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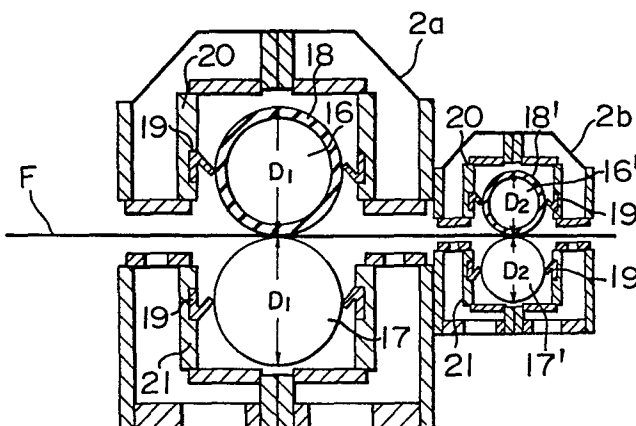
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**Continuous vacuum treating apparatus.**

A continuous vacuum treating apparatus for subjecting a workpiece (F) of soft material, such as a plastic molding to continuous surface treatment by an air-to-air system in vacuum, including a vacuum treating chamber (1) and a plurality of auxiliary vacuum treating chamber (1) and a plurality of auxiliary vacuum chambers (2a, 2b, 2c, 3a, 3b, 3c) located anterior and posterior to the vacuum treating chamber. The diameter of each of an upper seal roll (16) and a lower seal roll (17') of each of the auxiliary vacuum chambers (2b, 2c, 3b, 3c) located on the vacuum treating chamber side is smaller than the diameter of each of an upper seal roll (16) and a lower seal roll (17) of the auxiliary vacuum chamber (2a, 3a) located closest to the atmosphere.



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CONTINUOUS VACUUM TREATING APPARATUS

1 BACKGROUND OF THE INVENTION

(1) FIELD OF THE INVENTION

This invention relates to a continuous vacuum  
treating apparatus of an air-to-air system for continuously  
5 subjecting workpieces of soft material, such as plastic  
moldings, to surface treatment as with plasma in a vacuum  
treating chamber, wherein the plastic moldings refer to  
plastic films, plastic sheets, sheathed wires, etc.

(2) DESCRIPTION OF THE PRIOR ART

10 In one type of continuous vacuum treating appa-  
ratus of the air-to-air system known in the art, a  
plurality of roll seal boxes composed of seal rolls of  
metal are arranged on the inlet side and the outlet side  
of a vacuum treating chamber, and a workpiece of hard  
15 material, such as a metal tape, is conveyed from the  
atmosphere into the vacuum treating chamber through the seal  
roll boxes to apply a coat of metal to the surface of the  
workpiece as by vaporization deposition in a vacuum and  
then the workpiece thus treated is returned to the atmosphere  
20 through auxiliary vacuum chambers. Such continuous vacuum  
treating apparatus is disclosed in U.S. Patent No. 3,367,667,  
for example.

We have made a proposal to provide an apparatus  
for continuously subjecting workpieces of soft material,

1 such as plastic sheets, by an air-to-air system in a vacuum  
chamber to surface treatment as with plasma. This apparatus  
includes a plurality of auxiliary vacuum chambers located  
both anterior and posterior to the vacuum treating chamber  
5 with each auxiliary vacuum chamber being composed primarily  
of a pair of seal rolls.

In the apparatus referred to hereinabove, an  
airtight seal is satisfactorily provided to the auxiliary  
vacuum chambers. However, problems have been raised with  
10 regard to obtaining a compact overall size in a continuous  
vacuum treating apparatus and economizing on power.

More specifically, in order that the workpiece  
may be conveyed in good condition, it is necessary that an  
axial deflection of the pair of seal rolls constituting  
15 each auxiliary vacuum chamber caused by pressure differential  
be kept below a predetermined value (50  $\mu\text{m}$  for example).  
However, as subsequently to be described, a rise in the  
level of vacuum in the vacuum treating chamber can best be  
achieved by raising the level of vacuum in the auxiliary  
20 vacuum chamber located closest to the atmosphere. In this  
case, the differential pressure applied to the seal rolls  
is much smaller in the auxiliary vacuum chambers on the  
vacuum treating chamber side than in the auxiliary vacuum  
chamber closest to the atmosphere. Thus, in view of the  
25 need to keep the axial deflection of the seal rolls caused  
by pressure differential below the predetermined value, it  
is necessary to increase the diameter of the seal rolls in  
the auxiliary vacuum chamber closest to the atmosphere.

1 It has hitherto been usual practice in the prior art to  
use the seal rolls of the same diameter for the auxiliary  
vacuum chamber located closest to the atmosphere and the  
auxiliary vacuum chambers disposed on the vacuum treating  
5 chamber side.

