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(54) CALCIUM PHOSPHATE POLYMER COMPOSITE AND METHOD

KALZIUMPHOSPHATPOLYMERVERBUNDSTOFF UND VERFAHREN

COMPOSITE DE POLYMÈRE ET DE PHOSPHATE DE CALCIUM ET PROCÉDÉ DE PRODUCTION
DE CELUI-CI

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DescriptionFIELD OF THE INVENTION

5 [0001] The present invention relates generally to biomaterials for bone replacement. More particularly, the present invention relates to a mineral polymer composite.

BACKGROUND OF THE INVENTION

10 [0002] Over 10 million Americans carry at least one major implanted medical device in their body. Among these implants, bone fracture and damage cases constitute a large proportion, and result in more than 1.3 million bone-repair procedures per year in the USA. In general, bone tissue has the capability of postnatal self-construction. However, in severe pathological situations such as complicated fractures, trauma, bone tumors, congenital defects or spinal fusion, the damaged bone will not form or regenerate spontaneously. To repair the damaged bone, autografts, long-considered 15 the gold standard in bone grafting, have problems of resource limitation and morbidity associated with graft harvest, while the allogenic bones from tissue banks have the disadvantages of immune response due to genetic differences and the risk of inducing transmissible diseases. As a result, various synthetic materials have been developed for bone repair applications.

20 [0003] Since the discovery of osteoinductivity Bone Morphogenetic Proteins (BMPs), the bone repair process has been greatly advanced by applying these proteins for therapeutic use. Some of the BMPs, such as BMP-2, in particular have been well studied and have gained interest as therapeutic agents. BMP-2 induces bone formation *in vivo* by stimulating differentiation of mesenchymal stem cells toward an osteoblastic lineage, thereby increasing the number of differentiated osteoblasts capable of forming bone. The stimulation of BMP on osteoblast differentiation plays a major role in bone healing. Recently, regulatory agencies in the U.S., Europe, Canada and Australia have approved devices 25 containing BMP-2 and BMP-7 as bone-graft substitutes for the treatment of long bone fractures and interbody fusions of the spine. Despite its strong osteoinductive activity, clinical use of BMP-2 has been hampered by the lack of suitable delivery systems. An efficacious delivery system is needed to have sustained BMP release with appropriate dosing at the defect site. Both *in vitro* and *in vivo* studies have suggested that a dose response can be produced to affect the cell 30 activities and the bone formation rate. The longer the release time of the BMP-2, the more fully the cells expressed sustained osteoblastic traits *in vitro* and the more bone formation *in vivo*. Thus, there is a pressing need to develop a synthetic carrier that has high initial structural integrity and sustained release of single or multiple agents known to induce bone regeneration. At the same time, these materials should undergo slow controlled resorption, eliminating the need for subsequent surgical removal. Such materials could have great clinical value when incorporated into medical devices.

35 [0004] Metallic materials have been widely used due to their high mechanical strength. However, the high strength of metallic implants normally reduces the stress in the surrounding materials (stress shielding), which weakens the adjacent bones. In addition, metal implants may release ions, which can cause adverse tissue reactions.

40 [0005] Furthermore, bone fixation devices composed of metal have a number of known problems such as stress shielding at the implant site and possible removal in a second surgery. Thus, absorbable implants for bone fixation have been developed to provide strength for healing and biodegradation for eventual replacement of the device with bone tissue. Design of bone fixation devices must consider tensile and bending strengths, their respective elastic modulus, 45 biocompatibility, ability to support new bone growth, 3-dimensional structure and density, porosity and rate of degradation. Natural bone has a bending modulus in the range of about 3 to 30 MPa. An optimum bone fixation device is expected to be near or in this range for desired clinical utility. Although this has been generally recognized as a factor it has not been successfully put into practice.

50 [0006] Current devices are made from absorbable polymers and/or minerals, and often in a composite form. The minerals are most often calcium phosphate compounds. The absorbable polymers are most often synthetic aliphatic polyesters, polyethers, polycarbonates or their combinations. A problem with absorbable polymers is that in non-fiber form their strength is low. Absorbable fibers have much improved tensile strength, but suffer from low bending modulus. A problem with calcium phosphates is that despite high hardness, they are brittle. Thus, the right combination of these 55 components is lacking in the current absorbable bone fixation devices.

[0007] In contrast to metallic implants, polymer-based implants have a more stable bone/implant interface during physiological loading. In addition, some polymers are biodegradable *in vivo*, and can be gradually replaced by living tissue, which is the best repair for defects. Unfortunately, polymers have relatively poor mechanical properties, which greatly restrict their usefulness in many applications. A second drawback arises because nearly all polymeric materials are bioinert, so they are consequently not osteoconductive, resulting in poor surface continuity. In order to achieve the osteoconductivity of the polymeric material, calcium phosphate, a bioactive ceramic material, is added to the polymer matrix to produce calcium phosphate-reinforced polymer composites. Most of these composites still have the low mechanical strength as pure polymer materials. Thus, there is a pressing need to identify novel calcium phosphate-reinforced

polymer composites with sufficient mechanical strength for load-bearing skeletal implants.

[0008] Calcium phosphate (CaP)-reinforced polymer composites were originally envisioned as biomaterials for bone replacement on the basis of producing appropriate mechanical compatibility, as well as the required biocompatibility. According to published reports, up to 50 wt% of CaP was incorporated into the polymer matrix to achieve sufficiently high values of elastic modulus. Unfortunately, the composites lacked sufficient toughness for use in different applications.

[0009] There are a number of factors that influence the design of a skeletal implant. Structurally, bone is a nano carbonated hydroxyapatite (calcium phosphate) reinforced fibrous collagen composite. The calcium phosphate crystals, which take the form of platelets, are embedded within the collagen fiber matrix and are aligned along the fibers. These mineral-containing fibrils are arranged into lamellar sheets, which run helically with respect to the major axis of the cylindrical osteons. The preferential orientation of bone minerals and the interfacial bonding between the mineral and collagen fibers play an important role in determining the overall mechanical performance of the bone. Thus, the stiffness or average elastic modulus of bone is variable, but lies in the range of 3 to 30 GPa. At least three basic features must be addressed in device design: the property match between bone and the material of construction, the interface between this material and the bone, and the long-term stability of the overall assembly in the *in-vivo* environment.

[0010] Natural bone development and regeneration are regulated by a series of growth factors, so it is often desirable to deliver more than one of multiple exogenous growth factors during bone formation and repair. It has been found that a combination of BMP-2 and transforming growth factor- β (TGF- β) greatly enhanced bone healing compared to BMP-2 or TGF- β delivered separately. Unfortunately, most drug delivery systems are not able to systematically control the delivery multiple growth factors. It would be advantageous if sequential delivery can be designed into a carrier system.

[0011] To achieve a maximum benefit, it is best to mimic nature's delivery of multiple growth factors in a programmed, sequential manner. Thus, the type and delivery kinetics of growth factors, and the type of carrier material all play a decisive role in the therapeutic success of any bone-repair process.

Xiaoyan et al. (J. of biomedical material research, vol. 57, 2001, 141) discloses a composite bone repair material comprising poly(lactic acid) fibers coated with calcium phosphate. The fiber can be first braided before being immersed into an SBF solution or they can be directly immersed in the SBF solution.

[0012] According to a first aspect of the present invention there is provided a bone-repair composite as defined in claim 1.

[0013] The novel calcium phosphate/polymer fiber composite consists of many components with different degradation rates, such as polymer fibers, calcium phosphate, and low-melting temperature polymer coatings, all of which can be used as drug carrier materials. The biodegradable polymer fibers, including poly(L-lactic) acid (PLLA), polyglycolic acid (PGA), polydioxanone (PDO) are coated with a thin layer of calcium phosphate. They can then be braided using a method according to one embodiment to fabricate sutures. The braids are coated with a layer of low-melting temperature biodegradable polymer. In addition, braids are woven or knitted to form sheet-shaped composites. The unique design and fabrication sequence make it possible to use the composite as a sophisticated drug delivery system featuring designed release of more than one drug. The drugs are those that are suitable for varied bone repair applications, such as long-bone repair, spinal fusion, sternal bone closure, maxillofacial fixation and the like, although other drugs such as antibiotics are also feasible.

[0014] Preferably, the ratio of the core to the sheath is provided to maximize the mechanical strength of the bone-repair composite to mimic the mammalian bone. The bending modulus of the bone-repair composite is at least 3 GPa, wherein the bending modulus of the bone-repair composite is similar to a cortical bone. The bone-repair composite can be subjected to a hot compression molding at an elevated temperature, whereby melting the polymers having a lower melting temperature, and thus binding the polymers having a higher melting temperature with the polymers having a lower melting temperature. The bone-repair composite can be subjected to a cold compression molding using a solvent, wherein the solvent is vaporized to melt the sheath, thus binding the sheath to the core, wherein the solvent is selected from a group of solvents, such as toluene, xylene, ethyl acetate, and acetone. The second group of polymers includes a low-temperature melting polymer or a binding polymer. The bone-repair composite is unidirectional or multidirectional. The bone-repair composite further includes filling materials including drugs or bioactive agents, wherein the filling material is used as a binding material or for drug release. The polymer is selected from a group consisting of poly(L-lactic) acid (PLLA), polyglycolic acid (PGA), poly(ϵ -caprolactone) (PCL), and PDO. The calcium phosphate compound layer is selected from a group consisting of ion-substituted apatite, calcium phosphate, carbonate hydroxyapatite, fluorinated hydroxyapatite, chlorinated hydroxyapatite, silicon-containing hydroxyapatite, tricalcium phosphate, tetracalcium phosphate, monotite, dicalcium phosphate, dicalcium phosphate dihydrate, octocalcium phosphate, calcium phosphate mono-

hydrate, alpha-tricalcium phosphate, beta-tricalcium phosphate, amorphous calcium phosphate, biphasic calcium phosphate, tetracalcium phosphate, calcium deficient hydroxyapatite, precipitated hydroxyapatite, oxyapatite, calcium sulfate, and calcium containing phosphate minerals. The calcium phosphate compound layer is fully or partially aligned to a fiber axis or a polymer crystallites. The calcium phosphate compound layer is anchored to the polymer surface by electrostatic coordinative, or chemical tethering. The bone-repair composite is formed by varying the ratio of the core and the sheath.

[0015] In accordance with another embodiment of the invention, there is provided a method for making a bone repair synthetic composite according to claim 9. The method can further include the use of elevated temperature in combination with solvent. The use of solvent in a pultrusion process allows the composite to achieve a high calcium phosphate mineral concentration to reach an optimal level of modulus. The inner core structure is formed by assembling a plurality of yarns together; rolling a mesh structure, wherein the mesh structure is knitted, woven, non-woven, braided, stacked, flocked, or felted; or rolling the plurality of yarns and the mesh structure together. A tertiary structure of a desired shape is formed by binding a plurality of the secondary structures or the primary structures with a binding material. The inner core is designed to facilitate water access rate and cellular access rate both longitudinally and laterally, wherein the longitude access is controlled by time, degradation, and/or solubilization of the inner core, wherein the lateral access is controlled by braid density, coating, or binder of the binding material. The surface modifying chemical is alkaline, acidic, oxidizing, ionic or electrostatic. The mineral layer is either hydrodynamically aligned/coated or randomly applied onto the polymer fiber by dip or die coating of the polymer fiber using suspension of mineral particles in solvents or polymer solutions. The mineral is coated using an alternating soaking technique, a simulated body fluid technique, supersaturated calcium phosphate solutions, dip coating, sol-gel coating, electrophoresis, electrochemical coating, extrusion coating, pultrusion or brush-on coating methods.

[0016] There has thus been outlined, rather broadly, certain embodiments of the invention in order that the detailed description thereof herein may be better understood, and in order that the present contribution to the art may be better appreciated. There are, of course, additional embodiments of the invention that will be described below and which will form the subject matter of the claims appended hereto.

BRIEF DESCRIPTION OF THE DRAWINGS

[0017]

FIG. 1 is a chart showing comparative percent retained tensile strength for PLLA suture in pH 7.4 buffer solution at 37 °C and 50 °C.

FIG. 2 is a chart showing percent retained tensile strength for PLLA yarn in pH 7.4 buffer solution at 50 °C.

FIG. 3 depicts PLA yarns (a) before hydrolysis and (b) after hydrolysis with 1 N NaOH for 1 min according to an embodiment of the invention.

FIG. 4 depicts the amount of CaP deposited on a yarn with increasing repetition cycles and increasing deposition time.

FIG. 5 depicts ESEM images showing CaP deposition process on PLA yarn after (a) first (b) third (c) fifth and (d) sixth cycles using a cyclic soaking technique according to an embodiment of the invention.

FIG. 6 depicts an XRD pattern of monetite (CaHPO₄) deposited after a sixth cycle according to an embodiment of the invention.

FIG. 7(a), (b), (c), (d), and (e) depict ESEM images of the PLA film subjected to a cyclic soaking process according to an embodiment of the invention.

FIG. 8 is a schematic of the mechanism of nucleation and growth of CaP on a hydrolyzed polyester yarn surface according to an embodiment of the invention.

FIG. 9 depicts tensile stress-strain curves of the composites fabricated at various conditions according to an embodiment of the invention.

FIG. 10(a) and (b) depict the mechanical testing results for flexural properties of the composites prepared at various conditions according to an embodiment of the present invention.

FIG. 11 demonstrates the effect of etching time on the Young's modulus of PLLA drawable single fiber before and after HA coating.

FIG. 12 is a chart showing the stiffening effect of HA coating on unaligned fibers.

FIG. 13 demonstrates the effect of etching time on the tensile stress of PLLA drawable single fibers before and after HA coating. Treating conditions: [NaClO]= 0.05 M, 25.0±0.2 °C. Coating conditions: 3×SBF, 60 °C, 2 h.

FIG. 14(a) and (b) demonstrate alkaline-treated drawn yarn with biomimetic coating.

FIG. 15(a) and (b) depict a comparison of the alkaline-treated undrawn PLLA yarns with drawing and without drawing after biomimetic coating with hydroxyapatite.

FIG. 16 is a schematic of the fabrication of the novel composite according to an embodiment of the invention showing steps (a) - (h).

FIG. 17 depicts a composite construction according to one embodiment of the invention.

FIG. 18 depicts the Young's modulus and flexual strength of pure PCL, PCL-PLLA, and PCL-HA-PLLA.

FIG. 19 depicts HA particles used in a bone-repair composite.

FIG. 20 depicts a Stress-strain curve of a bone-repair composite.

FIG. 21 depicts an apparatus used for pultrusion of composite.

5 FIG. 22 illustrates the alignment of HA particles within PLLA fibers by electrospinning HA particles in a dimethylformamide solution.

FIG. 23 is a flowchart of a design for fabrication of composites according to an embodiment of the invention.

FIG. 24 depicts various composite constructions according to four embodiments (a) - (d) of the invention.

10 DETAILED DESCRIPTION

CYCLIC PRECIPITATION TECHNIQUE

[0018] The invention will now be described with reference to the drawing figures, in which like reference numerals

15 refer to like parts throughout. An embodiment in accordance with the present invention provides a method for making a bone repair synthetic composite with calcium phosphate and absorbable fibrous materials. After a few coating cycles, a desired amount of calcium phosphate is coated onto the fibrous materials. The fibrous materials are then assembled into a unidirectional composite using a poly(ϵ -caprolactone) matrix. Furthermore, growth factors may be incorporated within the absorbable fibrous materials, such that the release of the growth factors may be controlled through the various 20 degradation rates of the fibrous materials.

Introduction

[0019] Natural bone is a complex hierarchical structure of mineralized collagen consisting of an orderly deposition of 25 hydroxyapatite $[\text{Ca}_{10}(\text{PO}_4)_6(\text{OH})_2]$ (calcium phosphate) within a type I collagen matrix. Recent efforts for fabricating new functional biomaterials involved mimicking these hierarchical structures, albeit using complex chemistry and tedious procedures. Calcium phosphates, mainly as a hydroxyapatite coating on polymer surfaces, not only enhance tissue compatibility, but also can be deployed as hard-tissue generation matrix.

[0020] As used herein, the term "calcium compound," "calcium phosphate compound," "calcium phosphate mineral 30 compound" or "calcium phosphate" can be minerals or substances which can include some combination or compound including a form of calcium phosphate, including, but not limited to, ion-substituted apatite, calcium phosphate, carbonate hydroxyapatite, fluorinated hydroxyapatite, chlorinated hydroxyapatite, silicon-containing hydroxyapatite, monocalcium phosphate, monocalcium phosphate monohydrate, amorphous calcium phosphate, biphasic calcium phosphate, calcium deficient hydroxyapatite, oxyapatite, precipitated hydroxyapatite, bone-like apatite, tricalcium phosphate, tetracalcium 35 phosphate, monetite, dicalcium phosphate, dicalcium phosphate dihydrate, octacalcium phosphate, alpha-tricalcium phosphate, beta-tricalcium phosphate, calcium sulfate, or other calcium containing phosphate minerals.

[0021] Poly-L-lactic acid (PLLA) yarn is prepared by melt extrusion of thoroughly dried PLLA resin. The yarn can be 40 produced in a range of deniers by varying the number of filaments and the denier per filament. In a typical extrusion at a spinning temperature of about 240°C, undrawn 30 filament PLLA is collected on a bobbin then drawn about five times its original length with heat in the range of about 100 to 110°C to give 120 denier yarn with a tensile strength in the range of about 3.8 to 4.2 grams per denier. The drawing can be done in either one or more stages.

[0022] The PLLA yarn can be used to fabricate composites either directly with minimal strength enhancing steps or 45 indirectly through a braided suture structure that might involve annealing or hot-stretching to enhance strength and resorption characteristics. Yarns can be processed as is on skeins or after plying and overbraiding with a small sheath to keep the yarn in place but not interfere with coating steps. As one example, forty ends of 135 denier yarn is plied together and used as a core in an eight carrier braider with two bobbins of 120 denier PLLA yarn and a gear ration of 82/72 to obtain a braid with about 4 to 5 picks per inch.

[0023] PLLA fiber provides a retained strength profile that is well suited for orthopedic applications. Fully processed 50 PLLA suture will retain about 50 to 60% of its original tensile strength after eighteen months at 37°C in buffer solution. In accelerated *in vitro* testing at 50°C it has been found that one week at 50°C corresponds to about one month at 37°C (see FIG. 1). When unprocessed PLLA yarn is tested at 50°C (see FIG. 2) it retains about 50 to 60% of its initial strength at eight weeks which corresponds to about eight months at 37°C. Thus, depending on the processing of the PLLA yarn there is a range of about eight to eighteen months that will be needed for the PLLA to retain 50 to 60% of its original tensile strength.

[0024] A key step in the fabrication of these composites is the nucleation and growth of CaP on the supporting polymer 55 matrix. A biomimetic deposition process was developed wherein the polymer substrates were soaked in simulated body fluid (SBF). SBF contains ions such as Na^+ , K^+ , Ca^{2+} or Mg^{2+} with concentration and pH similar to that of human blood plasma. Contact of SBF with a surface can lead to the formation of calcium phosphate on the surface. Other coating

methods, such as plasma spray and co-precipitation can also be used. However, an inherent drawback of the biomimetic coating method using SBF is the amount of time required to deposit a large quantity of calcium phosphate (normally a few days to a few weeks), because the driving force for precipitation is small.

