



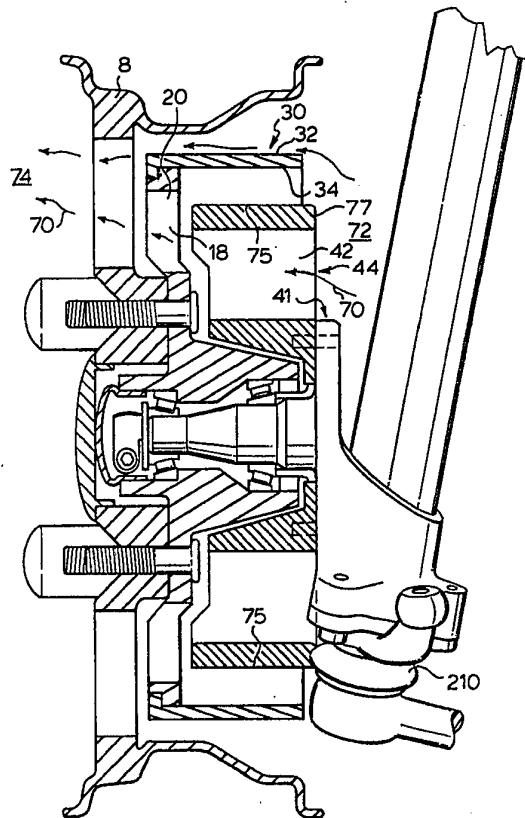
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification ⁶ : F16D</p>	<p>A2</p>	<p>(11) International Publication Number: WO 95/12765 (43) International Publication Date: 11 May 1995 (11.05.95)</p>
<p>(21) International Application Number: PCT/CA94/00607 (22) International Filing Date: 3 November 1994 (03.11.94) (30) Priority Data: 08/145,193 3 November 1993 (03.11.93) US (60) Parent Applications or Grants (63) Related by Continuation US 08/145,193 (CIP) Filed on 3 November 1993 (03.11.93) US 07/853,081 (CIP) Filed on 17 March 1992 (17.03.92) US 07/297,133 (CIP) Filed on 17 January 1989 (17.01.89) (71)(72) Applicant and Inventor: SIEGRIST, Eric [CA/CA]; Rural Route #2, Warton, Ontario N0H 2T0 (CA). (74) Agents: HALL, S., Warren et al.; Suite 301, 133 Richmond Street West, Toronto, Ontario M5H 2L7 (CA).</p>		<p>(81) Designated States: AU, CA, JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>Without international search report and to be republished upon receipt of that report.</i></p>

(54) Title: RING BRAKE COOLED BY AIR FLOW

(57) Abstract

The present invention relates to ring brake arrangements (5) and in particular to an effective arrangement for cooling of the brake. Heat is effectively transferred from the ring braking member (30) to a fanned hub arrangement (10) which transfers the heat energy to an axial air flow (70) which is pumped through the center of the brake. In addition heat is transferred to the brake caliper support bracket (41) from the brake caliper (40). The brake caliper support bracket (41) is located across the air flow (70) which serves to cool the same. This structure is particularly well suited for high brake demand requirements where heat build up causes problems or reduces braking efficiency. The brake can also be used to assist braking of trucks where the brake is located on the drive shaft. The brake is effective for most vehicle applications.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgystan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

TITLE: RING BRAKE COOLED BY AIR FLOWBACKGROUND OF THE INVENTION

5 The present invention relates to brakes and in particular relates to ring brakes and efficient dissipation of the energy generated under braking conditions. Brakes of this type have particular application as vehicle brakes.

10 Disk brakes for automobiles have proven highly popular and a number of these disk brakes do include some sort of internal air cooling in an effort to remove heat from the braking system. With any friction brake arrangement, there is a build-up of heat and the brake must dissipate this energy to the surrounding environment. This problem becomes more acute in race car applications or
15 higher load applications such as trucks or trains in that there is less opportunity to dissipate this energy to the surrounding environment between braking applications. Front wheel drive cars have high front wheel braking requirements which often are not now being met or have a
20 very short life.

To overcome a number of these problems, there are various high temperature materials which are used for the brake pads and the actual braking surfaces can also be of a high temperature material. Unfortunately, some of these
25 materials are susceptible to damage such as warping which can easily occur if sufficient water strikes these surfaces when they are hot. There is a real problem associated with brakes which do not effectively transfer energy to the environment at a sufficiently high rate. A low rate of
30 heat transfer leads to high brake temperatures which can substantially reduce performance, typically referred to as brake fade or, in more extreme cases, brake failure. The problems are not limited to merely the braking surfaces per se, as the energy does travel through surrounding
35 components and can reach the wheel bearings causing other temperature problems such as melting of the grease and/or premature failure of bearings. Most bearings have an upper

temperature range much lower than the temperatures for race car brakes. Furthermore, the hydraulic fluid used to actuate the brake pads and various hydraulic components thereof also have a maximum temperature limit much less
5 than the maximum temperature of the braking surfaces.

Drum type brakes do not generate as much heat as disk brakes as they do not generate the same brake horsepower. Furthermore a number of arrangements have been proposed which use a ring brake having pads on opposite
10 sides of the ring braking member. Such ring brakes have the capability of providing a large braking surface at a substantial distance from the axis of rotation whereby a large braking force can be generated. This implies that a high heat load will be generated under high brake load
15 conditions. Problems occur in trying to dissipate this heat load, particularly under repetitive braking applications.

Most recently speciality high temperature aluminum has been proposed for the disk of a disk brake, however the
20 high temperatures developed can cause sudden failure of the disk and have not functioned as well as ventilated iron based disks. The high temperatures also make the selection of a suitable brake pad material more limited and difficult.

25 The present invention seeks to provide a ring brake system which effectively dissipates heat from the ring braking member, the ring brake pads and the brake caliper arrangement.

30 SUMMARY OF THE INVENTION

The present invention provides a particular structure for a ring braking member which when rotated causes an axial air flow to move from one side of the brake to the other side of the brake through the center of the
35 brake. Rotation of the system produces a pumping action to encourage this air flow. The heat or energy generated during actuation of the brake is initially absorbed by the

ring braking member and the brake pads. Heat is subsequently transferred by conduction from the ring braking member to a fan hub and to radial type members of the fan hub which are located in the air flow. The radial
5 type members pump the air through the brake. These radial type members in addition to pumping the air provide effective energy transfer areas in contact with the air flow. The braking pads are also very hot under high load applications and this energy is conducted into the brake
10 caliper which supports the brake pads. The brake caliper transfers by conduction a large portion of the heat energy to a brake caliper support bracket which is placed across the air flow. This brake caliper support bracket is designed to act as a heat sink, removing energy from the
15 brake pads and caliper and is designed to transfer energy to the air flow as it flows through and around the brake caliper support bracket.

In a preferred embodiment the interior braking surface is also protected from the air flow by a shield
20 arrangement, preferably by a flanged type arrangement attached to the brake caliper structure to protect the interior braking surface from contaminants (water, dirt, oil) in the air flow. In addition, the interior surface can radiate energy to the flange which is positioned a
25 short distance from the braking surface to thereby further increase the rate of energy dissipation to the air flow passing through the caliper and over the shield arrangement.

According to an aspect of the invention the ring
30 braking member and the fan hub are of cast aluminum which generally has a high coefficient of thermal conduction and high specific heat relative to iron. It has been found that a thicker ring braking member of an aluminum alloy allows an efficient flow of heat energy out of the ring
35 braking member and into the fan hub. In this way energy is quickly dissipated throughout the structures and promotes dissipation of the heat energy to the air flow.

Preferably, the caliper is of cast aluminum and placed in the air flow to transfer energy thereto. It has been found with this arrangement that in most cases, the components may be made of aluminum alloys and a high rate of energy transfer to the air flow can be realized. In the brake arrangement large brake pads are used, and these pads provide a high braking force and also provide a large surface to remove heat from ring braking member and braking pads which is transferred to the caliper. These large surfaces also act to remove heat from the ring braking member as the braking pads, even in a release position, are fairly close to the interior and exterior braking surfaces (depending upon the exact temperatures the ring brake can, on occasion, serve to extract heat from the pads).

In a preferred aspect, the fan hub and ring braking member are die cast as a single aluminum alloy component.

BRIEF DESCRIPTION OF THE DRAWINGS

Preferred embodiments of the invention are shown in the drawings, wherein:

Figure 1 is a partial perspective view of a car;

Figure 2 is partial perspective view of a wheel of a car having the improved fanned hub wheel braking system;

Figure 3 is a partial perspective view showing the brake caliper arrangement and brake pads associated with the wheel spindle;

Figure 4 is a partial perspective view showing the fan hub and ring brake member in an operating relationship on the wheel spindle;

Figure 5 is a sectional view through the braking arrangement and is associated with wheel hub that is secured to the braking arrangement;

Figures 6 and 7 are side views showing the caliper retained in a modified mounting bracket;

Figure 8 is a partial perspective view of the brake caliper and its coordination with the modified mounting bracket;

Figure 9 is a side view of the mounting bracket and brake caliper;

Figure 10 is a partial side view of the mounting bracket and caliper showing movement of the brake caliper
5 within the mounting bracket;

Figure 11 is a sectional view showing the mounting arrangement and wheel hub;

Figures 12 and 13 show various temperatures at selected points in a disk braking system (prior art) and a
10 ring braking system of the present invention; and

Figure 14 is a top view schematic of a two composition brake pad.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

15 The car 2 as shown is supported by a wheel 4 and tire 6. The brake arrangement 5 is driven by the wheel 4. As shown in Figure 2 a fan or air pump arrangement 10 rotates with the wheel and causes an axial air flow from the interior of the brake to the exterior of the wheel. If
20 desired a reverse flow could be used.