Owing to this constructional arrangement, leaks  
through side pieces on opposite end faces of the seal rolls  
have increased in volume as the diameter of the seal rolls  
increases, and this has inevitably increased the capacity  
10 of the vacuum pumps and the size of the auxiliary vacuum  
chambers. Also, it has become necessary to increase the  
power of a system for driving each pair of seal rolls.

SUMMARY OF THE INVENTION

(1) OBJECT OF THE INVENTION

15 This invention has as its object the provision  
of a continuous vacuum treating apparatus enabling a compact  
size to be obtained in auxiliary vacuum chambers and allowing  
energy conservation to be achieved through a reduction in  
the drive force for driving the auxiliary vacuum chambers  
20 and the amount of air removed therefrom to make a vacuum.

(2) STATEMENT OF THE INVENTION

To accomplish the aforesaid object, the invention  
provides in a continuous vacuum treating apparatus  
comprising a vacuum treating chamber and a plurality of  
25 auxiliary vacuum chambers located anterior and posterior  
to the vacuum treating chamber for continuously treating

1 a workpiece in the vacuum treating chamber, the feature  
that the diameter of the seal rolls constituting each of the  
auxiliary vacuum chambers disposed on the vacuum treating  
chamber side is made smaller than the diameter of the seal  
5 rolls constituting the auxiliary vacuum chamber located  
closest to the atmosphere.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic vertical sectional view of  
the continuous vacuum treating apparatus comprising one  
10 embodiment of the invention;

Fig. 2 is a schematic plane view of the continuous  
vacuum treating apparatus shown in Fig. 1;

Fig. 3 is a sectional view of one of the  
auxiliary vacuum chambers of the continuous vacuum treating  
15 apparatus shown in Fig. 1, showing the constructional  
arrangement of the auxiliary vacuum chamber;

Fig. 4 is a sectional view taken along the line  
IV-IV in Fig. 3; and

Figs. 5 and 6 are views in explanation of the  
20 manner in which the side piece is mounted in the apparatus  
according to the invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

A preferred embodiment will now be described in  
detail by referring to the accompanying drawings.

25 Referring to Figs. 1 and 2, the continuous  
vacuum treating apparatus comprises a vacuum treating

1 chamber 1 for continuously subjecting a pliable workpiece  
F which may be a plastic film, formed as of a resin of the  
vinyl chloride base, to treatment with plasma in a vacuum,  
a plurality of auxiliary vacuum chambers 2 located anterior  
5 to the vacuum treating chamber 1 and a plurality of  
auxiliary vacuum chambers 3 located posterior to the vacuum  
treating chamber 1. The vacuum treating chamber 1 is  
evacuated via an exhaust pipe 5 by a vacuum pump 4 to achieve  
a pressure of about  $10^{-2}$  Torr therein.

10           The plurality of auxiliary vacuum chambers 2 and 3  
are evacuated via exhaust pipes 7 by vacuum pumps 6, to  
achieve pressures in a vacuum therein which are slightly  
higher than the pressure achieved in the vacuum treating  
chamber 1 but successively reduced in one auxiliary vacuum  
15 chamber to another from the atmospheric pressure level.

          The workpiece F to be treated is fed by feed  
means 8 through the auxiliary vacuum chambers 2 located  
anterior to the vacuum treating chamber 1 to the vacuum  
treating chamber 1 where it is subjected to treatment with  
20 plasma, before being moved through the auxiliary vacuum  
chambers 3 located posterior to the vacuum treating chamber  
1 and wound on take-up means 9. A drive motor 10 generates  
a drive force which is transmitted via a line shaft 11 and  
stepless transmissions 12, 13, 14 and 15 to the vacuum  
25 treating chamber 1 the auxiliary vacuum chambers 2 and 3  
and take-up means 9. The speeds of driving systems for the  
vacuum treating chamber 1, auxiliary vacuum chambers 2 and  
3 and take-up means 9 are suitably adjusted by the

1 transmissions 12, 13, 14 and 15, respectively.

Figs. 3 and 4 show the essential portions of the auxiliary vacuum chambers arranged in a plurality of numbers anterior to the vacuum treating chamber 1. Figs. 3 and 4 show the auxiliary vacuum chambers located anterior to the vacuum treating chamber 1, but the auxiliary vacuum chambers located posterior to the vacuum treating chamber 1 are similar to those shown in these figures.

