(19) DANMARK

(10) **DK/EP 2425686 T3**

Patent- og Varemærkestyrelsen

(12) # Oversættelse af europæisk patentskrift

(51) Int.Cl.: ***H 05 H 6/00 (2006.01)*** ***H 05 H 3/00 (2006.01)*** ***H 05 H 3/06 (2006.01)***

(45) Oversættelsen bekendtgjort den: **2019-04-23**

(80) Dato for Den Europæiske Patentmyndigheds bekendtgørelse om meddelelse af patentet: **2019-03-13**

(86) Europæisk ansøgning nr.: **09844184.3**

(86) Europæisk indleveringsdag: **2009-05-01**

(87) Den europæiske ansøgnings publiceringsdag: **2012-03-07**

(86) International ansøgning nr.: **US2009042508**

(87) Internationalt publikationsnr.: **WO2010126529**

(84) Designerede stater: **AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO SE SI SK TR**

(73) Patenthaver: **BTI Targetry, LLC, 1939 Evans Road, Cary, NC 27513, USA**

(72) Opfinder: **STOKELY, Matthew, Hughes, 2501 Ridge Road, Raleigh, NC 27612, USA**
WIELAND, Bruce, W., 114 Fieldstone Court, Chapel Hill, NC 27514, USA

(74) Fuldmægtig i Danmark: **AWA Denmark A/S, Strandgade 56, 1401 København K, Danmark**

(54) Benævnelse: **Partikelstrålemål med forbedret varmeoverførsel og tilhørende fremgangsmåde**

(56) Fremdragne publikationer:

WO-A1-96/06519
WO-A1-2008/003527
WO-A1-2008/073468
GB-A- 1 285 320
US-A- 4 843 246
US-A1- 2004 217 304
US-B1- 6 717 162

DESCRIPTION

TECHNICAL FIELD

[0001] The present invention relates generally to particle beam targets utilized for producing radionuclides. More particularly, the present invention relates to the cooling of targets during irradiation by a particle beam.

BACKGROUND

[0002] Radionuclides may be produced by bombarding a target with an accelerated particle beam as may be generated by a cyclotron, linear accelerator, or the like. The target contains a small amount of target material that is typically provided in the liquid phase but could also be a solid or gas. The target material includes a precursor component that is synthesized to the desired radionuclide in reaction to irradiation by the particle beam. As but one example, F-18 ions may be produced by bombarding a target containing water enriched with the 0-18 isotope with a proton beam. After bombardment, the as-synthesized F-18 ions may be recovered from the water after removing the water from the target. The production of F-18 ions in particular has important radiopharmaceutical applications. For instance, the as-produced F-18 ions may be utilized to produce the radioactive sugar fluorodeoxyglucose (2-fluoro-2-deoxy-D-glucose, or FDG), which is utilized in positron emission tomography (PET) scanning. PET is utilized in nuclear medicine as a metabolic imaging modality in the diagnosis of cancer.

[0003] The production of radionuclides such as F-18 ions is an expensive process, and thus any improvement to the production efficiency and yield would be desirable. Unfortunately, the application of the particle beam initiates the desired nuclear reaction in only a very small fraction of the radionuclide precursors in the target. The particle beam deposits a significant amount of heat into the target material residing in the target during bombardment. For instance, in the conventional production of F-18 ions, it has been found that only about one of every 2,000 protons stopping in the target water actually produces the desired nuclear reaction, with the rest of the proton beam merely depositing heat. Yet the amount of radioactive product that can be produced in a radionuclide target is proportional to the amount of heat that can be removed during bombardment of the target material of choice. Moreover, the rapidly increasing vapor pressure developed in the target chamber containing the target material as a result of the heat deposition may cause the target to structurally fail if the heat deposition is not adequately removed.

[0004] Radionuclide production yield could be increased by increasing the beam energy inputted to the target, but due to the foregoing problems the beam energy has been intentionally limited in conventional systems. Conventional radionuclide production systems may provide a means for cooling the beam targets generally by routing a heat transfer medium such as water to the target to carry heat away therefrom during bombardment. Conventional target designs, however, do not have sufficient capacity for heat removal, and as a result the radionuclide production yield and efficiency has been less than desirable in conventional targets.

[0005] In view of the foregoing, there is an ongoing need for beam targets utilized for radionuclide production that enable increased capacity and efficiency for removing heat and thus improved radionuclide production yield and efficiency. The heat energy deposited in the target material may cause boiling and generate bubbles or voids in the volume of target material. Bubbles or voids do not yield radionuclides; the particle beam simply passes through the bubbles or voids to the back of the target structure.

[0006] WO 2008/073468 A1 relates to a system and method provided for reclaiming an enriched radioisotope starting material from a target body. A chemical protective layer is disposed between a radioisotope starting material and a base material of the target body. After the target body is irradiated, the irradiated radioisotope starting material can be removed without removing the base material due to the protection provided by the chemical protective layer. The target body has the protective layers and has at its backside a hollow chamber being a coolant passage which in turn has tubular openings to the backside thereof. The tubular openings extend at the backside from the target body through the hollow chamber. The tubular openings may be connected internally within the base layer such that a channel is formed between the two tubular openings. Using external tubes coupled to the openings, coolant may enter through opening into the coolant passage disposed therebetween and exit the hollow chamber via opening back to the coolant source. Grooves disposed on the backside of the target body are configured to increase the surface area of the target body, thereby improving heat transfer from the target to the coolant.

SUMMARY

[0007] The present invention defines a particle beam target according to claim 1 as well as a method for cooling a particle beam target according to claim 13. Particular embodiments of the present invention are defined in the dependent claims.

[0008] Other devices, apparatus, systems, methods, features and advantages of the disclosure will be or will become apparent to one with skill in the art upon examination of the following figures and detailed description.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009] The invention can be better understood by referring to the following figures. The components in the figures are not necessarily to scale, emphasis instead being placed upon illustrating the principles of the invention. In the figures, like reference numerals designate corresponding parts throughout the different views.

Figure 1 is a simplified schematic view of an example of a radionuclide production apparatus or system as an example of an operating environment in which a target according to the present teachings may be implemented.

Figure 2 is a side, partially cut-away view of an example of a target according to the present teachings.

Figure 3 is a perspective view of the back side of the target illustrated in Figure 2.

Figure 3A is an elevation view of an entrance slot in front of the back side of the target.

Figure 4 is a perspective view of the front side of the target.

Figure 5 is another perspective view of the back side of the target.

Figure 6 is an elevation view of the front side of the target.

Figure 7 is a perspective, cross-sectional view of the target that has been cut-away at a plane that reveals peripheral bores fluidly interconnecting respective grooves and radial outflow bores.

Figure 8 is a cross-sectional elevation view of the target that has been cut-away at a plane that reveals the radial outflow bores.

Figure 9 is a cross-sectional elevation view of the target that has been cut-away at a plane that reveals one of the grooves in fluid communication with a corresponding pair of peripheral bores and radial outflow bores.

Figure 10 is a cross-sectional elevation view of the target that has been cut-away at a plane that reveals a target material inlet bore and outlet bore.

Figure 11 is a perspective view of an example of a target assembly in which the target may be included.

Figure 12 is a cross-sectional view of the target assembly illustrated in Figure 11.

Figure 13 is an exploded perspective view of the target and an associated sealing element and target window.

Figure 14 is an exploded perspective view of a conventional design of a target and associated sealing element and target window.

DETAILED DESCRIPTION

[0010] By way of example, Figures 1-13 illustrate various implementations of a target and associated radionuclide production apparatus or system. The various implementations provide a highly efficient solution for cooling a target cavity containing target material bombarded by particles (e.g., protons) for the purpose of obtaining a maximum amount of heat removal from the target material and thereby maximizing the amount of radioactive product that can be produced from that target material. As noted above, the amount of radioactive product that can be produced in a radionuclide target is proportional to the amount of heat that can be removed during bombardment of the target material of choice. In various implementations, a high rate of heat removal is accomplished at least in part by providing numerous individual, high-velocity, multi-stage coolant flow paths arranged in parallel and closely spaced to each other ad in close proximity to the target cavity containing the target material to be cooled. This configuration maximizes the heat flow from the target medium to the coolant by minimizing the heat conduction distance (i.e., the thickness of the target structure across which the heat must be transferred). The target may be implemented in connection with any type of liquid coolant and any type of radionuclide synthesis process. A target consistent with the present teaching has experimentally demonstrated superior performance in transferring heat away from target material, as compared to conventional targets.

[0011] Figure 1 is a simplified schematic view of an example of a radionuclide production apparatus or system **100** as an example of an operating environment in which a target **102** according to the present teachings may be implemented. The target 102 generally includes a front side (beam input side) **112** at which a particle beam **114** is directed and a back side (coolant input side) **116** which, in the presently described implementation, receives an input of any suitable liquid coolant (e.g., water). The target **102** also generally includes a target body that may include one or more parts assembled together. Insofar as the target **102** may include assembled components, the target **102** may also be referred to herein as a target assembly. The target **102** is typically constructed from a suitable metal or metal alloy, a few examples being silver, aluminum, gold, nickel, titanium, copper, platinum, tantalum, niobium, and stainless steel. At the front side **112**, the target **102** includes a target window **118** of any material suitable for transmitting the particle beam **114** therethrough while minimizing loss of beam energy. Typically, the target window **118** is constructed from a metal or metal alloy, a few examples being the commercially available HAVAR® alloy, titanium, tantalum, tungsten, and gold. The thickness of the target window **118** may range, for example, from 0.3 to 30 μm. A target chamber or cavity **120** is formed within the target body and defines an interior of the target body into which the particle beam **114** is directed via the target window **118**. In practice, the target cavity **120** contains a flowable target material that includes a radionuclide precursor, the composition of which will depend on the type of radionuclide being synthesized. As a non-limiting example, the internal volume (or size) of the target cavity **120** may range from 1.0 to 10 cm^3. A coolant inlet **122** and a coolant outlet **124** are also formed in the target body. The coolant inlet **122** and the coolant outlet **124** communicate with each other via a coolant flow system internal to the target body, as described in more detail below.

[0012] In some non-limiting examples, particularly where the target material is a liquid, the volume of the target cavity **120** after assembly of the target window **118** thereto ranges from 0.5 cc (or ml) to 20 cc. In other non-limiting examples, particularly where the target material is a solid, the volume of the target cavity **120** after assembly of the target window **118** thereto ranges from 0.1 cc to 20 cc. In other non-limiting examples, particularly where the target material is a gas, the volume of the target cavity **120** after assembly of the target window **118** thereto ranges from 100 cc to 10,000 cc (10 L).

