

AUSTRALIA  
PATENTS ACT 1990  
PATENT REQUEST: STANDARD PATENT

653731

We, PALL CORPORATION, being the person identified below as the Applicant, request the grant of a patent to the person identified below as the Nominated Person, for an invention described in the accompanying standard complete specification.

Full application details follow.

Applicant: PALL CORPORATION

Address: 30 Sea Cliff Avenue, Glen Cove, New York 11542,  
United States of America

Nominated Person: As above

Address: As above

Invention Title: "METHOD AND DEVICE FOR REMOVING HEPARIN"

Name of actual inventor: Vlado I. Matkovich, Peter J. Degan,  
Thomas C. Gsell, Thomas Bormann and Isaac Rothman

BASIC CONVENTION APPLICATION(S) DETAILS:

Application Number: 07/552,138  
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Country Code: US  
Date of Application: 13th July, 1990

Address for service is:

SHELSTON WATERS  
55 Clarence Street  
SYDNEY NSW 2000

Attorney Code: SW

DATED this 9th Day of July, 1991  
PALL CORPORATION

by



Fellow Institute of Patent Attorneys of Australia  
of SHELSTON WATERS  
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To: The Commissioner of Patents  
WODEN ACT 2606

File: D.B. P-103  
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AUSTRALIA

PATENTS ACT 1990

NOTICE OF ENTITLEMENT

We, PALL CORPORATION of 2200 Northern Blvd., East Hills, New York 11548, United States of America, being the applicant in respect of Application No. 80320/91, state the following:-

1. The person nominated for the grant of the patent has entitlement from the actual inventors by assignment.
2. The person nominated for the grant of the patent has entitlement from the applicants of the basic application listed on the patent request form by assignment.
3. The basic application listed on the patent request form is the first application made in a Convention country in respect of the invention.

For and on behalf of  
PALL CORPORATION

*Gilbert P. Weiner*

(Signature)

*May 25, 1994*

(Date)

Name: Gilbert P. Weiner, Esq. ....  
Title: Vice President & General Counsel

File: 16118

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SHELSTON WATERS

55 CLARENCE STREET, SYDNEY, AUSTRALIA



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(54) Title  
METHOD AND DEVICE FOR REMOVING HEPARIN

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(71) Applicant(s)  
PALL CORPORATION

(72) Inventor(s)  
VLADO I. MATKOVICH; PETER J. DEGAN; THOMAS C. GSELL; THOMAS BORMANN; ISAAC ROTHMAN

(74) Attorney or Agent  
SHELSTON WATERS , 55 Clarence Street, SYDNEY NSW 2000

(56) Prior Art Documents  
US 3099600  
US 3337409  
US 4226599

(57) Claim

1. A method for removing heparin from blood or plasma comprising:  
contacting the blood or plasma with a porous medium having a positively charged surface; and removing heparin from the blood or plasma without substantial removal of blood clotting factors.

4. A porous medium for removing heparin from blood or plasma comprising a substrate and a superstrate, said substrate selected from the group consisting of polyolefins, polyesters, and polyamides, and at least one superstrate selected from the group consisting of

a) trimethyl ammonium ethyl acrylic chloride;

b) diethylamino ethyl methacrylate;

c) "a" and a polar, non-ionic, ethylenically unsaturated monomer;

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- d) "b" and a polar, non-ionic, ethylenically unsaturated monomer;
- e) "a" and diethylene glycol dimethacrylate; and
- f) "b" and methyl methacrylate;  
said medium having a positively charged surface and being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

7. A porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from diethylamino ethyl methacrylate thereon, said medium being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

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COMPLETE SPECIFICATION

FOR A STANDARD PATENT

ORIGINAL

Name of Applicant: PALL CORPORATION

Actual Inventors: Vlado I. Matkovich, Peter J. Degan, Thomas C. Gsell, Thomas Bormann and Isaac Rothman

Address for Service: SHELSTON WATERS  
55 Clarence Street  
SYDNEY NSW 2000

Invention Title: "METHOD AND DEVICE FOR REMOVING HEPARIN"

The following statement is a full description of this invention, including the best method of performing it known to us:-

METHOD AND DEVICE FOR REMOVING HEPARIN

This invention relates to a method and a device for removing heparin from a blood sample, particularly whole blood or blood plasma. This invention also relates to a method for rapidly deheparinizing blood in order to enable clinical diagnoses based on blood coagulation factors. The invention may also be used diagnostically to detect the presence of heparin.

10 Heparin and other natural and artificial acid polysaccharides or mucosaccharides are polyanions which exhibit anticoagulant properties, and are often used therapeutically to reduce or prevent coagulation of a patient's blood.

15 Blood coagulation or clotting is the precipitation of fibrin from blood or plasma, and depends, in part, on a complex cascade of plasma proteins (factors). Some of these blood coagulation factors are routinely used as an indicator of a patient's clinical condition or of a patient's response to therapeutic drugs.

20

The primary coagulation assays, prothrombin times (PT) and activated partial thromboplastin times (aPTT), measure the amount of time required for the formation of the first filament of fibrin. The presence of heparin, however, artificially increases the PT and aPTT, thus reducing the accuracy of the coagulation assays, thereby providing a false indication of the patient's clinical condition. It is, therefore, very desirable to determine the accurate coagulation parameters of a patient's blood independent of

therapeutic or incidental heparin levels. In order to do this, heparin in the sample of the patient's blood must be efficiently removed (or neutralized), before the coagulation parameters are assayed.

5 Practitioners routinely remove or identify heparin using methods such as protamine neutralization, resin absorption, or thrombin/reptilase times, but these methods may be time consuming, cumbersome, and expensive.

10 In protamine neutralization, for example, a precisely determined dosage of protamine sulfate (a low molecular weight fish polypeptide extract) is typically used. The dosage is generally calculated based on a ratio of one mg of protamine neutralizing 15 90 units of lung heparin or 115 units of intestinal heparin. In cardiothoracic surgery, for example, 150-300 mg of protamine may be required. Determining the proper dosage requires the utmost precision because protamine, and other neutralizing 20 agents such as polybrene, are soluble in plasma. Any excess neutralizing agent not combined with heparin will remain in the plasma and may interfere with the coagulation test.

Furthermore, the number and noxiousness of 25 protamine sulfate's side effects exacerbates the inherent risks associated with its use, and may contribute to a patient's morbidity and/or mortality. Common side effects include decreased peripheral vascular resistance, vasodilation, 30 hypotension, decreased cardiac output, dyspnea, increased or decreased pulmonary arterial resistance, decreased arterial PO<sub>2</sub>, bleeding, or complement activation (via- the heparin-protamine complex). In patients connected to an 35 extracorporeal circuit, the major adverse reactions

may include immediate anaphylactic shock (an antibody-mediated allergic reaction which is not dose-dependent) or a delayed response characterized by non-cardiogenic pulmonary edema or persistent 5 hypotension (which probably is dose dependent).

An alternative to protamine neutralization is the removal of heparin from the blood, typically by the addition of a heparin complexing agent. Two means for removing heparin from blood plasma are 10 available commercially. One, the Probe-Tek Heparin Adsorbent, manufactured by Probe-Tek, Inc., is a cationic modified cellulose which is supplied as a premeasured dose of heparin adsorbent in a tube, to which 1 ml blood plasma is added. After gently 15 mixing and standing for one minute, the plasma with the adsorbent is centrifuged at 1500 times the force of gravity for 10 minutes. The supernatant is then carefully removed from the tube with a pipette, and used for testing.