Referring to Figs. 3 and 4, the auxiliary vacuum chamber 2a located closest to the atmosphere and the auxiliary vacuum chamber 2b located adjacent the auxiliary vacuum chamber 2a on a side of opposite the vacuum treating chamber 1 differ from each other in the size of the chamber and the diameter of the seal rolls. More specifically, the auxiliary vacuum chamber 2b nearer the vacuum treating chamber 1 is smaller than the auxiliary vacuum chamber 2a closest to the atmosphere in the size of the chamber and the diameter of the seal rolls. The numerals 16 and 17 designate the upper and lower seal rolls constituting the auxiliary vacuum chamber 2a closest to the atmosphere, the upper seal roll 16 having a coat 18 of resilient material, such as rubber, applied to its outer periphery by baking to become unitary with the seal roll 16 and the lower seal roll 17 having a coat of hard material, such as chromium, nickel, etc., applied to its outer periphery. The upper and lower seal rolls 16 and 17 each have a diameter  $D_1$  which is about 250 mm. The numerals 16' and 17' designate upper and lower seal rolls constituting the auxiliary vacuum

i chamber 2b nearer the vacuum treating chamber 1, the upper seal roll 16' having a coat 18' of resilient material applied to its outer periphery and the lower seal roll 17' having a coat of hard material, such as chromium, nickel, etc., applied to its outer periphery. The upper and lower seal rolls 16' and 17' of the auxiliary vacuum chamber 2b nearer the vacuum treating chamber 1 each have a diameter  $D_2$  which is about 100 mm or smaller by about 1/2.5 than the diameter  $D_1$  of the seal rolls 16 and 17 of the auxiliary vacuum chamber 2a closest to the atmosphere. In the embodiment shown and described herein, the diameters  $D_1$  of the auxiliary vacuum chamber 2a and the diameters  $D_2$  of the auxiliary vacuum chambers. 2b are described as having a ratio  $D_1/D_2$  of about 2.5/1. However, the invention is not limited to this ratio of  $D_1$  and  $D_2$ , and it is possible to keep the deflection of the seal rolls at a level below a predetermined value if the ratio  $D_1/D_2$  is in the range between 2/1 and 3/1. The reference numeral 19 designates ripple members secured to upper and lower cases 20 and 21 in positions in which they are in spaced juxtaposed relation and extend axially of the upper and lower seal rolls 16, 16' and 17, 17' along their outer peripheries. 22 and 22' are side pieces providing a seal to opposite end faces of the upper and lower seal rolls 16 and 17. Coats 23 and 23' of fluorine resin are applied by baking to surfaces of the side pieces 22 and 22' which are positioned against the seal rolls 16 and 17 respectively.

Figs. 5 and 6 show the manner in which the side

1 pieces 22 and 22' are mounted. As shown, the side pieces  
22 and 22' are mounted in such a manner that they are in  
contact with opposite end faces of the seal rolls 16 and  
17 and the cases 20 and 21. The side piece 22 sealing one  
5 end face (left end face shown in Fig. 3) is forced by the  
biasing force of coil springs 24 against the upper and  
lower seal rolls 16 and 17 and the cases 20 and 21 in a  
manner to be axially movable. A bearing housing 26 is  
located in a manner to enclose the side piece 22. By  
10 virtue of this structural arrangement, leaks between the  
side piece 22 and bearing housing 26 can be reduced to a  
minimum even if the side piece 22 is axially moved together  
with the seal roll 16 by the thermal expansion of the seal  
rolls 16 and 17 during operation of the continuous vacuum  
15 treating apparatus. This is conducive to increased vacuum  
maintained in the auxiliary vacuum chambers.

The side piece 22' sealing the other end face  
(right end face shown in Fig. 3) of the upper and lower seal  
rolls 16 and 17 is secured by bolts 25' to the cases 20 and  
20 21 so as to be immovable in an axial direction. Like the  
side piece 22, the side piece 22' is also enclosed by a  
bearing housing 26'.

For driving the upper and lower seal rolls 16 and  
17, a drive force is transmitted from the lower seal roll  
25 17 via gears 27 and 28 shown in Fig. 3 to the upper seal  
roll 16.

Operation of the continuous vacuum treating  
apparatus comprising a plurality of auxiliary vacuum chambers

1 of the aforesaid construction located anterior and posterior  
to the vacuum treating chamber will be described.

The workpiece F, such as a plastic film, is  
conveyed from the atmosphere side successively through the  
5 auxiliary vacuum chambers 2a, 2b and 2c to the vacuum  
treating chamber 1. At this time, a seal is provided  
between the upper seal roll 16 and lower seal roll 17  
constituting each auxiliary vacuum chamber through which the  
workpiece F is conveyed by forcing the coat 18 of resilient  
10 material on the upper seal roll 16 against the coat of hard  
material on the lower seal roll 17 so as to deflect the  
coat 18 of resilient material on the upper seal roll 16. A  
seal is provided between the upper and lower seal rolls 16  
and 17 and the upper and lower cases 20 and 21 by causing  
15 the ripple members 19 to be positioned against the upper and  
lower seal rolls 16 and 17. A seal is provided between the  
upper and lower seal rolls 16 and 17 and the side piece 22 by  
forcing the side piece 22 against the upper and lower cases  
20 and 21 through the resilient means 24.

