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(54) **Title:** MAGNETIC CORE WITH DISTRIBUTED GAP AND FLUX DENSITY OFFSET

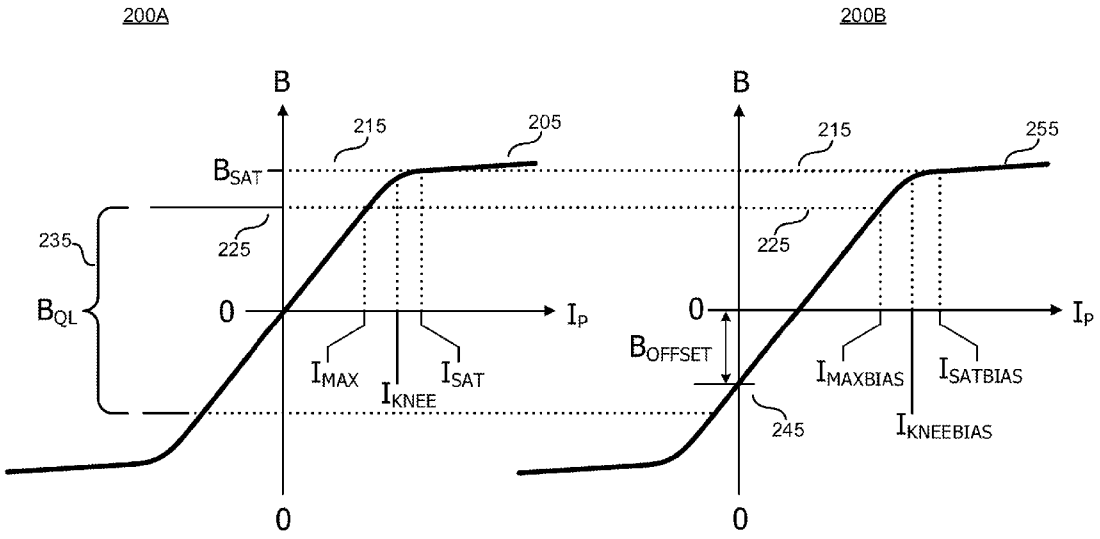

FIG. 2A FIG. 2B

(57) **Abstract:** An energy transfer element comprises a U-shaped core of powder core, the U-shaped core having two legs and a gap in a magnetic path, a bar comprising magnetizable material positioned in the gap such that the magnetic core and magnetizable material form a rectangular toroid, and one or more power windings wrapped around the magnetic path. The magnetizable material is capable of being magnetized. When the magnetizable material is unmagnetized, the magnetizable material has an initial flux density. When the magnetizable material is magnetized, the flux density produced by the magnetized material is offset from the initial flux density. The magnetizable material is an unmagnetized magnet or a suspension medium such as epoxy with magnetized magnetizable particles and powder core. The magnetizable particles are selected from a group comprising Neodymium Iron Boron (NdFeB) based materials or Samarium Cobalt (SmCo) based material.

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Magnetic Core with Distributed Gap and Flux Density Offset

CROSS REFEENCE TO RELATED APPLICATIONS

[001] This application claims priority under Article 8 of the Patent Cooperation Treaty (PCT) to U.S. Non-Provisional Application 17/137,823, filed December 30, 2020, the contents of which is incorporated in its entirety herein by reference.

BACKGROUND OF THE INVENTION

Field of the Invention

[002] The present invention relates generally to magnetic cores and more specifically to magnetic cores that may be used as energy transfer elements.

Discussion of the Related Art

[003] Electronic devices use power to operate. Switched mode power supplies are commonly used due to their high efficiency, small size and low weight to power many of today's electronics. Conventional wall sockets provide a high voltage alternating current. In a switching power supply, a high voltage alternating current (ac) input is processed by a switched mode power converter to provide a well-regulated direct current (dc) output through an energy transfer element. In operation, a switch is utilized to provide the desired output by varying the duty cycle, varying the switching frequency, or varying the number of pulses per unit time of the switch in a switched mode power converter.

[004] The energy transfer element for a switched mode power converter generally includes coils of wire wound around a core of material with relatively high magnetic permeability, e.g. ferrite or steel. For energy transfer elements such as transformers and coupled inductors, the energy transfer element can also include a structure called a bobbin or alternatively, a coil former, which provides support for the coils of wire and provides an area for the core to be inserted so the coils of wire can encircle a portion of the core. The core provides a path for a magnetic field generated by an electric current in the coils of wire. There is often a discrete region of relatively low

magnetic permeability introduced in the path of the magnetic field provided by the core, typically referred to as a gap. The length of the gap may be chosen to manage the distribution of energy in the energy transfer element. The material with relatively low magnetic permeability is typically air, and the gap is often referred to as an air gap, although the gap may contain other material with relatively low magnetic permeability, e.g. paper or varnish. In some compositions of magnetic core material, the gap is distributed uniformly throughout the material. The energy transfer element could also include a magnet, e.g. a permanent magnet, used with the core to provide flux density offset for the core of relatively high magnetic permeability material. The magnet could be inserted into the air gap of an energy transfer element. However, due to the changing magnetic fields of an energy transfer element, the permanent magnet may be susceptible to eddy currents. The eddy current can produce an undesirable power dissipation in the magnet. Furthermore, the inability to exactly match the thickness of the permanent magnet to the air gap dimensions may result in unacceptable tolerances and variability in the flux density offset rendering such schemes impractical in mass production of such energy transfer elements.

[005] Power supplies for electronic equipment may benefit from a magnetic energy transfer element that provides a flux density offset without excessive power loss in operation and may be manufactured at relatively low cost.

SUMMARY OF THE INVENTION

[006] An energy transfer element comprises a U-shaped core of powder core, the U-shaped core having two legs and a gap in a magnetic path, a bar comprising magnetizable material positioned in the gap such that the magnetic core and magnetizable material form a rectangular toroid, and one or more power windings wrapped around the magnetic path. The magnetizable material is capable of being magnetized. When the magnetizable material is unmagnetized, the magnetizable material has an initial flux density. When the magnetizable material is magnetized, the flux density produced by the magnetized material is offset from the initial flux density.

[007] The magnetizable material is an unmagnetized magnet or a suspension medium comprising epoxy with magnetized magnetizable particles and powder core. The

magnetizable particles are selected from a group comprising Neodymium Iron Boron (NdFeB) based materials or Samarium Cobalt (SmCo) based material.

[008] In one embodiment, the bar comprises magnetic material having a first and a second mitered end, and each leg of the U-shaped magnetic core has a mitered end such that the mitered ends of the bar mate to the mitered ends of the U-shaped magnetic core.

[009] In another embodiment, the bar that comprises magnetic material is positioned between the legs of the U-shaped magnetic core.

BRIEF DESCRIPTION OF THE DRAWINGS

[010] Non-limiting and non-exhaustive embodiments of the present invention are described with reference to the following figures, wherein like reference numerals refer to like parts throughout the various views unless otherwise specified.

[011] FIG. 1A and FIG. 1B illustrate the salient features of the construction of a prior art example energy transfer element that may be included in a power supply.

[012] FIG. 2A and FIG. 2B graphically illustrate the relationships between magnetic flux density in an energy transfer element and the current in a power winding of the energy transfer element.

[013] FIG. 3A and FIG. 3B illustrate the salient features of the core of an energy transfer element having unmagnetized and magnetized magnetic material in the gap.

[014] FIG. 4A and FIG. 4B illustrate the salient features of the construction of the energy transfer element on the cores of FIG. 3A and FIG. 3B that may be included in a power supply.

[015] FIG. 5 illustrates a cross-section of a magnetizer for magnetizing the energy transfer elements disclosed above.

[016] FIG. 6A and FIG. 6B illustrate the salient features of the construction of a powder core with distributed gap, showing one segment of the core that includes a magnetizable magnetic material that is magnetized after assembly.

[017] FIG. 7A and FIG. 7B illustrate the salient features of the construction of a powder core with distributed gap showing one portion of the core comprising particles of magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material.

[018] FIG. 8A and FIG. 8B illustrate the salient features of another construction of a powder core with distributed gap showing one portion of the core comprising particles of

magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material.

[019] FIG. 9A and FIG. 9B illustrate the salient features of yet another construction of a powder core with distributed gap showing one portion of the core comprising particles of magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material.

[020] FIG. 10A and FIG. 10B illustrate the salient features of the construction of a powder core with distributed gap showing multiple portions of the core comprising particles of magnetizable magnetic material that are magnetized and assembled.

[021] FIG. 11 illustrates a cross-section of a magnetizer for magnetizing a bar comprising magnetizable magnetic material prior to the assembly of the powder cores of FIGs. 7A-B, 8A-B, 9A-B, and 10A-B.

[022] FIG. 12 illustrates a cross-section of a magnetizer for magnetizing a bar comprising magnetizable magnetic material after assembly of a powder core in the geometry of FIG. 9B.

[023] FIG. 13 illustrates a cross-section of a magnetizer for magnetizing a bar comprising magnetizable magnetic material after assembly of the powder core illustrated in FIGs. 6A-B.

[024] FIG. 14A and FIG. 14B illustrate the salient features of the construction of a prior art example energy transfer element that may be included in a power supply.

[025] FIG. 15A and FIG. 15B illustrate the salient features of the construction of an energy transfer element having unmagnetized magnetic material in the gap.

[026] FIG. 16 illustrates a flowchart 1600 to assemble the energy transfer element 1500A, 1500B shown in FIGs. 1500A and 1500B, respectively.

[027] FIGs. 17A – 17F illustrate the salient features of the construction of an energy transfer element having unmagnetized magnetic material in the gap.

[028] FIG. 18 illustrates a flowchart 1800 to assemble the energy transfer element shown in FIGs. 17A – 17F.

[029] FIGs. 19A – 19F illustrate the salient features of the construction of an energy transfer element having unmagnetized magnetic material, where the thickness of the magnetic material is less than or equal to the gap.

[030] FIG. 20 illustrates a flowchart 2000 to assemble the energy transfer element shown in FIGs. 19A – 19F.

[031] FIGs. 21A – 121F illustrate the salient features of the construction of an energy transfer element having unmagnetized magnetic material in the gap having a thickness greater than the gap.

[032] FIG. 22 illustrates a flowchart 2200 to assemble the energy transfer element shown in FIGs. 21A – 21F.

[033] FIGs. 23A – 23F illustrate the salient features of the construction of an energy transfer element having deformable unmagnetized magnetic material in the gap.

[034] FIG. 24 illustrates a flowchart 2400 to assemble the energy transfer element shown in FIGs. 23A – 23F.

[035] FIG. 25 illustrates a cross-section of a magnetizer 2500 for magnetizing the energy transfer elements disclosed above.

[036] Corresponding reference characters indicate corresponding components throughout the several views of the drawings. Skilled artisans will appreciate that elements in the figures are illustrated for simplicity and clarity and have not necessarily been drawn to scale. For example, the dimensions of some of the elements in the figures may be exaggerated relative to other elements to help to improve understanding of various embodiments of the present invention. Also, common but well-understood elements that are useful or necessary in a commercially feasible embodiment are often not depicted in order to facilitate a less obstructed view of these various embodiments of the present invention.

DETAILED DESCRIPTION

[037] In the following description, numerous specific details are set forth in order to provide a thorough understanding of the present invention. It will be apparent, however, to one having ordinary skill in the art that the specific detail need not be employed to practice the present invention. In other instances, well-known materials or methods have not been described in detail in order to avoid obscuring the present invention.

[038] Reference throughout this specification to "one embodiment", "an embodiment", "one example" or "an example" means that a particular feature, structure or characteristic described in connection with the embodiment or example is included in at least one

embodiment of the present invention. Thus, appearances of the phrases "in one embodiment", "in an embodiment", "one example" or "an example" in various places throughout this specification are not necessarily all referring to the same embodiment or example. Furthermore, the particular features, structures or characteristics may be combined in any suitable combinations and/or subcombinations in one or more embodiments or examples. Particular features, structures or characteristics may be included in an integrated circuit, an electronic circuit, a combinational logic circuit, or other suitable components that provide the described functionality. In addition, it is appreciated that the figures provided herewith are for explanation purposes to persons ordinarily skilled in the art and that the drawings are not necessarily drawn to scale.

[039] It will be appreciated by those skilled in the art that magnetic assemblies and parts of magnetic assemblies may be described by various terms that are not necessarily technically accurate nor precise. For example, virtually any piece of magnetic material may be referred to as a magnetic core. A complete assembly of pieces of magnetic components exclusive of windings may also typically be referred to as a magnetic core.

[040] One prior art method for increasing the energy storage capability of inductors operating in dc applications is permanent magnet biasing. Typically, magnetized permanent magnets are placed into the air gap before core pieces are assembled around coils of wire. Alternatively, magnetized permanent magnets may be attached to exterior surfaces of an energy transfer element after the core and coils are assembled.

[041] FIG. 1A and FIG. 1B illustrate the salient features of the construction of a prior art example energy transfer element that may be included in a power supply. FIG. 1A is a top view 100A that shows a toroidal magnetic core 110 having a primary winding 115_1 and a secondary winding 115_2. The magnetic path within the toroidal magnetic core 110 includes a gap of distance d. B_W indicates the magnetic flux density from the magnetic field for the equivalent power winding current, e.g. the summation of each current, I_1 and I_2, applied through the number of turns of its corresponding winding, typically referred to as the ampere-turns. The total magnetic flux density from the magnetic field produced by the windings is B_W. FIG. 1B is a top view 100B that shows a permanent magnet 115 inserted into the gap. B_M indicates the magnetic

flux density from the permanent magnet 115 and is in opposition to the flux density B_W from the windings. The net magnetic flux density is the difference in magnitudes of the opposing flux densities, $B_W - B_M$.

[042] FIG. 2A and FIG. 2B graphically illustrate the relationships between magnetic flux density in an energy transfer element and the current in a power winding of the energy transfer element. FIG. 2A is a graph 200A that shows magnetic flux density plotted on the vertical axis with respect to an equivalent power winding current on the horizontal axis. The equivalent power winding current may be the sum of the ampere-turns in the windings of an energy transfer element. In the structure in FIG. 2A, for example, the current multiplied by the number of turns of winding 115_1 plus the current I_2 multiplied by the number of turns of winding 115_2 at any time would be the sum of the ampere-turns at that time. Current in the direction indicated by the arrow at the winding has a positive value, whereas current in the opposite direction has a negative value.

[043] The materials with relatively high magnetic permeability, e.g. 1000 or more times the permeability of free space μ_0, used in energy transfer elements typically have negligible flux density when there is no current to produce a magnetic field. As such, they are not considered to be permanently magnetized, and they do not exhibit properties that we would typically expect of permanent magnets. Therefore, the relationships between magnetic flux density and current in FIG. 2A and FIG. 2B are single-valued, having only one value of flux density on the vertical axis for each value of current on the horizontal axis. These materials are considered not magnetized, and they cannot be permanently magnetized.

[044] Materials for permanent magnets typically have multi-valued relationships between magnetic flux density and the magnetic field from an equivalent current. Exposure to a sufficiently strong magnetic field may change the state of the material from a first state or initial flux density, e.g. negligible flux density, to a second state that retains a relatively high magnetic flux density after the equivalent current is returned to zero. A material in the second state may be considered a permanent magnet that may introduce a desired flux density offset in an energy transfer element. These materials may be either magnetized or not magnetized, depending on their exposure to a magnetic field.

[045] The example energy transfer element for the graph of FIG. 2A has no flux density offset from a permanent magnet, so the flux density is at zero when the current is at zero. The magnetic flux density curve 205 in FIG. 2A highlights several distinguishing features. The curve 205 takes on positive and negative values with symmetry about the origin on both axes. There is positive flux density for positive current and negative flux density for negative current. Features are emphasized for positive values of current in the graph because the equivalent current in typical energy transfer elements is in only one direction. As the current I_P increases from zero, the energy transfer element operates in a quasi-linear region B_{QL} 235 until the current reaches a maximum value I_{MAX} that corresponds to the upper boundary 225 of the quasi-linear region. The slope of the curve 205 in the quasi-linear region 235 is positive and relatively constant. In other words, the flux density increases with increasing current at a nearly constant ratio. As the current increases beyond I_{MAX}, the slope of the flux density curve 205 decreases, reaching a lower relatively constant value for currents greater than a saturation current I_{SAT} that corresponds to a saturation flux density B_{SAT} 215. Operation at higher values of flux density is likely to produce current that may damage switching devices and other components in a power supply. As the slope of the curve 205 changes from its nearly constant value in the quasi-linear region B_{QL} 235 where the current is less than I_{MAX} to its much lower nearly constant value where the current is greater than I_{SAT}, there is region where the slope is changing rapidly between the two nearly constant values. The current between I_{MAX} and I_{SAT} where the slope of the flux density is changing most rapidly is identified as I_{KNEE} since it corresponds to the relatively sharp bend in the flux density curve 205.

[046] FIG. 2B is a graph 200B that shows magnetic flux density plotted on the vertical axis with respect to a power winding current I_P on the horizontal axis. In contrast to the graph of FIG. 2A, the example energy transfer element for the graph of FIG. 2B has a flux density offset from a permanent magnet.

[047] The flux density offset from the permanent magnet shifts the curve 205 of FIG. 2A to the right on the horizontal axis as shown by the curve 255 in FIG. 2B. The values on the vertical axis for the saturation flux density B_{SAT} 215 and the quasi-linear region B_{QL} 235 are unchanged because they are intrinsic properties of the magnetic material of the core. A flux density offset can change the relationship between the flux density

and an external stimulus, but it cannot change the intrinsic properties of the magnetic material. The flux density offset from a permanent magnet, such as for example one that may be placed in the gap of the assembly illustrated in FIG. 2A, is shown in FIG. 2B as B_M that produces a negative flux density 245 in the energy transfer element when the current I_P on the horizontal axis is zero.

