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(54) Title: SELECTIVE CATALYTIC REDUCTION ARTICLES AND SYSTEMS

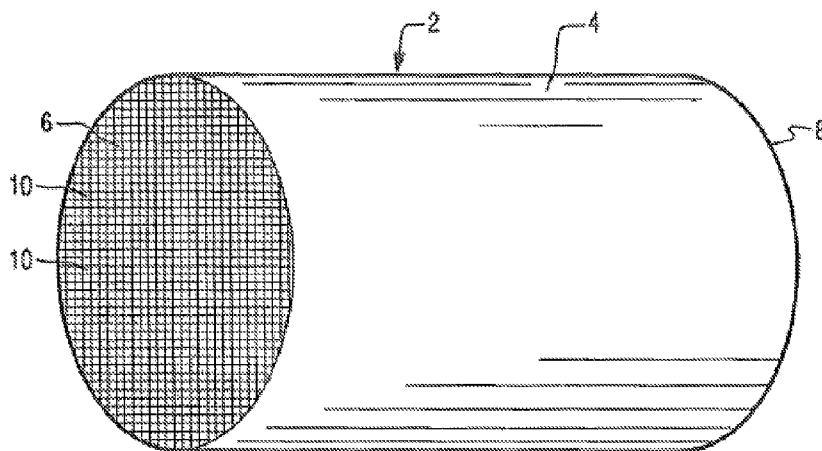


FIG. 1

(57) Abstract: Certain selective catalytic reduction (SCR) articles, systems and methods provide for high NO_x conversion while at the same time low N₂O formation. The articles, systems and methods are suitable for instance for the treatment of exhaust gas of diesel engines. Certain articles have zoned coatings disposed thereon, for example, a zoned coating comprising an upstream zone comprising a coating layer comprising a steam-activated iron-containing molecular sieve and a downstream zone comprising a coating layer comprising a high copper-containing molecular sieve.



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Selective Catalytic Reduction Articles and Systems

The present invention is aimed at selective catalytic reduction (SCR) articles and systems suitable for use in treating exhaust of an internal combustion engine.

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Background

Molecular sieves such as zeolites are employed in the catalysis of certain chemical reactions for example the selective catalytic reduction (SCR) of nitrogen oxides with a reductant such as ammonia, urea or hydrocarbons. Zeolites are crystalline materials having rather uniform pore sizes which, depending upon the type of zeolite and the type and amount of cations included in the zeolite lattice, range from about 3 to about 25 angstroms in diameter. Zeolites having 8-ring pore openings and double-six ring secondary building units, particularly those having cage-like structures are of interest as SCR catalysts. Included in this category are zeolites having a chabazite (CHA) crystal structure, which are small pore zeolites with 8 member-ring pore openings (ca. 3.8 angstroms) accessible through its 3-dimensional porosity. A cage like structure results from the connection of double six-ring building units by 4 rings.

Catalysts employed in the SCR process ideally should be able to retain good catalytic activity over the wide range of temperature conditions of use, for example from about 150°C to about 600°C or higher, under hydrothermal conditions. Hydrothermal conditions are encountered in practice because water is a byproduct of fuel combustion and high temperature hydrothermal conditions occur in diesel exhaust applications, such as during the regeneration of a soot filter, a component of exhaust gas treatment systems used for the removal of carbonaceous particles.

The SCR process converts nitrogen oxides (NOx) to nitrogen (N₂) and water (H₂O). An undesired SCR byproduct is nitrous oxide (N₂O). Desired are improved articles, systems and processes to selectively convert NOx within internal combustion engine exhaust streams to N₂ while minimizing the formation of undesired N₂O. Undesired N₂O formation may be observed as molar percent conversion of (NO + NO₂) to N₂O.

Nitrogen oxides (NOx) may include N₂O, NO, N₂O₃, NO₂, N₂O₄, N₂O₅ or NO₃.

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Summary

In one or more embodiments, the present disclosure provides catalytic articles, systems and methods for treating exhaust gas streams containing nitrogen oxides. The articles, systems and methods will exhibit high NOx conversion while at the same time minimize N₂O formation. In certain embodiments, the articles, systems and methods are suitable for treating lean exhaust gas streams of diesel internal combustion engines.

In one or more embodiments, the present disclosure relates to selective catalytic reduction articles, systems incorporating such articles, and methods utilizing such articles and systems. The

selective catalytic reduction articles advantageously provide for high NO_x conversion with simultaneously low formation of N₂O because of the utilization of at least two different catalytically active molecular sieves. More specifically, at least a first steam-activated iron-containing molecular sieve and a second copper-containing molecular sieve are utilized. The steam-5 activated iron-containing molecular sieve and the copper-containing molecular sieve are coated on at least one substrate. For example, a first coating layer of the first steam-activated iron-containing molecular sieve and a second coating layer of the second copper-containing molecular sieve are coated on the at least one substrate. The first and second coating layers can be coated on the same substrate or on different substrates. For example, a first substrate can have the first 10 coating layer with the first steam-activated iron-containing molecular sieve provided thereon (e.g., in the form of a washcoat), and a second substrate can have the second coating layer with the second copper-containing molecular sieve provided thereon (e.g., in the form of a washcoat). Preferably, the first substrate with the first coating layer is provided upstream of the second substrate with the second coating layer relative to the flow path of an exhaust stream (the second 15 substrate with the second coating layer thus being downstream of the first substrate with the first coating layer). As another example, a substrate can have a first coating layer with a first steam-activated iron-containing molecular sieve provided thereon (e.g., in the form of a washcoat), and the same substrate can have a second coating layer with the second copper-containing molecular sieve provided thereon (e.g., in the form of a washcoat). In such configuration, the second coating 20 layer is preferably provided downstream of the first coating layer relative to the flow path of an exhaust stream (the first coating layer thus being upstream from the second coating layer). The substrate is thus zoned so that a first zone includes the first coating layer and the second zone includes the second coating layer. The zones (and thus the coating layers) may overlap if desired or may be non-overlapping. It has been found that providing a first steam-activated iron-containing 25 molecular sieve and a second copper-containing molecular sieve beneficially achieves the results described herein in relation to NO_x conversion and low N₂O formation, particularly when the first steam-activated iron-containing molecular sieve is positioned upstream from the second copper-containing molecular sieve. The present disclosure particularly provides, in some embodiments, a selective catalytic reduction article comprising a substrate having a front upstream end and a rear 30 downstream end defining an axial length and having a catalytic coating thereon, where the catalytic coating comprises a first coating layer comprising an iron-containing molecular sieve and a second coating layer comprising a copper-containing molecular sieve.

Advantageously, the catalytic coating is zoned and comprises a first zone comprising the first coating layer comprising the iron-containing molecular sieve and a second zone comprising the second coating layer comprising the copper-containing molecular sieve. The iron-containing 35 molecular sieve for example comprises steam-activated FeCHA powder.

Also disclosed is a selective catalytic reduction system comprising a first selective catalytic reduction article comprising a first substrate comprising a first catalytic coating layer comprising an iron-containing molecular sieve and a second selective catalytic reduction article comprising a second substrate comprising a second catalytic coating layer comprising a copper-containing molecular sieve, where the first and second articles are in fluid communication.

Also disclosed is an exhaust gas treatment system comprising the reduction article or reduction system and a reductant injector in fluid communication with and upstream of the article or system.

Also disclosed are methods for treating an exhaust stream containing NO_x, comprising passing the exhaust stream through the reduction articles, reduction systems or treatment systems.

Also disclosed are methods for activating an iron-containing molecular sieve, the methods comprising adding iron to a molecular sieve followed by steam-calcination of the resulting iron-containing zeolite powder from about 500°C to about 800°C for a period of from about 20 minutes to about 12 hours in the presence of water vapor or preferably from about 650°C to about 750°C for a period of from about 20 minutes to about 2 hours in the presence of water vapor. Pre-activated iron-containing zeolite applied to a substrate provides outstanding SCR performance without further hydrothermal treatment of the coated substrate.

Also disclosed are selective catalytic reduction articles or systems capable of providing NO_x conversion of $\geq 90\%$ (preferably $\geq 99\%$), and N₂O formation of $\leq 50\%$ (preferably $\leq 40\%$) of that of an article or system, respectively, containing a uniform concentration of CuCHA as the only SCR catalyst under transient engine testing conditions. More particularly, selective catalytic reduction articles, systems, or methods of the present disclosure can be configured for providing $>90\%$ NO_x conversion while also providing $\leq 1.5\%$ N₂O formation, particularly the N₂O formation is $\leq 40\%$ of that compared to an article, system, or method containing or employing a uniform concentration of high Cu-containing CuCHA as the only SCR catalyst under transient engine testing conditions as otherwise described herein. Embodiments of the present disclosure also relate to improved performance by utilizing zoning. For example, a selective catalytic reduction article, system, or method according to the present disclosure can include a substrate with a front upstream zone including a catalytic coating and a second downstream zone including a catalytic coating, and can be adapted for providing $>90\%$ total NO_x conversion, particularly wherein the front upstream zone provides from about 30% to about 80% of the total NO_x conversion.