20 The second means, Hepasorb®, is manufactured by Organon Teknika Corporation and is a cellulose which has been modified to contain quaternary ammonium groups. Hepasorb (70 mg) is added to a test tube, and is agitated gently with 1 ml blood plasma for 25 about 10 seconds. It is cautioned that prolonged agitation can cause denaturation of the plasma proteins. After agitation the tube must be mixed slowly for 10 minutes at room temperature and centrifuged for 5 minutes at 12000 times the force 30 of gravity. The supernatant is then withdrawn from the centrifuge tube for testing.

All of these methods and products for removing heparin from a blood sample are difficult and time-consuming, require specialized equipment, require 35 about 20 minutes for even an experienced laboratory

worker to prepare a single sample of plasma for testing, require extreme care in the removal of the supernatant plasma after centrifuging to prevent contamination of the deheparinized plasma with adsorbent, and do not completely solve the need articulated by practitioners in the art.

For example, during surgery, the majority of deleterious reactions due to the presence of protamine occur immediately (i.e., they are not dose dependent). A filter for removing substantially all of the heparin typically used (about 15,000-30,000 units) would be most desirable, particularly if the filter could achieve a flow rate of about 2.5-6 liters/minute (for hemo-diluted patients) and have a priming volume of about 200-225 ml. Such a filter would eliminate the need for pre-operative testing to determine a patient's prior sensitization, would eliminate protamine's adverse side effects which may lead to morbidity and/or death, and would reduce time and costs associated with adverse protamine reactions.

It has been found that a porous medium having controlled surface properties can remove heparin from blood or plasma without removing therapeutically or clinically significant amounts of blood clotting factors. Porous media suitable for use according to the invention have a positive surface charge in aqueous solution. It has also been found that when the medium has been surface modified to provide a positive surface charge, it is possible to remove heparin from a blood sample, without removing a significant amount of blood clotting factors, simply by contacting the blood sample with the surface-modified medium. It has also been found that the required residence time is

typically very short (e.g. as little as fractions of a second), thus permitting the efficient removal or detection of heparin in a blood sample.

Furthermore, heparin can be removed from blood or  
5 plasma by contact with a medium of the present invention without the need for pre-filtration, or pretreatment with buffers or pH controllers. In this manner, heparin may be removed from a blood sample without adversely affecting subsequent  
10 testing of the blood sample for clotting time. Thus, the heparin-free sample may then be subjected to coagulation tests in order to determine true clotting time.

The present invention provides for a method for  
15 removing heparin from blood or plasma comprising contacting the blood or plasma with a porous medium having a positively charged surface; and removing heparin from the blood or plasma without substantial removal of blood clotting factors.

20 The present invention also provides for a method for returning the coagulation parameters of a heparin-containing blood or plasma sample to their accurate values comprising passing the sample through a porous medium comprising a substrate and a  
25 superstrate, said porous medium having a positive charge, thereby removing heparin from the sample.

The present invention further provides for a porous medium for removing heparin from blood or plasma without removing blood clotting factors comprising a substrate and a superstrate, said  
30 medium having a positively charged surface.

35 The present invention also provides for a filter assembly for removing heparin from blood or plasma comprising a housing having an inlet and an outlet and defining a fluid flow path; and at least

one porous medium positioned within the housing across the liquid flow path, said porous medium having a substrate and a superstrate and a positively charged surface.

5 The present invention also provides for a porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from trimethyl ammonium ethyl acrylic chloride thereon.

10 The present invention also provides for a porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from diethylamino ethyl methacrylate thereon.

15 The present invention also provides for a self-supporting porous medium comprising a substrate and a superstrate, wherein said substrate is polybutylene terephthalate and the superstrate has a positive charge and pendant quaternary ammonium groups derived from trimethyl ammonium ethyl acrylic chloride.

20 The present invention also provides for a self-supporting porous medium comprising a substrate and a superstrate, wherein said substrate is polybutylene terephthalate and the superstrate has a positive charge and pendant amine groups derived from diethylamino ethyl methacrylate.

25 The present invention also provides for a porous medium comprising a substrate and a superstrate, wherein the superstrate is derived from diethylamino ethyl methacrylate.

30 The present invention also provides for a porous medium comprising a substrate and a superstrate, wherein the superstrate is derived from trimethyl ammonium ethyl acrylic chloride.

The present invention also provides for a method for removing heparin from blood or plasma comprising contacting the blood or plasma with a porous medium having a positively charged surface; and removing a 5 therapeutically or clinically significant amount of heparin from the blood or plasma.

The present invention also provides for a filter assembly for removing heparin from blood or plasma comprising a housing having an inlet and an outlet and 10 defining a fluid flow path; and at least one porous medium positioned within the housing across the liquid flow path, said porous medium having a positively charged surface.

The present invention also provides for a filter 15 assembly which comprises a syringe; a housing removably attached to the syringe and having an inlet and an outlet and defining a fluid flow path; at least one porous medium positioned within the housing across the liquid flow path, said porous medium having a substrate 20 and a superstrate and a positively charged surface; and a cannula removably attached to the housing.

The present invention also provides for a filter assembly for removing heparin from blood in an extracorporeal circuit which comprises a housing having 25 an inlet and an outlet and defining a liquid flow path between the inlet and the outlet; at least one porous medium positioned within the housing across the liquid

flow path, said porous medium having a substrate and a superstrate and a positively charged surface.

According to a first aspect, the present invention consists in a method for removing heparin from 5 blood or plasma comprising:

contacting the blood or plasma with a porous medium having a positively charged surface; and

removing heparin from the blood or plasma without substantial removal of blood clotting factors.

10 According to a second aspect, the present invention consists in a method for allowing the coagulation parameters of a heparin-containing blood or plasma sample to be accurately determined without interference from therapeutic and incidental heparin 15 levels comprising passing the sample through a porous medium comprising a substrate and a superstrate, said porous medium having a positively charged surface and being capable of removing heparin from the sample without substantial removal of blood clotting factors.

