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- (73) Patenthaver: **Tyco Fire Products LP, 1400 Pennbrook Parkway, Lansdale, PA 19446, USA**
- (72) Opfinder: **Rogers, Kenneth, 986 Williamson Road, Horsham, PA Pennsylvania 19044, USA**
- (74) Fuldmægtig i Danmark: **RWS Group, Europa House, Chiltern Park, Chiltern Hill, Chalfont St Peter, Bucks SL9 9FG, Storbritannien**
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DESCRIPTION

Technical Field

[0001] This invention relates generally to residential sprinklers.

Background Of the Invention

[0002] Residential automatic fire protection sprinklers are typically designed to specific performance criteria or standard that has been accepted by industry. The performance criteria establishes the minimum performance standards for a given sprinkler to be considered sufficient for use as a residential fire protection product. For example, Underwriters Laboratories Inc. (UL) "Standard for Safety for Residential Sprinklers for Fire Protection Service" (October 2003) (hereinafter "UL 1626"), is believed to be an accepted industry standard.

[0003] The National Fire Protection Association (NFPA) also promulgates standards relating to residential fire protection such as, for example, (i) NFPA Standard 13 (2002) (hereinafter "NFPA 13"); (ii) NFPA Standard 13D (2002) (hereinafter "NFPA 13D"); and (iii) NFPA Standard 13R (2002) (hereinafter "NFPA 13R") (collectively "NFPA Standards"). In order for a residential sprinkler to be approved for installation under NFPA Standards, such sprinkler typically must pass various tests, for example, tests promulgated by UL under UL 1626, in order to be listed for use as a residential sprinkler. Specifically, UL 1626 generally requires a sprinkler, as described in Table 6.1 of Section 6, to deliver a minimum flow rate (litres per minute or "lpm" (gallons per minute or "gpm")) for a specified coverage area (square feet or "ft²") so as to provide for a desired average density of at least 2.04 litres per minute per square meter (0.05 gpm/ft²). For instance, for a 4.88 m x 4.88 m (16 ft. x 16 ft.) room size with a 23.8 m² 256 ft² coverage area, a residential sprinkler that can provide the minimum density in an optimum manner would utilize a flow of water of 49.21 L/m (thirteen gallons per minute (13 gpm)). Thus, 49.21 L/m (13 gpm) is the minimum flow listing for a coverage area of 23.8 m² (256 ft²). In addition to a sprinkler configuration providing the minimum density at the minimum flow listing, the sprinkler advantageously would achieve the minimum flow listing at the lowest possible pressure. The minimum flow rate tabulated in Table 6.1 can be used to calculate a predicted minimum fluid pressure needed to operate a sprinkler by virtue of a rated K-factor of the sprinkler. A rated K-factor of a sprinkler provides a coefficient of discharge of the flow passage of the sprinkler, is defined as follow:

$$K - factor = \frac{Q}{\sqrt{p}}$$

where Q is the flow rate in GPM and p is the pressure in pounds per square inch gauge. Thus, for a rated K-factor of 4.9 and a minimum flow rate of 13 gpm, the residual or calculated minimum pressure is seven pounds per square inch (7 psi.).

[0004] In order for a sprinkler to pass actual fluid distribution tests as described in Sections 26 and 27 of UL 1626 however, the actual minimum pressure of the test sprinkler may differ from the calculated or predicted minimum pressure, which can be calculated using the given minimum flow rate of Table 6.1 in UL 1626 and the rated K-factor of the sprinkler. Further, the actual minimum fluid flow rate to pass these distribution tests of UL 1626 for a specified coverage area may even be higher than the tabulated minimum flow rate given in Table 6.1 of UL 1626. Consequently, any attempt to provide for a listed sprinkler (i.e., an operational sprinkler suitable for the protection of a dwelling unit) cannot be predicted by applications of a known formula to known residential sprinklers.

[0005] In order to provide an aesthetically appealing configuration of a sprinkler for use in a residence, the sprinkler may be configured to use a flat plate to conceal the sprinkler itself until the sprinkler is actuated. This type of sprinkler is known as a residential flat plate concealed sprinklers. It is believed that known residential flat plate concealed sprinklers that are configured for use in a pendent manner range in K-factor from 4.1 to 5.6 (gpm/psi^{1/2}). EP 0 505 672 A2 discloses a residential flat plate concealed sprinkler.

[0006] In order for a residential flat plate concealed sprinkler to operate, a two step operation occurs when a fire hazard is to be addressed. First, the cover of the concealed sprinkler must disengage from the sprinkler. Second, the sprinkler must operate to allow water to flow. Because of the two step operation of the residential flat plate concealed sprinkler, and that such residential sprinklers are typically fully recessed into a ceiling, residential flat plate concealed sprinklers have an increased flow rate above the minimum flow listings in order to successfully pass UL 1626 fire tests.

[0007] It is believed that known residential flat plate concealed sprinklers have been unable to successfully pass the UL 1626 test standard for a 4.88m x 4.88m (16 ft. x 16 ft.) room size fire test at both the minimum flow rate 49.21 L/m (13 gpm) and the minimum operating pressure 48.26 kPa (7 psi). Furthermore, it is also believed that known residential flat plate concealed sprinklers have been unable to successfully achieve the minimum flow rates of 64.35 L/m (seventeen gallons per minute (17 gpm.)) for an 5.46m x 5.46m (18 ft. x 18 ft.) room size and 75.71 L/m (twenty gallons per minute) for a 6.1m x 6.1m (20 ft. x 20 ft) room size in accordance with UL 1626.

Disclosure or Invention

[0008] According to the present invention, there is provided a residential flat plate concealed sprinkler comprising:

a body having an inner surface defining a passageway for carrying a fluid, the passageway including an inlet and an outlet spaced apart along the longitudinal axis and defining a K-factor of about 5;

a closure assembly adjacent the outlet to occlude the outlet;

thermally responsive support means for maintaining the closure assembly adjacent the outlet;

a deflector assembly having a first position distal to the outlet and a second position distal to the first position, the deflector assembly including a plate;

a pair of telescopic guide members each having a proximal end and a distal end, the proximal end being coupled to the body, the distal end of the guide members being coupled to the plate; and

a thermally responsive trigger assembly that maintains the closure assembly adjacent the outlet, characterised in that,

the deflector assembly plate has a substantially oval outer perimeter having a first plate axis and a second plate axis, the distance between portions of the substantially oval outer perimeter along the first axis being greater than the distance between portions of the substantially oval outer perimeter along the second axis, a plurality of diametrically opposed pairs of slots disposed along the substantially oval outer perimeter, the plurality of slots disposed on either side of the first plate axis and the second plate axis further defining a first slot group having a first slot length, and at least a second slot group having a second slot length smaller than the first slot length; and

a projection coupled to the plate in each of the first position distal to the outlet and the second position distal to the first position;

the distal end of the guide members being coupled to the plate along the first plate axis between the pair of slots and adjacent an edge that forms each of the slot of each of the pair of slots; and the trigger assembly has a fusible link assembly spaced from the projection when the deflector assembly is in the first position, and

wherein the deflector assembly distributes a flow of fluid over a protection area ranging from about 13.38m² (about 144 square feet) to about 37.16m² (about 400 square feet), the fluid distribution having a density of at least 2.037 litres per minute per m² (0.05 gallons per minute per square foot (0.05 gpm/ft²)) so as to define a range of minimum operating pressures ranging from about 48.26kPa (seven pounds per square inch) to about 117.21kPa (seventeen pounds per square inch (7-17 psi.)) and a range of minimum operating fluid flows ranging from about 49.21L/m (thirteen gallons per minute) to about 75.71L/m (twenty gallons per minute (13-20 gpm)).

Brief Descriptions of the Drawings

[0009] The accompanying drawings, which are incorporated herein and constitute part of this specification, illustrate exemplary embodiments of the invention, and, together with the general description given above and the detailed description given below, serve to explain the features of the invention.

FIG. 1 shows a cut-away view of a preferred residential flat plate concealed sprinkler.

FIG. 2 is a cross-sectional view of the sprinkler of FIG. 1.

FIG. 3 is a preferred plate assembly of the sprinkler of FIG. 1.

FIG. 4A is a plan view of a preferred deflector plate assembly of the sprinkler of FIG. 1.

FIG. 4B is a cross-sectional view of the deflector plate assembly cut along line IVB-IVB of FIG. 4A.

FIG. 5A is a preferred projection member in the deflector plate assembly of FIG. 4A.

FIG. 5B is a cross-sectional view of the projection member along line VB-VB of FIG. 5A.

FIG. 6A is an alternate plan view of a preferred plate in the deflector plate assembly of FIG. 4A.