Also disclosed are SCR articles comprising a substrate having a front upstream end and a rear downstream end defining an axial length and having a catalytic coating thereon, where the catalytic coating comprises steam-activated FeCHA powder and CuCHA.

The invention includes, without limitation, the following embodiments:

5 Embodiment 1: A method for activating an iron-containing molecular sieve powder, the method comprising: adding iron into a molecular sieve to form an iron-containing molecular sieve; and carrying out steam-calcination of the iron-containing molecular sieve powder at a temperature of about 650°C to about 750°C for a period of about 20 minutes to about 2 hours in the presence of water vapor.

Embodyment 2: The method of any preceding or subsequent embodiment, wherein adding the iron into the molecular sieve comprises a process selected from the group consisting of ion-exchange, impregnation of an iron salt, and mixing a molecular sieve with iron oxide.

10 Embodiment 3: A method of preparing a catalytic article, the method comprising applying to a substrate a catalytic coating comprising a steam-activated iron-containing molecular sieve powder prepared according to any preceding embodiment.

Embodyment 4: The method any preceding or subsequent embodiment, wherein the coated substrate is adapted to achieve greater than 90% NO_x conversion at 250°C under fast SCR conditions without further steam-treatment.

15 Embodiment 5: A selective catalytic reduction article comprising a substrate having a front upstream end and a rear downstream end defining an axial length and having a catalytic coating thereon, where the catalytic coating comprises: a first coating layer comprising a steam-activated iron-containing molecular sieve; and a second coating layer comprising a copper-containing molecular sieve.

20 Embodiment 6: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the catalytic coating is zoned and comprises: a first, upstream zone comprising the first coating layer comprising the steam-activated iron-containing molecular sieve; and a second, downstream zone comprising the second coating layer comprising the copper-containing molecular sieve.

25 Embodiment 7: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the substrate is a porous wall-flow filter or a flow-through monolith.

Embodyment 8: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein one or both of the following conditions apply: a weight ratio of the steam-activated iron-containing molecular sieve to the copper-containing molecular sieve is about 1:10 to 30 about 10:1; a weight ratio of iron oxide in the steam-activated iron-containing molecular sieve to copper oxide in the copper-containing molecular sieve is about 1:15 to about 15:1.

35 Embodiment 9: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the steam-activated iron-containing molecular sieve includes iron oxide in an amount of about 1 wt% to about 15 wt%, based on the total weight of the iron-containing molecular sieve, and the copper-containing molecular sieve includes copper oxide in an amount of about 1 wt% to about 10 wt%, based on the total weight of the copper-containing molecular sieve.

Embodiment 10: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein one or both of the following conditions apply: the copper-containing molecular sieve has a Cu/Al atomic ratio of about 0.05 to about 0.55; the steam-activated iron-containing molecular sieve has a Fe/Al atomic ratio of about 0.05 to about 0.5.

5 Embodiment 11: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the first coating layer extends a distance from the front, upstream end of the substrate towards the rear, downstream end of the substrate and overlays a portion of the second coating layer, which extends from the rear, downstream end of the substrate a distance towards the front, upstream end of the substrate.

10 Embodiment 12: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the first coating layer extends a from the front, upstream end of the substrate to the rear, downstream end of the substrate and overlays an entirety of the second coating layer, which extends from the rear, downstream end of the substrate to the front, upstream end of the substrate.

15 Embodiment 13: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the second coating layer extends a distance from the front, upstream end of the substrate towards the rear, downstream end of the substrate and overlays a portion of the first coating layer, which extends a distance from the rear, downstream end of the substrate towards the front, upstream end of the substrate.

20 Embodiment 14: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the second coating layer extends from the front, upstream end of the substrate to the rear, downstream end of the substrate and overlays an entirety of the first coating layer, which extends from the rear, downstream end of the substrate to the front, upstream end of the substrate.

25 Embodiment 15: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the first coating layer and the second coating layer are adjacent and do not overlay each other.

30 Embodiment 16: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the first coating layer and the second coating layer are in direct contact with each other.

Embodiment 17: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are each 8-ring small pore molecular sieves.

35 Embodiment 18: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are both independently zeolites having a structure selected from the group consisting of AEI, AFT, AFX, CHA, EAB, ERI, KFI, LEV, SAS, SAT and SAV.

Embodiment 19: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein each of the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve have a CHA crystal structure.

5 Embodiment 20: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein each of the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are aluminosilicate zeolites having a CHA crystal structure and a silica to alumina ratio (SAR) of about 5 to about 40.

10 Embodiment 21: The selective catalytic reduction article of any preceding or subsequent embodiment, wherein the substrate includes an undercoat comprising an AMOx catalyst in the downstream zone.

15 Embodiment 22: A selective catalytic reduction system comprising: a first selective catalytic reduction article formed of a first substrate including a first catalytic coating layer comprising a steam-activated iron-containing molecular sieve; and a second selective catalytic reduction article formed of a second substrate including a second catalytic coating layer comprising a copper-containing molecular sieve: wherein the first selective catalytic reduction article and the second selective catalytic reduction article are in fluid communication.

20 Embodiment 23: The selective catalytic reduction system of any preceding or subsequent embodiment, wherein the first substrate of the first selective catalytic reduction article is zoned so as to have a first zone comprising the first catalytic coating layer and a second zone comprising a co-catalyst layer comprising a high copper-containing molecular sieve.

Embodiment 24: The selective catalytic reduction system of any preceding or subsequent embodiment, wherein the first substrate and the second substrate are each independently selected from the group consisting of a porous wall-flow filter and a flow-through monolith.

25 Embodiment 25: The selective catalytic reduction system of any preceding or subsequent embodiment, wherein the second substrate includes an undercoat comprising an AMOx catalyst.

Embodiment 26: An exhaust gas treatment system comprising: a selective catalytic reduction article or a selective catalytic reduction system according to any preceding or subsequent embodiment; and a reductant injector in fluid communication with and upstream of the selective catalytic reduction article or the selective catalytic reduction system.

30 Embodiment 27: The exhaust gas treatment system of any preceding or subsequent embodiment, further comprising one or more of a diesel oxidation catalyst, a soot filter, and an ammonia oxidation catalyst.

35 Embodiment 28: The exhaust gas treatment system of any preceding or subsequent embodiment, further comprising an internal combustion engine in fluid communication with and upstream of the selective catalytic reduction article or the selective catalytic reduction system.

Embodiment 29: A method for treating an exhaust stream containing NO_x, comprising passing the exhaust stream through a selective catalytic reduction article, a selective catalytic reduction system, or an exhaust gas treatment system of any preceding embodiment.

These and other features, aspects, and advantages of the disclosure will be apparent from 5 a reading of the following detailed description together with the accompanying drawings, which are briefly described below. The invention includes any combination of two, three, four, or more of the above-noted embodiments as well as combinations of any two, three, four, or more features or elements set forth in this disclosure, regardless of whether such features or elements are expressly combined in a specific embodiment description herein. This disclosure is intended to be 10 read holistically such that any separable features or elements of the disclosed invention, in any of its various aspects and embodiments, should be viewed as intended to be combinable unless the context clearly dictates otherwise. Other aspects and advantages of the present invention will become apparent from the following.

15 **Brief Description of the Drawings**

In order to provide an understanding of embodiments of the invention, reference is made to the appended drawings, which are not necessarily drawn to scale, and in which reference numerals refer to components of exemplary embodiments of the invention. The drawings are exemplary only, and should not be construed as limiting the invention.

20 FIG. 1 is a perspective view of a honeycomb-type substrate carrier which may comprise a catalyst article in the form of a washcoat composition in accordance with the present invention;

FIG. 2 is a partial cross-sectional view enlarged relative to FIG. 1 and taken along a plane parallel to the end faces of the substrate carrier of FIG. 1, which shows an enlarged view of a plurality of the gas flow passages shown in FIG. 1, in an embodiment wherein the substrate carrier 25 is a monolithic flow-through substrate;

FIG. 3 is a cutaway view of a section enlarged relative to FIG. 1, wherein the honeycomb-type substrate carrier in FIG. 1 represents a wall flow filter substrate monolith; and

FIG. 4a – FIG. 4j are partial cross-sections showing coating layers and/or coating zones on one or more substrates according to exemplary embodiments of the present disclosure.