20 According to a third aspect, the present invention consists in a porous medium for removing heparin from blood or plasma comprising a substrate and a superstrate, said substrate selected from the group consisting of polyolefins, polyesters, and polyamides, 25 and at least one superstrate selected from the group consisting of

a) trimethyl ammonium ethyl acrylic chloride;

- b) diethylamino ethyl methacrylate;
- c) "a" and a polar, non-ionic, ethylenically unsaturated monomer;
- d) "b" and a polar, non-ionic, ethylenically unsaturated monomer;
- 5 e) "a" and diethylene glycol dimethacrylate; and
- f) "b" and methyl methacrylate;

10 said medium having a positively charged surface and being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

According to a fourth aspect, the present invention consists in a porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from trimethyl ammonium ethyl acrylic chloride thereon, said medium being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

20 According to a fifth aspect, the present invention consists in a porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from diethylamino ethyl methacrylate thereon, said medium being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

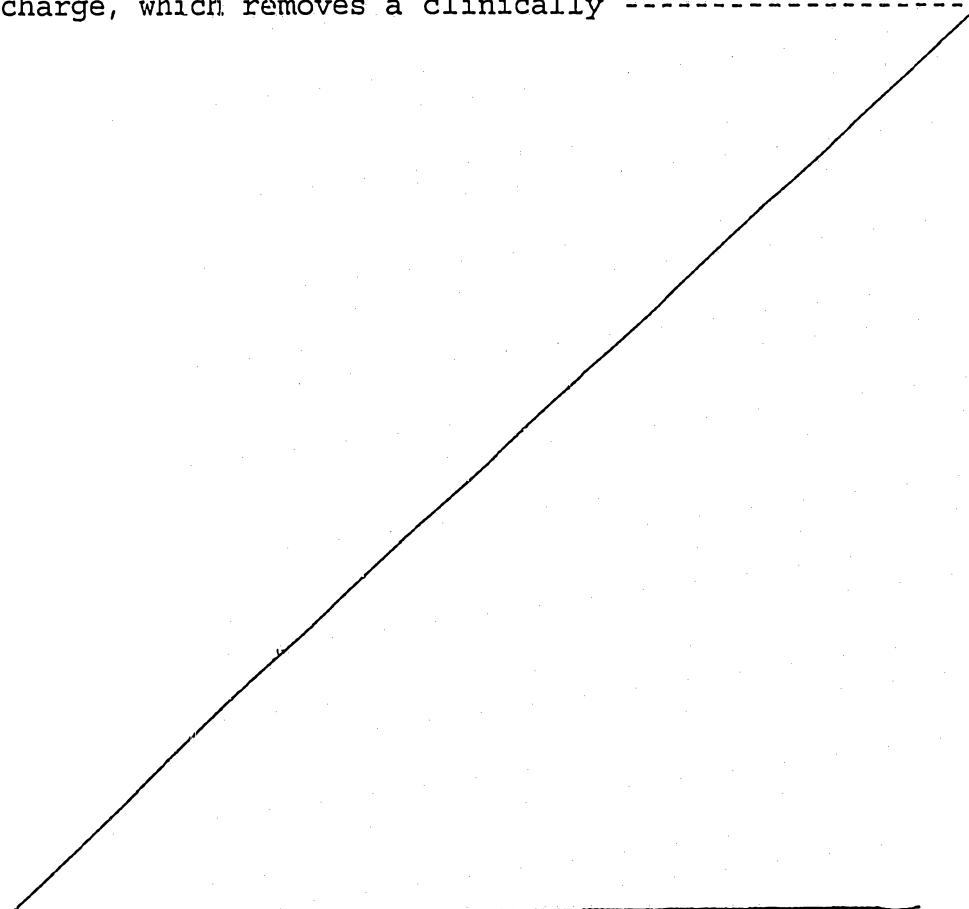
According to a sixth aspect, the present invention consists in a method for removing heparin from blood or plasma comprising:

5       contacting the blood or plasma with a porous medium having a positively charged surface and being capable of removing heparin without substantial removal of blood clotting factors; and

removing a therapeutically or clinically significant amount of heparin from the blood or plasma.

10      A porous medium in accordance with the invention comprises a porous medium having a positive surface charge, which removes a clinically -----

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significant amount of heparin from a heparin-containing liquid, such as blood, without removing other proteinaceous components from the liquid, wherein the positive surface charge preferably

5 comprises amino groups and/or quaternary ammonium groups on the surface of the porous medium. Porous medium, as used herein, refers to a self-supporting or non-self-supporting polymeric fibrous matrix, polymeric membrane, or a rigid porous medium. Self-

10 supporting, as used herein, refers to structures which have structural integrity, e.g., a fibrous matrix comprised of mechanically entangled fibers which maintains its unitary structure and its porous nature under intended conditions of use; that is,

15 the structure is resistant to compressive or deformation forces. Such structures are more readily produced, handled, and transported. Additionally, the likelihood of media migration, i.e., the undesirable sloughing off of small

20 particles of the medium which are then carried through the filter and into the downstream filtered product, is reduced with such self-supporting structures. Further, the self-supporting structures of the present invention substantially retain the

25 inherent adsorption characteristics of the medium with minimal increase in pressure drop across the structure, as compared to similar non-immobilized particles or non-self-supporting structures.

Heparin-containing liquid, as used herein, refers to

30 a fluid which contains heparin, such as blood or plasma. Blood, as used herein refers to whole blood; treated blood, such as blood diluted with a physiological solution; and one or more blood components, such as packed red cells. In an

35 embodiment of the invention, the porous medium is

self-supporting; in another embodiment of the invention, the porous medium may be either self-supporting or non-self-supporting and is disposed in a housing, such as a syringe or an extracorporeal filter.

As used herein, "without substantial removal of blood clotting factors" means that the porous medium of the invention remove heparin without removing other blood components which affect blood clotting, such as Factor IX, in amounts which adversely affect the accuracy of diagnostic tests, such as blood clotting tests. Porous media according to the present invention preferably exhibit a relatively low binding affinity for proteinaceous components of the blood. However, zero removal of proteinaceous blood components is not required. Also, the porous medium preferably should not cause any detectable blood hemolysis, although for the purposes of some diagnostic tests, a small degree of hemolysis may be tolerated without significantly affecting the test.

In accordance with an embodiment of the invention, a porous medium having a positive surface charge comprises amino and/or ammonium groups, particularly quaternary ammonium groups, on the surface of the medium in an amount sufficient to remove heparin from a blood sample. The presence of amino and/or ammonium groups on the surface of the medium provides the positive surface charge, and contributes to the production of a positive zeta potential on the surface of the medium. Typically, the positive surface charge is obtained by at least one ethylenically unsaturated monomer containing pendant amino and/or ammonium groups.

The amino and/or ammonium groups may be present

at the time of formation of the medium or they may be introduced after the medium is first formed.

In accordance with an embodiment of the invention, the porous medium may comprise a

5       substrate, surface-modified with a superstrate, for removing heparin from a blood sample. Substrate, as used herein, refers to a polymeric fiber (including hollow fibers), a polymeric fiber matrix, a polymeric membrane, or a solid porous medium.

10      Superstrate, as used herein, refers to a layer of polymer formed at and substantially covering the surface of the substrate. Substantially covering the surface, as used herein, refers to the amount required to form a porous medium which removes

15      heparin without removing blood clotting factors. A matrix, as the term is used herein, indicates a three-dimensional network of fibers, which together form a coherent self-supporting structure. The fibers themselves may be continuous, staple, or

20      melt-blown. The fibers may be made from any material compatible with blood and may be treated in a variety of ways to make the medium even more effective. Also, the fibers may be bonded, fused, or otherwise fixed to one another or they may simply

25      be mechanically entwined. A membrane, as the term is used herein, refers to one or more porous polymeric sheets, such as a woven or non-woven web of fibers, with or without a flexible porous substrate. The porous, polymeric sheet typically

30      has a substantially uniform, continuous matrix structure containing millions of very small capillary pores.

In an embodiment of the invention, the surface of the substrate may be modified to include a

35      polymer containing amino and/or ammonium groups,

particularly quaternary ammonium groups, and is suitable for use in removing a clinically significant portion of heparin in a heparin-containing liquid, such as blood, which is passed through the medium.

