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(54) Title: DEHYDRATION PROCESS THAT EMPLOYS AN IONIC LIQUID CHOLINE SALT

(57) Abstract: The invention relates to a process for dehydrating a water- containing medium, said medium being a pressurized gas having a pressure of at least 0.5 MPa, said process comprising: - contacting the water-containing medium with a dry ionic liquid choline salt to dehydrate the water-containing medium; and - separating a dehydrated medium from the hydrated ionic liquid choline salt. Ionic liquid choline salts offer the advantage that they can be regenerated very easily as they are surprisingly heat-stable. Furthermore, these liquid choline salts offer the advantage that they are non-toxic and largely inert. Thus, these ionic liquid choline salts can suitably be used to dehydrate water-containing media that are subsequently employed in the production of foodstuffs, beverages, nutritional formulations, pharmaceutical preparations etc.



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DEHYDRATION PROCESS THAT EMPLOYS AN IONIC LIQUID CHOLINE SALT

TECHNICAL FIELD OF THE INVENTION

5 The present invention relates to a process that employs a dry ionic liquid to dehydrate a water-containing medium, said medium being a pressurized gas having a pressure of at least 0.5 MPa. The pressurized gas can be in a gaseous, liquid or supercritical state.

BACKGROUND OF THE INVENTION

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Conventional processes for the dehydration of gasses, liquids and supercritical fluids often involve absorption/adsorption of water by a liquid or solid desiccant. The desiccant should have a much higher affinity for water than for the water-carrying medium and it should have a high water-holding capacity. Furthermore, ideally the desiccant should be regenerable, inert
15 and non-toxic. Finally, the desiccant should have a low solubility in the water-carrying medium.

Liquid desiccants offer a number of advantages over solid desiccants, including pumpability and easy handling. In addition, liquid desiccants offer the important advantage that they are
20 ideally suited for use in continuous (multistage) processes.

EP-A 1 310 543 describes a process for the continuous drying of a hydrocarbon stream comprising contacting the hydrocarbon stream with an ionic, liquid drying agent of a salt of a fluorinated sulphonic acid. The examples of this European patent application describe the
25 dehydration of heptane containing water using triethyl ammonium triflate.

EP-A 1 354 863 describes a process for the continuous drying of a hydrocarbon stream at a temperature being effective in drying the stream with an ionic liquid drying agent comprising a salt of sulphuric acid being in liquid or melted form at the drying temperature. The
30 examples describe dehydration of a stream of heptane saturated with water by contacting said stream with a dry ionic sulphate (diethylmethyammonium bisulphate).

SUMMARY OF THE INVENTION

The inventors have unexpectedly discovered that dry ionic liquid choline salts can advantageously be used as a desiccant to dehydrate a pressurized gas having a pressure of at least 0.5 MPa. The pressurized gas can be in a gaseous, liquid or supercritical state.

Ionic liquid cholines salts offer the advantage that they can be regenerated very easily as they are surprisingly heat-stable. Furthermore, these liquid choline salts offer the advantage that they are non-toxic and largely inert. Thus, these ionic liquid choline salts can suitably be used to dehydrate water-containing media that are subsequently employed in the production of foodstuffs, beverages, nutritional formulations, pharmaceutical preparations etc.

DETAILED DESCRIPTION OF THE INVENTION

Accordingly, one aspect of the invention relates to a process for dehydrating a water-containing medium, said medium being a pressurized gas having a pressure of at least 0.5 MPa, said process comprising:

- contacting the water-containing medium with a dry ionic liquid choline salt to dehydrate the water-containing medium; and
- separating a dehydrated medium from the hydrated ionic liquid choline salt.

The term “ionic liquid” as used herein refers to a salt in the liquid state. Ionic liquids are largely made of ions and short-lived ion pairs. These substances are variously called liquid electrolytes, ionic melts, ionic fluids, fused salts, liquid salts, or ionic glasses. Any salt that melts without decomposing or vaporizing usually yields an ionic liquid.

The term “choline salt” as used herein refers to the salt that is formed by N,N,N-trimethylethanolammonium cation with an undefined counter anion.