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Detailed Disclosure

Molecular sieves refer to materials having an extensive three-dimensional network of oxygen ions containing generally tetrahedral type sites and having a pore distribution of relatively uniform pore size. A zeolite is a specific example of a molecular sieve, further including silicon 35 and aluminum. Reference to a “non-zeolite-support” or “non-zeolitic support” in a catalyst layer refers to a material that is not a zeolite and that receives precious metals, stabilizers, promoters, binders and the like through association, dispersion, impregnation or other suitable methods.

Examples of such non-zeolitic supports include, but are not limited to, high surface area refractory metal oxides. High surface area refractory metal oxide supports can comprise an activated compound selected from the group consisting of alumina, zirconia, silica, titania, ceria, lanthana, baria and combinations thereof.

5 Present molecular sieves for instance have 8-ring pore openings and double-six ring secondary building units, for example, those having the following structure types: AEI, AFT, AFX, CHA, EAB, ERI, KFI, LEV, SAS, SAT or SAV. Included are any and all isotopic framework materials such as SAPO, AIPO and MeAPO materials having the same structure type.

10 Aluminosilicate zeolite structures do not include phosphorus or other metals isomorphically substituted in the framework. That is, "aluminosilicate zeolite" excludes aluminophosphate materials such as SAPO, AIPO and MeAPO materials, while the broader term "zeolite" includes aluminosilicates and aluminophosphates.

15 The 8-ring small pore molecular sieves include aluminosilicates, borosilicates, gallosilicates, MeAPSOs and MeAPOs. These include, but are not limited to SSZ-13, SSZ-62, natural chabazite, zeolite K-G, Linde D, Linde R, LZ-218, LZ-235, LZ-236, ZK-14, SAPO-34, SAPO-44, SAPO-47, ZYT-6, CuSAPO-34, CuSAPO-44 and CuSAPO-47. In specific embodiments, the 8-ring small pore molecular sieve will have an aluminosilicate composition, such as SSZ-13 and SSZ-62.

20 In one or more embodiments, the 8-ring small pore molecular sieve has the CHA crystal structure and is selected from the group consisting of aluminosilicate zeolite having the CHA crystal structure, SAPO, AIPO, and MeAPO. In particular, the 8-ring small pore molecular sieve having the CHA crystal structure is an aluminosilicate zeolite having the CHA crystal structure. In a specific embodiment, the 8-ring small pore molecular sieve having the CHA crystal structure will have an aluminosilicate composition, such as SSZ-13 and SSZ-62. Copper- and iron-containing 25 chabazite are termed CuCHA and FeCHA.

30 Molecular sieves can be zeolitic (zeolites) or may be non-zeolitic. Both zeolitic and non-zeolitic molecular sieves can have the chabazite crystal structure, which is also referred to as the CHA structure by the International Zeolite Association. Zeolitic chabazite include a naturally occurring tectosilicate mineral of a zeolite group with approximate formula (Ca,Na₂,K₂,Mg)Al₂Si₄O_{12.6}H₂O (i.e., hydrated calcium aluminum silicate). Three synthetic forms of 35 zeolitic chabazite are described in "Zeolite Molecular Sieves," by D. W. Breck, published in 1973 by John Wiley & Sons, which is hereby incorporated by reference. The three synthetic forms reported by Breck are Zeolite K-G, described in J. Chem. Soc., p. 2822 (1956), Barrer et. Al.; Zeolite D, described in British Patent No. 868,846 (1961); and Zeolite R, described in U.S. Pat. No. 3,030,181, which are hereby incorporated by reference. Synthesis of another synthetic form of zeolitic chabazite, SSZ-13, is described in U.S. Pat. No. 4,544,538. Synthesis of a synthetic form of a non-zeolitic molecular sieve having the chabazite crystal structure, silicoaluminophosphate 34

(SAPO-34), is described in U.S. Pat. No. 4,440,871 and U.S. Pat. No. 7,264,789. A method of making yet another synthetic non-zeolitic molecular sieve having chabazite structure, SAPO-44, is described for instance in U.S. Pat. No. 6,162,415.

A synthetic 8-ring small pore molecular sieve (for example having the CHA structure) may 5 be prepared via mixing a source of silica, a source of alumina and a structure directing agent under alkaline aqueous conditions. Typical silica sources include various types of fumed silica, precipitated silica and colloidal silica, as well as silicon alkoxides. Typical alumina sources include boehmites, pseudo-boehmites, aluminum hydroxides, aluminum salts such as aluminum sulfite or sodium aluminate and aluminum alkoxides. Sodium hydroxide is typically added to the reaction 10 mixture. A typical structure directing agent for this synthesis is adamantyltrimethyl ammonium hydroxide, although other amines and/or quaternary ammonium salts may be substituted or added. The reaction mixture is heated in a pressure vessel with stirring to yield a crystalline product. Typical reaction temperatures are in the range of from about 100°C to about 200°C, for instance from about 135°C to about 170°C. Typical reaction times are from about 1 hr to about 30 15 days and in specific embodiments, for instance from 10 hours to 3 days. At the conclusion of the reaction, optionally the pH is adjusted to from about 6 to about 10, for example from about 7 to about 7.5 and the product is filtered and washed with water. Any acid can be used for pH adjustment, for instance nitric acid. Optionally, the product may be centrifuged. Organic additives 20 may be used to help with the handling and isolation of the solid product. Spray-drying is an optional step in the processing of the product. The solid product is thermally treated in air or nitrogen. Alternatively, each gas treatment can be applied in various sequences or mixtures of gases can be applied. Typical calcination temperatures are in from about 400°C to about 850°C.

Molecular sieves having a CHA structure may be prepared for instance according to methods disclosed in U.S. Pat. Nos. 4,544,538 and 6,709,644.

25 The first and second molecular sieves may each have a silica to alumina ratio (SAR) of about 1 to about 50 or about 5 to about 40.

The present molecular sieves are copper-containing or iron-containing. The copper or iron resides in the ion-exchange sites (pores) of the molecular sieves and may also be associated with the molecular sieves but not "in" the pores. Upon calcination, non-exchanged copper salt 30 decomposes to CuO, also referred to herein as "free copper" or "soluble copper." The free copper may be advantageous as disclosed in U.S. Pat. No. 8,404,203. The amount of free copper may be less than, equal to or greater than the amount of ion-exchanged copper.

The copper- or iron-containing molecular sieves are prepared for example via ion-exchange from for example a Na⁺ containing molecular sieve (Na⁺ form). The Na⁺ form generally 35 refers to the calcined form without any ion exchange. In this form, the molecular sieve generally contains a mixture of Na⁺ and H⁺ cations in the exchange sites. The fraction of sites occupied by Na⁺ cations varies depending on the specific zeolite batch and recipe. Optionally, the alkali metal

molecular sieves are NH₄⁺-exchanged and the NH₄⁺ form is employed for ion-exchange with copper or iron. Optionally, the NH₄⁺-exchanged molecular sieve is calcined to the H⁺-form which may also be employed for ion-exchange with copper or iron cations.

5 Copper or iron is ion-exchanged into molecular sieves with alkali metal, NH₄⁺ or H⁺ forms with copper or iron salts such as copper acetate, copper sulfate, iron chloride, iron acetate, iron nitrate, iron sulfate and the like, for example as disclosed in U.S. Pat. No. 9,242,238. For instance a Na⁺, NH₄⁺ or H⁺ form of a molecular sieve is mixed with an aqueous salt solution and agitated at an elevated temperature for a suitable time. The slurry is filtered and the filter cake is washed and dried.

10 A method for activating an iron-containing molecular sieve includes adding iron into a molecular sieve followed by steam-calcination of the resulting iron-containing molecular sieve powder from about 500°C to about 800°C for a period of from about 20 minutes to about 12 hours in the presence of water vapor or from about 650°C to about 750°C for a period of from about 20 minutes to about 2 hours in the presence of water vapor. The steam-calcination periods are for 15 example from about 20 minutes to about 1 hour or 1.5 hours.

The steam-activation step does not require reducing conditions.

The resulting steam-activated iron-containing molecular sieve powders may be spray-dried or air-dried.

20 The resulting steam-activated iron-containing molecular sieves are for example steam-activated FeCHA powders.

Iron addition comprises for instance ion-exchange processes, impregnation of an iron salt or mixing a molecular sieve with iron oxide.

Suitable iron-containing molecular sieves are disclosed for instance in U.S. Pat. No. 9,011,807.