Additional details of the brake system are shown in Figures 3 through 5. The fan or air pump arrangement 10 includes a fan wheel generally shown as 12 which has a central hub 14 which among other things includes pockets 16
25 for receiving bearings. Exterior to the central hub 14 are the radial fan members 18 which are interconnected at an outer edge by the joining ring 20. The radially disposed radial members 18 when the fan wheel 12 is rotated about the central hub 14 cause an axial air flow from one side of
30 the fan wheel to the other. The joining ring 20 is isolated from the central hub 14 by the radial members 18. These radial members are generally shaped to interact with the air flow and have a large surface area in contact with the air flow for transferring heat energy to the air flow
35 as it moves across the radial members.

A ring braking member 30 is mechanically fastened to the joining ring 20 of the fan wheel and is in good

thermal transfer relationship with the joining ring 20. The ring braking member may be integral with the fan wheel in some configurations. The fan wheel 12 acts as a heat sink for the ring brake member 30 and this energy is
5 dissipated throughout the fan wheel 12. Fortunately the fan wheel when rotated allows a large amount of this energy to be dissipated to the air flow as it passes over the radial member 18. Thus, the central hub 14 and the bearing pockets 16 are not as likely to experience the high
10 temperatures of the ring brake and are substantially cooler than the joining ring 20. Furthermore this temperature differential continues to draw heat away from the braking ring member 30.

The braking ring member 30 has an exterior braking
15 surface 32 and an interior braking surface 34. The exterior braking surface has little tendency to accumulate dirt or material thereon as it is essentially thrown off with rotation of the braking ring member. In contrast the interior braking surface can trap material and a number of
20 holes have been provided between the exterior braking surface and the interior braking surface. It has also been found that these holes encourage an airflow radially throughout the braking ring member and remove heat at the surface where it is generated. A second series of holes
25 can be used to increase this effect. The open center of the brake accommodates and promotes this air flow.

A brake caliper 40 supports and positions the interior brake pad 50 and the exterior brake pad 48 to opposite sides of the ring braking member. The caliper 40
30 is received in, and supported by, the brake caliper support bracket 41. The caliper 40 is trapped within bracket 41 by plates 51 located to opposite sides of the bracket. The brake pads can be fairly large as generally indicated. The brake caliper support bracket 41 is mechanically fastened
35 to the support structure of the vehicle preferably via the mechanical fastening points indicated as 52 in Figure 3. The brake caliper support bracket 41 includes a number of

support arms 42 having ports 44 there through which are generally aligned with the air flow which passes through a central part of the brakes. Again these ports 44 have a large surface area over which the air flow passes to
5 accommodate energy transfer to the air flow. These support arms are generally symmetrical for left or right hand use. If a separate left and right bracket is used, one of the symmetrical arms is dropped and a weight savings is realized. Right and left brackets can be designed for high
10 strength and large surface area in contact with the air flow for effective heat dissipation.

It has been found that the brake pads 48 and 50 transfer a great deal of heat energy to the brake caliper 40 and brake caliper support bracket 41. These components
15 are designed to be located in the axial air flow within a large surface area for effective transfer of energy to the air flow. The truss like structure of the support bracket 41 collectively defines a number of ports having a large surface area contacting the air flow.

20 Actuation of the brake pads is accomplished preferably hydraulically and hydraulic fluid may be provided to the brake actuator within the caliper via line 54. The wheel 8 is secured to the fan wheel 12 via the wheel bolts 60. In this way, the wheel rotates the fan
25 wheel 12 and the radial type members 18 encourage an air flow 70 indicated in Figure 5 through the brake. Thus, it can be seen that air to the interior of the brake is pumped through the center of the brake to the exterior. The interior part of the brake is generally indicated as 72 and
30 the exterior or outside portion is indicated as 74. As can be seen the support arms 42 of the brake caliper support bracket 41 has a large surface that is in contact with the air flow 70. The ports 44 restrict passage of the air flow through the center of the brakes and as very little of this
35 air flow will contact the interior braking surface. Thus the bracket 41 also acts as a shield protecting the interior braking surface from contaminants (water and/or

dirt) in the air flow. The braking member 30 is extremely hot under heavy braking conditions, creating a large temperature differential relative to the fan wheel 12 driving the transfer of energy thereto. This heat path is encouraged with this design to get the heat energy to the radial members 18 which are designed to transfer the energy to the axial air flow. Typically the braking ring member 30 is mechanically fastened to the joining ring 20 and there is a good thermal energy conducting relationship therebetween. The system is designed to encourage heat energy transfer to the joining ring 20 and to the radial members 18. This heat energy is transferred into the fan wheel as the whole fan wheel is acting as a heat sink. However, the air flow serves to remove much of this heat energy.

The braking member 30 and the fan wheel 18 can be die cast of an aluminum alloy for many applications. In this case, the braking member 30 is preferably substantially thicker to add strength and to add material. The thicker brake member of aluminum more efficiently conducts the heat energy to the fan wheel and then to the air. To provide strength and temperature improvements, the alloy can contain significant silicon carbide.

It has been found with the system as described above that the brake caliper arrangement acts as a good heat sink and can effectively transfer heat energy to the air flow. The design and placement of the caliper arrangement in the air flow with a large surface area component over which the air flow must pass results in a high rate of energy transfer. Similarly there is excellent contact between the radial members 18 and the air flow and heat energy from the ring braking member 30 is effectively transferred to this air flow. The holes in the brake member 30 also causes an air flow through the holes which air flow absorbs some of the energy created during braking applications.

It can also be seen that the brake caliper arrangement has an outer surface 75 generally parallel with and in close proximity to the interior braking surfaces 34. Heat energy can be radiated from the interior brake surface 34 to this exterior surface 75. This exterior surface 75 also serves to isolate the axial air flow from the interior braking surface 34. For clarity, it has not been shown, but an additional flange can be provided on the brake caliper arrangement such that the fan blades 18 do not encourage an air flow between the interior surface 34 and surface 75 or substantially no air flow therebetween. The point is that the air flow can have contaminants particularly water and dirt and it may be preferable to more fully protect this interior surface if necessary. A blocking flange at the end 77 of the caliper overlapping the space from the ring braking member 30 can serve this purpose, if necessary. Contaminants can also be reduced by providing a reversing or somewhat convoluted path through which air passes to reach the interior surface. The brake dissipates energy faster without the shield.

The heat shield can also include a heat shield for mechanical components, particularly lubricated mechanical components, such as the ball joint 210 shown in Figure 5. This component is in close proximity to the heated surfaces of the brake system and may require protection to reduce thermal radiation from these hot surfaces. As can be appreciated, the present brake system dissipates energy to the air flow, however, this air flow is dependent upon rotation of the wheel. On occasion, heavy braking, which will generate a large thermal load, can be followed by a low rotation rate of the wheel and low axial air flow or even a stationary condition and no axial air flow. Under such conditions, the brake components can become quite hot and radiate energy to adjacent components. A thermal shield can reduce the amount of energy radiated in this manner and protect such components. With this system, the wheel hub 8 can also be in direct contact with the fan hub

and act as a further heat sink and energy dissipating surface. The mass of the wheel hub serves to reduce peak temperatures and protect the wheel bearings. It is preferred the wheel hub to be of aluminum alloy due to the heat absorption and the energy transfer characteristics of aluminum.

It has been found with this braking arrangement that a great deal of braking force can be provided and the heat energy resulting from braking can be dissipated to the air flow which passes from one side of the brake through the center of the brake to the other side of the brake. Depending upon the particular application, and the normal running speed of the fan hub it is possible to match the rate of energy distribution or transfer to the air flow versus the expected rate of heat energy generation due to braking. The point with the present invention is that an air flow through the braking system is utilized to allow heat energy generated at the braking surface and at the braking pads to be dissipated in an improved manner. This provides a further degree of design variability to meet the demands of particular applications. Use of aluminum components have advantages with respect to weight and energy conduction characteristics. Thicker components are less prone to thermal stress as a more uniform temperature is achieved.

The present brake has been described with respect to braking the wheel of a vehicle. However, it can also apply as a brake for a rotating drive shaft or other rotating shaft. In such alternate applications the shielding capability may not be as critical due to the particular environment in which the shaft is found. Such a brake has particular application for transmission brakes or drive shaft brakes for trucks. In some applications, a separate air flow can be produced and directed on the brake.

It has also been found that the fan wheel maintains the bearings that are in contact with the wheel

spindle as shown in Figure 5 at a satisfactory temperature and much lower than temperatures that are common with disk braking system where much of the heat energy causes high temperatures at the wheel bearings. The wheel rim also
5 acts as a heat sink and provides protection for the wheel bearings. The wheel rim also acts as a heat dissipating surface in contact with the air flow.

