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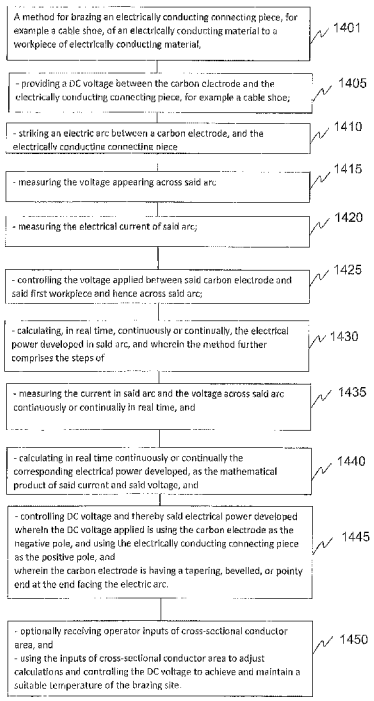
(54) Title: IMPROVED METHOD AND ARRANGEMENT FOR A MARTENSITE-FREE BRAZING PROCESS

Fig. 14B



(57) Abstract: A method for brazing an electrically conducting connecting piece, for example a cable shoe, of an electrically conducting material to a workpiece of electrically conducting material, by means of a temperature controlled brazing process in which the heat necessary for brazing is generated by striking an electric arc between a carbon electrode, and the electrically conducting connecting piece, where the voltage and current is electronically controlled by control electronics to achieve a temperature development to result in a martensite free brazing, and wherein the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole, and 0 wherein the carbon electrode is having a tapering, bevelled, or pointy end at the end facing the electric arc.

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IMPROVED METHOD AND ARRANGEMENT FOR A MARTENSITE-FREE BRAZING PROCESS

TECHNICAL FIELD

The present invention relates to an improved method for brazing for example a connecting piece of electrically conducting material, for example of metal, to a metal surface by means of an improved type of temperature-controlled brazing.

BACKGROUND

Temperature controlled brazing methods exist, whereby for certain types of material, for example steel, a martensite-free brazing can be obtained, i.e., brazing is effected without any deleterious structural changes (martensite formation) in the workpiece. A brazed joint is obtained with the part of the workpiece underneath the brazed joint being more or less free of martensite formation in for example railway track (rails), piping/pipelines, and wind power installations. The present invention relates to an improved method and an apparatus for carrying out the improved method.

Developments in railway traffic involve ever higher speeds and heavier axle loads. This in turn places increasing demands on the strength of railway track and its ability to withstand wear, and accordingly rails are manufactured from higher-alloyed steel in order to meet these more stringent requirements. The material from which rails are manufactured is sensitive to thermal influences that can cause structural changes known as martensite formation (hardening effect).

Martensite formation may lead to crack formation in the rail material and due to the higher loads, the rail may fracture, with catastrophic consequences for railway traffic. Consequently, it is very important to braze signal- and other wiring and cabling firmly to the rail by using a method that does not cause martensite formation in the rail.

Prior art in this field includes GB2376202 B, which discloses a method and an arrangement for a martensite-free brazing process.

SUMMARY OF THE INVENTION

The most serious problem in current methods employed on railway track is the large amount of heat that is produced underneath the brazing joint, which is caused by the electric arc that is generated in the brazing process and produces a deleterious structural change or martensite formation.

The gist of the present invention involves a special shape of an electrode used in the process, and further means for controlling an electrical voltage and an electrical current used in the process. Advantages of the method includes lower heat generation, lower power consumption, and an ability to conveniently braze connecting pieces for larger electrical conductor cross section areas than known technology. It is practically impossible today with known brazing technology to connect large cables, i.e., with cable cross section area larger than about 25-35 square millimetres, without significant martensite formation. Test of the new proposed method involving conductor cross section area of 120 square millimetres shows good results with none or only minimal martensite formation after brazing.

The present invention relates to a new method of temperature-controlled brazing together with an arrangement for carrying out the said method in which the problem of martensite formation, and at the same time power consumption, and heat production are reduced Further, the new method facilitates brazing of cable shoes for larger cross-sectional areas of the conducting wires involved.

An object of the present invention is to generate an electric arc via a carbon electrode so as to produce a brazed joint of a workpiece to a rail without the electric arc coming into direct contact with the rail and producing a connection of equal or better quality compared to prior art, but with less power consumption and less heat production.

A further object is to facilitate brazing of larger area electrical conductors than prior art allows.

In embodiments of the invention the carbon electrode itself constitutes an electrical resistance in the brazing process and the length, diameter and shape of the carbon electrode influence the electrical resistance in the process and consequently also influence the current intensity and voltage in the brazing process.

The carbon electrode provides an optimum control over the arc length during the brazing process since the carbon material has good refractory properties, whereas a metal electrode melts. Consequently, the carbon electrode undergoes a negligible change in length, during the brazing process as compared with a melting metal brazing pin.

Yet another object of the present brazing process as applied to the fixing of a cable shoe or other electrically conducting contact connection to a steel rail, is to prevent the electric arc coming into direct contact with the workpiece, which object is achieved if the electrically conducting contact connection consists of a solid plate of compact, electrically conducting material, for example copper. The brazing process, in this context, does not involve flux material or brazing material from any brazing pin forming an electrode. The brazing material does not have to flow through the cable shoe to the underlying workpiece (rail). Due to the construction of the cable shoe, flux material and brazing material are situated underneath the electrical contact connection or cable shoe itself. The whole plate of compact, electrically conducting material, for example copper, forms a buffer that prevents too high a temperature influencing for example the rail and leading to martensite formation. Furthermore, the electrode is not finally forced downwardly into the brazing and there is no risk of adversely affecting the brazed joint.

Another object of the present invention is to control the current intensity during the process. Raising the electrode increases the arc length. This in tum leads to a large voltage drop over the arc and to a reduced current intensity in the electrical circuit. The arc length cannot be increased completely arbitrarily since after a certain length the arc collapses due to the fact that the resistance becomes too great. A small interspacing between the electrode and workpiece, the so-called lifting height, reliably prevents the arc being extinguished during the brazing process. It is very advantageous to have a low current intensity during the process since this prevents martensite formation.

In the present invention it is preferred to use a guard ring of ceramics, but a guard ring consisting of a combination of both metal and ceramics materials may also be preferred since a combination effect increases the protection conferred on the brazing gun.

From the point of view of energy consumption, the material and design of the guard ring play an important role. The guard ring of embodiments of the present invention have been designed with a larger diameter to avoid to high temperatures of the guard ring and also with the advantage of being able to accommodate a larger volume of hot gases.

The guard ring together with the gripping sleeve also prevent the operator from coming into contact with the arc itself or with the hot gases that are formed. This reduces the need for protective equipment for the operator. This also eliminates the risk to the operator of eye injury and others who happen to look towards the arc during the brazing process.

According to a first aspect of the invention, there is provided a method for brazing an electrically conducting connecting piece, for example a cable shoe, of an electrically conducting material to a workpiece of electrically conducting material, by means of a temperature controlled brazing process in which the heat necessary for brazing is generated by striking an electric arc between a carbon electrode, and the electrically conducting connecting piece, the method comprising the steps of:

- providing a DC voltage between the carbon electrode and the electrically conducting connecting piece, for example a cable shoe;
- measuring the voltage appearing across said arc;
- measuring the electrical current of said arc;
- controlling the voltage applied between said carbon electrode and said first workpiece and hence across said arc;
- calculating, in real time, continuously or continually, the electrical power developed in said arc, and wherein the method further comprises the steps of
- measuring the current in said arc and the voltage across said arc continuously or continually in real time, and
- calculating in real time continuously or continually the corresponding electrical power developed, as the mathematical product of said current and said voltage, and
- controlling DC voltage and thereby said electrical power developed
wherein the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole, and
wherein the carbon electrode is having a tapering or pointy end at the end facing the electric arc.

The method may also include
- receiving of operator inputs of cross-sectional conductor area, and
- using the inputs to adjust calculations and controlling the DC voltage to achieve and maintain a suitable temperature of the brazing site.

According to a second aspect of the invention, there is provided an apparatus for brazing an electrically conducting connecting piece to a workpiece of electrically conducting material by means of a temperature-controlled brazing process in which the heat necessary for brazing is generated by striking an electric arc between a carbon electrode and the electrically conducting connecting piece, the apparatus including:

(a) means for engaging an electrically conducting connecting piece towards a workpiece, including a guard ring and a carbon electrode,

(b) means for supporting the electrode including means for moving the electrode between a position in which it engages the electrically conducting connecting piece in turn engaged by said means for engaging, and a retracted position in which it is lifted therefrom;

(c) a DC voltage unit for providing and applying a DC voltage of certain polarity between said electrically conducting connecting piece and said carbon electrode, and wherein said DC voltage unit includes a voltage regulating unit,

(d) a voltage sensor for measuring said voltage, between the electrically conducting connecting piece and the carbon electrode,

(e) a current sensor for measuring the electrical current passing through said carbon electrode;

(f) processing means including means for generating an output signal controlling said voltage-regulating unit and further including means for calculating, in real time, continuously or continually, the electrical power developed in said arc,

(g) switching means operable to connect said means for applying a voltage in electrical circuit with said electrode and with such electrically conducting connecting piece whereby, when said means for engaging is applied, and the switching means is operated to close said electrical circuit, said means for supporting and moving raises the electrode from the workpiece to strike an electric arc between the electrode and the electrically conducting connecting piece, and

(h) wherein the carbon electrode is provided with a pointy, tapering or bevelled first end for the electrical arc,

(i) wherein the DC voltage unit is configured such that the certain polarity being that the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole.

The apparatus may further be configured to automatically provide heat using a first electrical power during a first time-portion of the total brazing time, and a second electrical power during a second time-portion of the total brazing time. Preferably, the first electrical power is set to a value in order to rapidly heat up the brazing site, and the second electrical power is lower than the first electrical power, and of a value to maintain the achieved temperature at the brazing site.

To further tailor heating, a process having three or more distinct periods of different supply of heating may be provided. The process may for example have four periods or steps; Step 1 fast heating, Step 2 slow heating, Step 3 keeping the temperature, Step 4 slow cooldown.

The apparatus may still further be provided with input organs to set appropriate parameters for the electrical cross section area of the conductor to be brazed, and wherein the processor is configured to calculate time and voltage for the brazing, taking into account the parameters to provide appropriate voltage and time to accomplish a suitable amount of heat during an appropriate length of time.

This will have the advantage of a more precise tailoring of the brazing as regards e.g. times and temperatures.

According to a third aspect there is provided a cable shoe for a martensite free brazing, wherein a front portion is formed as a compact plate configured to be brazed into contact with a workpiece, a back end is formed to define a cable cavity for a cable, and wherein the cable shoe is further designed such that the cable cavity is extending into a tapering cavity, designed to give the cable shoe a uniform cross section area along its length from the compact plate to the beginning of the cable cavity. Tests have shown advantageously that cable shoes provided with the extended cavity, reduces the power needed to perform the brazing process. Further, the compact plate of the front portion may be provided with brazing material, such as an amount of silver alloy with or without flux material, that preferably is attached to the compact plate by pressing or by melting. Particularly advantageous is to manufacture the cable shoe by pressing a brazing clip comprising the silver alloy towards the compact plate, thereby attaching it to the compact plate.