25 Present steam-activated FeCHA molecular sieves are prepared by a method comprising ion-exchange of Fe into the molecular sieve followed by the steam-calcination step. Only one calcination step is required. The present method for steam-activation of FeCHA powder provides a method to pre-activate catalyst prior to coating on a substrate.

30 SCR articles containing the steam-activated FeCHA molecular sieves are for instance capable of providing NO_x conversion of ≥ 90%, ≥ 91%, ≥ 92%, ≥ 93%, ≥ 94% or ≥ 95% at 250°C or over the range of 350°C to 600°C under steady-state fast SCR conditions. The NO_x activity is measured for example under steady state conditions at maximum NH₃-slip conditions in a gas mixture of 500 ppm NO, 500 ppm NH₃, 10% O₂, 5% H₂O, balance N₂ at a volume-based space velocity of 80,000 h⁻¹.

35 Alternatively, present substrates containing coating layers comprising iron-containing molecular sieves may be steam-activated after being coated; that is, the finished monolith with present coatings may be steam treated.

NO_x conversion is defined as mol% conversion of NO and NO₂ combined. A high value is desired. N₂O formation is defined as mol% conversion of NO and NO₂ combined to N₂O. A low value is desired. Percent conversion of NO_x to N₂O is calculated based on the assumption that each molecule of N₂O is derived from one molecule of NO_x and one molecule of NH₃.

5 SCR performances such as the NO_x conversion and N₂O formation are for example measured at a gas hourly volume-based space velocity of 80000 h⁻¹ under pseudo-steady state conditions in a gas mixture of 500 ppm NO_x (fast SCR condition: NO₂/NO_x=0.5 or standard SCR conditions: NO₂/NO_x=0), 500 ppm NH₃, 10% O₂, 5% H₂O, balance N₂ in a temperature ramp of 0.5°C/min from 200°C to 600°C. Such SCR activity measurements are demonstrated in U.S. Pat. 10 No. 8,404,203.

NO_x conversion is defined as mol% conversion of NO and NO₂ combined. A high value is desired. N₂O formation is defined as mol% conversion of NO and NO₂ combined to N₂O. A low value is desired.

15 SCR articles containing steam-activated FeCHA are advantageously prepared by first steam-calcining FeCHA followed by applying it in a catalytic coating to a substrate. That is, FeCHA is steam-activated prior to forming the article.

Alternatively, a catalytic coating containing FeCHA may be applied to a substrate, which coated substrate may be steam-calcined to provide activated FeCHA.

20 Further, at least a portion of a catalytically active metal may be included during a molecular sieve synthetic process such that a tailored colloid contains a structure directing agent, a silica source, an alumina source and a metal ion (e.g. copper) source.

25 The amount of iron in the iron-containing molecular sieve is for example from about 1.0 to about 15 wt% and the amount of copper in the copper-containing molecular sieve is for example from about 0.4 to about 7.0 wt%, for example from about 1 to about 10 wt%, by weight, based on the total weight of the molecular sieve.

30 In some embodiments, the amount of copper in the copper-containing molecular sieve is about 2 to about 8 wt%, about 2.5 to about 6 wt%, or about 3 to about 5 wt%. In particular embodiments, the copper-containing molecular sieve can be provided in a zoned configuration – e.g., having two or more zones of copper-containing molecular sieve having different copper concentrations. A high copper zone, for example, can include copper-containing molecular sieve with a copper concentration of about 3 wt% or greater (e.g., about 3 to about 10 wt%, about 3 to about 8 wt%, about 3 to about 6 wt%, or about 3 to about 4 wt%). A low copper zone, for example, can include copper-containing molecular sieve with a copper concentration of about 2.5 wt% or less (with an understood minimum of 0.1 wt%). For example, a low copper zone can have a copper concentration of about 0.5 to about 2.5 wt%, about 1 to about 2.5 wt%, or about 2 to about 2.5 wt%. In some embodiments, a front zone (e.g., a zone proximate to an inlet of a substrate) can be a low copper zone, and a rear zone (e.g., a zone proximate to an outlet of a

substrate) can be a high copper zone. The section highlighted in Yellow belongs more correctly in the other patent.

Amounts of catalytic metals like copper or iron in a molecular sieve are reported as the oxide, CuO or Fe₂O₃.

5 The total dry weight of the molecular sieve includes the any added/exchanged metals like copper or iron.

The amount of copper in a molecular sieve, for example an aluminosilicate zeolite, may also be defined by the copper to aluminum atomic ratio. For example, the Cu/Al atomic ratio may be from about 0.05 to about 0.55.

10 The amount of iron in a molecular sieve, for example an aluminosilicate zeolite, may also be defined by the iron to aluminum atomic ratio. For example, the Fe/Al atomic ratio may be from about 0.05 to about 2.0. At the higher Fe/Al ratio, a portion of the iron will not be present in traditional ion-exchanged sites but rather as small iron oxide particles.

15 The molecular sieves of the upstream and downstream zones may be the same or may be different. For instance, they may be the same or different regarding their SAR. For example, the first molecular sieve may have a SAR lower than, equal to or greater than the SAR of the second molecular sieve.

20 The 8-ring small pore molecular sieves containing copper may each have a sodium content (reported as Na₂O on a volatile free basis) of below 2 wt%, based on the total weight of the calcined molecular sieve. In more specific embodiments, sodium content is below 1 wt% or below 2500 ppm. The molecular sieves may each have an atomic sodium to aluminum ratio of less than about 0.7, for example from about 0.02 to about 0.7. The molecular sieves may each have an atomic copper to sodium or iron to sodium ratio of greater than about 0.5, for example from about 0.5 to about 50.

25 The present copper- or iron-containing molecular sieves may exhibit a BET surface area, determined according to DIN 66131, of at least about 400 m²/g, at least about 550 m²/g or at least about 650 m²/g, for example from about 400 to about 750 m²/g or from about 500 to about 750 m²/g. The present molecular sieves may have a mean crystal size of from about 10 nanometers to about 10 microns, from about 50 nanometers to about 5 microns or from about 0.1 microns to about 0.5 microns as determined via SEM. For instance, the molecular sieve crystallites may have a mean crystal size greater than 0.1 microns or 1 micron and less than 5 microns.

30 The molecular sieves may be provided in the form of a powder or a spray-dried material which is admixed with or coated with suitable modifiers. Modifiers include silica, alumina, titania, zirconia and refractory metal oxide binders (for example a zirconium precursor). The powder or 35 the sprayed material, optionally after admixing or coating by suitable modifiers, may be formed into a slurry, for example with water, which is deposited upon a suitable substrate as disclosed for example in U.S. Pat. No. 8,404,203.

Advantageously, the amount of the iron-containing molecular sieves to the copper-containing molecular sieves in the present articles and systems is from about 1:10 to about 10:1, by weight. For instance, these represent weight ratios of iron-containing molecular sieves in the upstream zone to copper-containing molecular sieves in the downstream zone.

5 Advantageously, the weight ratio of iron to copper in the present articles and systems is from about 1:15 to about 15:1, based on weight of the oxides. This may represent the weight ratios of iron in the upstream zone to copper in the downstream zone.

The molecular sieves of the iron-containing molecular sieves may include 8-ring or alternatively, may also include 10-ring or 12-ring molecular sieves.

10 The term “catalyst” refers to a material that promotes a chemical reaction. The catalyst includes the “catalytically active species” and the “carrier” that carries or supports the active species. For example, molecular sieves including zeolites are carriers/supports for present copper and iron active catalytic species. Likewise, refractory metal oxide particles may be a carrier for platinum group metal catalytic species.

15 The catalytically active species are also termed “promoters” as they promote chemical reactions. For instance, the present copper- or iron-containing molecular sieves may be termed copper- or iron-promoted molecular sieves. A “promoted molecular sieve” refers to a molecular sieve to which catalytically active species are intentionally added.

20 Selective catalytic reduction (SCR) of nitrogen oxides (NO_x) means selective reduction to N₂.

The term “substrate” refers in general to a monolithic material onto which a catalytic coating is disposed, for example a flow-through monolith or monolithic wall-flow filter. In one or more embodiments, the substrate is a ceramic or metal having a honeycomb structure. Any suitable substrate may be employed, such as a monolithic substrate of the type having fine, 25 parallel gas flow passages extending from an inlet end to an outlet end of the substrate such that passages are open to fluid flow. The passages, which are essentially straight paths from their fluid inlet to their fluid outlet, are defined by walls on which a catalytic coating is disposed so that gases flowing through the passages contact the catalytic material. The flow passages of the monolithic substrate are thin-walled channels, which can be of any suitable cross-sectional shape and size 30 such as trapezoidal, rectangular, square, sinusoidal, hexagonal, triangular, etc. Such structures may contain from about 60 to about 900 or more gas inlet openings (i.e. cells) per square inch of cross-section.

