)

	Example 26	Compara- tive Example 1	Compara- tive Example 2	Compara- tive Example 3
Rust Prevention Test	o	o	o	o
Water Washing Resistance Test (residual oil or grease ratio; %)	80	40	80	87
Contact Heat Transfer Ratio between Metals	0.7 - 0.8	0.9 - 1.0	0.9 - 1.0	0.8 - 0.9
Roll Wearing Ratio in Actual Rolling Mill	0.8 - 0.9	0.9 - 1.0	0.7 - 0.8	0.7 - 0.8

Note 1 heat conductivity = 0.22 cal/cm·s·°C
melting point = 1455°C



Table 1-7

		Compara- tive Example 4	Compara- tive Example 5	Compara- tive Example 6
Base Oil	mineral oil (ISO VG 430)	Commer- cial hot rolling oil (A) (oil used at present)	Commer- cial hot rolling oil (B) (contain- ing 10% of graphite)	lubri- cating agent not added
Base Grease	synthetic oil (hydrocarbon type)			
	lithium soap grease (mineral oil type)			
	lithium soap grease (synthetic oil type)			
	polyurea grease (mineral oil type)			
Heat- Insulating Agent	calcium complex grease (mineral oil type)			
	melting type (A)	(KPO ₃) _n Na ₂ SiO ₄ NaCl		
	non-melting type (B)	silicon nitride amorphous carbon silicon dioxide		



Table 1-7 (Continued)

			Compara- tive Example 4	Compara- tive Example 5	Compara- tive Example 6
Extreme Pressure Additive	zinc dialkyl dithiophosphate				
	tricresyl phosphate				
	sulfurized lard				
Solid Lubricant	graphite (artificial				
	mica (natural)				
	boron nitride				
	MCA				
Consistency Number (JIS K 2220)			-		-
E-12 Model Hot Lubricating Per- formance Test	400°C	load resistance (kgf)	500	2000	500 >
		μ under above load	0.10	0.08	-
	600°C	load resistance (kgf)	500	1000	500 >
		μ under above load	0.16	0.10	-
	800°C	load resistance (kgf)	500 >	500	500 >
		μ under above load	-	0.10	-



Table 1-7 (Continued)

	Compara- tive Example 4	Compara- tive Example 5	Compara- tive Example 6
Rust Prevention Test	0	0	0
Water Washing Resistance Test (residual oil or grease ratio; %)	31	55	-
Contact Heat Transfer Ratio between Metals	1	0.8 - 0.9	1
Roll Wearing Ratio in Actual Rolling Mill	1	0.5 - 0.6	1 <

Industrial Applicability

The lubricating composition of the present invention exerts an effect of reducing the thermal crown of a work roll, which has an influences on the quality of a product, in the field of hot rolling steel, and is especially valuable in this field.

5



CLAIMS

1. A lubricating composition for hot-rolling steel, which comprises a base oil and a heat-insulating agent incorporated therein, wherein (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7 are used as the heat insulating agent.

2. A lubricating composition for hot-rolling steel, which comprises a base grease and a heat-insulating agent incorporated therein, wherein (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and/or (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7 is used as the heat-insulating agent.

3. A lubricating composition for hot-rolling steel according to claim 1, wherein an extreme pressure additive and/or a solid lubricant is further added to the base oil in addition to the heat-insulating agents (A) and (B).

4. A lubricating composition for hot-rolling steel according to claim 2, wherein an extreme pressure additive and/or a solid lubricant is further added to the base grease in addition to the heat-insulating agent (A) and/or the heat-insulating agent (B).

5. A lubricating composition for hot-rolling steel according to claim 1 or 2, wherein the amount added of the heat-insulating agent is 5 to 50% by weight.

6. A lubricating composition for hot-rolling steel (A) according to claim 1 or 2, wherein the heat-



insulating agent is a member selected from the group consisting of condensed phosphoric acid salts, sodium silicate, chromic acid salts and halides.

5 7. A lubricating composition for hot-rolling steel according to claim 1 or 2, wherein the heat-insulating agent (B) is a member selected from the group consisting of boron nitride, silicon nitride, amorphous carbon, K_3PO_4 , $Ca_3(PO_4)_2$, bentonite, SiO_2 and ZnO .

10 8. A lubricating composition for hot-rolling steel according to claim 1 or 2, wherein the heat-insulating agents (A) and (B) are contained at a weight ratio of from 49/1 to 1/49.

15 9. A lubricating composition for hot-rolling steel according to claim 1 or 2, wherein the base oil is a member selected from the group consisting of spindle oil, machine oil, dynamo oil, motor oil, cylinder oil, bright stock, beef tallow, lard, sperm oil, palm oil, coconut oil, linseed oil, rice bran oil, soybean oil, esters of fatty acids having 8 to 22 carbon atoms with
20 monohydric and polyhydric alcohols, α -olefins, polybutene, silicone oils and fluorine oils.