With the present system, even in a demanding race environment where brakes are used more frequently and on a
10 more demanding basis, the brake and the braking surfaces have a lower operating temperature, several hundred degrees below those of comparable disk brake systems. According to tests in a race car application, the temperature of the ring brake generally topped out between 500-700°F. This
15 temperature range was several hundred degrees lower than with existing disk brake systems. Some high temperature aluminum alloy materials can work satisfactorily at these and higher temperatures, and due to the properties of aluminum, the normal operating temperatures are
20 significantly lower. Normally, the ring braking member in aluminum is thicker than the iron counterpart but is lighter. Furthermore, the temperature of disc brake system continued to build due to the fact that the system could not dissipate the energy at a fast enough rate. If the
25 rate of heat generation is greater than the rate of heat dissipation the difference in the energy is accumulated in the braking system and depending upon the difference between these two rates the temperature of the brake can become very high quickly. Problems of this type are
30 reduced with the present system where a high rate of energy dissipation is realized and many components provide a high heat sink mass thereby reducing peak temperatures.

A modified brake caliper and mounting bracket are shown in Figures 6 through 11. The mounting bracket 140 is
35 basically 'C' shaped and is open either side thereof to allow compensation for thermal expansion. Thus, there is an open central cavity, generally shown as 150, in which

the brake caliper 102 is located and generally floats. The caliper 102 floats in that it moves within the mounting bracket when the opposed brake pads 104 are brought into braking engagement with the rotating ring braking member
5 120.

The brake caliper 102 is maintained in the mounting bracket 140 by a retaining arrangement, generally indicated as 115. This includes a mounting plate 108 secured by retaining bolts 110 to the brake caliper, with this
10 mounting plate having a retaining slot 109. The retaining slot 109 is sleeved over bolt 142 which projects from the mounting bracket 140. The mounting plate 108 is retained on the mounting bracket 140 by the cooperating washer 144, spring 146 and retaining nut 148. The mounting bracket 108
15 is slidable on the planar surface 145 provided on the mounting bracket 140.

A sleeve 215 of predetermined length is shown in Figure 8 and acts as a stop position for the washer 144 and retaining nut 148. Use of sleeve 215 predetermines the
20 force exerted by spring 146 and simplifies installation. Sleeves of different lengths can be used if different spring forces are desired. In some applications, the sleeve may be eliminated.

The brake, when operated in a generally cold
25 condition, is indicated in Figure 6. As can be seen, the brake caliper 102 is generally centered on the ring brake member 120, positioning the brake pads 104 either side of the ring braking member. The retaining arrangement 115 has allowed sufficient movement of the brake caliper to allow
30 this cleared position to be assumed. Application of the brake pads to engage ring brake member 120 is accomplished by means of a hydraulic piston arrangement located within the brake caliper 102 which urges the interior brake pad 104 towards the exterior brake pad. Any required movement
35 of the brake caliper 102 within the mounting bracket 140 is allowed by the retaining arrangement 115.

During severe braking conditions or multiple
braking conditions, the ring braking member 120 can become
very hot and there is a tendency for this member to bell
mouth somewhat at its free end 121. The retaining
5 arrangement 115, as shown in Figure 7, allows the brake
caliper 102 to accommodate this bell mouth occurrence, as
the brake caliper can move out of the vertical plane of the
mounting bracket 140. Thus, a tilting type action can
occur. It has also been found with this arrangement that
10 there can be sufficient pull back of the brake pads, such
that, in the release position, there will be sufficient
clearance between the ring brake member 120 and the free
end 121. The structure in Figure 7 has been exaggerated to
illustrate the operation of the components. This is also
15 advantageous when the fan hub and ring braking member are
die cast as a single component of aluminum. The ring
braking member can be slightly conical to ease
manufacturing. This is also advantageous where the fan
member and ring braking member are made as separate
20 components.

The brake caliper 102, as shown in Figure 8, is
preferably a cast aluminum alloy and has upper guide
surfaces 114 and 116 and lower guide surfaces 118 and 119.
Surfaces 114 and 116 cooperate with the upper wear plates
25 152 and 154 and the lower guide surfaces 118 and 119
cooperate with lower wear plates 156 and 158 of the
mounting bracket. As can be appreciated, when the brake
pads are in an operating position and engaging the ring
brake member 120, there is a tendency for the caliper to be
30 forced to a downstream side of the mounting bracket 140.
Furthermore, the brake pads are forced to this downstream
side and strike the wear plate 152. These brake pads
typically have a metal backing plate 153 and the edge of
this engages the wear plate 152. This can result in
35 substantial loads and wear, and therefore, wear plate 152
is preferably stainless steel or other suitable high
wearing thermal conducting material.

The wear plates 154, 158 and 152, 156 cooperate with the brake caliper to maintain the position of the brake caliper and to minimize wear while maintaining the free floating relationship of the brake caliper within the mounting bracket. The free floating arrangement accommodates interaction in a radial type direction of the mounting bracket 140, as indicated by the arrow 160 in Figure 10. To increase heat transfer from the caliper to the bracket, wear plates 154, 156 and 158 may be brass.

The brake caliper 102, when secured within the modified mounting bracket 140 by the retaining arrangement 115, provides a very simple arrangement which can easily be removed. The assembled system is shown in Figure 11 and it can be appreciated that release of the retaining arrangement allows the caliper to be removed and any service can be easily carried out.

As discussed, the wear plates are preferably stainless steel or brass. The wear plates are selected to provide an effective heat transfer path as well as to address the particular wear requirements. This effective heat transfer path allows heat from the brake caliper 102 to pass into the mounting bracket 140, which essentially works as a heat sink for the brake caliper. Air continues to flow through the mounting bracket 140 and past the caliper, thereby dissipating heat from the mounting bracket and caliper to the air flow.

Figure 12 shows a ventilated disc brake arrangement which is used on a high performance Ford Mustang™, and Figure 13 shows an iron ring brake, in accordance with the invention, which can be used on the same Ford Mustang.

Various tests were carried out on these brakes by modifying a lathe arrangement to turn the disc or the ring brake of the respective structures while applying a braking force to the braking member. It was generally found that the disc arrangement became unstable at a lower braking force than the ring braking member. A measurement of the braking force was made by attaching a torque arm to the

brake caliper structure, which is held in place by a hydraulic cylinder arrangement. The pressure of the cylinder was then used to measure the force, and based on the torque arm, a measurement of brake horsepower was made.

5 The disc arrangement remained at the edge of stability at approximately 7 brake horsepower for a continuous application. In contrast, the ring brake arrangement shown in Figure 13 was continuously run at approximately 9 brake horsepower, while maintaining stability. Stability was

10 mostly measured as a function of the variation in the fluid pressure. At a certain point, the brake would become quite unstable, indicated by widely changing fluid pressure, and each system was backed off to a point where the fluid pressure was more constant.

15 Various temperatures were measured on the apparatus of Figures 12 and 13 to measure the ability of each system to dissipate the energy. With the ventilated disc brake of Figure 12, a substantial heat build-up in the hub occurred, indicated by the area having a maximum temperature of

20 approximately 400°F and a minimum temperature of about 370°F. The disc adjacent an inside edge operated between 600°F and 700°F, whereas the outer extreme of the brake operated between 800°F and 850°F. In addition, pad temperatures were measured by a probe, located where

25 indicated in Figure 12. The caliper temperature was measured to provide an assessment of any heat build-up in the caliper. Application of the brake causes the temperature of the rotating member to rise as well as a temperature increase in the components in thermal

30 conduction therewith. In addition, the brake caliper absorbs heat energy.

Figure 13 indicates the maximum and minimum temperature range of various components of the ring brake system. In this case, the temperature is very hot adjacent

35 the free edge of the ring brake, indicated as an average temperature of 850°F to 895°F. The heat flows through the ring brake member to the fan blades, which had an average

temperature of 260°F to 280°F. Note, the substantial temperature drop across the surface of the ring brake. The inner edge of the ring brake member, for example, had a temperature of 630°F to 700°F. It should also be noted
5 that the center hub, which supports the wheel bearings, had an average temperature of 180°F to 220°F. This arrangement was also used to measure the bracket temperature at the general location indicated as well as a caliper temperature probe and a brake pad temperature probe.

10 The temperature differential experienced over the ring brake member from the outer free edge to the inner edge is quite high and it was found that it was preferable to split the pad to accommodate expansion thereof (see Figure 14). Furthermore, it was found that the pad
15 could be split generally in the direction of rotation of the braking member into an inside pad portion 202 and an outside pad portion 204. The outside pad portion is preferably made of a high temperature braking composition, as the temperatures that it is likely to experience will be
20 higher. In contrast, the inner portion of the pad can be of a lower temperature material due to the cooling effect due to close proximity to the fan blades. The two-pad composition is particularly appropriate in that it recognizes that continuous use of the brake under high
25 braking conditions produce high temperatures and these are best met by a high temperature material. In contrast, there are many normal operating conditions of the brake which will be at substantially reduced temperatures and a high temperature composition material, in fact, is not
30 particularly appropriate. Often this material only works effectively when it is hot and does not produce a large braking force when the material is cold. By splitting the pad and customizing the composition in the manner
35 described, it is possible to provide effective braking for all conditions and avoid the occurrence of substantial brake pad deterioration at high temperature regions, which would occur if a low temperature material was used

throughout. In addition, this arrangement overcomes the deficiencies of a system having a high temperature material throughout, which material does not provide good braking when cold. The coefficient of friction for many brake materials changes substantially with temperature and the split pad composition allows customization of the pads for the particular application. It can be appreciated that changes can be made to the appropriate compositions that are to be used for different braking applications, for example for race cars, for commercial vehicles, for normal passenger cars, etc. It was found that with the ring brake system the split pad reduced fluctuations in the fluid pressure, measured as a function of the torque. A slight angled gap serves to separate the pad portions. A number of graphs show this conclusion. It was also found that this brake causes air to flow from the interior of the brake to the exterior through the center thereof and thereby continuously changes the volume of air in contact with the brake discharging the air at the exterior of the wheel. This avoids recycling of the hot air.