The dry ionic salt that is employed in the present process is liquid when it is contacted with the water-containing medium. The invention encompasses the use of salts that are an ionic liquid salt under the condition employed in the process but not under, for instance, ambient conditions.

The term "dry ionic liquid" as used herein refers to an ionic liquid that is capable of absorbing/binding water. Naturally, it is preferred to employ a dry ionic liquid having a very low water activity or relative humidity. It is noted, however, that for some ionic liquids it can be advantageous if the dry ionic liquid contains a quantity of water as these ionic liquids may become very viscous if all water is removed therefrom.

It should be understood that the present invention also encompasses the use of a mixture of the ionic liquid choline salt and another liquid or solid component, provided the choline salt is present in the mixture in the form of an ionic liquid.

The dry ionic liquid choline salt preferably has a water activity of 0.08-0.4, more preferably of 0.09-0.25, most preferably of 0.1-0.2 when it is contacted with the water-containing medium.

In the present process the water-containing medium is preferably contacted with the dry ionic liquid at a temperature and a pressure at which the solubility of water in the dry ionic liquid (in mg/kg) is at least 5 times, more preferably at least 10 times and most preferably at least 20 times higher than the dry medium's solubility in the same dry ionic liquid (in mg/kg).

The contacting of the dry ionic liquid and the water-containing medium preferably takes place at a temperature in the range of 0-80°C, more preferably of 15-60°C, most preferably of 31-50°C.

The contacting of ionic liquid with the water-containing medium typically occurs at a pressure of at least 1 MPa, more preferably of 3-50 MPa and most preferably of 5-25 MPa.

The water-containing medium is suitably selected from a gas, a liquid and a supercritical fluid. In a preferred embodiment of the invention the water-containing medium is a liquefied gas or a supercritical fluid.

The water-containing medium preferably comprises at least 50%, more preferably at least 80% and most preferably at least 90%, by weight of the dry medium, of carbon dioxide, nitrous oxide, methane, ethane, ethylene propane, cyclopropane, propylene, butane and mixtures thereof. Even more preferably, the water-containing medium contains at least 50%,

more preferably at least 80% and most preferably at least 90% of carbon dioxide, said percentages being calculated by weight of dry medium.

Preferably, in the present process the hydrated ionic liquid is continuously removed and continuously replenished with dry ionic liquid. Thus, the process enables dehydration of the water-containing medium to the desired level in a single operation.

The water-containing medium is preferably contacted with the dry ionic liquid choline salt by dispersing the ionic liquid salt throughout the water-containing medium, e.g. by spraying the ionic liquid salt into the water-containing medium. In this way, rate limiting effects of the low diffusion rates in the relatively viscous ionic liquid salt can be minimized effectively.

In accordance with another advantageous embodiment the water-containing medium is contacted with the dry ionic liquid choline salt by dispersing said medium throughout the ionic liquid.

In another preferred embodiment of the present process a stream of the water-containing medium is contacted with a stream of the dry ionic liquid in a counter current fashion.

An important advantage of the use of the ionic liquid choline salt as a dehydration agent in the present process lies in the fact that water can be removed from the hydrated ionic liquid relatively easily. Thus, in a particularly preferred embodiment of the invention the process comprises drying the hydrated ionic liquid and reusing the dried ionic liquid so obtained as dry ionic liquid in the dehydration process.

The ionic liquid choline salt of the present invention offers the advantage that it is surprisingly heat stable. Thus, in a particularly preferred embodiment, the drying of the hydrated ionic liquid comprises heating said ionic liquid to a temperature in excess of 80°C, more preferably of 80-150°C and most preferably 100-130 °C.

The dry ionic liquid choline salt employed in the present process preferably is a salt of choline and a carboxylic acid. The carboxylic acid preferably is a hydroxyl substituted carboxylic acid, more preferably a 2-hydroxycarboxylic acid. Even more preferably, the carboxylic acid is selected from lactate, glycolate, α -hydroxybutyrate and combinations thereof. Most

preferably, the ionic liquid choline salt is selected from choline lactate, choline glycolate and combinations thereof.

5 The present invention encompasses an embodiment of the present process in which the dry ionic liquid choline salt is combined with another liquid or solid desiccant (e.g zeolite).