[048] The flux density offset increases the values of the current I_P required to reach the upper boundary 225 of the quasi-linear region B_{QL} 255, the saturation value B_{SAT} 215, and the flux density where the slope of the curve is changing most rapidly. In other words, currents I_{MAX}, I_{SAT}, and I_{KNEE} of FIG. 2A are respectively increased to $I_{MAXBIAS}$, $I_{SATBIAS}$, and $I_{KNEEBIAS}$ in FIG. 2B. Therefore, an energy transfer element that uses a core with a permanent magnet to provide a flux density offset may store and transfer more energy for a given maximum current than the energy transfer element with no permanent magnet. This disclosure describes materials and methods to introduce permanent magnets into magnetic paths of energy transfer elements.

[049] FIG. 3A and FIG. 3B illustrate the salient features of the construction of a magnetic core for an energy transfer element having unmagnetized and magnetized magnetic material in the gap. FIG. 3A is a top view 300A that shows a toroidal magnetic core 310 prior to magnetization. The magnetic path of the toroidal magnetic core 310 includes a gap of distance d. Unmagnetized magnetic material 320 is positioned in the gap. FIG. 3B is a top view 300B that shows after magnetization, the magnetic material 320 introduces the magnetic field B_M into the magnetic path of the magnetic core that may be used in an energy transfer element.

[050] FIG. 4A and FIG. 4B illustrate the salient features of the construction of an energy transfer element from the cores of FIGs. 3A and 3B that may be included in a power supply. FIG. 4A is a top view 400A that shows a toroidal magnetic core 410, prior to magnetization, having a primary winding 415_1 and a secondary winding 415_2. The magnetic path of the toroidal magnetic core 410 includes a gap of distance d. B_W indicates the magnetic flux density for the equivalent power winding current, e.g. the summation of each current, I_1 and I_2, applied through its corresponding winding.

[051] FIG. 4B is a top view 400B that shows after magnetization, the magnetic material 420 introduces the permanent magnetic field B_M into the magnetic path of the transfer element. The total magnetic flux density is the difference $B_W - B_M$.

[052] FIG. 5 illustrates a cross-section of a magnetizer for magnetizing the energy transfer elements disclosed above. The energy transfer element is placed inside the solenoid magnetizing fixture. The solenoid magnetizing fixture 500 is a double-walled cylinder 530 that sandwiches a solenoid conductor, e.g. a coil of wire, 540 between the walls. A current source 520 applies a current that is passed through the solenoid conductor to generate a magnetic field of a magnitude suitable to magnetize the permanent magnet material. In one example the permanent magnet material could comprise rare earth magnetic materials such as Neodymium Iron Boron (NdFeB), Samarium Cobalt (SmCo) or the like. For NdFeB materials, the magnetic field is typically greater than 3 tesla.

[053] Magnetic cores can be fabricated from a homogeneous mixture of particles that comprise relatively high permeability material and relative low permeability material. When cast into a desired shape, the result is a core that has an air gap distributed uniformly through its volume. Cores of this composition are referred to as "powder cores" because the mixture is initially in the form of a powder. Energy transfer elements assembled from powder cores that have a distributed gap require no additional discrete air gap. Although powder cores may be procured in the same standard shapes and geometries as styles that have high magnetic permeability, it is common to cast the pieces into the form of a toroid that has no discrete gap.

[054] The magnetic material in powder cores typically has relatively low residual flux density, and therefore they have negligible permanent magnetism. To obtain the benefits associated with a dc flux density offset in an energy transfer element or in an inductor in a filter element, the mixture may include a powder of a rare earth alloy with permanent magnet properties such as NdFeB or SmCo.

[055] The core may be cast with unmagnetized particles in the powder as usual. After the shape is cast, it may be magnetized with a current through a conductor that passes through an aperture in the core. It would not be sufficient to immerse either the core alone or the assembled energy transfer element in a magnetic field for magnetization since the permanent magnets are not localized to one small section of the core.

[056] A toroid, for example needs to have the flux density offset in a direction that is everywhere perpendicular to the radius of the toroid. In other words, the magnetic flux density from the permanent magnet must be parallel to the magnetic field from

the current in the windings. The core may be magnetized after it is assembled into an energy transfer element by passing sufficient current through a winding. Alternatively, the core may be magnetized before it is assembled into an energy transfer element by temporarily establishing a high current that passes through the aperture of the toroid.

[057] It is not necessary for the geometry of the core to be a toroid with circular inner and outer circumferences. The powder core that contains permanent magnet material may be any shape that provides a closed magnetic path and an aperture for a conductor of current.

[058] For purposes of illustration, the elements comprising only powder core are shown in the square pattern fill while elements that include magnetizable magnetic material are shown in the diamond pattern fill. The magnetizable magnetic material may be a mixture that contains particles of a binding compound such as for example epoxy and magnetic powder or a powder core material that further includes nonmagnetizable magnetic powder.

[059] FIG. 6A and FIG. 6B illustrate the salient features of the construction of a core for an energy transfer element having unmagnetized magnetizable magnetic material and the composition of a powder core. FIG. 6A is a top view 600A that shows a U-shaped core 610 made from powder core. A bar 605comprising unmagnetized magnetizable magnetic material as well as the same nonmagnetizable material as in the U-shaped core 610 is positioned across the legs of the U-shaped magnetic core. FIG. 6B is a top view 600B that shows after assembly and magnetization, the magnetic material 615 is in the magnetic path of the U-shaped magnetic core. In practice, the magnetic flux density is not completely confined within the boundaries of the core, and some of the magnetic field will extend past the boundary defined by the U-shape.

[060] FIG. 7A and FIG. 7B illustrate the salient features of the construction of a powder core with distributed gap showing one portion of the core comprising particles of magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material. FIG. 7A is a top view 700A that shows a U-shaped magnetic core 710 and a bar of powder core containing magnetized magnetic material 715. FIG. 7B is a top view 700B that shows after assembly, the bar of powder core containing magnetized magnetic material 715 spans the legs of the U-

shaped magnetic core. The structure 720 shows a closed magnetic path formed by the bar 715 and the U-shaped magnetic core 710. Since the magnetic flux density from the permanent magnet tends to extend linearly from the ends of the bar, the construction that spans the legs of the U-shaped portion is not optimum for inserting the flux density into the path of the field from the windings. Alternative constructions may be more effective in inserting the magnetic flux density from the bar section into the U-shaped section.

[061] FIG. 8A and FIG. 8B illustrate the salient features of another construction of a powder core with distributed gap showing one portion of the core comprising particles of magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material. FIG. 8A is a top view 800A that shows a U-shaped magnetic core 810 and a bar comprising magnetized magnetic material 825. FIG. 8B shows a top view 800B where the bar of powder core containing magnetized magnetic material 825 interposes the legs of the U-shaped magnetic core. The structure 835 shows a closed magnetic path formed by the bar 825 and the U-shaped magnetic core 810. The magnetic path is within the boundary defined by the U-shape.

[062] FIG. 9A and FIG. 9B illustrate the salient features of yet another construction of a powder core with distributed gap showing one portion of the core comprising particles of magnetizable magnetic material that is magnetized and assembled with another portion of the core having no magnetizable material. FIG. 9A is a top view 900A that shows a U-shaped powder core 910 having mitered corners and a bar of powder core containing magnetized magnetic material having mitered ends 925. FIG. 9B shows a top view 900B where the bar of powder core containing magnetized magnetic material 925 interposes the legs of the U-shaped powder core 910. The structure 935 shows a closed magnetic path formed by the bar 925 and the U-shaped magnetic core 910. The magnetic path is within the boundary defined by the U-shape.

[063] FIG. 10A and FIG. 10B illustrate the salient features of the construction of a powder core with distributed gap showing multiple portions of the core comprising particles of magnetizable magnetic material that are magnetized and assembled. FIG. 10A shows each side of the core is a bar of magnetic material 1045, 1065, 1060, 1070 formed from powder core that includes magnetizable powder. Each bar has a mitered

end 1045, 1065, 1060, 1070 that mates to the surface of the end of an adjacent bar. The FIG. 10B is a top view 1000B that shows an assembled four-sided magnetic core structure 1075. The structure 1075 shows a closed magnetic path formed by the bars the U-shape.

[064] FIG. 11 illustrates a cross-section of a magnetizer for magnetizing a bar of magnetizable magnetic material prior to the assembly of the cores of FIGs. 7A-B, 8A-B, 9A-B, and 10A-B. The energy transfer element is placed inside the solenoid magnetizing fixture. The solenoid magnetizing fixture 1100 is a double-walled cylinder 1110 that sandwiches a solenoid conductor, e.g. a coil of wire, 1115 between the walls. A current source 1120 applies a current that is passed through the solenoid conductor to generate a magnetic field of a magnitude suitable to magnetize the bar of magnetic material.

[065] FIG. 12 illustrates a cross-section of a magnetizer for magnetizing a bar of magnetizable magnetic material after assembly of the energy transfer element of FIGs. 9A-B. The assembled energy transfer element is placed inside the solenoid magnetizing fixture. In the example of FIG. 12, the bar comprising magnetizable material is oriented such that after magnetization, the north pole N is upward and the south pole S is downward. The solenoid magnetizing fixture 1200 is a double-walled cylinder 1210 that sandwiches a solenoid conductor, e.g. a coil of wire, 1215 between the walls. A current source 1220 applies a current that is passed through the solenoid conductor to generate a magnetic field of a magnitude suitable to magnetize the bar of magnetic material.

[066] FIG. 13 illustrates a cross-section of a magnetizer for magnetizing a bar comprising magnetizable magnetic material after assembly of the energy transfer element of FIGs. 6A-B. The assembled energy transfer element is placed inside the solenoid magnetizing fixture. The bar comprising magnetizable material is oriented such that after magnetization, the north pole N is upward and the south pole S is downward. The solenoid magnetizing fixture 1300 is a double-walled cylinder 1310 that sandwiches a solenoid conductor, e.g. a coil of wire, 1315 between the walls. A current source 1320 applies a current that is passed through the solenoid conductor to generate a magnetic field of a magnitude suitable to magnetize the bar of magnetic material.

[067] FIG. 14A and FIG. 14B illustrate the salient features of the construction of a prior art example energy transfer element that may be included in a power supply. FIG. 14A is a perspective view 1400A that shows an upper core piece, e.g. an upper magnetic core-half 1405, assembled over a lower core piece, e.g. a lower magnetic core-half 1415. Each magnetic core-half has a center post 1425 surrounded by a winding 1418 that represents one or more power windings. In a practical component, the turns of the power windings typically would be placed on a separate spool, sometimes referred to as a bobbin or a coil former, that would fit over the center posts to facilitate assembly. FIG. 14A shows a gap 1445 in the center post 1425 of the assembled core-halves. The dimension of the gap is typically selected along with the number of turns on the power windings to set the electrical parameters desired for a particular application.

[068] FIG. 14B is a cross-sectional view 1400B of the prior art example energy transfer element of FIG. 14A with the upper core-half 1405 and lower core-half 1415 having two power windings 1418_1, 1418_2. The primary power winding 1418_1 is represented by the smaller circles wrapped closest to the spool of the bobbin. The secondary power winding 1418_2 is represented by the large circles which are wrapped on the bobbin 1435 over the primary power winding.

[069] It will be appreciated by those skilled in the art that magnetic assemblies and parts of magnetic assemblies may be described by various terms that are not necessarily technically accurate nor precise. For example, virtually any piece of magnetic material may be referred to as a magnetic core. A complete assembly of pieces of magnetic components exclusive of windings may also typically be referred to as a magnetic core. Assemblies of magnetic cores typically comprise two core pieces. In many assemblies of magnetic cores, such as in the example of FIG. 14A, the two core pieces may be nearly identical. Hence, each core piece may be commonly referred to as a core member or core-half. In practice, the gap in a center post 1425 in the assembly of FIG. 14A for example, may be formed by removing material from the center post of only one of two identical core-halves. Each piece is still referred to as a core-half even though the piece that forms the gap is no longer identical to the piece that had no material removed. The assembly may be further referred to as a core pair. In this disclosure the term core-half may be used to refer to one of two nearly

identical pieces, for example 1405 and 1415, in an assembly to distinguish the assembly from alternative assemblies comprising pieces that are obviously not identical. For example, an assembly of two E-shaped pieces such as 1405 and 1415 may have the same geometrical features and magnetic properties as an assembly that uses one E-shaped piece with one I-shaped piece. The EE assembly comprises two core-halves whereas the EI assembly does not, although each assembly comprises two core members. It is noted that in the practice of the art each one of a magnetic core piece, a magnetic core member, a magnetic core element, a magnetic core-half, and a magnetic core assembly may be referred to as a magnetic core which does not imply any permanent magnet properties of the core but typically refers to the core material having relatively high magnetic permeability. The magnetic energy transfer element of FIG 14 can therefore be described as having a magnetic flux path comprising a region of relatively high magnetic permeability core material and a gap region having a low permeability which will be close to the permeability of free space.

[070] FIG. 15A and FIG. 15B illustrate the salient features of the construction of an energy transfer element having unmagnetized magnetic material in the gap. The gap is within an optional center post. FIG. 15A is a perspective view 1500A that shows an upper core piece, e.g. an upper magnetic core-half 1505, assembled over a lower core piece, e.g. a lower magnetic core-half 1515. In combination, the magnetic core halves form a center post 1525 surrounded by a winding 1518 that represents one or more power windings. In a practical component, the turns of the power windings typically would be placed on a separate spool, sometimes referred to as a bobbin or a coil former, that would fit over the center posts to facilitate assembly. FIG. 15A shows unmagnetized magnetic material in the center post of the assembled core-halves. The dimension of the gap is typically selected along with the number of turns on the power windings to set the electrical parameters desired for a particular application.

[071] FIG. 15B is a cross-sectional view 1500B of an example energy transfer element using the construction of FIG. 15A with the upper core-half 1505 and lower core-half 1515 having two power windings. The smaller circles wrapped closest to the spool of the bobbin represent a primary power winding. The large circles represent a secondary power winding that is wrapped over the primary winding on the spool of the bobbin. The unmagnetized magnetic material 1545 fills the region of the gap

between the upper core-half 1505 and the lower core-half 1515.

[072] There may be an optional varnish coating (not shown) to seal the assembly.

[073] The assembled energy transfer element 1500A, 1500B may be subject to an external magnetic field to permanently magnetize the magnetizable material 1545 in the gap.

[074] The magnetizable material may be a suspension mixture that contains magnetizable powder along with a suspension medium which can be an adhesive or epoxy or be an unmagnetized magnet.

[075] FIG. 16 illustrates a flowchart 1600 to assemble the energy transfer element 1500A, 1500B shown in FIGs. 1500A and 1500B, respectively.

[076] In step 1602, the cores are prepared with a desired gap in the magnetic path.

[077] In step 1604, the bobbin is prepared with windings.

[078] In step 1606, the unmagnetized material is applied to the gap between a set of cores.

[079] In step 1608, the bobbin with windings is fit to the core.

[080] The order of steps 1606 and 1608 are interchangeable.

[081] In step 1610, the energy transfer element is assembled.

[082] In step 1612, the cores are secured.

[083] In step 1614, the energy transfer assembly is magnetized.

[084] FIGs. 17A – 17F illustrate the salient features of the construction of an energy transfer element 1700 having unmagnetized magnetic material in the gap between two core halves wherein the finished assembly in FIG.17F is ready for magnetizing in accordance with the teachings of the present invention.

[085] FIG. 17A illustrates a cross-section of a set of cores with a gap.

[086] FIG. 17B illustrates a cross-section of a bobbin with windings. The primary power winding is reflected by the smaller circles wrapped closest to the spool of the bobbin. The secondary power winding is reflected by the large circles which are wrapped away from the spool of the bobbin.

[087] FIG. 17C represents a mixture of unmagnetized magnetic particles and uncured adhesive in a container. The mixture has the material properties of being electrically relatively high impedance and adhesive. Initially, the mixture is in a liquid phase, and after a process of binding or curing the mixture changes to a solid phase. The liquid phase has a viscosity such that the mixture maintains a uniform distribution of the unmagnetized particles. The solid phase may be a rigid solid.

[088] The mixture is configured to wet a surface of the unmagnetized particles. The mixture has adhesive and cohesive properties sufficient to keep the particles in suspension and remain substantially electrically insulated from each other during the process of assembling, curing, and magnetizing such that the mixture has substantially higher electrical impedance than the unmagnetized particles alone before mixing with the suspension medium. Suitable suspension mediums are epoxies or similar materials.

[089] The unmagnetized material consists of particles capable of permanent magnetic properties when magnetized. These materials include rare earth materials such as Neodymium Iron Boron (NdFeB) based material and Samarium Cobalt (SmCo) based material.

[090] In combination, the volumetric ratio of unmagnetized particles to suspension medium is typically greater than 1.

[091] FIG. 17D shows the mixture applied to the gap area.

[092] FIG. 17E shows the bobbin with windings fitted to the core.

[093] FIG. 17F illustrates an energy transfer element that is assembled and cured. The completed element is ready for magnetizing. The mixture has been formed by the force of assembly to fill the gap region and may optionally be extruded from the gap to secure the bobbin to the post.

[094] FIG. 18 illustrates a flowchart 1800 to assemble the energy transfer element 1700 shown in FIGs. 17A – 17F.

[095] In step 1802, the cores are prepared with a desired gap in the magnetic path.

[096] In step 1804, the bobbin is prepared with windings.

[097] In step 1806, the mixture of magnetic particles and suspension medium such as adhesive or epoxy is prepared. This step may occur at any point before step 1808.

[098] In step 1808, the mixture is applied to the gap between a set of cores.

[099] In step 1810, the bobbin with windings is fit to the core.

[100] The order of steps 1808 and 1810 are interchangeable.

[101] In step 1812, the energy transfer element is assembled.

[102] In step 1814, the adhesive is cured. Curing may be achieved by several techniques. In one technique, the temperature is raised to above the curing temperature of the epoxy. In another technique, the pressure is raised to above a curing pressure

associated with the curing material. In another technique, the epoxy is cured by radiation at a wavelength associated with the curing material. For each curing technique, the curing operational parameter is maintained to allow time for epoxy to cure.

[103] In step 1816, the energy transfer assembly is magnetized.

[104] FIGs. 19A – 19F illustrate the salient features of the construction of an energy transfer element 1900 having unmagnetized magnetic material, where the thickness is less than the gap between two core halves.