DRAWINGS

Embodiments of the present invention are described below in more detail with reference to the accompanying drawings, in which;
Fig. 1A shows diagrammatically an outline of the brazing process;
Fig. 1B shows a detail of Fig. 1A.
Fig. 1C shows schematically directions of movement of ions and electrons of the brazing arc;
Fig. 1D shows schematically directions of movement of ions and electrons of the brazing arc, with reversed polarity compared to Fig. 1C.;
Fig. 2 is a partial side view of a brazing gun embodying the invention;
Fig. 3 shows the brazing gun viewed in cross-section;
Fig. 4 is a side view of the brazing gun, partly in longitudinal (axial) section;
Fig. 5 shows a brazing operation on a rail;
Fig. 6 shows a brazing operation on a pipeline section;
Fig. 7 illustrates a brazed joint between the outer and inner wheel rims of a railway carriage;
Fig. 8 shows an electrically conducting connecting piece in the form of a cable shoe seen from the side;
Fig. 9 is also a side view of a cable shoe;
Fig. 10A shows a cable shoe seen from above;
Fig. 10B is a view of the cable shoe of Fig. 10A seen from behind;
Fig. 10 C is a side view of the cable shoe of Fig. 10A
Fig. 10 D is a front view of the cable shoe of Fig. 10A
Fig. 11 is a voltage/current/temperature diagram of a brazing process according to prior art;
Fig. 12A is a voltage/current/temperature diagram of a brazing process according to a new method applied to a first cross section area
Fig. 12B is a current/voltage/temperature diagram of a brazing process according to a new method applied to a second cross section area
Fig. 13 is a front view of a principal input panel for entering brazing parameter(s).
Fig. 14A is a control and regulation flow chart of the brazing process;
Fig. 14 B is a flow diagram over method steps;
Fig. 15A is a partial view of the front part of the brazing gun, partly in longitudinal (axial)

section.
Fig. 15B, C, D are side views of carbon electrodes of embodiments of the present invention.
Fig. 15 E is a top view of a circular cross section electrode and below a top view of a quadratic cross section electrode.

DETAILED DESCRIPTION

Fig. 1A illustrates diagrammatically the necessary components and the procedure of the brazing process per se, according to the embodiment concerned, the power source that is normally used being a battery 1 from which the current is conducted to an electronics unit 2. The electronics unit 2 being configured to process data received from the brazing gun 5 via its power supply cable and signal cable as well as data from the external power source. The electronics unit 2 being configured to process all information and to regulate the current and voltage supply to the brazing gun 5, for example by regulating the voltage level electronically. By said regulation, the time and current consumption can be controlled during the brazing process and in this way a satisfactory brazing can be achieved, with minimal energy consumption, also combined with a control of the temperature in the base material/workpiece.

When the circuit breaker 3 closes the electrical circuit comprising a lifting magnet in the brazing gun 5, the carbon electrode 6 that is situated in the electrode holder 7 initially short-circuits the circuit with the cable shoe 10, so that when subsequently the electromagnet lifts the carbon electrode 6 from the cable shoe 10 to light an electric arc 8 that is protected by one or more guard rings 9, it operates on a compact flat surface of a cable shoe 10, the cable shoe forming one pole and the carbon electrode 6 forming the other pole. Heat is transmitted via the cable shoe 10 and activates the flux material between the cable shoe 10 and a brazing material 12 and prepares and cleans the surface for a brazing between the brazing material 12 and cable shoe 10, and when the brazing material 12 heats up it activates the flux material 13 on the workpiece 14 and a brazed joint is formed by the brazing material 12 on the workpiece 14. Consequently, the cable shoe 10 is brazed firmly to the workpiece 14 without the electric arc 18 coming into direct contact with the said workpiece 14.

Furthermore, no undesired sparks/arcs are produced between the workpiece 14 and the cable shoe 10 since the electrical circuit is formed via a cable of the cable shoe 10 or via the guard ring 9, and not via the workpiece 14 per se.

In the new brazing process the whole plate of compact, electrically conducting material, for example copper, forms a buffer that prevents high temperatures affecting for example the rail and leading to martensite formation. Cupper particles will be emitted from the plate of the cable shoe during the brazing process and will be deposited in the form of a thin layer on the carbon electrode, see Fig. 1C. A small cavity may form in the cable shoe 10 during the brazing process. The cable shoe may be configured to allow for this cavity forming, without compromising the mechanical strength of the cable shoe to any significant level.

Fig. 1D shows schematically directions of movement of ions and electrons of the brazing arc, with reversed polarity compared to Fig. 1C. The oval area is showing the width of the arc, suggesting that a thinner, more focussed arc is achieved using a polarity corresponding

to a negative carbon electrode, Fig. 1C, and a wider or blurrier arc will result from connecting the carbon electrode to a positive polarity. Tests have shown that the choice of negative polarity of the carbon electrode reduces the energy needed to perform a brazing. The energy reduction is approximately around 30%.

From an energy point of view the guard ring, has an important role during the brazing process. The guard ring 9 is formed so that it exhibits a good thermally insulating function. The guard ring 9 may be formed of a ceramic material, and provided with a toothed lower edge. In this case the hot gases that are formed during the brazing process are discharged radially. When the guard ring is formed of metal, with a smooth lower surface, the gases will leave the guard ring in the axial direction and therefore more heat will be transmitted to the guard ring 9. The guard ring 9 retains its shape and function and is stable during the whole brazing process. The heat that is absorbed by the guard ring is conducted to the cable shoe 10. The result is that less electrical energy and/or power is consumed during the brazing process and a martensite-free brazing takes place.

Fig. 2 is a side view of the brazing gun 5, at the front of which can be seen the carbon electrode 6. Before starting the brazing process, the gun 5 together with the carbon electrode 6 is pressed down against the cable shoe 10, whereby the carbon electrode 6 being pressed flush with the lower edge of the guard ring 9. The guard ring 9 is secured in a ring holder 15. When the circuit breaker or start button 3 is pressed, the circuit is short-circuited, following which the lifting magnet raises the electrode 6 a certain height over the electrically conducting connecting piece 10 and an arc 8 is struck. The guard ring 9 and a gripping sleeve 18 shield the operator from the process. The figure also shows a screw 16 for ejecting the guard ring and a screw 17 for ejecting the electrode. During the brazing process the guard ring 9 can act as a terminal in a grounding operation, if manufactured of metal or other electrically conducting material.

Fig. 3 shows a section of the brazing gun 5 seen from the front, in which the circuit breaker 3 can be seen and in the centre of the mouth of the gun is located the carbon electrode 6 in the electrode holder 7 together with the ring holder 15 and gripping sleeve 18.

Fig. 4 shows an end part of the brazing gun 5 in section and shows the circuit breaker 3, the carbon electrode 6 in the electrode holder 7 and guard ring 9 of ceramic material in the ring holder 15 together with the gripping sleeve 18, the screw 16 for ejecting the guard ring and the screw 17 for ejecting the electrode. A very important component in the brazing process is the carbon electrode, which forms an electrical resistance, and in which the length, diameter and shape of the carbon electrode influences the electrical resistance in the process. The current strength and the voltage during the brazing procedure are controlled by the control electronics. The control electronics is configured to provide a voltage and a current as a function of time according to Figures 12B, 12C, and 12D to achieve a suitable brazing temperature at the brazing site, see further below.

Fig. 5 shows a brazing gun 5 that is used on a rail 14. An electrically conducting piece 10 in the shape of a cable clip is brazed firmly to the head of the rail. The brazing may also be carried out on the web part or on the foot of the rail.

Fig. 6 shows a brazing gun 5 that is used on a workpiece 14 in the form of a section of piping. An electrically conducting connecting piece 10 in the shape of a cable shoe is brazed firmly to the pipe. Stringent requirements apply above all to piping in nuclear power

stations, where brazing has to be carried out without causing structural changes in the piping material that could lead to crack formation. In the cases where pipes are filled with gas or oil, and also when they are filled with material that is temperature-sensitive, for example in the chemical industry, it is important to be able to work at low temperatures when brazing.

Fig. 7 shows a railway carriage wheel. An inner wheel 20 is secured to the wheel axle 21 and between the inner wheel and an outer wheel ring 19, the so-called tread, is arranged a damper 23 of for example rubber material. The figure shows how a connecting piece 22 of electrically conducting connecting material joins the inner wheel 20 to the outer wheel ring 19 so that a current can pass from the railway carriage to the railway track. On account of the risk of martensite formation and associated crack formation it has not hitherto been attempted to employ pin brazing in this connection. The present brazing process eliminates martensite formation in any case and enables brazing to be carried out in this field too.

Fig. 8 is a side view of a cable shoe 10, a connecting piece of electrically conducting material, in which a terminal connector 24 to the electrical circuit can be seen. The terminal connector 24 is secured to an electrical cable 25 leading to the cable shoe 10, the other side of which consists of a solid plate 26 of compact material. Around this continuous plate 26 of compact material is arranged a brazing clip 27, which is pressed against the plate 26 of the cable shoe 10 per se during manufacturing, and between the cable shoe 10 and the brazing clip 27 there is provided a flux material 28 that is activated during the brazing process.

Fig. 9 is also a side view of a cable shoe 10 in which the brazing per se is performed on a flat continuous compact plate 26 of the cable shoe 10 by means of the brazing gun 5, and in which can be seen the brazing clip 12, which is pressed against the cable shoe 10, a flux material 11 being heated between the lower side of the cable shoe 10 and the brazing clip 12. Another flux material 13 is provided between the workpiece 14 and the clip 27 and is activated when the brazing clip 27 is heated up and begins to clean the workpiece 14 before brazing of the electrically conducting connecting piece 10.

The brazing clip 12 is of uniform thickness prior to its application to the workpiece to which it is secured. Once the brazing material has been melted by the heat applied through the compact plate 26 of the cable shoe 10 surface tension in the molten material wetting the compact plate 26 and the workpiece 14 leads to a change in thickness, in the sense that the distance between the compact pate 26 and the workpiece, i.e. of the region occupied by the brazing material, is minimised, thus ensuring a firm bond and good electrical and thermal conductivity between the compact plate 26 and the workpiece. The flux material 11 and 13 fulfils the following tasks and has the following properties:
1) cleans the surfaces, 2) removes any oxides present, 3) prevents re-oxidation, 4) is displaced by the molten brazing material, 5) acts as an electrical conductor when the cable shoe 10 is grounded via the rail, 6) facilitates dissipation of heat due to the fact that it has a good thermal conductivity, and 7) wets the surfaces that are to be joined.

Another requirement is that the flux material 28 and 29 should be activated within a specific temperature range. The flux material, brazing material and brazing process must be matched to one another. The flux material is already activated at the start of the brazing process and will continue to be effective until the brazing has been accomplished.

A brazing that is carried out above ca. 500°C is termed hard brazing, as opposed to soft brazing, which takes place at lower temperatures. The brazing material that is used in the brazing process of the present application is intended for hard brazing. However, flux material that is intended for hard brazing is not suitable for the present process since the process takes place too quickly, in about 2 seconds. In the present brazing process, a flux material 10 is used that is normally suitable for soft brazing and accordingly is activated at a lower temperature but does not disintegrate before the brazing is completed due to the short operating time.

In order to reach a necessary brazing temperature but using as little energy as possible a large power input is required over a short period of time. Railway track, thick-walled pipes and similar metal profiles are effective heat sinks. A large power input creates a heat front that moves via the cable shoe down into the rail, where the temperature becomes suitable for hard brazing but does not lead to martensite formation.