The water-containing medium, when it is contacted with the dry ionic liquid, typically contains 0.01-10% water, more preferably 0.03-3% water and most preferably 0.1-1% water, said percentages being calculated by weight of dry medium.

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In the present process the water content of the water-containing medium is typically reduced by at least a factor 3. More preferably, said water content is reduced by at least factor 7, most preferably by at least a factor 10.

15 The present process typically yields a dehydrated medium having a water activity of not more than 0.45. Even more preferably, the dehydrated medium has a water activity of not more than 0.35, most preferably of not more than 0.25.

In a particularly advantageous embodiment of the present invention the process comprises:

- 20 a) contacting a dehydrated medium selected from a gas, a liquid or a supercritical fluid with a water-containing material to extract water from said water-containing material into said medium, thereby producing a dehydrated material and a water-containing medium; and
b) contacting the water-containing medium with a dry ionic liquid choline salt to dehydrate the water-containing medium.

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Preferably, the dehydrated medium is pressurized gas having a pressure of at least 0.5 MPa, more preferably of 3-50 MPa and most preferably of 5-25 MPa.

Advantageously, this process comprise the following additional step:

- 30 c) separating the dehydrated medium from the hydrated ionic liquid and recirculating said dehydrated medium to step a).

Even more preferably, the process additionally comprises the following steps:

- d) drying the hydrated ionic liquid to produce a dry ionic liquid; and

e) recirculating the dry ionic liquid to step b).

Steps a) and b) may be operated concurrently or successively. Preferably, steps a) and b) are operated concurrently. Steps a) and b), even when operated concurrently, may be executed in
5 different compartments.

The aforementioned process is particularly suitable for drying a water-containing material that comprises intact pieces of animal, fungal or plant tissue. Preferably, the water-containing material comprises at least 50 wt.%, more preferably at least 80 wt.% and most preferably at
10 least 90 wt.% of intact pieces of animal, fungal or plant tissue.

The dehydrated material produced in the process typically has a water content of less than 15 wt.%, more preferably of less than 10 wt.% and most preferably of less than 7 wt.%.

15 The invention is further illustrated by means of the following non-limiting examples.

EXAMPLES

Example 1

Choline lactate was introduced in a cylindrical pressure vessel having a diameter of 12 cm in sufficient quantity to form a layer of 2 cm thickness on the bottom of the vessel. Two slices of tomato (5 mm thick and 5 cm diameter) were placed in the vessel, approximately 5 cm above the surface of the ionic liquid.

Next, the vessel was pressurized with CO₂ to 100 bar and kept at a temperature of 40°C for 20 hours. The supercritical CO₂ was recycled from the top of the vessel to the bottom of the vessel via a centrifugal pump (115 kg/h)

After 20 hours in the pressure vessel the weight of tomato slices had decreased by 94%. The dehydrated tomato had an a_w of 0.40 and the choline lactate had an a_w of 0.41.

Example 2

The choline lactate that was used in Example 1 was analysed at the beginning and the end of the experiment. The analysed parameters included: a_w , amount of water present, CO₂ solubility and density. The results obtained are shown in Table 1.

Table 1

Choline lactate	a_w	water uptake	CO ₂ solubility	density
Starting material	0.12	-	--	1.2
Hydrated salt	0.41	8 wt.%	3.98 wt.%	1.1
Hydrated salt + extra water	0.89	30 wt.%	2.96 wt.%	1.0

Example 3

Choline lactate was hydrated by adding 20 g water to 30 g choline lactate. Next, the hydrated choline lactate was dried by keeping it at a temperature of 125°C or 150°C for 1 hour. It was found that that the hydrated choline lactate could be regenerated at these high temperatures with no adverse effect on the desiccating properties of the ionic liquid.

The procedure of hydrating and drying (at 125 °C) was repeated several times. No adverse effects on the desiccating properties of the ionic liquid were observed after these repeated hydration/drying cycles.

5 Example 4

Choline lactate was introduced in a cylindrical pressure vessel (1L) having a diameter of 8 cm in sufficient quantity to form a layer of approximately 2.5 cm thickness on the bottom of the vessel (111.2gr). One slice of tomato (5 mm thick and 5 cm diameter weighing 9.5 grams) was placed in the vessel, approximately 5 cm above the surface of the ionic liquid.

