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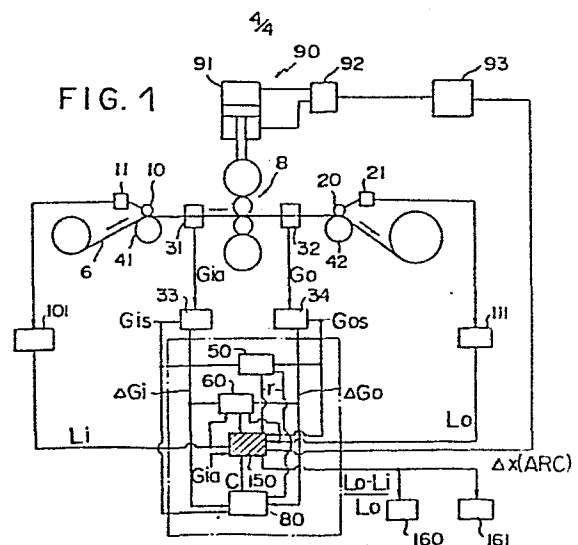
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Method of automatically controlling the rate of reduction in a rolling mill.

The invention describes a method for automatically controlling the rate of reduction suitable for ARC mode of the method for automatically controlling the strip thickness, the rate of reduction is controlled such that an output thickness of the material is calculated from an actually measured input thickness of the material and the desired rate of reduction based on the principle of the constant mass-flow rate of the material being rolled an input thickness is estimated from the calculated output thickness, an input length and an output length and an error signal between the estimated input thickness and the actually measured input thickness is diminished to zero.



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A METHOD OF AUTOMATICALLY CONTROLLING THE RATE OF
REDUCTION IN A ROLLING MILL

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The invention relates to a method of automatically
controlling the rate of reduction in a rolling mill for
rolling a material being rolled at a predetermined rate
of reduction.

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In recent years necessity has been voiced for improved
accuracies in plate thickness in the rolling of steel
sheets by means of rolling mills, particularly in the
cold rolling of thin steel sheets such as an electrical
steel sheet and a stainless steel sheet by means of
Sendzimir mills and consequently it is desired to improve
the accuracy in strip thickness control.

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As a method of controlling the strip thickness of a
device therefore there have heretofore been employed
automatic gauge control (for example see US-PS-42 44 025)
for diminishing to zero the deviation in the output side
strip thickness from a predetermined desired uniform
gauge thickness and automatic reduction rate control
(see US-PS-36 24 369).

1 The ARC contemplates to correct the input deviation by
the value corresponding to the rate of reduction,
whereby the output value of rate of reduction is low as
compared with the aforesaid AGCs, so that the load of
5 the screwdown system can be low, the responsibility
enhanced and the stability improved.

A specific method of ARC, in which the rate of reduction
is controlled at a predetermined value, is one in which
10 the rate of reduction is detected to control the roll
gap to become equal to the desired rate of reduction
in the same manner as in the ordinary strip thickness
control, in which the strip thickness of the output side
of the mill is measured to control the rate of reduction.

15 As methods of measuring the rate of reduction in this
case there have heretofore been known a method of measur-
ing the rate of reduction by use of a strip thickness
gauge, a method of measuring the percentage of elongation
20 from the strip length or strip speed by use of deflector-
odes, etc. With ARC by use of the former, the position,
where the strip thickness gauge is provided is apart from
the positions of work rolls, whereby a delay in time takes
place due to the travel of the material therebetween,
25 thus deteriorating the controllability. With ARC by use
of the latter, errors occurring due to slip between the
deflectorrolls and the steel sheet and the difference
between the diameters of rolls hamper the accurate mea-
surement of the percentage of elongation.

30 In addition another ARC contemplates to obtain a constant
rate of reduction by rolling at a predetermined pressure
by use of an accumulator and rolls being low in elasti-
city. However, particularly the mills having a multi-
35 roll arrangement have hysteresis due to friction and loose-
ness thus presenting such a disadvantage that a constant
rate of reduction is not easily obtainable. It is there-
fore the task of the present invention to provide a method of

1 automatically controlling the rate of reduction in a
rolling mill, capable of carrying out rolling at a con-
stant rate of reduction being stabilized with high
accuracy. This task is solved by a method of automati-
5 cally controlling the rate of reduction in a rolling
mill for rolling a material being rolled at a predeter-
mined rate of reduction, wherein the rate of reduction
is controlled in such a manner, that an output thickness
of the material being rolled is calculated from an
10 actually measured input thickness of the material and a
desired rate of reduction based on the principle of the
constant massflow rate of the material being rolled, an
input thickness is estimated from the output thickness
thus calculated, an input length and an output length
15 and the difference between the estimated input thickness
and an actually measured input thickness can be diminish-
ed to zero.