[0025] In the present invention, to achieve high modulus composites, polymer fibers were coated with CaP utilizing a cyclic-soaking technique, which permits controlled fabrication of composites with higher mechanical properties. A cyclic soaking technique was used for the nucleation and growth mechanism of CaP on poly(lactic acid) (PLA) fibers at room temperature. The deposition of CaP on the polymer surface was characterized using gravimetric measurements and environmental scanning electron microscopy (ESEM) images. These results are crucial for understanding the possible mechanism of mineralization in tissues in general, and fabrication of high-modulus composites for tissue engineering applications in particular.

Example

CaP Coating on Fully Drawn PLA Yarn

[0026] Commercially available poly-lactic acid (PLA) yarn ($M_w \sim 121$ kDa, $T_g \sim 55$ °C, $T_m \sim 175$ °C) was obtained from Teleflex Medical Incorporated. Each yarn contained about 30 filaments, with the filaments having an average diameter of 24.5 μ m. The PLA yarn was wound around a rectangular, using a custom-built winding machine that allowed for the control of winding speed and tension. During this stage, care was taken to avoid overlapping of the yarn on the frame. A linear spinning rate of 20 cm/min and a tension of approximately 6 N were used for all the experiments. The yarn was then soaked in 1 N NaOH for 1 min. at 25 °C to saponify the surfaces of fibers. The soaked yarn was rinsed in distilled water and air-dried.

[0027] The saponification process was checked in several ways. In one test, water contact angles of the treated PLA films were measured by the sessile drop technique (advancing angles) using a contact angle measurement apparatus (Rame-hart Model 100, USA). To fabricate the films, PLA yarn was dissolved in chloroform and solvent cast at room temperature to obtain a thin film which was hot-pressed (Model 2731, Carver Laboratory Press, USA) at 150 °C for about 2 min. under a hydraulic pressure of 100 MPa to remove any bubbles formed during solvent casting. The PLA film thus obtained was cut into 1 cm² pieces and treated with 1 N NaOH for 1 min at room temperature. The treated films were rinsed twice in distilled water and dried. A 5- μ L water drop was placed on the surface of each PLA film (NaOH treated and untreated), and the contact angle was measured to determine the wettability of the specimen. All measurements were recorded at room temperature and each test was repeated five times on different films.

[0028] CaP was deposited on the hydrolyzed PLA yarn using a cyclic soaking technique as follows: 100 mL of calcium nitrate (99% pure, Sigma) and 164 mL of ammonium orthophosphate (99% pure, Sigma) solutions were prepared at a concentration of 1 N, and the pH of each solution was brought up to 12 by adding ammonium hydroxide (Sigma, ACS reagent). The solutions were kept at room temperature while stirring vigorously. The treated yarn was initially soaked in the calcium nitrate solution for a set amount of time from about 0.5 h to about 1 h at room temperature. Then the yarn was washed in distilled water with simultaneous stirring and air-drying. The stirring rate during washing was varied between 80-800 rpm for 0.5 or 1 h to determine its effect on the amount and quality of CaP deposited on the yarn. The dried yarn was soaked in ammonium phosphate solution for the same amount of time, washed and dried in the same fashion as that for calcium nitrate solution. The amount of CaP deposited on the yarn was measured gravimetrically after each cycle. This cyclic soaking process was repeated six times, beyond which the deposited CaP was observed to detach from the PLA yarn. Fresh solutions of calcium nitrate and ammonium phosphate were used for each cycle, to avoid the deposition of CaP particles suspended in the used solutions.

Composite Preparation (not part of the invention)

[0029] To prepare the composites, the CaP-coated yarn was coated with 2 vol% PCL (MW = 43 kDa) solution and air-dried overnight in a vacuum to remove excess solvent. A Carver Laboratory Press (Model 2731, USA) was used for compression molding of composites. Initially, the parallel platens in the hot-press were heated to about 55 °C and maintained for about 30 min. A custom-made, three-piece aluminum rectangular mold containing six slots each of 4 cm x 0.5 cm x 0.5 cm dimensions was stacked with PLA yarn coated with CaP and PCL and held at 55 °C for about 2 min. under a hydraulic pressure of about 150 MPa. Finally, the mold was cooled to room temperature under the same pressure and the specimens were detached from the mold. Typically, specimens prepared using this mold had dimensions of 4 cm x 0.5 cm x 0.2 cm with the specimen thickness varying slightly for different types of composites.

CaP Coating on PLA Film (not part of the invention)

[0030] Poly(lactic acid) yarn dissolved in chloroform was solvent-cast at room temperature and hot-pressed at about

150 °C for about 2 min. to obtain a smooth film of 0.5-mm thickness. The PLA film was hydrolyzed in 1 N NaOH for 1 min, washed multiple times in distilled water and air-dried. CaP was deposited on the hydrolyzed PLA film using the same cyclic-soaking technique as employed for PLA yarn (see [0052]).

5 **Characterization of the PLA Yarn and PLA Film**

[0031] The gold-coated surfaces of the as-received PLA yarn, as-pressed PLA film, PLA yarn and film after hydrolysis and after each cycle of biominerization were observed using an environmental scanning electron microscope (Philips ESEM 2020) operating at 20 kV. An X-ray diffractometer (Bruker AXS D 5005) with a Ni-filtered Cu-K α radiation was 10 used for the X-ray defraction (XRD) measurements after the CaP powder was isolated by dissolving the CaP-coated yarn in tetrahydrofuran (THF) and repeatedly washing the residuals with ethanol. Data was collected using a scan speed of 1.0 °/min and a scan step of 0.02°.

15 **Mechanical Testing of Composites**

[0032] A three-point bending test (ASTM D790) was used to measure the flexural modulus and flexural strength at 20 break of the fabricated composites. An Instron test machine (1011 Instron Instruments, UK) with a 50-N load cell was employed with a cross-head speed of 1 mm/min. The ratio of length to thickness of the specimen was 16. The flexural stress and strain were calculated from the load and deflection data collected on a data acquisition system. Six specimens were tested for each type of composite (explained in Table 2) with a three-level full-factorial experimental design with no repetitions.

Results and Discussion

25 **Hydrolysis of PLA Yarn**

[0033] Surface hydrolysis of the PLA yarn was achieved by soaking the as-obtained yarn in an aqueous solution of 1 N NaOH for 1 min. The hydroxide anions in the solution are expected to hydrolyze the ester groups on the surface of the 30 yarn, resulting in the breakage of polymer chain and the formation of -COO⁻ and -OH groups on the termini of the two new chains. FIG. 3a, b shows PLA yarn before and after treatment, respectively. While the PLA yarn remained intact during hydrolysis, the average fiber diameter decreased slightly from 24.58±0.82 to 23.59±0.57 μ m ($t = 3.44$ and $p=0.002$) and the surface of individual fibers appeared slightly rougher [FIG. 3b]. The observed decrease in the diameter of the polyester yarn was likely due to hydrolysis at multiple points on the polymer chains near the surface, reducing the polymer to smaller fragments which were soluble in the solution. Surface hydrolysis of polyesters is known to result in 35 enhanced hydrophilicity, indicative of an increase in the amount of carboxylic acid and hydroxyl groups on the surface, which corresponds to the reduction in contact angle from 81.6° to 75.4° for the NaOH-treated PLA films. Previous studies have shown that carboxylic acid groups can promote the nucleation of CaP on substrates. Moreover, due to its higher surface energy, rougher surfaces might facilitate rapid growth of CaP compared to the smooth surfaces. Though higher concentration of NaOH or higher soaking time contributes to further increase of surface functionalization, it might result 40 in faster degradation or bulk hydrolysis of PLA yarn.

CaP Coating on PLA Yarn

[0034] Using a cyclic soaking technique at room temperature, the net amount of CaP deposition was found to increase 45 with soaking repetitions as well as with soaking time for each repetition. As shown in FIG. 4, the amount of deposited CaP increased with soak time. The amount of CaP deposited for 1-h soak time was larger than that for 0.5-h soak time at all repetitions. Gravimetric analysis indicated that around 35 wt% of CaP was deposited after 6 cycles each at 1-h soaking time.

[0035] In a similar study involving the calcium phosphate deposition on chitosan using a cyclic soaking method, 57 wt% of calcium phosphate was deposited after 15 repetitive cycles of 15 min each. There was also a decrease in the 50 amount of CaP retained on PLA yarn with increasing stirring rate ($p = 0.005$) during the washing of yarn in distilled water. Table 1 illustrates the decrease in the net amount of CaP deposited after a first repetition cycle with increasing stirring rate from 100 to 800 rpm and with increasing stirring time during washing of coated yarn in distilled water.

Table 1.

Stirring rate, rpm	Wt % of CaP deposited			
	0.5-h stirring time		1-h stirring time	
	0.5-h deposition time	1-h deposition time	0.5-h deposition time	1-h deposition time
100	8.14	9.21	7.62	9.71
300	7.59	8.85	7.22	9.1
500	7.1	8.07	7.01	8.66
800	6.77	7.9	6.84	8.15

[0036] Table 2 details the amount of CaP deposited on the yarn with increasing number of cycles and soaking time for each cycle. Even higher number of cycles resulted in the detachment of CaP from the yarn.

Table 2.

Repetition cycles	wt% CaP deposition		Flexural modulus, GPa	
	0.5-h soak time	1-h soak time	0.5-h soak time	1-h soak time
1	7.8	9.45	-	-
2	12.4	17.4	-	-
3	16.5	23.7	-	-
4	19.2	29.4	-	-
5	22.4	33.6	3.94	4.66
6	23.3	35.1	6.45	7.89

[0037] A consistent increase of modulus with increasing CaP content in the composites was observed (Table 2). A flexural modulus as high as 7.9 GPa was achieved for the composites prepared under the conditions of 1 h soaking at each step and after 6 soaking cycles. This value of modulus falls into the lower end of the elastic modulus of human cortical bone, 3-30 GPa. The toughness of the composite can be measured using a three-point bending test to find out the energy required to fracture the composite. None of the composites broke in a brittle fashion during the bending test, indicating that the composites not only had a high modulus, but also superior toughness. The toughness of the composite can be measured as the area under the stress-strain curve, having a unit of joules per cubic meter. The composite's shape, thickness, and size and the testing speed can be varied when applying the three-point bending test. Furthermore, the tension test can also be used to test the toughness of the composite. Annex A1 of ASTM D 882 provides a description for the tension test.

[0038] The macroscopic structure of the CaP deposited on the PLA yarn obtained from 1-h deposition time cycles was analyzed by ESEM. Compared to the plain hydrolyzed yarn shown in FIG. 3b, heterogeneous nuclei of CaP can be seen clearly on the surface of the yarn as shown in FIG. 5a. As the repetition cycles increased, the deposition on the fibers increased and the morphology of the yarn changed progressively as shown in FIG. 5a-d. These findings are in qualitative agreement with the gravimetric analysis of the deposit on the yarn. From the images in FIG. 5, it can be observed that the CaP was not coated uniformly on the entire surface of the yarn after first cycle. Rather, heterogeneous CaP deposits were observed in the ESEM images taken randomly over the entire surface of the hydrolyzed yarn. However, during subsequent cycles, these deposits grew to cover additional surfaces of the yarn. After the fifth and sixth cycles, the yarn surface was completely covered with large amounts of CaP. The carboxylate groups along the surface of the treated yarn should provide favorable sites for Ca^{2+} ions to bond to the substrate, thereby providing a site for the formation of CaP nuclei.

[0039] The CaP phase deposited on the PLA yarn as judged from the XRD pattern shown in FIG. 6 was observed to be monetite (CaHPO_4). Multiple peaks that could be assigned to monetite were detected around $2\theta = 26^\circ, 32^\circ$ and 40° . The peaks at $2\theta = 26^\circ, 31^\circ, 32^\circ$ and 33° were assigned to the (002), (211), (112) and (300) diffractions of monetite, respectively. Earlier investigations suggest that monetite is bioactive and can be used as bone-inducing mineral.

CaP Coating on PLA Film Using a Cyclic Soaking Method (not part of the invention)

[0040] To elucidate the observed phenomenon of CaP formation on the hydrolyzed polyester yarn *via* heterogeneous nucleation and growth process, CaP coating was done on the hydrolyzed PLA film surface using the same cyclic soaking procedure. The non-hydrolyzed film subjected to cyclic soaking treatment exhibited no signs of nucleation, while the hydrolyzed film (FIG. 7a) demonstrated the nucleation of CaP after first cycle (FIG. 7b). During the second, third and fourth cycles, the CaP grew rapidly from the initial deposits, though the surface of the film in the background can be clearly seen. FIG. 7d represents the film which was partially hydrolyzed and coated with calcium phosphate and the distinction between the coated and the non-coated areas can be clearly seen. The CaP grown on PLA film displayed a thin, platelet-like crystalline morphology as shown in FIG. 7e similar to the calcium phosphate deposited *via* the biomimetic process using SBF.

[0041] During the initial stages of nucleation, the interaction between Ca^{2+} and carboxyl groups on hydrolyzed polyester surface might lead to the formation of a complex such as $-\text{COO}-\text{Ca}^{2+}-\text{NO}_3^-$ or $-(\text{COO})_2\text{Ca}^{2+}$ through ion exchange. During soaking in ammonium phosphate solution, it is expected that phosphate ions will interact with the calcium ions on the yarn surface, as shown in FIG. 8.

[0042] FIG. 8 is a schematic of the mechanism of nucleation and growth of CaP on the hydrolyzed polyester yarn surface. In FIG. 8a, hydrolysis of polyester surface exposed the carboxyl groups on the surface containing sodium ions. In FIG. 8b, during the first soaking cycle in calcium nitrate solution, Na^+ ions are replaced with Ca^{2+} ions leading to the formation of $-(\text{COO})_2\text{Ca}$, with $-\text{COO}\text{Ca}^{2+}\text{NO}_3^-$ as by-product (not shown). FIG. 8c depicts the formation of bonds between HPO_4^{2-} and Ca^{2+} during the first soaking cycle.

[0043] An analysis of the nuclei formation and growth thereafter is essential in understanding the CaP forming conditions on the polymer substrate. Since the substrate was washed after each soaking cycle, formation of nuclei in the solution can be ruled out. It is generally believed that heterogeneous nucleation is dominant at low supersaturations. Moreover, heterogeneous nucleation is kinetically and thermodynamically favorable as the interaction between a growing nucleus and a substrate surface represents a lower net interfacial energy than a small nucleus in the surrounding solution. This indicates that the initial calcium binding to the substrate may govern the deposition process during the initial stages. The overall reaction occurring during the precipitation of monetite from these aqueous solutions can be written as:



[0044] These results can be compared to the reports involving biominerization of CaP on polymers by soaking the substrate in SBF for prolonged period of time to deposit the mineral. The induction period for the nucleation of calcium phosphate on polymer substrates in SBF was almost 24 h, independent of the kind of organic polymer. Calcium phosphate deposition was initiated by the nucleation of calcium phosphate induced by dissolved silicate and calcium ions arising from the bioactive glass. In a similar study involving calcium phosphate deposition on silk fibers using SBF route, the authors reported that the functionalized silk surface took 7 days to induce minimal amount of calcium phosphate in SBF, while the non-functionalized silk surface didn't show any signs of deposition even after 7 days. In all the above studies, CaP with bone mineral composition and structure (i.e., hydroxyapatite) was produced in SBF. However, the deposition of CaP on the substrate took much more time compared to the cyclic soaking technique.

Mechanical Properties of the Composites

[0045] FIG. 9 depicts tensile stress-strain curves of the composites fabricated at various conditions. The flexural properties of the composites are shown in FIG. 10. When the mechanical properties of the PLA-PCL-CaP composites were compared to those of constituent polymers with no CaP loading, significantly higher modulus values were observed, which demonstrates the indirect effect of deposition time and repetition cycles in improving the modulus multifold. Table 2 describes the notation used for the composites prepared at various soaking times and cycles. The composites prepared with 1-h soaking time and 6 repetitions (1-h-6x) exhibited a modulus value of 7.9 GPa while those prepared with 0.5-h soaking time and 5 repetitions (0.5-h-5x) showed 3.9 GPa. Nevertheless, all the composites tested in this study demonstrated modulus values in the range 2.4-7.9 GPa, which are at the lower end of the 3-30 GPa range of the bending modulus of human physiologic bone.

[0046] In general, the rule of mixtures provides the simplest method for the estimation of the mechanical properties of the composites in terms of its constituents. For the elastic modulus, the parallel model based on *iso*-strain and the series model based on the *iso*-stress assumptions have been usually employed. The parallel model (Eq. 2) provides the upper-limit value of the modulus E_p , while the series model (Eq. 3) gives the lower-limit E_s . The equations are:

$$E_p = \phi E_f + (1-\phi) E_m \quad (2)$$

$$E_s = [\phi/E_f + (1-\phi)/E_m]^{-1} \quad (3)$$

5 where ϕ is the volume fraction of the filler in the composite and E_f and E_m are the moduli of filler and matrix in the composite, respectively. The predicted modulus values from the models were calculated taking into account the modulus of pure PLA-PCL composite with no filler (2.45 GPa as observed for the PLA-PCL composite in this study) as E_m and the modulus of CaP (50 GPa) as E_f , density of PLA-PCL as 1.3 and density of CaP as 3.16. As expected, the moduli of the composites observed in this study fall within the upper and lower bounds calculated using the parallel and series models.

10 [0047] In addition, the bending moduli and flexural strength at yield of the composites tested in the present study are significantly higher than the values reported in literature for PLA-CaP composites. An important factor contributing for the observed increase in the bending yield strength of these composites, compared to the conventional PLA-CaP composites, is the unidirectional alignment of PLA yarn coupled with the CaP particles surrounding them. It can be expected that by increasing the CaP content in the composites, higher modulus can be achieved. For example, calculations 15 indicate that modulus values in the range of 10-15 GPa are possible, depending upon the level of each component.

BIOMIMETIC COATING TECHNIQUE

Calcium Phosphate Coating on Sodium Hydroxide Treated Drawn Yarns

20 [0048] Initially, drawn PLLA yarns are treated with sodium hydroxide. 500 mL sodium hydroxide solution with a chosen molar concentration (0.100-1.00 mol/L) was prepared with sodium hydroxide 1 mol/L solution and de-ionized water at room temperature. Then, a certain amount of drawn PLLA yarns were dipped into prepared sodium hydroxide solution for certain amount of time (2-60 min) at chosen temperature. Next, the treated drawn PLLA yarns were taken out of the sodium hydroxide solution and washed with de-ionized water 3-5 times before being wiped dry and left in the air over night.

25 [0049] After treating the PLLA yarns with sodium hydroxide, layers of calcium phosphate are coated on the PLLA yarns with a biomimetic coating method. First, a SBF solution is prepared by adding sodium chloride, sodium bicarbonate, potassium chloride, potassium hydrogen phosphate, magnesium chloride, 4-(2-hydroxyethyl)-1-piperazineethanesulfonic acid, calcium chloride and sodium sulfate into de-ionized water under sufficient stirring. Then, hydrochloric acid 30 solution was added and the pH value of the solution was adjusted to around 6.0-7.0. Next, sodium hydroxide treated drawn PLLA yarns were dipped into prepared SBF solution and warmed up to certain temperature (40-60 °C) under the biomimetic coating procedure. The treated drawn PLLA yarns were coated with calcium phosphate after 1-6 h and taken out of SBF solution. Then, the coated drawn PLLA yarns were washed with de-ionized water for several times. Lastly, the coated and washed drawn PLLA yarns were air dried overnight.