10

Next, the vessel was pressurized with gaseous CO₂ to 20 bar and kept at a temperature of 14°C for 18 hours.

After 18 hours in the pressure vessel the weight of the tomato slice had decreased by 20.5%.

15 The water activity of the choline lactate increased from 0.16 a_w to 0.18 a_w.

Although the reduction in water content of the tomato slice was marginal, this experiment clearly demonstrates the capability of the ionic liquid choline lactate to remove water from the CO₂ gas. Under the conditions employed in this experiment CO₂ can absorb not more than 0.1 g of water per litre of CO₂ (at 20 bar). The amount of water removed from the tomato slice corresponds to 2 g, which is many times more than the amount of water that can be absorbed by the amount of carbon dioxide that was used in the experiment (1 l).

20

25 Example 5

Choline lactate was introduced in a cylindrical pressure vessel (1L) having a diameter of 8 cm in sufficient quantity to form a layer of approximately 2.5 cm thickness on the bottom of the vessel (130.2gr). One slice of tomato (5 mm thick and 5 cm diameter weighing 7.5grams) was placed in the vessel, approximately 5cm above the surface of the ionic liquid.

30

Next, the vessel was pressurized with liquid CO₂ to 60 bar and kept at a temperature of 14°C for 12 hours.

After 12 hours in the pressure vessel the weight of tomato slices had decreased by 41.2%. The water activity of the choline lactate increased from 0.16 a_w to 0.21 a_w .

Example 6

- 5 An apparatus comprising an extractor (1L vessel) filled with wet sponges, a packed column (packing height = 64 cm; diameter = 38 mm) and a separator (1L vessel) filled with dried zeolite was used for carrying out the experiments described below.

- 10 Supercritical carbon dioxide was saturated with water in the extractor vessel, after which the saturated CO_2 was fed to the bottom of the packed column. Within the column the CO_2 was contacted with the choline lactate (counter current). The choline lactate was sprayed on the packed column, and was removed from the bottom of the column. The CO_2 was finally fed to a vessel containing 600gr of zeolite for post-drying.

- 15 Each of the experiments was run for approximately 30 minutes. Before each experiment the packed column was cleaned and dried. The moisture uptake by the choline lactate was determined by calculating the weight loss of the sponges and the weight gain of the zeolite.

- 20 Several tests were carried out with the experimental set-up described above, using different conditions in order to assess the influence of these parameters in the absorption process.

The experimental conditions used and the results obtained are summarised in Tables 1.

Table 1

	Pressure (bar)	Temp. (°C)	CO₂ flow rate (kg/h)	IL flow rate (ml/min)	Initial a_w IL	Final a_w IL
1	100	40	15	4	0.100	—
2	100	40	15	8	0.111	0.184
3	150	40	15	4	0.115	0.275
4	150	50	15	4	0.115	0.234
5	100	40	15	4	0.121	0.221
6	150	50	15	4	0.117	0.226
7	100	40	15	4	0.107	0.201
8	100	40	15	4	0.042	0.113

9	100	40	15	4	0.084	0.167
10	100	40	15	4	0.136	0.204

From the experiments it is clear that the choline lactate was capable of removing moisture from the super critical CO₂ using a packed column set up. This was clear from the weight loss of the sponges, and the increase in water activity of the choline lactate.

5

The experiments further show that the ionic liquid can take up water at low, even very low, water activity. It is noted that as the ionic liquid takes up more water, the rate at which this water uptake causes the water activity to increase steadily decreases.