20 A seal is provided to the auxiliary vacuum chambers  
2b and 2c located on the vacuum treating chamber side in the  
same manner as a seal is provided to the auxiliary vacuum  
chamber 2a closest to the atmosphere.

As described hereinabove, the auxiliary vacuum  
25 chamber 2a closest to the atmosphere where the differential  
pressure is high (between 600 and 700 Torr) is constituted  
by the pair of seal rolls 16 and 17 of large diameter, so  
that no deflection develops in the seal rolls 16 and 17

1 and the workpiece F can be readily conveyed.

In the auxiliary vacuum chambers 2b and 2c of low differential pressure (2 to 150 Torr) located on the vacuum treating chamber side, the diameter of the upper and lower rolls is smaller by about 1/2.5 than that of the upper and lower rolls of the auxiliary vacuum chamber closest to the atmosphere, so that deflection of the seal rolls above a predetermined value can be avoided and the vacuum in the chambers can be kept at a satisfactory level. This enables a high level of vacuum (0.03 Torr) to be achieved in the vacuum treating chamber 1. Since the size of the auxiliary vacuum chambers 2b and 2c is reduced, energy can be conserved through a reduction in the amount of air removed and the drive force for driving each auxiliary vacuum chamber. Returning to the description of the operation, the workpiece F introduced into the vacuum treating chamber 1 is treated with a plasma produced between a treating drum 30 serving as a cathode and a plurality of anodes 31 located around the treating drum 30 after being led to the treating drum 30. Following this treatment in the vacuum treating chamber 1, the workpiece F is continuously led through the auxiliary vacuum chambers 3 located posterior to the vacuum treating chamber 1 to be delivered to the atmosphere side.

25 Table 1 shows the degree of vacuum achieved in each of the auxiliary vacuum chambers 2a, 2b and 2c (3a, 3b and 3c) in relation to the differential pressure and the speed at which evacuation is accomplished by the vacuum pump. As

1 can be seen clearly in Table 1, the differential pressure  
in the auxiliary vacuum chamber 2a closest to the atmosphere  
is markedly higher than that in the auxiliary vacuum chamber  
2c nearest the vacuum treating chamber 1. Thus, one only  
5 has to take into consideration the axial deflection of the  
seal rolls 16 and 17 in the auxiliary vacuum chamber 2a  
closest to the atmosphere where the differential pressure is  
maximized.

According to the invention, the diameters of the  
10 seal rolls constituting the auxiliary vacuum chambers 2b  
and 2c (3b and 3c) located on the vacuum treating chamber  
side are made smaller than that of the seal rolls constitut-  
ing the auxiliary vacuum chamber 2a (3a) closest to the  
atmosphere. By virtue of this feature, it is possible to  
15 avoid the occurrence of an axial deflection of the seal  
rolls during the time the workpiece F is being conveyed while  
keeping the level of vacuum in the vacuum treating chamber  
1 at a high level, thereby enabling a compact size to be  
obtained in auxiliary vacuum chambers and allowing energy  
20 conservation to be achieved through a reduction in the amount  
of air removed and in the drive force required for driving  
the seal rolls.

Table 1

	Rate of removing air by vacuum pump	Degree of vacuum	Differential pressure
Atmosphere		760 Torr	600 to 700 Torr
Auxiliary vacuum chamber 2a	15,000 litre/min	60 to 160 Torr	10 to 150 Torr
Auxiliary vacuum chamber 2b	15,000 litre/min	10 to 50 Torr	2 to 49.5 Torr
Auxiliary vacuum chamber 2c	7,500 litre/min	0.5 to 8 Torr	0.47 to 7.97 Torr
Vacuum treating chamber 1	40,000 litre/min	0.03 Torr	

The total rate of removing air: 77,500 litre/min.

1                    Table 2 to Table 4 show the degree of vacuum achieved in each of the auxiliary vacuum chambers 2a, 2b and 2c (3a, 3b and 3c) in relation to the speed at which evacuation is accomplished during the time a workpiece is  
5 conveyed continuously through the auxiliary vacuum chambers to the vacuum treating chamber, showing the sealing effects achieved in the auxiliary vacuum chambers and the vacuum treating chamber.