The cable shoe 10 is a buffer against local overheating and produces a relatively smooth temperature distribution over the whole molten surface. An indirect heating-up takes place by means of a carbon electrode 6. An electric arc 8 is formed between the carbon electrode 6 and the cable shoe 10. This contrasts with conventional pin brazing, in which an arc acts directly on the rail and/or molten brazing on the rail.

Fig. 10A shows a cable shoe 10 seen from above. A front portion is formed as a compact plate 26 in which a brazing clip 27 is mounted. A dashed line indicates definition of a cable cavity 31 for a cable. The cable shoe 10 is further designed such that the cable cavity 31 is extending into a tapering cavity 33, designed to give the cable shoe 10 a uniform cross section area from the compact plate to the beginning of the fitted cable.

Fig. 10B is a view of the cable shoe of Fig. 10A seen from behind.

Fig. 10 C is a side view of the cable shoe of Fig. 10A, and Fig. 10 D is a front view of the cable shoe of Fig. 10A.

Thus, there is provided a cable shoe for a martensite free brazing, wherein a front portion is formed as a compact plate configured to be brazed into contact with a workpiece, a back end is formed to define a cable cavity for a cable, and wherein the cable shoe is further designed such that the cable cavity is extending into a tapering cavity, designed to give the cable shoe a uniform cross section area along its length from the compact plate to the beginning of the cable cavity. Tests have shown advantageously that cable shoes provided with the extended cavity, reduces the power needed to perform the brazing process. Further, the compact plate of the front portion may be provided with brazing material, such as an amount of silver alloy with or without flux material, that preferably is attached to the compact plate by pressing or by melting. Particularly advantageous is to manufacture the cable shoe by pressing a brazing clip comprising the silver alloy towards the compact plate, thereby attaching it to the compact plate.

With railway signal systems and cathode protection systems that operate at low voltages and currents, it is particularly important to have a low overall transition resistance in the brazed joints 50 as to prevent interference in the system.

With large currents and voltages, a high transition resistance generates heat in the brazed joint, which may damage and/or melt the latter. For this reason, it is important to have a

low transition resistance in the brazed joint since the connection also has to handle high return currents in the railway operating system. For a similar reason it is also important that the transition resistance is low in protective groundings.

Fig. 11 is a voltage/current/temperature diagram of a brazing process according to prior art;

Fig. 12A and B is a voltage/current/temperature diagram of the new brazing process. Compared to existing pin brazing, there is no similar large current surge when a short-circuit occurs. Both the voltage and current curves are comparatively more constant over time. The diagram shows that the present invention provides an optimal control of the brazing process. Consequently, the temperatures during the brazing process can also be regulated and controlled, which is a prerequisite for obtaining a martensite-free brazing.

Compared to some prior art martensite free brazing, the apparatus and method of the present invention may include a two-phase process in which voltage is automatically controlled to provide heat using a first electrical power during a first time-portion of the total brazing time, and a second electrical power during a second time-portion of the total brazing time. Preferably, the first electrical power is set to a value in order to rapidly heat up the brazing site, and the second electrical power is lower than the first electrical power, and of a value to maintain the achieved temperature at the brazing site.

Fig. 12A is a voltage/current/temperature diagram of a brazing process according to a new method applied to a first cross section area. A strength of the new method is the ability to achieve brazing of larger cross section areas. The cross-section area brazed and giving rise to the diagram of Fig. 12A is 16 square mm.
Fig. 12B is a current/voltage/temperature diagram of a brazing process according to a new method applied to a second cross section area. The cross-section area brazed and giving rise to the diagram of Fig. 12B is 120 square mm.

Fig. 13 shows a front view of a principal input panel for entering brazing parameter(s). Input buttons, keys or knobs are provided to enter settings, i.e., by repeatedly pressing a settings button, a list is scrolled to select a setting of a list of predefined settings for different cross section areas, e.g., 10, 16, 25, 35, 50, 70, 95, and 120 square millimetres. The settings may include voltage, and/or current, and time periods for providing a certain volage/current, as further shown in Figs 12A and 12B. The panel further includes a display showing the current setting. The panel further may include, fuses and/or control indicators, and on/off-button. Still further, the input panel may further have sockets for connecting plugs to the brazing gun, for connecting ground, and for connecting a charger for charging the batteries of the brazing apparatus.

Fig. 14A shows a regulation and control flow diagram of the brazing process.

Fig. 14B shows a flowchart of the method steps. There is provided a method for brazing an electrically conducting connecting piece, for example a cable shoe, of an electrically conducting material to a workpiece of electrically conducting material, by means of a temperature controlled brazing process in which the heat necessary for brazing is generated by striking 1410 an electric arc between a carbon electrode, and the electrically conducting connecting piece, the method comprising the steps of:
- providing 1401 an electrically conducting connecting piece, for example a cable shoe;
- providing 1401 a workpiece of electrically conducting material;

- providing 1405 a carbon electrode;
- providing 1405 a DC voltage between the carbon electrode and the electrically conducting connecting piece, for example a cable shoe;
- measuring 1415 the voltage appearing across said arc;
- measuring 1420 the electrical current of said arc;
- controlling 1425 the voltage applied between said carbon electrode and said electrically conducting connecting piece and hence across said arc;
- calculating 1430, in real time, continuously or continually, the electrical power developed in said arc, and wherein the method further comprises the steps of
- measuring 1435 the current in said arc and the voltage across said arc continuously or continually in real time, and
- calculating 1440 in real time continuously or continually the corresponding electrical power developed, as the mathematical product of said current and said voltage, and
- controlling 1445 DC voltage and thereby said electrical power developed

wherein the DC voltage applied is using the carbon electrode as the negative pole, and using 1445 the electrically conducting connecting piece as the positive pole, and wherein the carbon electrode is having a tapering, bevelled or pointy end at the end facing the electric arc.

The process may further include the steps of automatically provide heat using a first electrical power during a first time-portion of the total brazing time, and provide a second electrical power during a second time-portion of the total brazing time. Preferably, the first electrical power is set to a value to rapidly heat up the brazing site, and the second electrical power is lower than the first electrical power, and of a value to maintain the achieved temperature at the brazing site.

Fig. 15A shows in section the front part of the brazing gun 5 with a gripping sleeve 18 in the retracted position, and an electrode ejector 40 is shown with a screw 16 for a guard ring ejector and a screw 17 for the electrode ejector. The ejected carbon electrode 6 and the ejected guard ring 9 are also shown.

Fig. 15B to 15E shows alternate shapes of the carbon electrode having different top angles Beta and bevel angles Alfa α, as shown in Fig. 15 F. The carbon electrode may be provided with a circular or rectangular, particularly a quadratic section. A circular cross section is preferred. Thus, the carbon electrode is provided with a pointy or bevelled end preferably having a top angle Beta β of between 90 and 150 degrees, and more preferred an angle between 100 and 140, and even more preferred between 110 and 130 degrees, and most preferred between 118 and 122 degrees.

The basic concept of the present invention is to combine various functions and methods in such a way that they co-operate in an improved brazing process. The result of the co-operation is a new brazing process which is free of structural changes or martensite formation which saves energy and also facilitates the brazing of large cross section area of the conductor to be brazed. A carbon electrode is employed in the brazing process whose length and diameter influence the resistance in the electrical circuit and in which the carbon electrode is provided with a pointy or bevelled end, and acts as a temperature buffer and heat distributor. In addition, the electric arc is maintained between the carbon electrode and a smooth end of a cable shoe, see below, which has a stabilising effect on the arc and counteracts the tendency to varying currents over time.

A cable shoe has at least one smooth end of compact, electrically conducting material on which the electric arc from the carbon electrode acts. The lower side of the cable shoe has a clip of brazing material, which is secured during manufacture. The brazing produces a brazed joint of large area, resulting in a lower overall electrical transition resistance. A flux material is present between the cable shoe and the brazing clip, and a flux material is also present between the brazing clip and the workpiece, the flux material, brazing material and brazing process being suitably adapted to one another. The brazing material is suitable for soft brazing and is consequently active over a low temperature range, thereby providing a martensite-free brazing.

The advantages of a guard ring in the brazing process that consists for example of metal or another similar material is that the overall process requires less energy, and also the grounding procedure is facilitated compared to previous procedures. Grounding via the guard ring eliminates the need for special grounding contacts, for example ground terminals or magnetic grounding contacts, as well as the need for special preparation of the grounding carrier. Since in every grounding situation a new guard ring is used, the contact surfaces are always guaranteed to be clean.

The arrangement according to the invention reduces the length of the grounding circuit and eliminates extra transition resistance as well as sources of secondary sparks and arcs between the cable shoe and the workpiece. The shape of the guard ring together with the gripping sleeve shields the operator from electric arcs and hot gases during the brazing process.

The use of metal guard rings influences the brazing procedure by virtue of the fact that it utilises more of the energy released in the form of heat and channels it to the cable shoe.

In order to achieve a satisfactory brazing having regard to temperature, not as much electrical energy has to be supplied therefore to the brazing process.

With previously known methods the total intrinsic resistance in the circuit may be regarded as constant. A lower energy supply should in practice mean a shorter process time. However, the time then becomes far too short for a satisfactory brazing to be achieved.

By regulating the additional resistance and/or regulating the voltage the length of the brazing process can be controlled and, in this way, a satisfactory martensite-free brazing can be achieved with minimal expenditure of energy and in addition the temperature in the base material/workpiece can also be controlled.

With some previously known methods wide margins have been accepted as regards the developed electrical power in the process as well as the total emitted energy and also the overall length of the process. The current was limited either by incorporating a fixed electrical resistance in the circuit, or alternatively by interrupting the process when the necessary amount of emitted energy has been consumed. No account was taken of variations in battery voltage depending on the state of charge of the battery, discharge characteristics or other factors, nor of variations in current during one and the same brazing operation depending on the change in length of the electrode or arc fluctuations, or changes in current between different brazing cases depending on variations in the lifting height. These variations together with simple inadequate arrangements for estimating the amount of energy emitted have resulted in a varying time and varying power output for

otherwise comparable brazing processes, as well as difficulties in controlling the temperature in the relevant materials.

In the afore described new brazing process shown in Fig. 14, the brazing temperature and the martensite formation dependent on the latter may be controlled by calculating the electrically developed power and regulating the latter in real time either by an analogue procedure or by a digital procedure with high resolution. The developed power is calculated by instantaneously measuring the current and voltage, and the actual power is calculated as the mathematical product of these quantities. The calculated result is processed and fed into a processing unit whose output signal influences a voltage-regulating unit. In this way the voltage and thereby the current are regulated, and the developed electrical power is adjusted to an appropriate value. The processing unit, which may either exist as a separate unit or may be incorporated in the electronics unit 2, processes data in the form of current and voltage values, data from transmitters and operational adjustments, externally connected units as well as measured elapsed time, and handles this data having regard to physical, mathematical and logic structures in such a way that an appropriate regulation of the developed power takes place over time.

As an example, operator inputs of conductor cross sectional area are used by the processor, which is configured to adjust the control signal to control the voltage to produce a current that produces the right amount of power to heat up and maintain suitable temperature at the brazing.