Present substrates are 3-dimensional having a length and a diameter and a volume, similar to a cylinder. The shape does not necessarily have to conform to a cylinder. The length is an 35 axial length defined by an inlet end and an outlet end.

Flow-through monolith substrates for example have a volume of from about 50 in³ to about 1200 in³, a cell density of from about 60 cells per square inch (cpsi) to about 500 cpsi or up to

about 900 cpsi, for example from about 200 to about 400 cpsi and a wall thickness of from about 50 to about 200 microns or about 400 microns.

The substrate may be a “flow-through” monolith as described above. Alternatively, a catalytic coating may be disposed on a wall-flow filter soot filter, thus producing a Catalyzed Soot Filter (CSF). If a wall-flow substrate is utilized, the resulting system will be able to remove particulate matter along with gaseous pollutants. The wall-flow filter substrate can be made from materials commonly known in the art, such as cordierite, aluminum titanate or silicon carbide. Loading of the catalytic coating on a wall-flow substrate will depend on substrate properties such as porosity and wall thickness and typically will be lower than the catalyst loading on a flow-through substrate.

Wall-flow filter substrates useful for supporting the SCR catalytic coatings have a plurality of fine, substantially parallel gas flow passages extending along the longitudinal axis of the substrate. Typically, each passage is blocked at one end of the substrate body, with alternate passages blocked at opposite end-faces. Such monolithic carriers may contain up to about 700 or more flow passages (or “cells”) per square inch of cross-section, although far fewer may be used. For example, the typical carrier usually has from about 100 to about 300, cells per square inch (“cpsi”). The cells can have cross-sections that are rectangular, square, triangular, hexagonal, or are of other polygonal shapes. Wall-flow substrates typically have a wall thickness from about 50 microns to about 500 microns, for example from about 150 microns to about 400 microns. Wall-flow filters will generally have a wall porosity of at least 40% with an average pore size of at least 10 microns prior to disposition of the catalytic coating. For instance, wall-flow filters will have a wall porosity of from about 50 to about 75% and an average pore size of from about 10 to about 30 microns prior to disposition of a catalytic coating.

FIGS. 1 and 2 illustrate an exemplary substrate 2 in the form of a flow-through substrate coated with a washcoat composition as described herein. Referring to FIG. 1, the exemplary substrate 2 has a cylindrical shape and a cylindrical outer surface 4, an upstream end face 6 and a corresponding downstream end face 8, which is identical to end face 6. Substrate 2 has a plurality of fine, parallel gas flow passages 10 formed therein. As seen in FIG. 2, flow passages 10 are formed by walls 12 and extend through carrier 2 from upstream end face 6 to downstream end face 8, the passages 10 being unobstructed so as to permit the flow of a fluid, e.g., a gas stream, longitudinally through carrier 2 via gas flow passages 10 thereof. As more easily seen in FIG. 2, walls 12 are so dimensioned and configured that gas flow passages 10 have a substantially regular polygonal shape. As shown, the washcoat composition can be applied in multiple, distinct layers if desired. In the illustrated embodiment, the washcoat consists of both a discrete bottom washcoat layer 14 adhered to the walls 12 of the carrier member and a second discrete top washcoat layer 16 coated over the bottom washcoat layer 14. The present invention can be

practiced with one or more (e.g., 2, 3, or 4) washcoat layers and is not limited to the illustrated two-layer embodiment.

Alternatively, FIGS. 1 and 3 can illustrate an exemplary substrate 2 in the form a wall flow filter substrate coated with a washcoat composition as described herein. As seen in FIG. 3, the

5 exemplary substrate 2 has a plurality of passages 52. The passages are tubularly enclosed by the internal walls 53 of the filter substrate. The substrate has an inlet end 54 and an outlet end 56.

Alternate passages are plugged at the inlet end with inlet plugs 58, and at the outlet end with outlet

10 plugs 60 to form opposing checkerboard patterns at the inlet 54 and outlet 56. A gas stream 62

enters through the unplugged channel inlet 64, is stopped by outlet plug 60 and diffuses through

15 channel walls 53 (which are porous) to the outlet side 66. The gas cannot pass back to the inlet

side of walls because of inlet plugs 58. The porous wall flow filter used in this invention is

catalyzed in that the wall of said element has thereon or contained therein one or more catalytic

materials. Catalytic materials may be present on the inlet side of the element wall alone, the outlet

side alone, both the inlet and outlet sides, or the wall itself may consist all, or in part, of the

15 catalytic material. This invention includes the use of one or more layers of catalytic material on the

inlet and/or outlet walls of the element.

Catalyzed wall-flow filters are disclosed for instance in U.S. Pat. No. 7,229,597. This

reference teaches a method of applying a catalytic coating such that the coating permeates the

porous walls, that is, is dispersed throughout the walls. Flow-through and wall-flow substrates are

20 also taught for example in U.S. Pat. app. No. 62/072,687, published as WO2016/070090.

For example, in the present systems the first substrate is a porous wall-flow filter and the second substrate is a flow-through monolith or alternatively, the first substrate is a flow-through monolith and the second substrate is a porous wall-flow filter. Alternatively, both substrates may be identical and may be flow-through or wall-flow substrates.

25 The present catalytic coating may be on the wall surface and/or in the pores of the walls, that is "in" and/or "on" the filter walls. Thus, the phrase "having a catalytic coating thereon" means on any surface, for example on a wall surface and/or on a pore surface.

The term "exhaust stream" or "exhaust gas stream" refers to any combination of flowing

gas that may contain solid or liquid particulate matter. The stream comprises gaseous

30 components and is for example exhaust of a lean burn engine, which may contain certain non-gaseous components such as liquid droplets, solid particulates and the like. An exhaust stream of a lean burn engine typically further comprises combustion products, products of incomplete combustion, oxides of nitrogen, combustible and/or carbonaceous particulate matter (soot) and un-reacted oxygen and/or nitrogen.

35 Certain embodiments pertain to the use of articles, systems and methods for removing NOx from exhaust gases of internal combustion engines, in particular diesel engines, which

operate at combustion conditions with air in excess of that required for stoichiometric combustion, i.e. lean conditions.

The inlet end of a substrate is synonymous with the “upstream” end or “front” end. The outlet end is synonymous with the “downstream” end or “rear” end. A substrate will have a length and a width. An upstream zone is upstream of a downstream zone. A zone of a catalyzed substrate is defined as a cross-section having a certain coating structure thereon.

In the present exhaust gas treatment methods, the exhaust gas stream is passed through the SCR article, SCR system or exhaust gas treatment system by entering the upstream end and exiting the downstream end.

10 The ceramic substrate may be made of any suitable refractory material, e.g. cordierite, cordierite- α -alumina, aluminum titanate, silicon carbide, silicon nitride, zircon mullite, spodumene, alumina-silica-magnesia, zircon silicate, sillimanite, a magnesium silicate, zircon, petalite, α -alumina, an aluminosilicate and the like.

15 Substrates useful in the present invention may also be metallic and be composed of one or more metals or metal alloys. The metallic substrates may be employed in various shapes such as pellets, corrugated sheet or monolithic foam. Specific examples of metallic substrates include the heat-resistant, base-metal alloys, especially those in which iron is a substantial or major component. Such alloys may contain one or more of nickel, chromium, and aluminum, and the total of these metals may advantageously comprise at least about 15 wt% (weight percent) of the 20 alloy, for instance, about 10 to about 25 wt% chromium, about 1 to about 8 wt% of aluminum, and from 0 to about 20 wt% of nickel.

25 A catalytic coating contains one or more carriers containing active catalytic species. A catalytic coating may typically be applied in the form of a washcoat containing carriers having catalytically active species thereon. A washcoat is formed by preparing a slurry containing a specified solids content (e.g., 10-60% by weight) of carriers in a liquid vehicle, which is then coated onto a substrate and dried and calcined to provide a coating layer. When multiple coating layers are applied, the substrate is dried and calcined after each layer is applied and/or after the number of desired multiple layers are applied.

30 Coating layers of molecular sieves may be prepared using a binder, for example, a ZrO_2 binder derived from a suitable precursor such as zirconyl acetate or any other suitable zirconium precursor such as zirconyl nitrate. Zirconyl acetate binder provides a catalytic coating that remains homogeneous and intact after thermal aging, for example, when the catalyst is exposed to high temperatures of at least about 600°C, for example, about 800°C and higher, and high water vapor environments of about 10% or more. Other potentially suitable binders include, but are not 35 limited to, alumina and silica. Alumina binders include aluminum oxides, aluminum hydroxides, and aluminum oxyhydroxides. Aluminum salts and colloidal forms of alumina may also be used.