Table 2

	Degree of vacuum	Rate of removing air by vacuum pump
Auxiliary vacuum chamber 2a	60 Torr	30,000 litre/min
Auxiliary vacuum chamber 2b	20 Torr	15,000 litre/min
Auxiliary vacuum chamber 2c	1 Torr	15,000 litre/min
Vacuum treating chamber 1	0.03 Torr	40,000 litre/min

Table 3

	Degree of vacuum	Rate of removing air by vacuum pump
Auxiliary vacuum chamber 2a	200 Torr	15,000 litre/min
Auxiliary vacuum chamber 2b	65 Torr	30,000 litre/min
Auxiliary vacuum chamber 2c	6 Torr	15,000 litre/min
Vacuum treating chamber 1	0.05 Torr	40,000 litre/min

Table 4

	Degree of vacuum	Rate of Removing air by vacuum pump
Auxiliary vacuum chamber 2a	300 Torr	15,000 litre/min
Auxiliary vacuum chamber 2b	100 Torr	15,000 litre/min
Auxiliary vacuum chamber 2c	20 Torr	30,000 litre/min
Vacuum treating chamber 1	0.3 Torr	40,000 litre/min

1           As can be clearly seen in Table 2 to Table 4, with  
the total rate of removing air by the vacuum pumps to achieve  
the vacuum in the vacuum treating chamber and the auxiliary  
vacuum chambers being constant, the rate of removing air  
5 from the auxiliary vacuum chamber 2a closest to the  
atmosphere had better be raised to keep the vacuum in the  
vacuum treating chamber 1 at a high level. In this connec-  
tion, it is to be noted that a rise in the degree of vacuum  
in the auxiliary vacuum chamber 2a closest to the atmosphere  
10 leads to a rise in the level of vacuum in the vacuum treating  
chamber 1.

## WHAT WE CLAIM IS:

1. A continuous vacuum treating apparatus comprising:

a vacuum treating chamber (1) for continuously  
5 treating a workpiece (F) of soft material in a vacuum;  
and  
a plurality of auxiliary vacuum chambers  
(2a, 2b, 2c, 3a, 3b, 3c) located anterior and posterior  
to said vacuum treating chamber (1), each of said  
10 auxiliary vacuum chambers comprising an upper seal roll  
(16, 16') and a lower seal roll (17, 17') forming a pair  
maintained in contact with each other and arranged to  
extend perpendicular to a direction in which said work-  
piece (F) of soft material is conveyed, a plurality of  
15 pairs of ripple members (19) having the ripple members  
of each pair being located in spaced juxtaposed relation  
and extending axially of one of the seal rolls (16, 16',  
17, 17') along its outer periphery, and a pair of side  
pieces (22, 22') each positioned against one of opposite  
20 end faces of the pair of upper and lower seal rolls  
(16, 16', 17, 17') characterized in that the diameter  
of each of the upper and lower seal rolls (16', 17') of the  
auxiliary vacuum chambers (2b, 2c, 3b, 3c) disposed on  
the vacuum treating chamber side is made smaller than  
25 that of each of the upper and lower seal members (16,  
17) of the auxiliary vacuum chamber (2a, 3a) located  
closest to the atmosphere.

2. A continuous vacuum treating apparatus as  
claimed in claim 1, characterized in that the diameter  
30 of each of the seal rolls (16', 17') of each of the  
auxiliary vacuum chambers (2b, 2c; 3b, 3c) on the  
vacuum treating chamber side is about 1/2 to 1/3  
that of each of the seal rolls (16, 17) of the auxiliary  
vacuum chamber (2a, 3a) located closest the atmosphere.

3. A continuous vacuum treating apparatus as claimed in claim 1 or 2, characterized in that at least one of the upper seal roll (16, 16') and lower seal roll of each of said plurality of auxiliary  
5 vacuum chambers (2a, 2b) between which said workpiece (F) of soft material is inserted has a coat (23, 23') of soft material applied to its outer periphery and extending axially, said coat (23, 23') of soft material being axially deflected to provide a seal axially between the  
10 upper and lower seal rolls (16, 17; 16', 17').

4. A continuous vacuum treating apparatus as claimed in one of the claims 1 to 3, characterized in that said vacuum treating chamber (1) is adapted to  
15 subject said workpiece (F) of soft material of treatment with plasma.

5. A continuous vacuum treating apparatus as claimed in one of the claims 1 to 4, characterized in that each of said side pieces (22, 22') is enclosed by  
20 a bearing housing (26, 26').