Calcium Phosphate Coating on Sodium Hydroxide Treated Undrawn PLLA Yarns

35 [0050] Initially, undrawn PLLA yarns were treated with sodium hydroxide. A certain amount of sodium hydroxide solution (20-500 mL) with molar concentration 0.500 mol/L was prepared. Then, a certain amount of undrawn PLLA yarns were dipped into prepared sodium hydroxide solution for 10 min at room temperature. Next, treated undrawn PLLA yarns were taken out of the sodium hydroxide solution and washed with de-ionized water 3-5 times before being wiped dry and air dried over night.

40 [0051] After treating the undrawn PLLA yarns with sodium hydroxide, layers of calcium phosphate are coated on the undrawn PLLA yarns with a biomimetic coating method. First, a SBF solution is prepared by adding sodium chloride, sodium bicarbonate, potassium chloride, potassium hydrogen phosphate, magnesium chloride, an appropriate buffer like HEPES or Tris, calcium chloride and sodium sulfate into de-ionized under sufficient stirring. Then, hydrochloric acid 45 solution was added and the pH value of the solution was adjusted to around 6.0-8.0. Next, sodium hydroxide treated undrawn PLLA yarns were dipped into prepared SBF solution and heated up to certain temperature (40-60 °C). The treated undrawn PLLA yarns were coated with calcium phosphate after 1-4 h and taken out of SBF solution. Then, the 50 coated undrawn PLLA yarns were washed with de-ionized water for several times. Lastly, the coated and washed undrawn PLLA yarns were air dried over night.

55 [0052] In addition to the etching with sodium hydroxide solutions, the etching process can be carried out in sodium hypochlorite or calcium hydroxide solutions and then similarly coated with biomimetic calcium phosphate. Figures 11, 12 and 13 show the effect of treatment time on the Young's modulus of drawable PLLA filament before and after the biomimetic hydroxyapatite coating.

[0053] FIG. 11 demonstrates the effect of etching time on the Young's modulus of PLLA drawable single fiber before and after HA coating. The PLLA fibers were etched with $[\text{NaClO}] = 0.05 \text{ M}$, $25.0 \pm 0.2 \text{ }^\circ\text{C}$, and coated at $60 \text{ }^\circ\text{C}$, 2 h with 3×SBF. FIG. 12 is a chart showing the stiffening effect of HA coating on unaligned fibers. FIG 13 demonstrates the

effect of etching time on the tensile stress of PLLA drawable single fibers before and after HA coating. The PLLA fibers were treated with $[NaClO] = 0.05$ M, 25.0 ± 0.2 °C and coated with $3 \times SBF$, 60 °C, 2 h.

[0054] In both cases, a minimum etching time of six minutes yields coated filaments with increased values of Young's modulus. The data also shows that if the treatment time is too long the Young's modulus of the uncoated filament is reduced with the increased etching.

Primary Study on Calcium Phosphate Particles' Orientation on Sodium Hydroxide Treated PLLA Yarns

[0055] A comparison of undrawn PLLA yarns and drawn PLLA yarns were conducted. First, undrawn PLLA yarns with 3-4 cm length were warmed up in water bath to 55-65 °C. They were drawn to double length in the water bath, wiped dry and left in the air for 10 min. Next, a 20mL of sodium hydroxide solution with a molar concentration of 0.500 mol/L were prepared. Then, a same length of undrawn PLLA yarns and newly drawn PLLA yarns were dipped into the prepared sodium hydroxide solution for 10 min at room temperature. The treated PLLA yarns were taken out of the sodium hydroxide solution and washed with de-ionized water 3-5 times before being wiped dry and air dried over night.

[0056] Similar to the above stated method, a SBF solution was prepared. Then, the sodium hydroxide treated PLLA yarns were dipped into the prepared SBF solution and heated up to a certain temperature (40-60 °C). Extra SBF solution was also heated up at the same time. The treated PLLA yarns were coated with calcium phosphate after 0.5-1.0 h and taken out of SBF solution.

[0057] Next, the PLLA yarns coated after the first cycle (0.5-1.0 h) were drawn in hot water bath (60 °C) again to certain length and put back into extra SBF solution. After being coated with the second cycle (0.5-1.0 h), PLLA yarns were taken out of SBF solution. The coated PLLA yarns were washed with de-ionized water for several times and air dried over night.

Results & Discussion

[0058] FIG. 14 demonstrates alkaline-treated drawn yarn with biomimetic coating. In FIG. 14a, the drawn yarn was treated in 0.5 mol/L of sodium hydroxide for 60 minutes at 70°C and was then treated with the biomimetic method. A homogenous calcium phosphate coating layer is formed on the surface of the alkaline-treated PLLA yarns using the biomimetic coating process. In comparison, in FIG. 14b, the drawn yarn was treated in 1.0 mol/L of sodium hydroxide for 30 minutes at 25°C before subjecting the yarn to the biomimetic solution. Unlike FIG. 14a, the calcium phosphate coating layer is not homogeneously coated on the drawn yarn. Therefore, the longer soaking time, NaOH concentration, and/or the elevated temperature facilitate the preparation of the drawn yarn for the biomimetic coating.

[0059] FIG. 15 depicts a comparison of the alkaline-treated undrawn PLLA yarns with drawing and without drawing. In FIG. 15a, the alkaline-treated PLLA yarns were not subject to drawing. As shown, calcium phosphate particles were coated on the PLLA yarns. In comparison, in FIG. 15b, the alkaline-treated PLLA yarns were drawn from 2cm to 4 cm. It is noted that the calcium phosphate particles on the PLLA yarns are aligned and distributed on the drawn yarn. There are numerous benefits on coating the undrawn yarns with calcium phosphate. For example, the surface of the undrawn PLLA yarns can be modified more easily than the fully drawn yarns; thicker and denser calcium phosphate can be formed on these undrawn yarns; increased axial alignment of calcium phosphate coating can be achieved; these coated undrawn yarns can be coated again upon drawing to obtain thicker and denser calcium phosphate coating; and other agents for degradation or enhanced bone growth can be coated upon drawing.

Nucleation Model for CaP Deposition

[0060] The simplest picture of deposition of CaP on the yarn is one involving the random nucleation of crystals at equivalent sites that cover the yarn surface. Once the crystal is started, it grows in proportion to the time it is exposed to the solutions.

[0061] Definition of variables:

- 50 n = number of cycles
- N_A = density of growing sites
- N_{A0} = total density of sites
- p_D = probability of damage per cycle.
- p_N = probability that a site nucleates a crystal during each cycle
- 55 t_s = soak time per cycle
- w = mass of CaP deposited per active site, per cycle
- W = total deposited mass of CaP

[0062] The chance that one of the N_{A0} possible sites will become active during one cycle is p_N . Thus, the rate of change of the number of active sites N_A is given by the probabilistic expression:

$$5 \quad \frac{dN_A}{dn} = p_N(N_{A0} - N_A) \quad (4)$$

[0063] Integration of this expression gives:

$$10 \quad N_A = N_{A0}(1 - e^{-p_N n}) \quad (5)$$

[0064] It is assumed that the deposition rate of CaP is proportional to the number of active sites and the mass per cycle, w , deposited at each active site. The rate for the latter turns out to be a diminishing function of soaking time (see section 3.2) that needs to be determined empirically. It is assumed that $w = \alpha t_s^\beta$, where $\beta < 1$. Reducing the total deposition rate is the chance p_d that the deposit at an active site will be damaged during the rinsing steps that are part of each cycle. For simplicity, it is assumed that it will be removed completely, but the site remains active. Thus, during each cycle, the mass removed will be:

$$20 \quad N_A p_D W / N_A = p_D W \quad (6)$$

where W is the total mass deposited after n cycles. This expression is equivalent to assuming that the mass of the deposit that breaks will be equal to that of the average deposit. The net rate of CaP deposition will then be:

$$25 \quad \frac{dW}{dn} = wN_A - p_D W = \alpha t_s^\beta N_{A0}(1 - e^{-p_N n}) - p_D W \quad (7)$$

[0065] The analytical integration of this expression is not readily apparent; thus, it was analyzed in its differential form. After gaining the values of the four parameters αN_{A0} , β , p_N and p_D , the equation was integrated numerically with the first observation as the initial value. The results are shown in FIG. 2 as the curves labeled "nucleation model."

[0066] As with all analyses of this sort, exclusivity is not proven by a good result. For example, a model involving impinging deposits leading to retarded growth might work as well.

35 Conclusions

[0067] Monetite was successfully deposited onto the hydrolyzed polyester substrate using a cyclic soaking method from aqueous solutions of calcium nitrate and ammonium phosphate. The amount of CaP formed increased with increasing repetitions and soaking time at each repetition. A heterogeneous nucleation and growth mechanism was proposed to explain the observed phenomena of CaP deposition on the polyester surface. The composites prepared using this technique demonstrated flexural modulus in the range 2.4-7.9 GPa, which are at the lower end of the 3-30 GPa range of the bending modulus of human physiologic bone. Furthermore, it should be possible to fabricate various geometries of porous and bulk scaffolds with CaP using this cyclic soaking route depending on the mold and operating conditions.

[0068] Biomimetic coating technique was used on both drawn and undrawn yarns to generate homogeneous calcium phosphate coating. The present invention also demonstrates that the use of a sodium hydroxide under a certain concentration and temperature facilitates the uniform coating of calcium phosphate. Furthermore, the orientation of the coated calcium phosphate particles on the undrawn yarn can change upon drawing.

[0069] The yarns were washed with de-ionized water after each coating cycle. Finally, the CaP-coated yarns were coated with poly(ϵ -caprolactone) solution in tetrahydrofuran (THF), dried, and compression molded at an elevated temperature to form rectangular bars.

55 FABRICATION OF NOVEL COMPOSITES FOR BONE AND DELIVERY OF GROWTH FACTORS

Introduction

[0070] A new bone-repair synthetic composite material, which provides a sustained steady localized controlled release

of more than one growth factor and also has sufficient mechanical strength during the bone healing process, is needed. The new material can be described as an calcium phosphate/polymer composite consisting of hydroxyapatite, various thermoplastic binding resins, and a combination of biodegradable polymer fibers, which can be used as separate compartments for delivering different growth factors or delivering the same growth factor with different release rates. The invention provides an effective path for medical-device manufacturers to follow for designing highly functional devices for specific applications, such as long-bone repair, spinal fusion, sternal bone closure, and maxillofacial fixation. Aside from the pursuit of the stated goals, the understanding of polymer-based composite systems will be advanced, as the braiding process provides the opportunity to control precisely the deviation of the composite structure from uniaxiality and thus the deviation of mechanical properties from those of the ideal uniaxial structure.

10 Drug Delivery Synthetic Materials

[0071] A number of materials have been used as growth factor carriers, including, but not limited to, hydroxyapatite (calcium phosphate), synthetic polymers, demineralized bone, and collagen-based materials.

[0072] Most of the polymers used for carriers are biodegradable, and they can be divided into natural polymers and synthetic polymers. Natural polymers include collagen, hyaluronans, fibrin, chitosan, alginate and other animal- or plant-derived polymers. Notably, collagen sponge has become the most commonly specified natural polymer for use as a delivery carrier.

[0073] Human bone healing is a relatively slow process, requiring 2-3 months, depending on the patient health conditions and the repair site. Thus, a carrier material with sustained, steady, localized controlled release is required for the human bone healing process. Synthetic polymers, such as poly(L-lactic) acid (PLLA), polyglycolic acid (PGA), poly (D,L-lactide-co-glycolide) (PLGA), polydioxanone (PDO) and poly(ϵ -caprolactone) (PCL), are examples for localized release of growth factors, such as BMP and TGF- β .

[0074] As a biodegradable polymer, semi-crystalline PLLA fiber has been used in sutures, while amorphous PLA copolymers have been used in bone grafts and as drug carriers. One complication in the use of synthetic absorbable polymers like PLA is their degradation by hydrolysis to acidic products, which can accelerate the degradation rate of the polymer and induce local inflammation at the implantation site. However, if it is implanted together with calcium phosphate, the degradation of calcium phosphate forms alkaline products that neutralize the acidic degradation products (lactic acid) of the polymer. Moreover, the degradation rate of the polymer can be tailored to achieve the optimum BMP release rate by altering the polymer molecular weight and/or polymer composition. For example, the degradation rate of 50:50 glycolide-lactide copolymer (PLGA) can be higher than that of PLA. PCL is one semi-crystalline synthetic absorbable polymer that can be processed at low temperatures because of its low cost, extended resorption time and availability at low molecular weight.

[0075] Proteins are normally incorporated into polymers at room temperature. BMPs are highly sensitive to thermal processing and some types of chemical exposure, so the major challenge in developing the BMP carrier material is to incorporate sufficient BMP into the structure of the material without compromising the biological activity of the proteins. Unlike most of the ceramics and metals, amorphous polymer materials can often be processed at low temperatures, which make it easy to incorporate proteins into the polymer structure without harming the protein. The release of the protein from the amorphous polymer matrix involves both diffusion of the protein through the matrix and degradation of the matrix polymer. If the protein is incorporated into the structure of the polymer, the protein release rate is largely dependent on the degradation rate of the polymeric matrix, as the diffusivity of one polymer in another is very low. It has been demonstrated that with increasing degradation rate of a lactic acid/lysine copolymer matrix, the release rate of the protein increases.

45 In Vitro and In Vivo Tests

[0076] *In vitro* studies indicate that growth factors induce cell proliferation, cell differentiation, alkaline phosphatase (ALP) activity, and extracellular matrix formation. It was also evident that long-term continuous release of growth factors is crucial for bone formation *in vitro*. Recombinant technology has led to the expressing of human BMPs in quantities suitable for therapeutic applications in pre-clinical animal studies, including mice, rats, rabbits, dogs, sheep, and non-human primates. Bone formation rate can be accelerated due to the presence of BMP. However, faster and more bone healing was observed for the carrier material which provided sustained delivery of the growth factors.

55 Methodology

Fabrication of Novel Calcium Phosphate/Polymer Composites

[0077] A novel composite is fabricated for bone-repair applications using innovative processing techniques. Two ap-

proaches are employed to fabricate bar- and sheet-shaped composites, respectively.

[0078] The novel process of fabricating the composites is shown schematically in FIG. 16. Different biodegradable polymer fibers 102 (FIG. 16a) are employed to prepare the composites. The polymer fibers 102 are braided into braids 108 (FIG. 16d). These braids can either be coated with hydroxyapatite or non-coated. Some of the polymer fibers 102 are coated with hydroxyapatite using a biomimetic method and then with a thin layer of a low melting polymer to form coated fibers 104 (FIG. 16b, 16c) which is used to form the center core of the braid 118, as shown in FIGS. 17(a), (b), and (c), with uncoated polymer fibers 102 braided in a sheath over it (FIG. 17). Some of the secondary unidirectional structures can then be compression molded (FIG. 16e) to give a rod/bar-shaped composite (FIG. 16f) or used to form a mesh (FIG. 16g, 16h). Furthermore, the uncoated yarn 12 or the coated yarn 104 can also be used to make a mesh without the coating of the low-temperature polymer. The thus-fabricated composites are suitable for varied applications, such as long-bone repair, spinal fusion, sternal bone closure, and maxillofacial fixation. Examples of low melting temperature polymers includes polymers with a melting point below 175 °C, semi-crystalline polymers, PCL, polydioxanone, copolymers of PCL with PGA, PDO, TMC or PLA (L or D,L), non-crystalline polymers, PLA-PGA (50:50), poly-D,L-lactic acid, or any polymers having a lower melting temperature than the core structure. The details of the each processing step are described as follows:

Examples

Composite Components

[0079] Two synthetic biodegradable polymer fibers (poly(L-lactic acid) (PLLA) and polyglycolic acid (PGA)), one natural polymer (catgut), one polymer coating (the mixture of poly(ϵ -caprolactone) (PCL) and glycetyl monostearate), and one calcium phosphate coating (mainly hydroxyapatite (calcium phosphate)) are used in construction of the composites. The melting temperature, mechanical properties, and degradation rate of these materials are listed in the following table.

Table 3.

Properties	PGA	PLLA	Catgut	PCL	Cap
Melting temperature, °C	225	175	~200	60	>1600
Young's Modulus (Gpa)	7.0	6.0-7.0	0.1	0.4	100
Tensile strength (MPa)	730	500-550	50-100	240	40-300
50% tensile strength loss	14 days	18 months	7 days	12 months	>2 years

Nano-CaP Powder Coating

[0080] 20-30 of the PLLA fibers ($T_m=175^\circ\text{C}$) are formed into yarns. PCL ($T_m=60^\circ\text{C}$) was dissolved in toluene, which is a non-solvent for PLLA. Nano-CaP powders were added to the PCL solution to form a homogenous suspension. The PLLA yarns were then dip coated with the mixture of calcium phosphate and PCL, stacked in a mold, and subjected to compression molding at 60°C. The calcium phosphate load was 25 wt%, and the PLLA to PCL ratio was 6:1. During the compression molding, the PCL melted and acted as a "glue" to bind all the PLLA yarns together. The specimens were then subjected to a three-point bending test, where pure PCL was used as a control.

[0081] Figure 18 shows the flexural strength and Young's modulus of pure PCL, PCL-coated PLLA, and both PCL- and CaP-coated PLLA. The PCL-coated PLLA has much higher strength and Young's modulus than those of pure PCL. With the addition of calcium phosphate in the system, the composite became much stiffer and stronger. Its Young's modulus was at the lower end of that of cortical bone, 3-30 GPa. However, the composite is still too weak to be used at load-bearing applications.

Biomimetic Coating

[0082] To mimic the calcium phosphate formation in the biological environment, a biomimetic approach is employed to apply bone-like carbonated calcium phosphate onto the surface of the polymer yarns. The biomimetic coating method produces a calcium phosphate layer on the surface of various biomaterials in simulated body fluid (SBF), which has identical ion concentrations to human blood plasma at body pH (7.4) and temperature (36.5°C).

[0083] Being disclosed but not part of the invention, a biomimetic method is used to homogenously precipitate nano-calcium phosphate on the surface-modified polymer yarns to achieve a strong calcium phosphate coating. Further, the novel processing technique is employed to co-braid the PCL yarns with PLLA, PGA or PDO yarns. This unique design

has the following advantages: (1) instead of using yarns, the braids are bound together using PCL to minimize the PCL to PLLA ratio; (2) it allows to precisely control the amount and the distribution of PLC in the PLLA (or PGA, PDO) fibers; (3) the PCL automatically distributes in a uniform fashion between the fibers when it melts.

[0084] The bonding strength between the calcium phosphate coating and a polymer can be improved substantially by pretreatment of the polymer surface with either an alkaline or an acid solution to form polar groups that are confined substantially to the surface of the polymer. It has also been found that calcium phosphate precipitates may align along the fiber axis when carboxylate groups are present on the surface of the uniaxially stretched polymer fibers. As the synthetic polymer yarns used in this study have been prepared through extensive uniaxial stretching during the spinning process, they can be treated with acid or base to render carboxyl or carboxylate binding sites that induces the nucleation of calcium phosphate nano-particles with a preferential orientation. Thus, the yarns are dipped quickly into an acid, a base or a sequential combination of both solutions to attain the necessary surface treatment without modifying the polymer unfavorably. The pretreated yarns are soaked in the SBF solution for various periods, to attain composites with varying calcium phosphate loadings, including no exposure to SBF (zero loading). Such-obtained calcium phosphate precipitations orientate along the polymer fiber axis, which mimics the structure of the aligned calcium phosphate nano-particles on collagen fibrils in natural bone.

[0085] The surface properties of the composite before and after soaking in the SBF are thoroughly characterized by a series of techniques, including thin-film-XRD to examine the surface phase distribution, and Fourier transform infrared (FTIR) to determine the surface functional groups. Surface morphology changes are monitored by scanning electron microscope. The calcium and phosphate ion concentrations in SBF, before and after soaking, are measured by inductively coupled plasma atomic emission spectroscopy (ICP-AES).