Also, since the regulation is independent of the resistance of the power circuit there is no need to have a fixed installed resistor, and accordingly there is an energy saving since this resistor produces waste heat. In addition, a larger amount of energy can be withdrawn from the batteries since at the end of the discharge cycle the batteries can still drive the process despite the failing voltage level since there is no fixed resistor. Moreover the formation of the arc at the starting point of the process is facilitated for two reasons, on the one hand because the lifting height of the electrode and thus the length of the arc and consequently the following starting inertia can be minimised without any risk of excessive currents that in some previous methods caused temperature problems and regulating technology problems, and on the other hand much higher current and voltage values than were hitherto possible, are allowed at the starting point of the process without being limited to a fixed resistor, and consequently a reliable start to the process can be ensured.

In the afore described new brazing process the aforementioned processing unit may also be configured to handle signals from external transmitters, for example temperature sensors, as well as operational adjustments whose values affect the output data of the processing unit. In addition, signals from external units such as battery chargers, generators and motors are processed; these signals are also processed in the processing unit when appropriate control signals in the form of output data are produced so as to regulate this kind of unit(s) too.

Only some embodiments of the invention have been illustrated in the drawings, but it should be pointed out that many other modifications can be conceived within the scope of the following claims.

In a preferred embodiment, the carbon electrode is provided with a tapered, pointy or bevelled end having a top angle Beta β of between 70 and 150 degrees, more preferably

having a top angle between 70 and 110 degrees, and yet more preferably having a top angle between 90 and 110 degrees.

CLAIMS

1. A method for brazing an electrically conducting connecting piece, for example a cable shoe, of an electrically conducting material to a workpiece of electrically conducting material, by means of a temperature controlled brazing process in which the heat necessary for brazing is generated by striking an electric arc between a carbon electrode, and the electrically conducting connecting piece, the method comprising the steps of:

- providing (1405) a DC voltage between the carbon electrode and the electrically conducting connecting piece, for example a cable shoe;
- measuring (1415) the voltage appearing across said arc;
- measuring 1420) the electrical current of said arc;
- controlling (1425) the voltage applied between said carbon electrode and said electrically conducting connecting piece, and hence across said arc;
- calculating (1430), in real time, continuously or continually, the electrical power developed in said arc, and wherein the method further comprises the steps of
- measuring (1435) the current in said arc and the voltage across said arc continuously or continually in real time, and
- calculating (1440) in real time continuously or continually the corresponding electrical power developed, as the mathematical product of said current and said voltage, and
- controlling (1445) DC voltage and thereby said electrical power developed
wherein the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole, and
wherein the carbon electrode is having a tapering, bevelled, or pointy end at the end facing the electric arc.

2. A method according to Claim 1, wherein the method further comprises the steps of
- receiving of operator inputs of cross-sectional conductor area, and
- using the inputs of cross-sectional conductor area to adjust calculations and controlling the DC voltage to achieve and maintain a suitable temperature of the brazing site.

3. A method according to Claim 1 or 2, further including the step of automatically provide heat using a first electrical power during a first time-portion of the total brazing time, and a second electrical power during a second time-portion of the total brazing time.

4. A method according to Claim 1, further including the steps of raising the electrode from the first workpiece to strike an electric arc between the electrode and the electrically conducting connecting piece.

5. A method according to Claim 1 wherein the carbon electrode is provided with a pointy or bevelled end preferably having a top angle of between 90 and 150 degrees, and more

preferred an angle between 100 and 140, and even more preferred between 110 and 130 degrees, and most preferred between 118 and 122 degrees.

6. An apparatus for brazing an electrically conducting connecting piece to a workpiece of electrically conducting material by means of a temperature-controlled brazing process in which the heat necessary for brazing is generated by striking an electric arc between a carbon electrode and the electrically conducting connecting piece, the apparatus including:

(a) means for engaging an electrically conducting connecting piece towards a workpiece, including a guard ring and a carbon electrode,

(b) means for supporting the electrode including means for moving the electrode between a position in which it engages the electrically conducting connecting piece in turn engaged by said means for engaging, and a retracted position in which it is lifted therefrom;

(c) a DC voltage unit for providing and applying a DC voltage of certain polarity between said electrically conducting connecting piece and said carbon electrode, and wherein said DC voltage unit includes a voltage regulating unit,

(d) a voltage sensor for measuring said voltage, between the electrically conducting connecting piece and the carbon electrode,

(e) a current sensor for measuring the electrical current passing through said carbon electrode;

(f) processing means including means for generating an output signal controlling said voltage-regulating unit and further including means for calculating, in real time, continuously or continually, the electrical power developed in said arc,

(g) switching means operable to connect said means for applying a voltage in electrical circuit with said electrode and with such electrically conducting connecting piece whereby, when said means for engaging is applied, and the switching means is operated to close said electrical circuit, said means for supporting and moving raises the electrode from the workpiece to strike an electric arc between the electrode and the electrically conducting connecting piece, and

(h) wherein the carbon electrode is provided with a pointy, tapering or bevelled first end for the electrical arc,

(i) wherein the DC voltage unit is configured such that the certain polarity being that the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole.

7. Apparatus according to Claim 6, wherein the apparatus is configured to automatically provide heat using a first electrical power during a first time-portion of the total brazing time, and a second electrical power during a second time-portion of the total brazing time.

8. Apparatus according to claim 7, wherein the first electrical power is set to a value in order to rapidly heat up the brazing site, and the second electrical power is lower than the

first electrical power, and of a value calculated to maintain the achieved temperature at the brazing site.

9. Apparatus according to claim 6, wherein the apparatus is provided with input organs to set appropriate parameters for the electrical cross section area of the conductor to be brazed, and
wherein the processor is configured to calculate time and voltage for the brazing, taking into account the parameters to provide appropriate voltage and time to accomplish a suitable amount of heat during an appropriate length of time.

10. Apparatus according to claim 7, 8 or 9 including a gripping sleeve around said guard ring, whereby the guard ring together with gripping sleeve shields the operator from the arc and from hot gases.

11. Apparatus according to claim 10 in which the gripping sleeve ejects with a longitudinal movement spent electrodes and guard rings.

12. Apparatus according to any of claims 6 to 11, wherein said processing means is additionally capable of controlling external units such as battery chargers, generators, and motors in order to regulate these units.

13. Apparatus according to any of claims 6 to 12 in combination with an electrically conducting connecting piece for brazing to a workpiece, the electrically conducting connecting piece having on one side a layer of brazing metal, with a flux layer between the first workpiece and the layer of brazing metal.

14. The combination of claim 13, in which the layer of brazing metal is provided by a brazing clip applied to said first workpiece.

15. The combination of claim 14 including an electrical connection to the connecting piece to provide a grounding contact for the apparatus.

16. An apparatus according to any of claims 6 to 15, wherein the carbon electrode is provided with a pointy, tapered, or bevelled end preferably having a top angle of between 90 and 150 degrees, and more preferred an angle between 100 and 140, and even more preferred between 110 and 130 degrees, and most preferred between 118 and 122 degrees.

17. A brazing method substantially as hereinbefore described with reference to the accompanying drawings.

18. A brazing apparatus substantially as hereinbefore described with reference to, and as shown in, the accompanying drawings.

19. A cable shoe (10) wherein a front portion is formed as a compact plate (26), a back end is formed to define a cable cavity (31) for a cable, and wherein the cable shoe is further designed such that the cable cavity (31) is extending into a tapering cavity (33), designed to give the cable shoe a uniform cross section area along its length from the compact plate (26) to the beginning of the cable cavity (31).

20. The cable shoe according to claim 19, wherein the front portion is provided with brazing material, such as an amount of silver alloy with or without flux material, that preferably is attached to the compact plate by pressing or by melting.

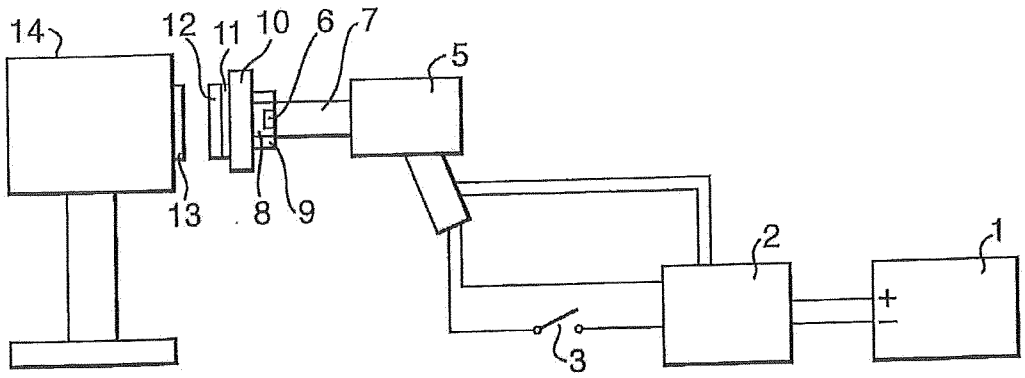


Fig. 1A

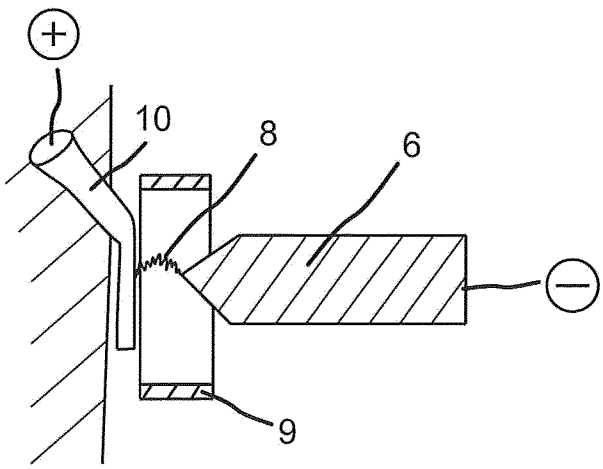


Fig. 1B

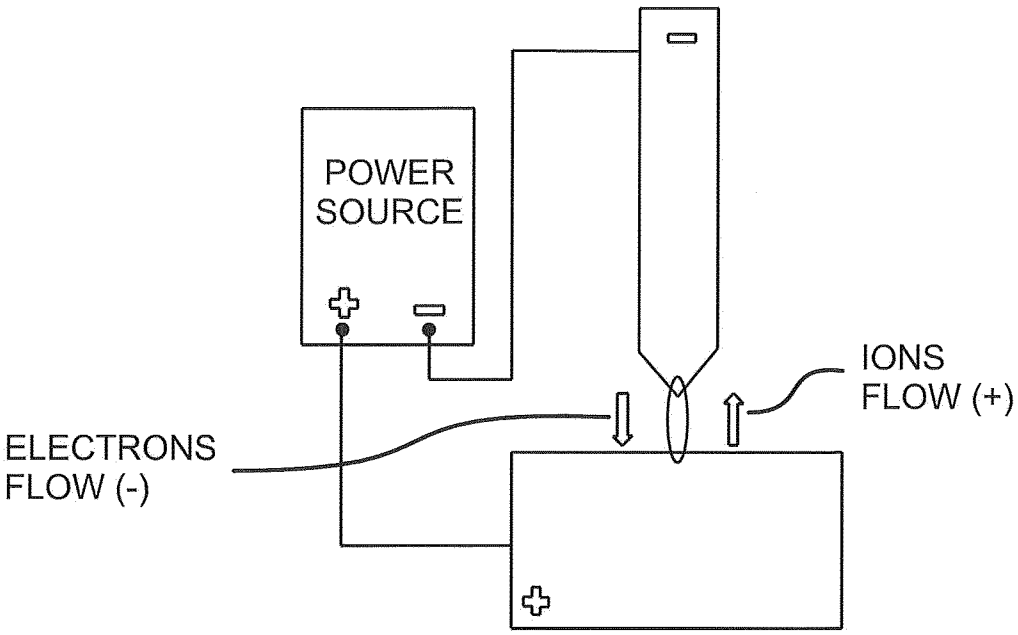

POWER
SOURCE
IONS
FLOW (+)
ELECTRONS
FLOW (-)

