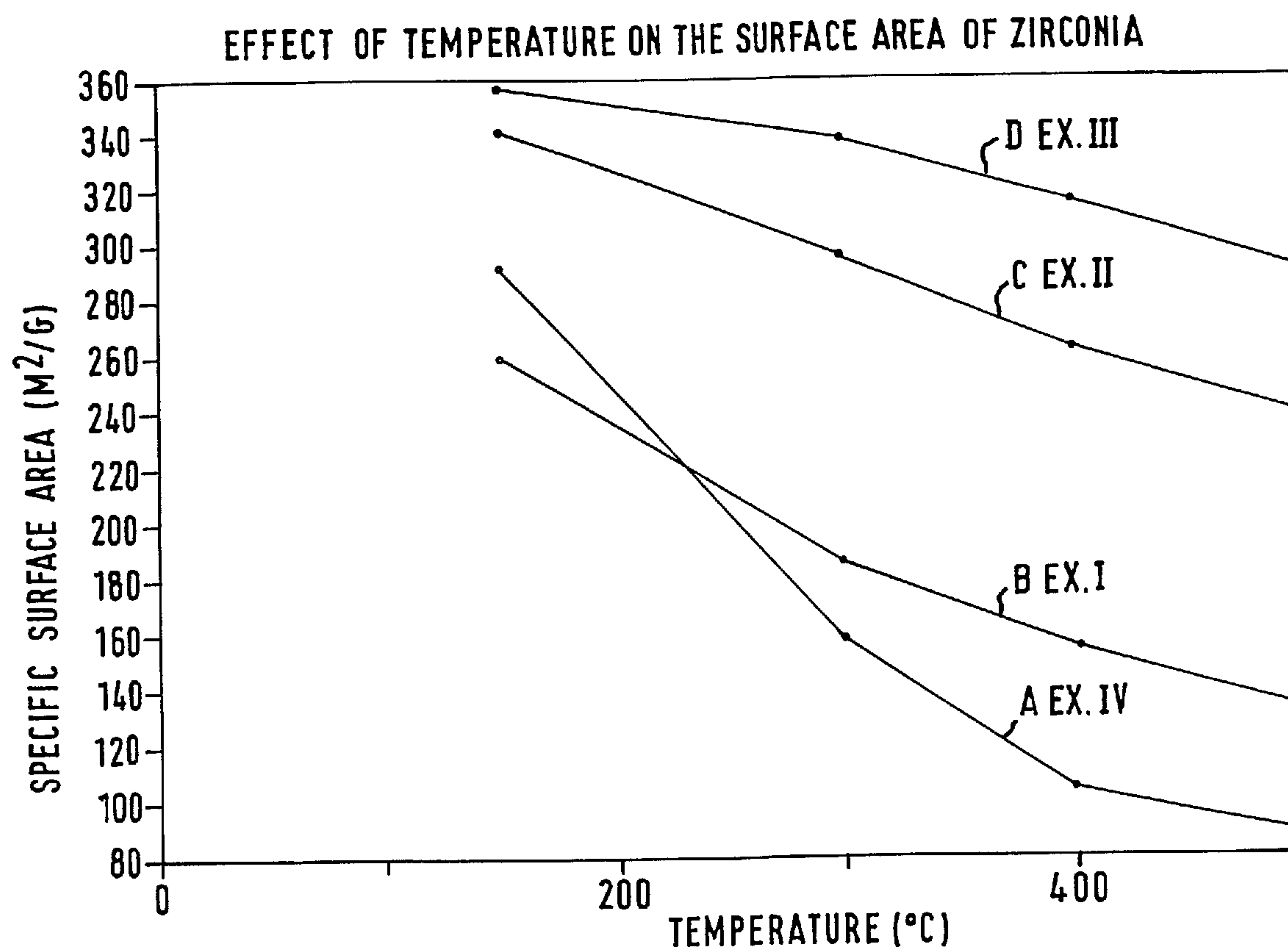




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(54) Titre : ZIRCONNE GRANDE SURFACE
(54) Title: HIGH SURFACE AREA ZIRCONIA



(57) **Abrégé/Abstract:**

High surface area zirconia, having a surface area after calcination, is obtainable by a process comprising aging zirconium hydroxide in the presence of an acid of an element of Group V or VI of the Periodic Table of Elements and calcining the zirconium material so-obtained. The preferred acid is phosphoric acid, in particular orthophosphoric acid. A high surface area zirconia is provided having a surface area of at least 180m²/g after calcination at a temperature of 300 °C.



