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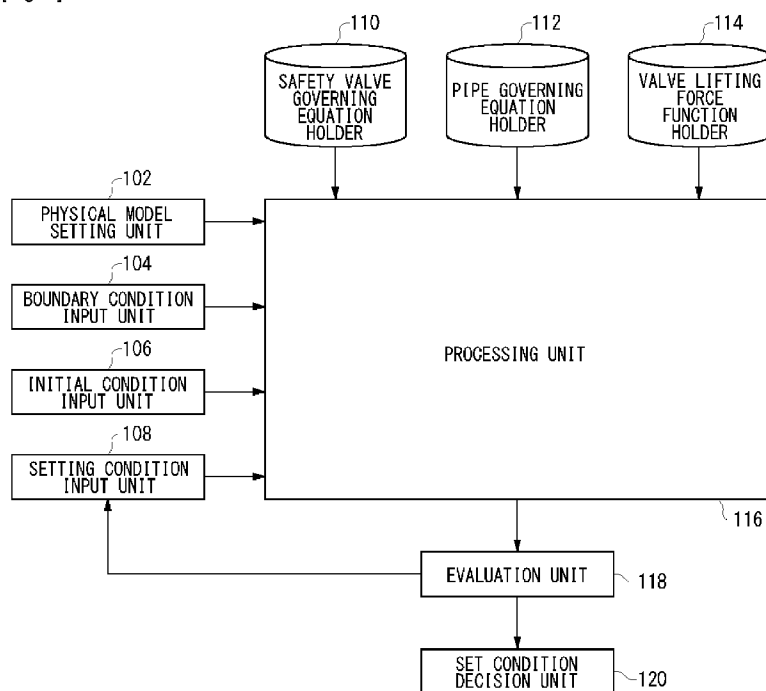
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[Continued on next page]

(54) Title: SAFETY VALVE VIBRATION ANALYZER

[Fig. 1]



(57) Abstract: The safety valve vibration analyzer (100) includes: a set condition input unit (108) in which set conditions of a physical model including a safety valve and an upstream pipe connected to the safety valve are inputted; a safety valve governing equation holder (110) that holds a safety valve governing equations; a pipe governing equation holder (112) that holds a pipe governing equation; a processing unit (116) that derives a time variation of a valve lift by using the set conditions inputted, the safety valve governing equations, and the pipe governing equations; and a valve lifting force function holder (114) that holds a valve lifting force function. The processing unit (116) derives the time variation of the valve lift by applying the valve lifting force function to the equation of motion of the valve disc.



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Description

SAFETY VALVE VIBRATION ANALYZER

Technical Field

[0001] The present invention relates to a safety valve vibration analyzer that analyzes vibration of a valve disc in a safety valve.

Background Art

[0002] A safety valve is a safety device that operates automatically when the pressure of an internal fluid rises abnormally, and used for protecting boilers, pressure vessels and pipes or the like. A spring loaded safety valve has a structure in which a valve disc is pressed against a valve seat by the spring. When the pressure of an internal fluid exceeds a set pressure, the valve is opened with an valve lifting force exerted thereon by the pressure of the fluid, becoming larger than the spring load, thereby the internal fluid being released outside the system and an excessive pressure being prevented. On the other hand, when the pressure of the internal fluid falls, a spring loaded safety valve is closed with the spring load becoming larger than the valve lifting force. A spring loaded safety valve is extremely reliable in its operation, because it has a simple mechanism with moving part of a spring and a valve disc.

[0003] Because the valve disc is supported by the spring, a spring loaded safety valve is sometimes unstable in the relation between the spring load and the pressure of the internal fluid, causing vibration with the valve disc repeating opening and closing. Vibration of the valve disc may cause pressure pulsation in a pipe, as well as damages from hitting between the valve disc and the valve seat, leaks from the valve seat, and abrasion of the valve sliding part Therefore, various studies have been made with respect to the vibration of a safety valve (see, for example, Non-Patent Documents 1 and 2.)

[Non Patent Citation 1] I.Harris and R.E.Lewis and T.A.Burton, "Dynamic Simulation of Safety Valve Installations", AIChE Symp.Ser., Vol.80, and No.236, 171-178, 1984

[Non Patent Citation 2] P.Coppolani, J.M.Henry, P.Caumette, J.L.Huet and M.Lott, and "Stability of Self Actuating Safety Valves in Liquid Service", Trans.Int.Conf.Structural Mech.Reactor Tech., Vol.9, No.F, 3-16, 1987

Disclosure of the Invention

[0004] Conventionally, the vibration of a safety valve has been thought to occur mainly due to an excessive pressure loss in an upstream pipe and a downstream pipe connected to the safety valve. However, the present inventor has, while analyzing the causes of vibration of an safety valve, considered whether there might be any cause other than

the pressure loss, and carried out experiments to check the existence of vibration when varying the length of an upstream pipe connected to a safety valve.

[0005] As a result of the above experiments, the present inventor has learned that vibration of a safety valve occurs more easily when the length of an upstream pipe is short rather than when it is long. According to a conventional theory, vibration of a safety valve is difficult to occur when the length of an upstream pipe is short, because the pressure loss is proportional to the length of a pipe. As understood from this, a conventional technique for analyzing the vibration of a safety valve is insufficient to accurately analyze the vibration of a safety valve and a practical analysis technique is not yet to be established.

[0006] In view of these circumstances, a general purpose of the present invention is to provide a safety valve vibration analyzer preferably capable of analyzing the vibration of a valve disc in a safety valve.

Means for Solving the Problem

[0007] For solving the aforementioned problem, a safety valve vibration analyzer according to an embodiment of the present invention, is for analyzing the vibration of a valve disc in a safety valve, and comprises: an input unit in which a set conditions of a physical model including a safety valve and an upstream pipe connected to the safety valve is inputted; a first holder that holds a safety valve governing equations including an equation of motion of the valve disc, a flow equation at the safety valve inlet, a flow equation at the safety valve outlet, and a mass conservation equation in a valve box; a second holder that holds a pipe governing equations including a mass conservation equation, an energy equation, and an equation of motion of a fluid flowing the upstream pipe; a processing unit that derives a time variation of a valve lift by using the set conditions inputted in the input unit, the safety valve governing equations held in the first holder, and the pipe governing equations held in the second holder; and a third holder that holds a valve lifting force function representing the relation between a lift and a valve lifting force exerting on the valve disc. The processing unit reads the valve lifting force function from the third holder and derives the time variation of the valve lift by applying the valve lifting force function to the equation of motion of the valve disc.

[0008] According to this embodiment, the equation of motion of the valve disc is properly represented by applying the valve lifting force function to the equation of motion of the valve disc, allowing the vibration of a valve disc in a safety valve to be accurately analyzed.

[0009] The valve lifting force function may be created by measuring the relation between the valve lift (disk displacement from closed position) and the valve lifting force.

[0010] The processing unit may derive the time variation of the valve lift by using the

equation of motion of the valve disc including the ratio of an orifice flow coefficient to an orifice critical flow coefficient of the safety valve. In this case, the equation of motion of the valve disc can be established in consideration of the change of the valve lifting force including the case where choking does not occur, based on the case where choking occurs, thereby allowing the vibration of a valve disc in a safety valve to be properly analyzed.

[0011] The equation of motion of the valve disc may be represented by Equation 1:

$$M_s \ddot{Z} + C_s \dot{Z} + KZ = (P_V - P_B) A_H \left\{ 1 + f(Z) \left(\frac{\psi}{\psi_c} \right)^2 \right\} - KZ_s$$

wherein M_s represents a mass of a moving part including the valve disc; C_s represents a damping coefficient; K represents a spring constant; Z represents the valve lift; P_V represents a safety valve inlet pressure; P_B represents a pressure in the valve box; A_H represents a valve disc holder area; $f(Z)$ represents the valve lifting force function; ψ represents an orifice flow coefficient; ψ_c represents an orifice critical flow coefficient; Z_s represents an initial deformation amount of a spring; and t represents time. The valve lifting force function $f(Z)$, and the ratio of the orifice flow coefficient to the orifice critical flow coefficient, ψ/ψ_c , are included in the first term on the right side of the equation. The vibration of a valve disc in a safety valve can be properly analyzed by using the equation of motion of the valve disc thus represented.

[0012] An evaluation unit that determines whether the set condition inputted in the input unit is good or not in response to the operation result provided by the processing unit, may be further provided. For example, when the amplitude of the vibration of a valve disc exceeds a predetermined value, the set condition inputted may be determined to be improper.

[0013] Note that any combination of the aforementioned components or any manifestation of the present invention realized by modifications of a method, device, system, storing media, computer program, and so forth, is effective as an embodiment of the present invention.

Effect of the Invention

[0014] According to the present invention, a safety valve vibration analyzer that can properly analyze the vibration of a valve disc in a safety valve, can be provided.

Brief Description of the Drawings

[0015] [fig.1] Fig. 1 is a diagram illustrating the structure of the safety valve vibration analyzer according to the embodiment of the present invention;

[fig.2] Fig. 2 is a diagram illustrating an example of a physical model of a pipe line set by an physical model setting unit;

[fig.3]Fig. 3 is a diagram illustrating the structure of a safety valve;

[fig.4]Fig. 4 is a diagram illustrating a mass conservation equation and an energy equation of a fluid in the pipe;

[fig.5]Fig. 5 is a diagram illustrating an equation of motion of a fluid in the pipe;

[fig.6]Fig. 6 is a graph illustrating an example of the valve lifting force function;

[fig.7]Fig. 7 is a flow chart illustrating the process flow of the safety valve vibration analyzer according to the embodiment;

[fig.8]Fig. 8 is a diagram illustrating an experiment system for measuring the vibration of a safety valve;

[fig.9]Fig. 9 is a graph showing experimental data and a simulation result in the case where the length of the upstream pipe X is 0 m;

[fig.10]Fig. 10 is a graph showing experimental data and a simulation result in the case where the length of the upstream pipe X is 1 m;

[fig.11]Fig. 11 is a graph showing experimental data and a simulation result in the case where the length of the upstream pipe X is 5 m;

[fig.12]Fig. 12 is a graph showing experimental data and a simulation result in the case where the length of the upstream pipe X is 10 m;

[fig.13]Fig. 13 is a graph showing experimental data and a simulation result in the case where the length of the upstream pipe X is 20 m;

[fig.14]Fig. 14 is a graph showing experimental data and a simulation result in the case where an area of the safety valve outlet A_D is 10.0 cm²;

[fig.15]Fig. 15 is a graph showing experimental data and a simulation result in the case where the area of the safety valve outlet A_D is 6.0 cm².