FIG. 6B is a cross-sectional view of the plate cut along line IVB-IVB in FIG. 6A.

FIG. 6C is another cross-sectional view of the plate cut along the line VIC-VIC in FIG. 6A.

FIG. 6D is yet another cross-sectional view of the plate cut along the line VID-VID in FIG. 6A.

FIGS. 7A-7C are schematic views of a fluid distribution test area as per UL 1626.

Mode(s) For Carrying Out the Invention

[0010] Shown in FIGS. 1-2 is an illustrative embodiment of a concealed pendant residential fire sprinkler 10 that can be used in residential applications, for example, to protect a floor area of a compartment in the residential dwelling unit. As used herein, the term "residential" is a "dwelling unit" as defined in the 2002 Edition of NFPA 13D and NFPA 13R, which can include commercial dwelling units (e.g., rental apartments, lodging and rooming houses, board and care facilities, hospitals, motels or hotels) to indicate one or more rooms, arranged for the use of individuals living together, as in a single housekeeping unit, that normally have cooking, living, sanitary, and sleeping facilities. The residential dwelling unit normally includes a plurality of compartments as defined in the NFPA Standards, where generally each compartment is a space that is enclosed by walls and ceiling. Accordingly, the sprinkler 10 can be configured for use in a residential sprinkler system, preferably a wet pipe residential sprinkler system for: (i) one and two family dwellings and mobile homes per NFPA 13D; (ii) residential occupancies up to and including four stories in height per NFPA 13R; or (iii) any other occupancy as per NFPA 13.

[0011] Referring to FIG. 1, a partially cut-away view of a preferred embodiment of the residential sprinkler 10 is shown coupled to a sprinkler system, preferably a wet sprinkler system 100, in a plenum space above a ceiling 200 of a known construction such as, for example, gypsum wallboard or ceiling tile. The sprinkler 10 includes a body 12 configured to couple the sprinkler 10 to the sprinkler system 100. Preferably, the sprinkler 10 is coupled to a branch line of the sprinkler system 100 by way of a threaded connection between the body 12 and a corresponding fitting on a branch line of the sprinkler system 100. Alternative connections are possible provided the connection facilitates fluid communication between the sprinkler system 100 and the sprinkler 10 in a manner described herein below.

[0012] The sprinkler 10 preferably includes a support cup or outer housing 14 disposed about the body 12. The outer housing 14 provides a chamber for housing the sprinkler operational components such as, for example, the trigger and deflector assemblies. Connected below the housing 14 is a detachable cover plate assembly 16 providing means to conceal the sprinkler components from view beneath the ceiling 200. The cover plate assembly 16 preferably includes a substantially flat plate 18 that presents a low profile with respect to the ceiling 200. The plate 18 can include decorative or textured surface treatment or coloring so as to aesthetically blend in or coordinate with the surrounding environment. In operation, a portion of the plate assembly 16 is configured to separate from the outer housing 12 and/or the operational components of the sprinkler 10 thereby allowing the sprinkler 10 to actuate and discharge a fire fighting fluid over the area beneath the ceiling 200.

[0013] A cross-sectional view of the sprinkler 10 is provided in FIG. 2. The body 12 is shown with the preferred outer thread 11 for coupling to the sprinkler system 100 and further preferably including a multi-flat area 13 for engagement with an installation tool such as, for example, a socket-type wrench (not shown). The multi-flat area 13 can include, for example, six contiguous flat sides to form a hexagon shaped outer perimeter to the body 12 about which the installation tool can grip to thread the sprinkler 10 into or out of the sprinkler system 100.

[0014] The sprinkler 10 is embodied as a concealed sprinkler. Accordingly, preferably threadedly engaged with the outer threads 11 of the body 12 is the outer housing 14. The outer housing 14 preferably includes an interior peripheral edge defining a centralized bore 42. The body 12 can be disposed through the central bore 42 and the interior peripheral edge of the outer

housing 14 can engage the outer threads 11 of the body 12 to couple the body and the housing to one another. The multi-flat portion 13 of the body 12 can be dimensioned so as to form a stop that engages an inner surface of the outer housing 14 to limit the axial engagement of the body 12 through the central bore 42 of the outer housing 14.

[0015] The inner surface of the outer housing 14 is preferably radially spaced from the longitudinal axis A-A to define a chamber 44 for preferably surrounding and housing the operational components of the sprinkler 10. The inner surface of the housing 14 can include a coupling mechanism 46 for coupling to the cover plate assembly 16. Preferably, the housing 14 includes a rolled thread 46a along the inner surface for engagement with a portion of the plate assembly 16 to couple the elements together.

[0016] Shown in FIG. 3 is a cross-sectional view of the preferably detachable plate assembly 16. The cover plate assembly 16 preferably includes a retaining sleeve portion 48 having a plurality of projections 46B for threaded engagement with the interior thread 46 A of the outer housing 14 to couple the plate assembly 16 and outer housing 14A together. Alternatively, retaining sleeve portion 48 can include a threaded portion for mutual engagement with the interior thread 46a of the outer housing 14. The sleeve preferably includes a mounting surface 50 for engaging the surface of the ceiling 200 thereby limiting the axial engagement of the plate assembly 16 with the outer housing 14.

[0017] A cover plate member is attached to the retaining sleeve 48 such that it substantially conceals the chamber of the outer housing 14 thereby concealing the operational components of the sprinkler 10 such as, for example, the deflector assembly 42 as seen in FIG. 2. The cover plate member is preferably attached to the retaining sleeve by a thermally responsive coupling 52 such as, for example, a tab or beading of solder 52, which is rated to hold the plate member to the retaining sleeve 48 up to a desired temperature. Above the threshold temperature, the solder 52 melts releasing the cover plate member and exposing the operational elements of the sprinkler 10 to address the heat source. The solder 52 is preferably rated between 46.1°C (115°F) to about 60°C (140°F) and more preferably from about 47.2°C (117°F) to about 58.3°C (137°F) and is even more preferably about 57.2°C (135°F). More preferably, three tabs of solder 52 are applied radially about the longitudinal axis. To facilitate the separation of the cover plate member and the retaining sleeve 48, the plate assembly 16 further preferably includes an ejection spring 53 which biases the cover plate member away from the retaining sleeve 48. The ejection spring 53 can be, for example, a compression spring member disposed between the deflector assembly 42 and the plate member 18. As described above, the cover plate member is preferably a substantially flat plate 18 to provide a low profile relative to the ceiling 200. Alternatively, the cover plate member 18 can include a step or curved profile so as to present, for example, a concave surface relative to the view below the ceiling 200.

[0018] The operational components of the sprinkler 10 can individually and collectively define sprinkler performance, i.e. water distribution and compliance with known sprinkler standards such as, for example, the October 2003 edition of UL 1626. More preferably, the operational components of the sprinkler 10 provide for a heat sensitivity or thermal responsiveness along with water distribution characteristics that, can effectively address a residential fire and thereby improve the chance for occupant to escape or be evacuated. The body 12 is an operational component having, as seen in FIG. 2, an inner surface 20 defining a passageway or conduit 22. The passageway 22 provides communication between a body inlet 24 and a body outlet 26 spaced apart along the sprinkler longitudinal axis A-A. The inlet 24 is configured to receive fluid from the sprinkler system 100 and the outlet 26 is configured to discharge the fluid for distribution over a protection area beneath the sprinkler 10. The body 12 is configured to define a discharge coefficient or K-factor of about 5 and more preferably at least 4.9. The K-factor relates in part to the shape of the passageway 22 and other dimensions of the passageway 22, inlet 24 and/or outlet 26. As used herein, a discharge coefficient or K-factor of the sprinkler 10 is quantified or rated as a flow of water Q out of the passageway 22 of the body 12 of the sprinkler 10 in gallons per minute (gpm.) divided by the square root of the pressure p of water fed into body 12 in pounds per square inch gauge (psig), where $K = Q / (p)^{1/2}$.

[0019] The sprinkler 10 is shown, in-part, in a non-actuated state, i.e., the outlet 26 is closed off by a closure assembly 28. The closure assembly 28 is preferably disposed adjacent the outlet 26 to occlude the passage way 22 thereby preventing discharge of fluid from the outlet. The closure assembly 28 preferably includes a plug 30 coupled to a washer 32 having a perimeter contiguous to the inner surface 20 of the body 12 forming the outlet 26. The washer 32 is preferably a Bellville type, Beryllium Nickel washer with a Teflon® coating, of about 0.508mm (0.02 inches). The plug 30 is preferably coupled to a seat member 34 by a compression screw or other fastener 36.