Example 1

[0086] Drawn PLA fiber yarn (30 filament, 120 denier) was wound around open plastic frames ($2^{1/4} \times 1^{1/8}$ in.). The amount of fiber on each frame varied since the process was done by hand. The fiber and frame were then weighed. The samples were then soaked in simulated body fluid solution (3x concentration) for 12 h to generate a layer of hydroxyapatite (HA) coating on the surface of the PLA fibers. The samples were left to dry overnight. After drying the weight was recorded and was used to calculate the percentage of HA by weight of each sample. The samples were then hot compacted into bars with dimensions around ($4 \times 0.5 \times 0.2$) cm at a temperature of 175°C for 30 min. Afterwards, each sample was subjected to a three-point bend test to determine flexural modulus and flexural strength. This was done at a strain rate of 1 mm/min. It is noted that etching is not used in this example. Nonetheless, etching can be used prior to biomimetic coating. Also, a low temperature binding sheath was not used in this example. Instead, the hot compaction was carried out near the melting point of the PLA, at 175°C , thus melting the outer PLA fiber yarns to bind the group of PLA fiber yarns. Calculations were made using the following equations:

$$E_f = \frac{L^3 m}{4bd^3} \quad (8)$$

$$\varepsilon_f = \frac{6Dd}{L^2} \quad (9)$$

$$\sigma_f = \frac{3PL}{2bd^2} \quad (10)$$

[0087] Definition of variables:

P: applied load, N

L: support span, m

b: width of the sample, m

d: thickness of the sample, m

m: slope of the tangent to the initial straight line portion of the load/deflection curve, N/m.

Table 4. Flexural Modulus, Strength, and Strain Of Some Self Reinforced PLA/HA Composites.

Wt% HA	wt% PLA	E _f (GPa)	σ _f ^{max} (MPa)	ε _f ^{max} %
9	91	2.2	145.9	13
31	69	3.0	29.9	7.6
43	57	3.4	44.0	12.1

[0088] The data obtained from samples containing 9, 31, and 43 wt% HA is shown in Table 4. The data suggest that the flexural modulus increases with HA concentration in spite of the concomitant decrease in PLA content. The data did not show any correlation between HA wt% and flexural strength of the composite. However, the data shows that the flexural strength increases greatly from 44 MPa to 146 MPa when the wt% of PLA fibers was increased. The strain data shows no significant difference between 9 and 43 wt% HA samples but at 31 wt% the maximum strain percent was quite low in comparison to the other samples. Data such as this suggests that a balance should be found between HA and PLA wt% in order to maximize flexural modulus and strength.

Example 2 (not part of the invention)

Direct Coating of Calcium Phosphate Precursors

[0089] Pre-formed or calcium phosphate precursors can be directly coated onto PLA fibers. A hydrothermal method is used to make the HA, then the particles are used with PCL to coat over the fibers. In addition, other calcium phosphates can be used.

[0090] The HA particles used in the composite were prepared by reacting of 200 mL calcium nitrate solution (2 g/dL) and 600 mL ammonium phosphate solution (2 g/dL). After drying, the precipitate was ground into powder, which has an average particle size of 120 nm and is shown in Figure 19. Ten mg of ground HA powder was then added into 10 mL PCL (Dow, MW 80,000) acetone solution (1% wt/wt), which was used to dip-coat the PLA fiber strand composed of 30 fibers with a 22-μm diameter for each fiber. Sixty meters of PCL-HA coated PLA fibers were then aligned and hot-pressed in a 40-mm × 5-mm × 2-mm mold at 80°C for 4 min. The resulting composite was taken out after cooling and its composition was PLA : PCL : HA = 83 : 15 : 2 wt% as determined by TGA. It is noted that etching is not used in this example. Nonetheless, etching is an optional process and can be used prior to biomimetic coating.

[0091] The stress-strain curve of the composite under small strain (<1%) is shown in Figure 20. The Young's modulus is 6.5 GPa for linear region (0~0.001%).

[0092] A pultrusion process was also used to prepare the PLA-PCL-HA composite. PLA fibers were pulled through a tapered die filled with molten PCL-HA mixture, which has an HA : PCL volume ratio ranges from 0.1 ~ 0.2. The apparatus used for the pultrusion is shown in Figure 21. The tensile test results were listed in Table 5.

Table 5. Tensile test results of pultruded composite

PLA	PCL	HA	Young's modulus (GPa)
0.09	0.82	0.09	1.1
0.18	0.74	0.08	1.9
0.09	0.76	0.15	1.2
0.20	0.66	0.14	2.2

[0093] Hydroxyapatite particles can also be aligned along the PLLA melt spun yarn by electrospinning HA particles in a solution of PLLA in dimethylformamide over melt spun PLLA yarn as shown in Figure 22. The process is carried out by first winding PLLA yarn onto a grounded rotating wheel or drum and then electrospinning filaments containing HA particles over the PLLA yarn. HA particles with aspect ratios greater than about 4:1 tend to align themselves within the PLLA electrospun filaments. When the HA containing filaments are wound over the melt spun PLLA yarn, the amount of alignment of the HA particles with the PLLA yarn will be proportional to the alignment of the electrospun yarn with the melt spun yarn. Samples prepared by this method can then be coated and hot pressed.

Example 3

[0094] PLLA ($M_n = 1.21 \times 10^5$, MWD=1.29) yarns (30 denier, $25 \pm 2 \mu\text{m}$) for samples I were pre-etched in 0.50 mol/L NaOH solution for 30 min at room temperature. After being rinsed with de-ionized water and air dried for 24 h, yarns I, II and III were coated with hydroxyapatite (HA) by a biomimetic method at 42 °C for 24, 12, and 24 h, respectively. As shown in Table 6, with NaOH etching pretreatment, sample I gained higher HA/PLLA weight ratio than both II and III. This suggested that thicker HA coating was obtain on the etched fiber (Sample I) because the initial specific surface of the yarns in all the three samples were the same. Also, sample III exhibited higher HA/PLLA weight ratio than that of sample II, indicating that a longer coating time gives a thicker coating.

Table 6. Comparison of composition and three point bending results of sample I, II and III

3PB Beam	PLLA wt%	HA wt%	PCLGA wt%	Max flexural stress/ MPa	Flexural Modulus/ GPa
I	74.04	9.92	16.04	132	5.4
II	77.66	6.743	15.60	87	4.2
III	70.13	6.86	23.02	45	3.8

[0095] The HA-coated PLLA yarns were vacuum dried overnight before being dipped into poly(ϵ -caprolactone-co-glycolic acid) (PCL:PGA=90:10) acetone solution for 5-10 min, whose concentration was 10% w/v. PLLA/HA/PCLGA composites were dried under vacuum for 24 h, after which the composites were hot pressed using a flat die to form beams for three point bending tests.

[0096] The flexural stress and modulus of the PLLA/HA/PCLGA composite beams with a dimension of 30.0mm×5.3mm×2.0mm are tested with a three-point bending test. At a strain rate of 5mm/min, the flexural stress of sample I was found to be 132.2 MPa and its modulus is 5.4 GPa. Comparing these values with those of sample II, it could be found that, with similar weight percentage of PCLGA coating, sample I with higher amount of HA demonstrated better mechanical properties (higher flexural stress and modulus). When comparing flexural stress and modulus of samples II and III, it was found that sample II with lower amount of PCLGA demonstrated better mechanical properties, which could be attributed to much lower flexural strength and modulus of the amorphous PCLGA coating layer.

Braids

[0097] As used herein, a "braid" shall include any structure using a combination of elements that are arranged with an inner element and an outer element. A typical structure of a braid consists of the center part, the core 118, and the outside part, the sheath 120. This configuration and the technology for its manufacture are adapted to create a novel composite for delivering growth factors during bone repair. The advantage of braiding is that it allows precise placement of different fibers within the composite and variation of the fiber ratios over a large range.

[0098] In the present invention, the fibers at the core 118 are coated with calcium phosphate before braiding. In contrast, the sheath 120 is subjected to substantial twisting, bending and sliding during the braiding, so it is not coated with calcium phosphate. The core is assembled with the sheath of yarn braided over its surface to form a tubular braid (see FIG. 17(a), (b), (c)), which is used as a building block for constructing different implants or devices.

[0099] In accordance with an embodiment of the present invention, the polymer yarns with or without calcium phosphate coating form a primary unit of the braided structure, as show in FIGS. 17(a), (b), (c). The primary units form the core 118 and the sheath 120 of the braids, which are the secondary units of the structure. The calcium phosphate-coated yarns form the core 118, while the uncoated ones form the sheath 120. The sheath 120 may be subjected to substantial torsion and bending during the braiding, so it is not coat with calcium phosphate. Finally, the core secondary units are assembled with the sheath secondary unit braided over its surfaces, which is the tertiary unit of the structure. The tertiary unit is used as a building block for constructing different implants or devices. The composition of the primary unit is adjusted to achieve the mechanical and chemical properties meeting the requirements for different load bearing skeletal implants.

Fabrication A: Bar-Shaped Composite

[0100] FIG. 23 is a flowchart outlining an exemplary operation according to the present disclosure for the construction of the novel composite. In operation, the process starts at step 202, where the primary units, PLLA, PGA, PCL, and PDO yarns 102 are gathered. Next, in step 204, the primary units are coated with hydroxyapatite (CaP) to form coated fibers 104, and in turn form the core secondary units 118. In conjunction with step 204, in step 206, the primary units can form a sheath 120. The sheath 120 is not coated with hydroxyapatite (CaP).

[0101] Then, in step 208, an appropriate ratio of core secondary structure and the sheath secondary structure (from steps 204 and 206) are braided together to form a tertiary unit. Next, in step 210, the tertiary unit is dip-coated with PLC mixture and compression molded in elevated temperature. In step 212, the tertiary unit is subjected to mechanical testing.

5 **Construction of the Primary Unit**

[0102] *Fibers:* Four synthetic biodegradable polymer fibers, poly(L-lactic acid) (PLLA), polyglycolic acid (PGA), poly(ϵ -caprolactone) (PCL) and polydioxanone (PDO), are used as in construction of the composites. The melting temperature, mechanical properties, degradation rate and accessibility to solvents of these fibers are listed in Table 7. The combination 10 of these polymers covers a wide range of chemical, physical and morphological variables.

Table 7. The melting temperature, degradation rate, and accessibility to solvents of PGA, PDO, PLLA, PCL, and collagen fibers.

		PGA	PDO	PLLA	PCL
15	Melting temperature, °C	225	109	175	60
	Young's Modulus (GPa)	7.0	1.5	6.0-7.0	0.4
20	Tensile strength (MPa)	730	600	500-550	240
	50% tensile strength loss	14 days	1 month	18 months	-
	100% mass loss	6-12 months	6-12 months	> 36 months	>24 months
25	Solvents	Toluene	Non-solvent	Non-solvent	Solvent
		Xylene	Non-solvent	Non-solvent	Solvent
		Ethyl acetate	Non-solvent	Non-solvent	Solvent
		Acetone	Non-solvent	Non-solvent	Solvent

30 [0103] FIGS. 17(a), (b), and (c) depict the composite construction of a novel composite. As shown, a combination of catgut, PGA, and PLLA fibers 102/104 form the core of the braid 118, and the PLLA fibers form the sheath 120 of the suture braid 130. The large cylinders represent polymer braids 130 and small cylinders represent polymer yarns 102. FIG. 17a is a composite construction which does not form part of the present invention composed of: a combination of PCL-coated PLLA 104, catgut 102b, and PGA 102c fibers form the core 118, PLLA 102 forms the sheath 120, and the braid 130 is then coated with PCL mixture 134. FIG. 17b illustrates that a porous structure at the core 118 is formed due to the early degradation of the catgut 102b. FIG. 17c further illustrates that with increasing the implantation time, PGA (102c) at the core degrades and creates more channels (white) in the structure.

35 [0104] The fibers 102 are pre-coated with calcium phosphate as described above. In some embodiments which do not fall within the scope of the present invention, the fibers at the core are coated with a mixture of PCL and glyceryl monostearate ($T_m \sim 50-70^\circ\text{C}$). It is found that adding glyceryl monostearate in PCL increased the porosity of the composite, which could be used to controlled release of proteins. This is the first time the use of PCL and glyceryl monostearate mixture as a coating on polymer fibers for this purpose. In the rest of the constructions, the core is polymer-coating free. The PCL mixture is dissolved in an organic solvent, such as toluene, xylene, or ethyl acetate, which does not attack PLLA, PGA, or catgut fibers. The thickness of the coating is controlled by adjusting the concentration of the dipping 40 solution, the coating speed, and the number of passes through the coating bath. The amount of the glyceryl monostearate in PCL is adjusted depending on the drug release rate requested.

45 [0105] In the fabrication of the composite, the ratio of core to sheath is maximized to improve the mechanical strength of the construction. The fibers at the core are aligned along the fiber axis providing a high Young's modulus contribution, while those in the sheath lie at an angle to the axis leading to reduction in contribution to the mechanical stiffness and strength of the composite. However, the preponderance of the fibers are in the core; thus, the braid still yields the composites with high mechanical strength. Upon the construction of the polymer braids, they are then coated with a layer of the mixture of PCL and glyceryl monostearate. The glyceryl monostearate acts as a crystallization modifier for the PCL. Other details of the dip-coating process are described above.

50 [0106] The polymer braids can be cut into the length of the compression mold, stacked up, and subjected to compression molding between 50-70°C. During the compression molding, the high melting temperature polymer yarns, such as PLLA ($T_m = 175^\circ\text{C}$), PGA ($T_m = 225^\circ\text{C}$), and catgut ($T_m > 200^\circ\text{C}$), remain intact, while the low melting temperature PCL and glyceryl monostearate mixture coating ($T_m = 50-70^\circ\text{C}$), melt and act as a "glue" to bind the yarns and the braids together (FIG. 24a). When the composite is implanted *in vivo*, the slow-degrading polymer fibers, such as PLLA and PGA, hold

the structure of the composite, and provide the necessary mechanical strength during the bone healing. Meanwhile, the fast-degrading fibers, such as catgut, will degrade first and create a porous structure between the polymer yarns at the core (FIG. 24b). It will also release growth factors and induce bone ingrowth into the pores of the structure. Increasing implantation time, PGA will start to degrade, and create a more porous structure at the core and thereby inducing more bone ingrowth (FIG. 24c).

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Construction of the Secondary and Tertiary Units

[0107] 20-30 primary units are formed into a secondary unit. The core secondary unit 118 is coated with calcium phosphate, while the sheath 120 is calcium phosphate-free. In the construction of a tertiary unit, the ratio of core to sheath is maximized to improve the mechanical strength of the construction. The fibers at the core are aligned along the fiber axis providing a high Young's modulus contribution, while those in the sheath lie at an angle to the axis leading to reduction in contribution to the mechanical strength of the composite. The calcium phosphate-coated yarns at the core mimics the highly organized structure of osteon in natural bone, where collagen fibrils are aligned with nano-calcium phosphate platelets orientated along the fibril axis. Thus, the composite yields the polymer braids with a maximum mechanical strength.

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[0108] In an embodiment, both the core 118 and the sheath 120 of the braid 130 are fabricated using a combination of the four polymer yarns available, PLLA, PCL, PDO and PGA. This yields composites with different microstructures, mechanical properties and drug release rates for load-bearing skeletal implants. Two composite fabrication techniques are employed to prepare the composites: hot compression molding and cold compression molding. In all of the experiments, a slot mold with positive displacement is used to make uniaxial composite samples. In an alternative embodiment, flow of the matrix material along the aligned fibers is allowed, leading to higher orientation of both the matrix and the fibers.

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Hot Compression Molding

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[0109] The polymer braids with various combinations at both the core and the sheath are cut into the length of the compression mold, stacked up, and subjected to hot compression molding. A compression molding temperature of 60-70°C can be used. During the compression molding, the high melting temperature polymer yarns, such as PLLA ($T_m = 175^\circ\text{C}$), PGA ($T_m = 225^\circ\text{C}$), and PDO ($T_m = 109^\circ\text{C}$), remain intact, while the low melting temperature PCL ($T_m = 60^\circ\text{C}$) yarns melt and act as a "glue" to bind the braids together. An example of variety of constructions are built as listed below, these examples are illustrative and not meant to be limiting.

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[0110] FIGS. 24 (a-d) depict various composite constructions after compressive molding (large cylinders represent polymer braids and small cylinders represent polymer yarns): (a) PLLA 102a as the core 118 and PCL 140 as the sheath 120, (b) a combination of PLLA 102a and PGA 102c or PDO 102d as the core 118 and PCL 140 as the sheath 120, (c) 35 PLLA 102a as the core 118 and PGA 102c or PDO 102d as the sheath 120, and (d) PLLA 102a as the core 118 and the combination of PGA 102c and PDO 102d as the sheath 120. (c) and (d) do not fall within the scope of the present invention.

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Construction One

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[0111] In an embodiment of the invention, the calcium phosphate-coated PLLA yarns 102a can be the core 118 of the braid 130, while the PCL yarns 140 can be the sheath 120. This design is the most basic construction among all the proposed structures. During the hot compression molding, the PCL at the sheath melts, penetrate into the calcium phosphate coating, and act as a "glue" to provide strong bonding of the calcium phosphate-coated PLLA braids. In contrast, the PLLA braids retain their structural integrity, become aligned, and bind together through the PCL melt (FIG 45 24a).

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Construction Two

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[0112] In another embodiment of the invention, a combination of calcium phosphate-coated PLLA 102a and PGA 102c (or PDO 102d) yarns can be used as the core 118, while the PCL 140 yarns can form the sheath 120, as shown in FIG. 24b. A similar aligned structure is formed after compression molding as described in Construction one. In comparison to Construction two, the PGA (or PDO) yarns at the core will degrade much faster than PLLA when the composite is implanted *in vivo*, thereby resulting in many hollow column channels in the structure. These columns will facilitate the early stage bone ingrowth, while the PLLA yarns will remain structurally sound and loose strength over the long-term.

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Construction Three

[0113] In another embodiment which does not fall within the scope of the present invention, the calcium phosphate-coated PLLA 102a yarns form the core 118 of the braid 130, while the uncoated PGA 102c can be the sheath 120, as shown in FIG. 24c. PCL dissolves in toluene, xylene, or ethyl acetate, which is a non-solvent for both PLLA and PGA. The braids are dip-coated with PCL, and dried in air. After compression molding, the PCL binds the polymer braids together. When this composite is implanted *in vivo* for a period, such as one month, a hollow shell around the PLLA core can be gradually formed due to the fast degradation of the PGA yarns, and the bone tissue can gradually grow into the shell during this period. The thickness of the shell can be controlled to achieve the optimum space to facilitate bone-ingrowth. In contrast, the PLLA core will remain aligned and supply the long-term mechanical strength for the implant. The whole implant will be finally replaced by the natural bone in approximately 2 years.

Construction Four

[0114] In another embodiment which does not fall within the scope of the present invention, the calcium phosphate-coated PLLA yarns 102a form the core 118 and a combination of PGA 102c and PDO 102d yarns form the sheath 120 of the construction, as shown in FIG. 24d. Like Construction three, the braids are dip-coated with PCL. After compression molding, the PCL binds all the braids together, while PGA and PDO remain holding the PLLA yarns at the core. After implanting *in vivo* for about two weeks, PGA will degrade, which will create a porous sheath to facilitate bone ingrowth. In the meantime, the PDO sheath will remain in place for an extra of two weeks, which will allow more time for bone tissue ingrowth.