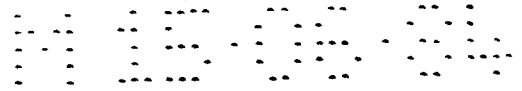


FIG. 1

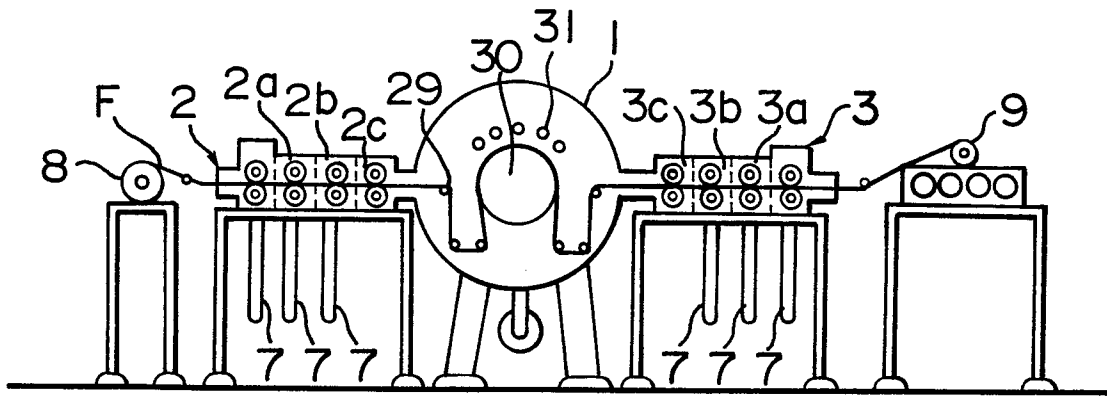


FIG. 2

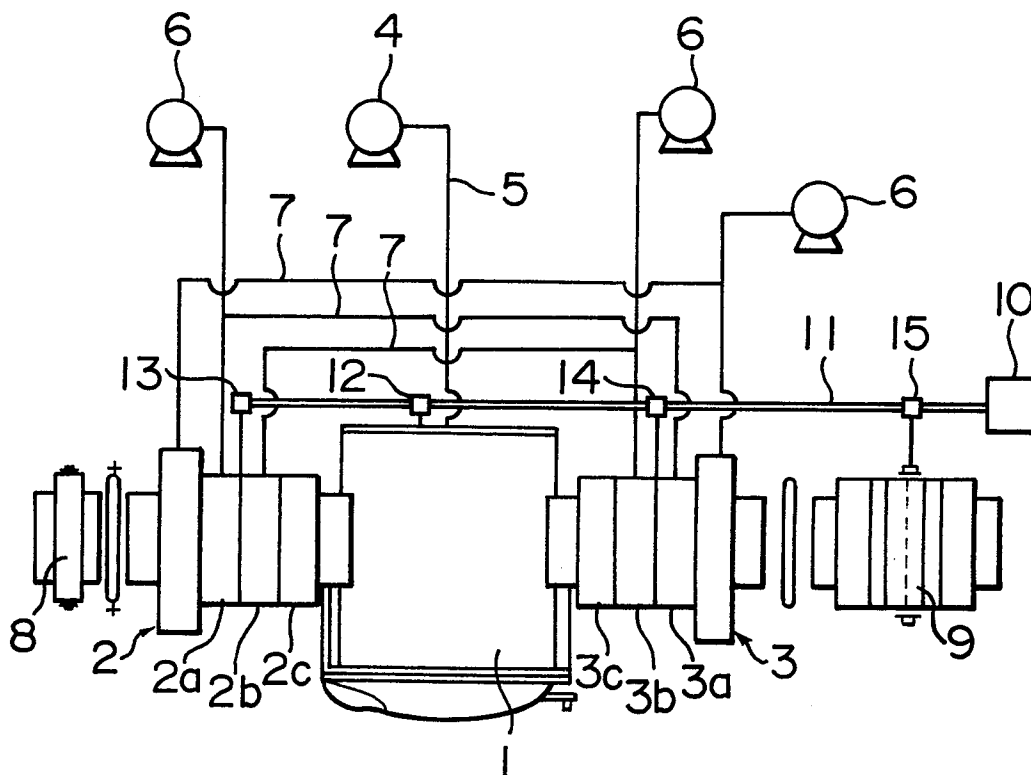


FIG. 3

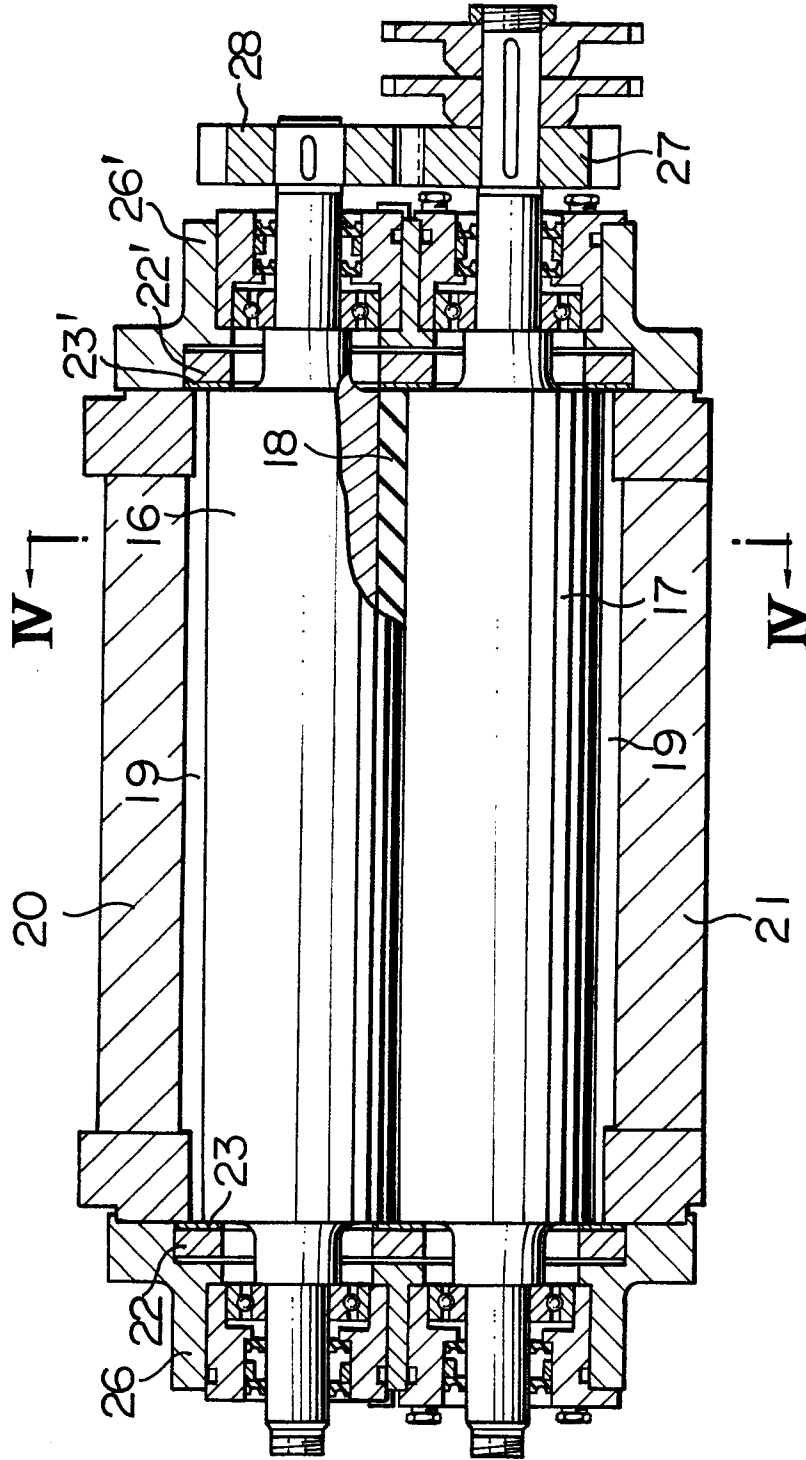


FIG. 4

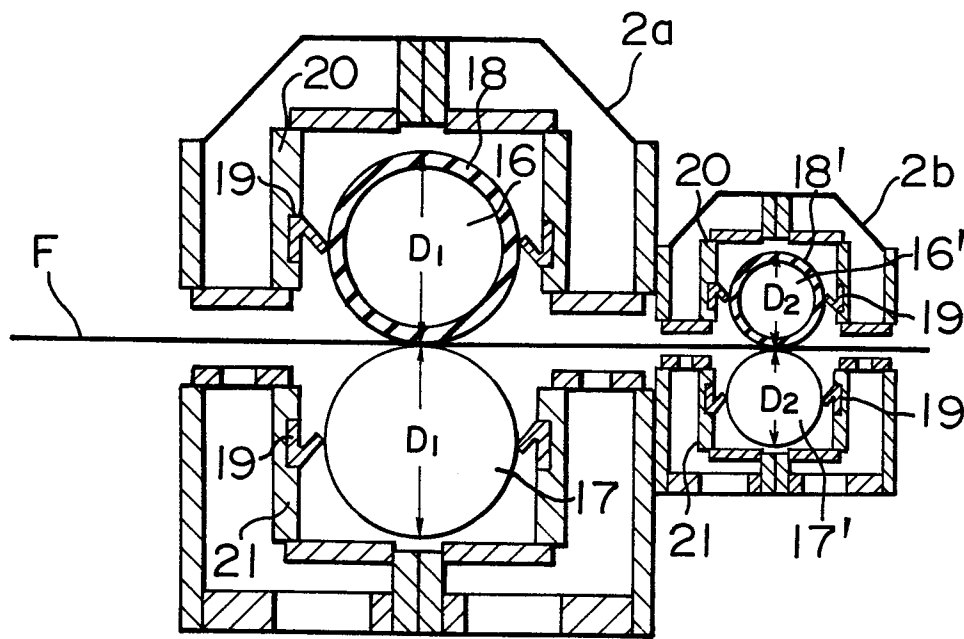


FIG. 5

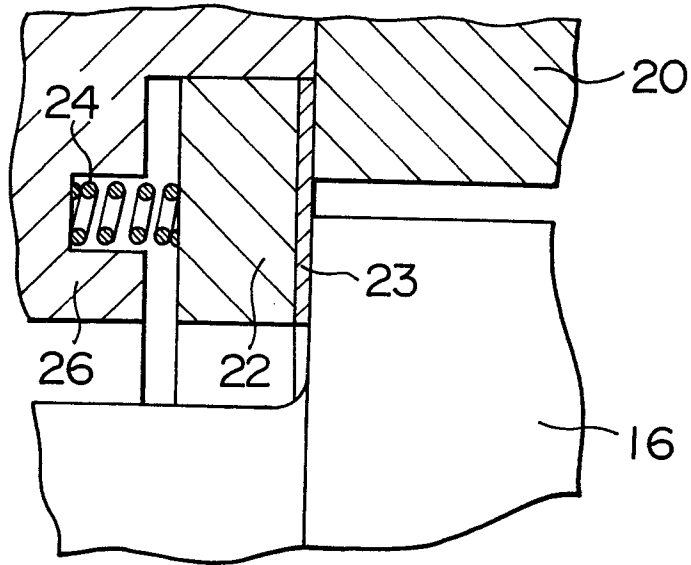
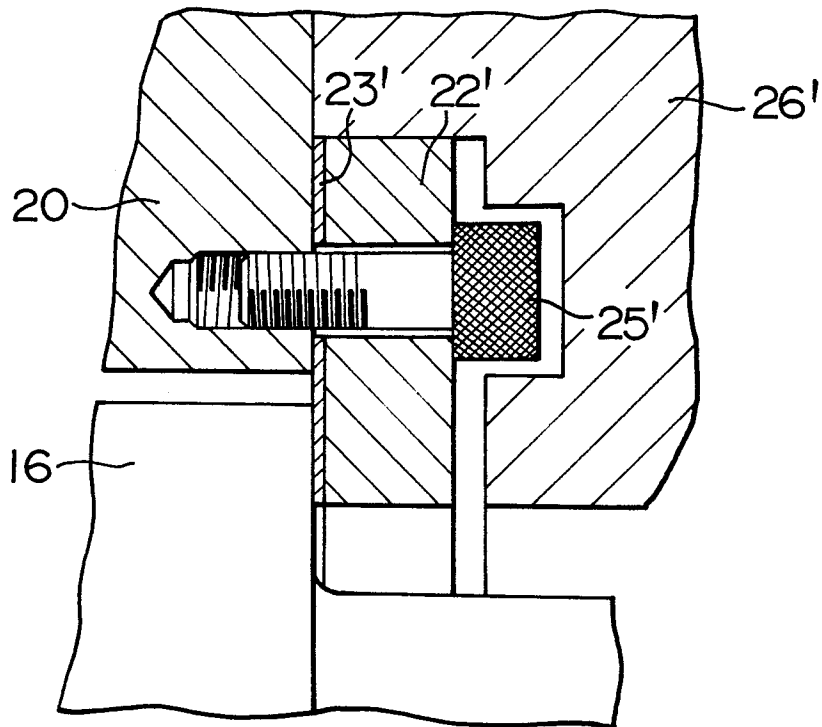


FIG. 6





EP 84106879.4

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. <sup>3</sup> )
A	DE - A1 - 3 129 997 (HITACHI LTD) * Claims; fig. 1,7 * --	1-5	C 23 C 13/10 B 29 D 7/20 B 05 D 3/00
A	DE - A1 - 3 124 280 (SHIN-ETSU) * Claims; fig. 1,4 * --	1-5	
A,D	US - A - 3 367 667 (WILLIAM S. ALLEN) * Totality * ----	1-5	
			TECHNICAL FIELDS SEARCHED (Int. Cl. <sup>3</sup> )
			C 23 C B 29 D B 05 D B 05 C
The present search report has been drawn up for all claims			
Place of search VIENNA		Date of completion of the search 11-09-1984	Examiner SCHÜTZ
<b>CATEGORY OF CITED DOCUMENTS</b> X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			