Silica binders include various forms of SiO_2 , including colloidal silica. Binder compositions may include any combination of zirconia, alumina, and silica.

Any of present coating layers may contain ZrO_2 or Al_2O_3 binders.

The catalytic coating may comprise more than one thin adherent layer. The coating is

5 disposed on and in adherence to the substrate. The entire coating comprises the individual "coating layers". The catalytic coating is "zoned", comprising zoned catalyst layers. This may also be described as "laterally zoned". For example, a first layer may extend from the inlet end towards the outlet end extending about 5% to about 100%, about 10% to about 90%, or about 20% to about 50% of the substrate length. A second layer may extend from the outlet end towards the
10 inlet end extending about 5% to about 100%, about 10% to about 90%, or about 20% to about 50% of the substrate length. The first and second layers may be adjacent to each other and not overlay each other. Alternatively, the first and second layers may overlay a portion of each other, providing a third "middle" zone. The middle zone may for example extend from about 5% to about 80% of the substrate length, for example about 5%, about 10%, about 20%, about 30%, about
15 40%, about 50%, about 60% or about 70% of the substrate length. Alternatively, the first layer may extend from the outlet end and the second layer may extend from the inlet end.

The first and second layers may each extend the entire length of the substrate or may each extend a portion of the length of the substrate and may overlay or underlay each other, either partially or entirely. Each of the first and second layers may extend from either the inlet end or the
20 outlet end.

The first coating layer may extend the entire length of the substrate and the second coating layer may overlay or underlay a portion or all of the first layer. For example, the second coating layer may extend from the outlet end towards the inlet end about 10%, about 20%, about 30%, about 40%, about 50%, about 60%, about 70% or about 80% of the substrate length.

25 The second coating layer may extend the entire length of the substrate and the first coating layer may overlay or underlay a portion or all of the second layer. For example, the first coating layer may extend from the inlet end towards the outlet end about 10%, about 20%, about 30%, about 40%, about 50%, about 60%, about 70% or about 80% of the substrate length.

The present zones are defined by the relationship of the first and second coating layers.

30 With respect to the first and second coating layers, there may only an upstream and a downstream zone or there may be an upstream zone, a middle zone and a downstream zone. Where the first and second layers are adjacent and do not overlap, there are only upstream and downstream zones. Where the first and second layers overlap to a certain degree, there are upstream, downstream and middle zones. Where for example, a first coating layer extends the entire length
35 of the substrate and the second coating layer extends from the outlet end a certain length and overlays a portion of the first coating layer, there are only upstream and downstream zones.

The first and/or second coating layers may be in direct contact with the substrate.

Alternatively, one or more “undercoats” may be present, so that at least a portion of the first and/or the second coating layers are not in direct contact with the substrate (but rather with the undercoat). One or more “overcoats” may also be present, so that at least a portion of the first and/or second coating layers are not directly exposed to a gaseous stream or atmosphere (but rather are in contact with the overcoat).

5 The first and second coating layers may be in direct contact with each other without a “middle” overlapping zone. Alternatively, the first and second coating layers may not be in direct contact, with a “gap” between the two zones. In the case of an “undercoat” or “overcoat” the gap 10 between the first and second SCR layer is termed an “interlayer.”

An undercoat is a layer “under” a coating layer, an overcoat is a layer “over” a coating layer and an interlayer is a layer “between” two coating layers.

The interlayer(s), undercoat(s) and overcoat(s) may contain one or more catalysts or may be free of catalysts.

15 The present catalytic coatings may comprise more than one identical layers, for instance more than one first and/or second layers.

The simplest articles of the present invention comprise a flow-through substrate or a wall-flow filter having a first coating layer extending from the inlet end of the monolith or filter towards the outlet end and a second coating layer extending from the outlet end towards the inlet end.

20 The present catalytic coating, as well as each zone of a catalytic coating or any section of a coating, is present on the substrate at a concentration (loading) of for instance from about 0.3 g/in³ to about 4.5 g/in³, or from about 0.4, about 0.5, about 0.6, about 0.7, about 0.8, about 0.9 or about 1.0 g/in³ to about 1.5 g/in³, about 2.0 g/in³, about 2.5 g/in³, about 3.0 g/in³, about 3.5 g/in³ or about 4.0 g/in³, based on the substrate. This refers to dry solids weight per volume of substrate, for

25 example per volume of a honeycomb monolith. The amount of base metal, for example copper, is only a portion of the catalytic coating, which also includes the molecular sieve. An amount of copper per volume would for instance be from about 0.2% to about 10% of the above values. An amount of copper per volume is the copper concentration. An amount of iron per volume is the iron concentration. An amount of a base metal-containing molecular sieve per volume is the 30 molecular sieve concentration. Concentration is based on a cross-section of a substrate or on an entire substrate.

The term “catalytic article” refers to an element that is used to promote a desired reaction. The present catalytic articles comprise a substrate having a catalytic coating disposed thereon.

35 A system contains more than one article, for instance, a first SCR article and a second SCR article. A system may also comprise one or more articles containing a reductant injector, a diesel oxidation catalyst (DOC), a soot filter or an ammonia oxidation catalyst (AMOx) or a lean NOx trap (LNT).

An article containing a reductant injector is a reduction article. A reduction system includes a reductant injector and/or a pump and/or a reservoir, etc.

The present treatment system may further comprise a diesel oxidation catalyst and/or a soot filter and/or an ammonia oxidation catalyst. A soot filter may be uncatalyzed or may be catalyzed (CSF). For instance, the present treatment system may comprise, from upstream to downstream – an article containing a DOC, a CSF, an urea injector, the present zoned SCR article or a first SCR article and a second SCR article and an article containing an AMOx. A lean NOx trap (LNT) may also be included.

An undercoat layer comprising an AMOx catalyst may be present in the downstream zone of a substrate. For instance an AMOx undercoat layer may extend from the outlet end towards the inlet end about 10%, about 20%, about 30%, about 40%, about 50%, about 60%, about 70% or about 80% of the substrate length of a present article.

An AMOx undercoat layer may also be present on a second substrate of a second downstream article. This undercoat layer may extend the entire length of the second substrate or about 10%, about 20%, about 30%, about 40%, about 50%, about 60%, about 70%, about 80% or about 90% of the second substrate length.

AMOx catalysts are taught for instance in U.S. Pub. No. 2011/0271664. An ammonia oxidation (AMOx) catalyst may be a supported precious metal component which is effective to remove ammonia from an exhaust gas stream. The precious metal may include ruthenium, rhodium, iridium, palladium, platinum, silver or gold. For example, the precious metal component includes physical mixtures or chemical or atomically-doped combinations of precious metals. The precious metal component for instance includes platinum. Platinum may be present in an amount of from about 0.008% to about 2 wt% based on the AMOx catalyst.

The precious metal component is typically deposited on a high surface area refractory metal oxide support. Examples of suitable high surface area refractory metal oxides include alumina, silica, titania, ceria, and zirconia, as well as physical mixtures, chemical combinations and/or atomically-doped combinations thereof. In specific embodiments, the refractory metal oxide may contain a mixed oxide such as silica-alumina, amorphous or crystalline aluminosilicates, alumina-zirconia, alumina-lanthana, alumina-baria, alumina-ceria and the like. An exemplary refractory metal oxide comprises high surface area γ -alumina having a specific surface area of about 50 to about 300 m^2/g .

The AMOx catalyst may include a zeolitic or non-zeolitic molecular sieve for example selected from those of the CHA, FAU, BEA, MFI and MOR types. A molecular sieve may be physically mixed with an oxide-supported platinum component. In an alternative embodiment, platinum may be distributed on the external surface or in the channels, cavities or cages of the molecular sieve.

Present embodiments that include a first selective catalytic reduction article and a second selective catalytic reduction article may be referred to as a “multi-component” or “multi-brick” system. A “brick” may refer to a single article such as a monolith or filter.

Advantageously, articles of a multi-component system may each contain substrates 5 containing zoned coatings as disclosed herein.

The catalytic articles are effective to catalyze the reduction of nitrogen oxides (NO_x) in the presence of a reductant, for example ammonia or urea. In operation, the reductant is periodically metered into the exhaust stream from a position upstream of the SCR article. The injector is in fluid communication with and upstream of the SCR article. The injector will also be associated 10 with a reductant reservoir and a pump.

Present articles, systems and methods are suitable for treatment of exhaust gas streams from mobile emissions sources such as trucks and automobiles. Articles, systems and methods are also suitable for treatment of exhaust streams from stationary sources such as power plants.