5 The substrate of this invention may be formed, for example, from any synthetic polymer capable of forming fibers and of serving as a substrate for grafting with ethylenically unsaturated monomeric  
10 materials. Preferably, the polymer should be capable of reacting with at least one ethylenically unsaturated monomer under the influence of ionizing radiation without the matrix being adversely affected by the radiation. Suitable polymers for  
15 use as the substrate include, but are not limited to, polyolefins, polyesters, polyamides, polysulfones, polyarylene oxides and sulfides, and polymers and copolymers made from halogenated olefins and unsaturated nitriles. Preferred  
20 polymers are polyolefins, polyesters, and polyamides. The most preferred polymer is polybutylene terephthalate (PBT). Preferred substrates may include ethylenically unsaturated monomers which yield an amino or ammonium group  
25 incorporated into the grafted polymer by means of a non-hydrolyzable linkage. This enables the product to better withstand certain environments, such as prolonged exposure to hot water and alkaline or acidic conditions, without substantial loss of the  
30 product's surface qualities. Further, the substrate may be configured into any geometric shape suitable for use as a porous medium, including but not limited to a web, a sheet, a solid body such as a disk or cylinder, or a hollow body such as a hollow  
35 cylinder; the porous medium may include additional

structures such as end caps, edge seals, a cage, a core, or a wrap. The medium preferably comprises a depth filter, which preferably comprises a mass of fibers, and more preferably, a mass of microfibers.

5        In accordance with an embodiment of the invention, the substrate may be treated or modified in order to form a substrate having a modifying agent or superstrate thereon. In accordance with an embodiment of the invention, the substrate may be

10      modified to form a superstrate comprising a polymer derived from at least one ethylenically unsaturated monomer containing pendant amino and/or ammonium groups, particularly quaternary ammonium groups. In a preferred embodiment, the medium is modified in

15      such a manner that the surface properties of the medium are controlled by the modifying agent such that the underlying structure does not adversely effect the blood sample's coagulation properties.

20      Examples of ethylenically unsaturated monomers containing pendant quaternary ammonium groups include but are not limited to polymerizable ethylenically unsaturated monomers which either contain an ammonium group or a functionality which is capable of being converted to an ammonium group.

25      For example, the monomer may contain primary, secondary or tertiary amino groups, and then any primary, secondary or tertiary amine groups in the grafted superstrate may be quaternized in situ. Suitable monomers include, but are not limited to

30      the quaternized derivatives of aminoalkyl acrylates and methacrylates, such as the methochlorides of dimethylaminoethyl acrylate or methacrylate; quaternized aminoalkyl acrylamides and methacrylamides, such as MAPTAC

35      (methacrylamidopropyltrimethylammonium chloride);

styernic compounds, such as the methochloride of dimethylaminostyrene; and vinylic compounds such as dimethyldiallylammonium chloride (DMDAC). If the monomer has pendant quaternary ammonium groups, the 5 most preferred monomer is trimethyl ammonium ethyl acrylic chloride (TMAEAC). If the monomer has pendant amino groups, the most preferred monomer is diethylamino ethyl methacrylate.

The presence of amino and/or quaternary 10 ammonium groups on the surface of the substrate provides the positive surface charge, and contributes to the production of a positive zeta potential on the surface of the substrate. Amino and/or quaternary ammonium groups may be present at 15 the time of formation of the superstrate or they may be introduced after the superstrate is first formed. Fiber-forming polymers tend to have strong negative zeta potentials. In addition, certain fiber forming processes, such as melt spinning or melt blowing, 20 create negatively charged functionalities (such as carboxyl groups) on the fiber surface. Such groups enhance the already strong negative zeta potential of the polymer. On the other hand, in a preferred embodiment, quaternary ammonium groups, because they 25 bear a full, permanent positive charge, neutralize and overcome the negative zeta potential of the substrate polymer surface. In another embodiment, unquaternized (free) primary, secondary or tertiary amino groups are capable of being protonated in 30 aqueous systems and bear a positive charge. The amount of positive charge may be sufficient to overcome the strong negative potential of some polymeric fiber materials, and thus, may be capable of removing heparin.

35 In an embodiment of the invention, the

superstrate may also include at least one other monomer in combination with the amino and/or ammonium group-containing monomer. These other monomers may be completely inert or may contain

5 functional groups which confer additional desired properties or exercise control over the surface properties already conferred by the amino or ammonium group-containing monomers, provided that the additional monomers do not also contain

10 functional groups which interfere with the formation of the grafted porous medium. Suitable monomers include polar, non-ionic, ethylenically unsaturated monomers. The polar monomer may promote hydrogen-bonding, may contain more than one polymerizable

15 ethylenically unsaturated group, and/or may impart hydrophilicity to the porous medium. When such monomers are incorporated into the grafted superstrate, the superstrate may become cross-linked. A cross-linked superstrate is more

20 resistant to change in its molecular conformation and, as a result, provides a fiber matrix whose surface properties are less affected by the chemical environment or heat. Certain monomers which contain both conjugated and non-conjugated polymerizable

25 double bond systems, such as allyl methacrylate (AMA), are particularly effective. These appear to increase the efficiency of grafting the superstrate to the substrate surfaces. The presence of monomers which have more than one polymerizable ethylenically

30 unsaturated group can be beneficial in another respect. For unknown reasons, the treatment of large, non-uniform shaped fiber matrices sometimes results in a matrix in which the surfaces are not treated uniformly; non-uniform treatment may result

35 in local variation in filtration capabilities within

the porous medium.

Such polar, non-ionic monomers include but are not limited to, polymethacrylate and polyacrylate esters of polyols, such as diethylene glycol

- 5 dimethacrylate (DEGDMA) and pentaerithritol triacrylate; acrylate and methacrylate esters of ethylenically unsaturated alcohols, such as AMA; hydroxyl-containing monomers including hydroxylalkyl acrylates, such as hydroxypropyl acrylate (HPA) and
- 10 methacrylates, such as hydroxyethyl methacrylate (HEMA); and materials such as triallyl trimellitate, divinylbenzene and other small monomers having more than one polymerizable ethylenically unsaturated functional group. If the positive surface charge is
- 15 provided by a monomer containing pendant ammonium groups, the most preferred non-ionic monomer is diethylene glycol dimethacrylate (DEGDMA). If the positive surface charge is provided by a monomer containing pendant amino groups, the most preferred
- 20 non-ionic monomer is methyl methacrylate. The inclusion of a monomer having a hydrophobic moiety, such as methyl methacrylate, may also be used to obtain precise control over the final hydrophilicity of the matrix by modifying the effect of monomers conferring hydrophilic characteristics.
- 25

In accordance with an embodiment of the invention, porous media of the invention can be produced from a pre-existing substrate by a process comprising the graft polymerization of the superstrate onto the surface of the substrate.

30 Alternatively, in an embodiment of the invention, the superstrate may be grafted onto the surface of individual fibers prior to the fibers being formed into a matrix, membrane, or rigid porous medium.