[0013] One or more target material transfer bores may be formed in the target **102** for inputting target material into and/or outputting target material from the target cavity **120.** In the present example, a target material inlet bore **132** and a separate target material outlet bore **134** are formed in the target body and fluidly communicate with the target cavity **120.** The locations of the inlet bore **132** and the outlet bore **134** are arbitrary in the schematic view of the Figure 1, and may depend on whether it is desired to load the target **102** with target material from the top or the bottom. For example, the inlet bore **132** may alternatively be located at the top of the target cavity **120** and the outlet bore **134** may be located at the bottom of the target cavity **120.** As a further alternative, the target **102** may include a single bore **132** or **134** utilized for both introducing target material (including precursors) to the target cavity **120** and removing target material (including radionuclides) from the target cavity **120**.

[0014] The illustrated example, in which a single fluid transfer bore **132** or **134** or both an inlet bore **132** and an outlet bore **134** are utilized, is directed primarily to the use of a liquid target material. It will be appreciated by persons skilled in the art that in other cases, such as where the target material is a solid or a gas, the inlet bore **132** and/or outlet bore **134** may be modified as necessary or not utilized at all. As one example of the use of a solid target material, molten target material could first be loaded into the target cavity **120** and allowed to solidify, and the target material is maintained in the solid phase during application of the particle beam due to the cooling provided by the present teachings.

[0015] The radionuclide production apparatus **100** includes a particle beam source **140** such as, for example, a cyclotron, a linear accelerator, or the like. The structure and operation of the particle beam source **140** may depend on the type of particle beam **114** utilized. As an example, the particle beam **114** may be a proton beam. The proton beam is typically applied at a beam power of about 0.5 kW or greater, up to a practical limit that avoids structural failure of the target **102** and impairment of the desired nuclear reaction. In conventional targets, the beam power typically does not exceed about 2 kW. In at least some implementations of the target **102** taught herein, it is expected that the beam power may be increased to about 10 kW or greater.

[0016] The radionuclide production apparatus **100** also includes a target material transport circuit or system **150.** The target material transport system **150** may include any suitable target material source (supply, reservoir, etc.) **152**, a device for moving the target material such as, for example, a pump **154**, and a target material input line **156** for conducting the target material from the target material source **152** to the inlet bore **132** and thus the target cavity **120.** The target material transport system **150** may be implemented as a loop, in which case the above-noted outlet bore **134** is included as well as a target material output line **158** that leads back to the target material source **152** or at least back to the pump **154**. By utilizing the loop configuration, the target material may be flowed through the inlet bore **132**, filling the target cavity **120**, and through the outlet bore **134** prior to activation of the particle beam **114.** In this manner, the target material transport system **150** may be utilized to purge the target cavity **120** of bubbles, gases, contaminants, or any other undesired components prior to application of the particle beam **114** and ensuing synthesis. In practice, the target cavity **120** may be filled from the top (in which case the inlet bore **132** may be located at the top, as in the illustrated example) or from the bottom (in which case the inlet bore **132** may be located at the bottom). The schematically illustrated positions of the target material source **152** and the pump **154** may be switched as needed for top-filling or bottom-filling.

[0017] In the present example, the target material transport system 150 may also be utilized to route as-produced radionuclides to a desired radionuclide destination 162 for further processing, such as a hot lab. For this purpose, a radionuclide output line **164** is schematically shown as fluidly communicating with the target material outlet line **158** (or, alternatively, with the target material inlet line **156**). A valve or other controllable flow-diverting means (not shown) may serve as an interface between the target material transport system **150** and the radionuclide output line **164** for this purpose.

[0018] The radionuclide production apparatus **100** also includes a coolant circulation circuit or system **170.** The coolant circulation system **170** may include any suitable coolant conditioning apparatus (heat exchanger, condenser, evaporator, and the like) **172** for providing coolant to the target **102,** receiving heated coolant from the target **102,** removing heat from the heated coolant, and repeating the cycle as needed during synthesis. The coolant circulation system **170** may also include a device for moving the coolant to and from the target **102** such as, for example, a pump **174,** a coolant input line **176** for conducting the coolant from the coolant conditioning apparatus **172** to the coolant inlet **122** of the target **102,** and a coolant output line **178** for conducting the heated coolant from the coolant outlet **124** of target **102** back to the coolant conditioning apparatus **172.**

[0019] In practice, the target material source **152** is provided with a suitable supply of target material, and the target cavity **120** is loaded with a suitable amount of target material by flowing the target material from the target material source **152** into the target cavity **120**. Once the target cavity **120** is filled (partially or entirely, depending on design) with a desired amount of target material, the particle beam source **140** is operated to generate a particle beam **114,** which is directed into the target cavity **120** via the target window **118** for interaction with the target material. Application of the particle beam **114** results in synthesis of radionuclides from the target material in the target cavity **120.** After a sufficient amount of time during the "beam-on" stage has elapsed, the particle beam **114** is switched off and the as-produced radionuclides are transported to the hot lab or other destination **162** for further processing.

[0020] As noted above, during application of the particle beam **114**, a large amount of energy is deposited as heat in the target material residing in the target cavity **120.** This heat generates a large amount of vapor within the target cavity **120** resulting in voids or bubbles within the target material. The voids or bubbles interfere with the particle beam's ability to cause the nuclear reaction needed for radionuclide synthesis, and the vapor pressure may quickly cause the target **102** to fail structurally. Hence, the heat must be rapidly removed from the target **102** and from the target material residing in the target **102.** This is accomplished through the operation of the coolant circulation system **170** during application of the particle beam **114** in conjunction with a coolant circulation system incorporated into the target **102**, as described by way of examples below.

[0021] A non-limiting example of radionuclide synthesis is the production of the F-18 ($^{18}F^{-}$) ion (fluorine-18) from the 0-18 (oxygen-18) precursor. In this case, the target material may be provided as 0-18 enriched water, i.e., water in which a desired fraction has the composition $H_2{}^{18}O$, and the particle beam is a proton beam. The nuclear reaction is specified as $^{18}O(p,n)^{18}F$. Other examples of radionuclides that may be produced include, but are not limited to, N-13, 0-15, and C-11. N-13 is produced from natural water as the target material utilizing alpha-particles according to the nuclear reaction $^{16}O(p,\alpha)^{13}N$.

[0022] The target **102** disclosed herein is particularly suited for use as a "batch" or "static" target. In a batch or static target, the target material is loaded in the target cavity **120**, the same amount of target material remains in the target cavity **120** during synthesis, and the target material (now including radionuclides) is thereafter removed from the target **102.** An alternative type of target is a recirculating target, in which the target material is circulated through the target cavity **120** during application of the particle beam. In a recirculating target, the target material itself may be utilized as a heat transfer medium to some degree because the target material carries heat away from the target and, prior to being recirculated back to the target, may be cooled by a heat exchange system located remotely from and external to the target body. The present teachings, however, encompass the use of the target **102** disclosed herein as a recirculating target as an option for increasing the heat-removal capacity of the recirculating target.

[0023] Figure 2 is a side, partially cut-away view of an example of a target **200** according to the present teachings, and Figure 3 is a perspective view from the back side. The target **200** may be utilized in a radionuclide production system such as illustrated by example in Figure 1, or in other, differently configured radionuclide production systems. The target **200** includes a target body **202** that may be mounted in a recess of a front target section **204.** A target cavity and various coolant passages defining a plurality of coolant paths (not shown) are formed in the target body **202** as described below. The front target section **204** closes off the front side of the target cavity, and includes a target window **218** for receiving a particle beam 114 as described above. The front target section **204** abuts a medial target section **206** that surround the target body **202.** The back side of the target **200** receives an input flow of coolant from a coolant input line **276** in a manner described below. In some implementations, an input plenum (or manifold, chamber, conduit, etc.) **208** of any suitable design is interposed between the coolant input line **276** and the back side of the target body **202** for receiving the input coolant.

The input plenum **208** may be formed by a coolant inlet body or region of the medial target section **206** for distributing coolant to the back side of the target body **202** in a manner described below. In this example, a plurality of parallel grooves **344** (Figure 3) is formed in the back side of the target body **202.** The input plenum **208** may taper in the direction of the back side to direct the input coolant flow to the grooves **344.** In the present example, the coolant outlet is implemented as a plurality of radial outflow bores **224** circumferentially distributed about the target body **202.** The radial outflow bores **224** may terminate at a lateral outer wall **210** of the target body **202.** The radial outflow bores **224** may fluidly communicate with one or more coolant output lines **178** (Figure 1) to enable removal of heat from the target **200** and the target material residing in the target **200,** as noted above. To facilitate routing the coolant from the radial outflow bores **224** to the coolant output line(s) **178,** an output plenum of any suitable design may be provided. For this purpose, in the illustrated example the output plenum includes one or more chambers **211** and radially distributed axial bores **213** formed in the medial target section **206.**

[0024] Referring to Figure 3, the input plenum **208** has an entrance **341** that may have any suitable shape and size. In this example, the input plenum **208** is shaped so as to transition to an elongated slot or slit **342** that serves as the entrance to the grooves **344** formed in the back side of the target body **202.** Figure 3A illustrates the elongated slot **342** in front of the grooves **344.** A portion of these grooves **344** are visible through the elongated slot **342.** The elongated slot **342** is oriented along a vertical direction in Figure 3A. It will be understood, however, that the term "vertical" is relative to the perspective of Figure 3A and that in practice no limitations are placed on the orientation of the target **200** or any of its components relative to any particular frame of reference. In the present example, the grooves **344** are oriented transversely relative to the elongated slot **342.** Thus, in the example specifically illustrated in Figure 3A, the grooves **344** may be characterized as being horizontal although again it will be understood that the term "horizontal" is utilized in a relative sense without any limitation being placed on a particular orientation for the grooves **344.** The elongated slot **342** is dimensioned such that coolant flowing through the elongated slot **342** will be divided into each of the grooves **344.** That is, all grooves **344** are exposed through the elongated slot **342** as shown in Figures 3 and 3A. Thus, for example, if fourteen grooves **344** are provided, the input flow of coolant passing through the elongated slot **342** will be divided into fourteen separate, individual input flow paths, with each input flow path being associated with a respective groove **344.**

[0025] Figure 4 is a perspective view of the front side of the target **200** (or at least the main target section **202**) according to the presently described example. For reference purposes, Figure 4 provides three mutually orthogonal axes that intersect at a point within the target **200** such as in a target cavity **420** thereof: a lateral axis **A** passing through the target cavity **420** from the front side to the back side, a longitudinal axis **B** passing through the target cavity **420** from the bottom to the top (from the perspective of Figure 4), and a transverse axis **C** also passing through the target cavity **420.** Also for reference purposes, the lateral axis **A** may be associated with a depth of the target **200,** the longitudinal axis **B** may be associated with a length or height of the target **200**, and the transverse axis **C** may be associated with a width of the target **200.** This system of three reference axes **A, B and C** will be utilized in conjunction with Figures 5-10 as well.