[0020] The closure assembly further includes a thermally responsive trigger assembly or lever 38 providing means for controlling displacement of the washer 32 from the outlet 26 to operate the sprinkler 10. More specifically, the lever 38 is preferably a fusible link assembly having two link halves held together by a solder link element 40 thereby maintaining the sprinkler 10 in a non-actuated state. When exposed to a sufficient level of heat, the solder element melts and the two link halves separate from one another so as to displace the closure assembly, operating the sprinkler 10 and permitting discharge of fluid from the outlet 26.

Alternative closure assemblies 28 and thermal triggers 38 can be provided so long as the alternative construction adequately occludes the passageway 22 when the sprinkler is in a non-actuated state and is adequately thermally responsive to actuate the sprinkler when needed. The trigger assembly 38 is preferably configured such that the sprinkler 10 has a temperature rating of ranging from about 57.2°C (135°F) to about 76.7°C (170°F) and more preferably is about 71.1°C (160°F). A higher sprinkler temperature rating can provide additional flexibility in sprinkler selection over a range of installation configurations and system designs.

[0021] Distal of the outlet 26 is the deflector assembly 42 providing means for distributing a fluid discharge from the outlet 26 over an area below the outlet. The deflector assembly 42 preferably includes a deflector plate assembly 42a, one or more guide members 42b and an inner or guide member housing 42c disposed about a distal portion of the body 12. In FIG. 2, the deflector assembly 42 is shown in both its non-deployed state (solid lines) and its deployed state (dashed lines). More specifically, the deflector assembly 42 has a first retracted position distal of the sprinkler outlet 26 and a second deployed position distal of the first position. Preferably, the plate 18 supports the deflector assembly 42 in its first position so as to locate at least the deflector plate assembly 42a at a minimum distance from the outlet 26.

[0022] In one preferred embodiment, the inner housing 42c is disposed about a flange at the distal end 27 of body 12. The inner housing 42c preferably extends coaxially within the outer housing 14. The inner housing 42c includes an interior surface at least partially circumscribed about the longitudinal axis and to which one or more guide members 42b are secured. The deflector assembly 42 includes a pair of elongated guide members 42b spaced parallel from one another about and extending distally along the direction of the longitudinal axis A-A preferably interior to the inner housing 42c. Each of the guide members 42b includes a proximal end coupled to a portion of the interior of the inner housing 42c. Coupled to the distal ends of the guide members 42b is the deflector plate assembly 42a, thereby locating the deflector plate assembly 42a in a first position distal of the outlet 26. The guide members 42b are telescoping members relative to the inner housing 42c, thus permitting the deflector plate assembly 42a to extend distally from the first position to a second position distal of the first.

[0023] The deflector plate assembly 42a is shown, in-part, in dashed line corresponding to the second or deployed position. In this preferred operational position, the deflector plate assembly 42a presents an upper surface 56 and an opposite lower surface 58, each substantially orthogonal to the longitudinal axis A-A for distributing a fluid discharge from the outlet 26. In particular, the upper surface 56 provides a distribution surface for distributing a minimum flow rate discharged from the outlet 26.

[0024] Operation of the sprinkler 10 provides that, upon exposure to a heat source, such as a fire, generating sufficient heat to melt the solder tabs 52, the plate 18 falls away from the retaining sleeve 48. The deflector assembly 42 then drops from its first or non-deployed position to a second or deployed position. The solder holding the fusible link 38 melts under the exposure to the increasing heat, the halves separate to actuate the sprinkler and displace the closure assembly. Upon displacement of the closure assembly, fluid discharges from the outlet 26 over the protection area.

[0025] Accordingly, the sprinkler 10 can be tested in accordance with UL 1626, Section 26 to identify an acceptable minimum operational flow rate of discharge from the sprinkler 10 capable of distributing a flow of fluid over a horizontal surface in a rectangular test area such as, for example schematically shown in FIG. 7C, such that the application rate or density for any 0.092m^2 are (one square foot area (1 ft.^2)) within the test area shall be at least 0.81 litres per minute per square meter (0.02 gallons per minute per square foot) provided that no more than four - 0.092m^2 (one square foot areas ($4 \times 1\text{ ft}^2$)) in any given quadrant of the test area is at least 0.611 litres per minute per square meter (0.015 gallons per minute per square foot). More preferably, a preferred embodiment of the sprinkler 10 can be satisfactorily tested in accordance with UL 1626 so as to identify a minimum operational flow rate of 49.21 litres per minute (thirteen gallons per minute (13 gpm)) that results in a fluid distribution over a 23.81m^2 ($4.88\text{m} \times 4.88\text{m}$) (256 square foot area ($16\text{ ft.} \times 16\text{ ft.}$)) having a density of 2.04 litres per minute per square meter (0.05 gallons per minute per square foot (0.05 gpm/ft^2)). Even more preferably, the test is conducted so as to identify an actual minimum operating pressure for the preferred sprinkler 10, having a nominal K-factor of 4.9 and a minimum operational flow of 49.21 litres per minute (thirteen gallons per minute (13 gpm)) capable of producing a fluid distribution over a 23.81m^2 ($4.88\text{m} \times 4.88\text{m}$) (256 square foot test area ($16\text{ ft.} \times 16\text{ ft.}$)) at a density of 2.04 litres per minute per square meter (0.05 gpm/ft^2), to be about 48263 N/m^2 (seven pounds per square inch (7 psi.)). Moreover, the preferred embodiment of the sprinkler 10 further provides for the minimal flow of 64.35 litres per minute (seventeen gallons per minute (17 gpm)) in successful fluid distribution tests for a 29.92m^2 ($5.46\text{m} \times 5.47\text{m}$) (324 square feet area ($18\text{ ft.} \times 18\text{ ft.}$)), and a minimal flow of 75.71 litres per minute (twenty gallons per minute (20 gpm.)) for a 37.21m^2 ($6.1\text{m} \times 6.1\text{m}$) (400 square foot test area ($20\text{ ft.} \times 20\text{ ft.}$)).

[0026] In addition, the sprinkler 10 can be tested in accordance with UL 1626, Section 27 to identify an acceptable level of fluid

distribution from the sprinkler 10 capable of distributing a flow of fluid over a vertical surface in a rectangular test area such as, for example schematically shown in FIGS. 7A and 7B, such that walls within the test coverage area are wetted within 0.711 meter (twenty-eight inches (28 in.)) of the ceiling with the sprinkler 10 discharging water in a uniform manner at a specified design flow rate. In a square coverage or test area each wall within the coverage area shall be wetted with at least five percent (5%) of the sprinkler flow. For rectangular coverage or test areas, each wall within the coverage area shall be wetted within a proportional water amount based on twenty percent (20%) of the total sprinkler discharge in accordance with the following formula:

$$WW=20\% (D/P)$$

where:

WW = Required amount of water collected on a wall in percent

D = Wall length (ft.) and

P = Total perimeter of coverage area (ft.)

[0027] It is believed that the various features of the sprinkler 10 and its operational components allow for compliance with UL 1626 at the minimal flow and pressures described above. The deflector plate assembly 42a and the upper surface 56 preferably includes or defines one or more of surfaces substantially orthogonal to the longitudinal axis. More preferably, the deflector plate assembly 42a includes, as seen for example in FIG. 4B, a first centralized surface 43 spaced axially from the outlet 26, a second surface 45 preferably circumscribing the first surface 43 and spaced distally from the first surface 43. Even more preferably, the deflector plate assembly 42a includes a third surface 47 circumscribing the first and second surfaces 43, 45 and spaced distally from the second surface 45. The plurality of surfaces 43, 45, 47 provide a surface over which fluid discharged from outlet 26 can impact, deflect and flow for distribution beneath the sprinkler 10.

[0028] The deflector plate assembly 42a, as seen in FIGS. 4A and 4B includes the substantially flat plate member 78 and a projection member 60. The flat plate member 78 and projection member 60 collectively form the upper surface 56 and lower surface 58 of the deflector plate assembly 42a to distribute the flow of fluid from the outlet 26. For example, water discharged from the outlet 26 deflects off the surfaces of the flat plate member 78 and the projection member 60 to deflect the water axially and radially to further impact other elements of the sprinkler 10 such as the inner surface of the outer housing 14, the inner housing 42c and/or the guide members 42b so as to provide a sprinkler performance and water distribution characteristic acceptable under UL 1626.