35 A porous medium of this invention is preferably

formed by contacting a substrate, either as a pre-existing matrix or as individual fibers prior to their formation into the matrix, with a grafting solution comprising the superstrate in a suitable solvent, and exposing the substrate to ionizing radiation under conditions which polymerize the superstrate and result in a filter medium having the desired surface properties. The monomers in the grafting solution preferably form a polymer bonded to the surface of the substrate fibers or fiber matrix. The term bonded, as used herein, refers to the superstrate being sufficiently attached to the substrate or to each other so that the superstrate will not significantly extract under the intended conditions of use.

When the superstrate comprises an amino and/or ammonium group-containing monomer in conjunction with a polar, hydrogen-bonding, non-ionic, polymerizable, ethylenically unsaturated monomer, the amino and/or ammonium group-containing monomer may be present in the grafting solution in an amount typically ranging from 0.1% to 10% by weight, and more preferably between 0.20% and 7% by weight. The more amenable the fibers of the matrix are to graft polymerization, the lower the concentration of monomer required to achieve the desired effect. Most preferred are monomer concentrations ranging from 0.3% to 5% by weight. The polar, hydrogen-bonding, non-ionic, polymerizable ethylenically unsaturated monomer may be present in an amount ranging from 0.1% to 10% by weight, more preferably from 0.25% to 5% by weight, and especially preferred are concentrations ranging from 0.3% to 2% by weight.

In accordance with the invention, however, it

is only required that the grafted superstrate contain sufficient amino and/or quaternary ammonium groups to overcome the negative potential inherent at the substrate surface.

5 To form the grafting solution, the monomer(s) may be dissolved in any solvent or combination of solvents which is capable of dissolving all of the monomer(s) and which does not interfere with the formation of the polymer. For example, when amino 10 or quaternary ammonium group-containing monomers are used together with HEMA and AMA, the preferred solvent is water. However, if monomers are used which are not fully soluble in water, an amount of a water-miscible inert organic solvent, such as 2- 15 methylpropan-2-ol or a mixture of 75% deionized water and 25% tertiary butyl alcohol, may be added in an amount sufficient to enable complete dissolution of the monomers. Some nonaqueous solvents, however, may decrease the solubility of 20 some quaternary ammonium group-containing monomers. Hence, non-aqueous solvents should not be added in an amount that renders the ammonium group-containing monomer insoluble.

25 The substrate, in the form of individual fibers, porous matrix, membrane, or shaped article, may be contacted with the coating solution by any appropriate means, including, but not limited to spraying, dipping, or vacuum impregnation. The amount of contact is preferably sufficient to 30 substantially completely, and more preferably, to completely coat the surface of the substrate. If a large enough portion of the substrate is left uncovered, the porous medium may remove blood components (particularly Factor IX) in quantities 35 that might effect the accuracy of a diagnostic blood

clotting test, and therefore, may, under some circumstances, be undesirable.

If the substrate is easily wetted by the coating solution, it should be sufficient to pass 5 the substrate through a bath of the coating solution. If the substrate is not easily wetted by the coating solution, mechanical means may be used to force the solution onto the fibers. For example, the fibers may be placed on a vacuum drum which will 10 draw the coating solution onto the fibers.

Alternatively, the substrate may be placed in a container which is then sealed, evacuated, and then filled with superstrate solution. If this method is used, the superstrate solution should preferably be 15 thoroughly degassed prior to being placed in the container.

Once the surface area of the substrate is saturated and preferably placed in contact with an excess amount of coating solution, the substrate is 20 exposed to ionizing radiation. Gamma radiation is preferred, and gamma radiation from a  $^{60}\text{Co}$  Cobalt source is most preferred, although other sources of ionizing radiation may be used, provided that the radiation is capable of initiating graft. 25 polymerization. Irradiation at any dose rate is acceptable, provided that the rate enables formation of a modified substrate having the desired surface properties. Dose rates from 1 to 1,000 kilorads/hr and preferably from 5 to 100 kilorads/hr may be 30 used. In general, higher dose rates may be typically required for substrates which appear to react poorly with the ammonium or amino group-containing monomer when no other comonomers are present. A dose rate of about 10 kilorads/hr for a 35 total dose of about 0.2 Mrads is especially

preferred for forming a superstrate from DMDAC, HEMA, and AMA on a PBT fiber matrix. Typically, total doses in the range of from 0.05 to 5 Megarads may be used.

5 After irradiation and formation of the positive charge on the surface of the substrate, the surface-modified substrate may be washed with water to remove any polymeric debris which is not bonded to the substrate. Any means of washing which causes water to flow across all the fibers, either loose or in a matrix, is appropriate, provided that it is sufficient to remove all of the unbound debris. For example, washing a fiber matrix is typically conducted by flowing deionized water through the

10 matrix for about 5 hours at a flow rate of about 0.47 liters (1/8 gallon) per minute (lpm) for each 645 square centimeters (100 square inches) of external surface area.

15 After washing, the surface-modified porous medium is dewatered and/or dried. Insufficient drying may result in the porous medium removing blood components other than heparin. Over-drying may cause embrittlement or other detrimental affects to the modified substrate. Typically, the porous medium may be dried at 100°C to 120°C for between 24 hours and 72 hours. In a preferred embodiment, the porous medium is dried at about 100°C for about 72 hours.

20 While not intending to be restricted to a certain theory, it is believed that the porous medium in accordance with the present invention removes heparin from a heparin-containing liquid by means of adsorption rather than by mechanical removal. Consequently, the total surface area of 25 the porous media may be selected to optimize the

properties of the device, depending on the specific application. As used herein, the term total surface refers not only to the gross or external surface(s) of the medium, but also to the internal surfaces of 5 the medium which are contacted by fluid during use.

Typically, the porous media useful in the subject invention will have a total surface area ranging from  $0.01 \text{ M}^2/\text{g}$  to  $20 \text{ M}^2/\text{g}$ , preferably from  $0.2 \text{ M}^2/\text{g}$  to  $10 \text{ M}^2/\text{g}$ .

10 Because of the efficiency of a porous medium used as heparin adsorbent, only a small amount of the medium need be used. Therefore, the percent voids of the adsorbent may be as small as a few microliters to ensure that no significant amount of 15 liquid is wasted by being held up in the adsorbent. Typically, the percent voids may be in the range from 50% to 95%.

Also because of the efficiency of porous media according to the present invention, the required 20 average residence time of the fluid sample in the void space of a porous medium is minimal. Typically, the residence time may be in the range from .1 second to 50 seconds.

In accordance with a preferred embodiment of 25 the invention, a blood sample is drawn into a syringe and forced by hand pressure through a modified matrix structure capable of adsorbing heparin, thereby removing the heparin from the plasma, if present. Preferably, about 1 ml plasma 30 is forced through the modified matrix secured in a filter holder (device) for 1 to 50 seconds preferably from 1 to 10 seconds. Typically, the porous medium of the present invention removes from about 1 to about 4 units of heparin for about every 35 2.54 square centimeters (1 square inch) of media.

The heparin-free plasma can be collected in a tube or vial for storage or can be expelled directly into cells or cuvettes commonly used in laboratory device for determining coagulation parameters.