Cold Compression Molding

[0115] Even temperatures as low as 60°C might affect the crystalline structure of the PLLA, PGA or PDO fibers. Thus, it is desirable to work at even lower temperatures, such as room temperature. As indicated in Table 3, toluene, xylene, and ethyl acetate are good solvents for PCL but they do not attack PLLA and presumably do not alter its crystalline morphology. A similar construction to Construction One can be employed where PLLA yarns can be the core, and PCL yarns can be the sheath of the braid. The polymer braids can be cut to the length of the mold and stacked in the mold. One of the three solvents listed above can be added in vapor form to the polymer stack so as to soften the PCL yarns. The softened PCL sheath can bind all the polymer braids together during cold compression molding at temperatures much lower than 60°C. The cold compression molding can also be employed to form the structure in the rest of the constructions as the three solvents listed above are also non-solvent for PGA and PDO.

Fabrication B: Sheet-Shaped Composite

[0116] In another embodiment, the PLLA fibers can also be woven or knitted into a piece of cloth, and then coated with calcium phosphate. The growth factors can be incorporated into the lattice structure of the calcium phosphate coating or directly deposit on the surface of the coating. The growth factor-loaded fabric can be inserted at the interface of the sternal bones to improve their closure after the cardiovascular surgery. The sternal bone of the patient is cut into half during the cardiovascular surgery, and stainless steel wires are normally used to hold the sternum together during the bone healing process. Unfortunately, the patient suffers a lot of pain due to the use of the stainless steel wire. Plus, the stainless steel wire may cause inflammation at the surgery site. Consequently, the healing process is long and painful for the patient. If high strength polyethylene suture is used in combination with the present invention, not only the pain of the patient will be reduced due to the use of the high strength polyethylene suture, but also the bone healing rate will be accelerated significantly due to composite insertion.

[0117] The crystallinity of the PLLA and PGA phases in the resulting composite can be investigated by XRD and differential scanning calorimetry (DSC). As appropriate, transmission electron microscope (TEM) and small-angle x-ray scattering (SAXS) analyses can be added to characterize the calcium phosphate alignment and distribution in the polymer and crystalline morphology of the polymer. The surface morphology of the composite can be assessed using environmental scanning electron microscopy (ESEM).

Mechanical Testing

[0118] The synergistic effect of using bone-like calcium phosphate precipitated on the surface of highly aligned polymer fibers, appropriate calcium phosphate loadings, and optimum processing conditions should improve the mechanical properties of the composite dramatically. The tensile and flexural tests can be conducted on the composites according to ASTM D638 and D790-02, respectively, and the Young's modulus and Poisson's ratio can be determined. Before

mechanical testing, the samples can be cut into standard geometries for each test. The data can be compared with the mechanical properties of the cortical bone (tensile strength: 60-160 MPa; Young's modulus: 3-30 GPa; shear modulus: 3.5 GPa; Poisson's ratio: 0.25) as well as with other composites designed for orthopedic applications.

5 **In Vitro Test**

[0119] To understand the effect of different polymer constructions on bone formation rate on the composites, an *in vitro* cell culture study can be carried out. The composites of each construction with the optimum processing conditions can be subjected to cell culture study. Alkaline phosphatase (ALP), mineral deposition, and bone nodule formation are 10 three important markers at different stages of bone formation *in vitro*. In the present invention, ALP, calcium deposition, and bone nodule formation assays are performed to reveal the optimum combination of polymers for bone formation.

Cell Attachment, Proliferation, ALP, Calcium Deposition, and Bone Nodule Formation

[0120] A rat osteosarcoma cell line can be used in the proposed study, as the cells are calcified easily *in vitro*. The 15 interactions between osteoblasts and different composites can be investigated. Cell attachment, proliferation and ALP activities can be performed on the surface of the composites. Tissue culture plastics can be used as controls, which have cells alone in the culture without any composite. The cell attachment can be carried out at different time points, such as 1, 3, 5 and 8 hours, using an alamarBlue fluorescent dye™ technique. An optimum time point for cell attachment 20 can be determined. Following cell attachment, osteoblasts undergo a high level of proliferation. The rate of proliferation can indicate the success of a substrate at promoting osteoblast growth. The same alamarBlue dye™ technique can be utilized in assessing the cell proliferation rate. Osteoblast proliferation can be determined on days 1,3, and 7. The cell morphology can be observed using scanning electron microscopy (SEM). After a slightly longer incubation period, such 25 as 17-21 days, calcium deposition proceeds. The calcium measurements can be undertaken using calcium crimson (a dye that stains calcium) and acridine orange staining followed by confocal microscopy observation. Bone nodule formation can be detected using von Kossa staining. Images can be taken using an optical microscope.

[0121] *Statistical Analysis:* A statistical analysis can also be conducted. Statistical significance can be determined 30 using a one-way of variance (ANOVA) to compare means between groups, with a P value of less than 0.05 being considered significant.

CONTROLLED RELEASE OF DRUGS

Introduction

[0122] Almost all the components, including the biomimetically formed calcium phosphate, the PLLA, PGA and catgut 35 fibers, and the PCL mixture coating in the proposed composite can be used as delivery carriers, which makes it possible to incorporate multi-growth factors into the structure. Controlled release can be achieved by varying the composite constructions, using different drug incorporation methods to add growth factors into different carrier components of the composite. In addition, due to the unique design of the composite structure, while the fast-degrading polymers break 40 down, the slow-degrading polymers can maintain the mechanical strength of the composite. Such a system can be ideal in conducting more sophisticated drug delivery.

[0123] In the present invention, two drug-delivery systems: single- and multi-drug are disclosed. Both *in vitro* and *in vivo* 45 studies are carried out to demonstrate a sustained and stable controlled release of drugs, as needed for optimum bone healing. In the *in vitro* model, a single drug delivery system is investigated to learn about the release properties of the composites and their components, with the aim of achieving an optimum drug release profile. In the *in vivo* study, both single- and multiple-drug delivery systems are studied.

In Vitro Study

[0124] Growth factor(s) are incorporated into different compartments of the composite to provide sequential release. 50 This unique characteristic of the system can be used to design a more sophisticated drug-release system. A systematic study is carried out to investigate the effect of the degradation rate, the drug incorporation method, and the crystallinity of the polymers on the drug release rate of the constructed composites.

55 **A Single-Component Carrier System**

[0125] BMP-2 may be released by one of the following three carriers: 1) polymer fibers, 2) PCL mixture coatings, and 3) calcium phosphate coatings. A total dose of 21 µg rhBMP-2 is placed on each implant based on previous experience.

For the polymer fibers (including PLLA, PGA, and catgut fibers), the BMP is directly deposited on the surface of these fibers and the release profile of the BMP is measured by BCA protein assay. To measure the BMP release, the polymer fibers are suspended in a N,N-bis(2-hydroxyethyl)-2-aminoethanesulfonic acid (BES) buffer for different time periods up to 8 weeks at 37°C. They are then removed from the solution, and the supernatant is evaluated by a BMP-2 enzyme-linked immunosorbent assay (ELISA).

[0126] In the case of PCL mixture coatings, the BMP is added to the coating solution and applied on the surface of BMP-free PLLA fibers. The glyceryl monostearate content in PCL varies between 0-10 wt% to alter the protein release rate in the coating. The release rate is increased with the content of glyceryl monostearate in the PCL as the porosity of the coating increases. For the calcium phosphate coating, BMP is incorporated into its lattice structure to create a sustained release profile. Briefly, BMP is added into the simulated body fluid solution, and co-precipitate with the calcium phosphate on the surface of the polymer. It is noted that only about 50% of the BMP had released after 5 weeks of implantation when BMP was incorporated into the lattice structure of calcium phosphate, but no release was observed at the first week of implantation. Finally, the BMP incorporated polymer braids are subjected to compression molding between 50-70°C, at which temperature most of the growth factors can survive.

A Multiple-Component Carrier System

[0127] A sustained steady controlled release profile may be designed using sequential release of the growth factor from different components of the composite. First, a low dose of BMP can be incorporated into a component with a fast releasing rate, such as catgut and PGA. Since a low dose is used, the "burst release" of the BMP won't create a local overdose effect. Second, the rest of the BMP can be incorporated into a component with a slow releasing rate, such as the calcium phosphate or the PCL mixture coating. It is hypothesized that a two-step sequential release can ensure a steady release started from day 0, and can last for up to 8 weeks. Such created release profile can be ideal for the human bone healing, which normally takes 2-3 months. It should be noted that drug release rate of the fast-degrading polymer may slow down due to the PCL mixture coating on its surface.

Measurement and Modeling of Release Kinetics

[0128] The proposed composites are at one time complex and simple. The geometry comprising yarns of different compositions and braids of different constructions embedded in a matrix with various filler loadings, is a complication. The macro sample size and the pseudo one-dimensional geometry are simplifying aspects of the problems of measuring and modeling degradation and drug-release kinetics. The high molecular weight of the growth factor is also a simplification in that it is hypothesized its solubility and diffusivity in the matrix will be vanishingly low. To study the release kinetics of the biodegrading composite, the following factors will be examined:

- 35 Influence of plasticization of the matrix on molecular diffusion;
- Influence of molecular weight during degradation on molecular diffusion;
- Combined degradation and molecular diffusion; and
- Diffusion from porous, degrading solids.

[0129] The release profiles, i.e., release rate vs. time, of the composites can vary significantly, but the studies cited here were essentially "take what you get" from the point of view of controlling the profile in a predictive fashion. In addition, the added complication of diffusion limitations brought about by growing bone tissue has not been addressed adequately.

[0130] With the composites proposed, growth factor release rate can be precisely controlled because of the flexibility in composition and structure. For simplicity of analysis, cylindrical composite rods can be subjected to one-dimensional degradation by capping the rod ends with epoxy. At the end of the degradation time, the rod can be sectioned and its morphology studied with spatially resolved surface techniques and the standard portfolio of morphological analyses using scanning electron microscope, optical microscope and atomic force microscope, as appropriate. In addition, bulk properties (molecular weight, drug concentration) can be studied by radial profiling followed by standard solution analyses.

[0131] Modeling of the degradation kinetics will follow the example of Lemaire *et al.*, but with changes to incorporate the unique geometries of the composites. Of somewhat incidental importance, but nevertheless interesting, is that release along the axis of the composites, i.e., from the ends, is a model situation for the analysis of Lemaire *et al.*

In Vivo Study:

[0132] The composite with the optimum release profile and reasonable mechanical strength will be used for the *in vivo* studies. Once it is certain that BMP is being stored and released from the three different compartments of the composite, as determined with *in vitro* tests, then single vs. multiple agent delivery can be compared *in vivo*. Applying

current understanding of normal wound repair, combinations of growth factors have great potential to enhance healing as bone formation and repair are regulated by many factors, including extracellular matrix and several growth factors. In natural, these growth factors participate in the bone repair at different sequences. A preliminary *in vivo* study will be carried out using a mouse model. Sixty mice each will receive four implants (two controls and two specimens) placed directly at both the calvarie and ectopic sites. It is important to have implants at both the calvarie and the ectopic sites, as the bone healing is much easier at the former site than the later. It is known that the bone-healing rate of mouse is much faster than that of human being, so it will be beneficial to have two implantation sites in the mouse model to test the bone forming induced by different drug delivery systems.

[0133] The composite without growth factors will be used as the control. 20 mice receive rhBMP-2 alone, 20 receive the combination of bothrhBMP-2 and TGF- β with rhBMP-2 releasing first, and the rest 20 also receive the combination of the two drugs but with TGF- β releasing first. A dose of 21 μ g of rhBMP-2 is placed on each implant, which receives rhBMP-2 alone, while 21 μ g of rhBMP-2 and 2 μ g TGF- β are placed on the implant for combined release based on previous research. The mice are sacrificed at 1, 2, 21, and 42 days after implant placement, and 5 mice at each time point are used in the study, for a total of 60 mice.

[0134] Samples containing the implants and surrounding tissues are harvested and fixed in 10% neutral-buffered formalin. Following fixation, the samples are analyzed by computer-aided microtomography (microCT) at a resolution of 12 μ m (μ CT40, Scanco Medical AG, Bassersorf, Switzerland) to assess the amount of new bone height, volume, bone mineral density and microarchitecture of new bone adjacent to each test implant for this study.

[0135] For the most part, the factors (materials, designs, process methods, system thermodynamic variables) are examined using straight-forward factorial designs that are analyzed using standard analysis of variance (ANOVA) and multi-variate linear modeling methods.

Claims

1. A bone-repair composite, comprising:
a core (118), the core (118) being a first primary unit including a combination of a first set of yarns (102) coated with a calcium phosphate mineral layer, the first set of yarns being made from a first group of one or more polymers selected from PLLA, PGA and PDO; and a sheath (120), the sheath (120) being a second primary unit including a combination of a second set of yarns (102) made of PCL, wherein the composite is made by covering the core with the sheath, and the composite is compression molded to allow the sheath to bond to the core.
2. A bone-repair composite of claim 1, wherein the composite has a bending modulus comparable to that of a mammalian bone.
3. A bone-repair composite of claim 2, wherein the ratio of the core (118) to the sheath (120) is provided to maximize the mechanical strength of the bone-repair composite to mimic the mammalian bone.
4. A bone-repair according to claim 1, wherein the sheath (120) contains filling materials as aids in drug delivery, porosity or cohesion in the composite.
5. A bone-repair composite of claim 1, wherein the composite is subject to a hot compression molding at an elevated temperature, thereby melting the polymers having a lower melting temperature, and thus binding the polymers having a higher melting temperature with the polymers having a lower melting temperature.
6. A bone-repair composite of claim 1, wherein the composite is subjected to a cold compression molding using a solvent, wherein the solvent is vaporized to melt the sheath (120), and thus binding the sheath (120) to the core (118).
7. A bone-repair composite of claim 1, wherein the composite is subjected to an elevated temperature with a solvent, wherein the sheath (120) is melted and binds to the core (118).
8. A bone-repair composite of any of the preceding claims, wherein the calcium phosphate mineral layer is fully or partially aligned to a fiber axis or a polymer crystallites.
9. A method for making a bone repair synthetic composite comprising the steps of: forming an inner core (118) structure with a first set of yarns, the first set of yarns being made from a first group of one or more polymers selected from PLLA, PGA and PDO, wherein the inner core (118) structure is a first primary unit; coating the first set of yarns with a calcium phosphate mineral layer; forming an outer sheath (120) structure with a second set of yarns being made

of PCL, wherein the outer sheath (120) structure is a second primary unit; forming a secondary structure by combining an appropriate ratio of the inner core (118) structure to the outer sheath (120) structure; cutting the secondary structure into a length of a compression mold; arranging the secondary structure into the compression mold; and compression molding the secondary structure at an elevated temperature to melt at least the PCL into a polymer matrix which binds the secondary structure to generate a tertiary structure having the mechanical strength of a mammalian bone.

- 5 10. A method of claim 9, wherein the inner core (118) structure is formed by:
assembling a plurality of yarns together; rolling a mesh structure, wherein the mesh structure is knitted, woven, non-woven, braided, stacked, flocked, or felted; or rolling the plurality of yarns and the mesh structure together.
- 10 11. A method of claim 9, wherein the inner core (1180) is designed to facilitate water access rate and cellular access rate both longitudinally and laterally.
- 15 12. A method of claim 11, wherein the longitude access is controlled by time, degradation, and/or solubilization of the inner core (118) and/or
wherein the lateral access is controlled by braid density, coating, or binder of the binding material.
- 20 13. A method of claim 11, wherein the mineral layer is hydrodynamically aligned/coated on the polymer fiber by dip or
die coating of the polymer fiber using suspension of calcium phosphate particles in solvents or polymer solutions.
- 25 14. A method of claim 11, wherein growth factors or other biological agents is added to the core (118).
15. A method of claim 9, further comprising drawing the coated yarn to form a coated drawn yarn, wherein the calcium phosphate particles are oriented along the coated drawn yarn.

Patentansprüche

- 30 1. Verbundmaterial zur Knochenreparatur, umfassend:
einen Kern (118), wobei der Kern (118) eine erste Primäreinheit ist, die eine Kombination aus einem ersten Satz von Fäden (102) beinhaltet, die mit einer Calciumphosphat-Mineralschicht überzogen sind, wobei der erste Satz von Fäden aus einer ersten Gruppe von einem oder mehreren Polymeren, ausgewählt aus PLLA, PGA und PDO, hergestellt wird; und eine Hülle (120), wobei die Hülle (120) eine zweite primäre Einheit ist, die eine Kombination eines zweiten Satzes von Fäden (102) aus PCL beinhaltet, wobei das Verbundmaterial durch Bedecken des Kerns mit der Hülle hergestellt wird und das Verbundmaterial formgepresst wird, damit sich die Hülle mit dem Kern verbinden kann.
- 40 2. Verbundmaterial zur Knochenreparatur nach Anspruch 1, wobei das Verbundmaterial einen Biegemodul aufweist, der mit dem eines Säugetierknochens vergleichbar ist.
3. Verbundmaterial zur Knochenreparatur nach Anspruch 2, wobei das Verhältnis des Kerns (118) zu der Hülle (120) vorgesehen ist, um die mechanische Festigkeit des Verbundmaterials zur Knochenreparatur zu maximieren, um den Säugetierknochen nachzuahmen.
- 45 4. Knochenreparatur nach Anspruch 1, wobei die Hülle (120) Füllmaterialien als Hilfsmittel bei der Arzneimittelabgabe, Porosität oder Kohäsion in dem Verbundmaterial enthält.
5. Verbundmaterial zur Knochenreparatur nach Anspruch 1, wobei das Verbundmaterial bei einer erhöhten Temperatur einer Heißverformung unterzogen wird, wodurch die Polymere mit einer niedrigeren Schmelztemperatur geschmolzen werden und so die Polymere mit einer höheren Schmelztemperatur mit den Polymeren mit einer niedrigeren Schmelztemperatur verbunden werden.
- 55 6. Verbundmaterial zur Knochenreparatur nach Anspruch 1, wobei das Verbundmaterial einem Kaltpressverfahren unter Verwendung eines Lösungsmittels unterzogen wird, wobei das Lösungsmittel verdampft wird, um die Hülle (120) zu schmelzen und so die Hülle (120) an den Kern (118) zu binden.
7. Verbundmaterial zur Knochenreparatur nach Anspruch 1, wobei das Verbundmaterial einer erhöhten Temperatur

mit einem Lösungsmittel ausgesetzt ist, wobei die Hülle (120) geschmolzen wird und sich an den Kern (118) bindet.

8. Verbundmaterial zur Knochenreparatur nach einem der vorhergehenden Ansprüche, wobei die Calciumphosphat-Mineralschicht vollständig oder teilweise auf eine Faserachse oder einen Polymerkristalliten ausgerichtet ist.