Explanation of Reference

- [0016] 10 PHYSICAL MODEL
- 12 SAFETY VALVE
- 14 UPSTREAM PIPE
- 16 DOWNSTREAM PIPE
- 20 NOZZLE
- 25 VALVE DISC
- 26 VALVE BOX
- 30 SPRING
- 36 SAFETY VALVE INLET
- 38 SAFETY VALVE OUTLET
- 50 PIPE ELEMENT
- 100 SAFETY VALVE VIBRATION ANALYZER
- 102 PHYSICAL MODEL SETTING UNIT
- 104 BOUNDARY CONDITION INPUT UNIT

106 INITIAL CONDITION INPUT UNIT
108 SETTING CONDITION INPUT UNIT
110 SAFETY VALVE GOVERNING EQUATION HOLDER
112 PIPE GOVERNING EQUATION HOLDER
114 VALVE LIFTING FORCE FUNCTION HOLDER
116 PROCESSING UNIT
118 EVALUATION UNIT
120 SET CONDITION DECISION UNIT
200 EXPERIMENT SYSTEM

Best Mode for Carrying Out the Invention

- [0017] Hereinafter, the safety valve vibration analyzer according to the embodiment of the present invention will be described with reference to the drawings. The safety valve vibration analyzer can analyze the vibration of a valve disc in a safety valve or the pressure in a pipe or a valve box or the like, by inputting a set condition of a physical model which is set for a pipe line including a safety valve and a pipe. A user can prevent the vibration of a safety valve from happening or identify a cause of creating the vibration, by using the safety valve vibration analyzer.
- [0018] Fig. 1 is a diagram illustrating the structure of the safety valve vibration analyzer 100 according to the embodiment of the present invention. As illustrated in Fig. 1, the safety valve vibration analyzer 100 includes: the physical model setting unit 102, the boundary condition input unit 104, the initial condition input unit 106, the set condition input unit 108, the safety valve governing equation holder 110, the pipe governing equation holder 112, the valve lifting force function holder 114, the processing unit 116, the evaluation unit 118, and the set condition decision unit 120.
- [0019] The safety valve vibration analyzer 100 is practiced by a CPU, a memory, and a program loaded on the memory, or the like, and a function block realized by the co-operation thereof is illustrated herein. The program may be built in the safety valve vibration analyzer 100, or supplied from outside in a form of being stored in a recording medium. Therefore, it would be understood by those skilled in the art that these functional blocks can be realized in a variety of forms by hardware only, software only or the combination thereof.
- [0020] The physical model setting unit 102 sets the physical model of a pipe line including a safety valve and a pipe connected to the safety valve. Fig. 2 is a diagram illustrating an example of a physical model of a pipe line set in the physical model setting unit 102.
- [0021] The physical model 10 of the pipe line illustrated in Fig. 2 includes the safety valve 12, the upstream pipe 14 connected to the upstream side of the safety valve 12, and the downstream pipe 16 connected to the downstream side of the safety valve 12. At the

end part of the opposite side to the safety valve inlet 36 of the upstream pipe 14, the upstream side pipe inlet 13 is provided, and at the end part of the opposite side to the safety outlet 38 of the downstream pipe 16, the downstream side pipe outlet 15 is provided. The upstream side pipe inlet 13 and the downstream side pipe outlet 15 have open ends, respectively. Boundary conditions at the upstream side pipe inlet 13, the downstream side pipe outlet 15, the safety valve inlet 36, and the safety valve outlet 38 are set in the boundary condition input unit 104 described later.

[0022] The present embodiment will be described assuming that an operation fluid is air; however, the operation fluid may be other types of gases without being limited to air. Air introduced from the upstream side pipe inlet 13 flows along the upstream pipe 14, the safety valve 12, and the downstream pipe 16 to be released from the downstream side pipe outlet 15.

[0023] Fig. 3 is a diagram illustrating the structure of the safety valve 12. The safety valve 12 illustrated in Fig. 3 has the structure in which the valve disc 25, which is made of a disc holder 22 and a disc 24, is pressed against the upper end part of the nozzle 20 by the spring 30. The nozzle 20 communicates with the upstream pipe 14, and the valve disc 25 is, when the pressure of the upstream pipe 14 rises to exceed a predetermined set pressure, displaced upward against the spring power of the spring 30, thereby air flowing into the valve box 26. Air introduced into the valve box 26 flows into the downstream pipe 16 through the safety valve outlet 38.

[0024] Boundary conditions at the upstream side pipe inlet 13, the downstream side pipe outlet 15, the safety valve inlet 36, and the safety valve outlet 38, are inputted in the boundary condition input unit 104. In the present embodiment, boundary conditions are set as follows: at the safety valve inlet 36, it is assumed that a rate of the outflow W of the upstream pipe 14 and a rate of the inflow W_s of the safety valve 12 are equal, that is, $W=W_s$. At the safety valve outlet 38, it is assumed that a rate of the outflow W_D of the safety valve 12 and a rate of the inflow W of the downstream pipe 16 are equal, that is, $W=W_D$. At the upstream side pipe inlet 13, the pressure P in the upstream pipe 14 is set to be constant on the assumption that a pressure vessel with large capacity is connected. At the downstream side pipe outlet 15, the pressure P in the downstream pipe 16 is set to be constant on the assumption that a header with a large diameter is connected.

[0025] Set conditions of a physical model of a pipe line including the safety valve 12, the upstream pipe 14, and the downstream pipe 16, are inputted in the set condition input unit 108. As the set conditions, parameters used for vibration analysis, i.e., the shape of a safety valve, the size of a pipe line, or the like, are inputted. A set condition refers to a parameter necessary for the analysis of a physical model, and specifically, to a parameter required for the governing equation of a safety valve or a pipe described

later.

[0026] An initial condition of a predetermined parameter at the time $t = 0$, is inputted in the initial condition input unit 106. For example, initial conditions, such as a valve lift and a speed of the valve disc at the time $t = 0$, are inputted in the initial condition input unit 106.

[0027] The safety valve governing equation holder 110 holds a safety valve governing equations including an equation of motion of the valve disc, a flow equation at the inlet of the safety valve, a flow equation at the outlet of the safety valve, and a mass conservation equation in the valve box. Each equation will be shown below.

[0028] The equation of motion of a valve disc is represented by the following equation (1):

$$M_s \ddot{Z} + C_s \dot{Z} + KZ = (P_v - P_b) A_H \left\{ 1 + f(Z) \left(\frac{\psi}{\psi_c} \right)^2 \right\} - KZ_s \quad \dots (1)$$

wherein M_s represents a mass of a moving part (kg); C_s represents a damping coefficient (N·s/m); K represents a spring constant (N/m); Z represents a Valve lift (m); P_v represents a safety valve inlet pressure (Pa); P_b represents a pressure in the valve box (Pa); A_H represents a valve disc holder area (m²); $f(Z)$ represents a valve lifting force function; y represents an orifice flow coefficient; y_c represents an orifice critical flow coefficient; Z_s represents an initial spring deformation amount (m); and t represents time (s). The mass of the moving part M_s is the sum of the disc holder 22, the disc 24, the spindle 28, the lower spring seat 34, and the spring 30 (for the spring 30 1/3 of the spring total mass is effective to the mass of the moving part).

[0029] The first term on the right side of Equation (1) represents a valve lifting force F exerting on the valve disc 25. As shown in Equation (1), in the safety valve vibration analyzer 100 according to the present embodiment, the valve lifting force F includes: the difference ($P_v - P_b$) of the safety valve inlet pressure P_v and the valve box internal pressure P_b multiplied by the valve disc holder area A_H ; and further the valve lifting force function $f(Z)$ multiplied by the square of the ratio y/y_c of the orifice flow coefficient y to the orifice critical flow coefficient y_c of the safety valve (hereinafter, referred to as the flow coefficient ratio.) The valve lifting force F can be properly represented by including this term.

[0030] The valve lifting force function $f(Z)$ is a function indicating the relation between the valve lift and the valve lifting force exerting on the valve disc, and is defined by the structure of a safety valve. The valve lifting force function $f(Z)$ is held in the valve lifting force function holder 114 described later, and is created by actual measurement of the relation between the valve lift and the valve lifting force. By applying the valve lifting force function $f(Z)$ to the equation of motion of the valve disc, the valve lifting force F exerting on the valve disc can be properly represented, allowing a proper

vibration analysis to be made.

- [0031] The Orifice flow coefficient y varies in accordance with the relation between the critical pressure P_c , which is defined by the following Equation (2), and the safety valve inlet pressure P_v .

$$P_c = P_v \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa}{\kappa - 1}} \quad \dots (2)$$

- [0032] When the valve box internal pressure P_B is equal to or less than the critical pressure P_c ($P_B \leq P_c$), the orifice flow coefficient y is represented by the following Equation (3). The coefficient is a constant and the orifice flow coefficient y in this case is the orifice critical flow coefficient y_c .

$$\psi = \psi_c = \sqrt{\kappa \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa + 1}{\kappa - 1}}} \quad \dots (3)$$

- [0033] On the other hand, when the valve box internal pressure P_B is more than the critical pressure P_c ($P_B > P_c$), the orifice flow coefficient y is represented by the following Equation (4). As shown in Equation (4), the coefficient is a function of the pressure ratio P_B/P_v of the valve box internal pressure P_B to the safety valve inlet pressure P_v .

$$\psi = \sqrt{\frac{2\kappa}{\kappa - 1} \left[\left(\frac{P_B}{P_v} \right)^{\frac{2}{\kappa}} - \left(\frac{P_B}{P_v} \right)^{\frac{\kappa + 1}{\kappa}} \right]} \quad \dots (4)$$

- [0034] In the present embodiment, the equation of motion of the valve disc is established with the influence of choking occurring when air flows into the valve box 26 from the nozzle 20, being considered, by applying the flow coefficient ratio y/y_c , which is calculated by using Equations (3)-(4), to the equation of motion of the valve disc. For example, when the valve box internal pressure P_B is less than the critical pressure P_c and is in the choking condition, the flow coefficient ratio y/y_c is 1, therefore the valve lifting force F is what $A_H (P_v - P_B)$ is multiplied by $1 + f(Z)$. On the other hand, when the valve box internal pressure P_B is more than the critical pressure P_c , the flow coefficient ratio y/y_c is less than 1, therefore the valve lifting force F is less than what is in the choking condition. Thus, by applying the flow coefficient ratio y/y_c to the equation of motion of the valve disc, variation in the valve lifting force F by choking is taken into consideration, allowing a proper vibration analysis to be made. It is noted that the flow coefficient ratio is squared for representing it as a kinetic energy in Equation (1).