[105] FIG. 19A illustrates a set of cores with a gap of distance d.

[106] FIG. 19B illustrates a bobbin with windings. The primary power winding is reflected by the smaller circles wrapped closest to the spool of the bobbin. The secondary power winding is reflected by the large circles which are wrapped away from the spool of the bobbin.

[107] FIG. 19C is a solid piece of unmagnetized magnetic material with a height less than or equal to distance d.

[108] These materials include rare earth materials such as Neodymium Iron Boron (NdFeB) based material and Samarium Cobalt (SmCo) based material.

[109] FIG. 19D shows the unmagnetized magnetic material fixed in the gap area.

[110] FIG. 19E shows the bobbin with windings fitted to the core.

[111] FIG. 19F illustrates an energy transfer element that is assembled with the solid piece of unmagnetized magnetic material.

[112] FIG. 20 illustrates a flowchart 2000 to assemble the energy transfer element 1900 shown in FIGs. 19A – 19F.

[113] In step 2002, the cores are prepared with a desired gap of distance d in the magnetic path.

[114] In step 2004, the bobbin is prepared with windings.

[115] In step 2006, unmagnetized magnetic material of thickness h, where $h \leq d$, is placed in the gap between a set of cores.

[116] In step 2008, the unmagnetized magnetic material is secured in the gap between the set of cores.

[117] In step 2010, the bobbin with windings is fit to the core.

[118] The order of steps 2008 and 2010 are interchangeable.

[119] In step 2012, the energy transfer element is assembled.

[120] In step 2014, the energy transfer assembly is magnetized.

[121] FIGs. 21A – 21F illustrate the salient features of the construction of an energy transfer element 2100 having unmagnetized magnetic material in the gap having a thickness greater than the distance between two core halves.

[122] FIG. 21A illustrates a set of cores with a gap of distance d.

[123] FIG. 21B illustrates a bobbin with windings. The primary power winding is reflected by the smaller circles wrapped closest to the spool of the bobbin. The secondary power winding is reflected by the large circles which are wrapped away from the spool of the bobbin.

[124] FIG. 21C is a solid piece of unmagnetized magnetic material with a height h greater than distance d.

[125] These materials include rare earth materials such as Neodymium Iron Boron (NdFeB) based material and Samarium Cobalt (SmCo) based material.

[126] FIG. 21D shows the unmagnetized magnetic material fixed in the gap area. Some of the magnetic material is removed so that $h \leq d$. If the material is sufficiently hard, it may be ground to the correct thickness.

[127] FIG. 21E shows the bobbin with windings fitted to the core.

[128] FIG. 21F illustrates an energy transfer element that is assembled and ready for magnetizing.

[129] FIG. 22 illustrates a flowchart 2200 to assemble the energy transfer element 2100 shown in FIGs. 21A – 21F.

[130] In step 2102, the cores are prepared with a desired gap of distance d in the magnetic path.

[131] In step 2104, the bobbin is prepared with windings.

[132] In step 2106, unmagnetized magnetic material of thickness h, where $h > d$, is placed in the gap between a set of cores.

[133] In step 2108, material is removed from the unmagnetized magnetic material such that $h \leq d$.

[134] In step 2110, the bobbin with windings is fit to the core.

[135] In step 2112, the energy transfer element is assembled.

[136] In step 2114, the energy transfer assembly is magnetized.

[137] FIGs. 23A – 23F illustrate the salient features of the construction of an energy transfer element 2300 having deformable unmagnetized magnetic material in the gap between the two core halves.

[138] FIG. 23A illustrates a set of cores with a gap of distance d.

[139] FIG. 23B illustrates a bobbin with windings. The primary power winding is reflected by the smaller circles wrapped closest to the spool of the bobbin. The secondary power winding is reflected by the large circles which are wrapped away from the spool of the bobbin.

[140] FIG. 23C is a deformable solid piece of unmagnetized magnetic material with a height h greater than distance d. The material may be a mixture of unmagnetized magnetic powder and uncured adhesive. The mixture has the material properties of being substantially higher electrical impedance than the unmagnetized magnetic powder alone and adhesive. Initially, the mixture is in a compliant phase allowing for deformation under pressure for example and after curing, the mixture changes to a solid phase. The compliant phase has a viscosity such that the mixture maintains a uniform distribution of the unmagnetized powder. The solid phase may be a rigid solid that is non-rigid within a range of temperatures, e.g. glass. When the compliant phase is a non-rigid solid, it may deform in response to an assembling force that is elastic or inelastic.

[141] FIG. 23D shows the unmagnetized magnetic material fixed in the gap area.

[142] FIG. 23E shows the bobbin with windings fitted to the core.

[143] FIG. 23F illustrates an energy transfer element that is assembled and ready for magnetizing.

[144] FIG. 24 illustrates a flowchart 2400 to assemble the energy transfer element shown in FIGs. 23A – 23F.

[145] In step 2402, the cores are prepared with a desired gap of distance d in the magnetic path.

[146] In step 2404, the bobbin is prepared with windings.

[147] In step 2406, the deformable unmagnetized magnetic material of thickness h, where h > d, is fixed in the gap between a set of cores.

[148] In step 2408, the bobbin with windings is fit to the core.

[149] The order of steps 2406 and 2408 are interchangeable.

[150] In step 2410, the energy transfer element is assembled.

[151] In step 2412, the energy transfer assembly is magnetized.

[152] FIG. 25 illustrates a cross-section of a magnetizer 2500 for magnetizing the energy transfer elements disclosed above. The energy transfer element is placed inside the solenoid magnetizing fixture 2500. The solenoid magnetizing fixture 2500 is a double-walled cylinder 2510 that sandwiches a solenoid conductor, e.g. a coil of wire, 2515 between the walls. A current source 2520 applies a current that is passed through the solenoid conductor to generate a magnetic field of a magnitude suitable to magnetize the permanent magnet material. For NdFeB materials, the magnetic field is typically greater than 3 tesla.

[153] The above description of illustrated examples of the present invention, including what is described in the Abstract, are not intended to be exhaustive or to be limitation to the precise forms disclosed. While specific embodiments of, and examples for, the invention are described herein for illustrative purposes, various equivalent modifications are possible without departing from the broader spirit and scope of the present invention. Indeed, it is appreciated that the specific example voltages, currents, frequencies, power range values, times, or similar parameters, are provided for explanation purposes and that other values may also be employed in other embodiments and examples in accordance with the teachings of the present invention.

[154] Example 1: A method for making an energy transfer element comprising: forming a U-shaped magnetic core of powder core, the magnetic core having a gap in its magnetic path; adding one or more power windings to the U-shaped magnetic core; placing unmagnetized magnetizable material that produces an initial flux density into the gap; and applying a magnetic field to the unmagnetized magnetic material such that the unmagnetized magnetic material becomes magnetized, wherein the flux density produced by the magnetized material is offset from the initial flux density.

[155] Example 2: The method of example 1, wherein placing unmagnetized magnetizable material into the gap comprises: applying a mixture comprising epoxy and magnetizable particles; and
curing the mixture.

[156] Example 3: The method of example 2, wherein the volumetric ratio of magnetizable particles to suspension medium is greater than 1.

[157] Example 4: The method of example 2, wherein curing the mixture comprises raising a temperature of the mixture to above a curing temperature associated with the suspension medium.

[158] Example 5: The method of example 2, wherein curing the mixture comprises allowing time for the suspension medium to cure.

[159] Example 6: The method of example 2, wherein curing the mixture further comprises irradiating the mixture.

[160] Example 7: The method of example 1, wherein placing unmagnetized magnetizable material into the gap comprises: inserting an unmagnetized magnet into the gap.

[161] Example 8: The method of example 1, wherein placing unmagnetized magnetizable material into the gap comprises: applying a mixture comprising epoxy, magnetizable particles, and powder core; and curing the mixture.

[162] Example 9: An energy transfer element comprising: a U-shaped core of powder core, the U-shaped core having two legs and a gap in a magnetic path; and a bar comprising magnetizable material positioned in the gap such that the magnetic core and magnetizable material form a rectangular toroid, wherein the magnetizable material is capable of being magnetized, wherein when the magnetizable material is unmagnetized, the magnetizable material has an initial flux density, and wherein when the magnetizable material is magnetized, the flux density produced by the magnetized material is offset from the initial flux density; and one or more power windings wrapped around the magnetic path.

[163] Example 10: The energy transfer element of example 9, wherein the magnetizable material comprises magnetizable particles suspended in a suspension medium.

[164] Example 11: The energy transfer element of example 10, wherein the magnetizable particles are selected from a group comprising Neodymium Iron Boron (NdFeB) based materials or Samarium Cobalt (SmCo) based material.

[165] Example 12: The energy transfer element of example 9, wherein the magnetizable material is a suspension medium comprising epoxy with magnetized magnetizable particles and powder core.

[166] Example 13: The energy transfer element of example 9, wherein the magnetizable material is an unmagnetized magnet.

[167] Example 14: The energy transfer element of example 9 wherein: the bar comprises magnetic material having a first and a second mitered end, and each leg of the U-shaped magnetic core has a mitered end such that the mitered ends of the bar mate to the mitered ends of the U-shaped magnetic core.

[168] Example 15: The energy transfer element of example 9, wherein the bar that comprises magnetic material is positioned between the legs of the U-shaped magnetic core.

CLAIMS

What is claimed is:

1. A method for making an energy transfer element comprising:

forming a U-shaped magnetic core of powder core, the magnetic core having a gap in its magnetic path;

adding one or more power windings to the U-shaped magnetic core;

placing unmagnetized magnetizable material that produces an initial flux density into the gap; and

applying a magnetic field to the unmagnetized magnetic material such that the unmagnetized magnetic material becomes magnetized,

wherein the flux density produced by the magnetized material is offset from the initial flux density.

2. The method of claim 1, wherein placing unmagnetized magnetizable material into the gap comprises:

applying a mixture comprising epoxy and magnetizable particles; and

curing the mixture.

3. The method of claim 2, wherein the volumetric ratio of magnetizable particles to suspension medium is greater than 1.

4. The method of claim 2, wherein curing the mixture comprises raising a temperature of the mixture to above a curing temperature associated with the suspension medium.

5. The method of claim 2, wherein curing the mixture comprises allowing time for the suspension medium to cure.

6. The method of claim 2, wherein curing the mixture further comprises irradiating the mixture.

7. The method of claim 1, wherein placing unmagnetized magnetizable material into the gap comprises:

inserting an unmagnetized magnet into the gap.

8. The method of claim 1, wherein placing unmagnetized magnetizable material into the gap comprises:

applying a mixture comprising epoxy, magnetizable particles, and powder core; and

curing the mixture.

9. An energy transfer element comprising:

a U-shaped core of powder core, the U-shaped core having two legs and a gap in a magnetic path; and

a bar comprising magnetizable material positioned in the gap such that the magnetic core and magnetizable material form a rectangular toroid,

wherein the magnetizable material is capable of being magnetized,

wherein when the magnetizable material is unmagnetized, the magnetizable material has an initial flux density, and

wherein when the magnetizable material is magnetized, the flux density produced by the magnetized material is offset from the initial flux density; and

one or more power windings wrapped around the magnetic path.

10. The energy transfer element of claim 9, wherein the magnetizable material comprises magnetizable particles suspended in a suspension medium.

11. The energy transfer element of claim 10, wherein the magnetizable particles are selected from a group comprising Neodymium Iron Boron (NdFeB) based materials or Samarium Cobalt (SmCo) based material.

12. The energy transfer element of claim 9, wherein the magnetizable material is a suspension medium comprising epoxy with magnetized magnetizable particles and powder core.

13. The energy transfer element of claim 9, wherein the magnetizable material is an unmagnetized magnet.

14. The energy transfer element of claim 9 wherein:

the bar comprises magnetic material having a first and a second mitered end, and

each leg of the U-shaped magnetic core has a mitered end such that the mitered ends of the bar mate to the mitered ends of the U-shaped magnetic core.

15. The energy transfer element of claim 9, wherein the bar that comprises magnetic material is positioned between the legs of the U-shaped magnetic core.

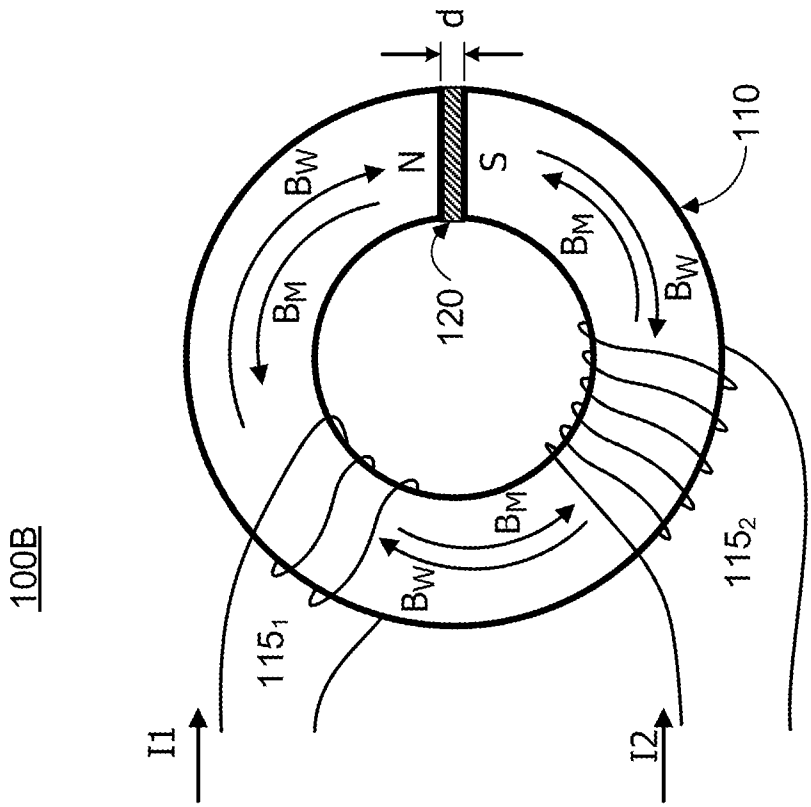


FIG. 1B (PRIOR ART)

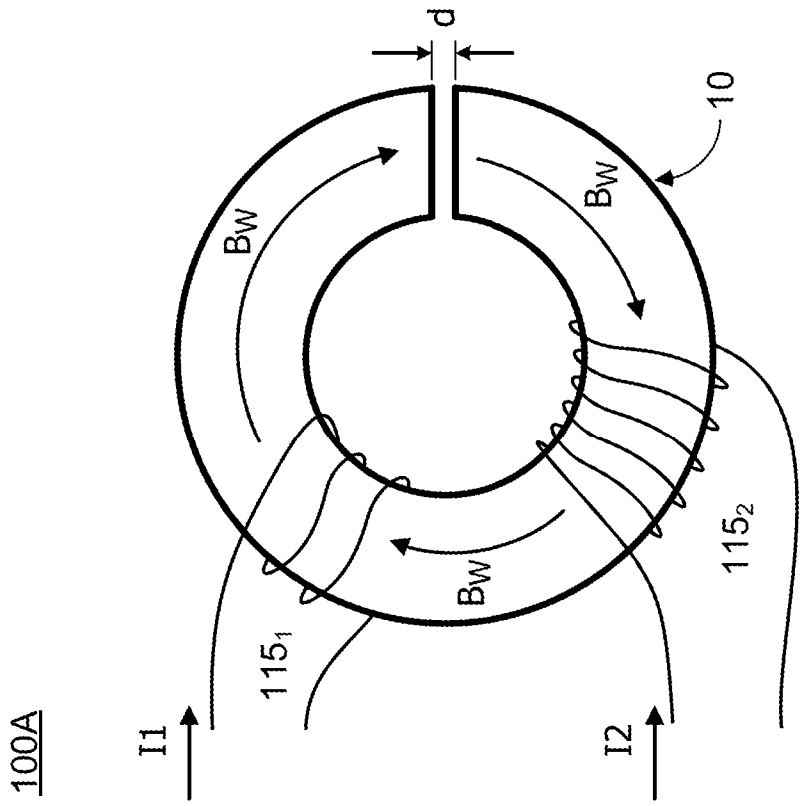


FIG. 1A (PRIOR ART)