- 5        Porous media in accordance with the invention may be configured in a device which can be attached to the end of a syringe. The liquid can then be expelled through the adsorbent into a suitable collection tube, thereby producing a heparin-free liquid.
- 10      Alternatively, the absorbing medium can be configured in a device such that it can first be attached to a syringe. The free end of the device can be inserted into a liquid sample, and the liquid can be withdrawn through the absorbing medium into the syringe, thereby removing any heparin from the liquid.
- 15      The device can then be removed from the end of the syringe and the deheparinized liquid can be expelled into a suitable collection tube. In a third embodiment, the absorbing medium can be
- 20      configured in a device such that the device can be attached to the end of a syringe, the free end of the device can be immersed in a liquid sample and liquid can be withdrawn into the syringe through a check valve in the device, thereby bypassing the absorbing medium, and then be expelled through the absorbing medium into a suitable collection tube.
- 25      In a fourth embodiment the device may be configured to be attached to the end of a syringe and immersed in a liquid sample. The liquid can then be withdrawn into the syringe through the absorbing medium and then be expelled using the syringe, bypassing the absorbing medium via a check valve, directly into a suitable collection tube. In a fifth embodiment, the porous medium may be
- 30      incorporated into an extracorporeal circuit in, for
- 35

example, an extracorporeal filter or dialysis filter.

For example, a typical syringe filter assembly may comprise a barrel syringe, a filter in

- 5 accordance with the invention removably attached to one end of the syringe, and a "snorkel" or tip removably attached to the filter. The filter typically comprises a porous medium according to the invention in the form of a disc membrane encased
- 10 within a housing having first and second fittings on opposite sides of the disc. The first fitting may be removably attached to the syringe, and the second fitting may be removably attached to the snorkel. The snorkel may comprise a flexible, semi-rigid or
- 15 rigid cannula-like structure which is of a specific length so as to allow access to plasma in a standard vacutainer tube without allowing red cells to be drawn into the syringe. Typically, withdrawing the plunger of the syringe draws plasma sequentially
- 20 into the snorkel, through the filter, and into the syringe. The surface area of the filter is large enough to allow plasma to flow easily through the filter with only the delta-p across the filter generated by a reasonably steady withdrawal of the
- 25 plunger. A typical diameter of the membrane is about 2.54 centimeters (one inch). The snorkel and filter may then be discarded, and the filtered plasma in the syringe may be dispensed into a tube.

- 30 A typical filter assembly for use in an extracorporeal circuit comprises a housing, having an inlet and an outlet, and a porous medium according to the invention disposed in the housing for the removal of heparin from the blood sample. The porous medium may have a disc-like or cylindrical
- 35 shape and may be packed in the housing to contact

liquid flowing longitudinally or axially through the filter element. Any housing of suitable shape to provide an inlet and an outlet for a liquid and a space for a porous medium disposed between the inlet and outlet can be employed. Housings can be designed in a variety of shapes. For example, a square or octagon shaped housing and other possible forms designed to accommodate a porous medium would in principle all be functional. These shapes are 5 within the scope of the claimed invention.

10

General Procedure for Measuring Zeta Potential

Zeta potential was measured using a 1.27 cm. ( $\frac{1}{2}$  inch) diameter x 0.64 cm. ( $\frac{1}{4}$  inch) thick cylindrical plug of fiber matrix, cut from the innermost 1.27 15 cm. ( $\frac{1}{2}$  inch) of a filter medium (nearest the core of the filter), or if a fibrous web, the sample was cut from a 1.27 cm. ( $\frac{1}{2}$  inch) thick stack of webs.

The zeta potential was measured by placing the sample in an acrylic filter holder which held the 20 sample snugly between two platinum wire screens 100 x 100 mesh (i.e., 100 wires in each direction per 2.54 cm. (1 inch)). The meshes were connected, using copper wire, to the terminals of a Triplett Corporation model 3360 Volt-Ohm Meter, the mesh on the upstream side for the sample being connected to the positive terminal of the meter. A pH-buffered 25 solution was passed through the sample using a differential pressure of 114.3 cm. (45 inches) of water column across the filter holder and the effluent was collected. For measurements at pH 7, a 30 buffered solution was made by adding 6 ml pH buffer (Fisher Scientific Co. catalog number SB108-500) and 5 ml pH 7.4 buffer (Fisher Scientific Co. catalog number SB110-500) to 1 liter pyrogen-free deionized

water. For measurements at pH 9, a buffered solution was made by adding 6 ml pH 7 buffer (Fisher Scientific Co. catalog number SB114-500) and 2 ml pH 10 buffer (Fisher Scientific Co. catalog number

5 SB116-500) to 1 liter pyrogen-free deionized water. The electrical potential across the filter holder was measured during flow (it required about 30 seconds of flow for the potential to stabilize) and was corrected for cell polarization by subtracting

10 from it the electrical potential measured when flow was stopped. During the period of flow the pH of the liquid was measured using a Cole-Parmer model J-5994-10 pH meter fitted with an in-line model J-5993-90 pH probe. The conductivity of the liquid

15 was measured using a Cole-Parmer model J-1481-60 conductivity meter fitted with a model J-1481-66 conductivity flow cell. Then the polarity of the volt meter was reversed, and the effluent was flowed backwards through the filter holder using a

20 differential pressure of 114.3 cm. (45 inches) of water column. As in the first instance the electrical potential measured during flow was corrected for cell polarization by subtracting from it the electrical potential measured after flow was stopped. The average of the two corrected potential

25 was taken as the streaming potential.

The zeta potential of the fiber matrix was derived from the streaming potential using the following relationship (J. T. Davis et al.,

30 Interfacial Phenomena, Academic Press, New York, 1963):

$$\text{Zeta Potential} = \frac{4 \pi \eta}{D} \frac{E_s \lambda}{P}$$

where  $\eta$  is the viscosity of the flowing solution,  $D$  is its dielectric constant,  $\lambda$  is its conductivity,  $E_s$

is the streaming potential and  $P$  is the pressure drop across the sample during the period of flow. In these tests the quantity  $4 \pi \eta / DP$  was equal to 0.800.

5       Porous media in accordance with this invention have positive zeta potentials in aqueous solution at approximately neutral pH. Preferably, they have a positive zeta potential under mildly alkaline conditions, for example, at a pH as high as 9.

10      The preparation and evaluation of substrates having surface properties controlled by a superstrate imparting a positive charge to the surface of the substrate is described in the Examples below.

15      While the invention is susceptible to various modifications and alternative forms, certain specific embodiments thereof are described in the examples set forth below. It should be understood, however, that these examples are not intended to limit the invention to the particular embodiments disclosed, but, on the contrary, the intention is to cover all modifications, equivalents, and alternatives falling within the spirit and scope of the invention.

20      In order that the invention herein described may be more fully understood, the following examples are for illustrative purposes only and are not to be construed as limiting this invention in any manner.

25

General Procedure for Measuring Surface Area

30      Measurement of fiber surface area, for example by gas (nitrogen) adsorption -- popularly referred to as "BET" measurement -- is a useful technique, as the surface area is a direct indication of the extent of fiber surface available to remove heparin.