- [0035] A flow rate equation at the safety valve inlet 36 is represented by the following

Equation (5):

$$W_s = \frac{A_s C_d \psi P_v}{\sqrt{z R T_0 / M_w}} \quad \dots (5)$$

wherein W_s represents a rate of the inflow (kg/s); A_s represents an effective orifice area (m²); C_d represents a nozzle flow coefficient; z represents a gas compressibility factor; M_w represents a gas average molecular weight (kg/kmol); R represents the gas constant (8314 J•kg/kmol/K); and T_0 represents a total temperature (K).

[0036] The effective orifice area A_s in Equation (5) is represented by the following Equation (6):

$$A_s = \min(\pi d_H Z, A_0) \quad \dots (6)$$

wherein d_H represents a disc holder diameter (m); and A_0 represents a nozzle orifice area (m²).

[0037] A flow rate equation at the safety valve outlet 38 is represented by the following Equation (7):

$$W_D = \frac{A_D C_{dD} \psi P_B}{\sqrt{z R T_0 / M_w}} \quad \dots (7)$$

wherein W_D represents a rate of the outflow (kg/s); A_D represents the safety valve outlet area (m²); and C_{dD} represents an outlet area flow coefficient. The orifice flow coefficient ψ in Equation (7) is used by replacing the valve box internal pressure P_B and the safety valve inlet pressure P_v in Equation (4) with the safety valve downstream pressure P_D and the valve box internal pressure P_B , respectively.

[0038] The mass conservation equation in the valve box is represented by the following Equation (8); Equation (9) represents a gas density ρ_B (kg/m³) in the valve box; and Equation (10) represents an equation of state in the valve box:

$$\frac{dM_B}{dt} = W_s - W_D, \quad \dots (8)$$

$$\rho_B = \frac{M_B}{V_B}, \quad \dots (9)$$

$$P_B = \frac{\rho_B z R T_B}{M_w} \quad \dots (10)$$

wherein M_B represents a gas mass in the valve box (kg); T_B represents a gas temperature in the valve box (K); and V_B represents the a valve box capacity (m³).

[0039] The pipe governing equation holder 112 holds a pipe governing equations including a mass conservation equation, an energy equation, and an equation of motion of a fluid

flowing the pipe, such as the upstream pipe 14 and the downstream pipe 16. Fig. 4 is a diagram illustrating the mass conservation equation and the energy equation of a fluid in the pipe. A pipe is divided into pipe elements of which each element has its length of the divided length $D_x(m)$ as shown in Fig. 4, and the governing equation is applied to each pipe element. Each equation will be shown below.

[0040] The mass conservation equation in one pipe element 50 shown in Fig. 4, is represented by the following Equation (11). Equation (12) represents the gas density r in the pipe element 50, and Equation (13) represents the equation of state in the pipe element 50:

$$\frac{dM}{dt} = W_{in} - W_{out} \quad \dots (11)$$

$$\rho = \frac{M}{A\Delta x} \quad \dots (12)$$

$$P = \frac{\rho zRT}{M_w} \quad \dots (13)$$

wherein M represents a gas mass (kg) in the pipe element 50; W_{in} represents a rate of the inflow (kg/s) into the pipe element 50; W_{out} represents a rate of the outflow (kg/s) from the pipe element 50; r represents a gas density (kg/m³) in the pipe element 50; A represents the flow area of the pipe (m²); P represents a gas pressure (Pa) in the pipe element 50; and T represents a gas temperature (K) in pipe element 50.

[0041] The energy equation in the pipe element 50 is represented by the following Equation (14):

$$T + \frac{U^2}{2C_p} = T_0 = \text{const.} \quad \dots (14)$$

wherein U represents a gas velocity (m/s) in the pipe element 50; C_p represents the gas specific heat under constant pressure (J/kg/K). Equation (14) means that the higher the gas velocity U , the lower the gas temperature T .

[0042] Fig. 5 is a diagram illustrating the equation of motion of a fluid in the pipe. In Fig. 5, U_u represents a gas velocity on the side of the upstream of the pipe element 50 having its length of D_x , P_u represents a gas pressure on the same side, and r_u represents a gas density on the same side. U_d represents a gas velocity on the side of the downstream of the pipe element 50, P_d represents a gas pressure on the same side, and r_d represents a gas density on the same side.

[0043] The equation of motion of a fluid in the pipe element 50 is generally represented by the following Equation (15):

$$\rho \left(\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} \right) = - \frac{\partial P}{\partial x} - f \frac{1}{D} \cdot \frac{\rho U |U|}{2} \quad \dots (15)$$

wherein f represents a friction factor of a pipe, and D represents the inner diameter of a pipe.

[0044] Equation (16) representing the change rate of the gas flow rate can be obtained by deforming Equation (15). $F1$ in Equation (16) is represented by Equation (17); $F2$ by Equation (18) or Equation (19); and $F3$ by Equation (20).

$$\frac{dU}{dt} = F1 + F2 + F3 \quad \dots (16)$$

$$F1 = - \frac{1}{\rho} \frac{\partial P}{\partial x} = - \frac{P_d - P_u}{\rho \Delta x} \quad \dots (17)$$

$$F2 = -U \frac{\partial U}{\partial x} = -U_u \frac{U - U_u}{\Delta x} \quad \dots (18)$$

$$F2 = -U \frac{U_d - U}{\Delta x} \quad \dots (19)$$

$$F3 = -f \frac{1}{D} \cdot \frac{U |U|}{2} \quad \dots (20)$$

[0045] In Equations (16) to (20), $F1$ represents a pressure term; $F2$ represents an inertia term; and $F3$ represents a friction loss term. Equation (18) represents the inertia term when a fluid flows from the upstream side to the downstream side; and equation (19) represents the inertia term when a fluid flows from the downstream side to the upstream side.

[0046] The valve lifting force function holder 114 holds the valve lifting force function $f(Z)$ representing the relation between the valve lift and the valve lifting force exerting on the valve disc. As described above, the valve lifting force function is a function created by actual measurement of the relation between the valve lift and the valve lifting force, and is defined by the structure of the safety valve.

[0047] Fig. 6 is a graph illustrating an example of the valve lifting force function. The horizontal axis of Fig. 6 represents the valve lift (mm), and the vertical axis represents $1+f(Z)$. The valve lifting force function holder 114 holds a valve lifting force function as illustrated in Fig. 6. The valve lifting force function holder 114 may hold a plurality of valve lifting force functions in accordance with the types of the safety valves.

[0048] When creating the valve lifting force function $f(Z)$, a valve lifting force is measured for every valve lift by using a load cell, after removing the spring of the safety valve and adjusting the valve lift with the use of a jig. The valve lifting force function $f(Z)$ is

calculated from the valve lifting forces measured and the pressures in the safety valve inlet and the valve box.

[0049] The processing unit 116 carries out a vibration analysis of the safety valve using: the physical model set in the physical model setting unit 102; the boundary conditions inputted in the boundary condition input unit 104; the initial conditions inputted in the initial condition input unit 106; the set conditions inputted in the set condition input unit 108; the safety valve governing equations held in the safety valve governing equation holder 110; and the pipe governing equations held in the pipe governing equation holder 112. Herein, the time variations of the valve lift Z , the upstream pipe pressure P_v , and the valve box internal pressure P_b , are derived as the vibration analysis of a safety valve. When calculating, the processing unit 116 appropriately reads the valve lifting force function from the valve lifting force function holder 114, and derives the time variations of the valve lift Z , the upstream pipe pressure P_v , and the valve box internal pressure P_b , by applying the valve lifting force function $f(Z)$ to the equation of motion of the valve disc.

[0050] Specifically, numerical integration of differential equations of: the equation of motion of the valve disc of Equation (1); the mass conservation equation in the valve box of Equation (8); the mass conservation equation of the fluid flowing in the pipe of Equation (11); and the equation of motion of the fluid of Equation (16), by the Runge-Kutta method, are carried out with the use of the relations of Equations (2) to (7), Equation (9), Equation (10), Equations (12)-(14), and Equations (17)-(20). The time variation of the valve lift Z is found by integrating the equation of motion of the valve disc of Equation (1); and the time variation of the upstream pipe pressure P_v and the valve box internal pressure P_b are found as a result of integration of the mass conservation equation in a valve box of Equation (8), the mass conservation equation of the fluid of Equation (11), and the equation of motion of the fluid of Equation (16). For the numerical integration, the Euler method also can be applied.

[0051] The evaluation unit 118 determines whether the set conditions inputted in the set condition input unit 108 is good or not in response to the operation result provided by the processing unit 116. For example, when vibration occurs by an set condition inputted, the inputted set conditions are determined to be improper. The occurrence of vibration is determined, for example, based on the judgment of whether the amplitude of the vibration exceeds a predetermined value. At the time, the evaluation unit 118 may give a command to the set condition input unit 108 that new set conditions should be inputted. The command may be automatically given to the vibration analysis program, or may be shown to a user inputting set conditions through a monitor or a sound.

[0052] The set condition decision unit 120 decides that set conditions are proper when the

set conditions are determined to be proper from the evaluation result made by evaluation unit 118.