[0026] As illustrated in Figure 4, the target cavity **420** includes a lateral inner wall **422** that defines the cross-section of the target cavity **420** in the plane of the longitudinal axis **B** and the transverse axis **C**. The cross-section of the target cavity **420** may include an oblong section that adjoins a rounded top end and a rounded bottom end. That is, the target cavity **420** is elongated in the longitudinal direction. In the present example, the target cavity **420** may open at the front face of the target **200** and may be bounded by the front target section **204** (Figure 2) after assembly. A channel **424** surrounding the target cavity may be formed in the front face for receiving a suitable gasket or other sealing component (not shown), thereby forming a fluid seal at the interface between the main target section **202** and the front target section **204.** Figure 4 also shows the circumferential series of radial outflow bores **224** that open at the outer surface of the main target section **202.** In the present context, term "radial" is relative to the intersection point of the three reference axes **A, B and C** and is not intended to limit the target **200** as having a circular shape or any other particular shape. Figure 4 also shows a target inlet (or outlet) bore **432.** The target inlet bore **432** may open at a flat section to facilitate fluid connection with a fitting or other component.

[0027] Figure 5 is a perspective view of the back side of the target **200** (or at least the main target section **202**) according to the present example. The plurality of transversely oriented grooves **344** is formed in the back face. The grooves **344** are adjacent to the target cavity **420** (Figure 4). The respective widths of the grooves **344** are sized so as to be somewhat greater than the width of the cross-section of the target cavity **420** at all elevations of the target cavity **420.** Accordingly, the grooves **344** may collectively exhibit the rounded and oblong shape of the target cavity **420** that characterizes the present example. As described in more detail below, the widths of the grooves **344** enable coolant to be routed in close proximity with the target cavity **420** in the lateral direction to maximize heat transfer from the target cavity **420.**

[0028] Figure 6 is an elevation view of the back side of the target **200.** Each groove **344** is separated from an adjacent groove **344** by a thin, transverse groove wall **646.** Each groove **344** runs in the transverse direction between a first groove end 652 and an opposing second groove end **654.** Each groove end **652** and **654** fluidly communicates with at least one peripheral bore **656** and **658.** Some of the grooves **344** may communicate with more than one peripheral bore **656** and **658.** Thus, the number of grooves **344** may be equal to half the number of peripheral bores **656** and **658**, or less than half the number of peripheral bores **656** and **658.** In the illustrated example, the upper two grooves **344** and the bottom two grooves **344** each communicate with two peripheral bores **656** and **658** at their respective ends **652** and **654** for ease of fabrication and to facilitate the close spacing between adjacent peripheral bores **656** or **658.** As described in more detail below, the peripheral bores **656** and **658** circumscribe the cross-section of the target cavity **420** (Figure 4) in close proximity therewith and run in the lateral direction toward the front side of the target **200.** From Figures 3 and 6, it can be seen that each individual groove **344** splits the coolant input flow from the elongated slot **342** (Figure 3) into two flows that run in opposite transverse directions to respective peripheral bores **656** and **658** located at the first groove end **652** and second groove end **654.**

Assuming the width of the elongated slot **342** is uniform as illustrated in Figure 3 and the elongated slot **342** is positioned centrally between the first groove ends **652** and the second groove ends **654,** each groove **344** may split the coolant input flow generally evenly into the two transverse directions. In alternative implementations, the width and/or the position of the elongated slot **342** may vary along the longitudinal axis **B** to consequently vary the flow of coolant into various grooves **344** and corresponding peripheral bores **656** and **658.**

[0029] In the illustrated example in which fourteen grooves **344** are provided, the fourteen coolant flow paths entering the grooves **344** are thus divided into twenty-eight transverse coolant flow paths. In the illustrated example in which some of the groove ends **652** and **654** include more than one peripheral bore **656** or **658,** additional flow splitting occurs. Specifically, the present example includes twenty-eight groove ends **652** and **654** but thirty-six peripheral bores **656** and **658.** Thus, some of the twenty-eight flow paths running transversely to the twenty-eight groove ends **652** and **654** are further divided. As a result, a total of thirty-six coolant flow paths are provided in the corresponding peripheral bores **656** and **658** in the present example. The thirty-six coolant flow paths run through the peripheral bores **656** and **658** in the lateral direction in close proximity to each other and to the target cavity **420,** thereby enabling a highly efficient means for removing heat from the target material in the target cavity **420.** In other implementations, the number of coolant flow paths running in the various directions described herein may be different, the presently illustrated implementation being but one example.

[0030] In some examples, the thickness of each groove wall **646** (in the longitudinal direction) ranges from 0.002 to 0.125 inch (0.00508 to 0.3175 cm). The cross-sectional area of each groove **344** may be defined by the width of the groove **344** in the transverse direction and the height of the groove **344** in the longitudinal direction (between adjacent groove walls **646).** In some examples, the height of each groove **344** ranges from 0.01 to 0.125 inch (0.0254 to 0.3175 cm). In some examples, the diameter of each peripheral bore **656** and **658** ranges from 0.01 to 0.25 inch (0.0254 to 0.635 cm).

[0031] In the example illustrated in the Figure 6, the peripheral bores **656** and **658** may generally be divided into a first set associated with the first groove ends **652** and a second set associated with the second groove ends **654.** In each first or second set, the peripheral bores **656** and **658** are closely spaced with each other to maximize the amount of "coverage" of the target cavity **420** and thus the amount of surface area of the peripheral bores **656** and **658** available for transferring heat from the target cavity **420.** In some examples, the gap or spacing **648** between any pair of adjacent peripheral bores **656** or **658** of the first or second set ranges from 0.002 to 0.125 (0.00508 to 0.3175 cm). The minimal amount of target structure between adjacent peripheral bores **656** or **658** result in the dense coverage of the target cavity discussed above.

[0032] It will be noted that in Figure 6 the uppermost peripheral bore **656** of the first set is spaced at a greater distance from the uppermost peripheral bore **658** of the second set (across the longitudinal axis **B)** in comparison to the spacing **648** between adjacent peripheral bores **656** or **658** of the first or second set. The same may be said for the respective lowermost peripheral bores **656** or **658** of the first and second sets. This additional spacing is done in the present implementation merely to accommodate the location of the target material inlet bore and outlet bore, which by example are respectively positioned at the top and bottom of the target cavity **420** as shown in Figures 3-5 and 10. It will be understood, however, that in other implementations the target material inlet bore and outlet bore may be located in other positions whereby additional spacing between any two adjacent peripheral bores **656** or **658** occurs at a different location or not at all. Apart from the foregoing, the division of the peripheral bores **656** and **658** into first and second sets is conceptual and done for illustrative purposes.

[0033] Figure 7 is a perspective, cross-sectional view of the target that has been cut-away at a plane of the lateral axis **A** and longitudinal axis **B** that reveals two of the peripheral bores **656** fluidly interconnecting respective grooves **344** and radial outflow bores **224.** The target cavity **420** is bounded by the lateral inner wall **422** and an adjoining back inner wall **726.** The lateral inner wall **422** is adjacent to the circumferentially surrounding peripheral bores **656** and separated from the peripheral bores **656** by a relatively small distance through an annular portion **728** of the target structure. In some examples, the annular portion **728** has a thickness (in any radial direction relative to the lateral axis **A)** ranging from 0.002 to 0.5 inch (0.00508 to 1.27 cm). In other non-limiting examples, the thickness of the annular portion **728** ranges from 0.005 to 0.15 inch (0.0127 to 0.381 cm). In the illustrated example, the peripheral bores **656** run parallel to the lateral inner wall **422** such that the thickness of the annular portion **728** is uniform along the lateral direction. In alternative implementations, however, the peripheral bores **656** and/or the lateral inner wall **422** may be oriented such that this parallelism is not maintained. In the illustrated example, the series of peripheral bores **656** largely spans the entire extent of the area of the lateral inner wall **422** coaxially about the lateral axis **A** (see also Figure 6). Consequently, the peripheral bores **656** collectively provide a large surface area for transferring heat from the lateral inner surface **422,** through the annular portion **728,** and to the coolant flowing through the peripheral bores **656.** Each peripheral bore **656** is bounded by an inner peripheral bore wall **758** that extends from the corresponding groove **344** to the corresponding radial outflow bore **224.** Each inner peripheral bore wall **758** has a surface area, and the total surface area of the plurality of peripheral bores **656** may be defined as the summation of the surface areas of the individual inner peripheral bore walls **758.**

[0034] As also shown in Figure 7, the back inner wall **726** of the target cavity **420** is adjacent to the grooves **344** and separated from the grooves **344** by a relatively small distance through a back (or longitudinal) portion **730** of the target structure. In some examples, the back portion **730** has a thickness (in the lateral direction, over at least a majority of the grooves **344)** ranging from 0.002 to 0.5 (0.00508 to 1.27 cm). In the illustrated example, the series of parallel grooves **344** spans beyond the extent of the area of the back inner wall **726** to facilitate maximizing coverage of the target cavity **420** by the peripheral bores **656,** although in other examples may span at least a majority of the area of the back inner wall **726.** Moreover, the transverse groove walls or septa **646** (Figure 6) are thin. Consequently, the grooves **344** collectively provide a large surface area for transferring heat from the back inner wall **726**, through the back portion **730,** and to the coolant flowing through the grooves **344.** The total cross-sectional area of the plurality of grooves **344** may be defined as the summation of the cross-sectional areas of the individual grooves **344.**

[0035] As noted above, each groove **344** generally defines two coolant flow paths running along the transverse direction, with one coolant flow path running to the peripheral bore(s) **656** located at one groove end **652** (Figure 6) and the other coolant flow path running the opposing peripheral bore(s) **658** located at the other groove end **654** of the same groove **344.** Each coolant flow path then takes an orthogonal turn into a corresponding peripheral bore **656** or **658** and runs in the lateral direction, again in close proximity to the target cavity **420.** Thus, the coolant continues to remove heat from the target cavity **420** as it flows toward the front side of the target **200** along the lateral flow paths. To maximize heat removal, the peripheral bores **656** and **658** may extend over a large majority of the depth of the target cavity **420.** Each peripheral bore **656** and **658** runs to at least one radial outflow bore **224**. The radial outflow bores **224** may be sized (e.g., cross-sectional flow area) larger than the peripheral bores **656** and **658** and positioned such that more than one peripheral bore **656** and **658** terminates at the same radial outflow bore **224.** Thus, the number of radial outflow bores **224** may be equal to or less than the number of peripheral bores **656** and **658.** This configuration also minimizes the pressure drop in the radial outflow bores **224.** The cross-sectional flow area of each radial outflow bore **224** may progressively increase along the radial direction from the end of the peripheral bore **656** or **658** to the outer lateral wall **210** of the target structure, as illustrated in Figure 7.