For many applications the low temperature pad can be effective for brake surface temperatures less than 700°F and the high temperature pad can be effective for temperatures of 800°F or higher. In conventional passenger cars, particularly compact cars, aluminum ring brake members can be used. These ring brake members are typically between about 200 to 400 thousandths of an inch thick.

In contrast, the disc brake causes air to be discharged at the periphery thereof, which would typically be within a wheel well, and there is a tendency for the temperature of the air in the wheel well to increase. Furthermore, it was found that the actual discharge temperature of the air was much higher for the disc brake than the ring brake. The actual disc was at a higher temperature, which would lead to this conclusion, however, the lower temperature air through the ring brake provided a

larger temperature differential which can appreciably affect the rate of energy transfer. It is also believed the ventilated disk is prone to corrosion which further decreases the ability to dissipate energy to the air.

5 The brake caliper arrangement of the ring brake effectively removed heat and this heat was transferred to the mounting bracket having the air flowing therethrough. Therefore, although the brake pads became quite hot, there was a good transfer of energy to the caliper which was able
10 to transfer the heat energy to the mounting bracket and subsequently to the air flow. In this way, the brake was able to continuously dissipate energy and reduce the tendency of most brake systems to act as a heat sink and merely continue to rise in temperature. Basically, a number
15 of these components reached a steady state or approximate steady state at very demanding braking applications of between 7 and 9 brake horsepower as determined in the manner discussed above. Note that the determination of the brake horsepower was the same for both systems and provided an
20 effective manner to compare the two systems. Therefore, the measurement provides an effective relative measurement, regardless of whether the actual measurement of brake horsepower for each system may be imprecise.

 It was found with this test apparatus that the ring
25 brake arrangement could provide a higher continuous braking force and was able to dissipate heat in a more effective manner to the environment. The brake arrangement is less complicated to make than the ventilated disc brake and furthermore, the brake system can be of the same weight or
30 lighter. It was found that the prototype unit (having an iron ring braking member) was approximately two pounds lighter than the disc brake for the high performance Mustang. Therefore, the ring brake of the present invention is easily manufactured, has the ability to
35 provide differential braking in different brake applications, and is easily maintained. Further weight savings are realized with aluminum components.

One high temperature aluminum alloy is Duralcan referred to in SAE Technical Paper Series 931087. This is a composite aluminum having 20 volume percent silicon carbide in an aluminum-silicon casting alloy matrix.

5 Material of this type have high specific stiffness and improved friction and wear behaviour. This paper outlines certain test materials and their performance in braking applications. Fortunately, the lower temperatures due to better heat dissipation and energy transfer of the ring

10 brake system makes this type of system effective. It is believed even aluminum alloy having 15 percent silicon carbide which is more common and less expensive is practical for many applications and is easier to die cast. Die casting reduces machining of the braking surfaces which

15 can be difficult.

Aluminum has the ability to absorb heat and transfer it quickly. The aluminum ring brake member is made thicker to provide strength and to provide an effective heat flow path to the fan hub. The holes in the

20 ring brake also cause an air flow and remove heat at the braking surface. The thicker ring brake is tolerated as the material is light and provides a net weight saving for the same braking effect or better braking if the weight is maintained. The aluminum ring braking member tends to heat

25 up and cool down more uniformly whereby thermal stress is reduced. It is also preferred to use the wheel rim as a further heat sink/energy dissipation surface.

Aluminum is about 2.6 times lighter than iron and the specific heat is about 1.8 times greater. Therefore, a

30 compromise between weight saving (more material) and efficient dissipation of energy (i.e. more material makes heat flow path better and more mass can absorb more energy) can be reached for the particular braking requirements. The brake pad material is selected for the ring brake

35 material and many compositions are effective due to the lower maximum temperature.

Although preferred embodiments of the invention have been described herein in detail, it will be understood by those skilled in the art, that variations may be made thereto without departing from the spirit of the invention
5 or the scope of the appended claims.

THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE
PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. A vehicle brake (5) comprising
 - 5 a ring braking member (30) having braking surfaces (34,32) to both the interior and exterior of said member, a support arrangement (10) securing said ring braking member (30) for rotating about a center axis of said support arrangement (12),
 - 10 said support arrangement (12) including a hub (14) of a diameter less than the diameter of said ring braking member (30) with said hub (14) being connected to said ring braking member by intermediate radial members (18) spaced about said hub (14) and having air passages therebetween open to the exterior and open to a central cavity open at
15 the interior of said brake (5), said radial members (18) promoting the passage of an axial air flow (70) through the center of said brake between the exterior and interior of the brake when said support arrangement (12) is rotated
20 about the center axis,
 - a brake caliper arrangement including a brake caliper (40) supporting and controlling opposed braking pads (48,50) located to opposite sides of said ring braking member, said brake pads (48,50) when actuated by movement
25 of said brake caliper (40) commonly braking said ring brake member (30),
 - a support bracket (41) for said brake caliper (40) located within said central cavity and across said axial air flow (70) and of a structure which allows said axial
30 air flow (70) to pass through said support bracket (41) and effectively transfer heat energy from said support bracket (41) to said axial air flow (70),
 - said support bracket (41) contacting said brake caliper (40) to form an effective thermal transfer
35 relationship therewith such that said support bracket (41) acts as a heat sink for said brake caliper (40) and indirectly acts as a heat sink for said brake pads (48,50).

2. A vehicle brake as claimed in claim 1 wherein said support bracket (41) has an exterior surface (75) in close proximity to the interior braking surface (34) and shields the interior braking surface (34) from dirt and water which can be drawn into the center of said brake (5) by the axial air flow (70), said shield being opposite said interior braking surface and of a depth generally equal to the depth of the interior braking surface.
3. A vehicle brake (5) as claimed in claim 2 wherein said radial members (18) are designed to pump said axial air flow through said brake when said ring braking member (30) is rotated.
4. A vehicle brake (5) as claimed in claim 1 wherein said brake caliper bracket (41) is designed to cause a portion of said axial air flow (70) to pass therethrough to increase the surface area in contact with said air flow (70) and the rate at which heat energy is transferred from said brake caliper bracket (41) to said axial air flow (70) when said support arrangement is rotated about said center axis.
5. A vehicle brake as claimed in claim 4 wherein any of said braking member, said brake caliper (40) and said brake caliper bracket (41) are of an aluminum or aluminum alloy.
6. A vehicle brake as claimed in claim 1 wherein said bracket (41) is designed as a truss structure having at least one port (44) through which the axial air flow passes as it flows through the brake from the interior to the exterior of said brake.
7. A vehicle brake as claimed in claim 1 wherein said support arrangement (12) includes a joining ring (20)

integral with ends of said radial members remote said hub (14).

8. A vehicle brake as claimed in claim 7 wherein said joining ring (20) cooperates with said ring braking member (30) to provide overlapping surfaces to align said ring braking member (30) with said support arrangement (12), said ring braking member (30) being mechanically secured to said joining ring (20) in a manner to provide effective heat conduction therebetween.

9. A vehicle brake (5) as claimed in claim 8 wherein said ring brake member (30) and said support arrangement (12) is of a cast aluminum or aluminum alloy.

10. A vehicle brake (5) as claimed in claim 6 wherein said truss is designed to cooperate with said brake caliper (40) and the interior brake pad (50) of the opposed brake pads (48,50) to restrict contact of said axial air flow with said interior braking surface (34) by a majority of said axial air flow flowing through the at least one port (44) of said truss thereby reducing the likelihood of contaminating the interior braking surface (34) with water or dirt that may be included in the axial air flow (70).

11. A vehicle brake (5) as claimed in claim 1 wherein each brake pad (48,50) has a high temperature region of a first composition for generating more brake force at high temperatures and a low temperature region of a second composition different from said first composition for generating high brake force at lower temperatures.

12. A brake pad (200) comprising a brake engaging surface which is divided into at least a first and second area (202,204), said first area (202) being of a composition designed for braking at a low temperature range and said second area (204) being of a composition designed

for braking at a different temperature range higher than said low temperature range.

13. A brake pad (200) as claimed in claim 12 wherein
5 said pad is divided into two areas (202,204) which are physically separated by a recessed portion (206).

14. A brake pad (200) as claimed in claim 12 wherein
10 said high temperature region (204) is for temperatures greater than 800°F at the braking surface.