A B S T R A C T

HIGH SURFACE AREA ZIRCONIA

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HIGH SURFACE AREA ZIRCONIA

The present invention relates to high surface area zirconia and to a process for producing such zirconia.

A process for the preparation of zirconia is known from French patent No. 2,590,887 (FR 2,590,887), which
5 discloses the use of an additive to obtain a relatively high surface area zirconia. The product retains a relatively high surface area after sintering (calcination), that is the state in which it is used as a catalyst or a catalyst support. The additives
10 disclosed in FR 2,590,887 are the oxides of silicon, rare earth metals and aluminium, and are used in an amount of about 1 to 10 %wt, preferably 2 to 5 %wt. A simple mixing process may be used in the preparation, resulting in an intimate mixture of the zirconia and
15 the oxides. Coprecipitation of a zirconium oxide precursor with the precursors of the additives mentioned is also suitable. The preferred method of preparation disclosed in FR 2,590,887 is the impregnation of zirconium oxide with a solution of at
20 least one salt precursor of the additives. The highest specific surface area achieved in FR 2,590,887 was 90 m²/g after a treatment at 400 °C. Treatments at a higher temperature resulted in lower specific surface areas. One of the examples of FR 2,590,887 is a
25 comparative example and used no additives. The specific surface area reached in the comparative example was 80 m²/g after a heat treatment at 400 °C and 20 m²/g after a heat treatment at 900 °C.

US patent No. 4,440,875 (US 4,440,875) discloses a
30 process for the production of hydrocarbons from

synthesis gas wherein a catalyst consisting of zirconium oxide promoted with at least one alkali metal compound is used. Preferably the zirconium oxide has a specific surface area in the range from 20 to 500 m²/g.

5 The only example, however, describes a specific surface area of just 122 m²/g resulting after a calcination step carried out in air for 2 hours at 450 °C. The catalyst was obtained by dissolving zirconium oxychloride in water and gradually adding ammonia to
10 the solution until the pH value of the solution was in the range from 7 to 10. The precipitated zirconium hydroxide was separated from the solution by filtration and washed. The filtration residue was subsequently calcined.

15 The Journal of Physic. Chem. Institute 24-06-85 of the Soviet Union describes the production of zirconium dioxide with a high specific surface area by treating a solution of zirconium nitrate with ammonia and washing, separating and drying the resulting gel. The product
20 was then heated for 2 to 10 hours at 150° to 175 °C under a steam pressure of 6 to 10 atm. The specific surface area is stated to have been 105 m²/g.

US patent No. 4,822,575 (US 4,822,575) teaches a process for the preparation of zirconium compositions
25 which upon calcination form zirconia. The zirconium compositions are said in US 4,822,575 to be prepared by the addition of an ammonia source to an aqueous zirconium sulphate solution to give a solution pH in the range of from 0.1 to 2.5.

30 A general conclusion to be drawn from the several disclosures discussed above is that heretobefore it has been very difficult to prepare a zirconia product having a specific surface area after sintering (calcination) of greater than 100 m²/g. In general the

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surface area was 80 to 100 m²/g, the highest surface area achieved being 122 m²/g.

Most surprisingly, there has now been found a novel process which can yield zirconia products having a surface area
5 after calcination of greater than 125 m²/g. It has been found that, unlike the processes of the prior art, zirconia having a surface area after calcination of in excess of 150 m²/g and even in excess of 200 m²/g can be conveniently prepared.

Accordingly, in a first aspect the present invention
10 provides a process for the preparation of high surface area zirconia comprising aging zirconium hydroxide in the presence of an acid of an element of Group V or VI of the Periodic Table of Elements and calcining the zirconium material so-obtained.

The invention further provides a process for the
15 preparation of zirconia comprising aging zirconium hydroxide, which zirconium hydroxide has been prepared by precipitation from a solution of a zirconium salt by the addition to the solution of an alkali or ammonium compound, in the presence of an acid of an element of Group V or VI of the Periodic Table of
20 Elements for at least 0.25 hours at a temperature from 0 to 100 °C and calcining the zirconium material so obtained for at least 0.5 hours at a temperature above 250 °C.

The acid is preferably an oxygen-containing acid. The acids of elements in Group V of the Periodic Table are
25 preferred acids, in particular the acids of phosphorous, nitrogen and sulphur, especially phosphorous.

Oxygen-containing phosphorous acids which may be used in the process include orthophosphoric, metaphosphoric, hypophosphoric and pyrophosphoric acid. Orthophosphoric acid

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is especially preferred. A mixture of two or more acids may also be employed to age the zirconium hydroxide.