- [0053] Fig. 7 is a flow chart illustrating the process flow of the safety valve vibration analyzer according to the embodiment. A user at first sets a physical model of a pipe including the safety valve 12, the upstream pipe 14, and the downstream pipe 16 in the physical model setting unit 102 (S10).
- [0054] Next, the user inputs boundary conditions at the upstream side pipe inlet 13, the downstream side pipe outlet 15, the safety valve inlet 36, and the safety valve outlet 38 in the boundary condition input unit 104 (S12). The user then inputs initial conditions in the initial condition input unit 106 (S14). The user then inputs set conditions of the set physical model in the set condition input unit 108 (S16).
- [0055] After completing the above input operations, the processing unit 116 operates time variations of the valve lift Z , the upstream pipe pressure P_v , and the valve box internal pressure P_B , using a physical model set in the physical model setting unit 102, boundary conditions inputted in the boundary condition input unit 104, initial conditions inputted in the initial condition input unit 106, set conditions inputted in the set condition input unit 108, the safety valve governing equations held in the safety valve governing equation holder 110, the pipe governing equations held in the pipe governing equation holder 112 (S18-S22). When operating, the processing unit 116 appropriately reads the valve lifting force function $f(Z)$ from the valve lifting force function holder 114, and operates by applying the valve lifting force function $f(Z)$ to the equation of motion of the valve disc.
- [0056] After completing the operation, the evaluation unit 118 determines whether the set conditions inputted in the set condition input unit 108 are proper or not, in response to the analysis result by processing unit 116 (S24). When the set conditions are not proper, the evaluation unit 118 gives a command to the set condition input unit 108 that new set conditions should be inputted (N of S26). When the set conditions are proper (Y of S26), the set condition decision unit 120 decides that the set conditions are proper (S28). With the above steps, the process flow of the safety valve vibration analyzer 100 ends.
- [0057] A comparison between a simulation result and experimental data obtained by using the safety valve vibration analyzer 100 according to the present embodiment, will be shown below.
- [0058] Fig. 8 is a diagram illustrating an experiment system for measuring the vibration of the safety valve 200. The experiment system 200 includes: the safety valve 12; the upstream pipe 14 connected to the upstream side of the safety valve 12; the container 70 connected to the upstream pipe 14 via the ball valve 74; the compressor 72 for maintaining the pressure of the container 70 to be constant (20 barG); the reducing part

78 on the downstream side of the safety valve 12; and the downstream pipe 16 connected to the safety valve via the ball valve 76. The laser displacement transmitter 82 for measuring the displacement of the valve disc was provided to the safety valve 12, and the pressure sensors 80 for measuring the pressure were provided to the upstream pipe 14 and the safety valve 12, respectively. Vibration experiments of the safety valve were conducted with the use of the experiment system 200 about the case where the length x of the upstream pipe 14 was varied and the case where the safety valve outlet area A_D was varied.

- [0059] A vibration simulation of the safety valve was conducted after set conditions, which were set to the physical model structured likewise to the experiment system 200, were inputted in the safety valve vibration analyzer 100 according to the present embodiment.
- [0060] Figs. 9-13 show the experimental data and the simulation results when the length x of the upstream pipe is varied. Fig. 9 shows the experimental data and the simulation result in the case where the length of the upstream pipe is 0 m. Fig. 10 shows the experimental data and the simulation result in the case where the length of the upstream pipe is 1 m. Fig. 11 shows the experimental data and the simulation result in the case where the length of the upstream pipe is 5 m. Fig. 12 shows the experimental data and the simulation result in the case where the length of the upstream pipe is 10 m. Fig. 13 shows the experimental data and the simulation result in the case where the length x of the upstream pipe is 20 m. (a) represents the time variation of the valve lift Z , (b) represents the time variation of the upstream pipe pressure P_v , and (c) represents the time variation of the valve box internal pressure P_B , respectively.
- [0061] From the experimental data, it is found that: when the length x of the upstream pipe is 0m, the valve disc hardly vibrates as shown in Fig. 9, and the upstream pipe pressure P_v and the valve box internal pressure P_B are stable; when the length of the upstream pipe is 1 m and 5 m, as shown in Figs. 11-12, the valve lift Z , the upstream pipe pressure P_v , and the valve box internal pressure P_B vary periodically with large amplitude, as shown in Figs. 11 and 12; and however, with the length x of the upstream pipe becoming long to 10m and 20m, the valve lift Z , the upstream pipe pressure P_v , and the valve box internal pressure P_B vary small.
- [0062] On the other hand, in the simulation result, the timing at which a vibration occurs is almost same as that of the experiment whereas the amplitude of the simulation differs slightly from the experiment. In Fig. 12 (a), the experimental data shows that the valve disc vibrates at the time of 0.02 s then attenuates, and vibrates again at the time of 0.09 s after the attenuation. The interval between the vibrations of 0.07 s is almost the same time during which a pressure wave, which is generated by the safety valve opening, reciprocates along the 10 m long pipe, allowing the occurrence of vibration relating to

the pressure wave propagation to be correctly simulated. The reason why the occurrence of vibration can be simulated so correctly is: the equation of motion of the valve disc is established by applying the valve lifting force function $f(Z)$ and the flow coefficient ratio y/y_C ; and the mutual influence between the safety valve and the pipe is taken into consideration by adopting the mass conservation law and the equation of motion of the pipe.

- [0063] Figs. 14 and 15 show the experimental data and the simulation results when the safety valve outlet area A_D is varied. Fig. 14 shows the experimental data and the simulation result in the case where the safety valve outlet area A_D is 10.0 cm². Fig. 15 shows the experimental data and the simulation result in the case where the safety valve outlet area A_D is 6.0 cm². (a) represents the time variation of the valve lift Z , (b) represents the time variation of the upstream pipe pressure P_v , and (c) represents the time variation of the valve box internal pressure P_B , respectively.
- [0064] It is found from the experimental data that, when the safety valve outlet area A_D is large, 10.0 cm², a vibration hardly occurs as shown in Fig. 4, whereas when the safety valve outlet area A_D becomes small, 6 cm², a vibration occurs. The simulation in which the safety valve vibration analyzer 100 is adopted, can obtain the result almost the same as the experimental data. In accordance with the safety valve vibration analyzer 100 according to the present embodiment, a simulation in which the influence of the safety valve outlet area is taken into consideration, can be conducted.
- [0065] As shown in Figs. 9-15, in accordance with the safety valve vibration analyzer 100 according to the present embodiment, vibration analysis of a safety valve in which the influences of the length of the upstream pipe and the safety valve outlet area are taken into consideration, can be conducted correctly. A preferable pipe system can be designed by using the safety valve vibration analyzer 100, in which vibration of a safety valve can be minimized, for example, by varying the length of an upstream pipe with the position where the safety valve is placed being adjusted, even in a pipe system having the same length.
- [0066] The present invention has been described above based on an embodiment. These embodiments are intended solely for the purpose of illustration, and it should be understood by those skilled in the art that various modifications are possible in combining those various components and various processing and those modifications also fall in the scope of the present invention.
- [0067] For example, in the above embodiment, a physical model is structured such that a pressure vessel with large capacity is connected to the upstream side pipe inlet 13 and a header with a large diameter is connected to the downstream side pipe outlet 15; however, another different physical model can be structured such that other pipes, such as a main pipe and a header pipe, is connected to the upstream side pipe inlet 13 and

the downstream side pipe outlet 15.

Industrial Applicability

[0068] The present invention can be utilized for a safety valve vibration analyzer that analyzes vibration of a valve disc in a safety valve.

Claims

- [1] A safety valve vibration analyzer that analyzes vibration of a valve disc in a safety valve, the safety valve analyzer comprising:
 an input unit in which set conditions of a physical model including the safety valve and an upstream pipe connected to the safety valve is inputted;
 a first holder that holds a safety valve governing equations including an equation of motion of the valve disc, a flow equation at the safety valve inlet, a flow equation at the safety valve outlet, and a mass conservation equation in a valve box;
 a second holder that holds a pipe governing equations including a mass conservation equation, an energy equation, and an equation of motion of a fluid flowing the upstream pipe;
 a processing unit that derives a time variation of a valve lift by using the set conditions inputted in the input unit, the safety valve governing equations held in the first holder, and the pipe governing equations held in the second holder; and
 a third holder that holds a valve lifting force function representing the relation between the valve lift and a valve lifting force exerting on the valve disc, wherein
 the processing unit reads the valve lifting force function from the third holder and derives the time variation of the valve lift by applying the valve lifting force function to the equation of motion of the valve disc.
- [2] The safety valve vibration analyzer according to claim 1, wherein the valve lifting force function is created by measuring the relation between the valve lift and the valve lifting force.
- [3] The safety valve vibration analyzer according to claim 1 or 2, wherein the processing unit derives the time variation of the valve lift using the equation of motion of the valve disc comprising a ratio of an orifice flow coefficient to an orifice critical flow coefficient of the safety valve.
- [4] The safety valve vibration analyzer according to any one of claims 1 to 3, wherein the equation of motion of the valve disc is represented by Equation 1:

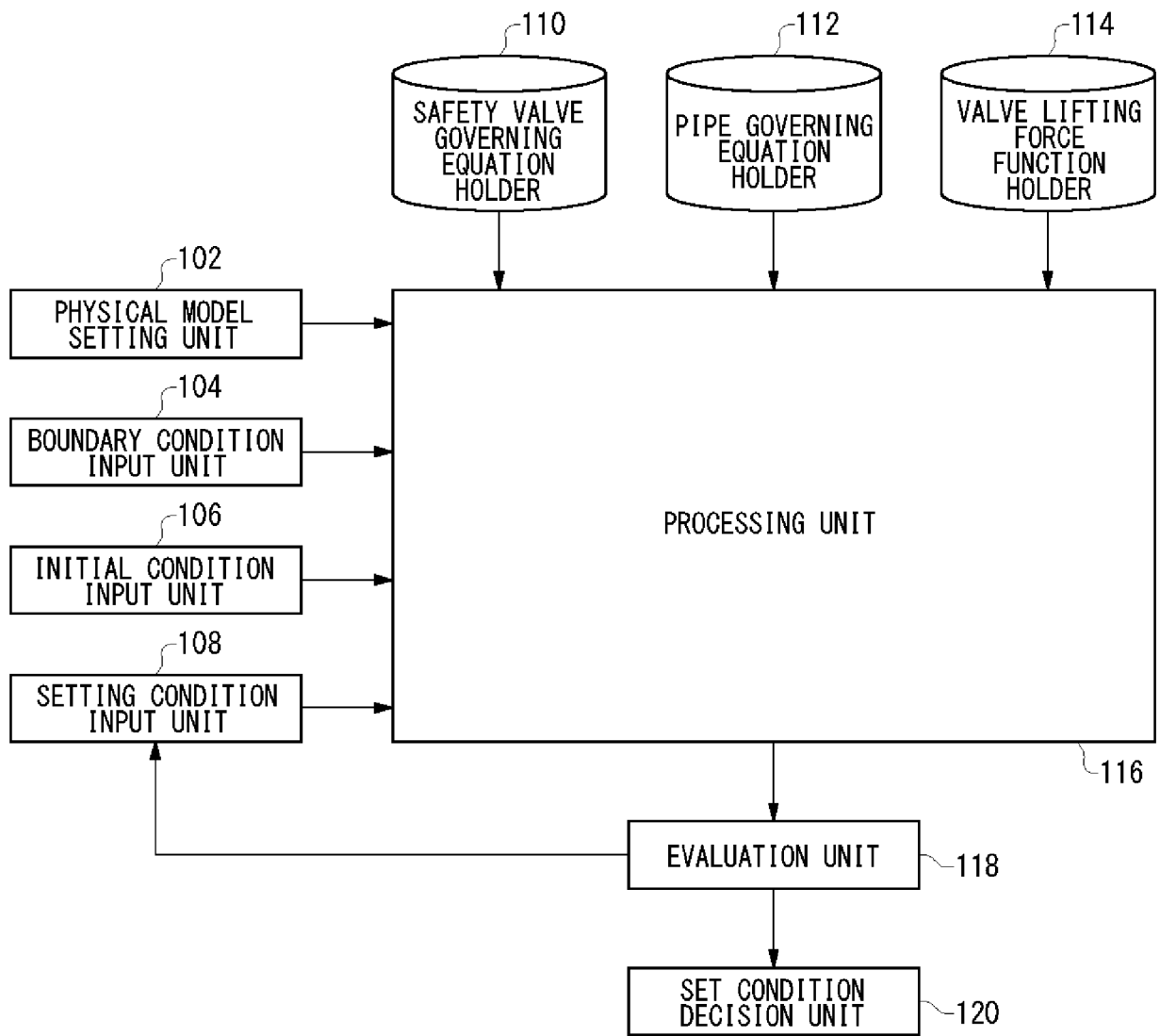
$$M_s \ddot{Z} + C_s \dot{Z} + KZ = (P_v - P_b) A_H \left\{ 1 + f(Z) \left(\frac{\psi}{\psi_c} \right)^2 \right\} - KZ_s$$