15. A brake pad (200) as claimed in claim 14 wherein
said low temperature region (202) is particularly effective
for temperatures at the braking surface of less than 700°F.

16. A brake pad (200) as claimed in claim 13 wherein
said low temperature region (202) is particularly effective
for braking at braking surface temperatures less than 700°F
and wherein said high temperature region (204) is for
20 temperatures greater than 800°F.

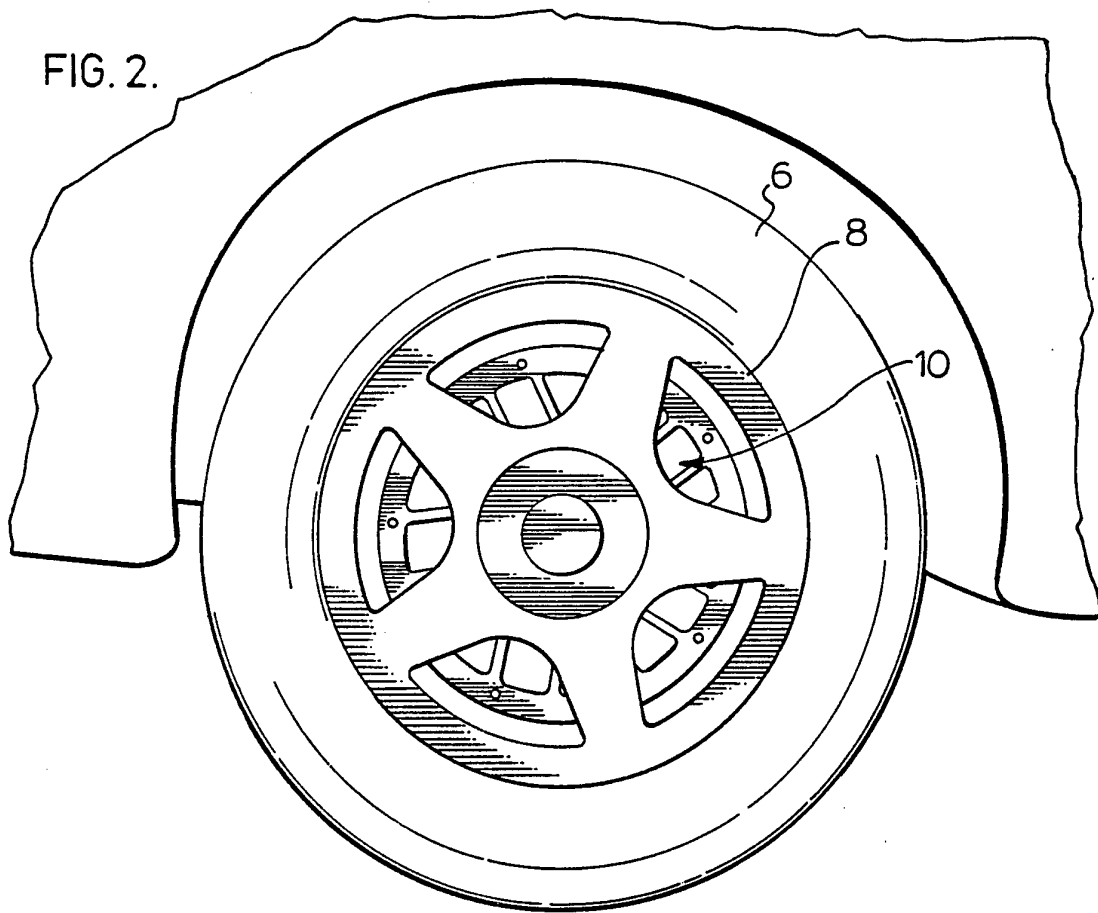
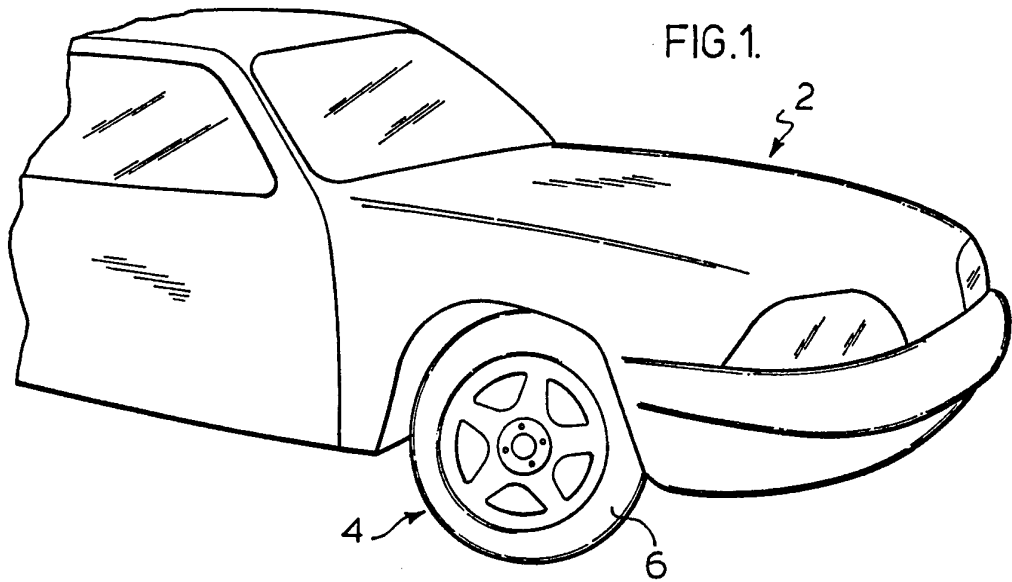
17. A brake pad (200) as claimed in claim 14 wherein
said recessed portion (206) is at a shallow angle relative
to the direction of rotation (208).

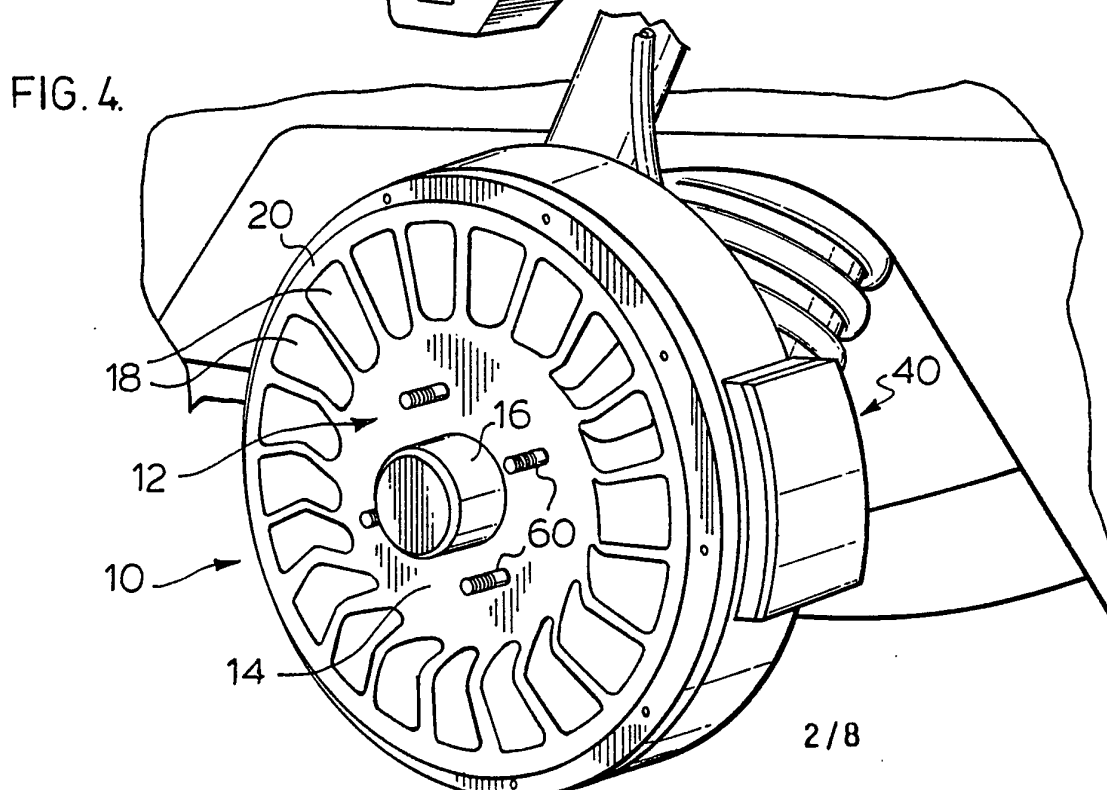
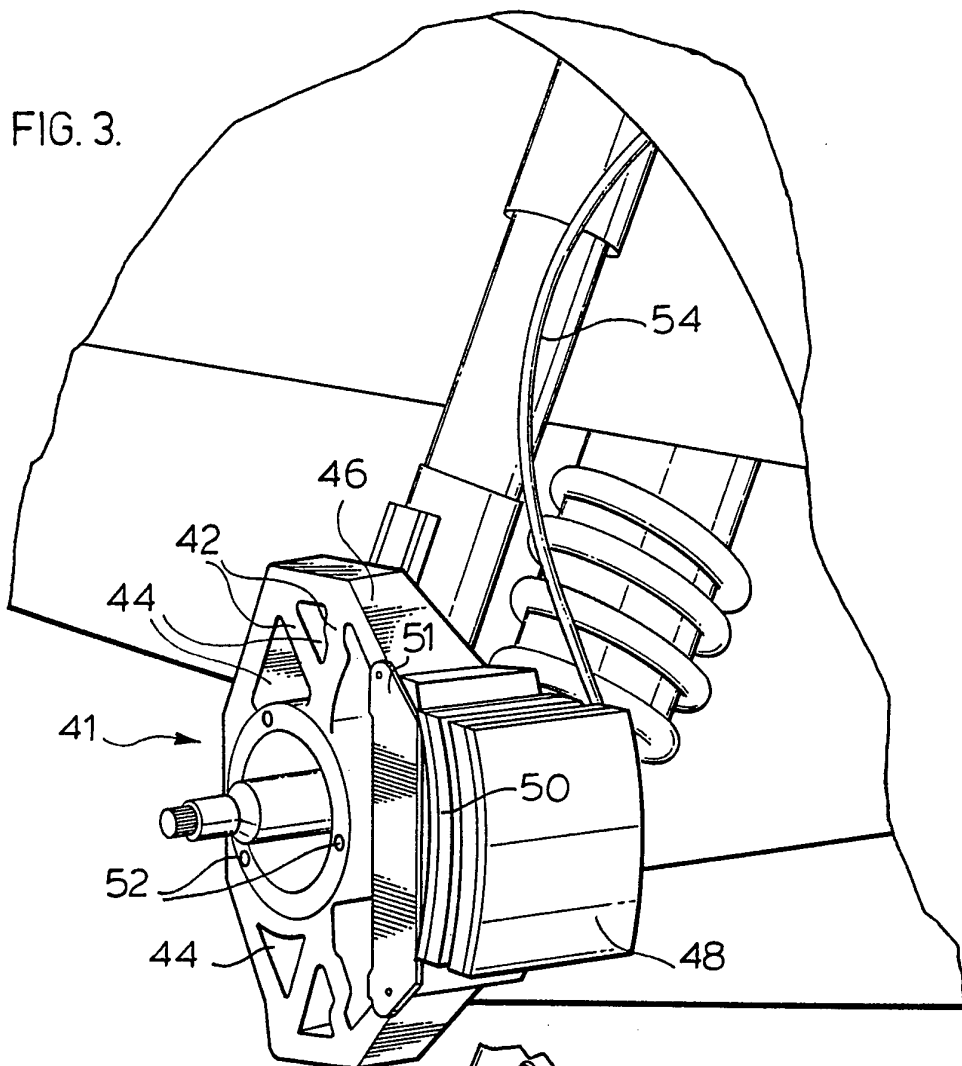
25 18. A brake pad (200) as claimed in claim 12 for engaging a cylindrical braking member having opposed braking surfaces to either side thereof.