[0036] Once the coolant reaches a radial outflow bore **224,** the coolant then takes an orthogonal turn into the radial outflow bore **224**. The coolant then runs in a radial outward direction to the end of the radial outflow bore **244** at the lateral outer surface **210** of the target **200**. While flowing in the radial outflow bore 244, the coolant continues to pick up heat energy. In the illustrated example, the radial outflow bores **244** are located in close proximity to the front side of the target **200** that receives the particle beam **214.** In some non-limiting examples, the radial outflow bores **244** are located at a distance from the front side along the lateral axis **A** ranging from 0.01 to 0.5 inch (0.0254 to 1.27 cm). Moreover, the radial outflow bores **244** are dimensioned so as to provide a large surface area available for heat transfer from the structural (solid) body constituting the target **200**. By this configuration, the coolant flowing through the radial outflow bores **244** is able to remove heat from the structural target body as well as from the target material being irradiated in the target cavity **420.** Upon reaching the lateral outer surface of the target **200**, the coolant may then be flowed away from the target **200** and recirculated back to the grooves **344** in the manner described above.

[0037] It thus can be seen that both the grooves **344** on the back side of the target **200** and the peripheral bores **656** and **658** running through the depth of the target **200** cover the inside surfaces of the target cavity **420** very densely and with a minimum of wall thickness between the coolant and the target cavity **420.** The radial outflow bores **224** provide additional heat-removing capacity in the manner described above. Moreover, the transverse grooves **344,** peripheral bores **656** and **658** and radial outflow bores **224** are dimensioned and positioned in a configuration that maintains a high-velocity coolant flow through the target **200** from input to output, thereby enabling the coolant to rapidly carry away the heat being deposited by the particle beam **214.** This foregoing configuration therefore maximizes heat removal from the target cavity **420.**

[0038] Figure 8 is a cross-sectional elevation view of the target **200** that has been cut-away at a plane of the longitudinal axis **B** and transverse axis **C** that reveals the radial outflow bores **224**. For reference purposes, the center of the target **200** is taken to be the geometrical center of the target cavity **420**, and the origin of the intersecting lateral axis **A**, longitudinal axis **B** and transverse axis **C** has been located at this center. Utilizing this frame of reference, each radial outflow bore **224** is located along a radius projected from the center. As noted above, one or more of the radial outflow bores **224** may fluidly communicate with more than one peripheral bore **656** or **648** (Figure 7). In the illustrated example, each radial outflow bore **224** communicates with two peripheral bores **656** or **658.** Thus, the thirty-six lateral coolant flow paths running through the respective peripheral bores **656** and **658** are reduced to eighteen radial coolant flow paths in the eighteen radial outflow bores **224** illustrated in Figure 8.

[0039] Figure 9 is a cross-sectional elevation view of the target **200** that has been cut-away at a plane of the lateral axis **A** and transverse axis **C** that reveals one of the grooves **344** in fluid communication with a corresponding pair of peripheral bores **656** and **658** and radial outflow bores **224.** Once an input flow of coolant to the back side of the target **200** is established, the resulting coolant flow paths may be summarized as follows. Initially, the coolant is flowed to the grooves **344** generally along the lateral direction, as indicated by an arrow **902.** The coolant input flow **902** encounters the grooves **344** in close proximity with back inner wall **726** of the target cavity **420**, and thus the coolant is able to immediately begin removing heat from the target cavity **420.** When the input flow **902** encounters the grooves **344**, the input flow **902** is initially divided along the longitudinal direction into each groove **344**. Thus, each groove **344** is associated with a coolant input flow path **902** separate from the other grooves **344**. The grooves **344** are orthogonal to the initial input flow **902.** Thus, in each groove **344** the input flow **902** is further divided such that one part of the input flow **902** is diverted to one groove end **652** while the other part of the input flow **902** is diverted to the opposing groove end **654** of the same groove **344**. The resulting two transverse coolant flow paths in the groove **344** are indicated by arrows **904** and **906.** When each transverse coolant flow **904** and **906** reaches a groove end **652** or **654,** that transverse coolant flow **904** and **906** is then diverted orthogonally into the peripheral bore **656** or **658** located at that groove end **652** or **654** (or one of the peripheral bores **656** or **658** in the case where more than one peripheral bore **656** or **658** is formed at a single groove end **652** or **654**). The resulting lateral coolant flow paths are indicated by arrows **912** and **914**. The lateral coolant flows **912** and **914** then run through the respective peripheral bores **656** and **658** to the corresponding radial outflow bores **224.** As coolant is fed into the radial outflow bores **224,** it is diverted into corresponding radial coolant outflow paths as indicated by arrows **916**. The coolant in each radial outflow bore **224** reaches the outer lateral wall **210** of the target **200** and is conducted away to an external heat exchanging device as described previously in this disclosure.

[0040] Figure 9 may be considered as showing the top end of the target cavity **420** at which the target material inlet bore **432** is located by example (or where the outlet bore may be located in another example). Alternatively, Figure 9 may be considered as showing the bottom end of the target cavity **420** at which the target material outlet bore (or inlet bore **432**) is located. The following description will refer to the target material inlet bore **432**, as located at the top end in the present example, with the understanding that the discussion may also apply to the target material outlet bore and/or to the bottom end of the target cavity **420.** In the illustrated implementation, the inlet bore **432** is surrounded by an inlet pocket or depression **982** formed in the lateral inner wall **422** of the target cavity **420.** The inlet pocket **982** may have any size and shape suitable for complete filling of the target cavity **420.** The length of the inlet pocket **982** in the lateral direction may be elongated relative to the width of the inlet pocket **982** in the transverse direction. In the present example, the inlet pocket **982** is elongated in the lateral direction and the width of the inlet pocket **982** in the transverse direction gradually tapers down (decreases) in the lateral direction toward the front side of the target **200.** The target material inlet bore **432** is located in the region of the inlet pocket **982** having the maximum width. The resulting "teardrop" shape of the inlet pocket **982,** with the target material inlet bore **432** located in the bulk of the teardrop, has been found to be effective for complete filling of the target cavity **420.** Likewise, an outlet pocket (not shown) may surround the outlet bore, and may have any size and shape suitable for complete recovery of target material. In the present example, the outlet pocket may be sized and shaped similarly to the illustrated inlet pocket **982.**

[0041] Figure 10 is a cross-sectional elevation view of the target **200** that has been cut-away at a plane of the lateral axis **A** and longitudinal axis **B** that reveals the target material inlet bore **432** and an outlet bore **1034**. In this example, the inlet bore **432** fluidly communicates with an inlet pocket **982** as described above, and the outlet bore **1034** fluidly communicates with an outlet pocket **1084**. As noted above, the respective sizes and shapes of the inlet pocket **982** and the outlet pocket **1084** may be the same or different. In the illustrated example, the above-noted tapering of each pocket **982** and **1084** also occurs along the longitudinal axis **A**, with each pocket **982** and **1084** being deepest in the vicinity of the inlet bore **432** or outlet bore **1034.**

[0042] Figure 11 is a perspective view of an example of a target assembly **1100** in which the target **200** may be included, and Figure 12 is a cross-sectional view of the target assembly **110**. The target assembly **1100** may be utilized in a radionuclide production system such as illustrated by example in Figure 1, or in other, differently configured radionuclide production systems. The target assembly **1100** generally includes the front target section **204** and the medial target section **206** as described above. In addition, the target assembly **1100** in this example includes a back target section **1121**. The back target section **1121** may include a chamber **1223** (Figure 12) that serves as part of the output plenum for carrying away heated output coolant from the target body **202**. The back target section **1121** may also include bores communicating with respective coolant input fittings **1125** and coolant output fittings **1127**. In the present example, the coolant input fittings **1125** communicate with the input plenum **208** and the coolant output fittings **1127** communicate with the chamber **1223** of the output plenum.

The target assembly **1100** may also include a beam guide **1130** for directing a particle beam from a particle beam source (e.g., the particle beam source **140** shown in Figure 1) to the target window **218** (Figure 12).

[0043] As also shown in Figure 12, various adjacent components of the target assembly **1100** may be fluidly sealed by sealing elements (e.g., o-rings, gaskets, etc.) seated in grooves or channels formed in or on such components. In particular, the arrangement of the target window **218** interposed between the target body **202** and the front target section **204** may be fluidly sealed by a sealing element seated in a channel **1241** formed in the front side of the target body **202**, and/or by a sealing element seated in a channel **1243** formed in the front target section **204.** Generally, the target window **218** may have any shape and planar size, so long as the outer diameter (or other relevant dimension, more generally perimeter) of the target window **218** is large enough that the target window **218** covers the opening of the target cavity **420**. In practice, the outer perimeter of the target window **218** is large enough to accommodate the use of fluid sealing means such as the illustrated sealing element/channel **1241** and/or **1243**. Figure 12 illustrates one non-limiting example in which the area of the target window **218** is coextensive with that of the front side of the target body **202.**

[0044] Continuing with Figure 11, the location of the peripheral bores **656** in relation to the target cavity **420**, as well as to other components of the target **200** and associated target assembly **1100**, optimizes the ability of the coolant circulating through the target **200** to remove heat from the target **200.** The peripheral bores **656** closely surround the target cavity **420** and span most of the axial depth of the target cavity **420** to maximize the amount of heat transfer therefrom. Relative to the lateral axis running through the target cavity **420**, the peripheral bores **656** are arranged about a perimeter at a radial distance not much greater than the radial extent of the target cavity **420.** This arrangement of the peripheral bores **656** may be characterized in relation to the target window **218** and the associated sealing element/channel **1241** and/or **1243.** It can be seen that the perimeter of the peripheral bores **656** is less that the outer perimeter of the target window **218.** Stated in another way, the area taken up by the arrangement of peripheral bores **656** is within the area of the target window **218.** Additionally or alternatively, the perimeter of the peripheral bores **656** is less that the perimeter of the sealing element/channels **1241** and **1243.** This arrangement of the peripheral bores **656** is facilitated by the provision of the radial outflow bores **244,** which allow the peripheral bores **656** to run close to the target cavity **420** and close up to the target window **218.** Additionally, the radial outflow bores **244** maximize heat removal from the target window **218** and the region of the target body **202** proximal to the target window **218.**