wherein M_s represents a mass of a moving part including the valve disc; C_s represents a damping coefficient; K represents a spring constant; Z represents the valve lift; P_v represents a safety valve inlet pressure; P_b represents a valve box internal pressure; A_H represents a valve disc holder area; $f(Z)$ represents the valve

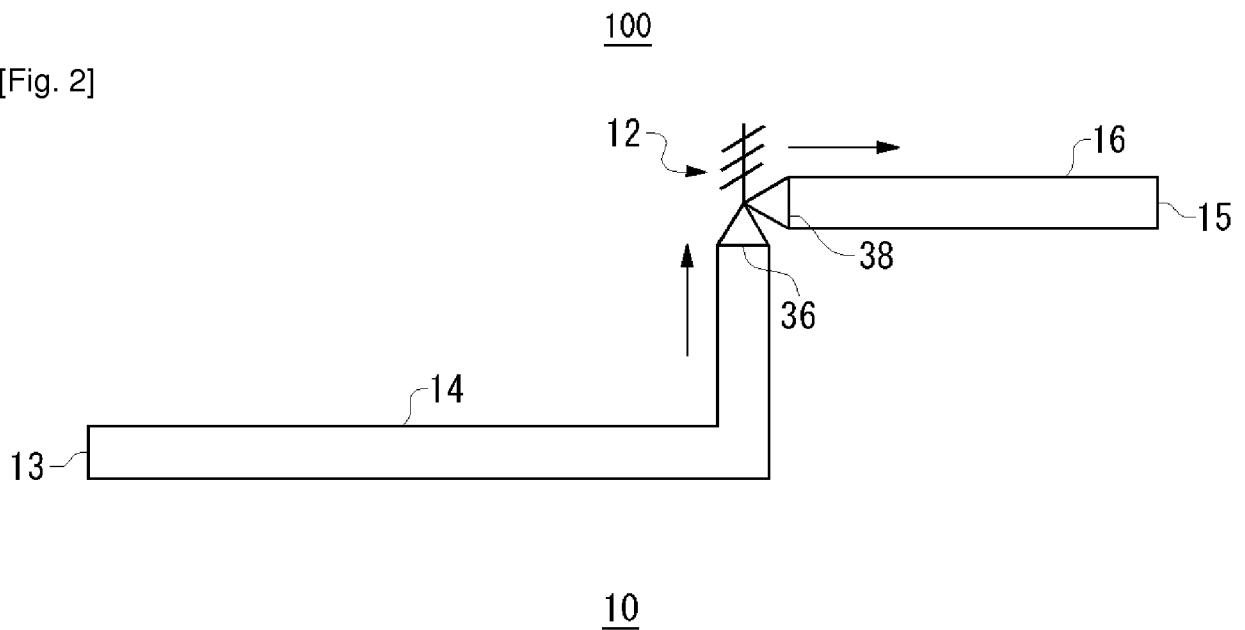
lifting force function; y represents an orifice flow coefficient; y_c represents an orifice critical flow coefficient; Z_s represents an initial deformation amount of the spring; and t represents time.

- [5] The safety valve vibration analyzer according to any one of claims 1 to 4, further comprising:
an evaluation unit that determines the set condition inputted in the input unit are good or not in response to the operation result provided by the processing unit.

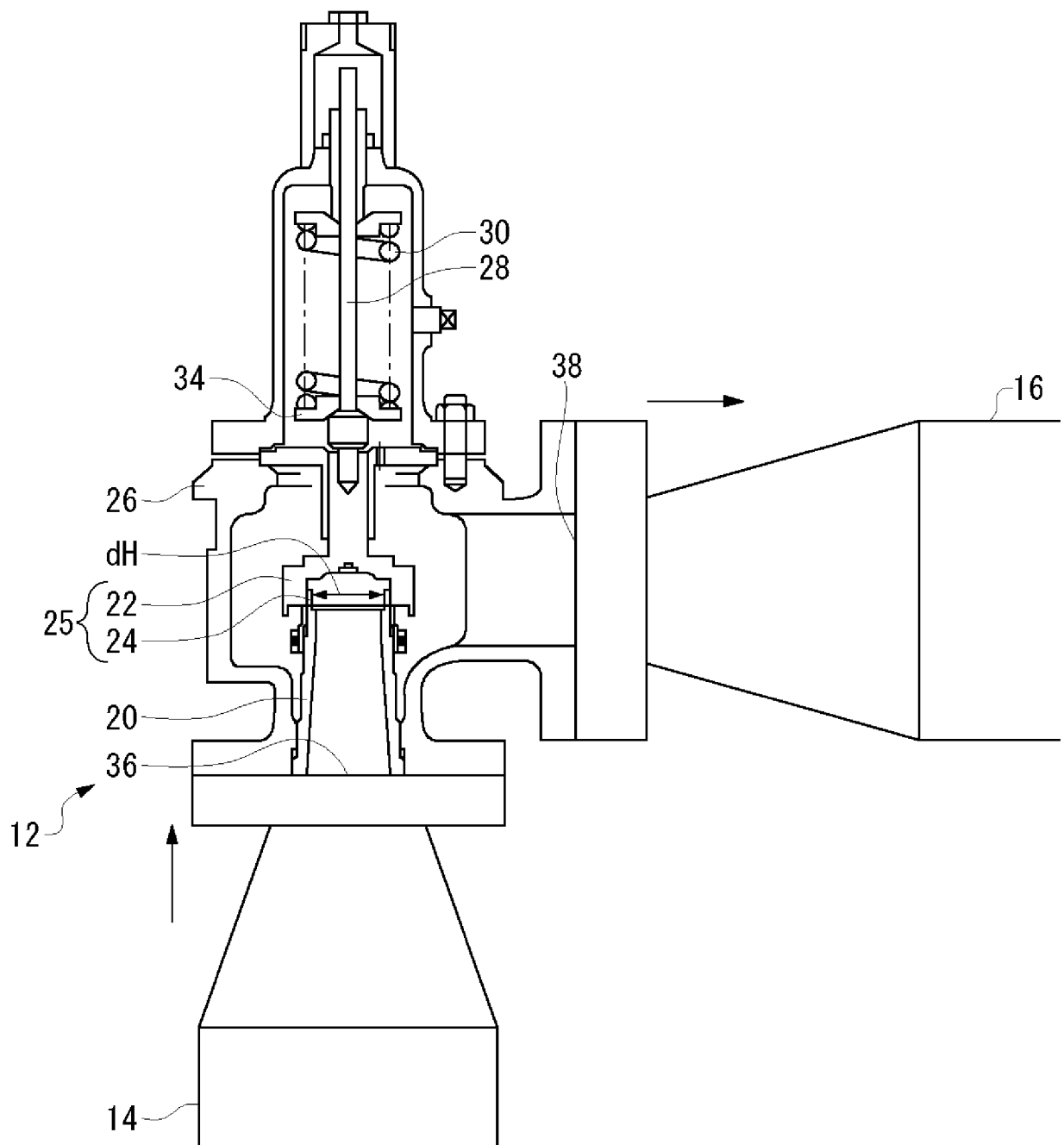
[Fig. 1]



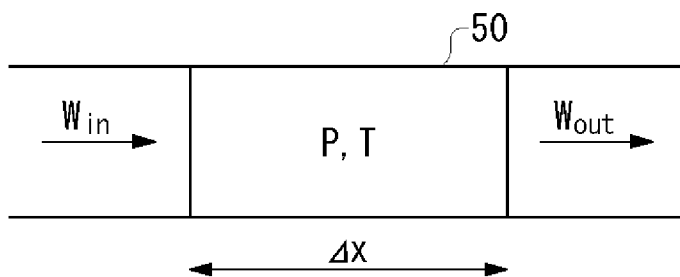
[Fig. 2]



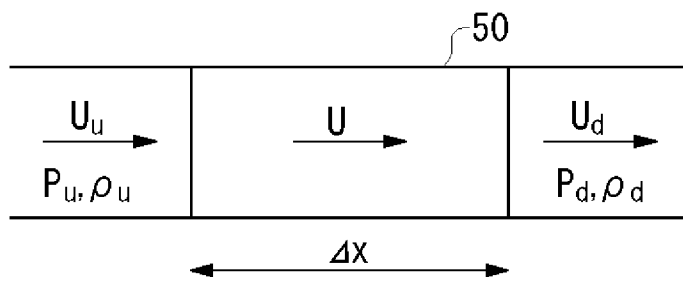
[Fig. 3]