Calcination is suitably carried out at elevated temperature, for example at a temperature above 250 °C, preferably above 300 °C, more preferably above 350 °C, still more preferably of from 450° to 550 °C. Calcination is preferably conducted for a period of at least 0.5 hour, preferably from 1 to 4 hours, typically about 2 hours. The calcination is preferably carried out using an oxygen containing gas, especially air.

However, inert gases, for example nitrogen, helium and argon, may also be used.

5 The duration of the aging of the zirconium hydroxide in the presence of the acid is not critical, provided a minimum duration of about 0.25 hours is observed, and is preferably in the range of from 0.25 to 48 hours, more preferably in the range of from 0.5 to 24 hours.

10 The zirconium hydroxide is contacted with a sufficient amount of the acid so as to age the zirconium hydroxide. Preferably, the acid is present in a solution having a molar concentration in the range of from 0.1 to 4, more preferably 0.2 to 3.5, especially 0.25 to 3. Acid in a molar concentration of at least 15 0.5 gives particularly good results.

The aging may be conducted at any suitable temperature, preferably in the range of from 0° to 100 °C, more preferably from 20° to 40 °C. Ambient temperature is a most convenient temperature for the 20 aging.

In a preferred embodiment, the zirconium hydroxide for use in the process is prepared by precipitation from a solution of a zirconium salt by the addition to the solution of an alkali or ammonium compound. Thus, 25 the present invention provides a process comprising mixing a solution of a zirconium salt with an alkali or ammonium compound to yield a precipitate, the precipitate then being aged in the presence of one or more oxygen-containing acids of an element of Group V or VI of the Periodic Table of Elements, and sub- 30 sequently calcined.

The zirconium salt may be any zirconium compound soluble in the selected solvent. Typical zirconium salts include zirconium nitrate, zirconium sulphate and 35 zirconium chloride; ammonium zirconium salts, for

example ammonium zirconium carbonate; and zirconyl salts, for example zirconyl chloride.

Any suitable solvent may be used to form the solution of the zirconium salt, including polar solvents, for example ethanol, glycol and water and mixtures thereof. Water is a most convenient solvent.

Suitable alkali or ammonium compounds for mixing with the solution of the zirconium salt include urea, hexamethylene tetraamine, (both generating hydroxyl ions by hydrolysis), ethanolamines, and alkali metal hydroxides, for example sodium and potassium hydroxide. Preferably, a solution of ammonia is used. The quantity of alkali or ammonium compound mixed with the solution of the zirconium salt should be sufficient to cause precipitation.

The zirconium hydroxide precipitate is separated from the solution of the zirconium salt, conveniently by filtration.

The presence of alkali compounds in the final zirconia product may be deleterious to the performance of the product as a catalyst or catalyst carrier. Accordingly, it may be preferred to wash the precipitate once or a plurality of times. The precipitate is most conveniently washed with water. Washing is carried out after filtration of the solution of the zirconium salt, but preferably prior to calcination of the aged material.

The precipitate product obtained can be dried after aging prior to sintering (calcination) if desired, although drying is not strictly necessary. Suitable drying techniques are well known in the art.

The zirconia produced by the process of the present invention is particularly useful as a catalyst or as a catalyst support. In particular, the zirconia may be used as a catalyst or catalyst support in a

process for the preparation of hydrocarbons from synthesis gas (a mixture of carbon monoxide and hydrogen). Thus, in a further aspect the present invention provides a process for the preparation of the hydrocarbons from synthesis in which a catalyst is employed, which catalyst comprises zirconia prepared by a process as hereinbefore described.

The zirconia may itself act as a catalyst for certain reactions, or, alternatively may be mixed with oxides of catalytically active materials, for example manganese, zinc, copper, cobalt and/or chromium. The zirconia is suitable for use in the iso-synthesis process.

It has been found that an essential difference between the zirconia of the prior art and zirconia prepared according to the process as hereinbefore described is that the amorphous structure of the latter material is substantially maintained during the calcination. Further, it appears that the acidity of the material prepared by the present process is considerably higher, as apparent from the adsorption of an excess of ammonia by the material and an increase in the temperature at which desorption is measured. The adsorption capacity of the zirconia product of the present process is about three times that of hitherto known zirconia, with the desorption occurring at 325 °C instead of 200 °C as with zirconia of the prior art.