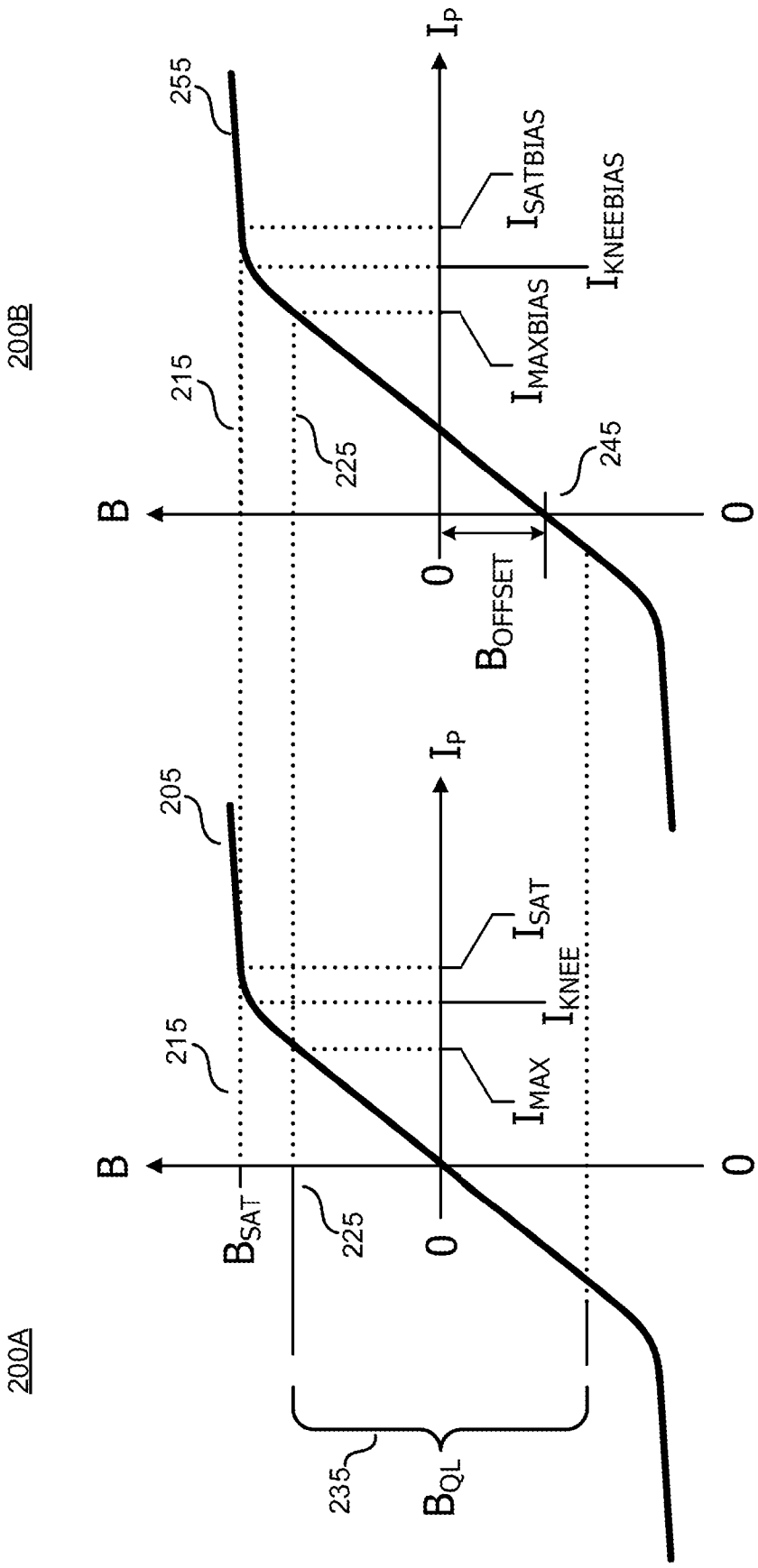

200A
205
215
225
235
B
B_{SAT}
B_{QL}
0
I_P
I_{SAT}
I_{KNEE}
I_{MAX}
200B
255
215
225
245
B
B_{OFFSET}
0
I_P
$I_{SATBIAS}$
$I_{KNEEBIAS}$
$I_{MAXBIAS}$