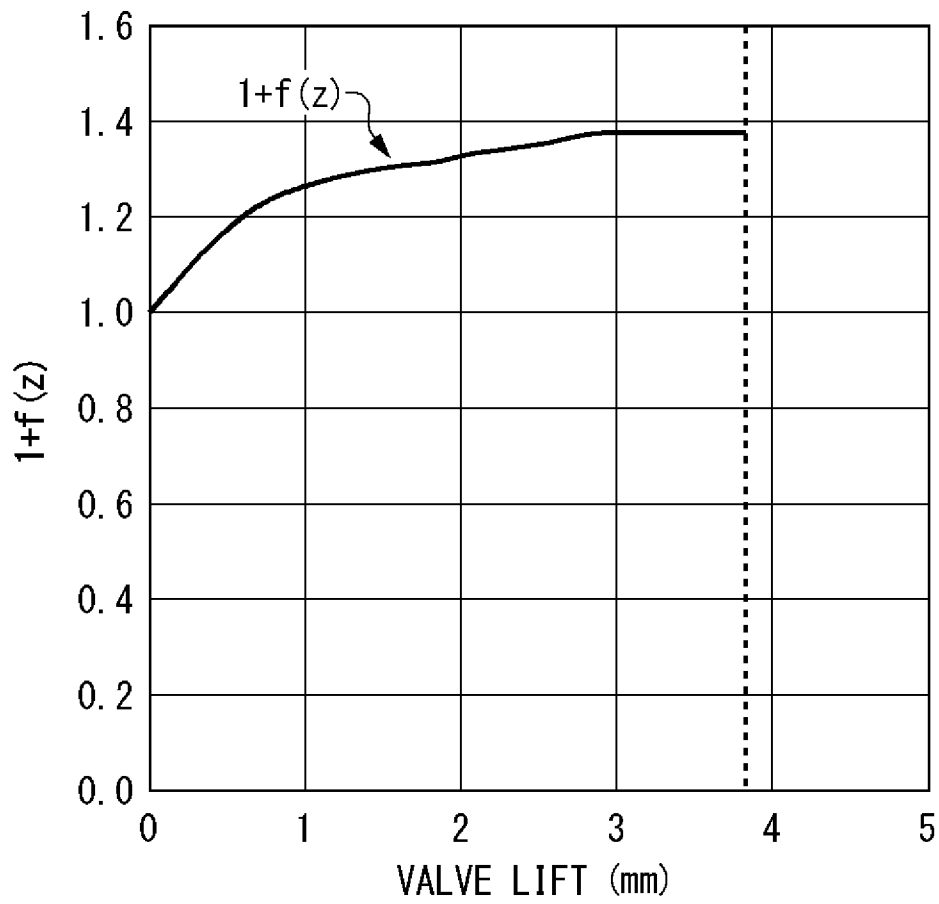
[Fig. 4]



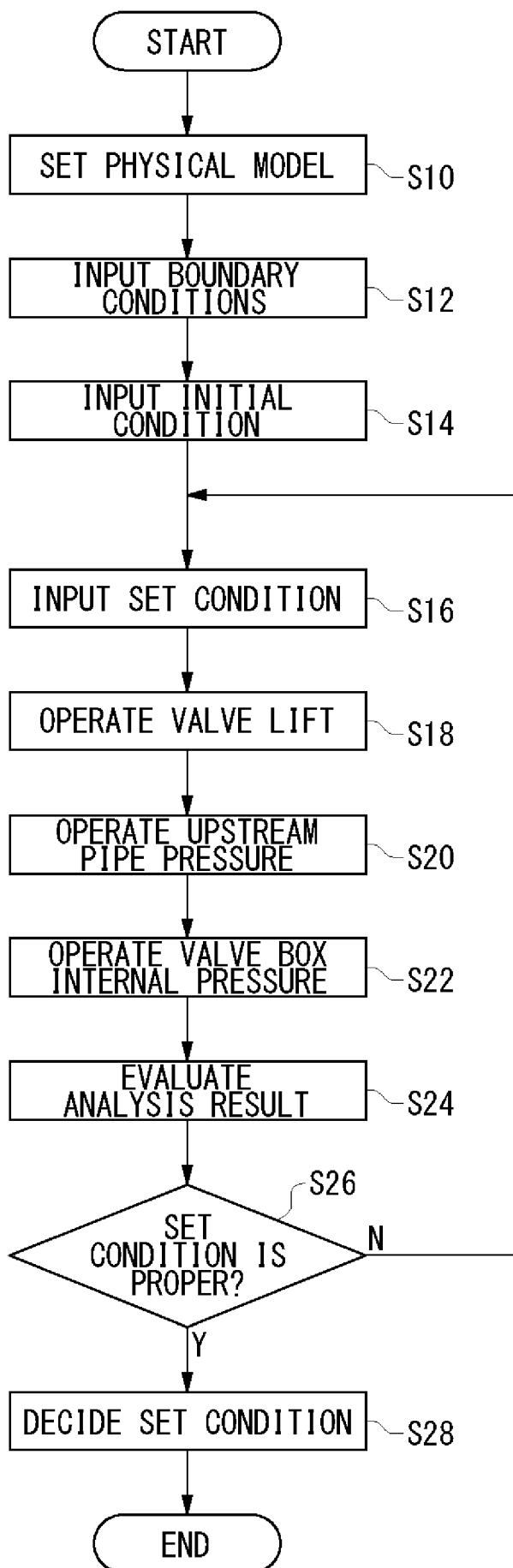
[Fig. 5]



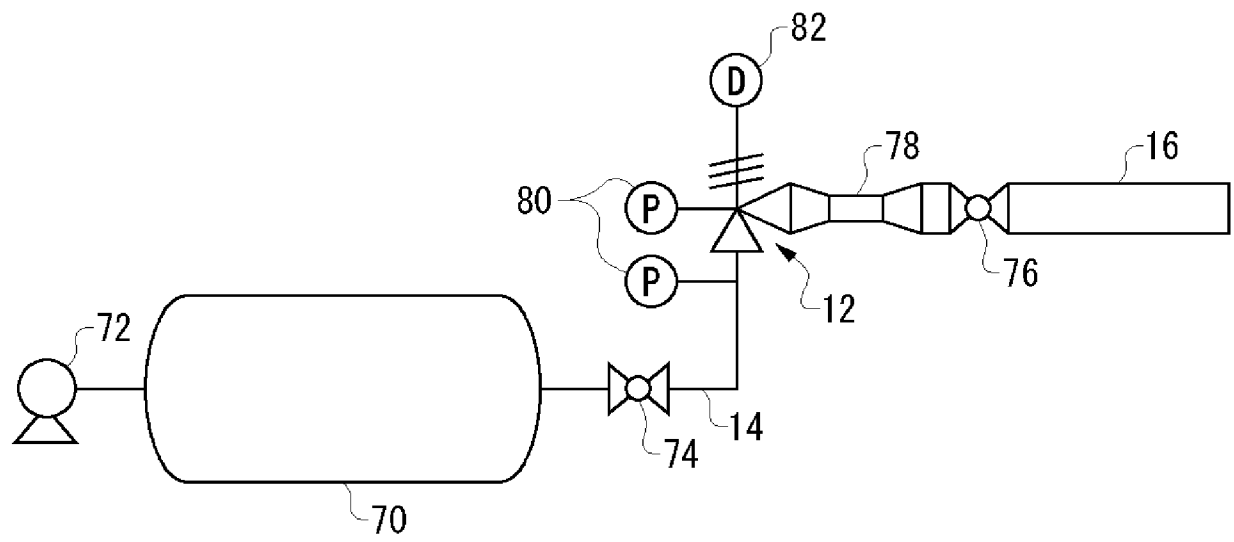
[Fig. 6]



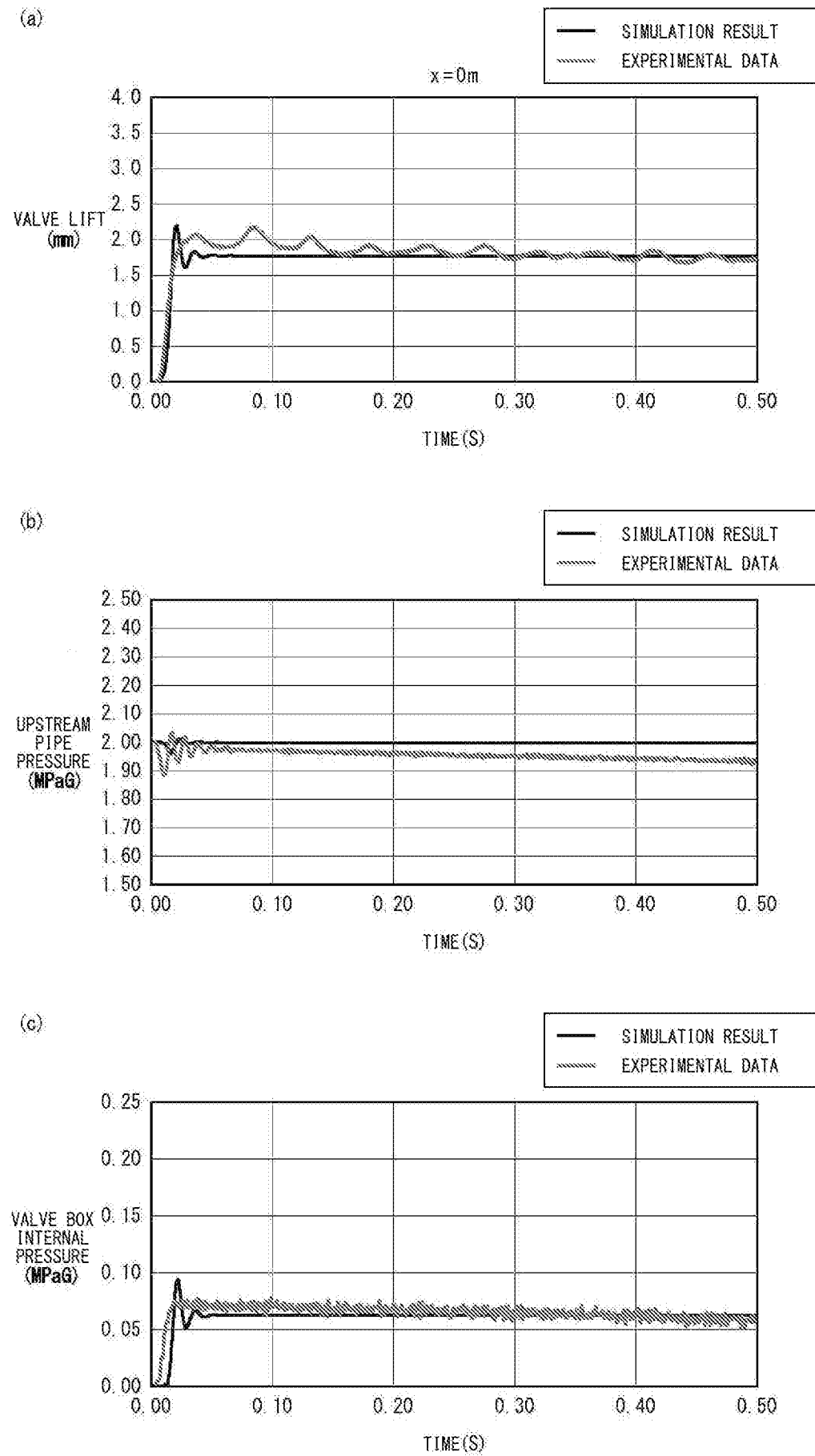
[Fig. 7]