5 9. Verfahren zur Herstellung eines synthetischen Verbundmaterials zur Knochenreparatur, umfassend die Schritte: Bilden einer inneren Kernstruktur (118) mit einem ersten Satz von Fäden, wobei der erste Satz von Fäden aus einer ersten Gruppe von einem oder mehreren Polymeren, ausgewählt aus PLLA, PGA und PDO, hergestellt ist, wobei die Struktur des inneren Kerns (118) eine erste Primäreinheit ist; Beschichten des ersten Satzes von Fäden mit einer Calciumphosphat-Mineralschicht; Bilden einer Struktur der Außenhülle (120) mit einem zweiten Satz von Fäden aus PCL, wobei die Struktur der Außenhülle (120) eine zweite Primäreinheit ist; Bilden einer Sekundärstruktur durch Kombinieren eines geeigneten Verhältnisses der Struktur des inneren Kerns (118) zu der Struktur der äußeren Hülle (120); Schneiden der Sekundärstruktur in eine Länge einer Pressform; Anordnen der Sekundärstruktur in der Pressform; und Formpressen der Sekundärstruktur bei einer erhöhten Temperatur, um mindestens das PCL zu einer Polymermatrix zu schmelzen, die die Sekundärstruktur bindet, um eine Tertiärstruktur mit der mechanischen Festigkeit eines Säugetierknochens zu erzeugen.

10 10. Verfahren nach Anspruch 9, wobei die Struktur des inneren Kerns (118) gebildet wird durch: Zusammensetzen einer Vielzahl von Fäden; Walzen einer Gewebestruktur, wobei die Gewebestruktur gestrickt, gewebt, nicht gewebt, geflochten, gestapelt, beflockt oder gefilzt ist; oder Zusammenrollen der Vielzahl der Fäden und der Gewebestruktur.

15 11. Verfahren nach Anspruch 9, wobei der innere Kern (1180) so gestaltet ist, dass die Wasserzugangsrate und die zelluläre Zugangsrate sowohl in Längs- als auch in Querrichtung erleichtert wird.

20 12. Verfahren nach Anspruch 11, wobei der Längenzugang durch Zeit, Abbau und/oder Solubilisierung des inneren Kerns (118) gesteuert wird und/oder wobei der seitliche Zugang durch Geflechtdichte, Beschichtung oder Bindemittel des Bindematerials gesteuert wird.

25 13. Verfahren nach Anspruch 11, wobei die Mineralschicht hydrodynamisch auf die Polymerfaser durch Tauch- oder Düsenbeschichtung der Polymerfaser unter Verwendung einer Suspension von Calciumphosphatpartikeln in Lösungsmitteln oder Polymerlösungen ausgerichtet/beschichtet wird.

30 14. Verfahren nach Anspruch 11, wobei dem Kern (118) Wachstumsfaktoren oder andere biologische Agenzien hinzugefügt werden.

35 15. Verfahren nach Anspruch 9, ferner umfassend das Ziehen des beschichteten Fadens zur Bildung eines beschichteten gezogenen Fadens, wobei die Calciumphosphatpartikel entlang des beschichteten gezogenen Fadens orientiert sind.

40

Revendications

1. Composite pour la réparation osseuse, comprenant :

45 une partie centrale (118), la partie centrale (118) étant une première unité primaire incluant une combinaison d'un premier ensemble de fils (102) revêtus d'une couche minérale de phosphate de calcium, le premier ensemble de fils étant fabriqué à partir d'un premier groupe à base d'un ou de plusieurs polymères choisis parmi du PLLA, du PGA et du PDO ; et une enveloppe (120), l'enveloppe (120) étant une seconde unité primaire comprenant une combinaison d'un second ensemble de fils (102) fabriqués en PCL, où le composite est fabriqué en recouvrant la partie centrale avec l'enveloppe, et le composite est moulé par compression pour permettre à l'enveloppe de se lier à la partie centrale.

50 2. Composite pour la réparation osseuse selon la revendication 1, dans lequel le composite a un module de flexion comparable à celui d'un os de mammifère.

55

3. Composite pour la réparation osseuse selon la revendication 2, dans lequel le rapport de la partie centrale (118) sur l'enveloppe (120) est fixé pour maximiser la résistance mécanique du composite pour la réparation osseuse afin d'imiter l'os de mammifère.

4. Réparation osseuse selon la revendication 1, dans laquelle l'enveloppe (120) contient des matériaux de remplissage facilitant l'administration du médicament, la porosité ou la cohésion dans le composite.
5. Composite pour la réparation osseuse selon la revendication 1, dans lequel le composite est soumis à un moulage par compression à chaud à température élevée, faisant ainsi fondre les polymères ayant une température de fusion plus basse, et liant ainsi les polymères ayant une température de fusion plus élevée avec les polymères ayant une température de fusion plus basse.
10. Composite pour la réparation osseuse selon la revendication 1, dans lequel le composite est soumis à un moulage par compression à froid utilisant un solvant, dans lequel le solvant est vaporisé pour faire fondre l'enveloppe (120) et lier ainsi l'enveloppe (120) à la partie centrale (118).
15. Composite pour la réparation osseuse selon la revendication 1, dans lequel le composite est soumis à une température élevée avec un solvant, dans lequel l'enveloppe (120) est fondu et se lie à la partie centrale (118).
20. Composite pour la réparation osseuse selon l'une quelconque des revendications précédentes, dans lequel la couche minérale de phosphate de calcium est entièrement ou partiellement alignée par rapport à un axe de fibres ou à des cristallites de polymère.
25. Procédé de fabrication d'un composite synthétique pour la réparation osseuse comprenant les étapes : de formation d'une structure de partie centrale (118) interne avec un premier ensemble de fils, le premier ensemble de fils étant fabriqué à partir d'un premier groupe d'un ou de plusieurs polymères choisis parmi du PLLA, du PGA et du PDO, où la structure de la partie centrale (118) interne est une première unité primaire ; de revêtement du premier ensemble de fils avec une couche minérale de phosphate de calcium ; de formation d'une structure d'enveloppe (120) externe avec un second ensemble de fils en PCL, où la structure d'enveloppe (120) externe est une seconde unité primaire ; de formation d'une structure secondaire en combinant un rapport approprié de la structure de partie centrale (118) interne sur la structure de l'enveloppe (120) externe ; de découpage de la structure secondaire dans une longueur d'un moule de compression ; de disposition de la structure secondaire dans le moule de compression ; et de moulage par compression de la structure secondaire à une température élevée pour faire fondre au moins le PCL en une matrice polymère qui lie la structure secondaire pour générer une structure tertiaire ayant la résistance mécanique d'un os de mammifère.
30. Procédé selon la revendication 9, dans lequel la structure de la partie centrale (118) interne est formée par : l'assemblage d'une pluralité de fils entre eux ; le laminage d'une structure maillée, où la structure maillée est tricotée, tissée, non tissée, tressée, empilée, floquée ou feutrée ; ou le laminage conjoint de la pluralité de fils et de la structure maillée.
35. Procédé selon la revendication 9, dans lequel la partie centrale (1180) interne est conçue pour faciliter un niveau d'accès de l'eau et un niveau d'accès aux cellules à la fois longitudinalement et latéralement.
40. Procédé selon la revendication 11, dans lequel l'accès longitudinal est contrôlé par le délai, la dégradation et/ou la solubilisation de la partie centrale (118) interne, et/ou dans lequel l'accès latéral est contrôlé par la densité de la tresse, le revêtement, ou le liant du matériau de liaison.
45. Procédé selon la revendication 11, dans lequel la couche minérale est alignée hydrodynamiquement / revêtue sur la fibre polymère par un trempage ou un revêtement à la filière de la fibre polymère en utilisant une suspension de particules de phosphate de calcium dans des solvants ou des solutions de polymère.
50. Procédé selon la revendication 11, dans lequel des facteurs de croissance ou d'autres agents biologiques sont ajoutés à la partie centrale (118).
55. Procédé selon la revendication 9, comprenant en outre l'étirage du fil revêtu pour former un fil étiré revêtu, dans lequel les particules de phosphate de calcium sont orientées le long du fil étiré revêtu.

**COMPARATIVE PERCENT RETAINED TENSILE STRENGTH
FOR PLLA SUTURE IN pH =7.4 BUFFER SOLUTION
37°C (MONTHS) VS 50°C (WEEKS)**