FIG. 2A

FIG. 2B

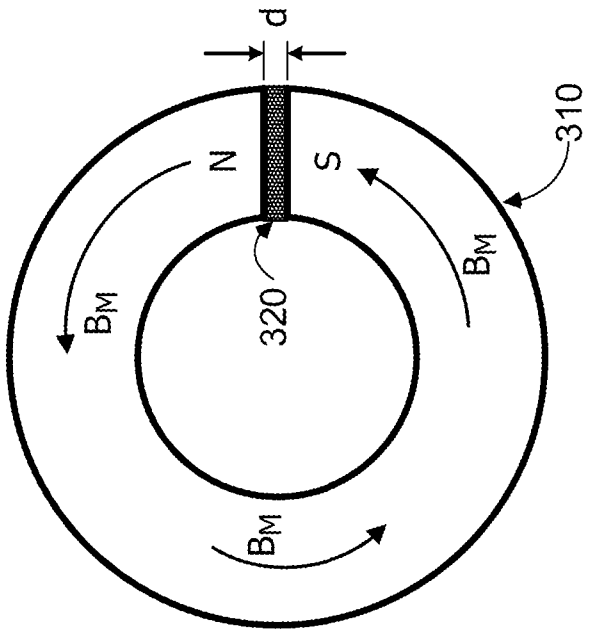


FIG. 3B

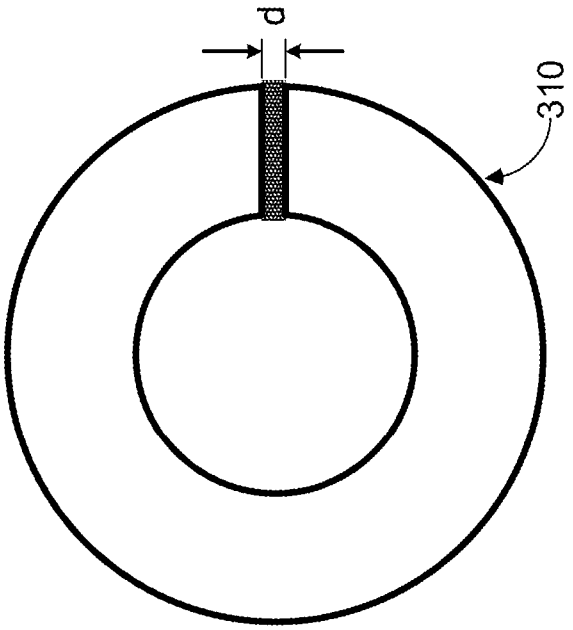


FIG. 3A

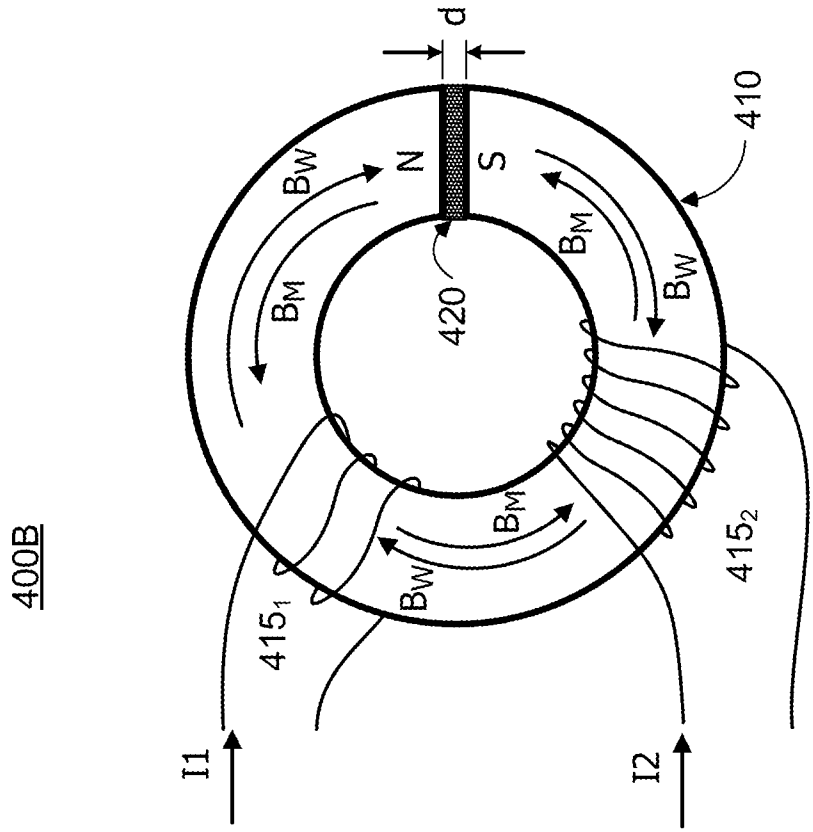

400B
d
410
N
S
B_W
B_M
420
B_M
B_W
B_M
B_W
415_1
415_2
I1
I2

FIG. 4B

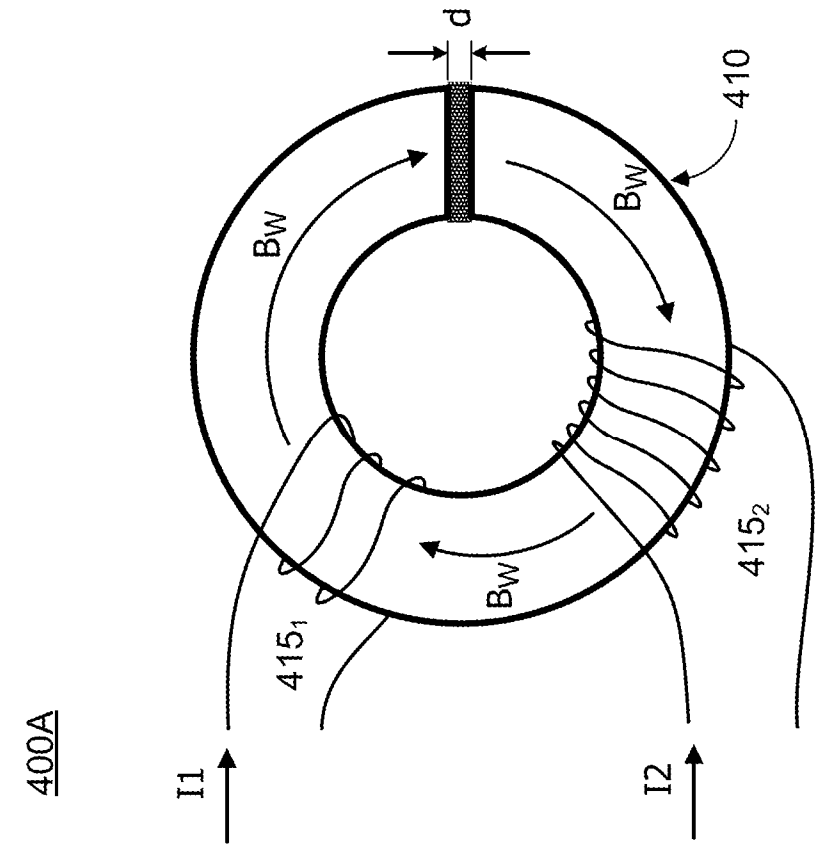

400A
d
410
B_W
B_W
B_W
B_W
415_1
415_2
I1
I2

FIG. 4A

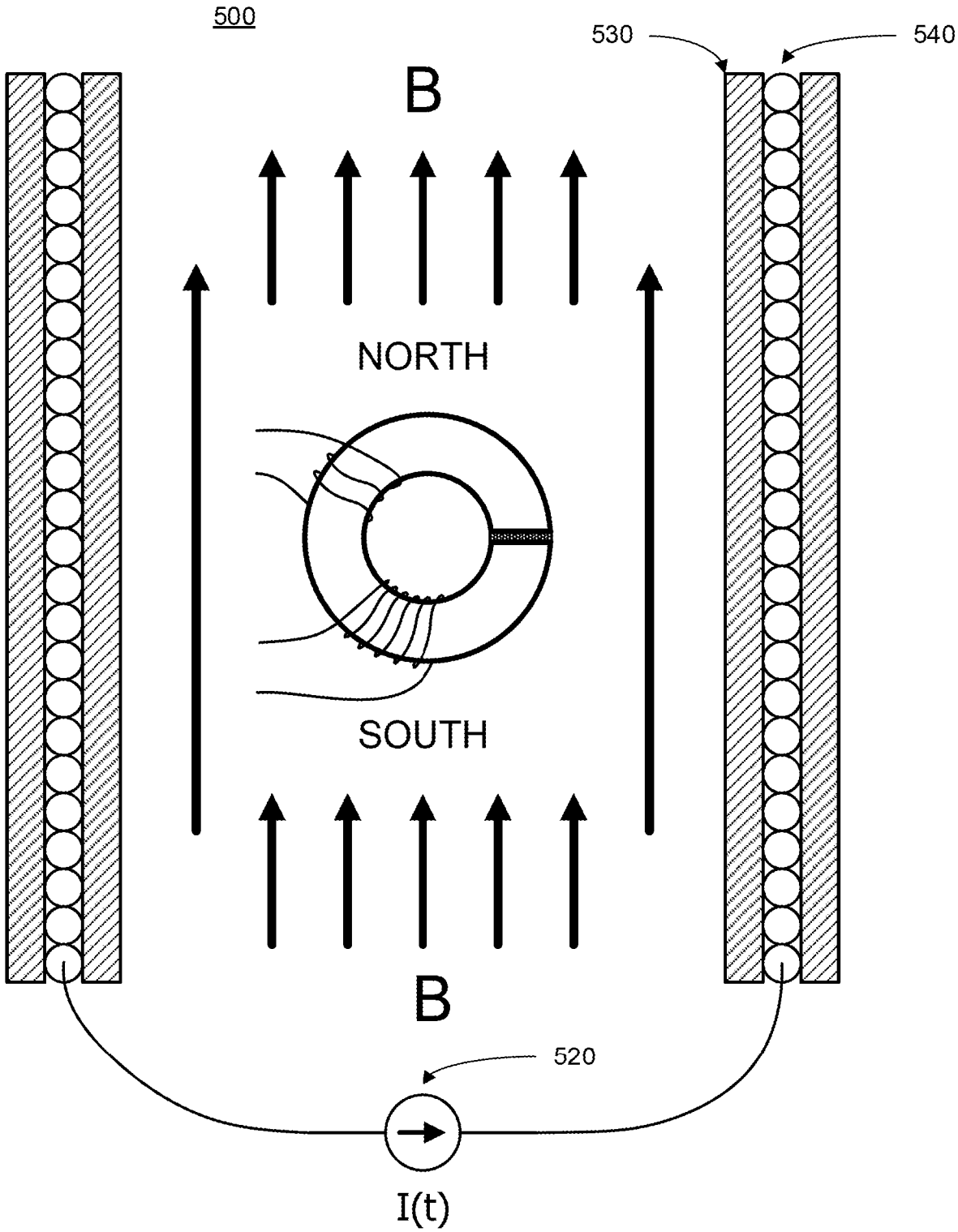


FIG. 5

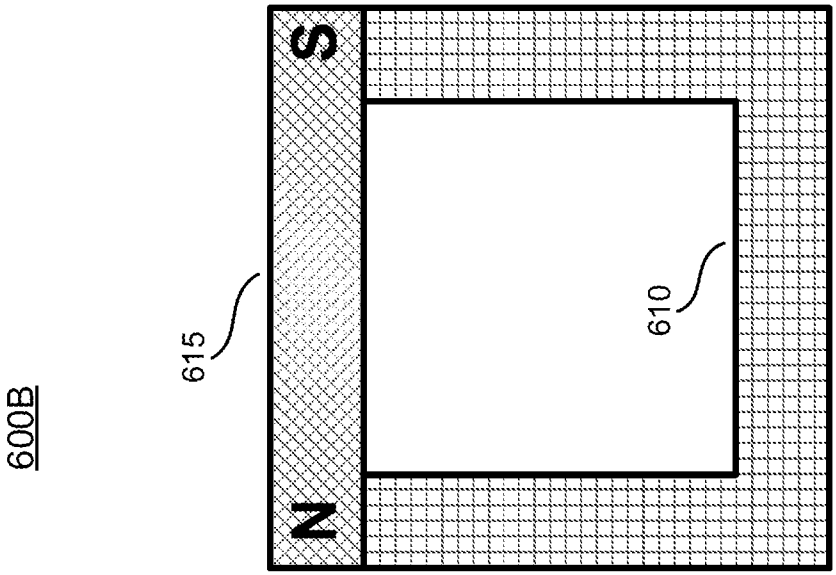


FIG. 6B

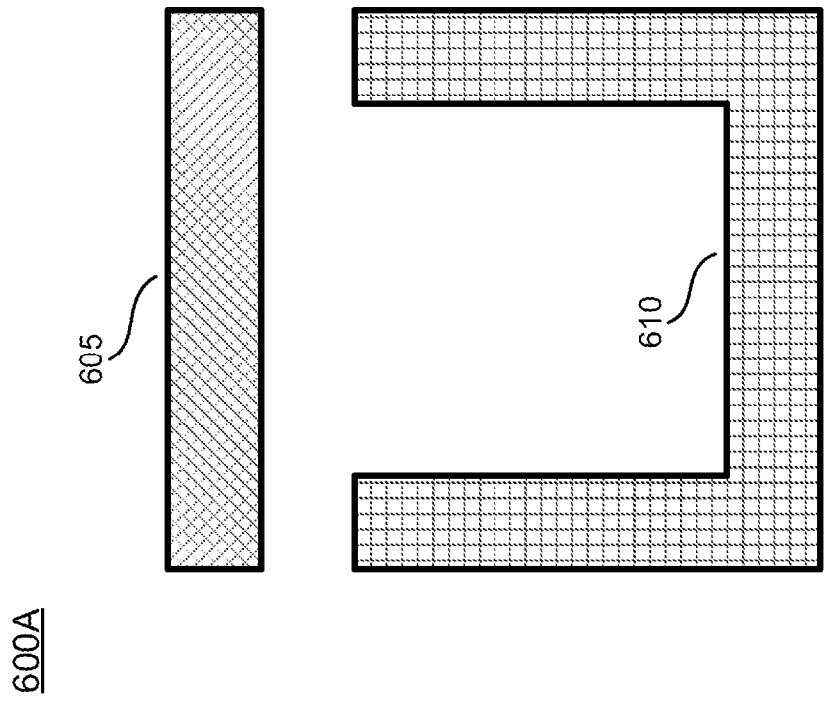


FIG. 6A

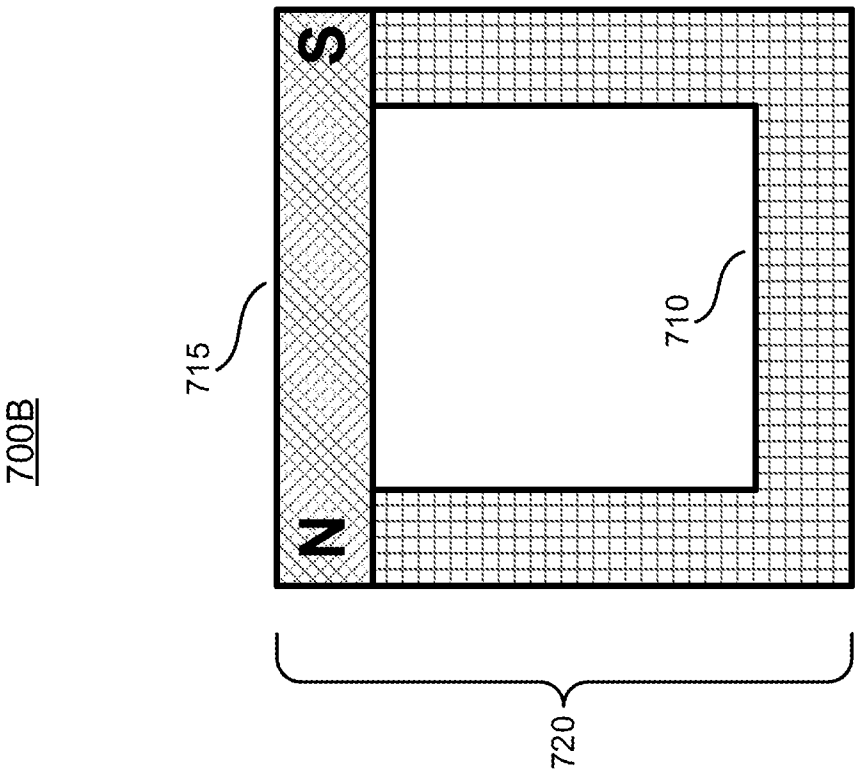


FIG. 7B

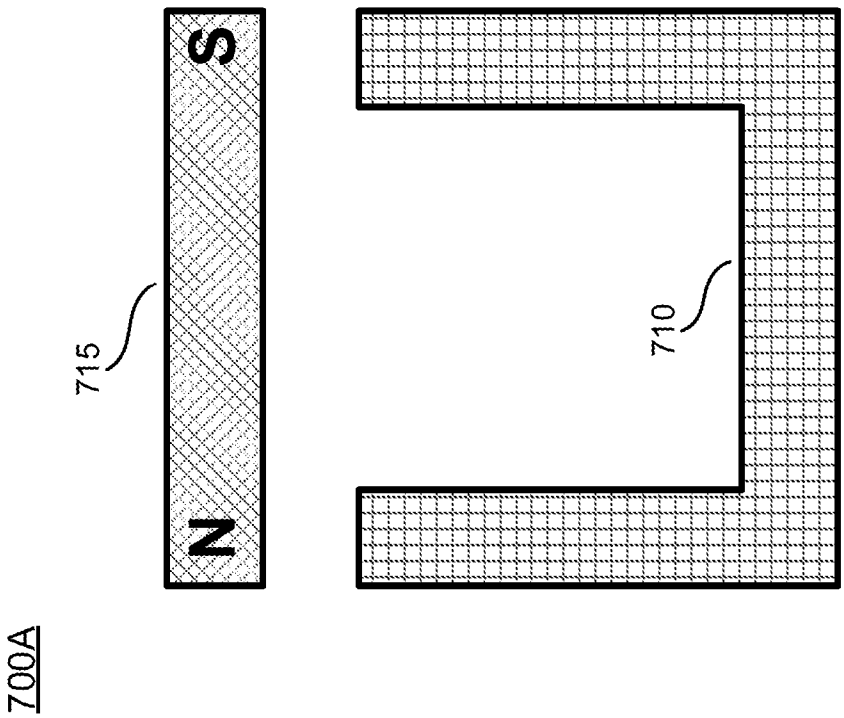