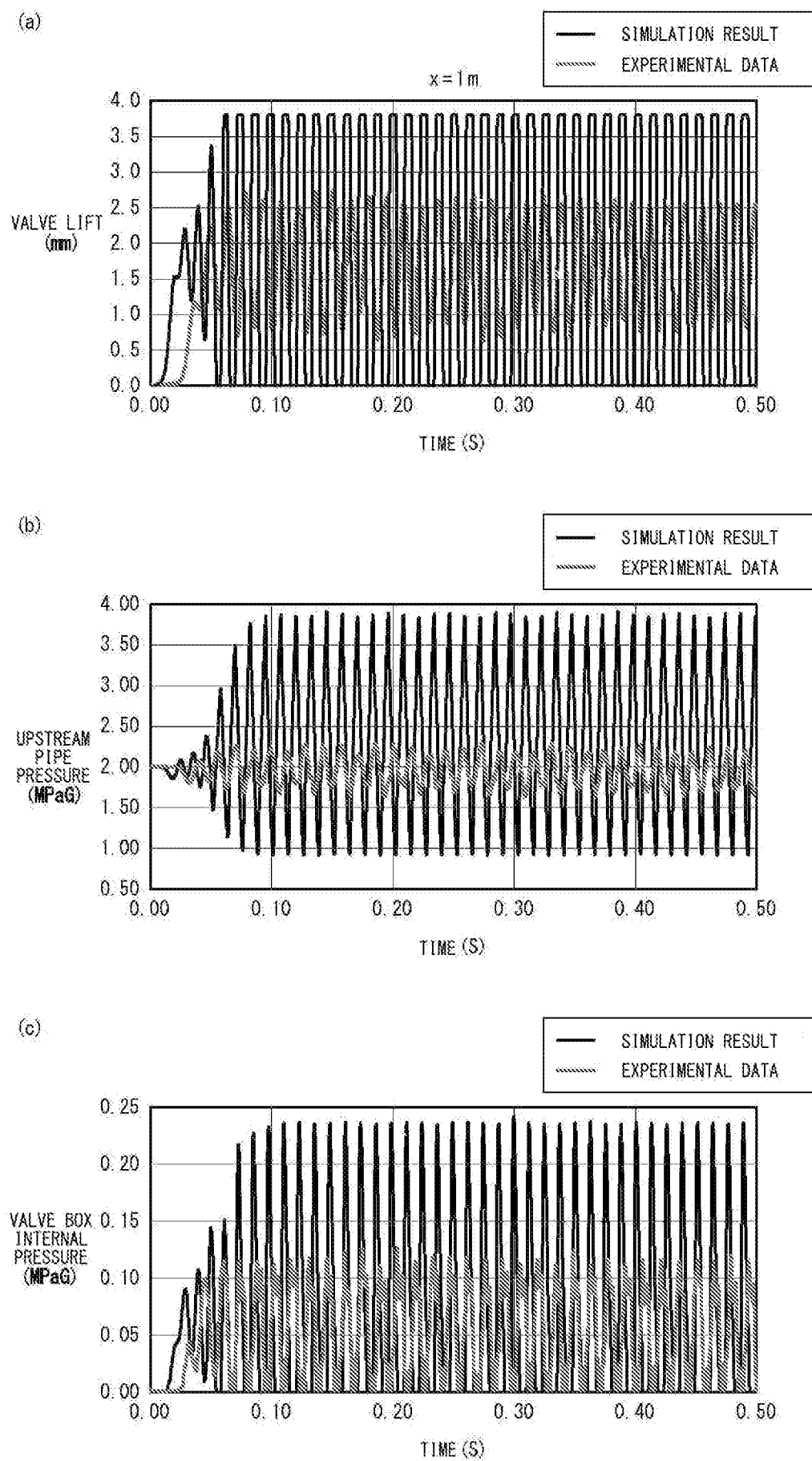
[Fig. 8]

200

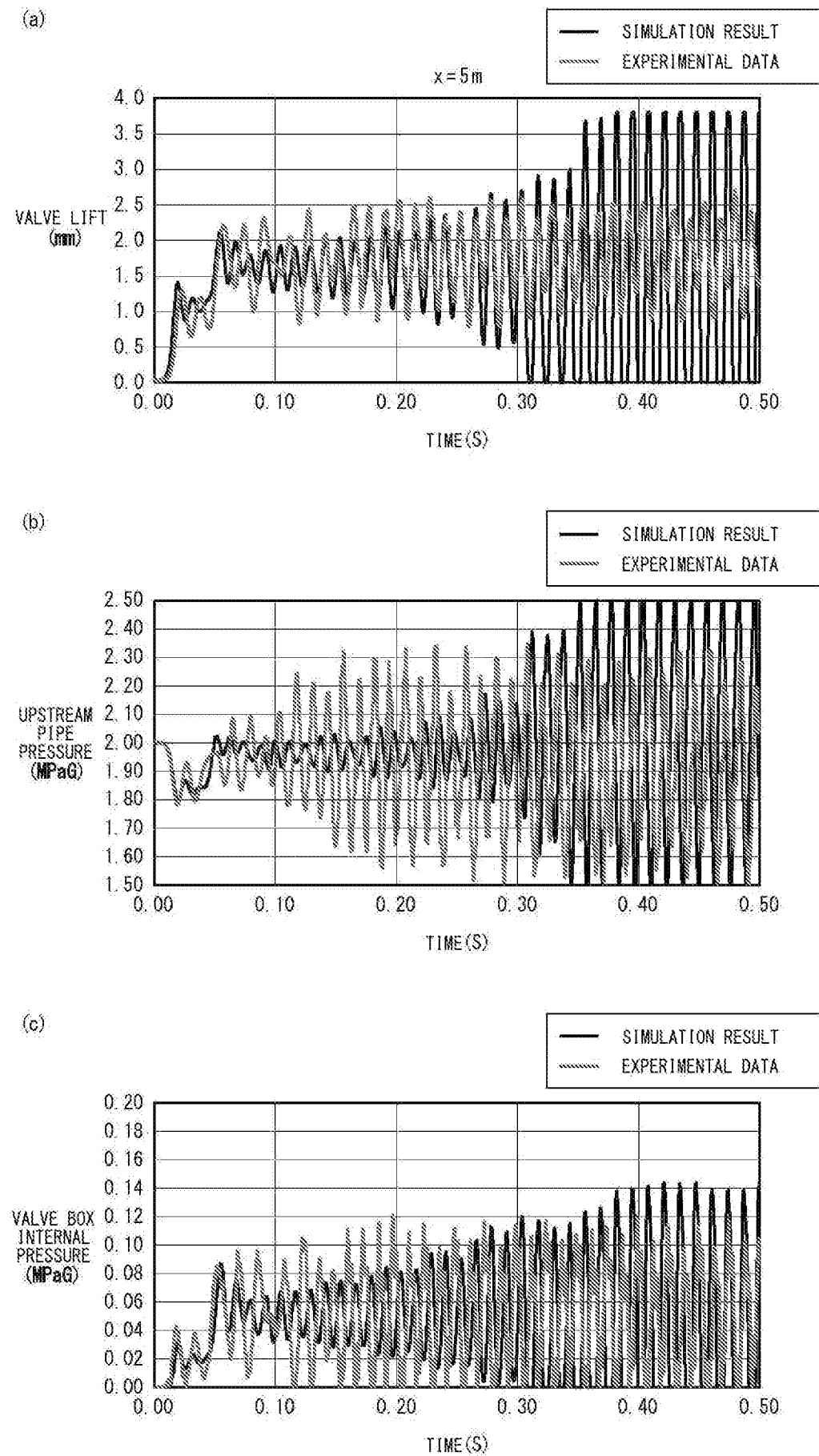
[Fig. 9]