10. A lubricating composition for hot-rolling steel according to claim 1 to 2, wherein the base grease
25 is a member selected from the group consisting of lithium soap grease, calcium soap grease, sodium soap grease, aluminum soap grease, calcium complex grease, polyurea grease and organo-clay grease.

11. A lubricating composition for hot-rolling steel according to claim ~~1 or 2~~³, wherein the solid
30 lubricant is a member selected from the group consisting of natural graphite, artificial graphite, molybdenum disulfide, natural mica, artificial mica, boron nitride, soft metals, talc, polytetrafluoroethylene, melamine/cyanuric acid adducts and phthalocyanine.

35 12. A lubricating composition for hot-rolling steel according to claim ~~1 or 2~~³, wherein the extreme pressure additive is a member selected from the group



consisting of sulfur compounds, phosphorus compounds, chlorine compounds and organic metal compounds.

13. A lubricating composition for hot-rolling steel substantially as hereinbefore described with reference to any one of Examples 1 to 26.

DATED this FOURTH day of MAY 1992

Nippon Steel Corporation, Kyodo Yushi Co., Ltd.

Patent Attorneys for the Applicant
SPRUSON & FERGUSON



LUBRICATING COMPOSITION FOR HOT-ROLLING STEEL

ABSTRACT OF THE DISCLOSURE

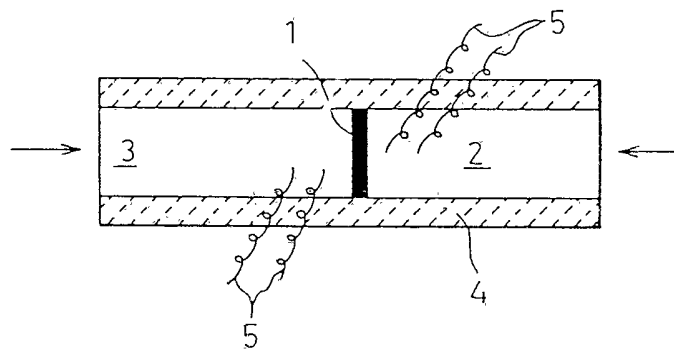
Disclosed is a lubricating composition for hot-rolling steel, which comprises a base oil or base grease and a heat-insulating agent. Especially, (A) an inorganic compound which is melted by an absorption of heat at a temperature lower than 1200°C and (B) an inorganic powder which is not melted or decomposed at a temperature lower than 1200°C and has a heat conductivity lower than 0.01 cal/cm.s.°C at room temperature and a friction coefficient smaller than 0.7 are incorporated in specific amounts singly or in combination in the composition. This lubricating composition has an excellent heat-insulating effect and effectively prevents the thermal crown of a work roll.



DRAWINGS

$\frac{1}{2}$

Fig.1



$2/2$

Explanation of Reference Numerals in the Drawing

- 1: sample
- 2: low-temperature material
- 3: high-temperature material
- 4: heat-insulating material
- 5: thermocouple

INTERNATIONAL SEARCH REPORT

International Application No PCT/JP89/00591

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ³		
According to International Patent Classification (IPC) or to both National Classification and IPC Int. Cl. ⁴ C10M141/10//B21B45/02, (C10M141/10, C10M125:02, C10M125:26, C10M125:24, C10M125:18), C10N10:02, C10N10:04, C10N40:24		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
IPC	C10M141/00 - 141/12, 169/04, 125/02, 125/26, 125/24, 125/18, C10N10:02, 10:04, 40:24	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ⁹		
Category [*]	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
Y	JP, A, 59-81394 (Kobe Steel, Ltd.) 11 May 1984 (11. 05. 84) Claim, page 3, lower left column, line 12 to lower right column, line 12 (Family : none)	1 - 12
Y	JP, A, 52-101363 (Origin Electric Co., Ltd.) 25 August 1977 (25. 08. 77) Claim, page 4, upper left column, line 12 to page 5, upper left column, line 19 (Family : none)	1 - 12
Y	JP, A, 58-1796 (Kobe Steel, Ltd.) 7 January 1983 (07. 01. 83) Claim, (amended claim, P. 6) (Family : none)	1 - 12
Y	JP, A, 60-6211 (Nippon Steel Corporation) 12 January 1985 (12. 01. 85) Claim, page 4, upper left column, line 2 to page 6, upper right column, line 2 (Family : none)	1 - 12
[*] Special categories of cited documents: ¹⁰ "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
September 6, 1989 (06. 09. 89)	September 18, 1989 (18. 09. 89)	
International Searching Authority	Signature of Authorized Officer	
Japanese Patent Office		