[0029] The projection member 60 is preferably centrally located with respect to the plate member 78 and aligned with the longitudinal axis A-A. As seen in FIGS. 4A, 4B, the projection member 60 has a central core 62 having preferably a substantially planar proximal tip 63 and axially extending therefrom a substantially cylindrical body. The projection member 60 can include a member 64 extending radially from the core 62. More preferably, diametrically disposed about the core 62 are radially extending members 64. Alternatively, a plurality extending members can be radially disposed about the core 62 or further in the alternative, an enlarged flange can be circumscribed about the central core 62. The projection member 60 preferably includes an oblique or angled surface 66 extending contiguously from the core 62 to the radially extending members 64. The surface 66 can define an angle ranging from about twenty to thirty degrees (20°-30°) relative to the substantially planar surface and is more preferably about twenty-three degrees (23°) relative to the substantially planar surface. More preferably the projection member 60 is of integral or unitary construction in which the angled surface 66 is circumscribed about the longitudinal axis so as to define a substantially frusto-conical plane and further define a projection cone geometry. The planar tip 63 and radially extending members 64 respectively and preferably provide the first central surface 43 and the second surface 45 as described above.

[0030] The central core 62 of the projection member 60 is preferably engaged with the plate member 78. More preferably, the plate member 78 preferably includes a central bore 80 disposed about the substantially cylindrical body of the core 62. The plate member 78 preferably includes at least two lateral bores 82a and 82b disposed about the central bore 80. More preferably, the lateral bores 82a and 82b are aligned with and laterally spaced outside the radially extending members 64 as more clearly seen in FIG. 4A. The lateral bores 82a, 82b are preferably engaged or coupled to the preferred parallel guide members 42b so as to centrally locate the deflector plate assembly 42a along the longitudinal axis A-A distal of the outlet 26 as seen in FIG. 2. More specifically, the guide members 42b can include pin elements preferably fixedly disposed within the lateral bores 82a, 82b. The radially extending members 64 and the adjacent pin elements of the guide members 42b preferably provides a fluid flow surface or channel therebetween to distribute a fluid flow toward the flow distributing features of the plate member 78. The flow channels can provide for successful flow collection and wall wetting during UL 1626 testing. Referring again to FIG. 4A, the radially extending members 64 can include a void 65 defined at its lateral end adjacent to the guide member 42c through which a fluid

discharge can flow.

[0031] The plate member 78 is substantially oblong or oval in shape, preferably substantially disposed in a plane substantially perpendicular to the longitudinal axis A-A and defined by orthogonal plate axes IVB-IVB and VIC-VIC, as seen in the plan view of FIG. 4A. More specifically, the plate member 78 has a perimeter defining at least one arcuate edge 84 and one substantially straight edge 86. Preferably, the plate member 78 has a perimeter defining two diametrically opposed arcuate edges 84 intersecting the major plate axis IVB-IVB and two substantially parallel straight edges 86 opposed about the major plate axis IVB-IVB and orthogonal to the minor plate axis VIC-VIC. Preferably, the maximum spacing between the two parallel straight edges 86 along the minor axis VIC-VIC ranges from about 27.94mm (1.1 inches) to about 38.1mm (1.5 inches) and is preferably about 37.75mm (1.25 inches).

[0032] In one preferred embodiment of the plate member 78, a point along the defined arcuate edge 84 can further define a circle circumscribed about the longitudinal axis A-A. The defined straight edges 86 of the plate member 78 each further preferably define a chord length of the circle. Accordingly, the plate diameter defined by diametrically opposed points along arcuate edges 84 and merger axis IVB-IVB preferably ranges from about 31.75mm (1.25 inches) to about 38.1mm (1.5 inches) and is more preferably about 34.29mm (1.35 inches). Alternatively, the diameter defined by the plate member 78 can be a function of sprinkler height such the plate diameter to sprinkler height ratio ranges from about 0.5 to about 0.75 and is preferably about 0.70.

[0033] A preferred plate member 78 is shown in FIGS. 6A-6D without the projection member 60 engaged therewith. The plate member 78 includes an upper surface 78a and lower surface 78b each preferably parallel to the plane defined by the intersection of the major axis IVB-IVB and the minor axis VIC-VIC. More preferably, at least one of the upper and lower surfaces 78a, 78b has an angled portion, as seen for example in FIG. 6C and 6D, that is angled at an angle α relative to the plane defined by the intersection of the major axis IVB-IVB and the minor axis VIC-VIC. The angle α can range from about five degrees to about ten degrees (5° - 10°) and is more preferably about six degrees (6°). The angle α is preferably such that the lower surface is generally concave relative to the view from below the ceiling 200. More preferably, the angled portion is disposed at the outer perimeter of the plate member 78 thereby providing the plate member 78 with an angled lip. Even more preferably, the angle α of the upper surface 78a or the lower surface 78b is provided for only a portion of the plate member 78, for example, a radial span of about sixty degrees centered about the minor axis VIC-VIC. More specifically, the angled portion is preferably limited to the surface of the plate defining the diametrically opposed straight edges 86. Thus preferably, two angled portions of the plate member 78 are diametrically spaced apart about the major axis IVB-IVB, and more preferably define bend lines 79a and 79b. The bend lines 79a and 79b are preferably diametrically spaced at about one inch from one another, or more alternatively are spaced at length equivalent to about eight-three percent (83%) of the straight edge to straight edge width.

[0034] The angled portions of the plate member 78 are preferably configured to provide compliance with the wall wetting requirements Section 27 of UL and 1626. Moreover of the angled portions of the plate member 78 are preferably configured to minimize water spray overthrow and thus provide compliance with operation cold-soldering test of Section 22 of UL 1626 where a first preferred sprinkler 10 is actuated adjacent to a unactuated second preferred sprinkler 10 located at about 8 feet from the actuated sprinkler 10. Specifically, the straight edges 86 of the plate member 78 of the first sprinkler 10 can be spaced parallel the straight edge 86 in the plate member 78 of the second sprinkler 10. To satisfy the requirements of the test, while the first sprinkler 10 is discharging fluid at 689.47 kN/m^2 (100 psig) or more, the first sprinkler 10 cannot prevent the actuation of the second sprinkler 10 as the second sprinkler is being exposed to heat and flame, as provided for in Subsection 22.2 of UL 1626. At approximately 689.47 kN/m^2 (100 psig) or greater, it is believed that the fluid flowing radially along the surfaces of the plate member 78 has sufficient velocity to produce a downward flow separation at the angled portion of the plate member 78 and straight edges 86. Although the plate member 78 is preferably shown with the straight edges 86 and angular portion, any surface irregularity, geometry or treatment can be incorporated into the plate member 78 provided the surface irregularity can cause flow separation at fluid pressure of 689.47 kN/m^2 (100 psig) or greater so as to prevent wetting of adjacent sprinklers located 8 or more feet in the directions of the plane defined by the A-A and IVB-IVB axes without the diminishing the effectiveness of the fluid distribution pattern provided by the deflector assembly 42. Accordingly, the sprinkler 10 provides for a minimum sprinkler spacing of about 2.44 meter (eight feet). Maximum spacing between adjacent sprinkler is preferably equivalent to the length of the coverage area being covered by the sprinkler. Accordingly, where the sprinkler 10 is configured for a coverage areas of 4.88m x 4.88m (16 ft. x 16 ft.), 5.47m x 5.47m (18 ft. x 18 ft.), and 6.1m x 6.1m (20 ft. x 20 ft.) the maximum spacing is respectively: 4.88m (16 ft.), 5.47m (18 ft.), and 6.1m (20 ft.).

[0035] Shown generally in FIG. 4A and in greater detail in FIG. 6A, is the plate member 78 further including one or more slots 88 that define an opening or void extending from the upper surface 78a to the lower surface 78b to provide features for the distribution of a fluid flow. In addition, the slots 88 preferably initiate at the perimeter of the plate member 78 and extend radially toward the center of the plate member 78 to define a slot length L_s . Each of the slots 88 is preferably defined by a pair of spaced

apart walls extending in the direction of slot elongation so as to define a slot width W_s . The slot to width ratio $W_s:L_s$ can range from about 0.1 to about 0.15. The slot width W_s can vary along the length of the slot becoming wider or smaller at any portion of the slot along the slot length L_s . The walls defining the slots 88 can further taper relative to one or both of the upper and lower surfaces 78a, 78b or alternatively and more preferably be orthogonal to the upper and lower surfaces. Preferably, one or more of the slots 88 include a chamfer along at least a portion of at least one of the upper and lower surfaces 78a, 78b. The chamfers of sprinkler 10 can facilitate compliance with the flow collection requirements of the tests of UL 1626.