Fig. 1C

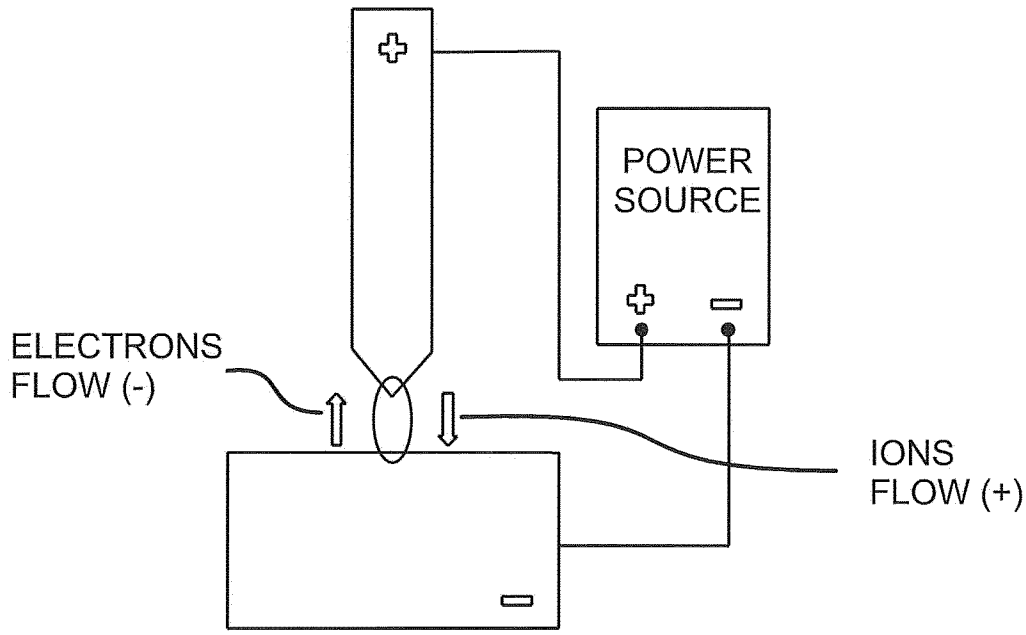

POWER
SOURCE
ELECTRONS
FLOW (-)
IONS
FLOW (+)