[0045] The advantages provided by the present teachings may be further illustrated by comparing Figures 13 and 14. Figure 13 is an exploded perspective view of the target **200,** a sealing element **1351**, and the target window **218.** The peripheral bores **656** (Figure 12) may be placed within the perimeter of the channel **1241** in which the sealing element **1351** is seated, as well as within the perimeter of the target window **218.** Coolant from the peripheral bores **656** is carried away by the radial outflow bores **244,** enabling the peripheral bores **656** to be immediately adjacent to the target cavity **240.** Figure 13 also shows an alternative circular cross-section for the target cavity **240.** By contrast, Figure 14 is an exploded perspective view of a conventional design of a target **1400** and its associated sealing element **1451** and target window **1418.** In Figure 14, the sealing element **1451** is seated in a recess **1441** formed in the target body and the target window **1418** is mounted in another recess **1445** concentrically surrounding the sealing element recess **1441.** This conventional target **1440** has a radial distribution of axial bores **1456** for conducting coolant from the back side to the front side of the target **1400.** These axial bores **1456,** however, must be arranged far away from the target cavity **1440** to avoid the target window **1418** and the sealing element **1451.** Hence, the axial bores **1456** are located outside the perimeter of both the sealing element recess **1441** and the target window **1418.**

[0046] In general, terms such as "communicate" and "in . . . communication with" (for example, a first component "communicates with" or "is in communication with" a second component) are used herein to indicate a structural, functional, mechanical, electrical, signal, optical, magnetic, electromagnetic, ionic or fluidic relationship between two or more components or elements. As such, the fact that one component is said to communicate with a second component is not intended to exclude the possibility that additional components may be present between, and/or operatively associated or engaged with, the first and second components.

[0047] Furthermore, the foregoing description is for the purpose of illustration only, and not for the purpose of limitation-the invention being defined by the claims.

REFERENCES CITED IN THE DESCRIPTION

Patent documents cited in the description

- WO2008073468A1 [0006]

P A T E N T K R A V

1. Partikelstrålemål (102, 200) omfattende:

et mållegeme (202) omfattende en frontside (102), en bagside (116) og en lateral, ydre væg (210), som udstrækker sig fra frontsiden til bagsiden; og

en flerhed af parallelle riller (344) dannet i bagsiden (116), hvor hver af rillerne omfatter en første rilleende (652) og en anden rilleende (654), og løber langs en transversal retning fra den første rilleende (652) til den anden rilleende (654), hvor den transversale retning er vinkelret på en lateral akse (A);

k e n d e t e g n e t ved

en målkavitet (420) anbragt i mållegemet (202), hvor målkaviteten (420) omfatter en indre bagvæg (726) en lateral, indre væg (422) og et tværsnit afgrænset af den laterale, indre væg (422), hvor den indre bagvæg (726) er anbragt i en afstand fra bagsiden (116) i forhold til den laterale akse (A), og hvor den laterale, indre væg (422) udstrækker sig fra den indre bagvæg (726) mod frontsiden (102) langs retningen af den laterale akse (A);

hvor en flerhed af perifere boringer (656, 658) udstrækker sig gennem mållegemet (202) fra flerheden af riller (344) mod frontsiden (102), hvor de perifere boringer (656, 658) er anbragt til at omskrive målkavitetens (420) tværsnit i nærhed af den laterale, indre væg (422), hvor hver rille (344) er i fluid kommunikation med mindst én perifer boring (656) ved den første rilleende (652) og mindst én anden perifer boring (658) ved den anden rilleende (654); og

en flerhed af radiale udløbsboringer (224), som udstrækker sig i respektive radiale retninger i forhold til den laterale akse (A) fra flerheden af perifere boringer (656, 658) til den laterale, ydre væg (210), hvor hver radial udløbsboring (224) er i fluid kommunikation med mindst én af de perifere boringer (656, 658),

hvor mållegemet (202) definerer en flerhed af strømningsveje (904, 906, 912, 914, 916) til flydende kølemiddel, hvor hver strømningsvej til flydende kølemiddel løber fra en respektive rille (344) til mindst én af den første rilleende (652) og den anden rilleende (654) af rillen (344), gennem mindst én perifer boring (656, 658), gennem mindst én radial udløbsboring (224) og til den laterale, ydre væg (210).

2. Partikelstrålemål (102, 200) ifølge krav 1, som desuden omfatter en målmaterialeindløbsboring (432, 1034), som udstrækker sig gennem mållegemet (202) og ind i fluid kommunikation med målkaviteten (420).

3. Partikelstrålemål (102, 200) ifølge krav 2, hvor målkaviteten (420) har en indløbslomme (982, 1084) dannet i den laterale, indre væg (422) og omskrivende målmaterialeindløbsboringen (432, 1034).

4. Partikelstrålemål (102, 200) ifølge krav 3, hvor indløbslommen (982, 1084) har en lateral dimension, som løber i en retning mod frontsiden, og en bredde tværgående på den laterale dimension, og hvor bredden aftager langs den laterale dimension i en retning væk

fra den tilsvarende indløbsboring (432, 1034).

5. Partikelstrålemål (102, 200) ifølge krav 3, hvor indløbslommen (982, 1084) har en lateral dimension, som løber i en retning generelt mod frontsiden, og en bredde tværgående på den laterale dimension, og hvor den laterale dimension er langstrakt i forhold til bredden.

6. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-5, hvor mindst én af flerheden af riller (344) er i fluid kommunikation med mere end én perifer boring (656, 658) ved den første rilleende (652) og mere end én perifer boring (656, 658) ved den anden rilleende (654), og hvor antallet af riller (344) er mindre end halvdelen af antallet af perifere boringer (656, 658).

7. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-6, hvor mindst én af flerheden af radiale udløbsboringer (224) er i fluid kommunikation med mere end én perifer boring (656, 658), og hvor antallet af radiale udløbsboringer (224) er mindre end antallet af perifere boringer (656, 658).

8. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-7, hvor tværsnitsstrømningsarealet af hver perifer boring (656, 658) er mindre end tværsnitsstrømningsarealet af hver radial udløbsboring (224).

9. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-8, hvor flerheden af radiale udløbsboringer (224) er anbragt nærmere på frontsiden end på bagsiden.

10. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-9, hvor målkaviteten (420) har en dybde langs den laterale akse (A), og hvor flerheden af perifere boringer (656, 658) udstrækker sig fra flerheden af riller (344) langs i det mindste en størstedel af dybden.

11. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-10, hvor flerheden af perifere boringer (656, 658) udstrækker sig i en retning parallelt med den laterale, indre væg (422).

12. Partikelstrålemål (102, 200) ifølge ethvert af kravene 1-11, som desuden omfatter et kølemiddelindløbslegeme (206), som ligger an mod bagsiden, og som dækker flerheden af perifere boringer (656, 658), hvor kølemiddelindløbslegemet (206) omfatter en langstrakt slids (342) i fluid kommunikation med hver af rillerne (344), hvor kølemiddelindløbslegemet (206) definerer en indløbsstrømningsvej (276) til flydende kølemiddel, som løber gennem den langstrakte slids (342) og ind i hver af rillerne (344), således at indløbsstrømningsvejen (276) til flydende kølemiddel forgrener sig til hver af strømningsvejene til flydende kølemiddel, og hvor hver strømningsvej til flydende kølemiddel er opdelt i en første strømningsvej (904) til flydende kølemiddel, der løber til den første rilleende (652), og en anden strømningsvej (906) til flydende kølemiddel, som løber til den anden rilleende (654).

13. Fremgangsmåde til at køle et partikelstrålemål (102, 200), hvor partikelstrålemålet (102, 200) omfatter en målkavitet (420) til at rumme et målmateriale, og er i stand

til at modtage en partikelstråle (114) til at producere radionuklider fra målmaterialet, hvor fremgangsmåden omfatter:

at strømme et kølemiddel til en bagside af partikelstrålemålet (102, 200), hvor bagsiden er modstående en frontside af målet (102, 200), ved hvilken frontside partikelstrålen (114) modtages;

at opdele kølemidlet i en flerhed af kølemiddelinputstrømninger i en tilsvarende flerhed af riller (344) anbragt i bagsiden, hvor rillerne (344) løber i en transversal retning;

i hver rille (344) at splitte kølemiddelinputstrømningen i en første transversal strømningsvej (904) til kølemiddel rettet langs den transversale retning mod en første rilleende (652) og en anden transversal strømningsvej (906) til kølemiddel rettet langs en modstående transversal retning mod en anden rilleende (654);

i hver rille (344) at omlede kølemidlet i den første transversale strømningsvej (904) til kølemiddel ind i en perifer boring (656), og at omlede den anden transversale strømningsvej (906) til kølemiddel ind i en anden perifer boring (658), hvor hver perifer boring (656, 658) er en del af en flerhed af perifere boringer (656, 658), som løber fra en respektive første eller anden rilleende (652, 654) mod frontsiden, og hvor flerheden af perifere boringer (656, 658) omskriver målkaviteten (420), hvor kølemidlet strømmer fra hver første transversal strømningsvej (904) til kølemiddel og anden transversal strømningsvej (906) til kølemiddel ind i en tilsvarende lateral strømningsvej (912, 914) til kølemiddel rettet langs en lateral retning generelt vinkelret på den transversale retning;

at omlede kølemidlet i flerheden af perifere boringer (656, 658) ind i en flerhed af radiale udløbsboringer (224) anbragt ved en ende af de perifere boringer (656, 658) modsat flerheden af første rilleender (652) og anden rilleender (654), hvor kølemidlet strømmer fra hver lateral strømningsvej (912, 914) til kølemiddel ind i én af en flerhed af radiale strømningsveje (916) til kølemiddel, som løber gennem de respektive radiale udløbsboringer (224) langs en radial retning generelt vinkelret på den laterale retning og rettet væk fra målkaviteten (420); og,

medens kølemidlet strømmes gennem flerheden af første transversale strømningsveje (904) til kølemiddel, anden transversale strømningsveje (906) til kølemiddel, laterale strømningsveje (912, 914) til kølemiddel og radiale strømningsveje (916) til kølemiddel, at fjerne varme fra målmaterialet indeholdt i målkaviteten (420).