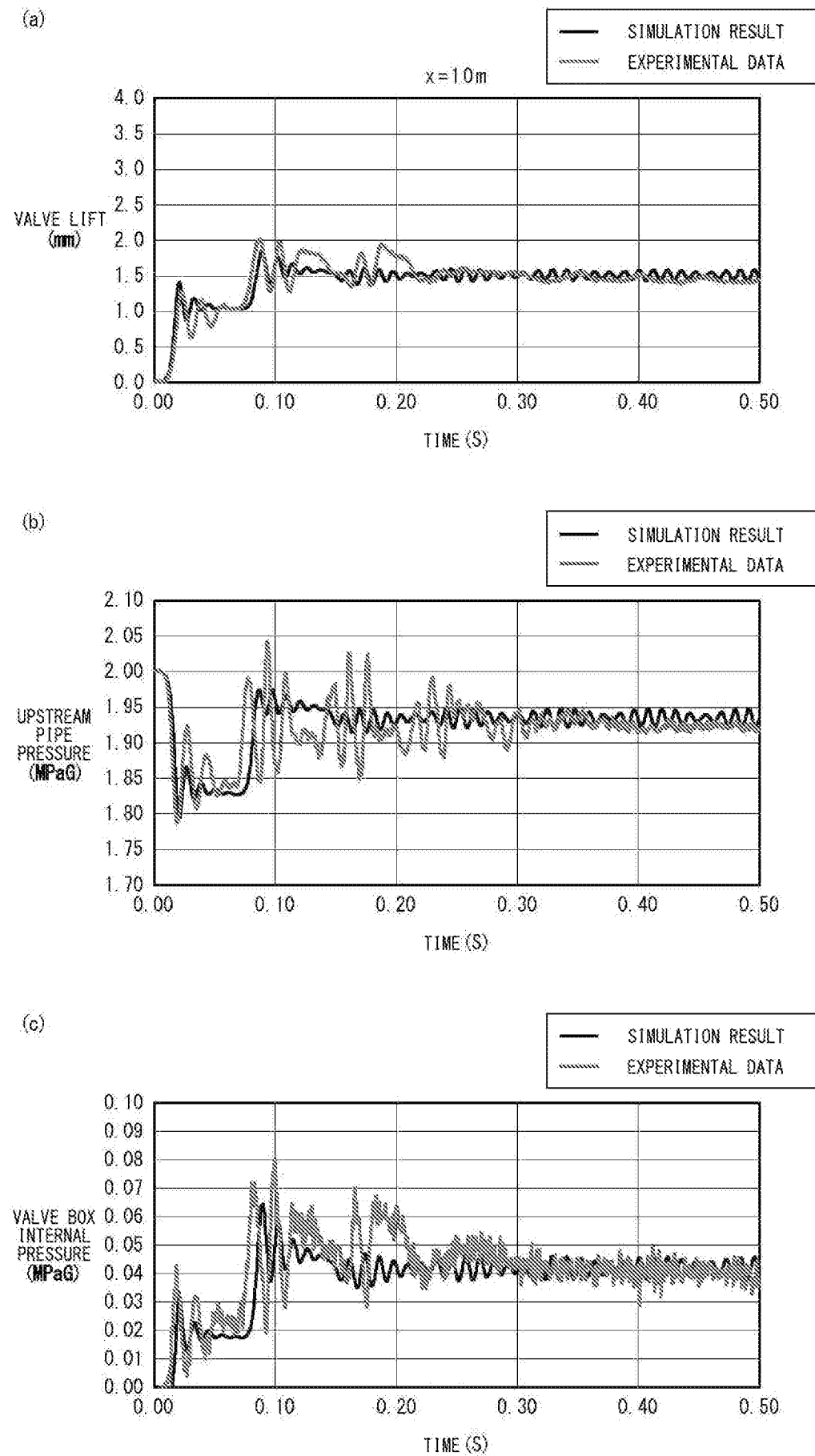
[Fig. 10]



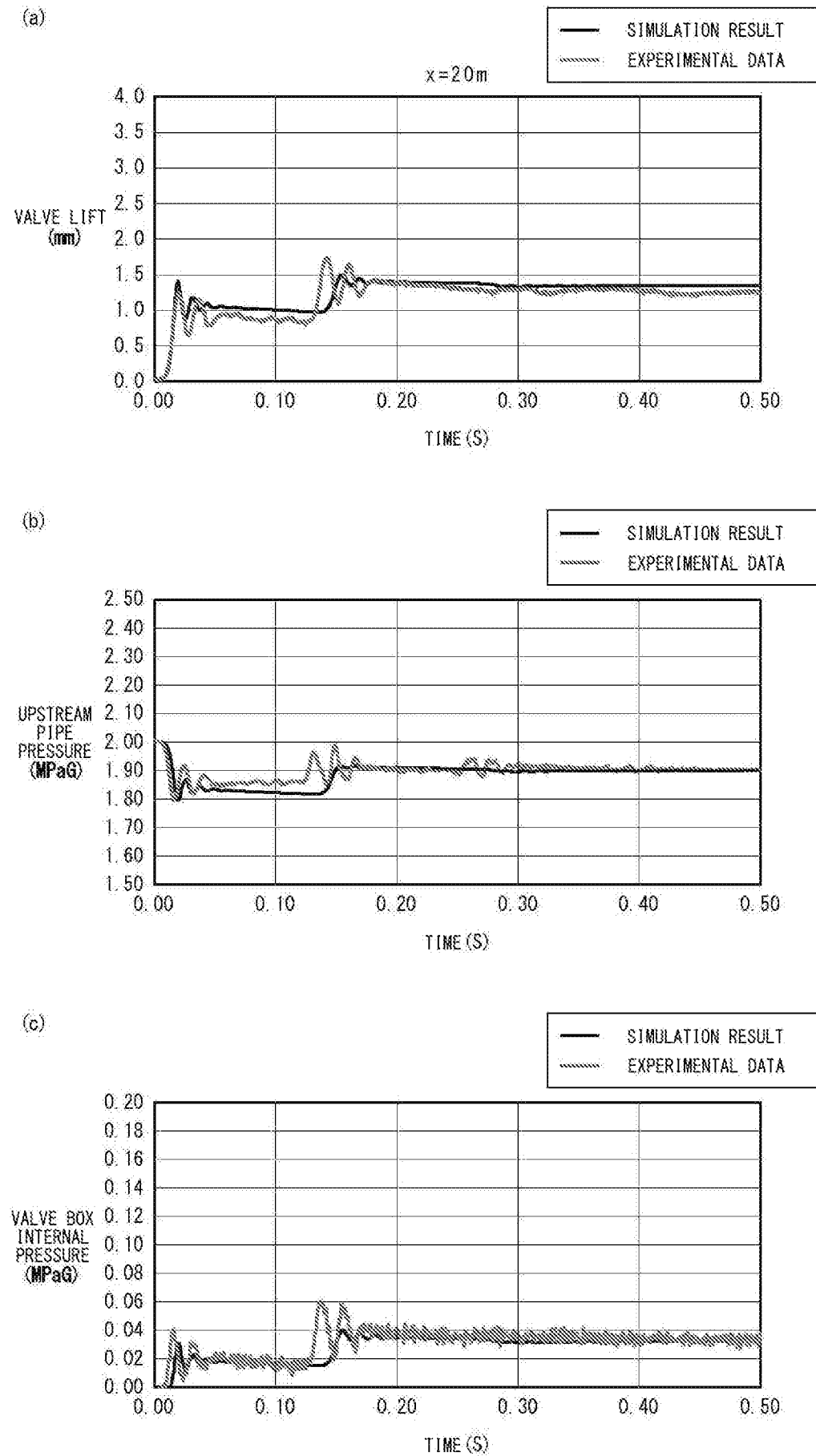
[Fig. 11]



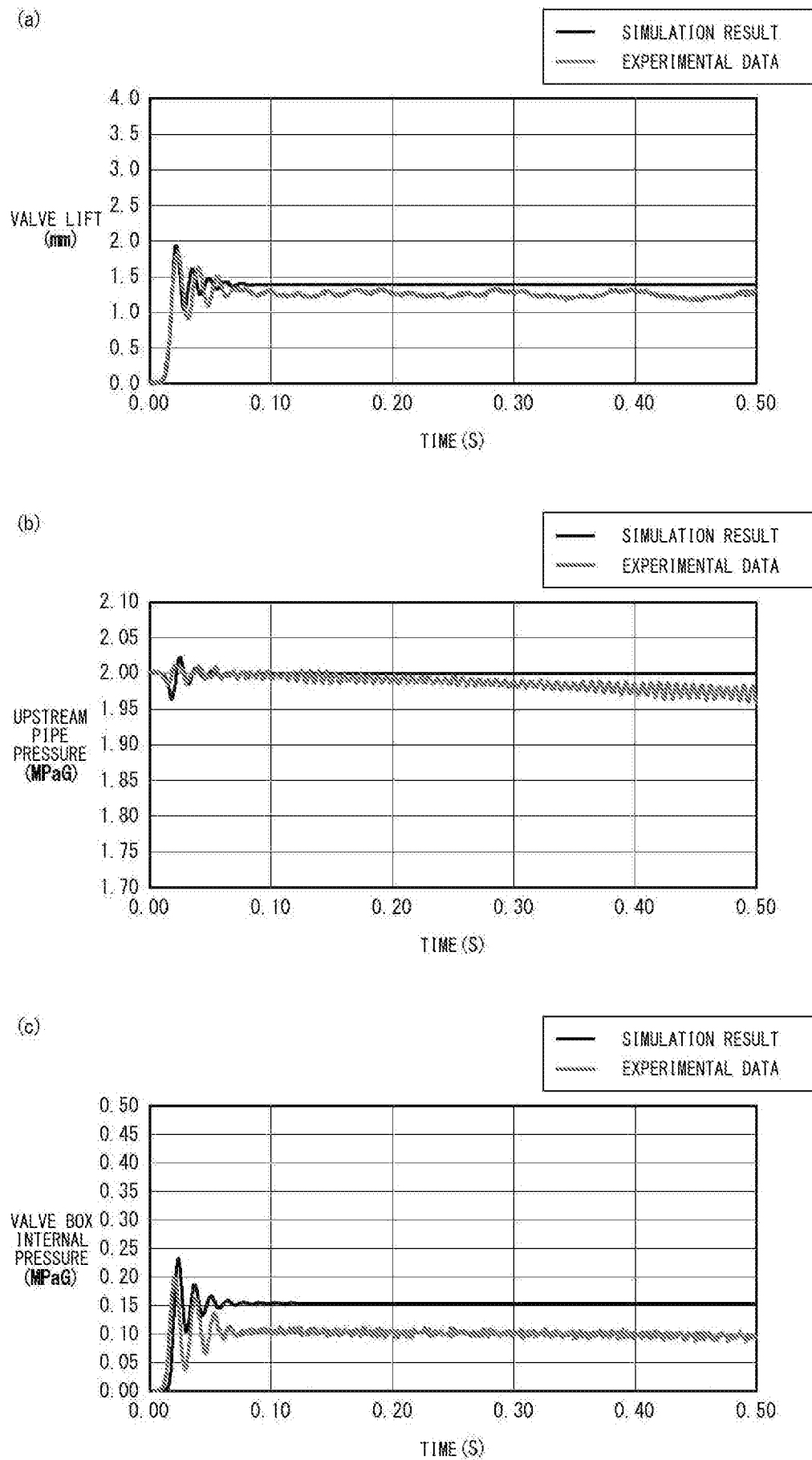
[Fig. 12]



[Fig. 13]



[Fig. 14]



[Fig. 15]