Accordingly, in a further aspect the present invention provides a high surface area zirconia obtainable by a process as hereinbefore described. Zirconia having a surface area after calcination of greater than 125 m²/g. It has been found that a high surface area zirconia can be obtained, which material retains a markedly higher surface area after calcination at high temperatures than hitherto known

zirconia products. Thus, the present invention also provides a high surface area zirconia having a surface area of at least $180\text{m}^2/\text{g}$, in particular at least $230\text{m}^2/\text{g}$, after calcination at a temperature of 300°C .

5 The present invention is further described, by way of example only, in the following specific Examples, in which Examples 1, 2 and 3 illustrate processes and products of the present invention.

Example 1

10 1 l of 0.25 M zirconium solution (produced by dissolving 66.10 g of $\text{ZrO}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$ in demineralised water and diluting to 1 l, resulting in an 0.25 molar solution) was brought into a glass reactor equipped with a double wall for temperature control and baffles to ensure effective mixing. Whilst stirring, ammonia
15 (10% aqueous solution) was added dropwise at a rate of 1.35 ml/min. During the addition, the pH value increased from 0.9 to 8.5. The solution was stirred for a further 0.5 hours whereby the pH value decreased to 8.4. The resulting solution was filtered and the
20 precipitate washed three times with 1 l of demineralised water by repeated suspension and filtering.

Subsequently 109.4 g of the wet precipitate (LOI=90.62%) was suspended in 100 ml of 0.25 molar
25 aqueous phosphoric acid (H_3PO_4) solution and stirred for 24 hours. The solid material was filtered and washed on the filter with water. The resulting solid was dried at 120°C .

Example 2

30 The general process of Example 1 was followed, with the exception that the wet precipitate obtained was suspended in 100 ml of 0.5 molar aqueous phosphoric acid (H_3PO_4) solution and stirred for 24 hours.

Example 3

The general process of Example 1 was followed, with the exception that 116.12 g of the wet precipitate (LOI=88.7%) was suspended in 100 ml of 1 molar aqueous phosphoric acid (H_3PO_4) solution and stirred for 24 hours.

Example 4

A zirconyl nitrate solution was produced by dissolving 71.04 g of zirconyl nitrate in demineralised water, the solution being diluted with demineralised water to 1 l, to give a 0.25 M zirconium solution. 50 ml of the zirconium solution was introduced into a 1 l reactor and 50.0 g of urea was added. Whilst stirring, the solution was heated to 90 °C in about 1.5 hours, during which the pH value decreased from 2.2 to 1.0. Stirring at 90 °C was maintained for about 16 hours, at which point the pH sharply increased to 6.5 (final pH value). After 24 hours the process was stopped. The precipitate was filtered and washed three times with demineralised water by repeated suspension and filtration. The resulting solid was dried at 120 °C.

Evaluation of the products obtained in Examples 1 to 4.

The products obtained in Examples 1 to 4 were evaluated by heating the products for 1 hour at temperatures of 150°, 300°, 400° and 500 °C. The results are indicated in the Figure, in which curve A indicates the product of Example 4, curve B indicates the product of Example 1, curve C indicates the product of Example 2 and curve D indicates the product of Example 3.

As can be seen from the Figure, the aging of zirconium hydroxide by contact with phosphoric acid resulted in a marked increase in the surface area and surface area stability of the product, particularly at

higher temperatures. It can also be seen that an increase in the molar concentration of the phosphoric acid from 0.25 to 0.5 and 1 (curves B, C, and D respectively) in the aging step resulted in a marked increase in the surface area of the product after heating.

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CLAIMS:

1. A process for the preparation of zirconia comprising aging zirconium hydroxide, which zirconium hydroxide has been prepared by precipitation from a solution of a zirconium salt
5 by the addition to the solution of an alkali or ammonium compound, in the presence of an acid of an element of Group V or VI of the Periodic Table of Elements for at least 0.25 hours at a temperature from 0 to 100 °C and calcining the zirconium material so obtained for at least 0.5 hours at a temperature
10 above 250 °C.
2. A process according to claim 1, characterized in that the acid is an oxygen containing acid.
3. A process according to either of claims 1 or 2, characterized in that the acid is an acid of phosphorus.
- 15 4. A process according to claim 3, characterized in that the acid is orthophosphoric acid.
5. A process according to any one of claims 1 to 4, characterized in that the acid is present in a molar concentration in the range of from 0.25 to 3.
- 20 6. A process according to any one of claims 1 to 5, characterized in that the zirconium hydroxide is aged for a period in the range of from 0.25 to 24 hours.
7. A process according to any one of claims 1 to 6, characterized in that calcination is conducted at a temperature
25 of above 300 °C.
8. A process according to any one of claims 1 to 7, characterized in that the alkali or ammonium compound is ammonia.