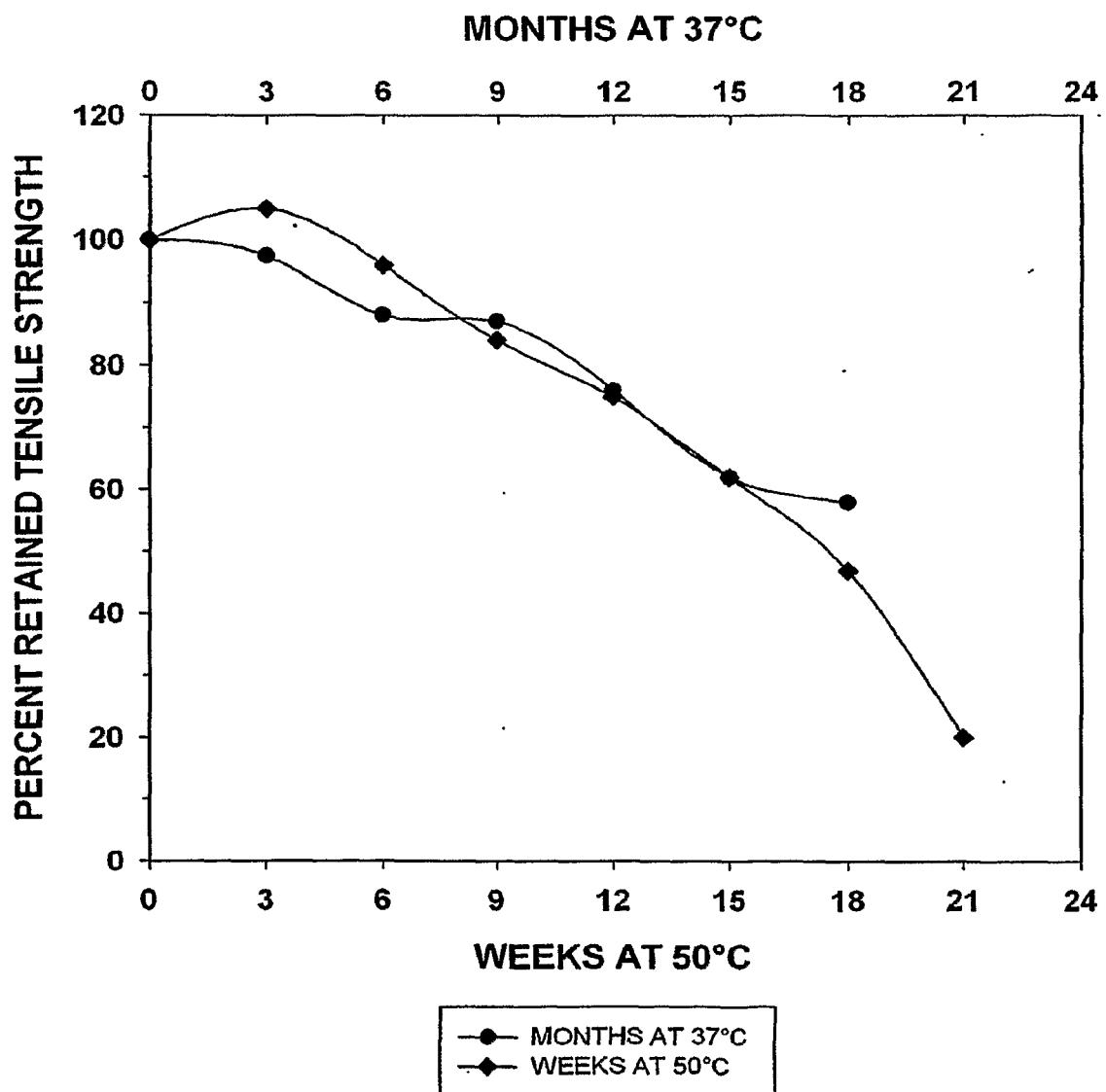


FIG. 1

**PERCENT RETAINED TENSILE STRENGTH
FOR PLLA YARN IN pH = 7.4 BUFFER SOLUTION
AT 50°C**

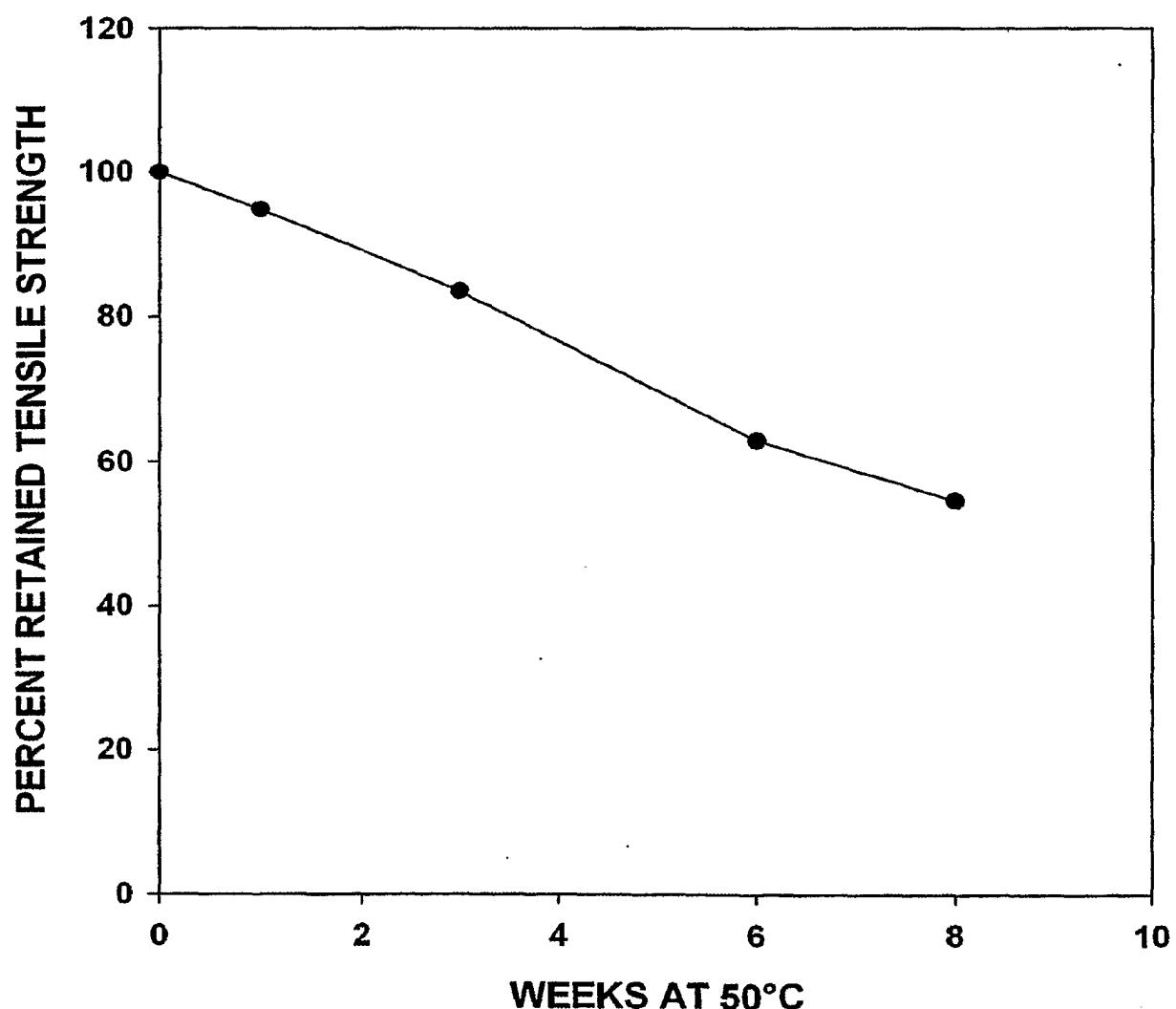


FIG. 2

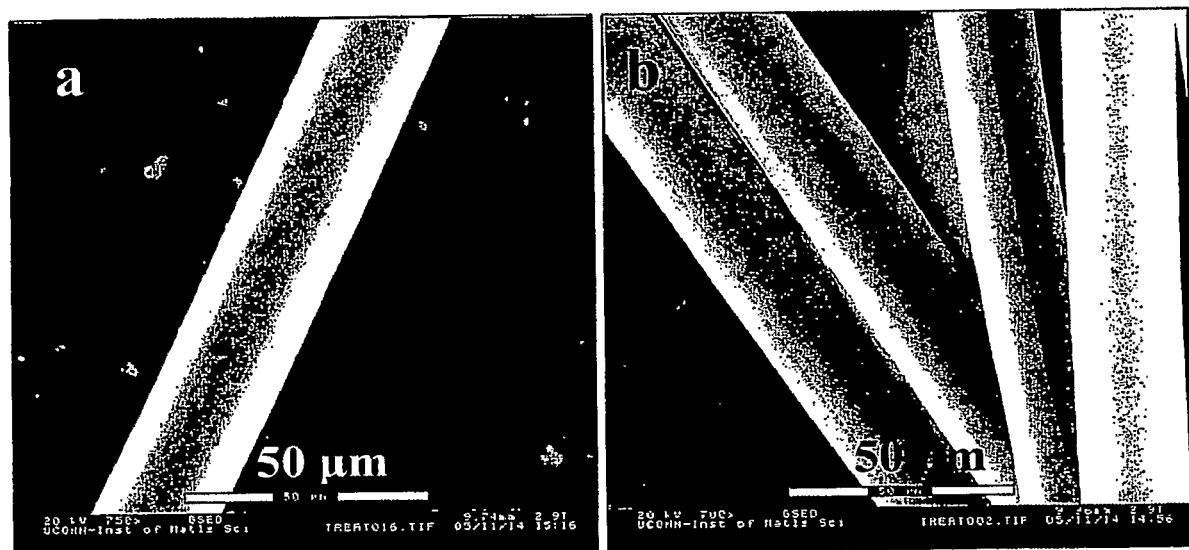


FIG. 3

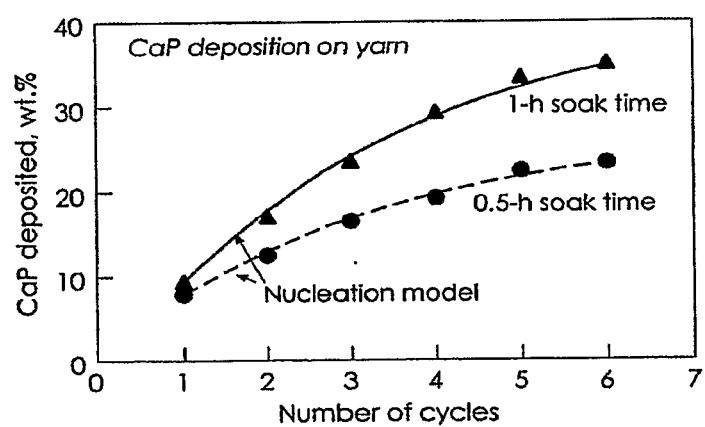


FIG. 4

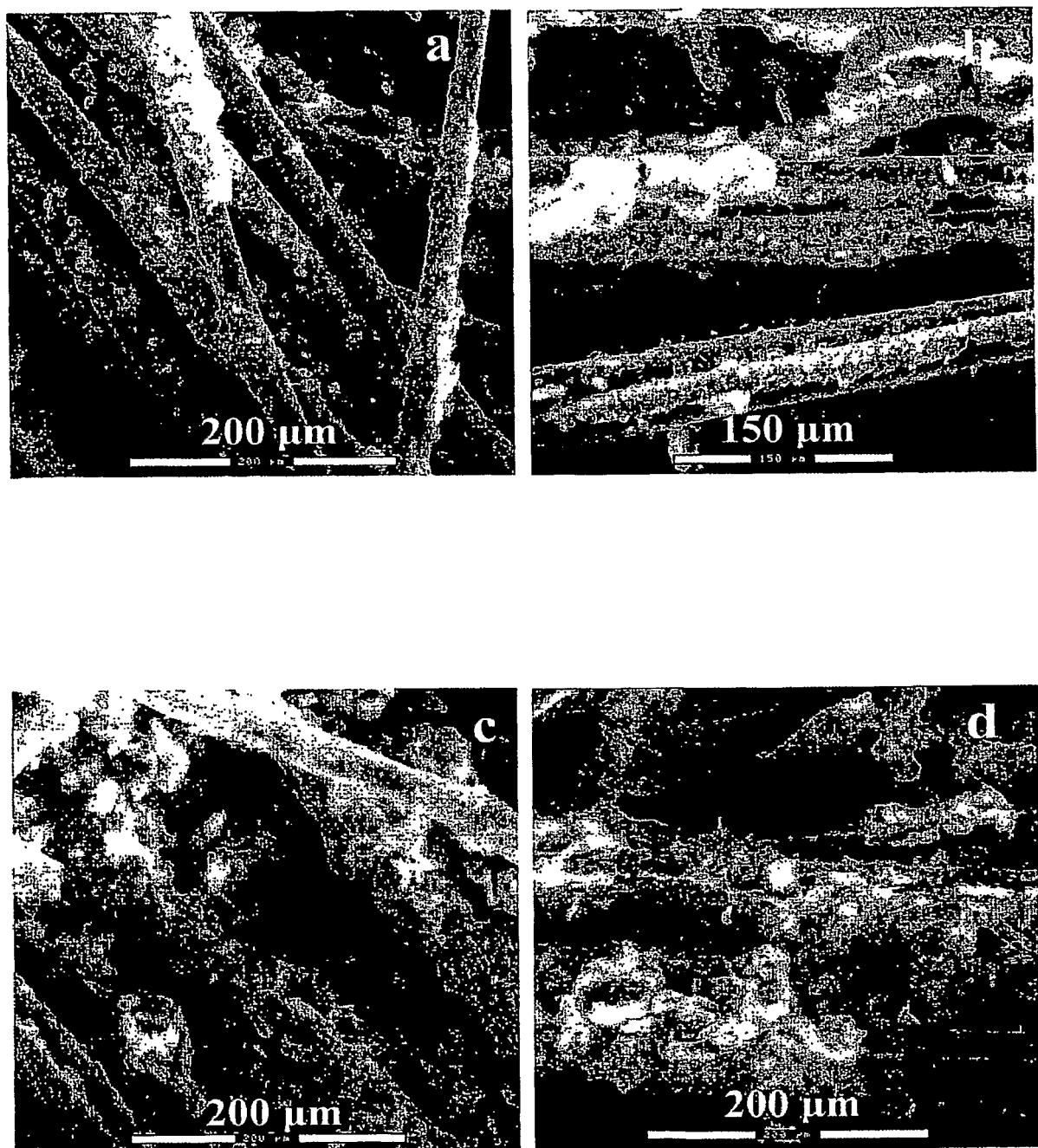


FIG. 5

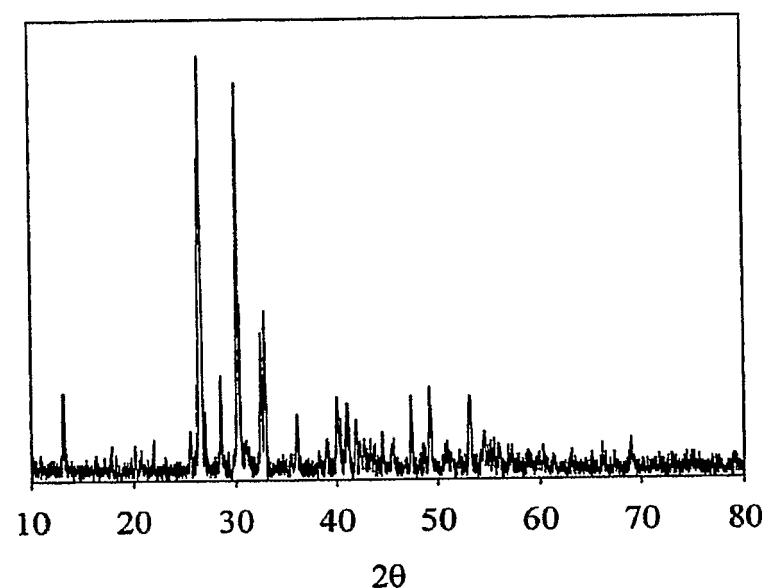


Fig. 6

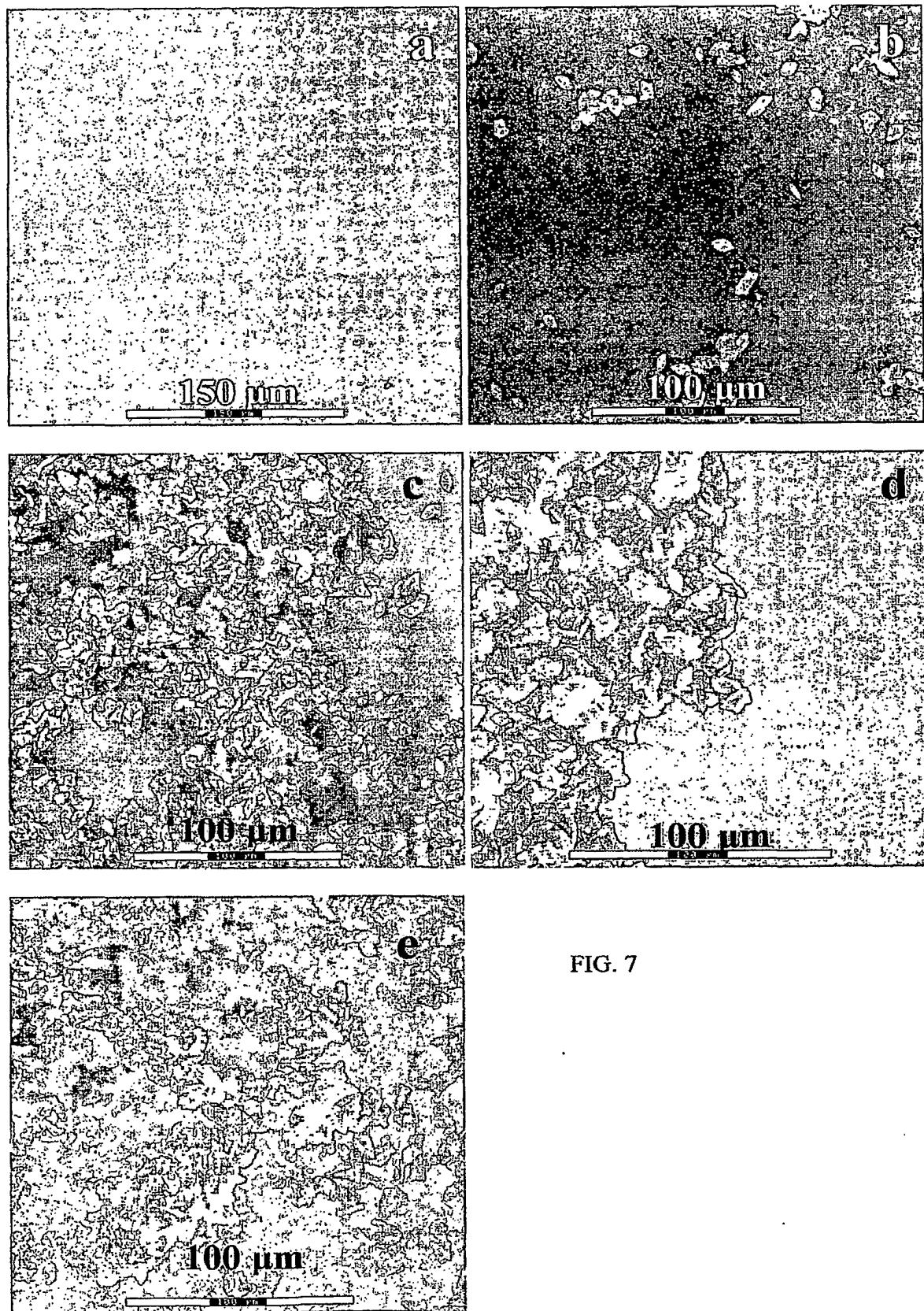


FIG. 7

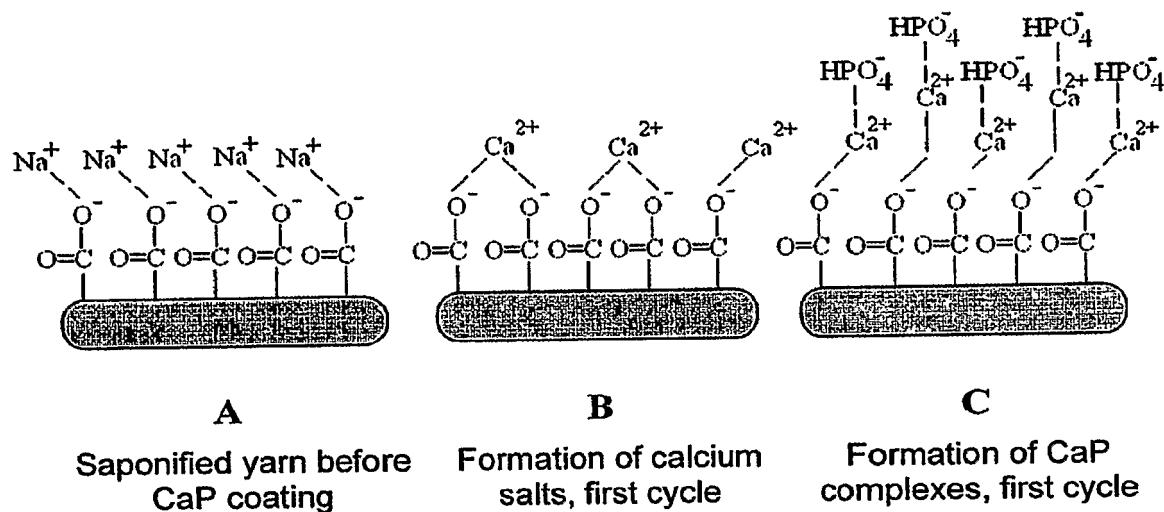


FIG. 8

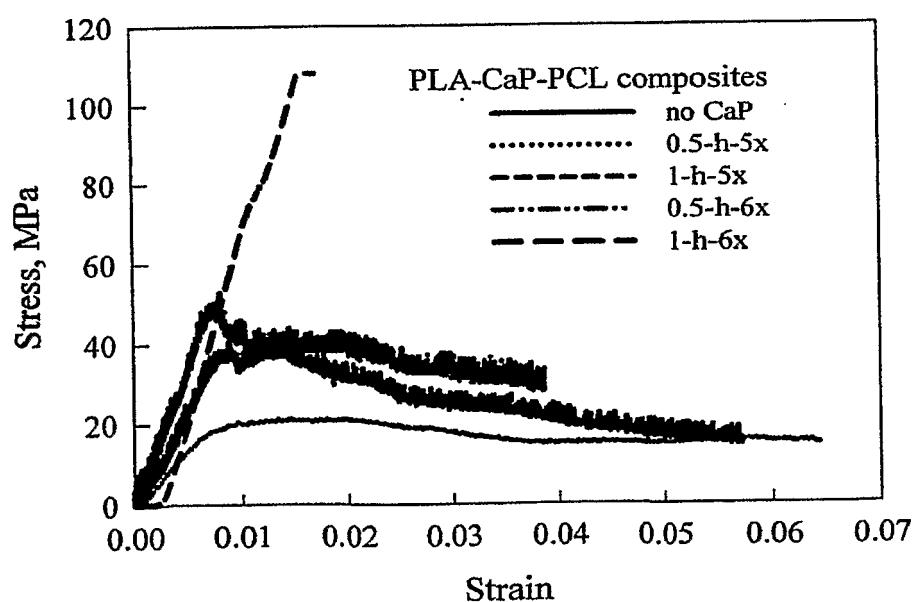


FIG. 9

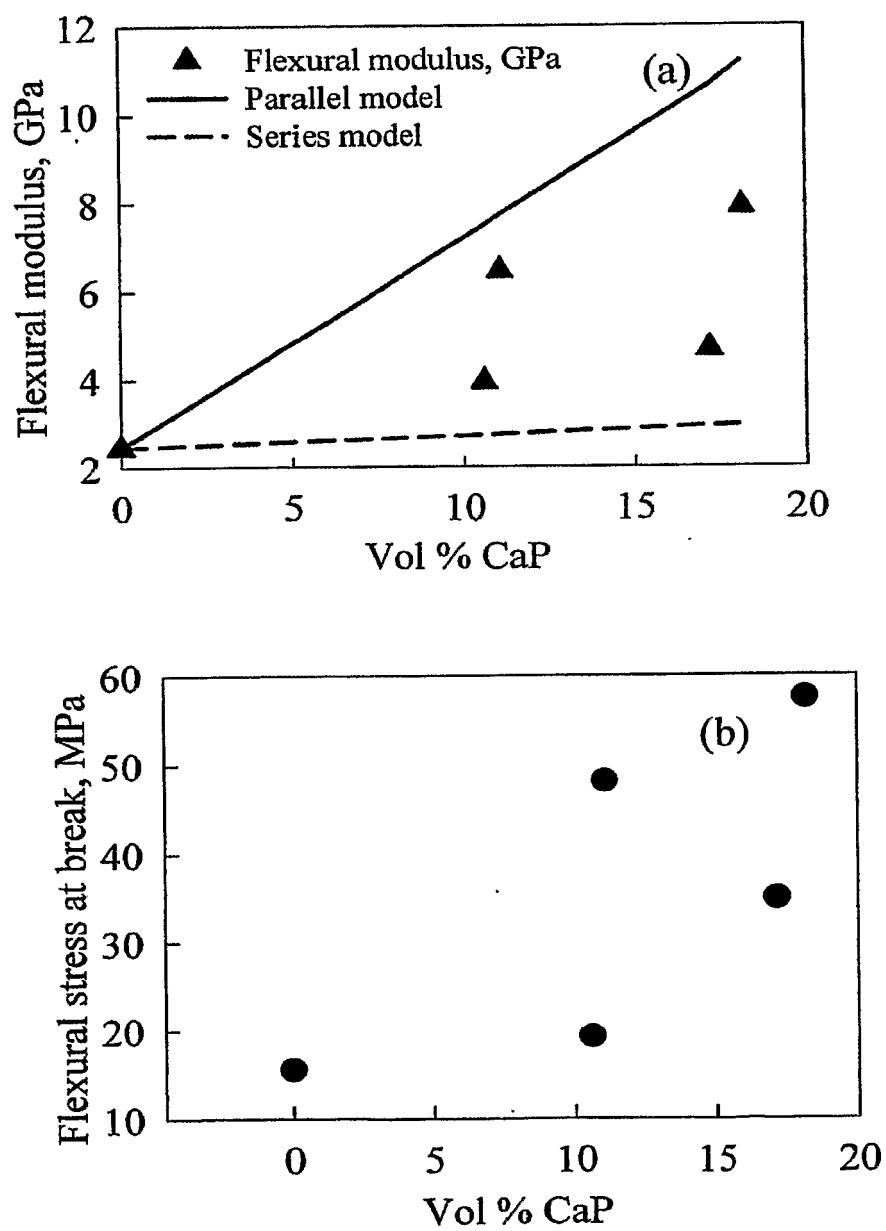


FIG. 10

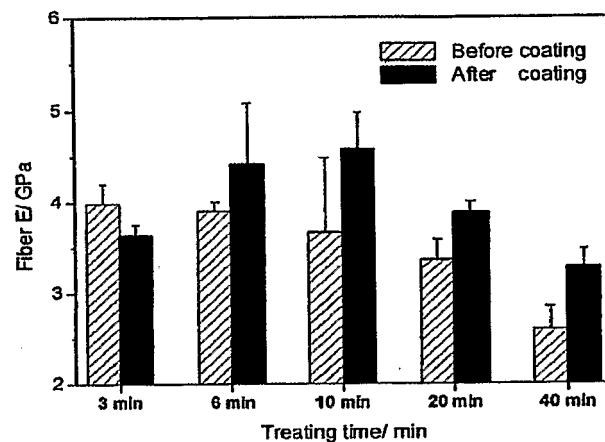


FIG. 11

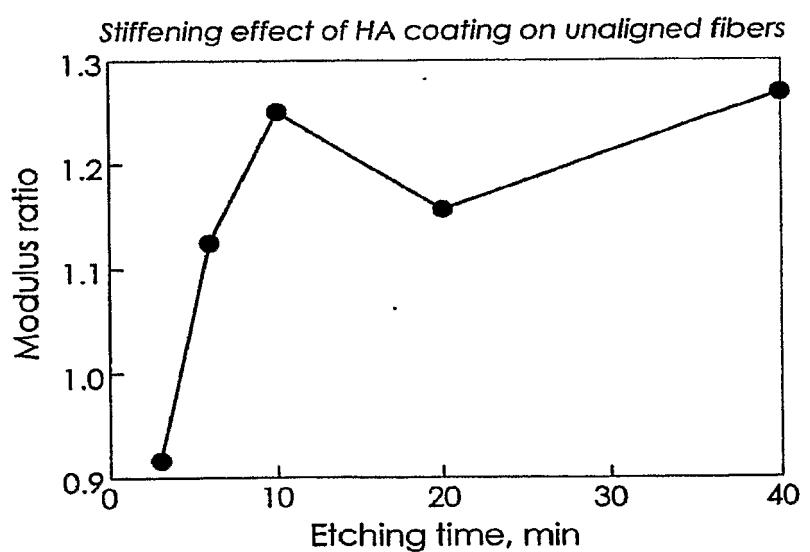


FIG. 12

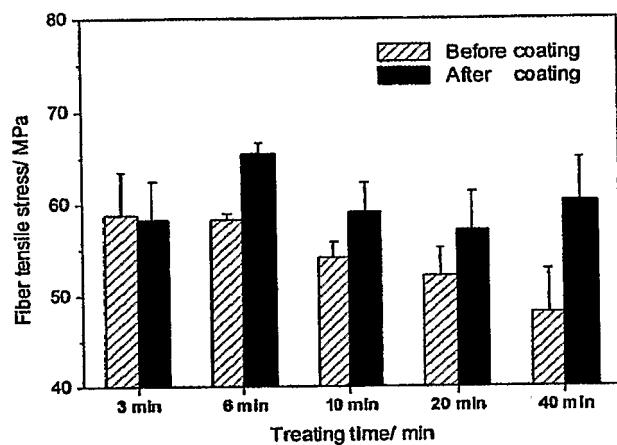


FIG. 13