With these features there is no delay in time due to the
20 travel of the material and calculation includes the
input thickness, so that satisfactory response to the
input thickness can be obtained. According to preferred
embodiment of the present invention said estimated input
thickness is feedback corrected by a correction value
25 obtained by adding an averaging difference between a
calculated output thickness deviation and an actually
measured thickness deviation of the material being
rolled over a predetermined length of the material.
With these features it is possible, to obviate the steady
30 variations from the desired value in the rate of reduc-
tion due to errors in measurement of the strip length,
changes in strip width or the like in the above mentioned
methods of automatically controlling the rate of reduction.

35 Detailed description will herewith be given of the method
of the present invention with reference to the drawings,
in which Fig. 1 is a block diagram, showing a reduction
control system, in which the method of automatically

1 controlling the rate of reduction according to the
present invention is applied to a reversing mill, Fig. 2
is a diagram showing an example of the changes in thick-
ness deviation in the use of the inventive method and
5 Fig. 3 is a diagram showing an example of recorded
results of the rate of reduction in the use of the
invention. To explain the inventive features the
block diagram, shown in Fig. 1, will be explained in
the following:

10

This diagram shows input length detecting means includ-
ing a small touch roll 10, a pulse generator 11 and an
input length counter 101 for detecting an input length
Le of an material 6 being rolled in the mill 8, an input
15 thickness gauge 31 for detecting an actually measured
input thickness G_{ia} of the material 6 an input thickness
deviation output circuit 33 for feeding a difference
 ΔG_i between the actually measured input thickness G_{ia}
fed from the input thickness gauge 31 and input thick-
ness reference value G_{is} , an input thickness deviation
20 shift register 60 for storing the input thickness
deviation ΔG_i fed from the input thickness deviation
output circuit 33, successively shifting same in accord-
ance with the measured distances in response to output
signal fed from the aforesaid input length counter 101
25 and feeding data immediately before the positions of
the work rolls, a desired reduction output circuit 50
for calculating a desired rate of reduction R from the
input thickness reference value G_{is} and an output
thickness reference value G_{os} and feeding same, output
30 length detecting means including a small touch roll
20, a pulse generator 21 and an output length counter
111 for detecting an output length L_o of the material
6, a calculating circuit 150 for initiating calculation
each time a predetermined length is detected by means
35 of the input length counter 101, calculating an estimat-
ed input thickness G_{ic} through an equation:

$$1 \quad G_{ic} \text{ (ARC)} = \frac{L_o}{L_i} G_{os} + \Delta G_i (1-r) \quad (1)$$

or

$$5 \quad G_{ic} = \frac{L_o}{L_i} G_{os} + \Delta G_i (1-r) + c \quad (2)$$

From the input length L_i fed from the input length counter 101, the output length L_o fed from the output length counter 111, the input thickness deviation ΔG_i immediately before the positions of work rolls fed from the input thickness deviation shift register 60, the output thickness reference value G_{os} and the desired rate of reduction are fed from the desired reduction output circuit 50 and feeding an error signal Δx (ARC) between the estimated input thickness G_{ic} (ARC) and the actually measured input thickness G_{ia} fed from the input thickness gauge 31, a correction value calculating circuit 80 for obtaining a calculated output thickness deviation $\Delta G_i (1-r)$ from the input thickness deviation G_i fed from the input thickness deviation output circuit 33 and the desired rate of reduction R fed from the desired reduction output circuit 50, calculating a feedback correction value C for correcting an error from the calculated output thickness deviation $\Delta G_e (1-r)$ and the actually measured output thickness deviation ΔG_o through an equation

$$25 \quad C = \frac{\sum_{j=1}^n \Delta G_o - \sum_{j=1}^n \Delta G_i (1-r)}{n} \quad (3)$$

and feeding same to the calculating circuit 150 a screw-down apparatus 90 including a hydraulic cylinder 91, an electro hydraulic servo-valve 92 and a screwdown servo mechanism 93 for controlling the positions of the work rolls in accordance with the error signal Δx (ARC) fed from the calculating circuit 150 and a recorder 160 and an indicator 161 for recording and indicating a rate of reduction $\frac{L_o - L_i}{L_o}$ calculated from the input length L_i and

the output length L_o in the calculating circuit 150. The inventive method is now as follows:

1 Firstly, the input length L_i is measured such that the
number of rotations of the touch roll 10 provided on the
center line of the deflector roll 41 disposed forwardly
of the mill 8 is converted into pulses by means of the
5 pulse generator 11 and counted by means of the input
length counter 101. The digital or analog input length
 L_i thus obtained is fed to the calculating circuit 150.