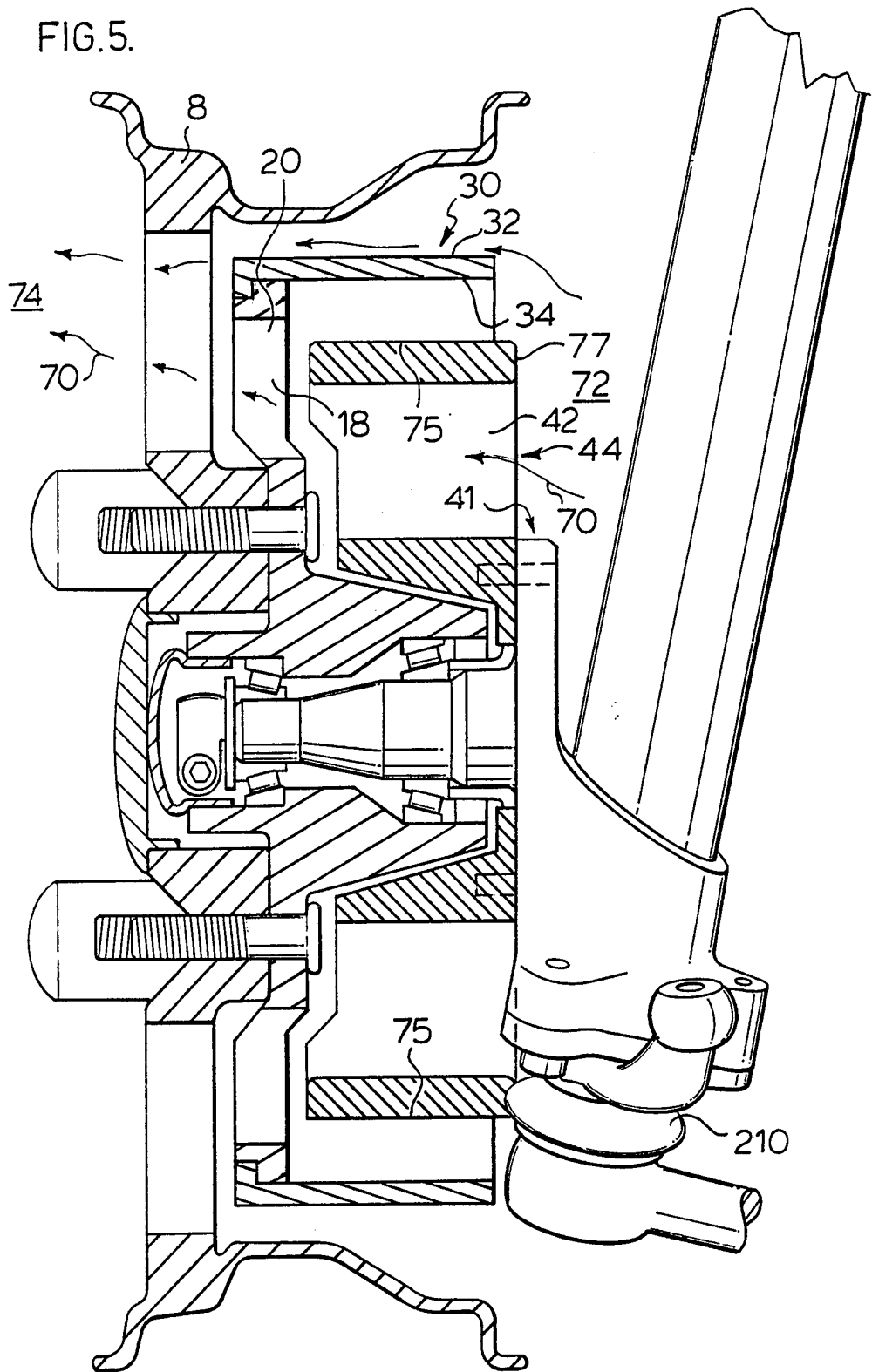
30 19. A vehicle brake (5) comprising a rotating braking member (30) having two opposed planar braking surfaces (32,34) which are engaged by braking pads (48,50), each planar surface having a free exterior edge and an interior edge which is connected to a structural fan hub arrangement
35 (12) for transferring the braking force to a rotating wheel component requiring braking, and means (40,41) for applying said brake pads to said rotating brake member (30), wherein