国 際 調 査 報 告

国際出願番号PCT/JP 89/ 00591

I. 発明の属する分野の分類		
国際特許分類 (IPC) Int. Cl. C10M141/10, B21B45/02, (C10M141/10, C10M125:02, C10M125:26, C10M125:24, C10M125:18), C10N10:02, C10N10:04, C10N40:24		
II. 国際調査を行った分野		
調 査 を 行 っ た 最 小 限 資 料		
分 類 体 系	分 類 記 号	
IPC	C10M141/00-141/12, 169/04, 125/02, 125/26, 125/24, 125/18, C10N10:02, 10:04, 40:24	
最小限資料以外の資料で調査を行ったもの		
III. 関連する技術に関する文献		
引用文献の カテゴリー※	引用文献名 及び一部の箇所が関連するときは、その関連する箇所の表示	請求の範囲の番号
Y	JP, A, 59-81394 (株式会社 神戸製鋼所) 11. 5月, 1984 (11. 05. 84) 特許請求の範囲, 第3頁左下欄第12行-右下欄 第12行 (ファミリーなし)	1-12
Y	JP, A, 52-101363 (オリジン電気株式会社) 25. 8月, 1977 (25. 08. 77) 特許請求の範囲, 第4頁左上欄第12行-第5頁左上欄 第19行 (ファミリーなし)	1-12
Y	JP, A, 58-1796 (株式会社 神戸製鋼所) 7. 1月, 1983 (07. 01. 83) 特許請求の範囲 (補正後のもの, 第6頁) (ファミリーなし)	1-12
Y	JP, A, 60-6211 (新日本製鐵株式会社)	1-12
※引用文献のカテゴリー 「A」 特に関連のある文献ではなく、一般的技術水準を示すもの 「E」 先行文献ではあるが、国際出願日以後に公表されたもの 「L」 優先権主張に疑義を提起する文献又は他の文献の発行日若しくは他の特別な理由を確立するために引用する文献 (理由を付す) 「O」 口頭による開示、使用、展示等に言及する文献 「P」 国際出願日前で、かつ優先権の主張の基礎となる出願の日の後に公表された文献 「T」 国際出願日又は優先日の後に公表された文献であって出願と矛盾するものではなく、発明の原理又は理論の理解のために引用するもの 「X」 特に関連のある文献であって、当該文献のみで発明の新規性又は進歩性がないと考えられるもの 「Y」 特に関連のある文献であって、当該文献と他の1以上の文献との、当業者にとって自明である組合せによって進歩性がないと考えられるもの 「&」 同一パテントファミリーの文献		
IV. 認 証		
国際調査を完了した日	国際調査報告の発送日	
06. 09. 89	18. 09. 89	
国際調査機関	権限のある職員	4H 8519
日本国特許庁 (ISA/JP)	特許庁審査官	守 安 智

第2ページから続く情報

(I 欄の続き)

12. 1月. 1985 (12. 01. 85)
 特許請求の範囲, 第4頁左上欄第2行—第6頁右上欄
 第2行 (ファミリーなし)

V. ☐ 一部の請求の範囲について国際調査を行わないときの意見

次の請求の範囲については特許協力条約に基づく国際出願等に関する法律第8条第3項の規定によりこの国際調査報告を作成しない。その理由は、次のとおりである。

1. ☐ 請求の範囲 _____ は、国際調査をすることを要しない事項を内容とするものである。
2. ☐ 請求の範囲 _____ は、有効な国際調査をすることができる程度にまで所定の要件を満たしていない国際出願の部分に係るものである。
3. ☐ 請求の範囲 _____ は、従属請求の範囲でありかつPCT規則6.4(a)第2文の規定に従って起草されていない。

VI. ☐ 発明の単一性の要件を満たしていないときの意見

次に述べるようにこの国際出願には二以上の発明が含まれている。

1. ☐ 追加して納付すべき手数料が指定した期間内に納付されたので、この国際調査報告は、国際出願のすべての調査可能な請求の範囲について作成した。
2. ☐ 追加して納付すべき手数料が指定した期間内に一部分しか納付されなかったので、この国際調査報告は、手数料の納付があった発明に係る次の請求の範囲について作成した。
請求の範囲 _____
3. ☐ 追加して納付すべき手数料が指定した期間内に納付されなかったので、この国際調査報告は、請求の範囲に最初に記載された発明に係る次の請求の範囲について作成した。
請求の範囲 _____
4. ☐ 追加して納付すべき手数料を要求するまでもなく、すべての調査可能な請求の範囲について調査することができたので、追加して納付すべき手数料の納付を命じなかった。

追加手数料異議の申立てに関する注意

- ☐ 追加して納付すべき手数料の納付と同時に、追加手数料異議の申立てがされた。
- ☐ 追加して納付すべき手数料の納付に際し、追加手数料異議の申立てがされなかった。