FIG. 7A

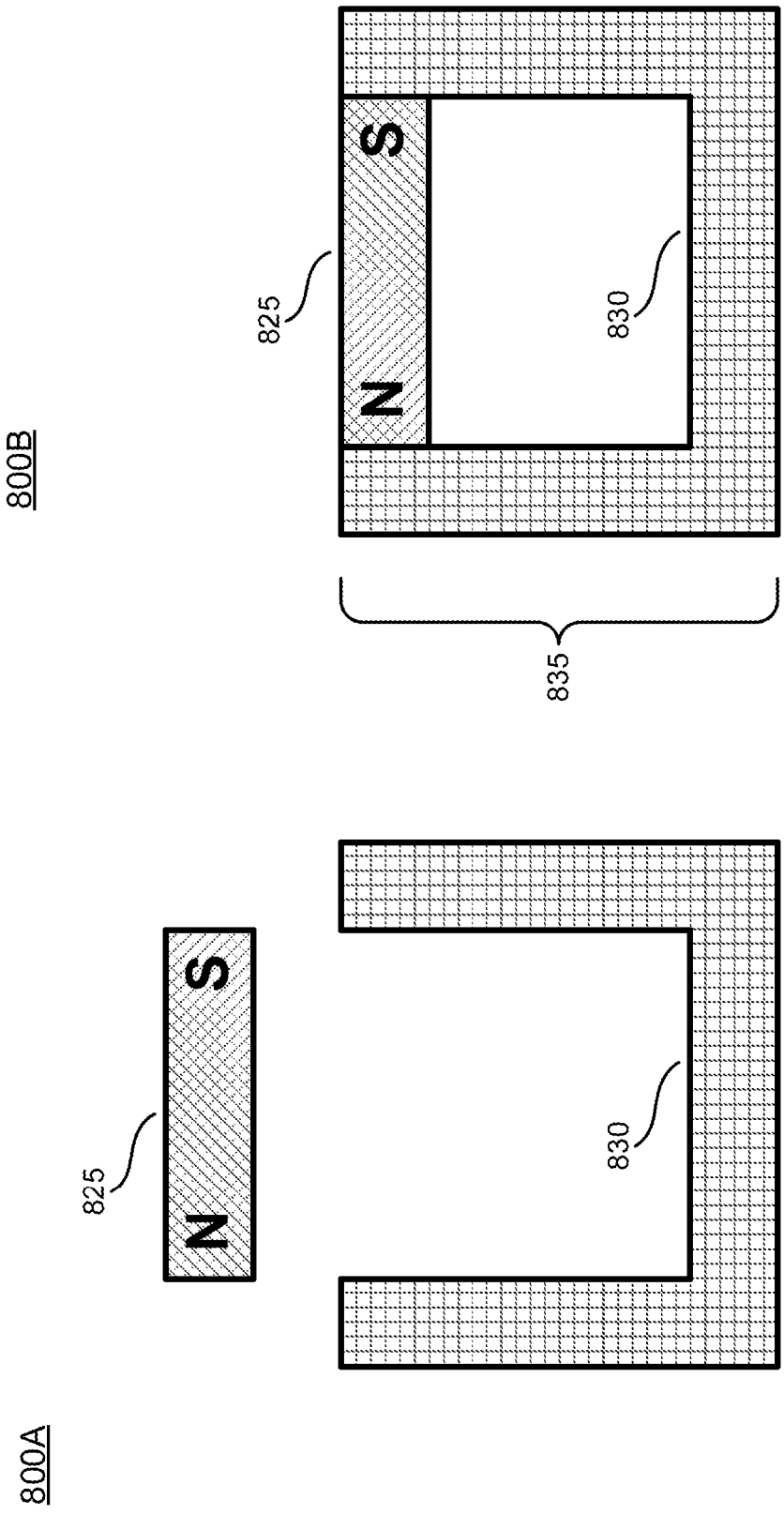


FIG. 8A

FIG. 8B

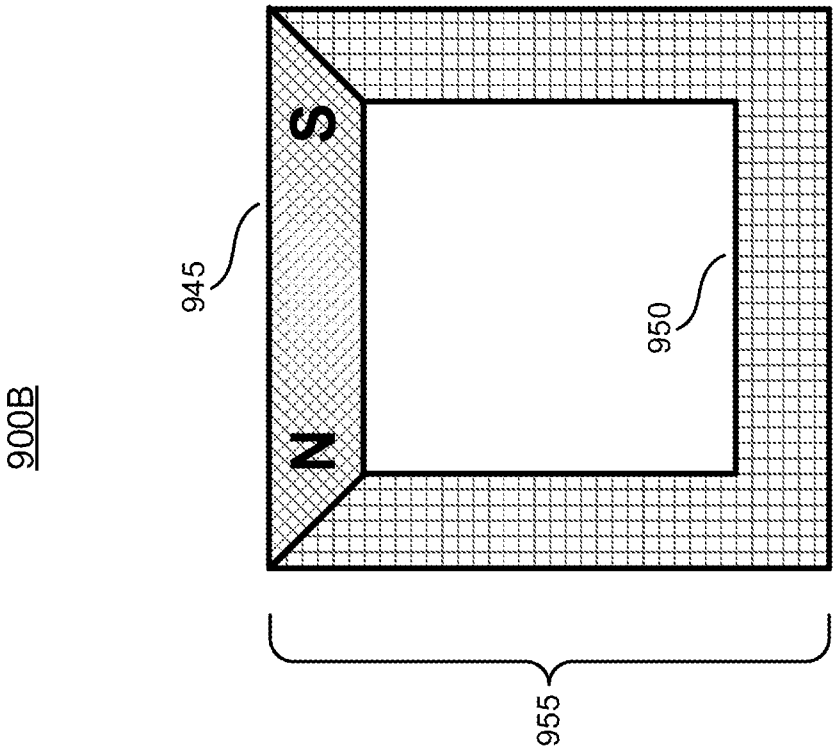


FIG. 9B

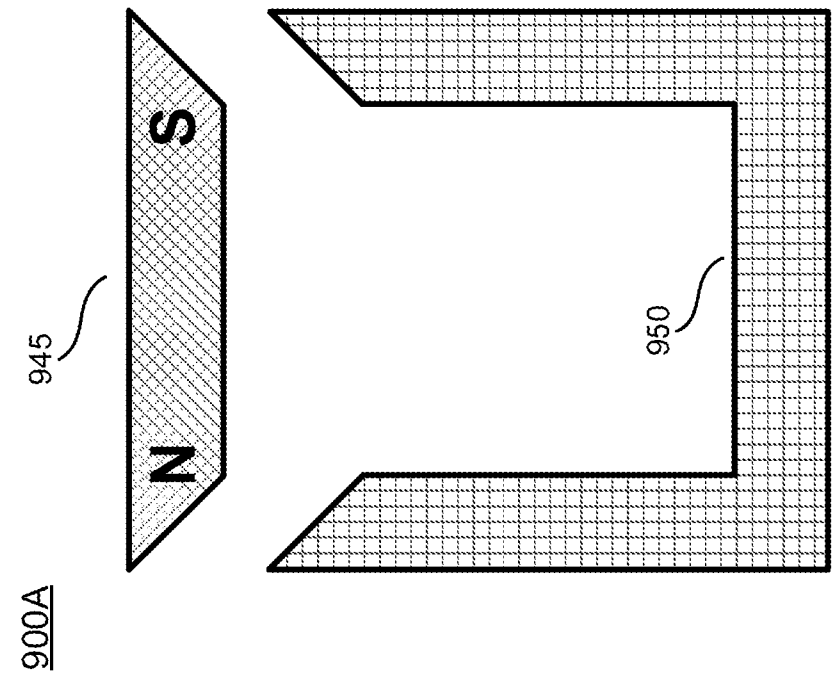


FIG. 9A

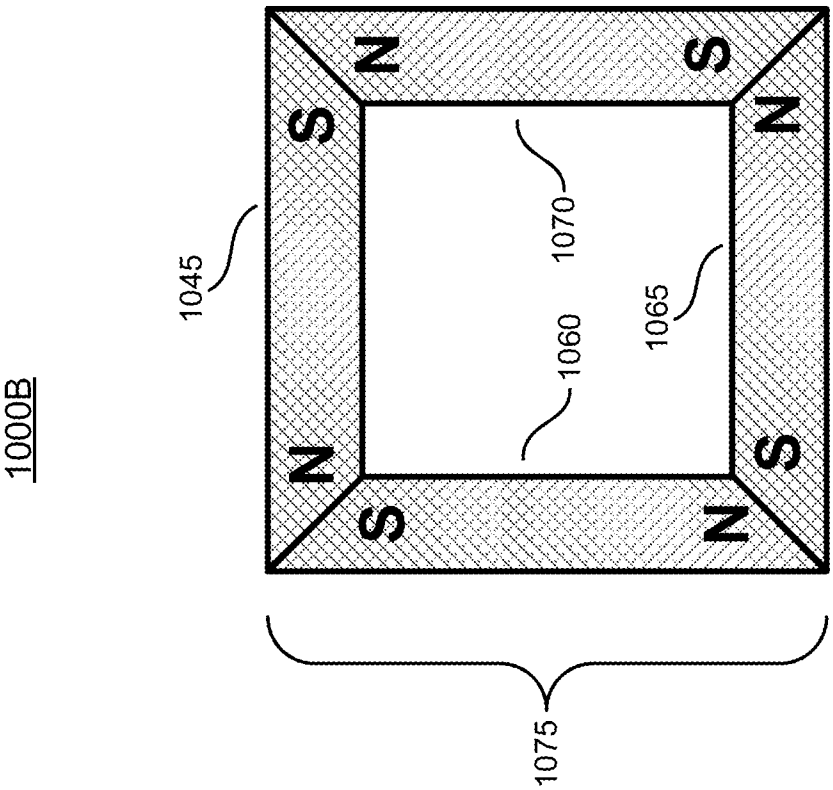


FIG. 10B

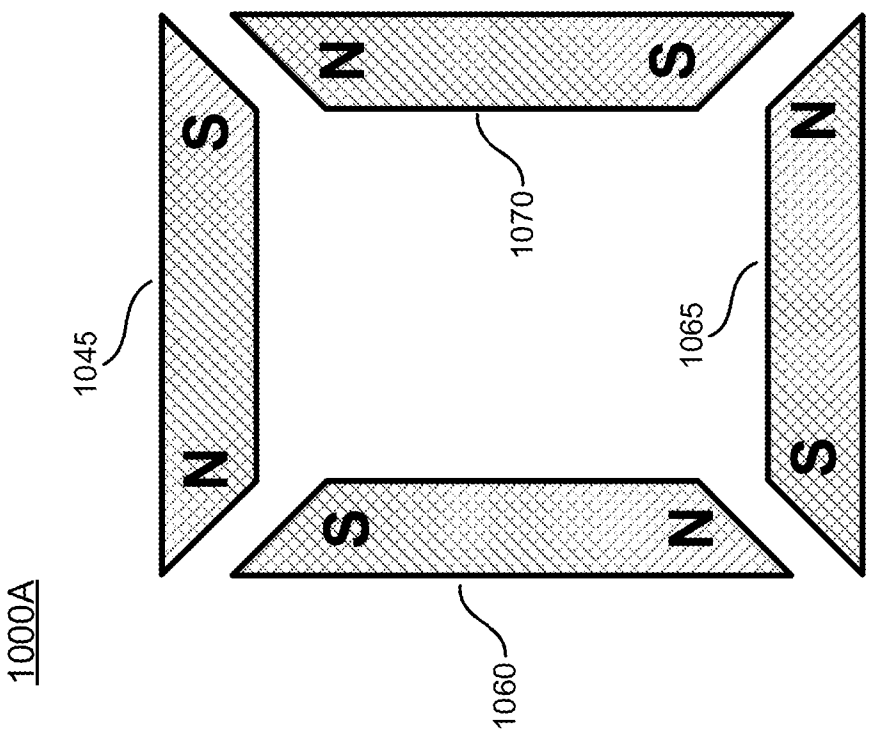


FIG. 10A

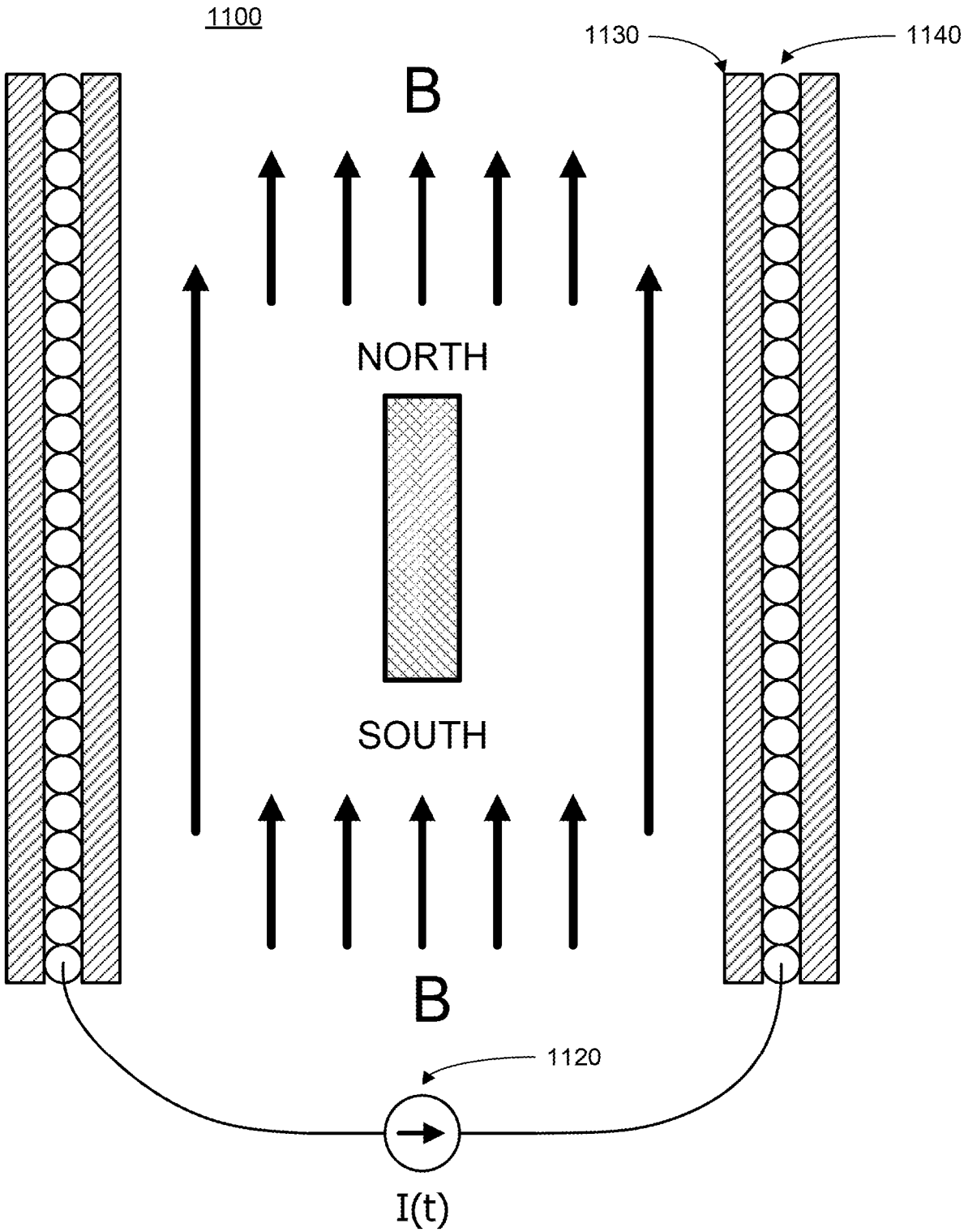


FIG. 11

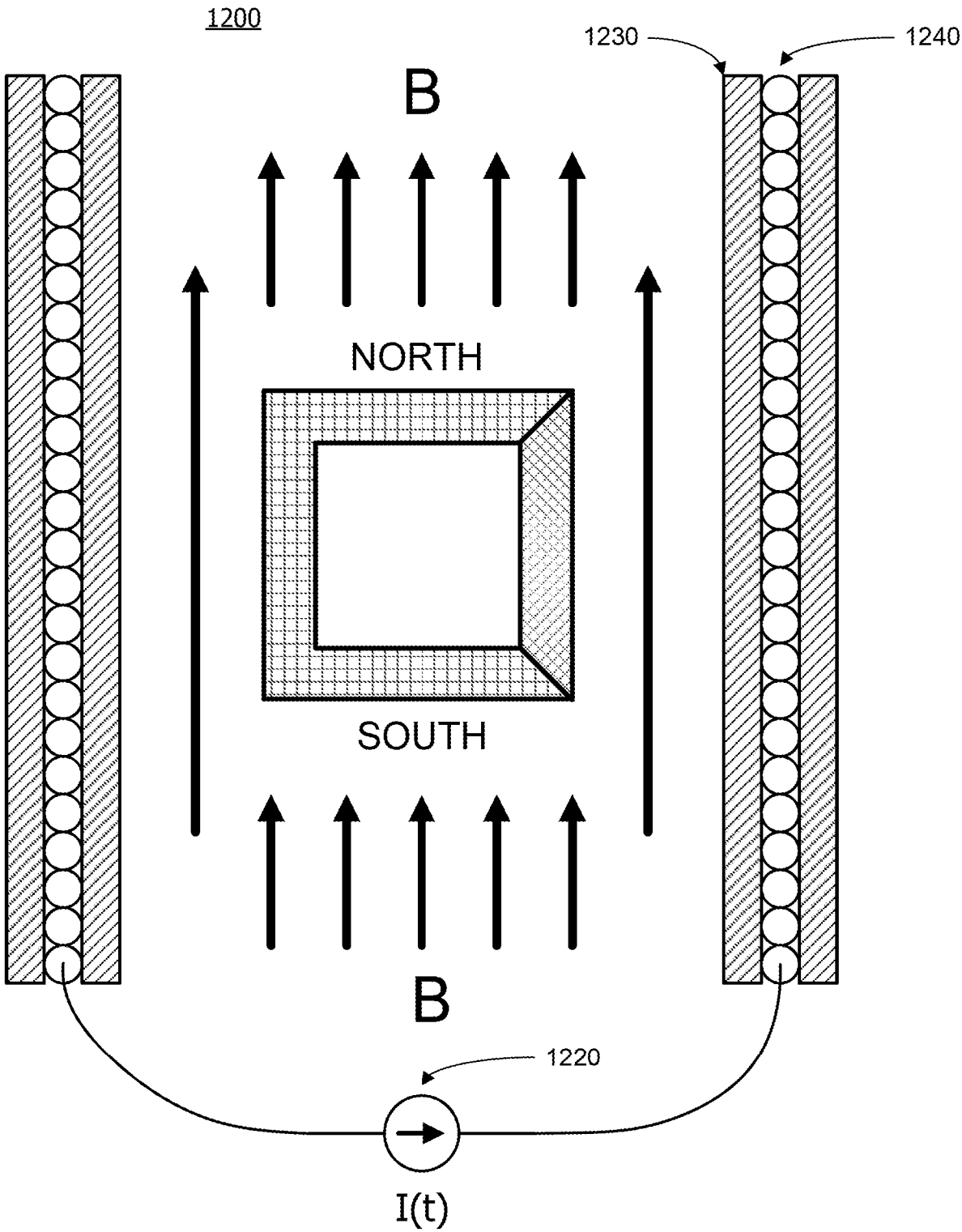


FIG. 12

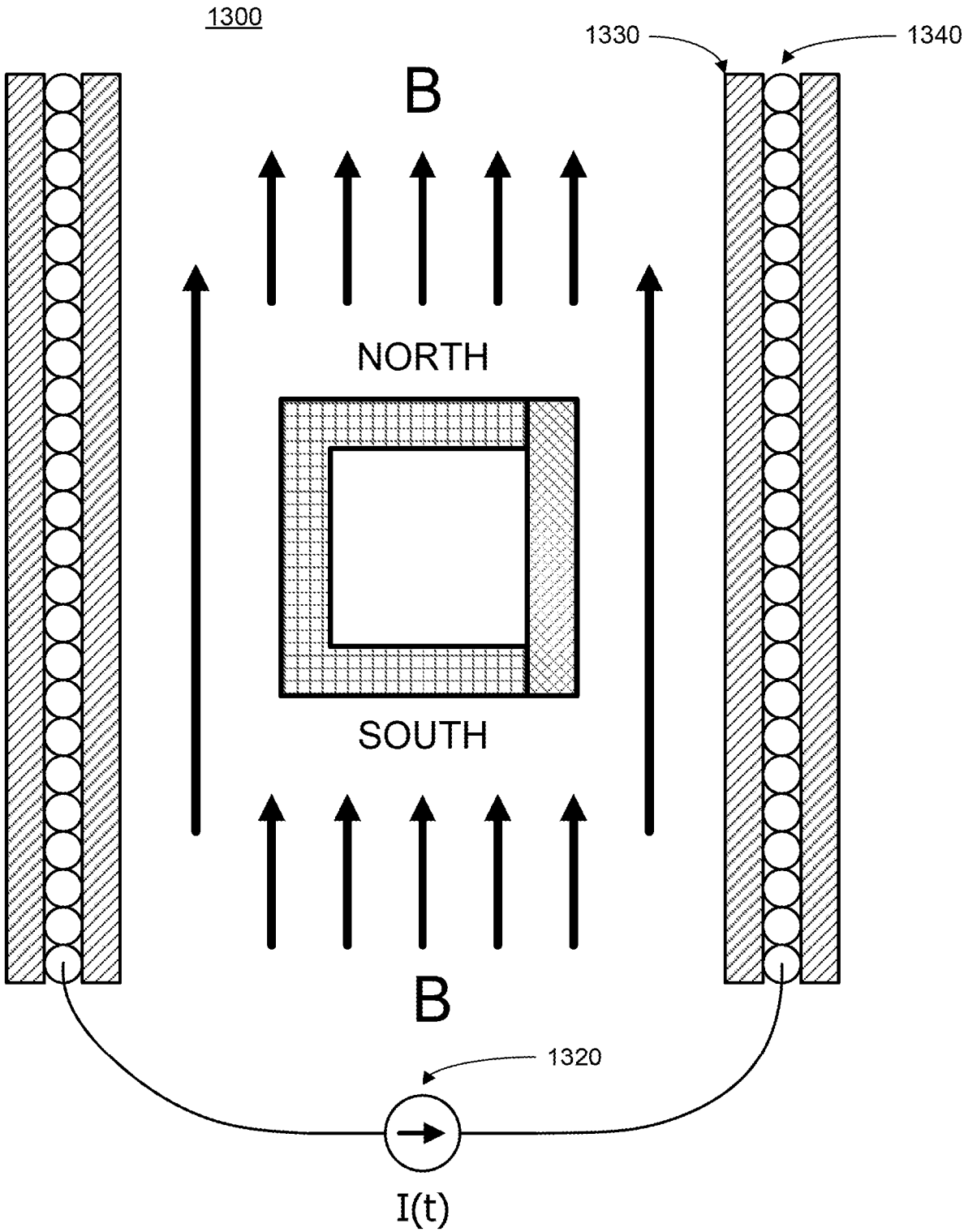


FIG. 13

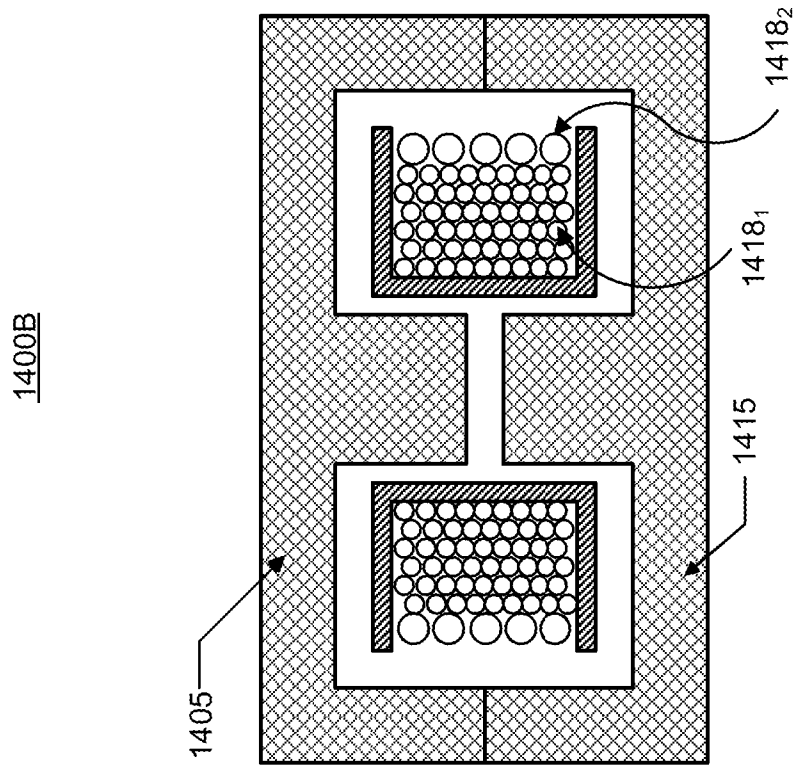


FIG. 14B (PRIOR ART)

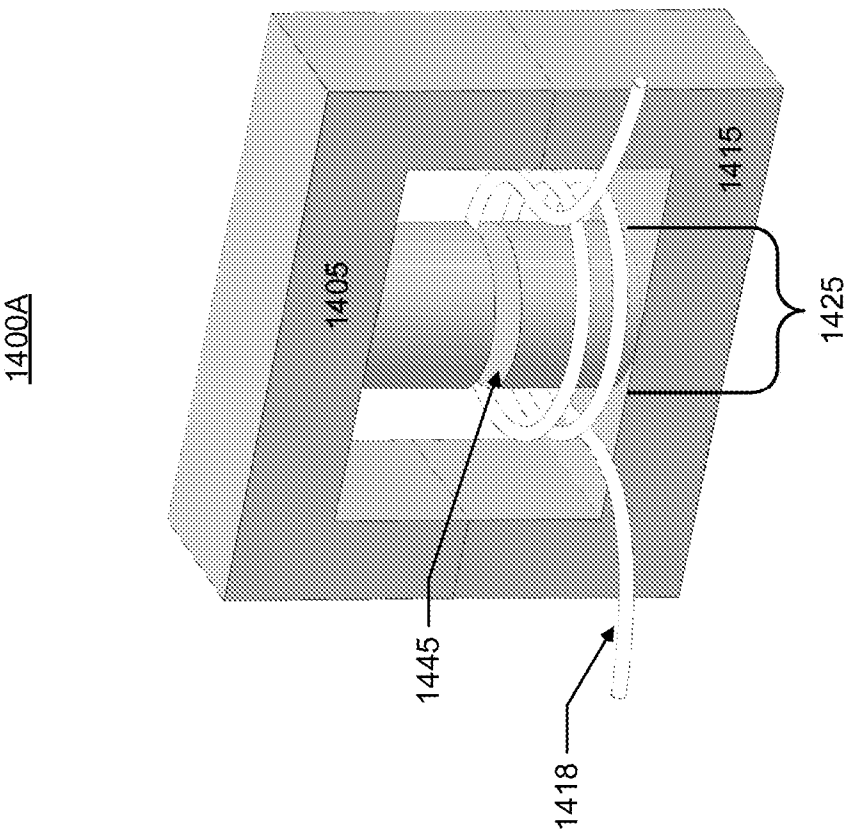


FIG. 14A (PRIOR ART)