Subsequently, the actually measured input thickness G_{ia}
10 is measured by means of the input thickness gauge 31
interposed between the deflector roll 41 and the positions
of work rolls, compared with the input thickness refer-
ence value G_{is} in the thickness deviation output circuits
33, and the input thickness deviation ΔG_i thus obtained
15 is fed to the input thickness deviation shift register
60. The input thickness deviations ΔG_i thus supplied
are successively shifted in response to outputs from
the input length counter 101, whereby the input thick-
ness deviation ΔG_i immediately before the positions of
20 work rolls is fed from the shift register 60 to the
calculating circuit 150.

The desired rate of reduction r is calculated from the
input and output thickness reference signals G_{is} and G_{os} ,
25 which have been set by the operator, in the desired re-
duction calculating circuit 50, and then, fed to the
calculating circuit 150 as a constant.

The output length is detected by means of the pulse
30 generator 21 of the touch roll 20 being in contact with
the deflector roll 42 disposed at the output side of the
mill 8, passed through the output length counter 111,
and fed to the calculating circuit 150 as the digital
or analog output length signal L_o . In the calculating
35 circuit 150, an estimated input thickness G_{ie} is calcu-
lated through the equation (1) from the abovedescribed
various data, i.e., the input length L_i , the output
length L_o , the input thickness deviation G_i , the output

1 thickness reference value G_0 , and the desired rate of
reduction r at every sampling of the input pulse gener-
ator 11, an error signal Δx (ARC) between the estimated
input thickness G_{ic} and the aforesaid actually measured
5 input thickness G_{ia} fed to the screwdown servo-mechanism
93 of the screwdown apparatus 90. The electro-hydraulic
servo-valve 92 controls the reduction action of the
hydraulic cylinder 91 in a manner to diminish the afore-
said error signal Δx (ARC) to zero at all times.

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In addition, the feedback mechanism is for correcting
errors in the rate of reduction due to the difference
in diameter between the touch rolls at the input and
output sides and the influence of the width spread of
15 the material being rolled is performed by use of the
output thickness deviation. More specifically a calcu-
lated output thickness deviation is obtained from the
input thickness deviation $\Delta G_i (1-r)$, the calculated
output thickness does obtain this compared with an
20 actually measured output deviation ΔG_o and the differ-
ence therebetween thus obtained is used as the correction
value against the static control disturbance. A correc-
tion value C in the equation(3) is obtained everytime
after a plurality of n samplings have been conducted
25 and correction is carried out by the form of the equation
(2).

The rate of reduction is usually represented by $\frac{(G_i - G_o)}{G_i}$.

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However, since the position of the thickness gauge is
spaces apart from the position of rolling reduction,
it is necessary to allow the material 6 to reach the
thickness gauge disposed at the output side before the
true rate of reduction can be obtained. Consequently
35 to use the strip thickness as the representation of the
rate of reduction the complicated mechanism
is like tracking system is necessary and the response

1 become low. Therefore, in this invention the rate of
reduction is easily obtained by calculating $(L_o - L_i)/L_o$
from the actually measured length through the equation
 $G_{10} = \frac{L_o}{L_i} G_c$. The recorder 160 and the indicator 161
5 respectively record or indicate the rate of reduction
 $L_o = L_i/L_o$ which has been calculated in the aforesaid
calculating circuit 150.

10 Figs. 2 and 3 are recording charts showing the deviation
of strip thickness and the rate of reduction in the case
of applying the present invention. Fig. 2 shows an
example where a test coil being trapezoidal shape and
having a strip thickness of approximately ± 10 micro-
metre is rolled at a certain rate of reduction, in which
15 is best shown the condition that the change in output
thickness indicated by D follows the change in input
thickness indicated by E. Additionally, according to
the record of the rate of reduction, it is found that
the material is rolled within $\pm 1\%$ with respect to
20 the desired value 9%.

It should be apparent to those skilled in the art, that
the inventive method can be carried out with numerals
and various other arrangements by those skilled in the
25 art without departing from the spirit and the scope of
the invention.

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1 CLAIMS:

- 5 1. A method of automatically controlling the rate of
reduction in a rolling mill for rolling a material
being rolled at a predetermined rate of reduction,
the rate of reduction is controlled in such a manner,
that an output thickness of the material being rolled
10 is calculated from an actually measured input thick-
ness of the material and a desired rate of reduction
based on the principle of the constant mass-flow
rate of the material being rolled, an input thickness
is estimated from the output thickness first calcu-
15 lated, an input length and an output length, and a
difference between the estimated input thickness
and an actually measured input thickness can be
diminished to zero.
- 20 2. A method according to claim 1, wherein said
estimated input thickness is feedback corrected by
a correction value obtained by adding and averaging
a difference between a calculated output thickness
deviation and an actually measured thickness devia-
25 tion of the material being rolled over a predetermined
length of material.

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