The surface area of melt blown PBT webs can be used to calculate average fiber diameter:

$$\text{Total volume of fiber in 1 gram} = \frac{1}{1.38} \text{ cc}$$

5 (where 1.38 = fiber density of PBT, g/cc)

$$\text{hence } \frac{\pi d^2 L}{4} = \frac{1}{1.38} \quad (1)$$

$$\text{Area of the fiber is } \pi d L = A_f \quad (2)$$

$$10 \text{Dividing (1) by (2), } \frac{d}{4} = \frac{1}{1.38 A_f}$$

$$\text{and } d = \frac{4}{1.38 A_f} = \frac{2.9}{A_f} \text{, or } (0.345 A_f)^{-1}$$

15 where L = total length of fiber per gram, d = average fiber diameter in centimeters, and  $A_f$  = fiber surface area in  $\text{cm}^2/\text{g}$ . If the units of d are micrometers, the units of  $A_f$  become  $\text{M}^2/\text{g}$  (square meters/gram), which will be used hereinafter.

#### General Procedure for Determining BSA

20 The Bovine Serum Albumin (BSA) protein absorption test is performed according to a standardized procedure. In this procedure, a solution containing 0.1 mg/ml unlabelled BSA and about  $10^5 \text{ cpm/ml}$   $^{125}\text{I}$ -labelled BSA was prepared in a phosphate buffered saline (PBS) solution having a pH 25 of 7.2. The PBS solution contained 0.2 grams per liter of monobasic sodium phosphate, 1.2 grams per liter of anhydrous, dibasic sodium phosphate, and 8.77 grams per liter sodium chloride in deionized water.

30 A sample of a porous test medium was placed in a syringe-type filter holder. Fluid communication

between a reservoir holding the BSA test solution and the syringe-type filter was provided by a length of Tygon™ tubing and a peristaltic pump arranged in series. Prior to insertion of a porous test medium 5 sample into the filter holder, the potential non-specific protein binding sites on both the tubing and the filter holder were blocked by recirculating 1.0 ml of the BSA solution through the tubing and filter holder at a flow rate of 0.3 ml/min for a 10 period of 15 minutes. Following recirculation, the BSA solution was drained from the tubing and filter holder. Residual BSA solution was removed from the tubing and filter holder by circulating about 2.0 ml of PBS through the tubing and filter holder at a 15 flow rate of about 0.3 ml/min for several minutes at ambient temperature.

A 1.3 mm diameter disc of porous polymeric test medium was placed into the blocked filter holder. The  $^{125}\text{I}$ -BSA solution was then transferred from the 20 reservoir to the filter holder at a flow rate of 0.8 ml/min/cm<sup>2</sup>. The test was continued for a period of 5 minutes, during which time 391 micrograms/cm<sup>2</sup> of BSA were transferred to the filter holder. The test medium was then removed from the filter holder and 25 blotted dry on filter paper. The amount of protein (BSA) adsorbed by the membrane disc was determined by radioactive counting in a gamma counter.

#### General Procedure for Determining CWST

Although the media according to the invention 30 may remain untreated, they are preferably treated to make them even more effective for removing heparin. For example, a medium may be surface modified to increase the critical wetting surface tension (CWST) of the medium. As disclosed in U.S. Patent No.

4,880,548, the CWST of a porous medium may be determined by individually applying to its surface a series of liquids with surface tensions varying by 2 to 4 dynes/cm and observing the absorption or non-absorption of each liquid over time. The CWST of a porous medium, in units of dynes/cm, is defined as the mean value of the surface tension of the liquid which is absorbed and that of the liquid of neighboring surface tension which is not absorbed within a predetermined amount of time.

Liquids with surface tensions lower than the CWST of a porous medium will spontaneously wet the medium on contact and, if the medium has through holes, will flow through it readily. Liquids with surface tensions higher than the CWST of the porous medium may not flow at all at low differential pressures and may do so unevenly at sufficiently high differential pressures to force the liquid through the porous medium. In order to achieve adequate priming of a fibrous medium with a liquid such as blood, the fibrous medium preferably has a CWST in the range of about 53 dynes/cm or higher.

General Procedure for Determining  
Activated Partial Thromboplastin Time

Activated Partial Thromboplastin Time (aPTT) for plasma was determined using the MLA Electra Model 800, a commercial automated instrument designed for measuring clotting time and which is manufactured by Medical Laboratory Automation, Inc. of Pleasantville, New York.

The aPTT was performed according to Proctor, et al., Am. J. Clin. Pathol., 36:312 (1961), the procedure recommended by the manufacturer in the operating instructions for the MLA Electra 800. The reagents used in the test were Actin FS Activated

PTT Reagent, a product of American Dade division of American Hospital Supply (del Caribe, Inc.), and 0.02M calcium chloride solution, also supplied by American Dade.

5    EXAMPLES

A web of melt-blown, polybutylene terephthalate fibers having an average fiber diameter of about 2.6 micrometers fibers was used as a substrate in the following examples. The web had 10 a basis weight of 5.2 grams per 0.093 square meters (1 square foot).

The web was subject to surface modification by radiation grafting by the following steps:

Cylindrical rolls of the above-described web, were 15 formed having a diameter of approximately 7.62 cm. (3 inches) and a length of 25.4 cm. (10 inches) and each was then saturated with a monomer solution as set forth in Table 1 (Examples 1 and 2). Prior to contact with the monomer solution, the dry roll of 20 the web was placed in a sealed metal canister and the canister was evacuated. The monomer solution then was admitted and the roll was saturated by backfilling. The saturated roll was then exposed to a dose of gamma radiation as set out in Table 1, to 25 achieve the desired surface modification following which the roll was washed by applying deionized water down through the length of the roll at a rate of about 75 ml per minute for 16 hours. The web was then thoroughly dried in a recirculating air oven in 30 about 0.91 meter (3 foot) long sheets, at 100°C for the time specified.

In each example, four layers of the particular surface modified microfiber web were assembled into an injection molded housing having a diameter of 25

millimeters and subjected to the aPTT test for coagulation time, as described earlier. The results for these devices made using the media of Examples 1 and 2 are given in Table 3.

5 Also, the medium of each Example was tested for BET surface area, CWST, zeta-potential, and BSA protein binding according to the aforementioned procedures. The results for these tests are given in Table 2.

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TABLE 1

| Example No. | Monomer 1<br>(conc.)   | Monomer 2<br>(conc.)                                | Tertiary<br>Butyl Alcohol<br>(conc.) | Total<br>Dose <sup>3</sup><br>(MRAD) |
|-------------|--|---|--------------------------------------|--------------------------------------|
| 1           | Diethylamino<br>ethyl meth-<br>acrylate (0.3 wt%)            | Methyl<br>methacrylate<br>(0.15 wt%)                | 6.0 vol% <sup>1</sup>                | 0.134                                |
| 2           | Trimethyl ammonium<br>ethyl acrylic<br>chloride<br>(4.0 wt%) | Diethylene<br>glycol<br>dimethacrylate<br>(0.5 wt%) | 25.0 vol% <sup>2</sup>               | 3.0                                  |

<sup>1</sup> The monomer solution was prepared by mixing 6 parts by volume of tertiary butyl alcohol with 94 parts by volume water and then adding to this solution 0.3 wt% diethylamino ethyl methacrylate and 0.15 wt% methyl methacrylate based on the tertiary butyl alcohol/water solution which is assumed to have a specific gravity of 1.0.