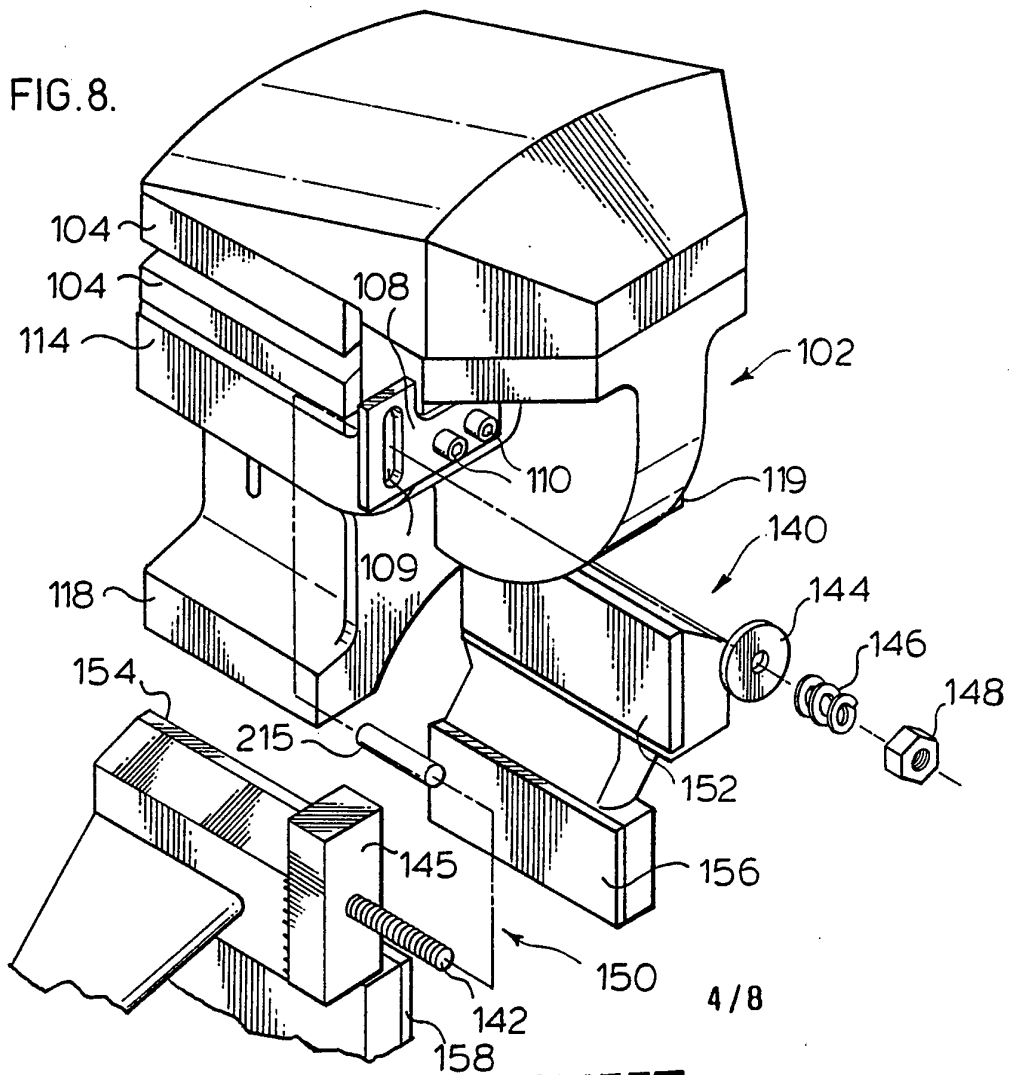
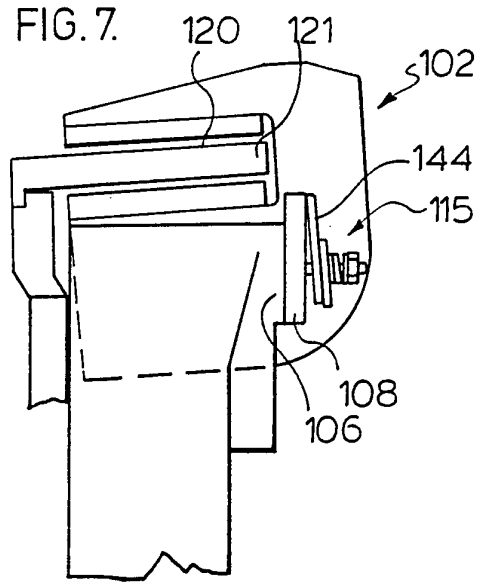
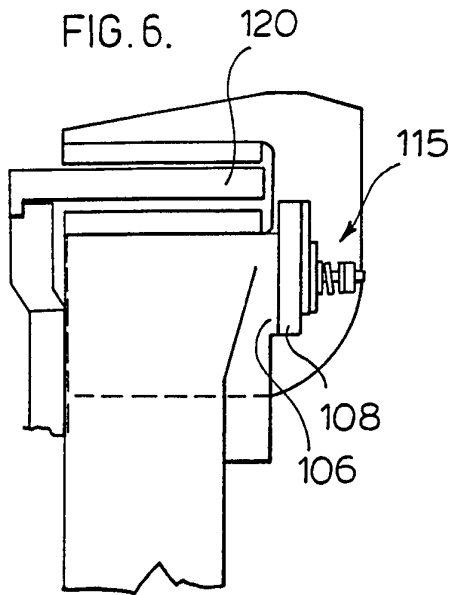
said rotating braking member (30) and said fan hub arrangement (12) are each made of an aluminum alloy.

20. A brake (5) as claimed in claim 19 wherein said
5 rotating braking member (30) is slightly conical having said opposed braking surfaces to either side of said conical shape.

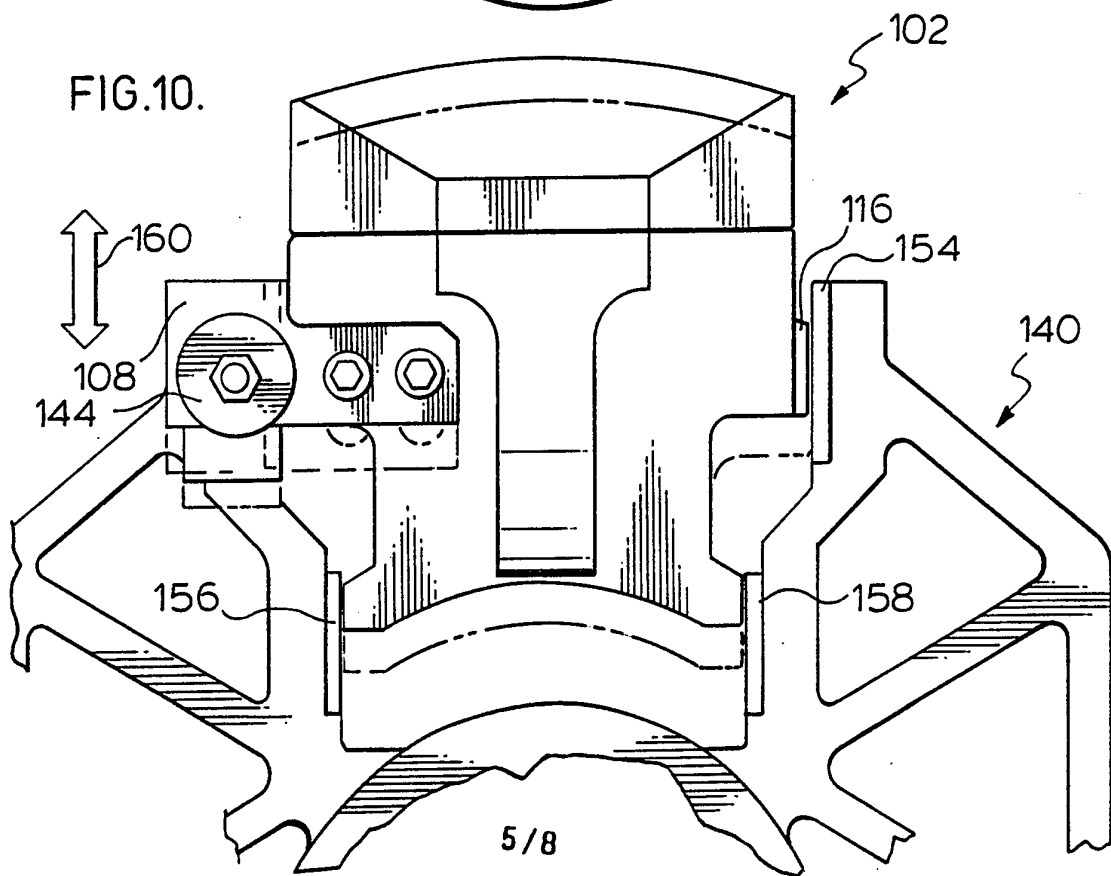
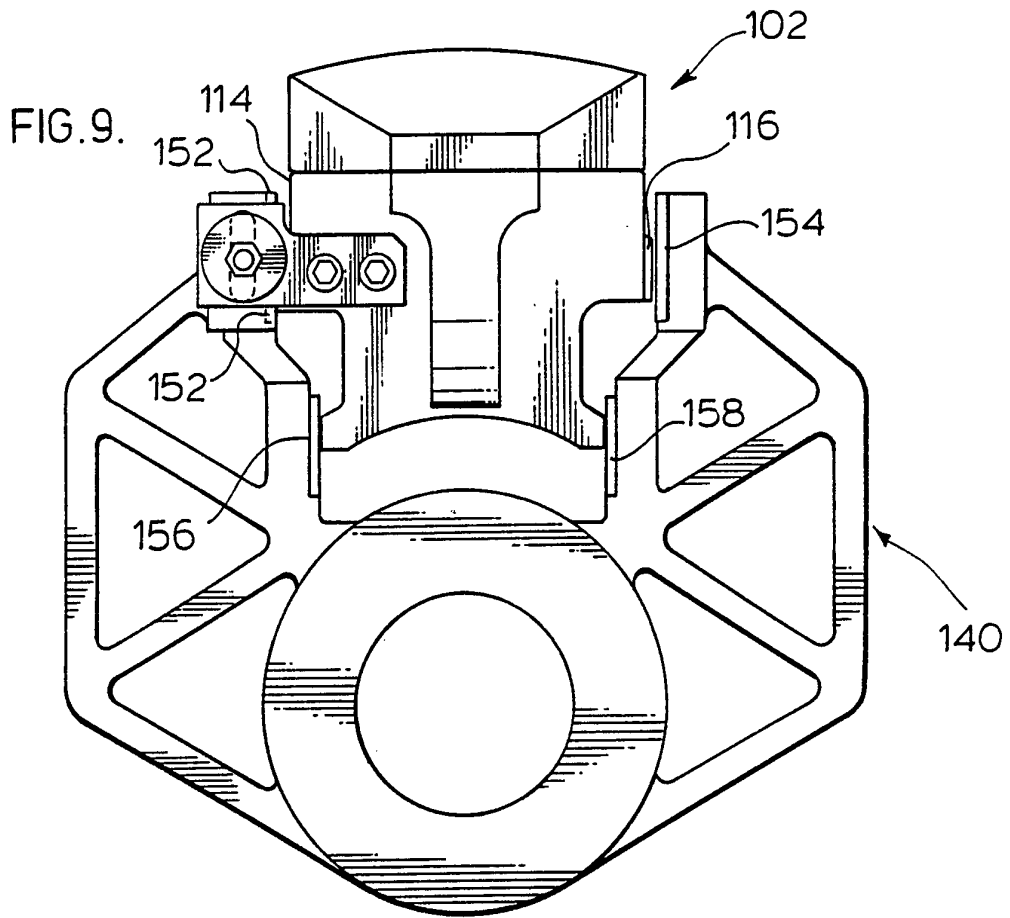