Fig. 1D

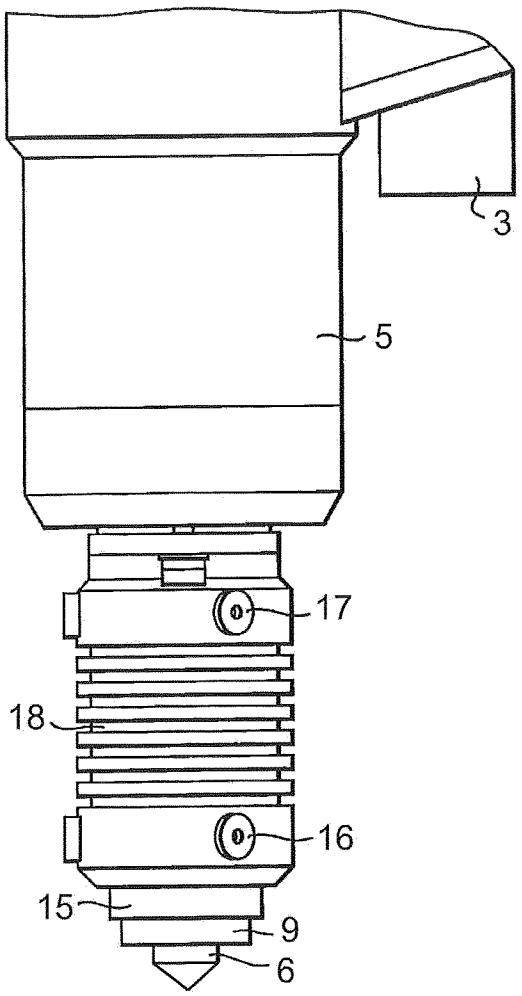


Fig. 2

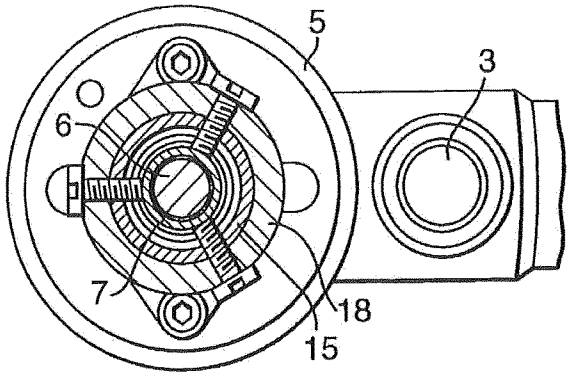


Fig. 3

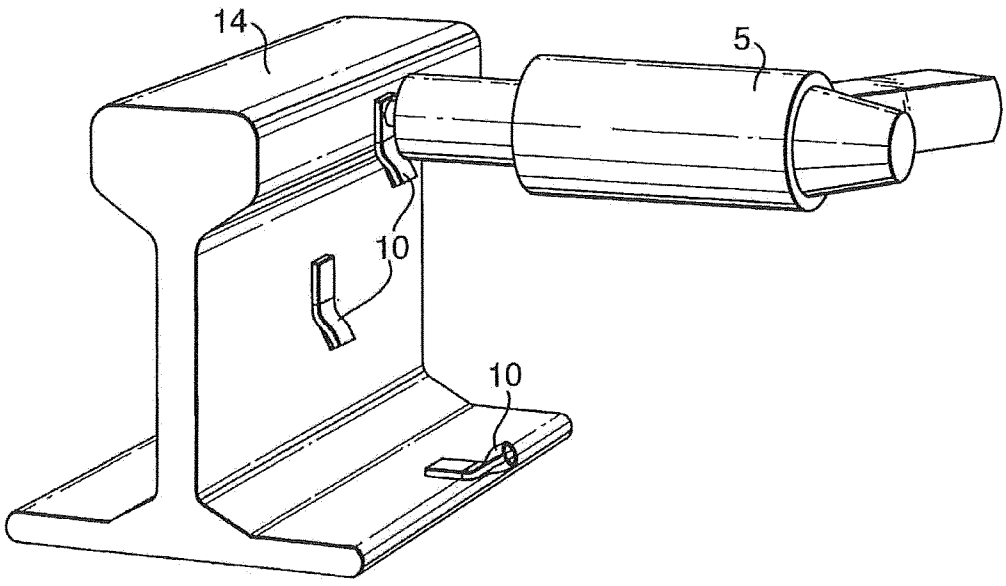


Fig. 5

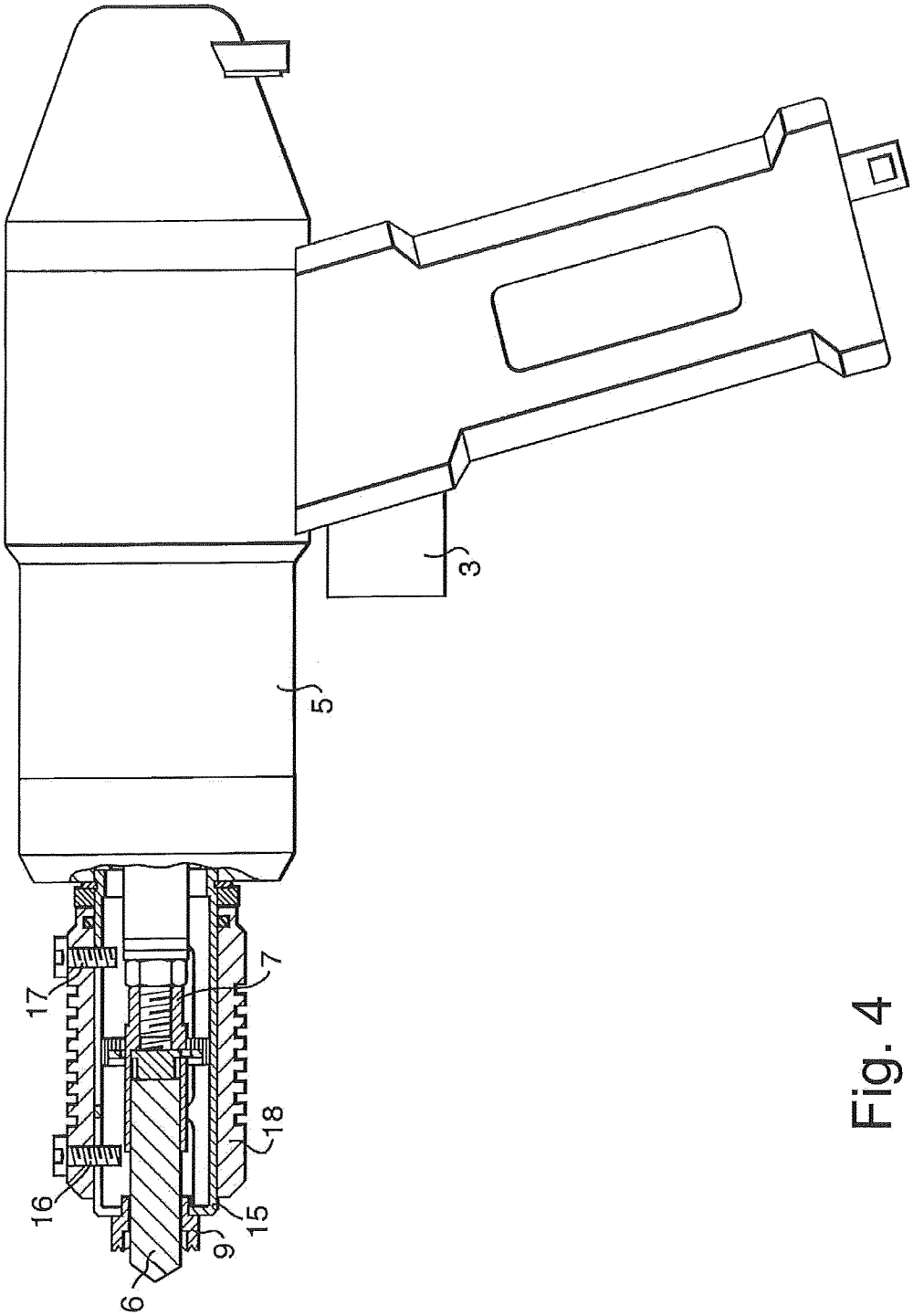


Fig. 4

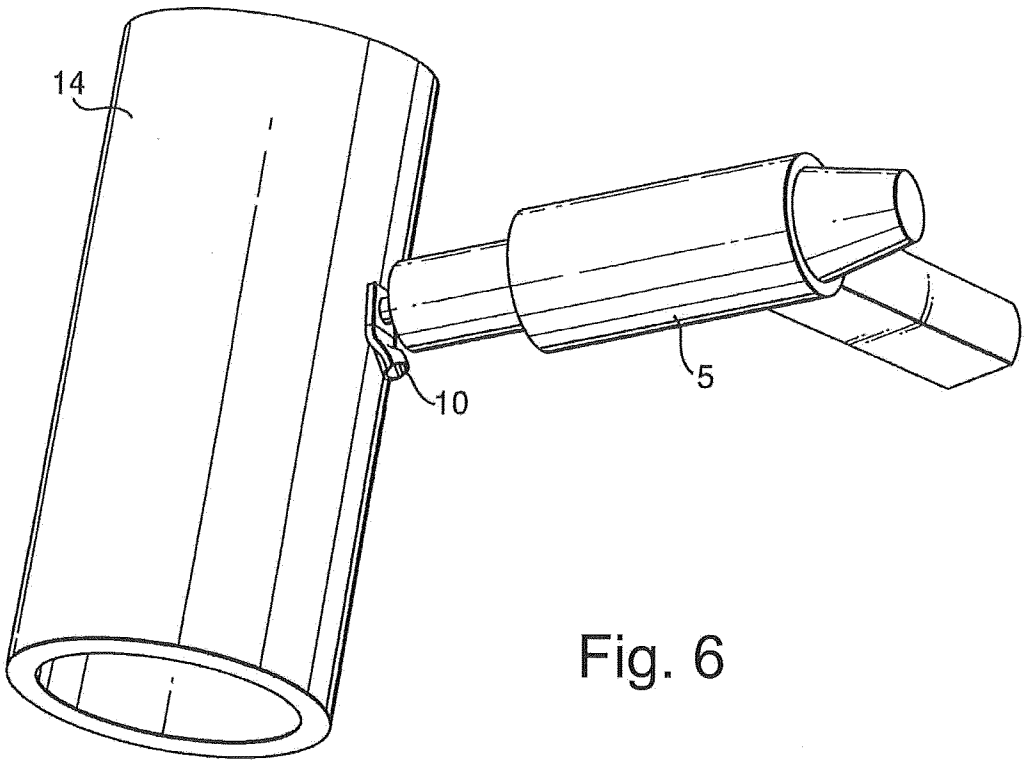


Fig. 6

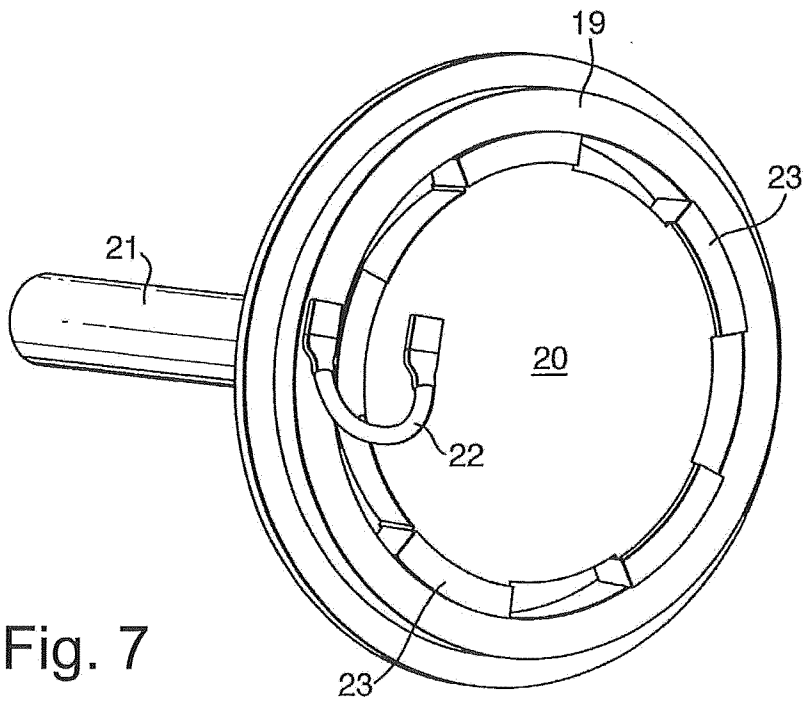


Fig. 7

Fig. 8

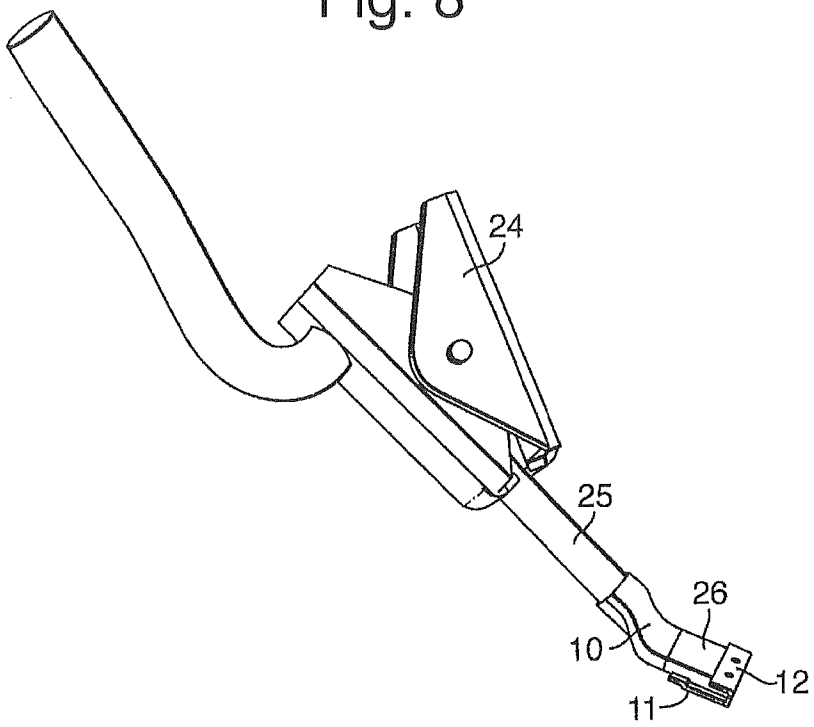
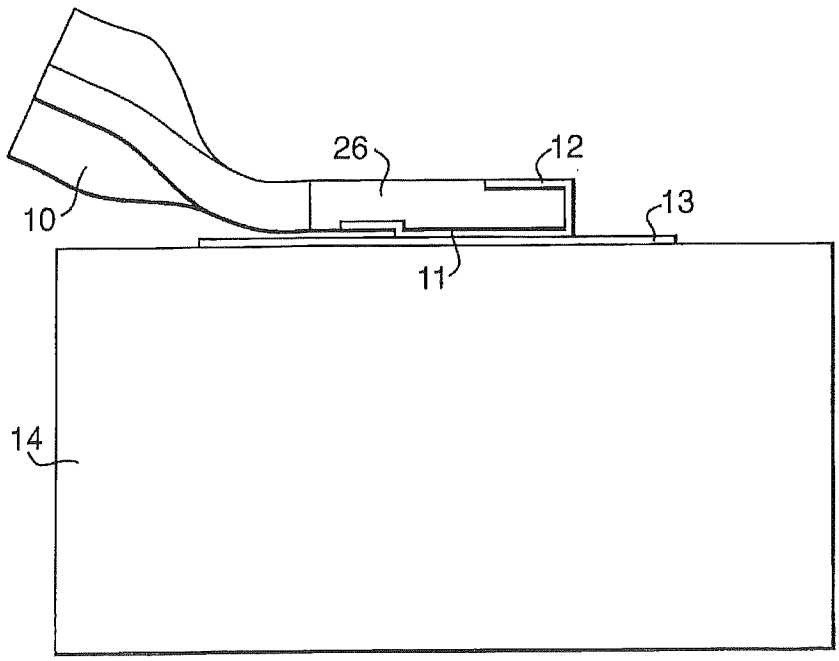