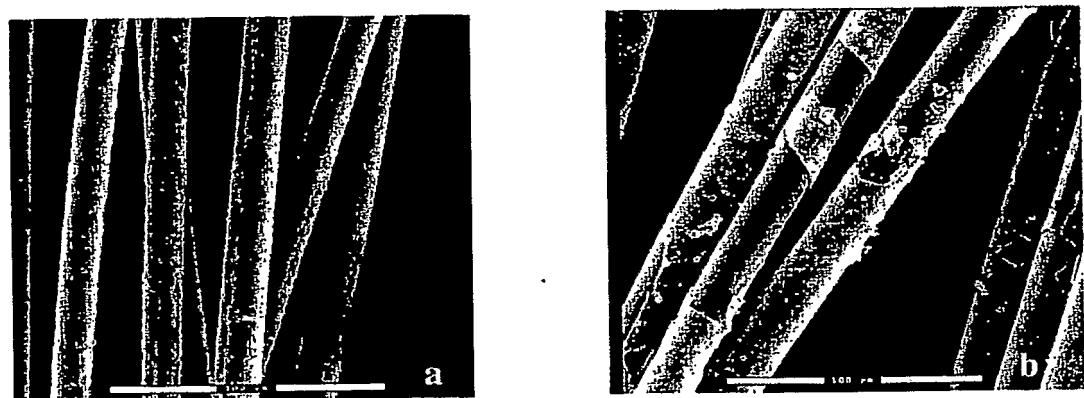


FIG. 14

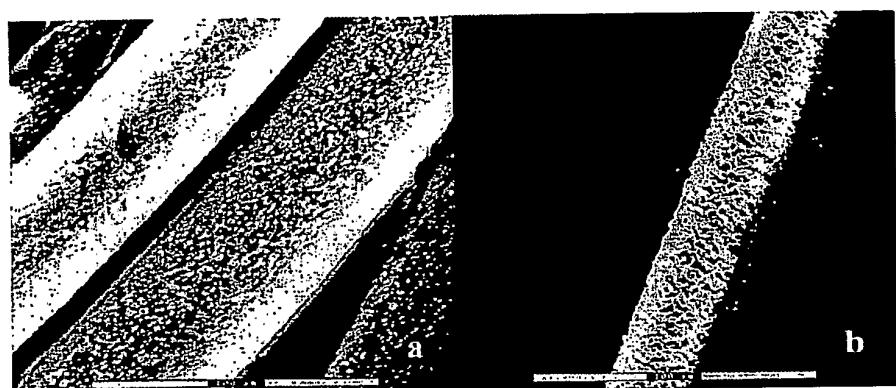


FIG. 15

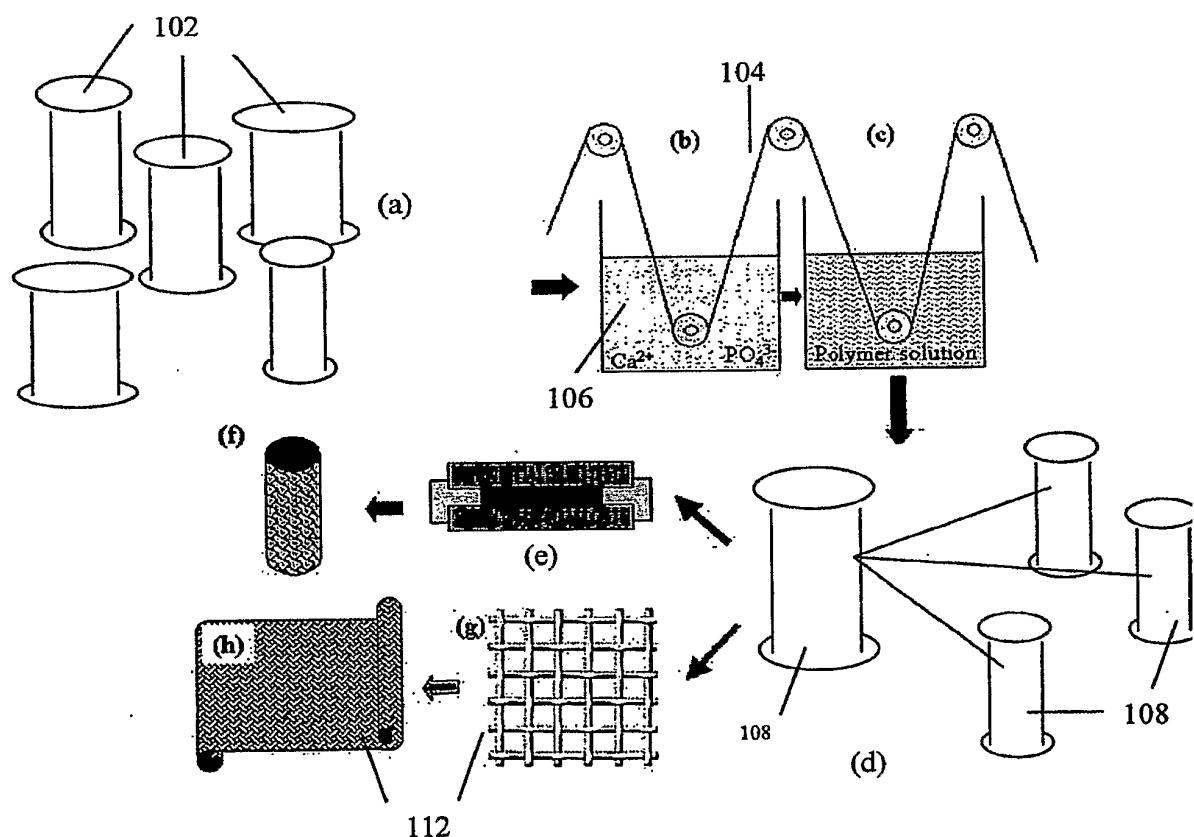


FIG. 16

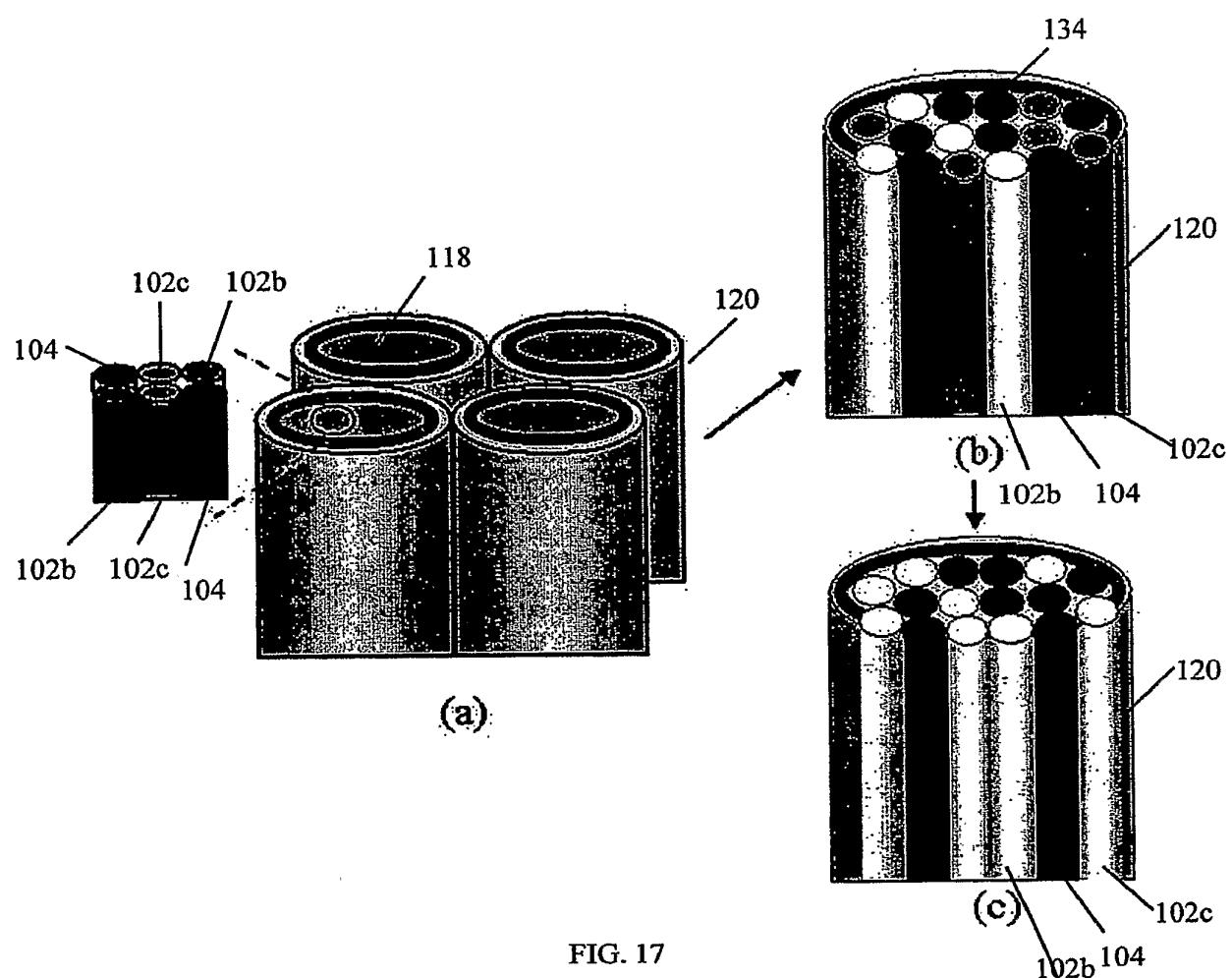


FIG. 17

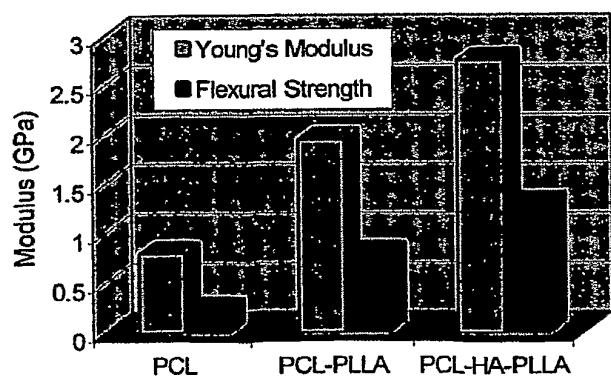


FIG. 18

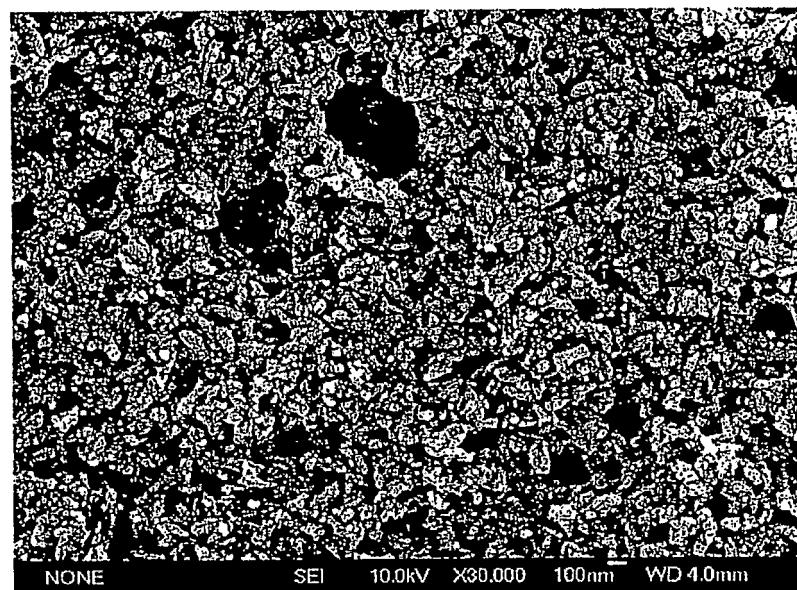


FIG. 19

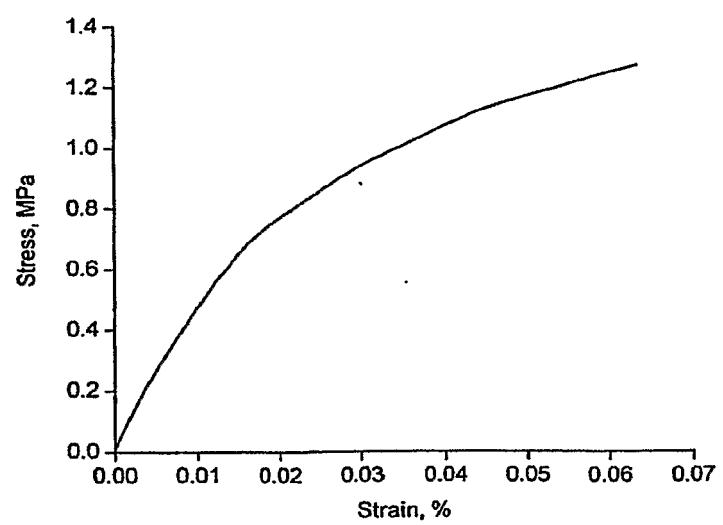


FIG. 20

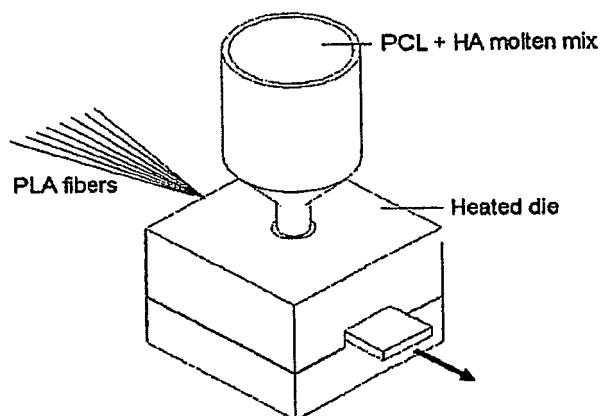


FIG. 21

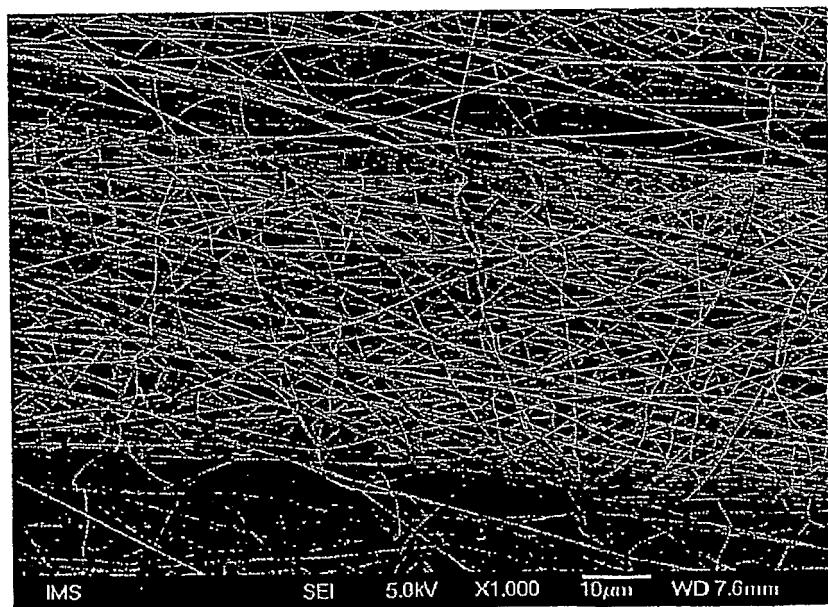


FIG. 22

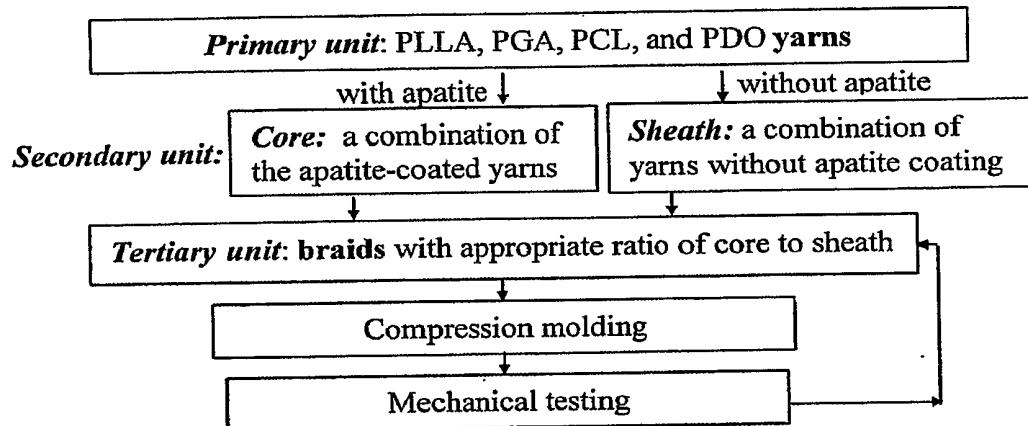


FIG. 23

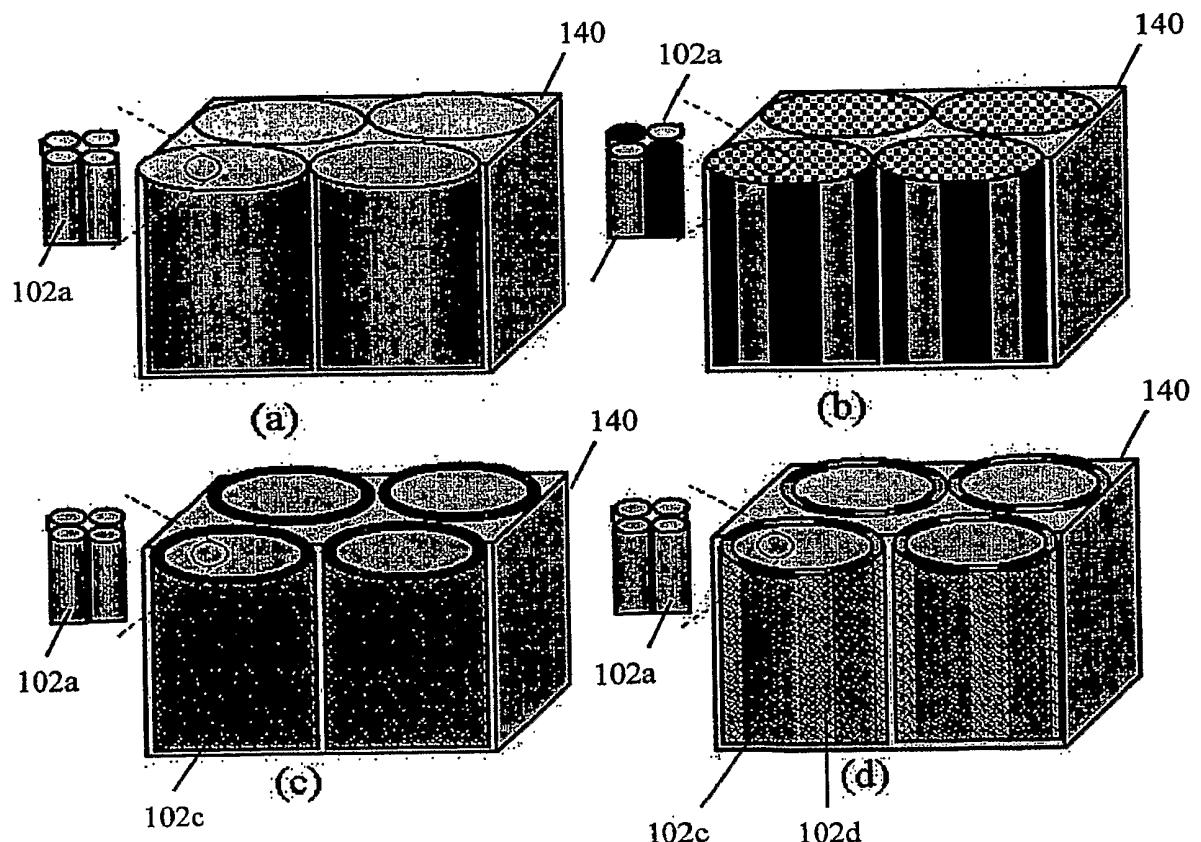


FIG. 24

REFERENCES CITED IN THE DESCRIPTION

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Non-patent literature cited in the description

- **XIAOYAN et al.** *J. of biomedical material research*, 2001, vol. 57, 141 [0010]