[0036] Any one of the slots 88 preferably includes a portion extending linearly so as to define a straight portion. The slot 88 can further include a non-linear portion, for example, defining a curve. More specifically, the spaced apart walls defining the slot 88 can curve along the slot length in a parallel fashion to define a curved slot. Alternatively, the walls defining the slot 88 can variably curve away and toward one another so as to substantially define an oblong shaped void in the plate member 78. Preferably, a portion of the walls defining the slot 88 curve relative to one another so as to define a circular bore or void along the slot 88. Accordingly, the slot 88 can be formed so as to include a linear portion and a non-linear portion in communication or continuous with the linear portion. Thus, the slot 88 can include a circular bore portion in communication with a straight portion. Moreover, the circular bore portion of the slot 88 can define a slot width that is greater than, or alternatively smaller than, the slot width of the straight portion. For example, as seen in FIGS. 6A, a slot 88 can include a straight portion 88a in communication with and terminating radially inward at tip defined by a circular bore portion 88b. The circular bore portion 88b can include a countersink or alternatively include a counterbore. Moreover the slot 88 can include a series of portions of varying geometry along its slot length. For example, a preferred slot 94, as seen for example in FIGS. 6A and 6D, can include a first straight portion 94a defining a slot axis, a second circular bore portion 94b having a center along the slot axis, and a third circular bore portion 94c having a center along the slot axis spaced from the center of the second circular bore portion 94b. Circular bore portion 94c preferably has a smaller diameter than the second circular bore portion 94b. Moreover, any one of circular bores 94b and 94c can include a countersink or a counterbore. Accordingly, the slot width W_s can vary along the slot length L_3 where, for example, the first straight portion 94a has a slot width, the second circular bore portion 94b has a second slot width greater than the first slot width and the third circular bore portion 94c has a third slot width smaller than the slot widths of the first straight and second circular bore portions 94a, 94b.

[0037] The plate member 78 includes one or more pairs of diametrically opposed slots 88. The plate member 78 includes one or more groups of diametrically opposed slots such as, for example, slot group 90, 92, 94 and 96. Each of the group of slots 90, 92, 94, 96 can vary from one another by varying any one of the previously described slot features. For example, the slot groups 90, 92, 94, 96 can each have a slot length L_s each defining a ratio relative to the maximum radius of the plate member 78. In one preferred embodiment of the plate member 78, for example each of the first group of slots 90 defines a first ratio of about 0.25, each of the second group of slots 92 defining a second ratio of about 0.41, each of the third group of slots 94 defining a third ratio of about 0.23, and the fourth group of slots each defining a fourth ratio of about 0.29. Additional features may distinguish the groups of slots where for example, the third group of slots 94 includes a circular bore portion as described above. Any given group of slots is preferably periodically radially disposed about the plate member 78. The angular spacing between slots can range from about 15° to about 120° depending upon the number slots in the group and/or the desired spacing relative to the major axis IVB-IVB and minor axis VIC-VIC. More preferably, the groups of slots are further evenly interposed among one another such that a slot of a one group and a slot of another group are angularly spaced apart by about fifteen degrees (15°).

[0038] The various components of the sprinkler 10 including the body 12, the outer housing 14, the cover plate assembly 16, and the components of the deflector assembly can be made from any material capable of being machined, shaped, formed or fabricated provided the material can provide the requisite thermal responsiveness and fluid distribution characteristics. Preferably, materials for construction of the sprinkler components include brass, bronze, nickel, copper, steel, stainless steel or any combination thereof.

[0039] Accordingly, the preferred deflector plate assembly 42a and its features as described above can, alone or in combination with the remainder of the deflector assembly 42 and/or the outer housing 14 can be part of the means for distributing fluid in a residential dwelling unit so that the sprinkler 10 is able to meet testing requirements of UL 1626. In the horizontal distribution test, UL 1626, Section 26 requires placing the selected sprinkler 10 over a protective area sub-divided into four quadrants with the sprinkler 100 placed in the center of the quadrants I-IV. A detailed layout of one quadrant is illustrated in Figure 7C. In this quadrant, water collection pans are placed over the quadrant (e.g., quadrant III) of the protective area so that each 0.093 square meter (square foot) of the quadrant is covered by collector pan of 0.093 square meter (one-square foot) area. For pendent sprinklers, the top of the collector pan is 2.44 meter (eight feet) below a generally flat ceiling of the test area, as seen for example in FIG. 7A. The coverage area CA is generally the product of a coverage width CW and length CL, as seen in FIG. 1C, and can be for example, 4.88m x 4.88m (16 feet by 16 feet), 5.47m x 5.47m (18 feet by 18 feet), or 6.1m x 6.1m (20 feet by 20 feet). The length L of the quadrant III is generally the one-half the coverage length CL and the width W is generally one-half the coverage width CW, where each 0.093 square meter (square foot) of the quadrant is covered by collection pans of 0.093 square meter

(one-square foot) area with the top of each collection being about 2.44 meter (eight feet) below a generally flat ceiling of the coverage area and the amount of fluid collected is at least 0.81 litres per minute per square meter (0.02 gallons per minute per square foot) for any of the collection pans except that no more than four collection pans for each quadrant receive at least 0.611 litres per minute per square meter (0.015 gallons per minute per square foot).

[0040] In accordance with the test, water or another suitable fire fighting fluid is supplied to the selected sprinkler 10 at a desired rate with the sprinkler 10 being tested via a one-inch internal diameter pipe with a T-fitting having an outlet at substantially the same internal diameter as the inlet 24 of the selected sprinkler 100. The duration of the test is twenty-minutes and at the completion of the test, the water collected by the collection pan CP (as delineated by the square like grid) is measured to determine if the amount deposited complies with the minimum density requirement for each coverage area.

[0041] As promulgated by Section 27 of UL 1626, a vertical fluid distribution test provides for an arrangement to determine the vertical fluid distribution of any sprinkler suitable for the protection of a dwelling unit. In the test arrangement for the residential pendent sprinkler 100, the sprinkler 100 is placed over a center of a coverage area CA at one-half the coverage length CL or width CW (Figures 7A and 7B) of the coverage area. A suitable fire-fighting fluid such as water is delivered to the sprinkler 10 at a specified flow rate with the sprinkler 10 being tested via a 25.5mm (one-inch) internal diameter pipe. Water collection pans of 0.093m² (one-square foot) area are placed on the floor against the walls of the test area so that the top of the pan is 2.083m (six feet, ten inches) below a nominally 2.44m (eight feet) height H generally flat ceiling. The duration of the test is ten minutes at which point the walls within the coverage area should be wetted to within 0.71m (28 inches) of the ceiling at the specified design flow rate. Where the coverage area is square, each of the four walls must be wetted with at least five percent of the sprinkler flow. Where the coverage area is rectangular, each of the four walls must be wetted with a proportional water amount collected that is generally equal to 20 percent times a total discharge of the sprinkler 10 at the rated flow rate of the residential fire sprinkler times the length of the wall divided by the perimeter of coverage area CA.

[0042] As utilized in this test, the deflector assembly 42 including the slots 88 of the plate member 78 is believed to allow the break up of the flow stream extending from the outlet 26 perpendicular to the frame arms 14 in order to meet a maximum 6.096m (20-foot) spacing between sprinklers in the operational test of Section 22 of UL 1626. The preferred plate member 78 in combination with the projection member 60 is believed to provide for a sufficient fluid distribution over the test coverage area perpendicular to the longitudinal axis A-A. Further, it is believed that the features described above in relation to the deflector assembly 42 allows the sprinkler 10 to provide an operating flow rate of 49.21 litres per minute (thirteen gallons per minute (13 gpm)) of water at an operating pressure of about 48263 N/m² (seven pounds per square inch gauge (7 psig.)) fed to the inlet 26 so that a density of at least 2.04 lpm/m² (0.05 gpm/ft²) of fluid is provided to a coverage area of 4.88m x 4.88m (16 feet by 16 feet) under at least the horizontal distribution test of UL 1626.

[0043] Moreover, the above described features provide a sprinkler performance in the preferred sprinkler 10 having a minimal operating flow of 64.35 litres per minute (seventeen gallons per minute (17 gpm)) in a successful fluid distribution and fire tests for a 29.92m² (5.47m x 5.47m) (324 square feet area (18 ft. x 18 ft.)), and a minimal operating flow of 75.71 litres per minute (twenty gallons per minute (20 gpm)) for a 37.21m² (6.1m x 6.1m) (400 square foot test area (20 ft. x 20 ft.)). More preferably, the sprinkler 10 can provide a minimal flow of 64.35 litres per minute (seventeen gallons per minute (17 gpm)) in successful fluid distribution and fire tests for a 29.92m² (5.47m x 5.47m) (324 square feet area (18 ft. x 18 ft.)) at an operating pressure of about 82737 N/m² (twelve pounds per square inch (12 psi.)), and further provide a minimal flow of 75.71 litres per minute (twenty gallons per minute (20 gpm.)) for a 37.21m² (6.1m x 6.1m) (400 square foot test area (20 ft. x 20 ft.)) at less than 117210 N/m² (seventeen pounds per square inch) and even more preferably at an operating pressure of about 115142 N/m² (16.7 psi.).