14. Fremgangsmåde ifølge krav 13, hvor den første rilleende (652) og den anden rilleende (654) i mindst én af flerheden af riller (344) hver er i fluid kommunikation med mere end én perifer boring (656, 658), og hvor, for den mindst ene rille (344), at omlede kølemidlet fra den første rilleende (652) og den anden rilleende (654) omfatter at opdele kølemidlet ind i hver perifer boring (656, 658), som er i kommunikation med den første rilleende (652) og den anden rilleende (654).

15. Fremgangsmåde ifølge krav 13 eller 14, hvor mindst to af de perifere boringer (656, 658) begge er i fluid kommunikation med den samme radiale udløbsboring (224), og

hvor, for de mindst to perifere boringer (656, 658), at omlede kølemidlet fra de perifere boringer (656, 658) omfatter at kombinere kølemidlet ind i den samme radiale udløbsboring (224).

DRAWINGS

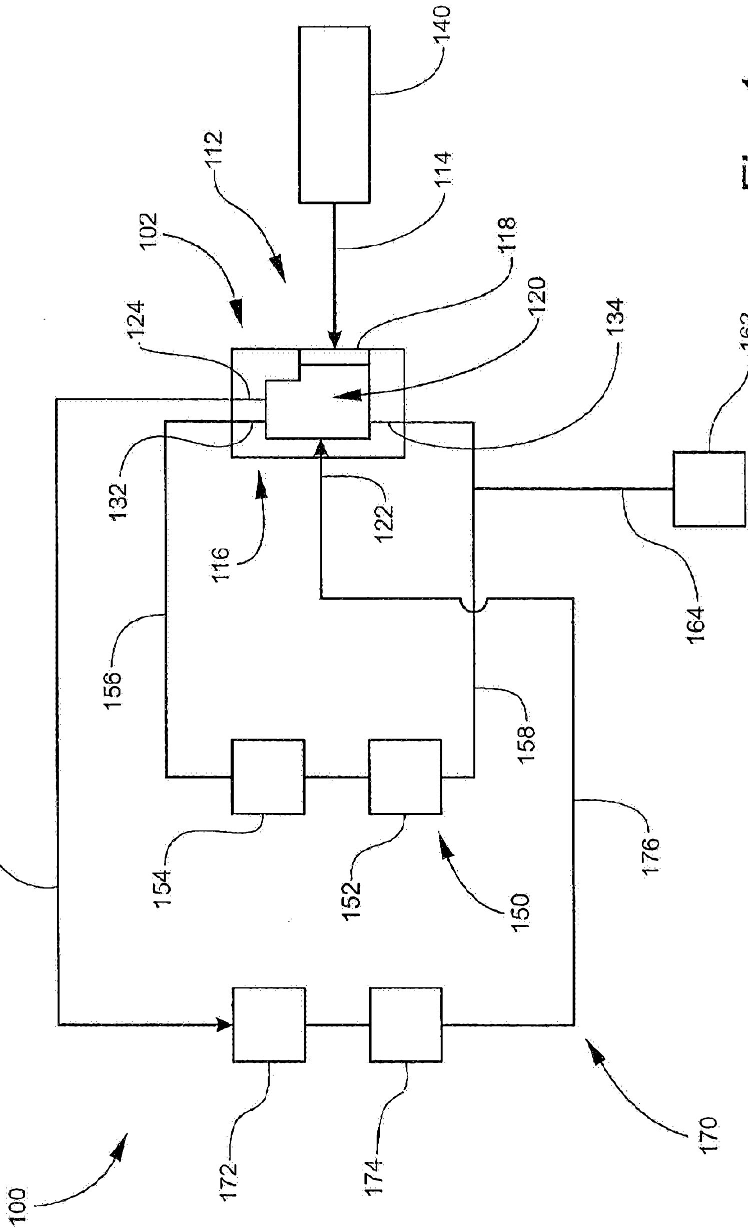

Fig. 1

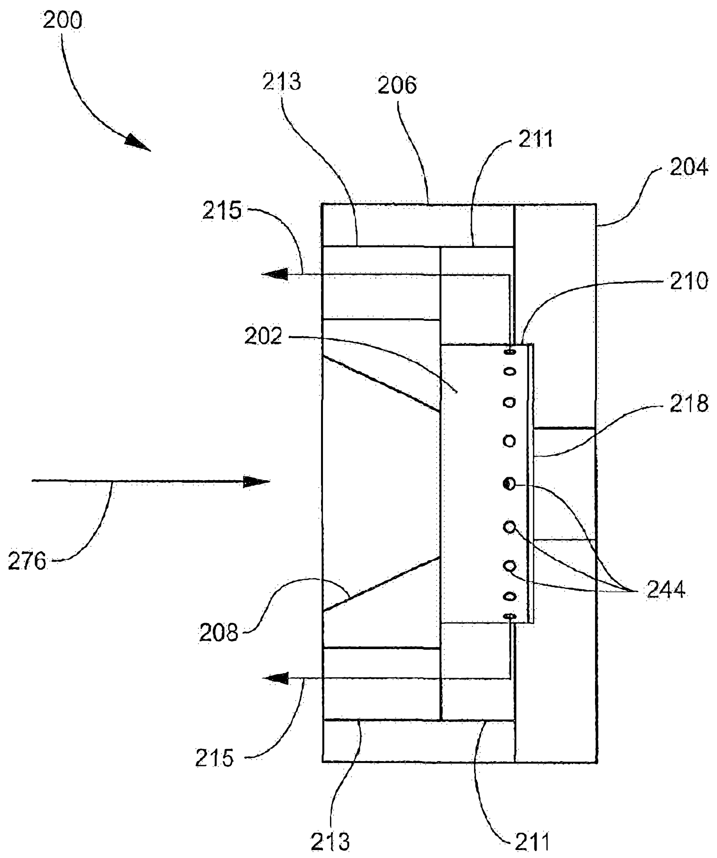

Fig. 2

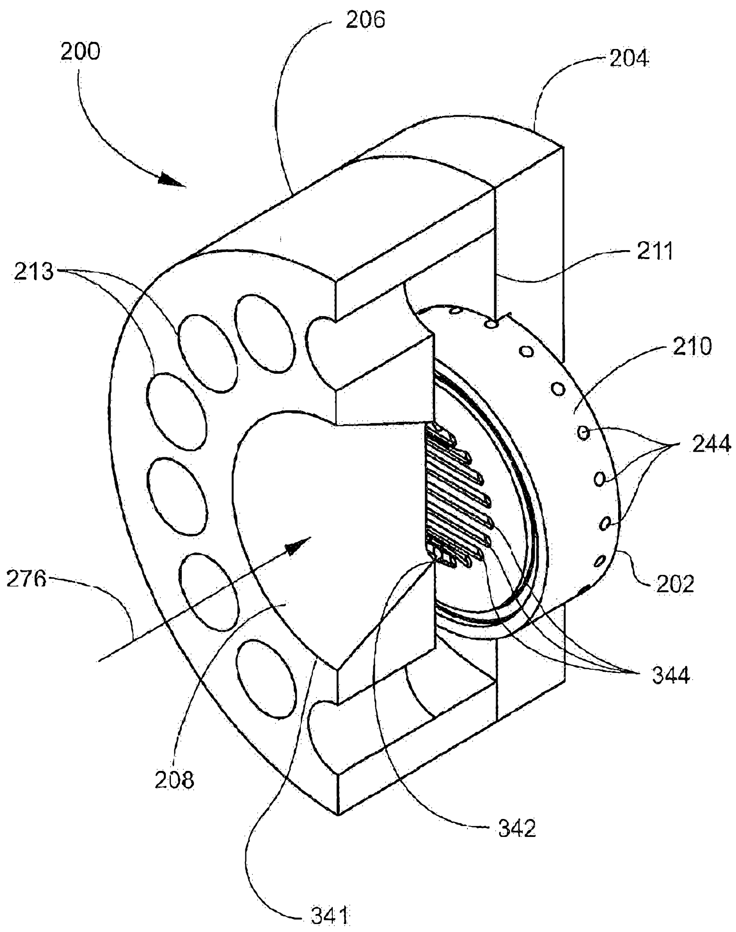

Fig. 3

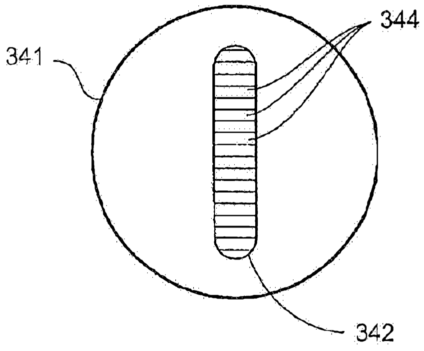

Fig. 3A

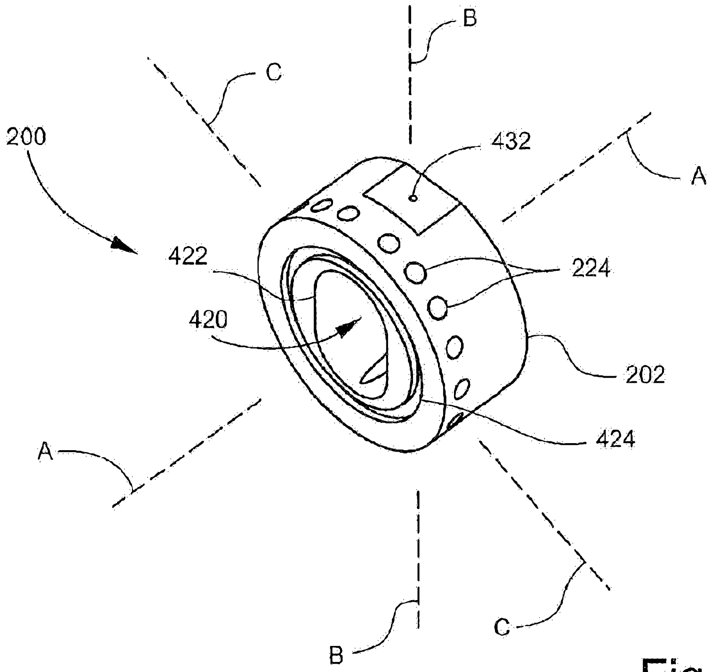

Fig. 4

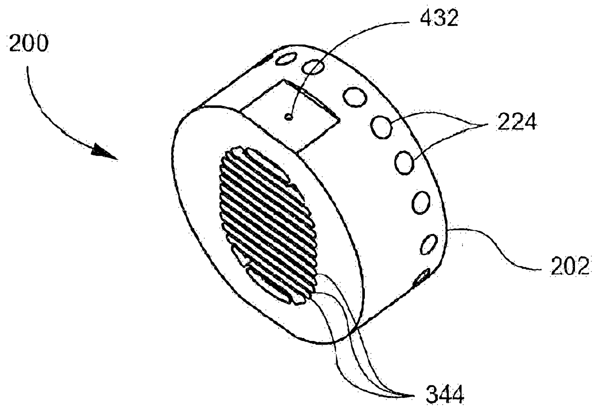

Fig. 5

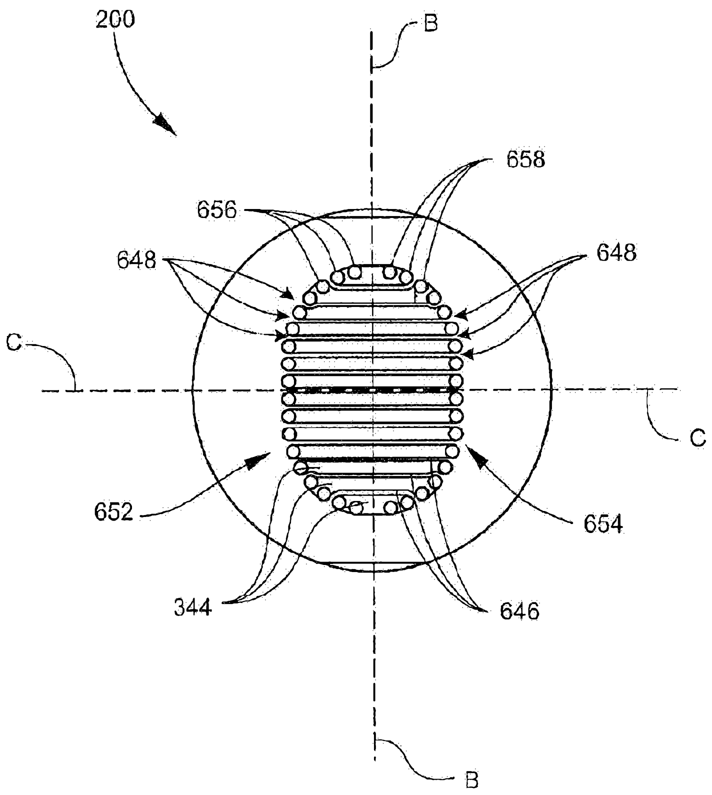

Fig. 6

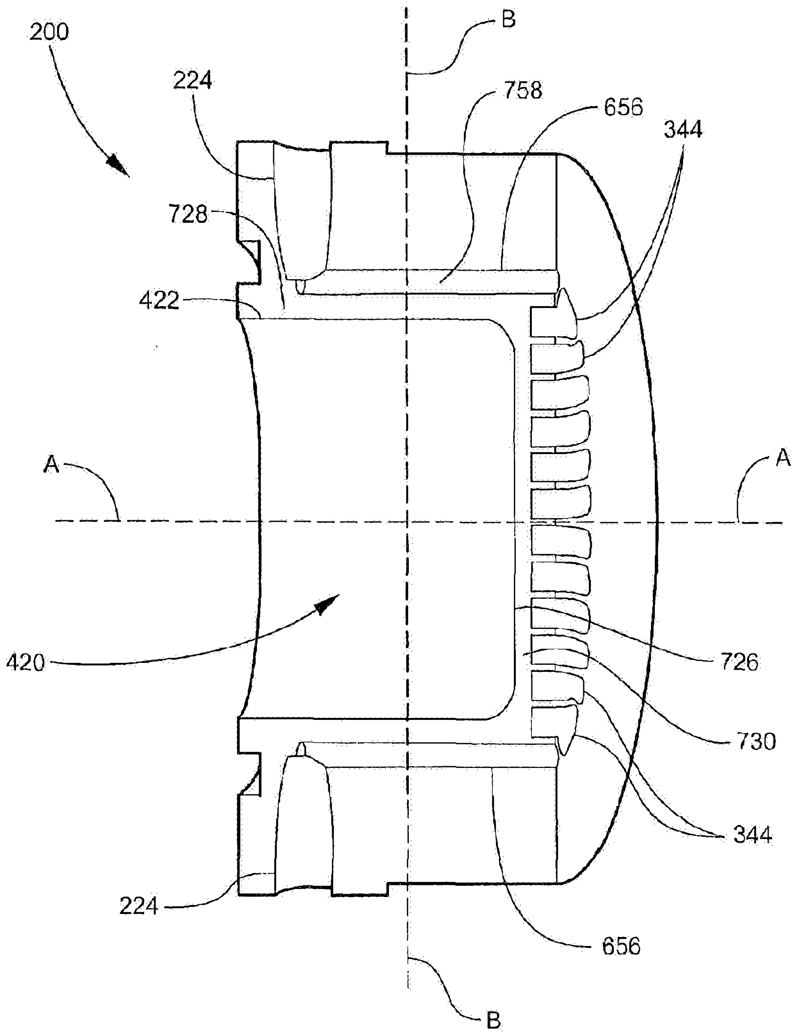

Fig. 7

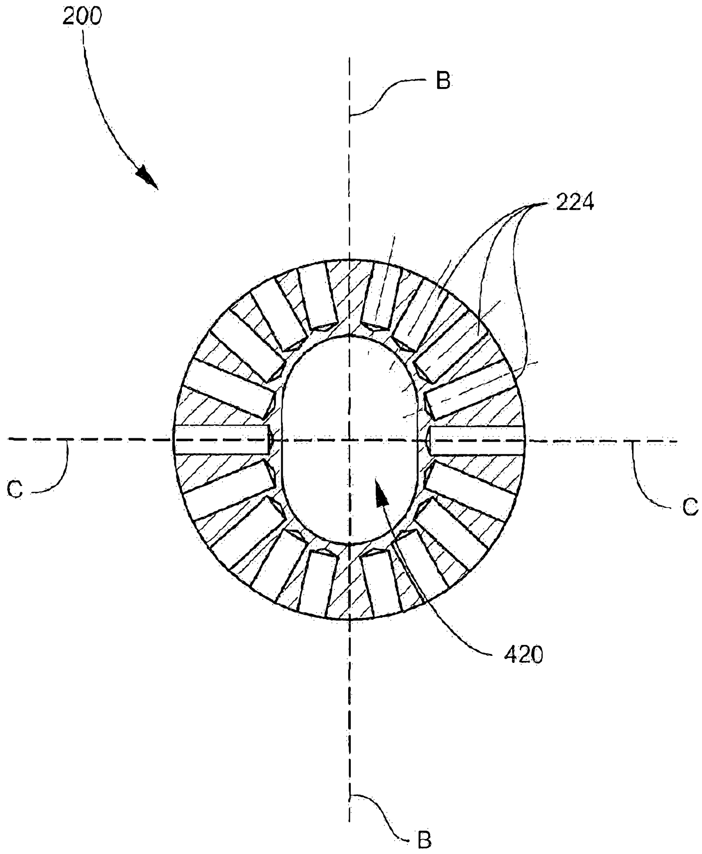

Fig. 8

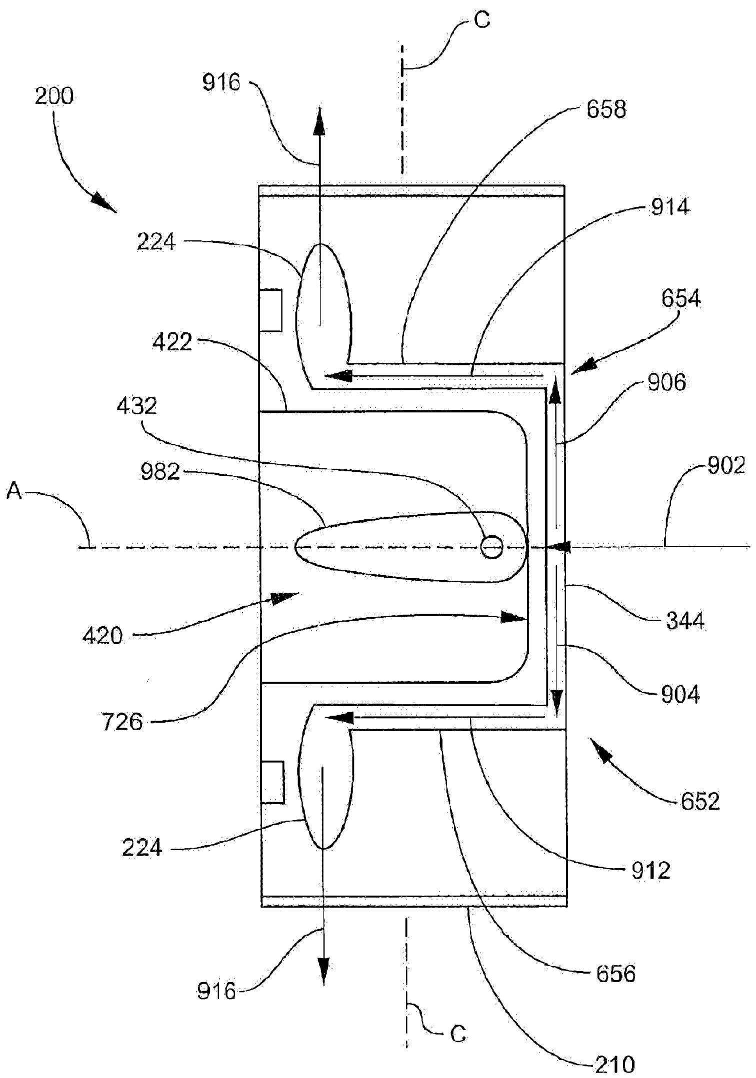
C
200
916
658
914
224
654
422
906
432
982
902
A
344
420
904
726
652
224
912
916
656
C
210