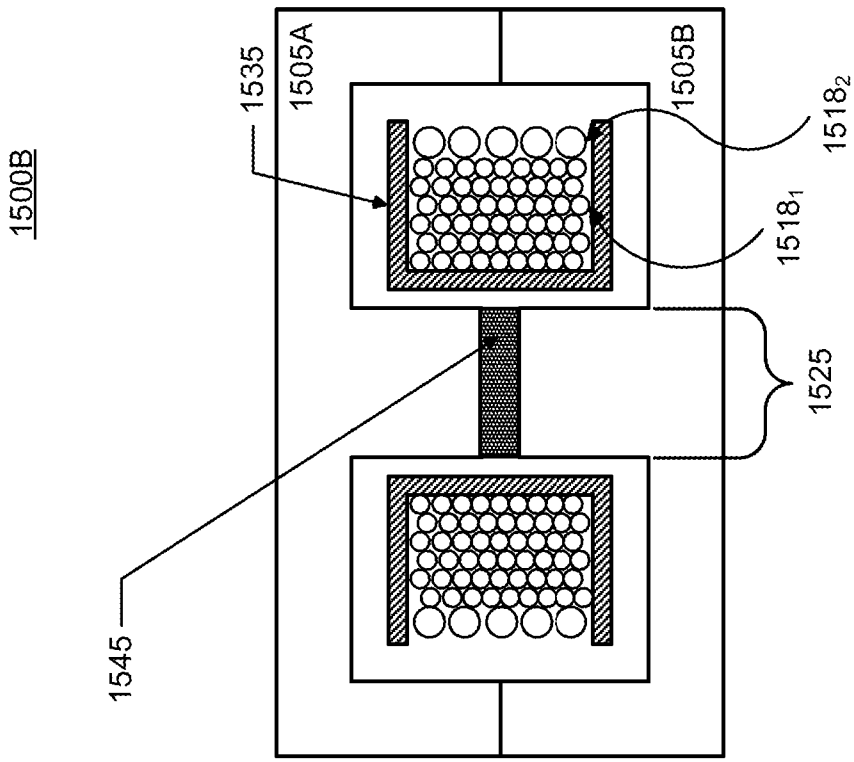


FIG. 15B

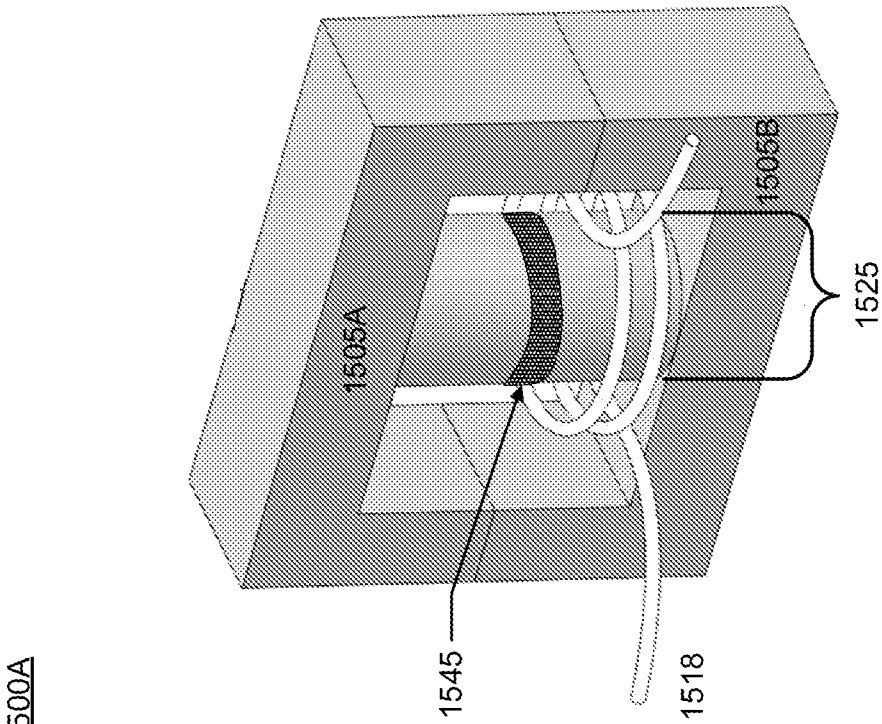


FIG. 15A

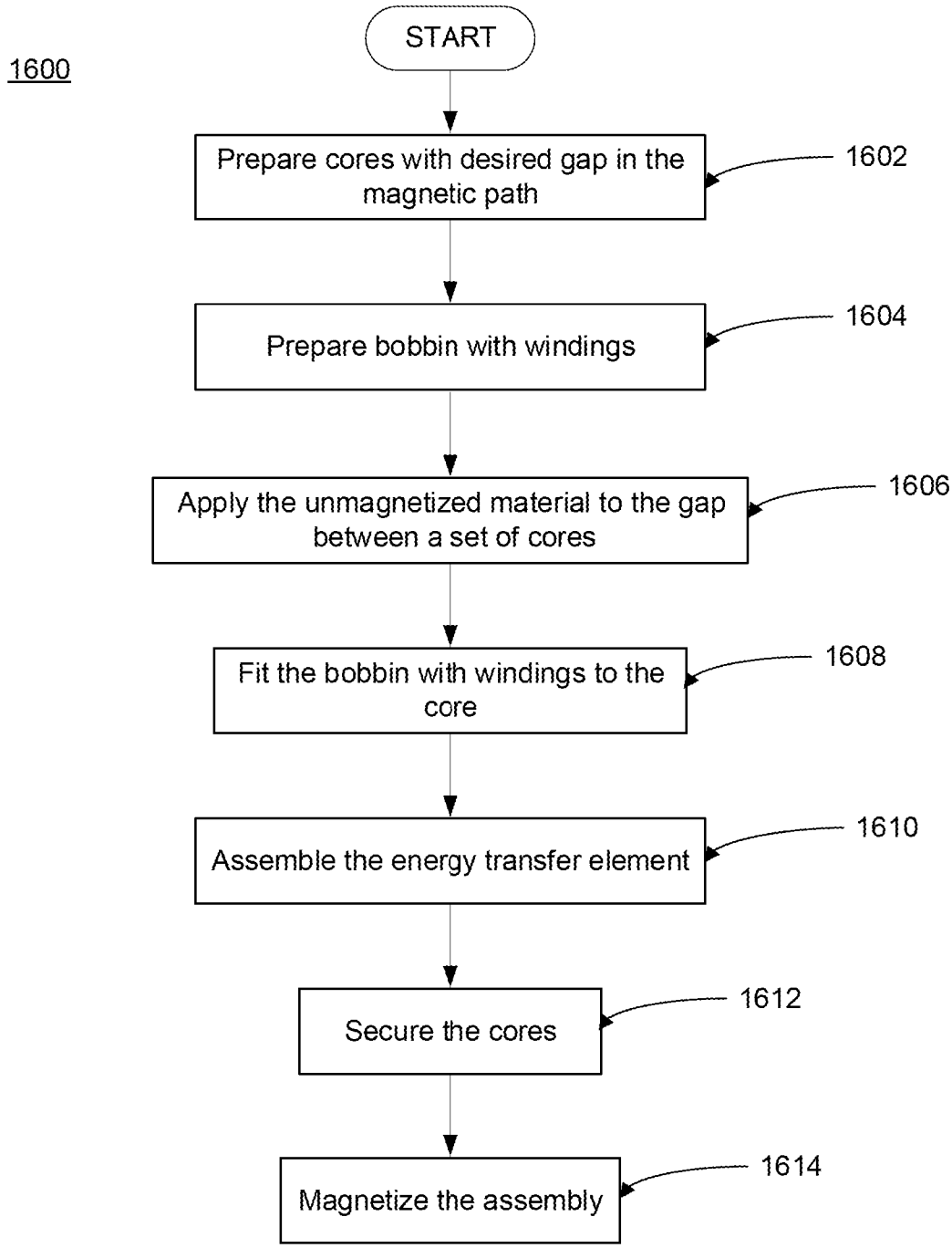
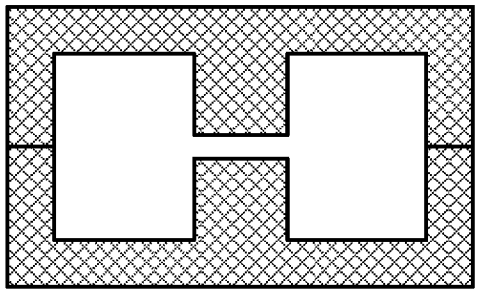
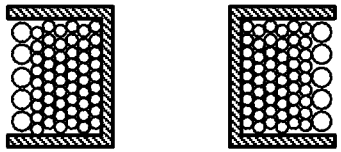

1600
START
Prepare cores with desired gap in the magnetic path
1602
Prepare bobbin with windings
1604
Apply the unmagnetized material to the gap between a set of cores
1606
Fit the bobbin with windings to the core
1608
Assemble the energy transfer element
1610
Secure the cores
1612
Magnetize the assembly
1614

FIG. 16



Set of Cores with Gap

FIG. 17A



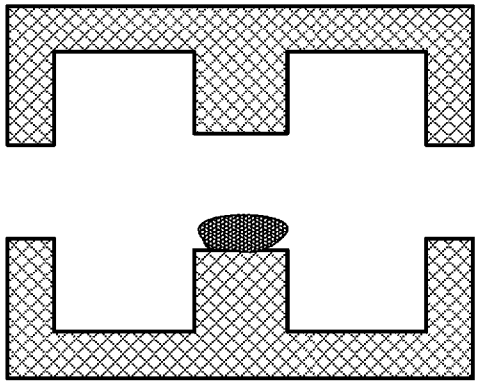
Bobbin with Windings

FIG. 17B

1700

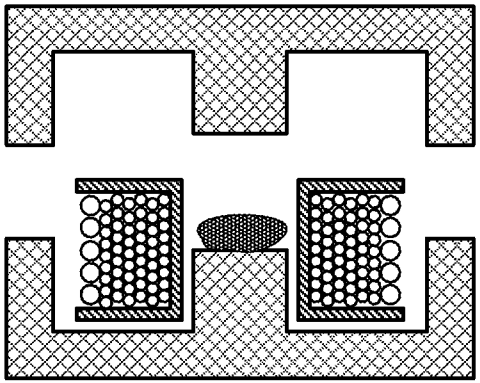
Mixture of Magnetic Particles and Uncured Adhesive

FIG. 17C



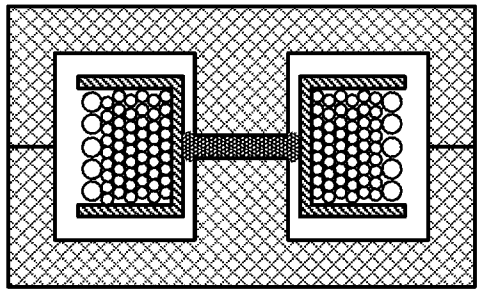
Mixture Applied to Gap Area

FIG. 17D



Bobbin with Windings Fitted to Core

FIG. 17E



Energy Transfer Element Assembled and Cured Ready for Magnetizing

FIG. 17F

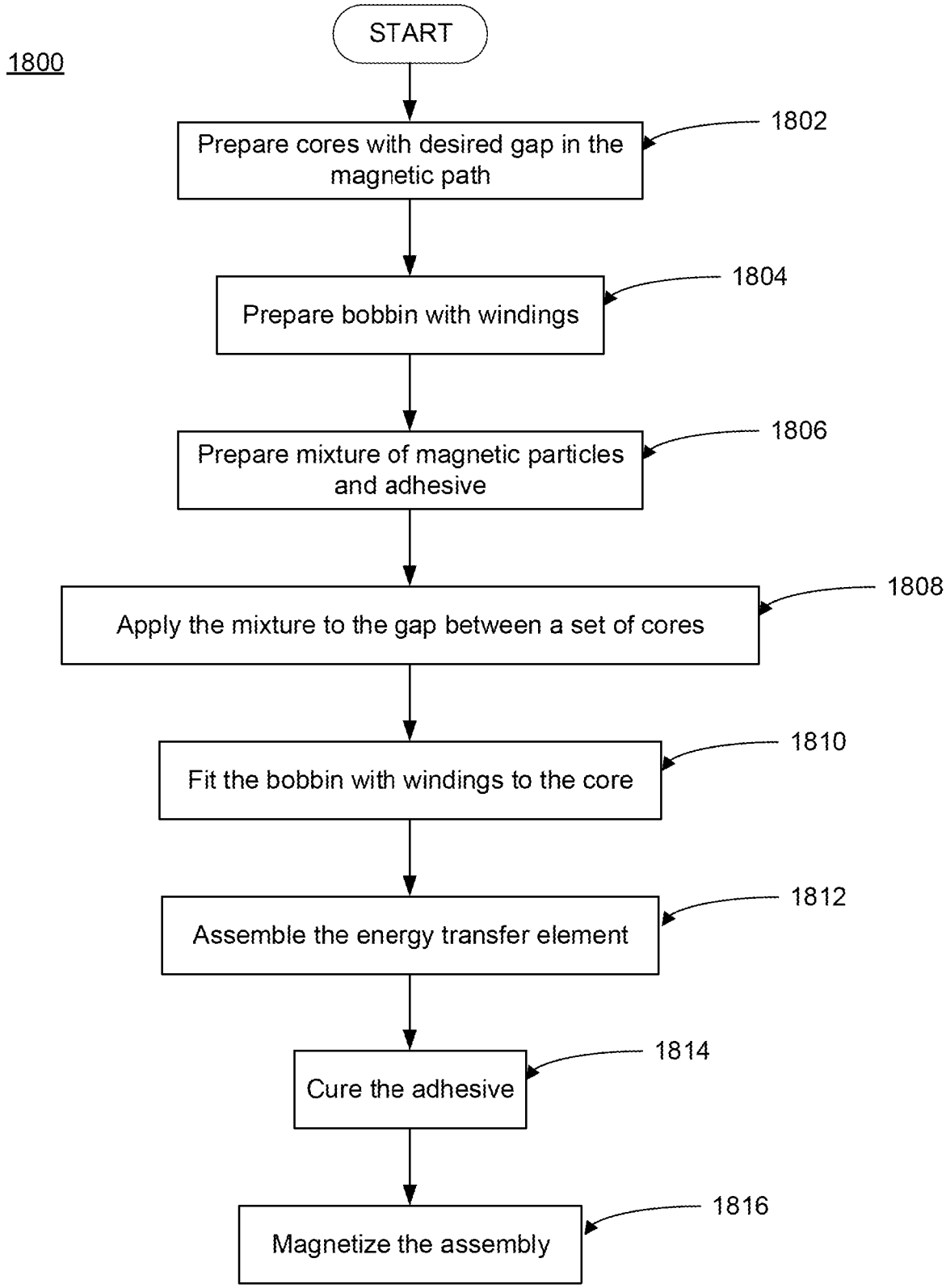
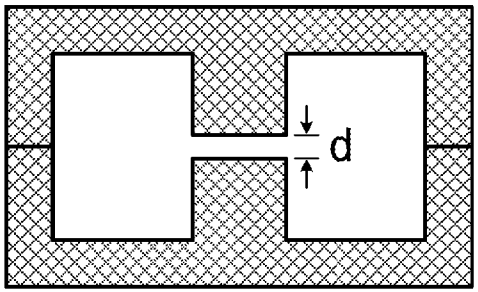
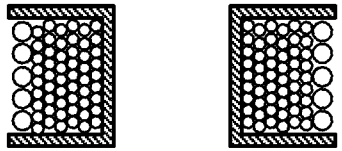

1800
START
Prepare cores with desired gap in the magnetic path
1802
Prepare bobbin with windings
1804
Prepare mixture of magnetic particles and adhesive
1806
Apply the mixture to the gap between a set of cores
1808
Fit the bobbin with windings to the core
1810
Assemble the energy transfer element
1812
Cure the adhesive
1814
Magnetize the assembly
1816

FIG. 18



Set of Cores with Gap of Distance d

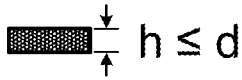
FIG. 19A



Bobbin with Windings

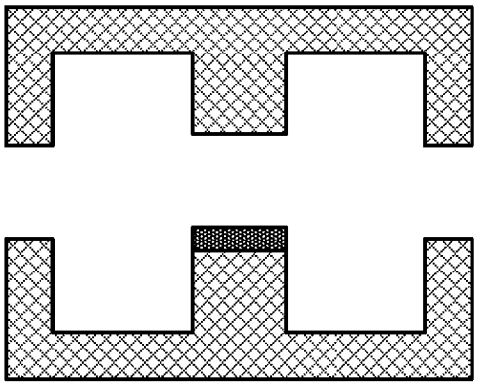
FIG. 19B

1900



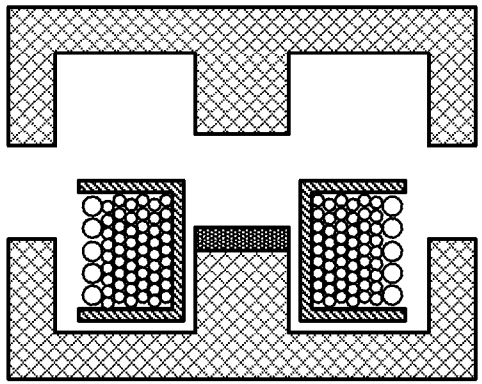
Solid Piece of Unmagnetized Magnetic Material with Height Less than or Equal to d

FIG. 19C



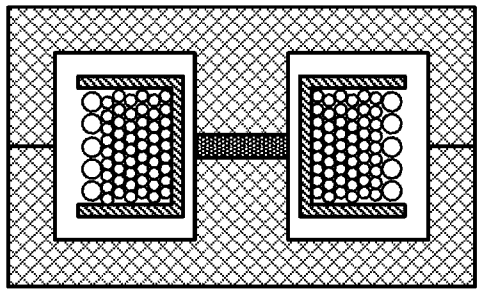
Unmagnetized Magnetic Material Fixed in Gap Area

FIG. 19D



Bobbin with Windings Fitted to Core

FIG. 19E



Energy Transfer Element Assembled and Ready for Magnetizing

FIG. 19F

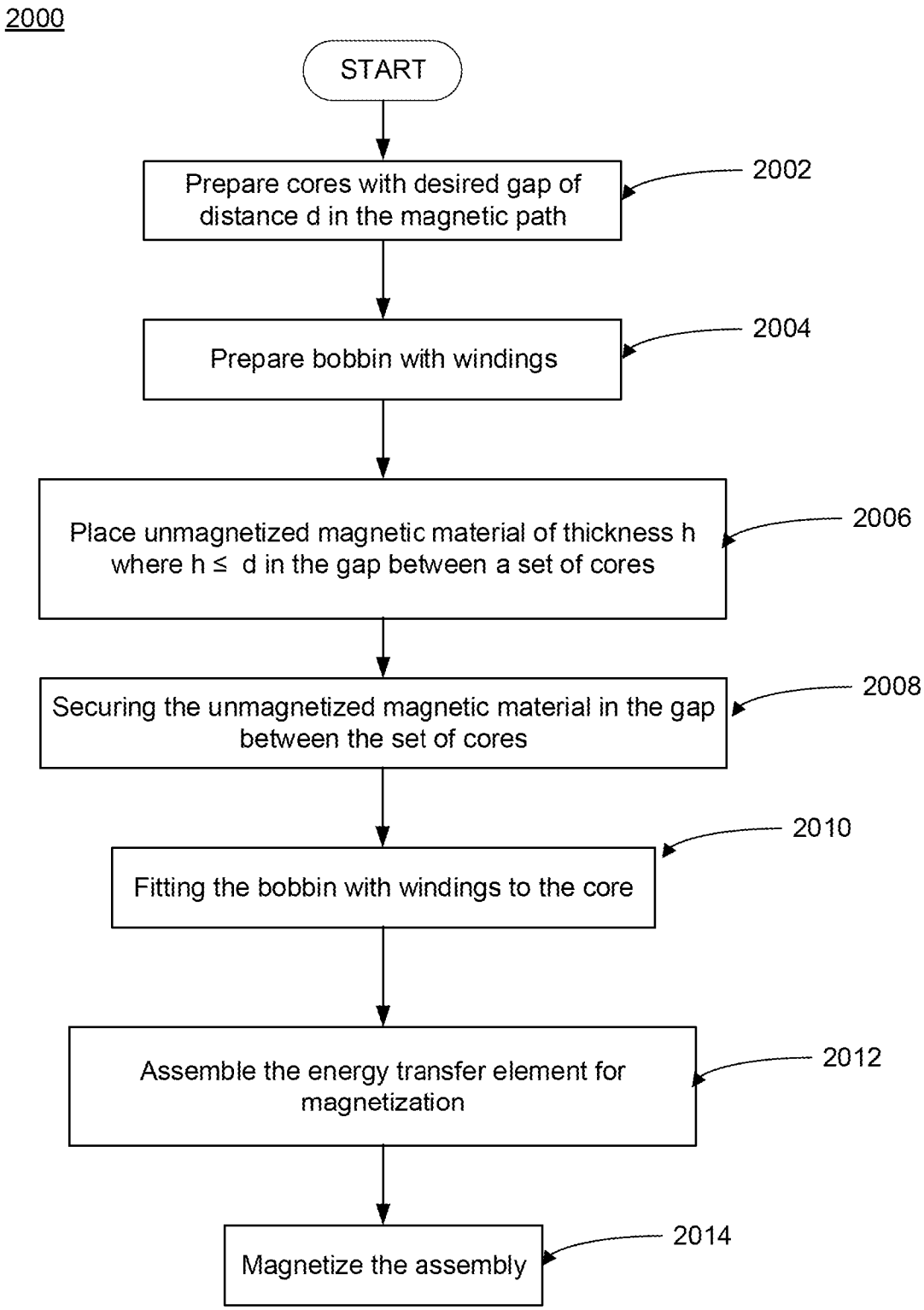
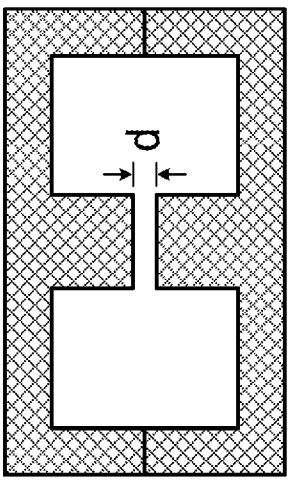

2000
START
Prepare cores with desired gap of distance d in the magnetic path
2002
Prepare bobbin with windings
2004
Place unmagnetized magnetic material of thickness h where h ≤ d in the gap between a set of cores
2006
Securing the unmagnetized magnetic material in the gap between the set of cores
2008
Fitting the bobbin with windings to the core
2010
Assemble the energy transfer element for magnetization
2012
Magnetize the assembly
2014

FIG. 20



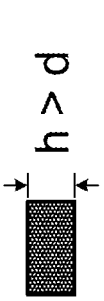
Set of Cores with Gap of Distance d

FIG. 21A

Bobbin with Windings

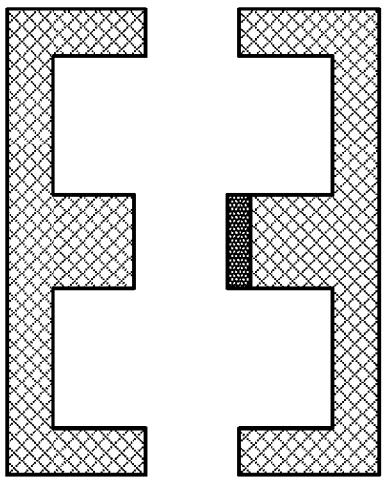
FIG. 21B

2100



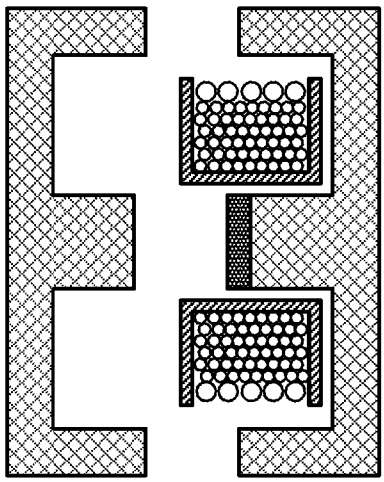
Solid Piece of Unmagnetized Magnetic Material with Height Greater than d