[0044] Besides the above described fluid distribution tests, actual fire tests can also be performed in accordance with Section 28 of UL 1626 for the preferred embodiments. In particular, a fire test can be performed with sprinkler 10 to limit the temperature in a location of the test area so as to satisfy the criteria of Section 28.1 of UL 1626. More specifically, a test area can be constructed with the preferred sprinklers 10 installed in accordance with Section 28.2 of UL 1626. Actual fire tests conducted with sprinkler 10 can limit temperatures for each rated spacing as specified by the installation requirements having no more than two sprinklers 10 operate, such that: (i) the maximum temperature three inches below the ceiling at the tested locations does not exceed 600°F (316°C); (ii) the maximum temperature 1.60 meters (five and one-quarter feet (5¼ ft.)) above the floor shall not exceed 93.3°C (200°F) nor exceed 54.4°C (130°F) for more than any continuous two minute period; and (iii) the maximum ceiling temperature 6.35mm (¼ inch) behind the finished ceiling surface shall not exceed 260°C (500°F).

[0045] As a preferably concealed pendent sprinkler, the sprinkler 10 provides for as much vertical adjustment ranging from

about 6.35mm (¼ inch) to about 19.05mm (¾ inch) and preferably about 12.7mm (½ inch) when installing the sprinkler in a sprinkler system 100 relative to a fixed pipe drop. This vertical adjustment can reduce the accuracy to which fixed pipe drops of system 100 must be cut to ensure a proper installation.

[0046] Finally, because the preferred embodiments of the sprinkler 100 are able to pass all of the performance tests required by UL 1626, the preferred embodiments are able to be listed by a listing authority, such as, for example, UL, for design and installation as a residential fire sprinkler, as defined in Section 3.6.2.10 of NFPA 13. The above described features of the preferred embodiment of the sprinkler 10 can, in a residential fire protection system, as per NFPA 13, 13D and 13R, provide an optimized fire protection at lower minimum design pressures for design protection area of 13.38m² (144 square feet) or greater. Consequently, at least the deflector assembly 42 alone or in combination with the other operational components of the sprinkler 10, preferably provides the means for distributing fluid over a coverage area of a residential dwelling unit. Thus, the sprinkler 10 can be installed in a preferably wet residential sprinkler system in accordance with the NFPA Standards to provide a suitable fluid density over a maximum coverage area of 23.78m² (256 square feet) or less in which the sprinkler 10 has a minimum discharge flow rate of about 49.21 litres per minute (thirteen gallons per minute (13 gpm)) and a minimum design or an operating pressure of about 48263N/m² (seven pounds per square inch) delivered to the sprinkler. In addition, the preferred sprinkler 10 can be installed in a residential sprinkler system for a maximum coverage area of about 29.92m² (324 square feet), given that the sprinkler 10 can deliver a minimum flow rate of about 64.35 litres per minute (seventeen gallons per minute (17 gpm)) at a minimum design pressure of about 82737 N/m² (twelve pounds per square inch (12 psi)) and further provide for a maximum coverage area of about 37.21m² (four hundred square feet (400 ft.²)) given that the sprinkler 10 can deliver a minimum flow rate of about 75.71 litres per minute (twenty gallons per minute (20 gpm)) at a minimum design pressure of about 11720 N/m² (seventeen pounds per square inch (17 psi)). More specifically, with the lower minimum operating design pressures, the preferred embodiments can be utilized in the design of fire protection system for coverage area of 29.92m² (324 square feet) or greater at approximately a fifteen percent lower design pressure than known residential fire sprinklers. Accordingly, the sprinkler 10 provides a preferred device and method for protecting a coverage area that can range from about 13.38m² (144 square feet) to about 37.21m² (400 square feet) by introducing a fire fighting fluid to the sprinkler body 12 at a minimum operating pressure ranging from about 48263 N/m² to 117210 N/m² (seven pounds per square inch to about seventeen pounds per square inch (7-17 psi)). The preferred device and method further provide for discharging the fluid from the sprinkler body 12 at a flow rate ranging from about 49.21 litres per minute to 75.71 litres per minute (thirteen gallons per minute to about 20 gallons per minute (13-20 gpm)) and distributing the fluid over the coverage area at a density of about 2.04 litres per minute per square meter (0.05 gallons per minute per square foot (0.05 gpm/ft²)).

[0047] One preferred embodiment of the sprinkler 10 is shown and described in Tyco Fire & Building Produce Data Sheet Series LFI Residential Congealed Pendent Sprinklers, Flat Plate 4.9 K (January 2006). Shown below is a tabulated summary of the minimum flow and residual pressures for the preferred sprinkler having a 71°C (160°F) temperature rating for various coverage areas. In addition, the preferred sprinkler can provide for a maximum working pressure of about 1206kN/m² (175 pounds per square inch (175 psi)).

Table 1

Maximum Coverage Area	Maximum Sprinkler Spacing m (feet)	Minimum Flow litres per min ute (gpm) & Residual Pressure N/m² (psi)
3.65 x 3.65 (12 ft. x 12 ft.)	3.65m (12 ft.)	49.21 1pm/48263 N/m ² (13 gpm. / 7 psi)
4.27 x 4.27 (14 ft. x 14 ft.)	4.27m (14 ft.)	49.21 1pm/48263 N/m ² (13 gpm. / 7 psi)
4.88 x 4.88 (16 ft. x 16 ft.)	4.88m (16 ft.)	49.21 1pm/48263 N/m ² (13 gpm. / 7 psi)
5.47 x 5.47 (18 ft. x 18 ft.)	5.47m (18 ft.)	64.35 1pm/82737 N/m ² (17 gpm. / 12 psi)
6.1 x 6.1 (20 ft. x 20 ft.)	6.1m (20 ft.)	75.71 1pm/115142 N/m ² (20 gpm./16.7 psi)

[0048] Table 1 provides for various maximum coverage areas for the preferred sprinkler 10 and further provides preferred

minimal flow rates and operating fluid pressure. The provided minimal flow rates and operating pressures can also be used for a sprinkler 10 used to protect a coverage area having dimensions less than or between those indicated so as to ensure adequate distribution density for the actual coverage area.

[0049] While the present invention has been disclosed with reference to certain preferred embodiments, numerous modifications, alterations, and changes to the described embodiments are possible without departing from the scope of the present invention, as described herein. Accordingly, it is intended that the present invention not be limited to the described embodiments, but that it have the full scope defined by the language of the following claims.

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- [EP0505672A2 \[0005\]](#)

Non-patent literature cited in the description

- Standard for Safety for Residential Sprinklers for Fire Protection Service Underwriters Laboratories Inc. (UL) 20031000 [\[0002\]](#)
- Tyco Fire & Building Produce Data Sheet Series LFI Residential Congealed Pendent Sprinklers Flat Plate 4.9 K, 2006, [\[0047\]](#)

Patentkrav

1. Boligsprinkler med pladeafdækning (10), der omfatter:
et legeme (12), der har en indvendig overflade (20), der
5 definerer en passage (22) til at transportere en væske,
hvilken passage (22) indbefatter en indgang (24) og en udgang
(26), der er anbragt i en indbyrdes afstand langs længdeaksen
(A-A) og definerer en K-faktor på omtrent 5;
en lukkeenhed (28), der støder op til udgangen (26) for at
10 lukke udgangen (26) til;
varmefølsomme støtteanordninger til at fastholde lukkeenheden
stødende op til udgangen (26);
en deflektorenhed (42), der indeholder en første position
distalt i forhold til udgangen (26) og en yderligere position
15 distalt i forhold til den første position, hvilken
deflektorenhed (42) indbefatter en plade (78);
et par af teleskopiske styreelementer (42b), der hver især har
en proksimal ende, idet den proksimale ende er forbundet med
legemet (12), og idet den distale ende af styreelementerne
20 (42b) er forbundet med pladen (78); og
en varmefølsom udløserenhed (38), der fastholder lukkeenheden
(28) stødende op til udgangen (26), hvor
deflektorenhedspladen (78) har en i det væsentlige oval ydre
omkreds med en første pladeakse (IVB) og en yderligere
25 pladeakse (VIC), idet afstanden mellem dele af den i det
væsentlige ovale ydre omkreds langs den første akse (IVB) er
større end afstanden mellem dele af den i det væsentlige ovale
ydre omkreds langs den yderligere akse (VIC), en flerhed af
diametralt modsatte par af riller (88), der er anbragt langs
30 den i det væsentlige ovale ydre omkreds, idet flerheden af
riller (88), der er anbragt på begge sider af den første
pladeakse (IVB) og den yderligere pladeakse (VIC) desuden
definerer en første rillegruppe, der har en første
rillelængde, og i det mindste en yderligere rillegruppe, der
35 har en yderligere rillelængde, der er mindre end den første
rillelængde; og
et fremspring (60), der er forbundet med pladen (78) i hver af
den første position distalt i forhold til udgangen (26) og den