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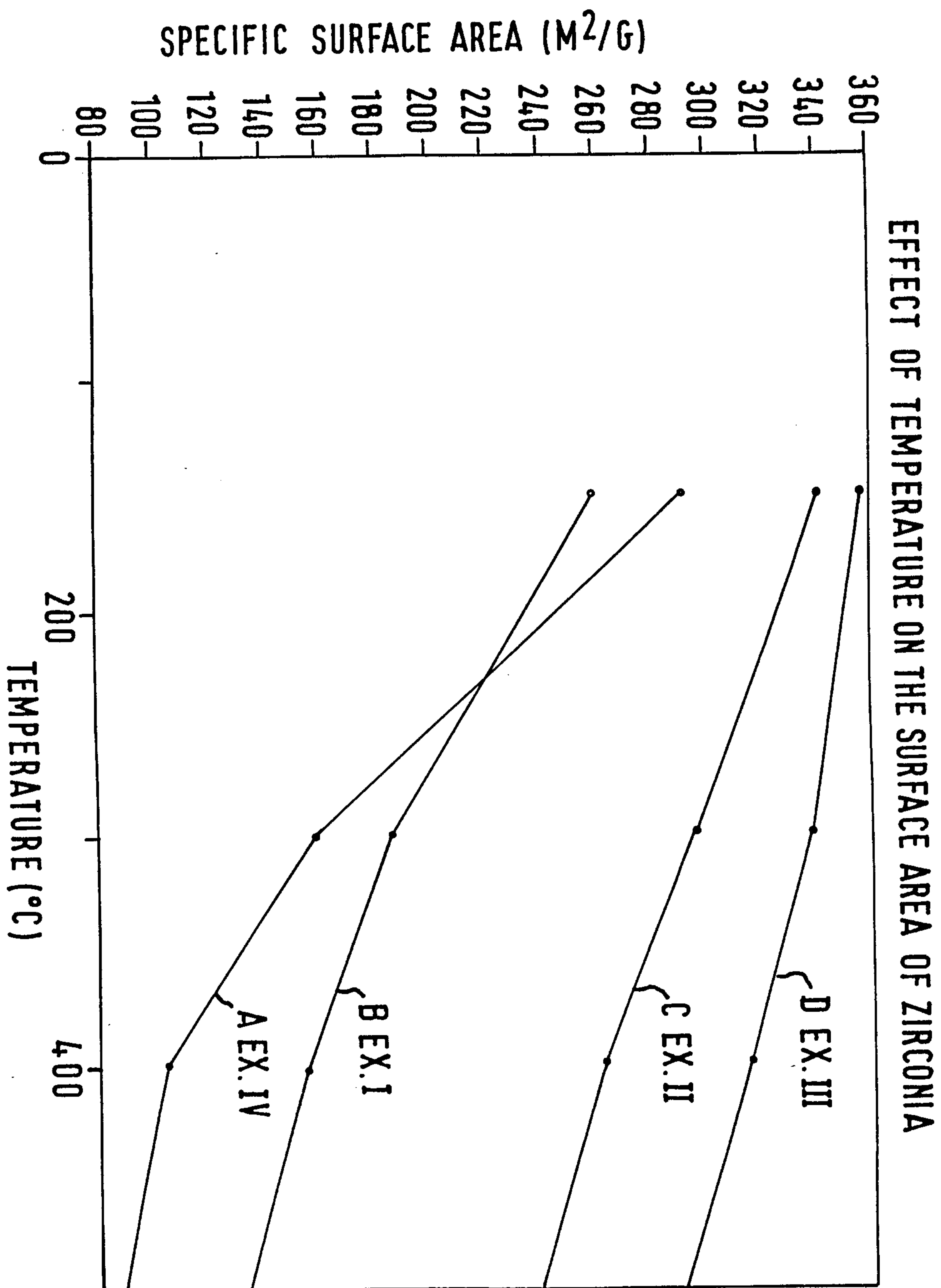
9. High surface area zirconia obtainable by a process according to any one of claims 1 to 8, having a surface area of at least 230 m²/g after calcination at a temperature of 300 °C.

10. Use of a high surface area zirconia according to claim 9 as a catalyst or catalyst support in a process for the preparation of hydrocarbons from synthesis gas.

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PATENT AGENTS



Patent Application
1998-05-20

EFFECT OF TEMPERATURE ON THE SURFACE AREA OF ZIRCONIA