Fig. 9



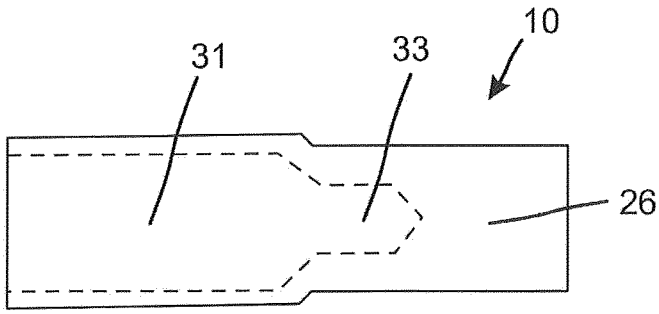


Fig. 10A

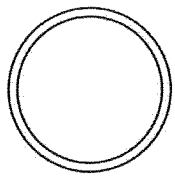


Fig. 10B

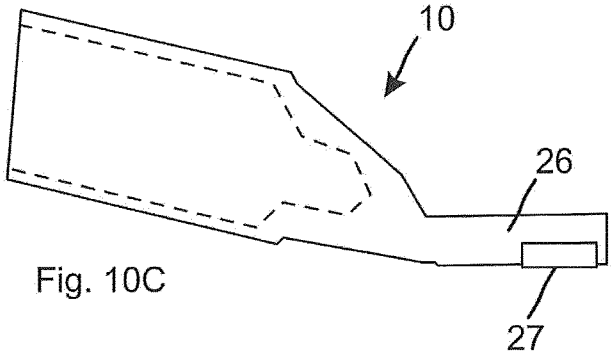


Fig. 10C

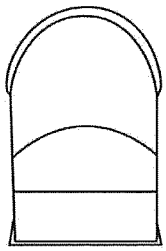


Fig. 10D

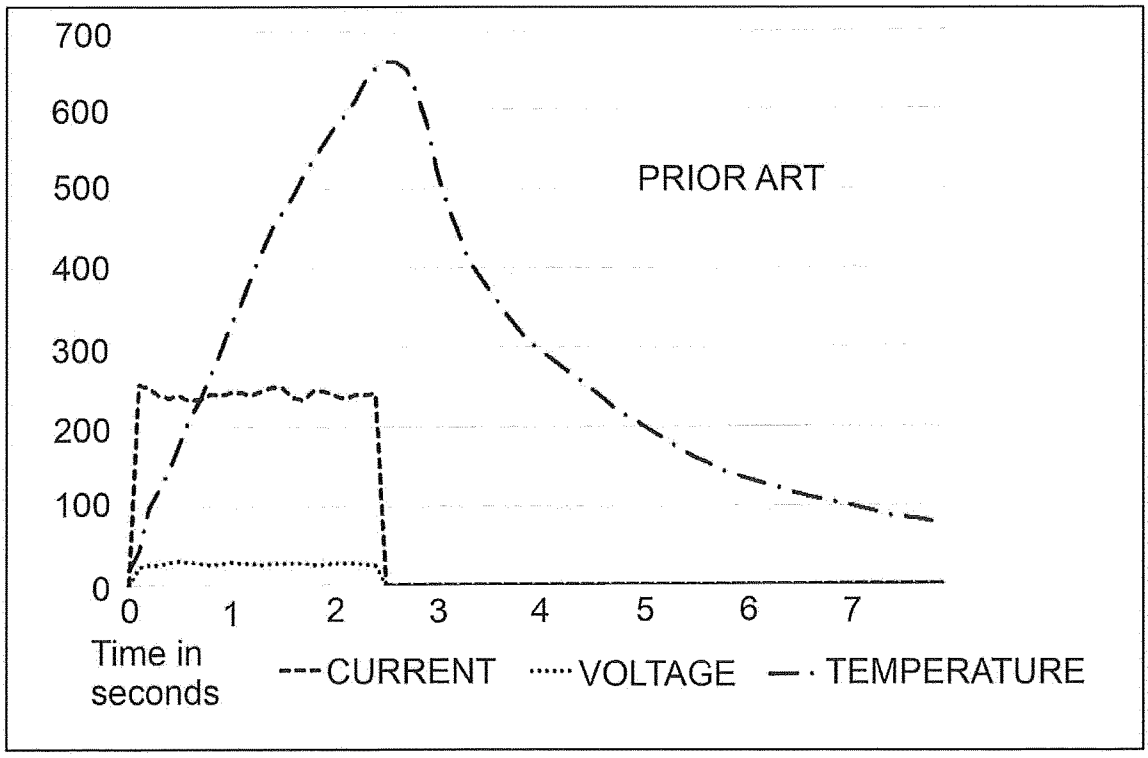


Fig. 11

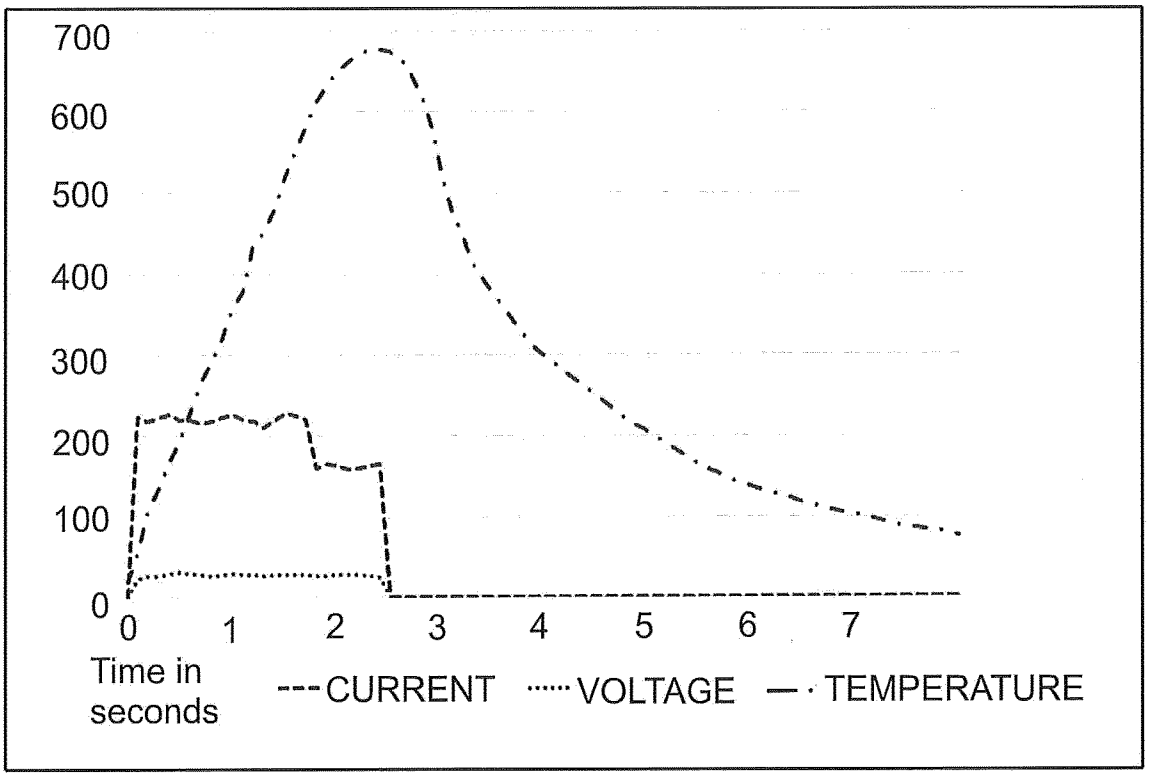


Fig. 12A

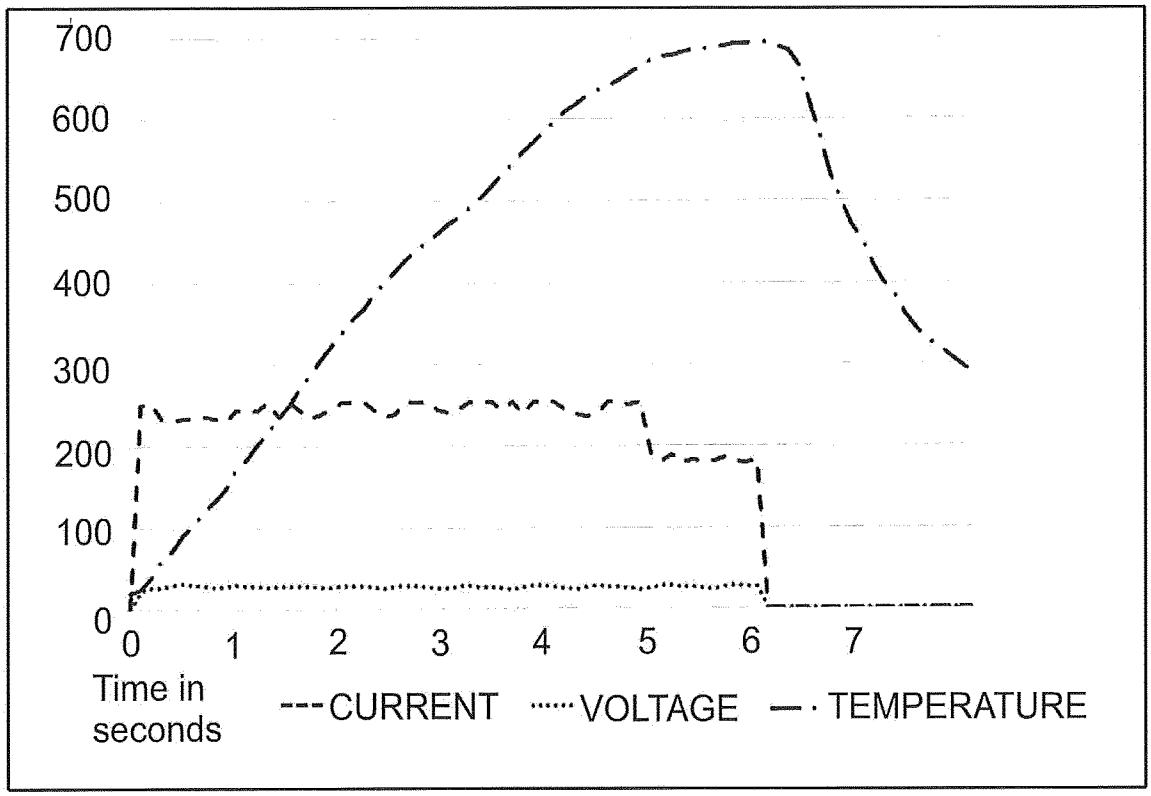


Fig. 12B

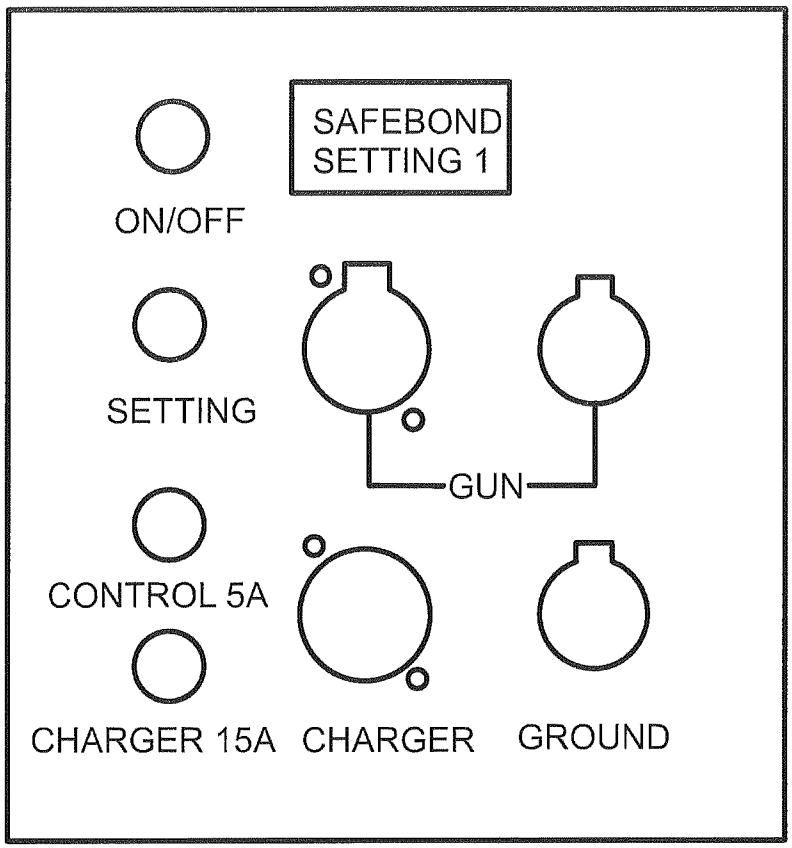
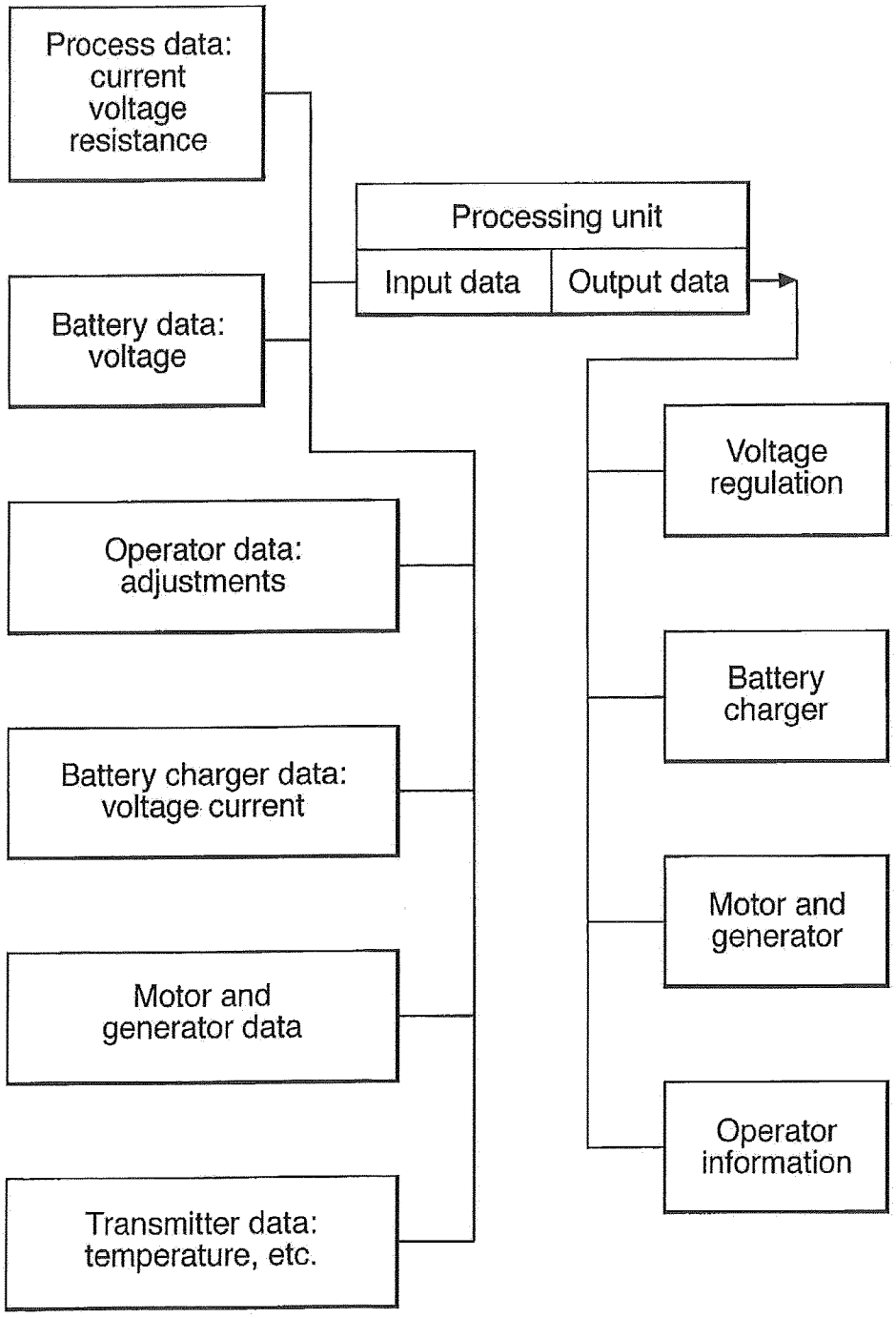