yderligere position distalt i forhold til den første position; idet den distale ende af styreelementerne (42b) er forbundet med pladen (78) langs den første pladeakse (IVB) mellem parret af riller og stødende op til en kant, der udformer hver enkelt rille i hver enkelt par af riller; og idet udløserenheden (38) indeholder en smelteledenhed, der er anbragt i en afstand til fremspringet (60), når deflektorenheden (42) befinder sig i den første position, og

hvor deflektorenheden (42) fordeler en strøm af væske over et beskyttelsesområde, der ligger på mellem omtrent 13,38 m² (omtrent 144 engelske kvadratfod) og omtrent 37,16 m² (omtrent 400 engelske kvadratfod), idet væskefordelingen har en tæthed på i det mindste 2,037 liter pr. minut pr. m² (0,05 gallon pr. minut pr. engelsk kvadratfod (0,05 gpm/ft²)) for at definere et spektrum af minimale driftstryk, der ligger på mellem 48,26 kPa (syv pund pr. engelsk kvadrattomme) og omtrent 117,21 kPa (sytten pund pr. engelsk kvadrattomme (7-17 psi)) og et spektrum af minimale driftsvæskestrømme, der ligger på mellem omtrent 49,21 l/m (tretten gallon pr. minut) og omtrent 75,71 l/m (tyve gallon pr. minut (13-20 gpm)).

2. Sprinkler (10) ifølge krav 1, der desuden omfatter varmekølsomme pladeanordninger til at fastholde en minimal afstand mellem udgangen (26) og deflektorpladeenheden (42a);

hvor de varmekølsomme pladeanordninger omfatter en dækpladeenhed (16), der indeholder en dækplade (18) og et varmekølsomt fastgørelsesmiddel (52), der forbinder dækpladen (18) med et udvendigt kabinet, således at dækpladen (18) går i indgreb med deflektorenheden (47) og indeholder deflektorenheden (42) inden i det udvendige kabinet (14).

3. Sprinkler (10) ifølge krav 2, ved hvilken dækpladeenheden (16) omfatter:

en fastholdelsesbøsning (48), der indeholder en koblingsmekanisme til at forbinde dækpladeenheden (16) med det udvendige kabinet, hvilken fastholdelsesbøsning (48) har en indvendig overflade, der definerer en passage med en indgang og en udgang, der er placeret i en indbyrdes afstand langs

længdeaksen (A-A);

en plade (18), der er placeret stødende op til udgangen på fastholdelsesbøsningen (48) for at støtte og skjule i det mindste en del af anordningen til fordeling inden i passagen
5 på fastholdelsesbøsningen (48), hvilken plade indbefatter et varmfølsom koblingsstykke (52) til at forbinde pladen (18) med fastholdelsesbøsningen (48), der støder op til udgangen på fastholdelsesbøsningen (48).

10 4. Sprinkler (10) ifølge krav 1, ved hvilken deflektorenheden (42) har en første position distalt i forhold til udgangen (26), der definerer en minimal afstand mellem udgangen (26) på legemet (12) og deflektorenheden (42), og deflektorenheden (42) har en yderligere position distalt i
15 forhold til den første position, der definerer den maksimale afstand mellem udgangen (26) på legemet (12) og deflektorenheden (42).

5. Sprinkler (10) ifølge krav 1, ved hvilken
20 deflektorpladeenheden (42a) omfatter en flerhed af overflader distalt i forhold til udgangen (26) på legemet (12), hvilken flerhed af overflader indeholder en proksimal overflade (78a), en distal overflade (78b) og i det mindste en mellemliggende overflade, der er placeret mellem den proksimale og den
25 distale overflade (78a, 78b).

6. Sprinkler (10) ifølge krav 1, ved hvilken pladen (42a) definerer et midtpunkt langs længdeaksen og en maksimal radius, der er afgrænset rundt om midtpunktet for at definere
30 en cirkel, hvilken plade har et første par af diametralt modsatte kanter (84), der er placeret langs cirklen, og et yderligere par af diametralt modsatte kanter (86), der hver især definerer en korde af cirklen.

35 7. Sprinkler (10) ifølge krav 1, ved hvilken fremspringet (60) har en kerne (62), der flugter med længdeaksen (A-A), og i det mindste et lateralt element (64), der strækker sig i radial retning fra kernen (62).

8. Sprinkler (10) ifølge krav 1, ved hvilken i det mindste en ud af flerheden af riller (88) på pladen indbefatter en første del (88a), der har en første rillebredde, og en
5 yderligere del (88b), der har en yderligere rillebredde, der adskiller sig fra den første rillebredde.

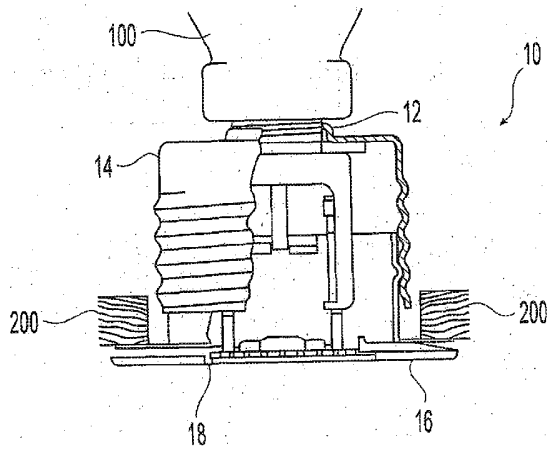
9. Sprinkler (10) ifølge krav 8, ved hvilken pladen (78) indbefatter en øvre overflade (78a) og en nedre overflade
10 (78b), idet i det mindste en ud af den øvre og den nedre overflade (78a,78b) indbefatter en første del, der er placeret i et første plan, og en yderligere del, der er placeret i et yderligere plan, der befinder sig i en vinkel i forhold til det første plan.

15 10. Sprinkler (10) ifølge et hvilket som helst af kravene 1 til 9, ved hvilken beskyttelsesområdet er på omtrent $23,78 \text{ m}^2$ (256 engelsk kvadratfod (256 ft^2)), den minimale driftsvæskestrøm er på omtrent $49,21 \text{ l/m}$ (tretten gallon pr. minut (13 gpm)) og det minimale driftstryk er på omtrent $48,26 \text{ kPa}$ (syv pund pr. engelsk kvadrattomme (12 psi)).

25 11. Sprinkler (10) ifølge et hvilket som helst af kravene 1 til 9, ved hvilken beskyttelsesområdet er på omtrent $30,10 \text{ m}^2$ (324 engelsk kvadratfod (324 ft^2)), den minimale driftsvæskestrøm er på omtrent $64,35 \text{ l/m}$ (sytten gallon pr. minut (17 gpm)) og det minimale driftstryk er på omtrent $82,73 \text{ kPa}$ (tolv pund pr. engelsk kvadrattomme (12 psi)).

30 12. Sprinkler (10) ifølge et hvilket som helst af kravene 1 til 9, ved hvilken beskyttelsesområdet er på omtrent $37,16 \text{ m}^2$ (400 engelsk kvadratfod (400 ft^2)), den minimale driftsvæskestrøm er på omtrent $75,71 \text{ l/m}$ (tyve gallon pr. minut (20 gpm)) og det minimale driftstryk er på omtrent
35 $117,21 \text{ kPa}$ (sytten pund pr. engelsk kvadrattomme (17 psi)).