Ammonia is a typical reductant for SCR reactions for treating exhaust of stationary power 15 plants while urea is the typical SCR reducing agent used for treatment of exhaust of mobile emissions sources. Urea decomposes to ammonia and carbon dioxide prior to contact with or on the SCR catalyst, where ammonia serves as the reducing agent for NO_x.

The articles, systems and methods described herein can for example provide high NO_x conversion. For example, a present catalytic article may exhibit an aged NO_x conversion at 200°C 20 or at least 50%, at least 55% or at least 60% measured at a gas hourly space velocity of 80000 h⁻¹. A present catalytic article may exhibit an aged NO_x conversion at 450°C of at least 70%, at least 75% or at least 80% measured at a gas hourly volume-based space velocity of 80000 h⁻¹ under steady state conditions in a gas mixture of 500 ppm NO, 500 ppm NH₃, 10% O₂, 5% H₂O, balance N₂. The cores are hydrothermally aged in a tube furnace in a gas flow containing 10% H₂O, 10% 25 O₂, balance N₂ for 5 hours at 750°C. Such SCR activity measurements are demonstrated in U.S. Pat. No. 8,404,203.

Further, articles, systems and methods herein may provide NO_x conversion under transient HDD FTP conditions of $\geq 90\%$ and also an N₂O formation of $\leq 1.5\%$.

For example, some present selective catalytic reduction articles or systems are capable of 30 providing NO_x conversion of $\geq 90\%$ and N₂O formation of $\leq 40\%$ compared an article or system, respectively, containing a uniform concentration of CuCHA as the only SCR catalyst under transient engine testing conditions. An article containing a uniform concentration of CuCHA contains a catalytic coating comprising a CuCHA at a uniform concentration on the substrate; CuCHA is the only SCR catalyst present as a reference. Likewise, as a system reference, both 35 substrates contain uniform concentrations of the same CuCHA as the only SCR catalyst.

That is, present articles and systems provide as good or better NO_x conversion while forming less N₂O.

Also disclosed are SCR articles comprising a substrate having a front upstream end (which may define an inlet) and a rear downstream end (which may define an outlet), the two ends defining an axial length, and the substrate having a catalytic coating thereon at least partially along the axial length between the two ends, where the catalytic coating comprises steam-activated FeCHA and CuCHA.

5 In this case, the coating may extend the entire length of the substrate or a partial length from the outlet or inlet ends, for instance about 10%, about 20%, about 30%, about 40%, about 50%, about 60%, about 70%, about 80% or about 90% of the axial length.

When a catalytic coating contains both steam-activated FeCHA and CuCHA, the weight ratio may be from about 1:10 to about 10:1, for example about 1:9, about 1:8, about 1:7, about 1:6, 10 about 1:5, about 1:4, about 1:3, about 1:2, about 1:1, about 2:1, about 3:1, about 4:1, about 5:1, about 6:1, about 7:1, about 8:1 or about 9:1.

15 Present selective catalytic reduction articles or systems or methods are for example capable of providing y total NO_x conversion where the front upstream zone provides from about 0.6 y to about 0.9 y of the total NO_x conversion, for example measured under transient HDD FTP conditions. For instance, the upstream zone provides about 0.5 y , about 0.6 y , about 0.7 y , about 15 0.8 y or about 0.9 y of the total NO_x conversion.

20 Exemplary embodiments of the invention are shown below. It is understood that the embodiments are provided as examples, and further combinations of catalytic coatings are encompassed. Further, as exemplified, coating zones and coating layers may be interchangeable in that a coating layer may define a coating zone.

In one embodiment, as seen in FIG. 4a, a substrate 100 can be coated with a single coating layer 101 that is a combination of multiple catalytically active molecular sieves. For example, the single coating 101 can be a combination of steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide) and copper-containing molecular 25 sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%). In another embodiment, referring again to FIG. 4a, a substrate 100 can be coated with a single layer 101 that is a combination of: iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); and iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper).

30 In a further embodiment, a substrate 100 can be coated with two non-overlapping zones. As seen in FIG. 4b, a first zone 102 proximate to the front or inlet end 100a of the substrate 100 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a combination of iron-containing molecular sieve and 35 copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1). A second zone 103 proximate to the rear or

outlet end 100b of the substrate 100 can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 1:1 to about 1:100).

5 In still a further embodiment, as seen in FIG. 4c, a substrate 100 can be coated with a first coating layer 104 extending from the front or inlet end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100 and a second coating layer 105 that is coated over the first coating layer 104 proximate to the rear or outlet end 100b of the substrate 100 and extending across only a partial length of the substrate 100 (i.e., terminating before reaching the front or inlet end 100a of the substrate 100). The first coating layer 104 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide);

10 iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1). The second coating layer 105 can comprise any one of the following: copper-15 containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 20 1:1 to about 1:100).

25

In another embodiment, as seen in FIG. 4d, a substrate 100 can be coated with a first coating layer 106 extending from the front or inlet end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100 and a second coating layer 107 that is coated over the first coating layer 106 proximate to the front or inlet end 100a of the substrate 100 and extending across only a partial length of the substrate 100 (i.e., terminating before reaching the rear or outlet end 100b of the substrate 100). The first coating layer 106 can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 1:1 to about 1:100). The second coating layer 107 can comprise any one of the following:

steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1).

5 In yet another embodiment, as seen in FIG. 4e, a substrate 100 can be coated with a first coating layer 108 extending from the front or inlet end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100 and a second coating layer 109 that is coated over the first 10 coating layer 108 also extending from the front or inlet end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100. The first coating layer 108 can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper- 15 containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 1:1 to about 1:100). The second coating layer 109 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 20 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1).

25 In a further embodiment, as seen in FIG. 4f, a first substrate 100 can be coated with a first coating layer 110, and a second, separate substrate 100' can be coated with a second coating layer 111. The first coating layer 110 on the first substrate 100 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular 30 sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1). The second coating layer 111 on the second, separate substrate 100' can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low 35 iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-

containing molecular sieve being about 1:1 to about 1:100). The first substrate 100 is upstream from the second, separate substrate 100' relative to the flow path of an exhaust stream. The first coating layer 110 can extend from a front or inlet end 100a to a rear or outlet end 100b of the first substrate 100, and the second coating layer 111 can extend from a front or inlet end 100a' to a rear or outlet end 100b' of the second substrate 100'.

5 In still a further embodiment, as seen in FIG. 4g and FIG. 4i, a substrate 100 can be coated with a first coating layer 112 proximate to the front or inlet end 100a of the substrate 100 and extending only partially along the length of the substrate 100 (i.e., terminating before reaching the rear or outlet end 100b of the substrate 100). The substrate 100 can be coated with a second 10 coating layer 113. As seen in FIG. 4f, the second coating layer 113 extends from the front or inlet end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100 (and thus is coated completely over the first coating layer 112). As seen in FIG. 4h, the second coating layer 113 extends from the rear or outlet end 100b of the substrate 100 only a partial length toward the front or inlet end 100a of the substrate 100 to a point so that the second coating layer 113 is 15 coated over a portion of the substrate 100 and also over a portion of the first coating layer 112.

The first coating layer 112 on the substrate 100 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a 20 combination of iron-containing molecular sieve and copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1). The second coating layer 113 on the substrate 100 can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing 25 molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 1:1 to about 1:100). As described above, the second coating layer 113 can partially cover the first coating layer 112 or completely cover the first coating layer 112.

30 In an additional embodiment, as seen in FIG. 4h and FIG. 4j, a substrate 100 can be coated with a first coating layer 115 proximate to the rear or outlet end 100b of the substrate 100 and extending only partially along the length of the substrate 100 (i.e., terminating before reaching the front or inlet end 100a of the substrate 100). The substrate 100 can be coated with a second coating layer 114. As seen in FIG. 4h, the second coating layer 114 extends from the front or inlet 35 end 100a of the substrate 100 to the rear or outlet end 100b of the substrate 100 (and thus is coated completely over the first coating layer 115). As seen in FIG. 4j, the second coating layer 114 extends from the front or inlet end 100a of the substrate 100 only a partial length toward the

rear or outlet end 100b of the substrate 100 to a point so that the second coating layer 114 is coated over a portion of the substrate 100 and also over a portion of the first coating layer 115. The first coating layer 115 on the substrate 100 can comprise any one of the following: steam-activated iron-containing molecular sieve (e.g., with about 1 to about 10 wt% iron oxide); iron and copper-containing molecular sieve in a high iron to copper ratio (e.g., 10:1 to 1:1 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a high iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 100:1 to about 1:1). The second coating layer 114 on the substrate 100 can comprise any one of the following: copper-containing molecular sieve, preferably at a high copper concentration (e.g., about 3 to about 10 wt%); iron and copper-containing molecular sieve in a low iron to copper ratio (e.g., 1:1 to 1:100 iron to copper); a combination of iron-containing molecular sieve and copper-containing molecular sieve in a low iron-containing molecular sieve to copper-containing molecular sieve ratio (e.g., weight ratio of iron-containing molecular sieve to copper-containing molecular sieve being about 1:1 to about 1:100). As described above, second coating layer 114 can partially cover the first coating layer 115 or completely cover the first coating layer 115.