Fig. 9

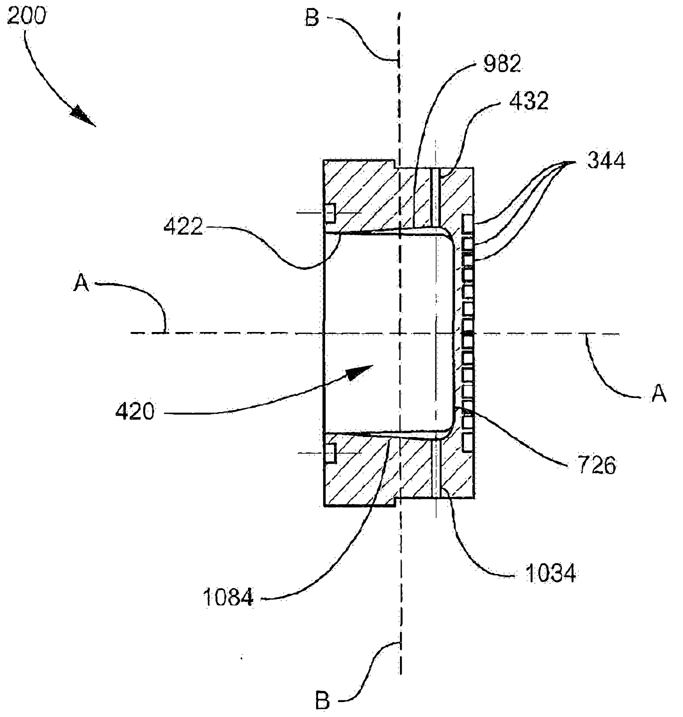

Fig. 10

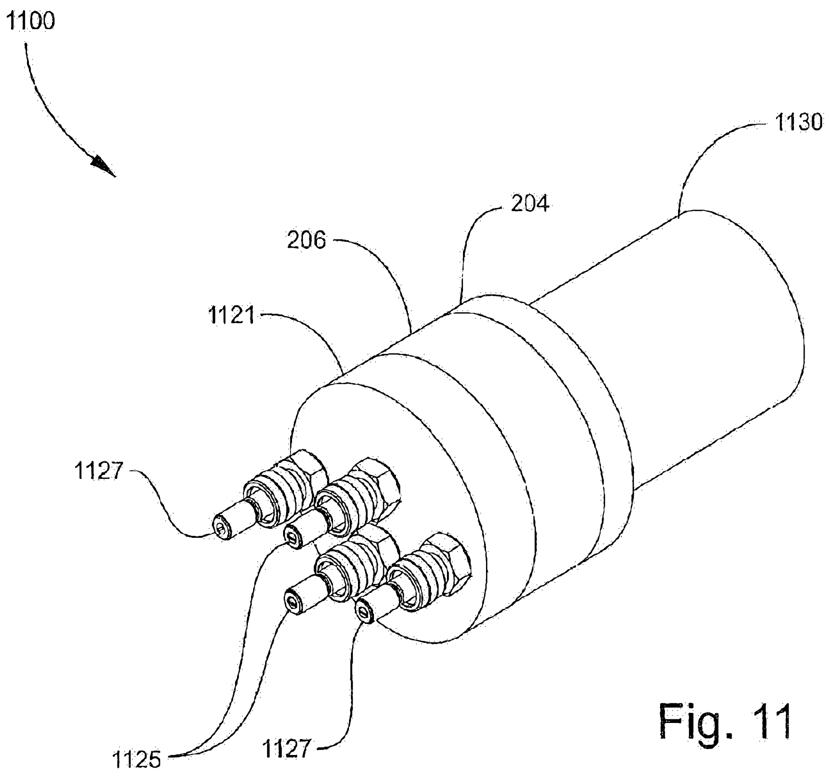

Fig. 11

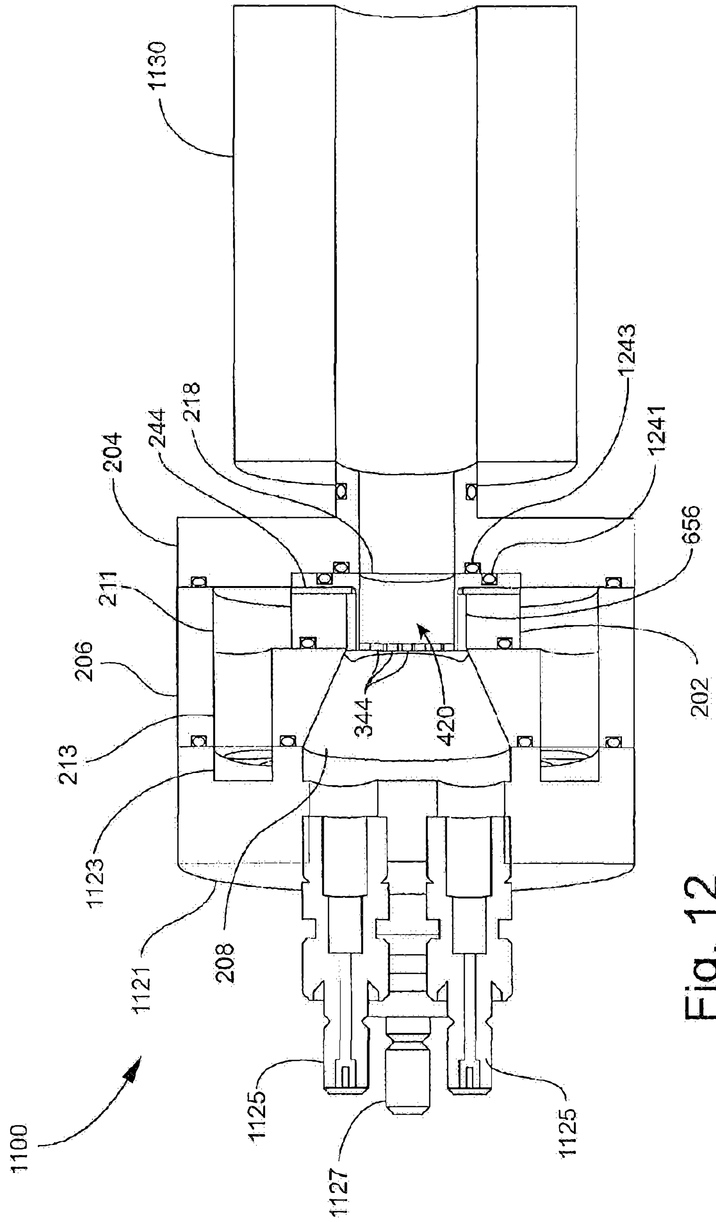
1130
204
244
218
1243
1241
656
211
206
202
213
344
420
1123
208
1121
1100
1125
1127
1125

Fig. 12

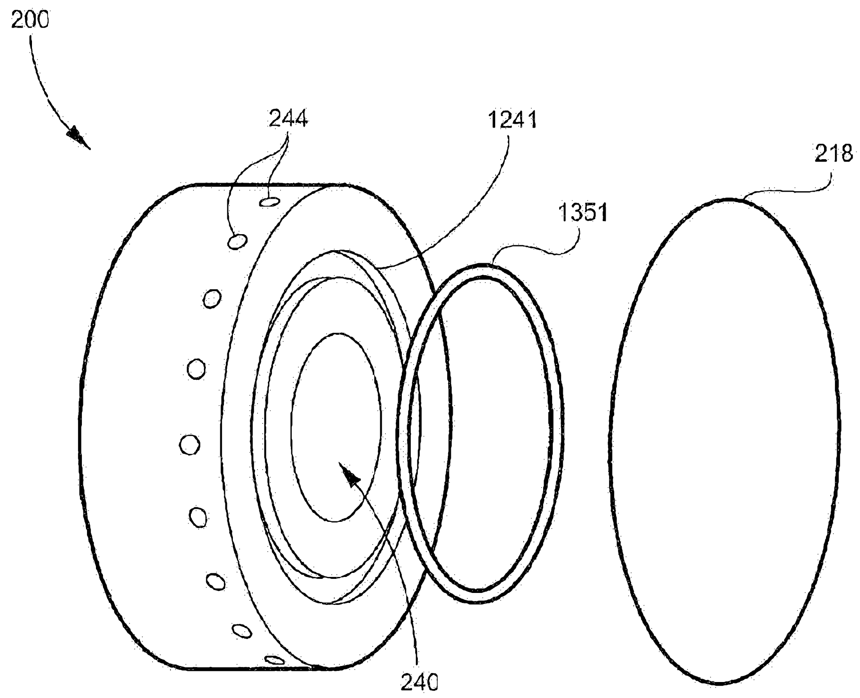

Fig. 13

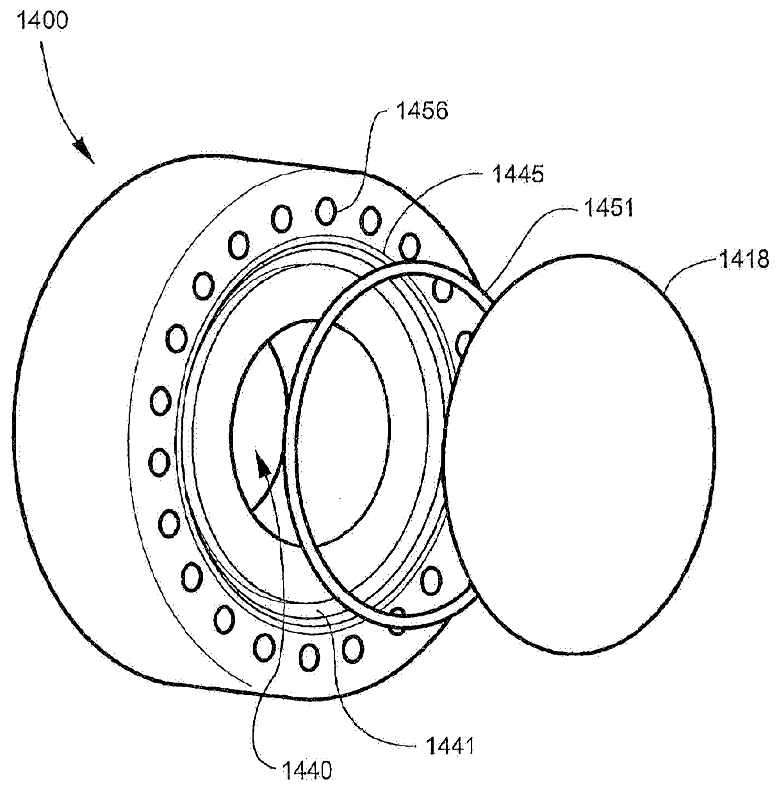

Fig. 14
(Prior Art)