<sup>2</sup> The monomer solution was prepared by mixing 25 parts by volume of tertiary butyl alcohol with 75 parts by volume water and then adding to this solution 4.0 wt% trimethyl ammonium ethyl acrylic chloride and 0.5 wt% diethylene glycol dimethacrylate based on the tertiary butyl alcohol/water solution which is assumed to have a specific gravity of 1.0.

<sup>3</sup> The dose rate was 6.7 kilorads/hour for Example 1 and 500 kilorads/hour for Example 2.

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TABLE 2

| Example No.             | Surface Area<br>(M <sup>2</sup> /g) | CWST<br>(dynes/cm) | Zeta-Potential<br>(mv/pH) | BSA Binding<br>( $\mu$ g/cm <sup>2</sup> ) |
|-------------------------|-------------------------------------|--------------------|---------------------------|--|
| 1                       | 1.08                                | 87                 | +23/6.82                  | 52   |
| 2                       | 1.07                                | 93                 | +20/9.09                  | 118  |
| Control<br>(unmodified) | 1.12                                | 51                 | -49/6.90                  | 126  |

TABLE 3

| Device With<br>Medium From<br>Example No. | aPTT Time of Filtrate (sec)  |   |   |
|---|------------------------------|---|---|
|   | Plasma<br>Without<br>Heparin | Plasma With<br>0.4 Total<br>Units of<br>Heparin | Plasma With<br>1.0 Total<br>Units of<br>Heparin |
| 1   | 29.2                         | 32.0  | 64.1  |
| 2   | 32.5                         | 33.4  | 31.3  |
| Control<br>(Unfiltered)                   | 30.8                         | 58.0  | No Clot   |

Example 1 was dried for 24 hours. Example 2 for 72 hours.

The results in Table 3 clearly demonstrate the ability of products of the present invention to return the clotting time (aPTT) of plasma contaminated with heparin back to its normal value, 5 without undue prolongation of the clotting time of the uncontaminated plasma.

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While the invention has been described in some detail by way of illustration and example, it should 10 be understood that the invention is susceptible to various modifications and alternative forms, and is not restricted to the specific embodiments set forth in the Examples. It should be understood, however, that these Examples are not intended to limit the 15 invention but, on the contrary, the intention is to cover all modifications, equivalents, and alternatives falling within the spirit and scope of the invention.

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:-

1. A method for removing heparin from blood or plasma comprising:
  - contacting the blood or plasma with a porous medium having a positively charged surface; and
- 5 removing heparin from the blood or plasma without substantial removal of blood clotting factors.
2. The method of claim 1 comprising contacting the blood or plasma with a self-supporting porous medium.
3. A method for allowing the coagulation parameters 10 of a heparin-containing blood or plasma sample to be accurately determined without interference from therapeutic and incidental heparin levels comprising passing the sample through a porous medium comprising a substrate and a superstrate, said porous medium having a 15 positively charged surface and being capable of removing heparin from the sample without substantial removal of blood clotting factors.
4. A porous medium for removing heparin from blood or plasma comprising a substrate and a superstrate, said 20 substrate selected from the group consisting of polyolefins, polyesters, and polyamides, and at least one superstrate selected from the group consisting of
  - a) trimethyl ammonium ethyl acrylic chloride;
  - b) diethylamino ethyl methacrylate;
  - 25 c) "a" and a polar, non-ionic, ethylenically unsaturated monomer;

d) "b" and a polar, non-ionic, ethylenically unsaturated monomer;

e) "a" and diethylene glycol dimethacrylate; and

f) "b" and methyl methacrylate;

5 said media having a positively charged surface and being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

5. The porous medium of claim 4 wherein the porous 10 medium is unsupported.

6. A porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix having a polymer derived from trimethyl ammonium ethyl acrylic chloride thereon, said medium being capable of 15 removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

7. A porous medium for removing heparin from blood or plasma comprising a polybutylene terephthalate matrix 20 having a polymer derived from diethylamino ethyl methacrylate thereon, said medium being capable of removing heparin, without substantial removal of blood clotting factors and without pH adjustment, from blood or plasma.

25 8. A method for removing heparin from blood or plasma comprising:

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contacting the blood or plasma with a porous medium having a positively charged surface and being capable of removing heparin without substantial removal of blood clotting factors; and

5 removing a therapeutically or clinically significant amount of heparin from the blood or plasma.

9. The porous medium of claim 4 wherein the porous medium is positioned across a liquid flow path within a housing having an inlet and an outlet and defining a  
10 fluid flow path.

10. The porous medium of claim 9 wherein the housing is removably attached to a syringe and to a cannula.

11. The method of claim 1, 3 or 8 comprising removing heparin from blood in an extracorporeal circuit.

15 12. The method of claim 11 wherein the blood flows through a filter assembly in the extracorporeal circuit at a rate of about 2.5 to about 6 liters/minute.

13. The method of claim 1, 3 or 8 or the porous medium of claim 4 wherein the positively charged surface  
20 contains amino and/or ammonium groups.

14. The method of claims 1, 3 or 8 or the porous medium of claims 4, 6 or 7 wherein the porous medium is a polymeric fibrous matrix, polymeric membrane, or a rigid porous medium.

25 15. The method of claims 1, 3 or 8 comprising contacting the blood or plasma with a porous medium comprising a substrate selected from the group

consisting of polyolefins, polyesters, and polyamides, and at least one superstrate selected from the group consisting of

- a) trimethyl ammonium ethyl acrylic chloride;
- 5 b) diethylamino ethyl methacrylate;
- c) "a" and a polar, non-ionic, ethylenically unsaturated monomer;
- d) "b" and a polar, non-ionic, ethylenically unsaturated monomer;
- 10 e) "a" and diethylene glycol dimethacrylate; and
- f) "b" and methyl methacrylate.

16. The method of claim 1, 3 or 8 or the porous medium of claim 4, 6 or 7 wherein the surface area of the medium is in the range from about  $0.01 M^2/g$  to 15 about  $20 M^2/g$ .

17. The method of claim 1, 3 or 8 or the porous medium of claim 4, 6 or 7 wherein the porous medium is capable of removing a clinically significant amount of heparin from a blood or plasma sample when the porous medium is contacted with the sample for a period of 20 about 0.1 second to about 50 seconds.

18. The porous medium of claim 4 or the method of claim 3 or 15 wherein the substrate is a polybutylene terephthalate fiber matrix.

25 19. The method of claim 1, 3 or 8 comprising removing heparin from blood or plasma without pH adjustment.

20. The porous medium of claim 4 wherein the supersubstrate is grafted to the substrate by a linkage which is non-hydrolyzable at physiological pH.

21. The porous medium of claim 6 or 7 wherein the 5 polymer is grafted to the matrix by a linkage which is non-hydrolyzable at physiological pH.

22. A method for removing heparin from blood or plasma, which method is substantially as herein described with reference to any one of the Examples but 10 excluding any control.

23. A porous medium for removing heparin from blood or plasma, substantially as herein described with reference to any one of the Examples but excluding any control.

DATED this 29th day of June 1994

PALL CORPORATION

Attorney: RUTH M. CLARKSON  
Fellow Institute of Patent Attorneys of Australia  
of SHELSTON WATERS

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ABSTRACT

A porous medium having a positive surface charge removes heparin from a heparin-containing liquid, without removing other proteinaceous 5 components from the liquid. Methods and devices are disclosed.