10

CLAIMS

1. A process for dehydrating a water-containing medium, said medium being a pressurized gas having a pressure of at least 0.5 MPa, said process comprising:
 - 5 • contacting the water-containing medium with a dry ionic liquid choline salt to dehydrate the water-containing medium; and
 - separating a dehydrated medium from the hydrated ionic liquid choline salt.
2. Process according to claim 1, wherein solubility of water in the dry ionic liquid (in mg/kg)
10 is at least 10 times higher than the dry medium's solubility in the same dry ionic liquid (in mg/kg).
3. Process according to claim 1 or 2, wherein the process comprises drying the hydrated ionic liquid and reusing the dried ionic liquid as dry ionic liquid in the dehydration
15 process.
4. Process according to claim 3, wherein the drying of the hydrated ionic liquid comprises heating said ionic liquid to a temperature in excess of 80°C.
- 20 5. Process according to any one of the preceding claims, wherein the dry ionic liquid is a salt of choline and a carboxylic acid.
6. Process according to any one of the preceding claims, wherein the water-containing medium, when it is contacted with the dry ionic liquid, contains 0.01-10% water, said
25 percentage being calculated by weight of dry medium.
7. Process according to any one of the preceding claims, wherein the water-containing medium comprises at least 50% by weight of dry medium of carbon dioxide, nitrous oxide, methane, ethane, ethylene propane, cyclopropane, propylene, butane and mixtures
30 thereof.
8. Process according to claim 7, wherein the water-containing medium comprises at least 50% by weight of dry medium of carbon dioxide.

9. Process according to any one of the preceding claims, wherein the water-containing medium is a pressurized gas having a pressure of at least 3 MPa.
10. Process according to any one of the preceding claims, wherein the water-containing medium is a liquefied gas or a supercritical fluid.
11. Process according to any one of the preceding claims wherein the process comprises continuously removing the hydrated ionic liquid and continuously replenishing said hydrated ionic liquid with dry ionic liquid.
12. Process according to any one of the preceding claims, wherein a stream of the water-containing medium is contacted with a stream of the dry ionic liquid in a counter current fashion.
13. Process according to any one of the preceding claims, said process comprising:
- a) contacting a dehydrated medium selected from a gas, a liquid or a supercritical fluid with a water-containing material to extract water from said water-containing material into said medium, thereby producing a dehydrated material and a water-containing medium; and
 - b) contacting the water-containing medium with a dry ionic liquid choline salt to dehydrate the water-containing medium.
14. Process according to claim 13, said process further comprising the following steps:
- c) separating the dehydrated medium from the hydrated ionic liquid and recirculating said dehydrated medium to step a);
 - d) drying the hydrated ionic liquid to produce a dry ionic liquid; and
 - e) recirculating the dry ionic liquid to step b).
15. Process according to claim 13 or 14, wherein the water content of the water-containing material is reduced by at least a factor 3.
16. Process according to any one of claims 13-15, wherein the water-containing material comprises intact pieces of animal or plant tissue.

INTERNATIONAL SEARCH REPORT

International application No

PCT/NL2011/050909

A. CLASSIFICATION OF SUBJECT MATTER

INV. B01D53/26 B01D53/28 A23B7/022 A23L3/42 C10M133/08
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

B01D A23B A23L C10M C10G C07C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 1 310 543 A1 (TOPSOE HALDOR AS [DK]) 14 May 2003 (2003-05-14) abstract paragraphs [0001], [0008], [0013], [0016] - [0019] -----	1-16
A	EP 2 093 278 A1 (EVONIK GOLDSCHMIDT GMBH [DE]) 26 August 2009 (2009-08-26) abstract paragraphs [0003], [0013] - [0015], [0046] -----	1-16
A	WO 2008/147181 A1 (UNIV DELFT TECH [NL]; GROSS JOACHIM [NL]; JANSSENS PETER JOHANNES [NL]) 4 December 2008 (2008-12-04) abstract; claims 1,4,6 page 1, lines 1-4 page 3, lines 4-12 -----	1-16

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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INTERNATIONAL SEARCH REPORT

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Patent document cited in search report		Publication date		Patent family member(s)		Publication date
EP 1310543	A1	14-05-2003	EP	1310543	A1	14-05-2003
			JP	4298264	B2	15-07-2009
			JP	2003183674	A	03-07-2003
			US	2003091489	A1	15-05-2003

EP 2093278	A1	26-08-2009	CA	2652704	A1	05-08-2009
			CN	101502770	A	12-08-2009
			EP	2093278	A1	26-08-2009
			JP	2009185287	A	20-08-2009
			US	2010029519	A1	04-02-2010

WO 2008147181	A1	04-12-2008	NL	2000654	C2	20-11-2008
			WO	2008147181	A1	04-12-2008