SAFEBOND
SETTING 1
ON/OFF
SETTING
GUN
CONTROL 5A
CHARGER 15A
CHARGER
GROUND

FIG. 13

Fig. 14A


Process data: current voltage resistance
Battery data: voltage
Operator data: adjustments
Battery charger data: voltage current
Motor and generator data
Transmitter data: temperature, etc.
Processing unit
Input data
Output data
Voltage regulation
Battery charger
Motor and generator
Operator information

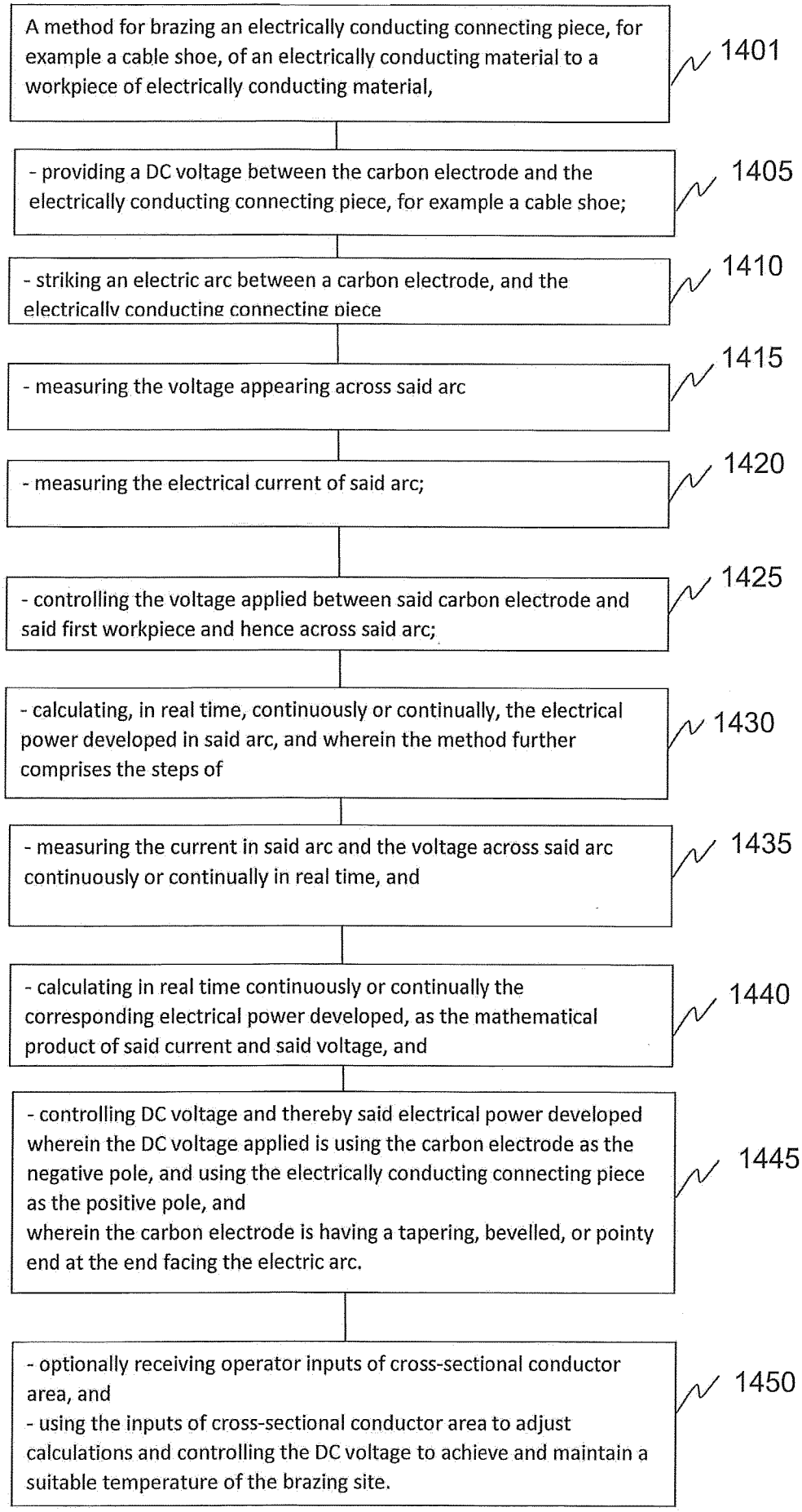

A method for brazing an electrically conducting connecting piece, for example a cable shoe, of an electrically conducting material to a workpiece of electrically conducting material,
1401
- providing a DC voltage between the carbon electrode and the electrically conducting connecting piece, for example a cable shoe;
1405
- striking an electric arc between a carbon electrode, and the electrically conducting connecting piece
1410
- measuring the voltage appearing across said arc
1415
- measuring the electrical current of said arc;
1420
- controlling the voltage applied between said carbon electrode and said first workpiece and hence across said arc;
1425
- calculating, in real time, continuously or continually, the electrical power developed in said arc, and wherein the method further comprises the steps of
1430
- measuring the current in said arc and the voltage across said arc continuously or continually in real time, and
1435
- calculating in real time continuously or continually the corresponding electrical power developed, as the mathematical product of said current and said voltage, and
1440
- controlling DC voltage and thereby said electrical power developed wherein the DC voltage applied is using the carbon electrode as the negative pole, and using the electrically conducting connecting piece as the positive pole, and
wherein the carbon electrode is having a tapering, bevelled, or pointy end at the end facing the electric arc.
1445
- optionally receiving operator inputs of cross-sectional conductor area, and
- using the inputs of cross-sectional conductor area to adjust calculations and controlling the DC voltage to achieve and maintain a suitable temperature of the brazing site.
1450

Fig. 14B

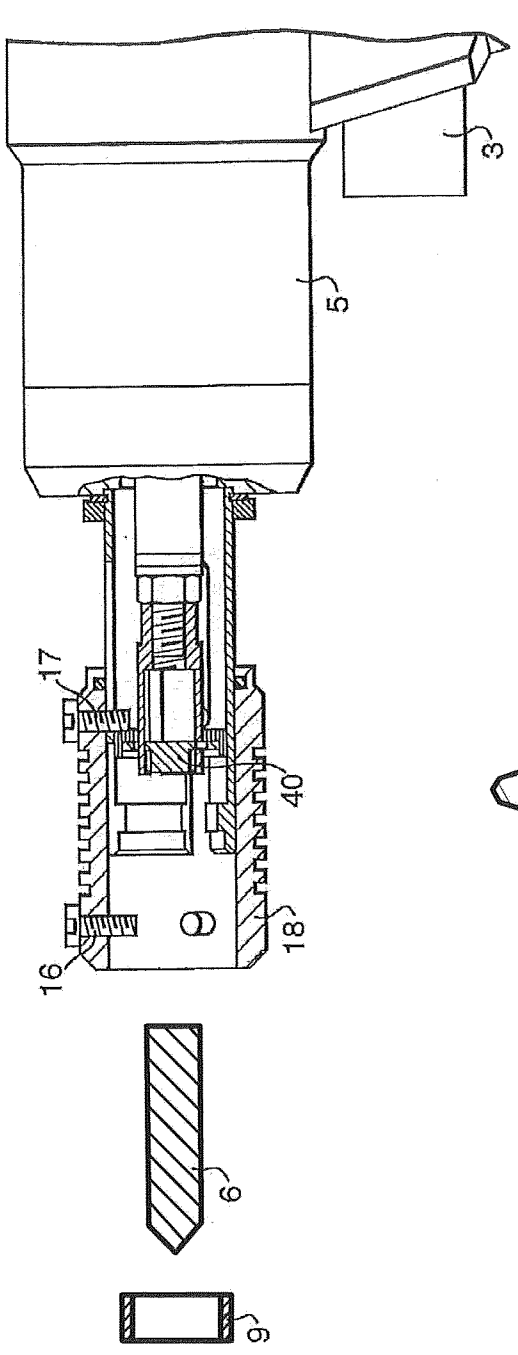


Fig. 15A

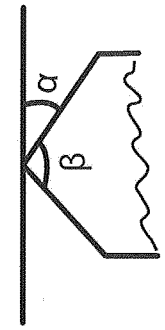


Fig. 15F

Fig. 15E

Fig. 15D

Fig. 15C

Fig. 15B

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2022/059130

A. CLASSIFICATION OF SUBJECT MATTER
INV. B23K1/00 B23K3/03 B23K101/38 B23K103/12 B23K101/26
B23K103/22
ADD.
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
B23K H01R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 2002/190097 A1 (PETTERSEN OLA [SE]) 19 December 2002 (2002-12-19) paragraphs [0001], [0009], [0014], [0022], [0042] - [0048], [0055], [0071], [0079] - [0082]; claims 1,2; figures 1,2,12	1-18
Y	US 2020/016674 A1 (MATSUZAKI KENJI [JP] ET AL) 16 January 2020 (2020-01-16) paragraphs [0001], [0002], [0011], [0016], [0023], [0024]; figure 1	1,2,4-6, 9-18
Y	US 2 297 303 A (HUMFELD LAWRENCE W) 29 September 1942 (1942-09-29) claim 1; figure 1	1,4-6, 12-18

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[X] Further documents are listed in the continuation of Box C.
[X] See patent family annex.

* Special categories of cited documents :

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"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
20 July 2022	29/07/2022

Name and mailing address of the ISA/	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Schloth, Patrick

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INTERNATIONAL SEARCH REPORT

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C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 2007/187459 A1 (PETTERSEN OLA [SE]) 16 August 2007 (2007-08-16) paragraphs [0001], [0007], [0020], [0103]; figures 1,3	1,3,6-8, 12-18
X	US 2002/173207 A1 (PETTERSEN OLA [SE]) 21 November 2002 (2002-11-21) paragraph [0052]; claim 2; figures 7-9	19,20

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No
PCT/EP2022/059130

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