FIG. 21C



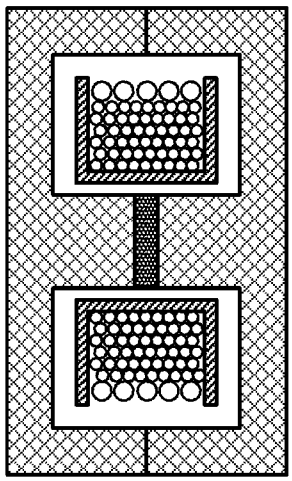
Unmagnetized Magnetic Material Fixed in Gap Area, Some Magnetic Material Removed so that h ≤ d

FIG. 21D



Bobbin with Windings Fitted to Core

FIG. 21E



Energy Transfer Element Assembled and Ready for Magnetizing

FIG. 21F

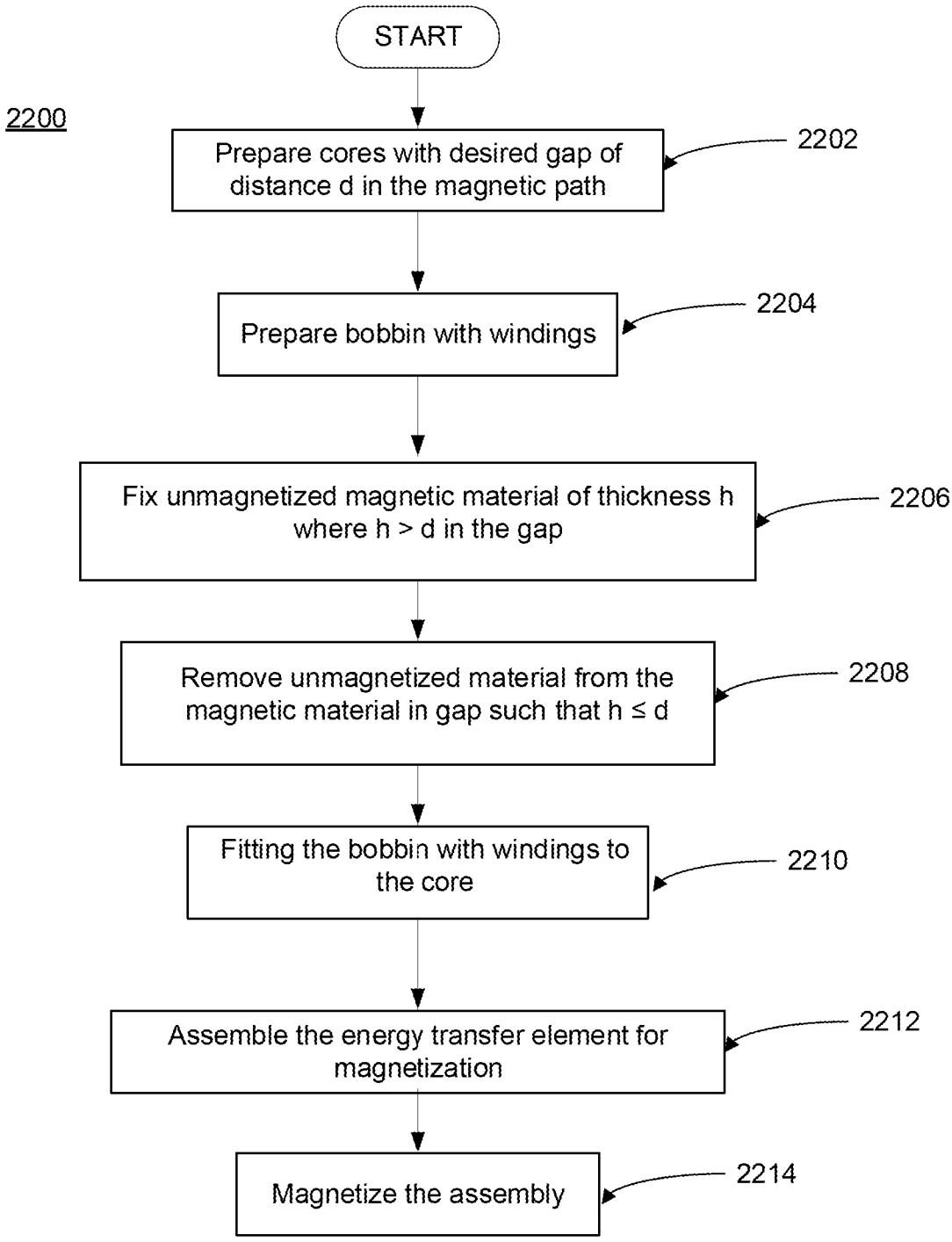
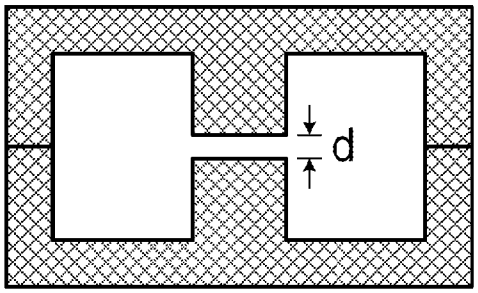
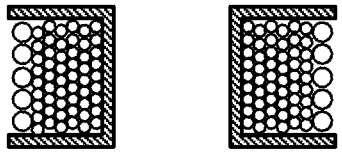

START
2200
Prepare cores with desired gap of distance d in the magnetic path
2202
Prepare bobbin with windings
2204
Fix unmagnetized magnetic material of thickness h where h > d in the gap
2206
Remove unmagnetized material from the magnetic material in gap such that h ≤ d
2208
Fitting the bobbin with windings to the core
2210
Assemble the energy transfer element for magnetization
2212
Magnetize the assembly
2214

FIG. 22



Set of Cores with Gap of Distance d

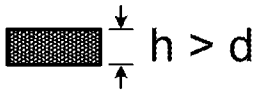
FIG. 23A



Bobbin with Windings

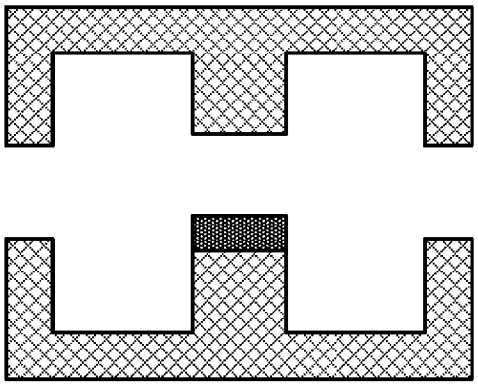
FIG. 23B

2300



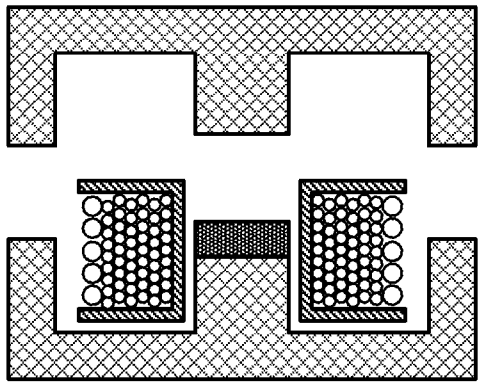
Deformable Solid Piece of Unmagnetized Magnetic Material with Height Greater than Distance d

FIG. 23C



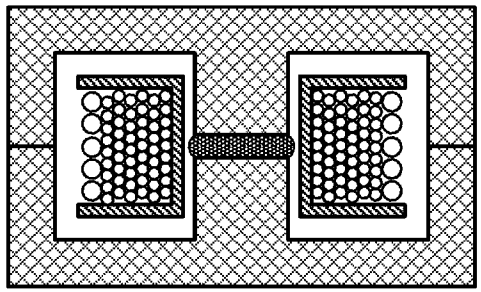
Unmagnetized Magnetic Material Fixed in Gap Area

FIG. 23D



Bobbin with Windings Fitted to Core

FIG. 23E



Assembly with Magnetic Material Deformed to Fit Gap Ready for Magnetizing

FIG. 23F

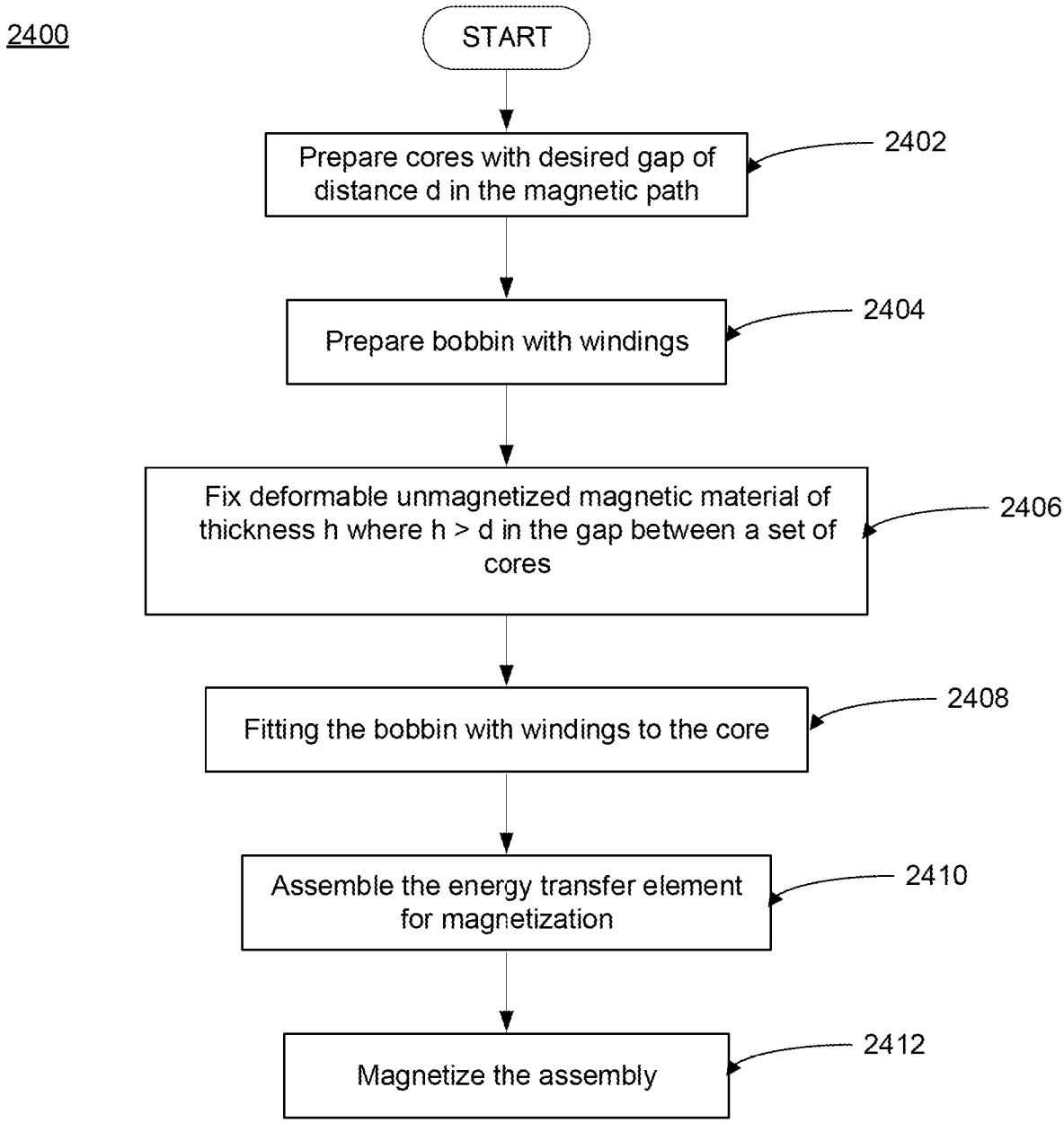

2400
START
Prepare cores with desired gap of distance d in the magnetic path
2402
Prepare bobbin with windings
2404
Fix deformable unmagnetized magnetic material of thickness h where h > d in the gap between a set of cores
2406
Fitting the bobbin with windings to the core
2408
Assemble the energy transfer element for magnetization
2410
Magnetize the assembly
2412

FIG. 24

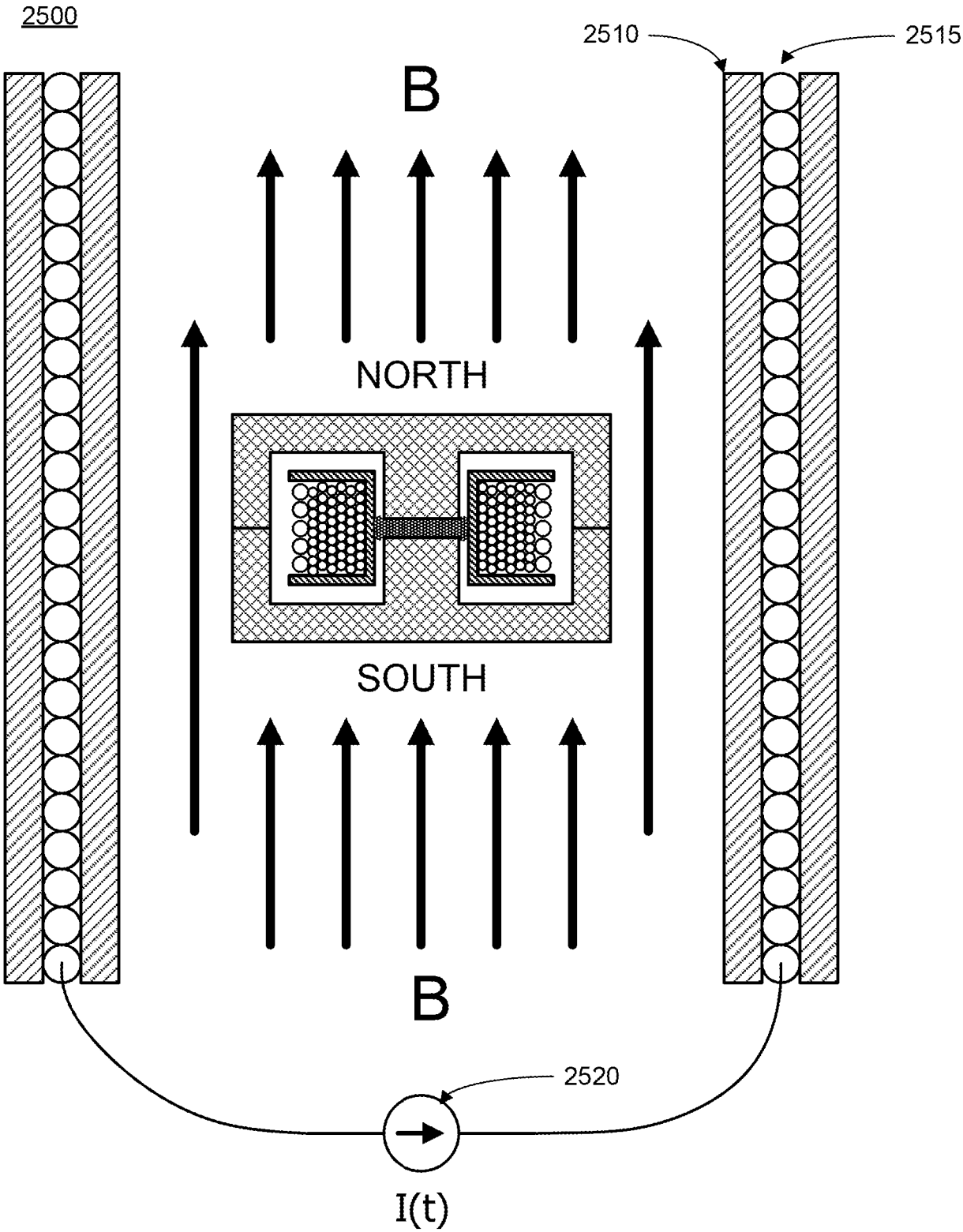


FIG. 25

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US2021/014104

A. CLASSIFICATION OF SUBJECT MATTER

IPC(8) - H02K 1/02; H01F 3/00; H01F 3/14; H02K 1/00 (2021.01)
CPC - H02K 1/02; H01F 3/00; H01F 3/14; H02K 1/00 (2021.02)

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

see Search History document

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

see Search History document

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

see Search History document

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2003/0030529 A1 (MIN et al) 13 February 2003 (13.02.2003) entire document	1-15
A	US 2014/0285138 A1 (DUSCHL-GRAW) 25 September 2014 (25.09.2014) entire document	1-15
A	US 3,921,114 A (BRIDEWELL et al) 18 November 1975 (18.11.1975) entire document	1-15
A	US 8,125,208 B2 (GYLAND) 28 February 2012 (28.02.2012) entire document	1-15
A	PERLEY et al. "An accurate flux density scale from 1 to 50 GHz", The Astrophysical Journal Supplement Series, Volume 204, Number 2, 25.01.2013. Retrieved on 17.03.2021. Retrieved from <URL: https://iopscience.iop.org/article/10.1088/0067-0049/204/2/19/meta> entire document	1-15

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:
"A" document defining the general state of the art which is not considered to be of particular relevance
"D" document cited by the applicant in the international application
"E" earlier application or patent but published on or after the international filing date
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
"O" document referring to an oral disclosure, use, exhibition or other means
"P" document published prior to the international filing date but later than the priority date claimed
"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
19 March 2021	APR 08 2021
Name and mailing address of the ISA/US Mail Stop PCT, Attn: ISA/US, Commissioner for Patents P.O. Box 1450, Alexandria, VA 22313-1450 Facsimile No. 571-273-8300	Authorized officer Blaine R. Copenheaver Telephone No. PCT Helpdesk: 571-272-4300