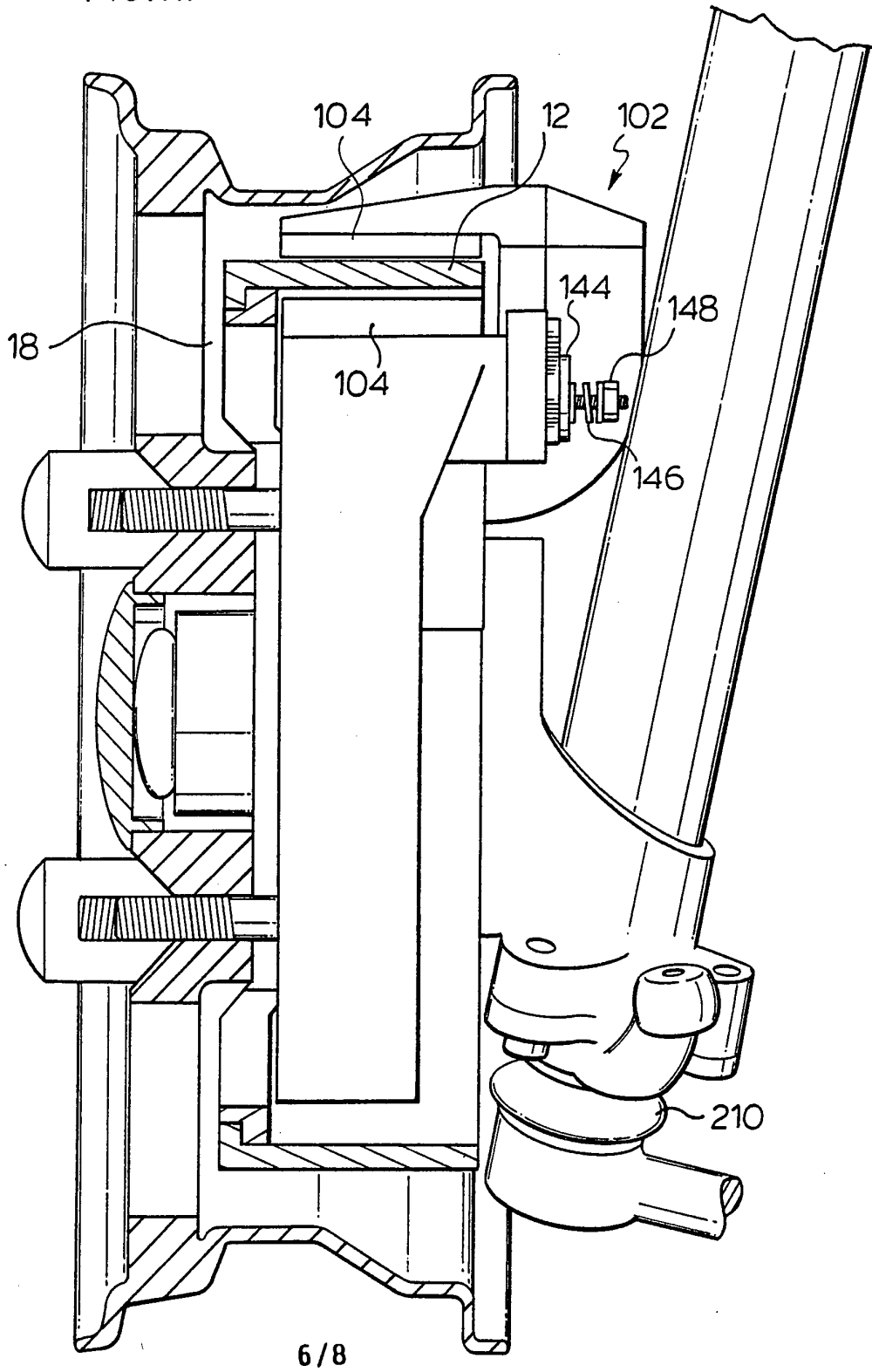


SUBSTITUTE SHEET



SUBSTITUTE SHEET

FIG.11.



6/8

SUBSTITUTE SHEET

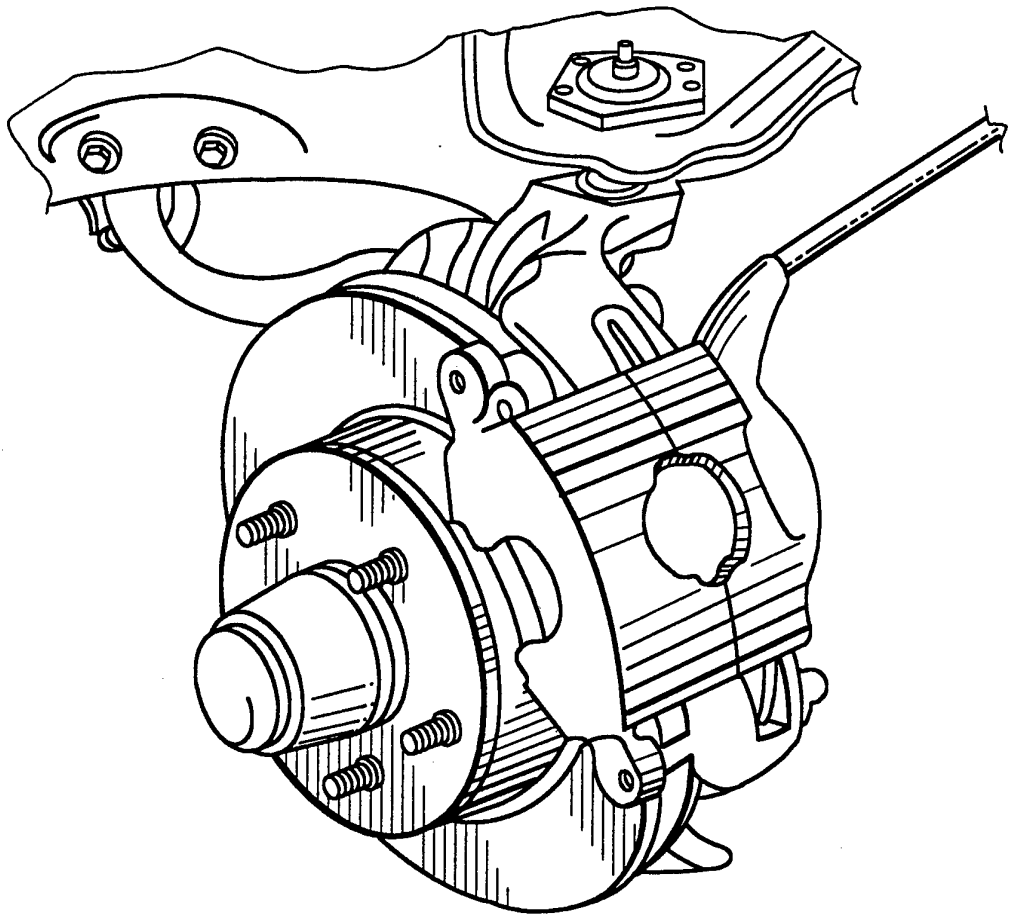


FIG.12

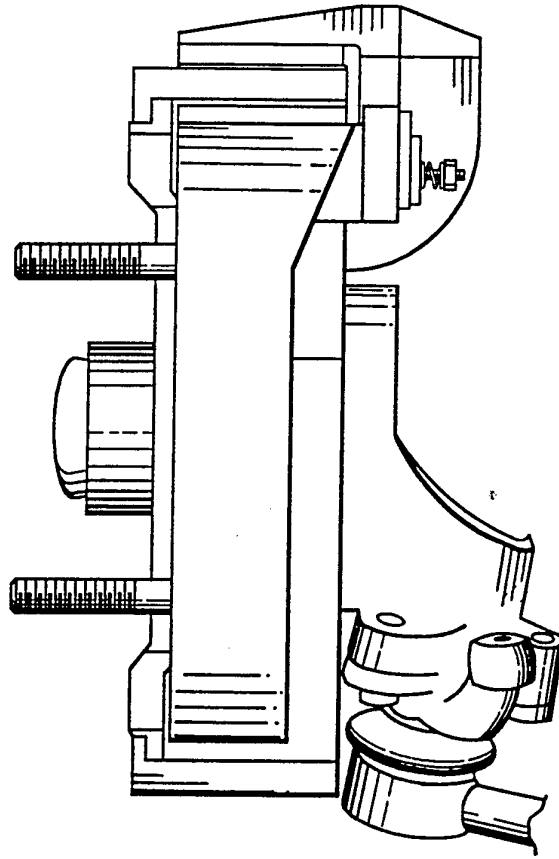


FIG. 13