DRAWINGS

*Fig. 1*

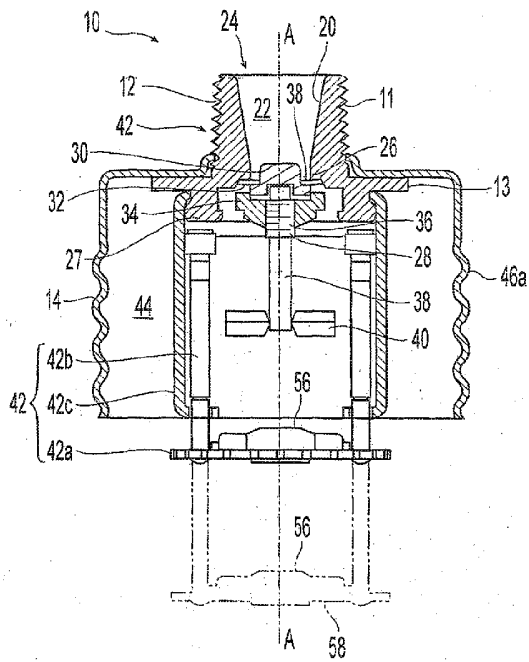


Fig. 2

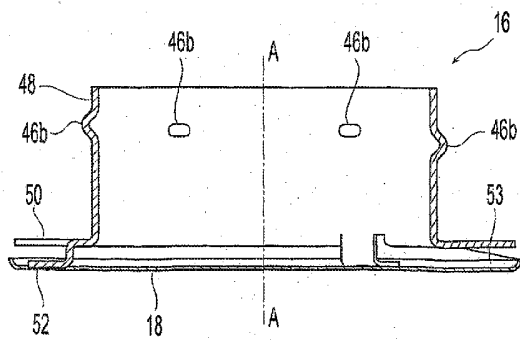


Fig. 3

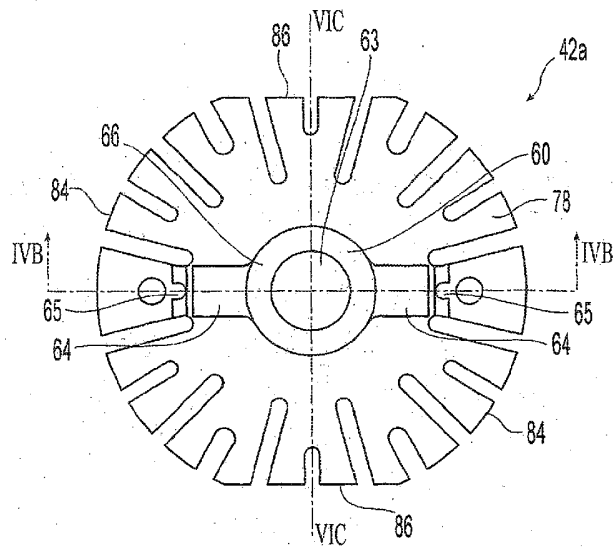


Fig. 4A

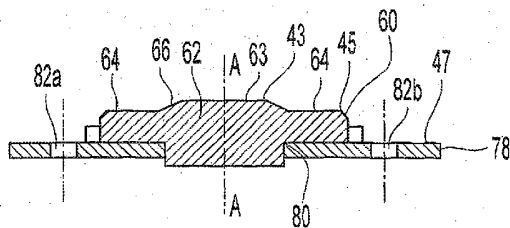


Fig. 4B

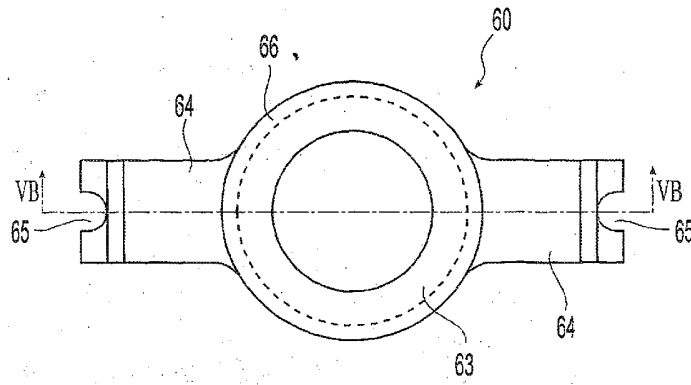


Fig. 5A

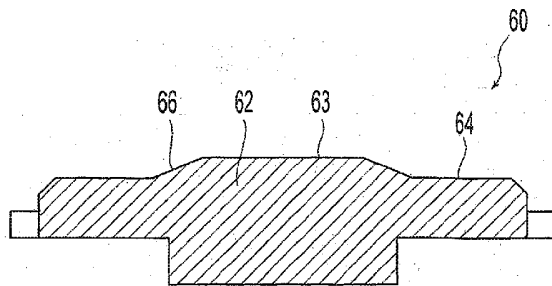


Fig. 5B

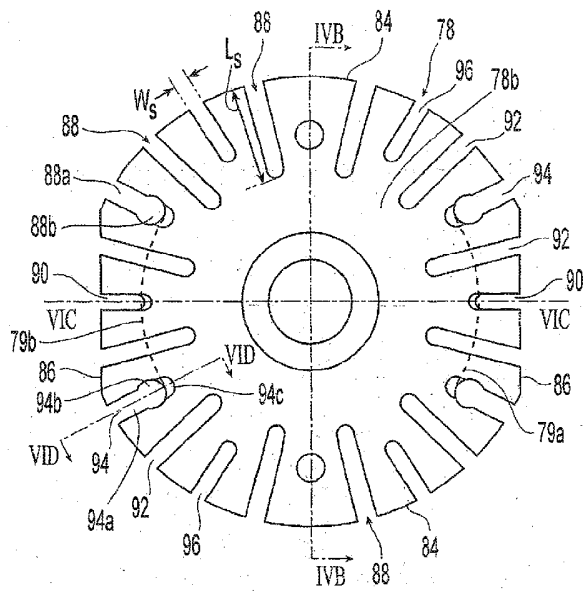


Fig. 6A

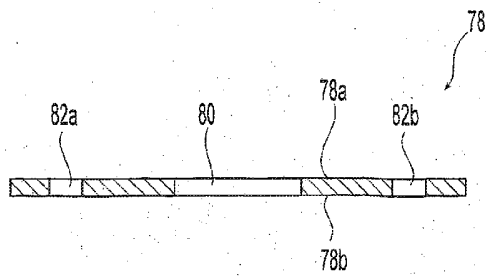


Fig. 6B

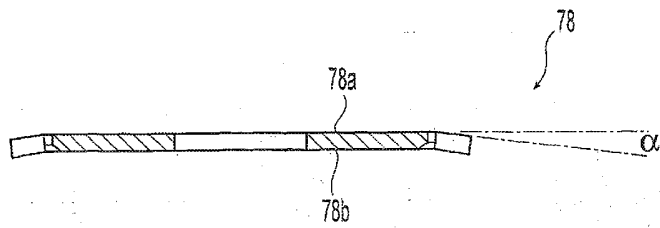


Fig. 6C

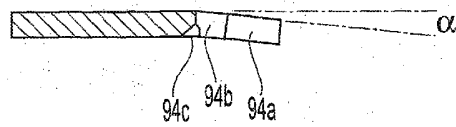


Fig. 6D

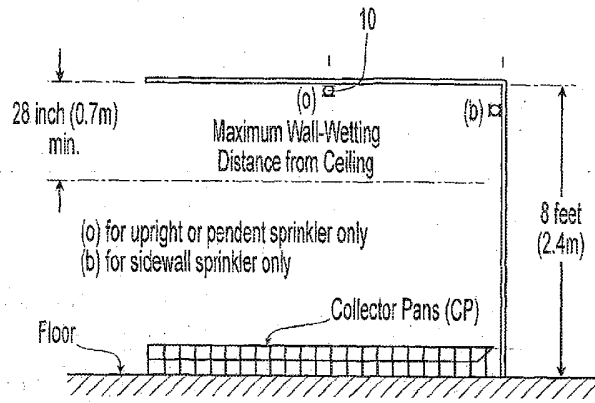


Fig. 7A

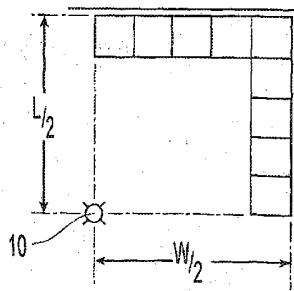


Fig. 7B

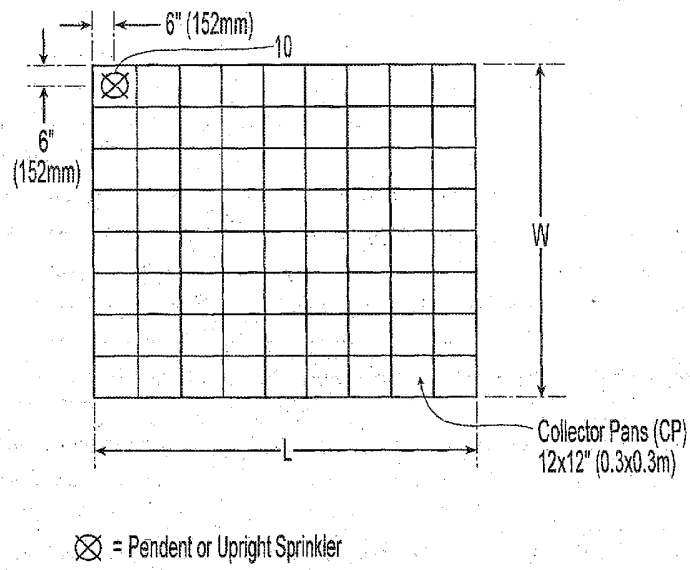


Fig. 7C