“Platinum group metal components” refer to platinum group metals or one of their oxides. “Rare earth metal components” refer to one or more oxides of the lanthanum series defined in the Periodic Table of Elements, including lanthanum, cerium, praseodymium and neodymium.

“Substantially free” means for instance “little or no”, for instance, means “no intentionally added” and having only trace and/or inadvertent amounts. For instance, it means less than 2 wt% (weight %), less than 1.5 wt%, less than 1.0 wt%, less than 0.5 wt%, 0.25 wt% or less than 0.01 wt%, based on the weight of the indicated total composition.

“Substantially all” means for example at least 90% at least 91%, at least 92%, at least 93%, at least 94%, at least 95%, at least 96%, at least 97%, at least 98%, at least 99% or at least 99.5%, by weight or by number.

The articles “a” and “an” herein refer to one or to more than one (e.g. at least one) of the grammatical object. Any ranges cited herein are inclusive. The term “about” used throughout is used to describe and account for small fluctuations. For instance, “about” may mean the numeric value may be modified by \pm 5%, \pm 4%, \pm 3%, \pm 2%, \pm 1%, \pm 0.5%, \pm 0.4%, \pm 0.3%, \pm 0.2%, \pm 0.1% or \pm 0.05%. All numeric values are modified by the term “about” whether or not explicitly indicated. Numeric values modified by the term “about” include the specific identified value. For example “about 5.0” includes 5.0.

Unless otherwise indicated, all parts and percentages are by weight. Weight percent (wt%), if not otherwise indicated, is based on an entire composition free of any volatiles, that is, based on dry solids content.

All U.S. patent applications, published patent applications and patents referred to herein are hereby incorporated by reference.

Examples SCR Articles, Preparation and Testing

5

Example 1 Steam-Activated FeCHA

Molecular sieves having a CHA structure are prepared according to methods disclosed in U.S. Pat. Nos. 4,544,538 and 6,709,644. Employed is a CHA zeolite having a silica-to-alumina (SAR) ratio of approximately 30. Iron is incorporated into the CHA zeolite through Fe ion-exchange at about 60°C for about 2 hours at pH about 4 using Fe(3+) nitrate or Fe(2+) sulfate in the presence of ammonium acetate. The mixture is then washed with deionized water, filtered and vacuum/air-dried. Samples are prepared targeting 2.3 wt% Fe₂O₃ loading based on the iron zeolite. Post-treatments of the air-dried zeolite powders are 1) air-dry only, 2) calcination in air at 450°C or 3) calcination in a pilot scale rotary calciner at a temperature of 650 to 800°C in the presence of steam.

Washcoat slurries are prepared by mixing water and FeCHA to generate a target 40% by weight solids slurry also containing binder. Catalytic coatings containing FeCHA zeolite are deposited via a washcoat process on cellular ceramic monoliths having a cell density of 400 cpsi and a wall thickness of 6 mil. The coated monoliths are dried at 110°C. The coating process provides a catalyst loading of 2.1 g/in³.

Hydrothermal treatment of the coated monoliths with steam are achieved by allowing an approximately 10%O₂, 10% H₂O in N₂ flow over the monolith at the required temperature (650°C or 750°C) at space velocity of 9000h⁻¹ for the specified amount of time.

NO_x conversion and N₂O formation are measured at a gas hourly volume-based space velocity of 80000 h⁻¹ under pseudo-steady state conditions in a gas mixture of 500 ppm NO_x (fast SCR condition: NO₂/NOx=0.5 or standard SCR conditions: NO₂/NOx=0), 500 ppm NH₃, 10% O₂, 5% H₂O, balance N₂ in a temperature ramp of 0.5°C/min from 200°C to 600°C. NOx conversion results under fast conditions are as follows. NOx conversion is reported as mol% and measured as NO and NO₂.

30

test	temp	fresh	650°C/10h steam	750°C/5h steam
1	250°C	25%	----	93%
	600°C	94%	----	92%
2	250°C	29%	81%	92%
	600°C	97%	97%	92%
35	250°C	94%	----	----
	600°C	96%	----	----

The prepared powders of test 1 are post-treated by 1) air-dry only. The prepared powders of test 2 are post-treated by 2) 450°C calcination in air. The prepared powders of test 3 are post-treated by steam-calcination at 750°C. The monoliths are subsequently coated with the thus post-treated catalyst powders. "Fresh" means the monolith is not hydrothermally treated.

It is seen steam-activation of FeCHA provides for greatly improved low temperature (250°C) SCR performance and that more than one calcination step is not required. Furthermore, steam-calcination of iron-zeolite does not have a negative impact on the high temperature (600°C) SCR performance. Steam-calcination of zeolite powders thus provides a method to pre-activate catalyst prior to coating.

Example 2 Zoned FeCHA / CuCHA Catalytic Coatings

Catalytic coatings containing FeCHA zeolite and CuCHA zeolite are disposed via a washcoat process on cellular ceramic monoliths having a cell density of 400 cpsi and a wall thickness of 6 mil. The coated cores are dried at 110°C and calcined at about 450°C for 1 hour. All CuCHA catalysts have loading of 3.0 g/in³ and all FeCHA catalysts have a loading of 2.1 g/in³. The front and rear zones are of equal coating volume. All samples are hydrothermally aged in the presence of 10% H₂O/air at 750°C for 5 hours. The front zone extends from the inlet end of the core to about 50% of the total length of the core and the rear zone extends from the outlet end of the core to about 50% of the total length of the core. Reference samples have uniform coatings.

SCR testing of aged samples is performed under Heavy Duty Diesel US Federal Test Procedure (HDD FTP) cycle conditions. The transient temperature of the HDD FTP test ranges from 225°C and 325°C. The cumulative inlet NO_x per cycle (1200 sec) is 5 g/L. The transient space velocity ranges from 20K to 120K hr⁻¹. Reported are HDD FTP NO_x conversion and N₂O formation results. Front and rear zone iron and copper is weight %, based on the total weight of the zeolite. Weight percent Cu is reported as CuO, weight percent Fe is reported as Fe₂O₃.

NO_x conversion is defined as mol% conversion of NO and NO₂ combined. A high value is desired. N₂O formation is defined as mol% conversion of NO and NO₂ combined to N₂O. A low value is desired. Percent conversion of NO_x to N₂O is calculated based on the assumption that each molecule of N₂O is derived from one molecule of NO_x and one molecule of NH₃.

Reference Comparative Examples with Equal Front and Rear Cu Loadings

	front zone Cu (wt%)	rear zone Cu (wt%)	NOx conversion (%)	N ₂ O formation (%)
5	ref1)	0.6	86.6	1.0
	ref2)	1.2	91.1	1.7
	ref3)	2.3	93.8	2.5
	ref4)	2.7	94.4	2.8
	ref5)	3.4	93.8	3.0

10

Inventive Samples

	front zone Fe (wt%)	rear zone Cu (wt%)	NOx conversion (%)	N ₂ O formation (%)
15	2a)	2.3	90.9	0.7
	2b)	2.3	90.5	1.0
	2c)	2.3	91.2	1.0
	2d)	2.3	90.7	1.1
	2e)	4.4	89.1	0.7
	2f)	4.4	87.9	0.6
	2g)	4.4	93.7	1.4
	2h)	4.4	91.6	1.0
	2i)	4.4	91.4	1.1
	2j)	9.3	83.9	0.6
	2k)	9.3	89.2	0.4
	2l)	9.3	93.3	0.6
20	2m)	9.3	94.5	1.7
	2n)	9.3	95.9	1.8

The reference samples are uniform coatings containing CuCHA at various weight percents.

30 It is seen that inventive samples 2a-2n exhibit excellent NOx conversion (generally $\geq 90\%$) while reducing N₂O formation greatly compared to the reference samples resulting in overall better performance. Inventive samples 2c, 2g, 2h, 2i, 2l, 2m and 2n achieve NOx conversion of $\geq 91\%$ and a maximum N₂O formation of $\leq 1.8\%$.

Claims

1. A method for activating an iron-containing molecular sieve powder, the method comprising:

5 adding iron into a molecular sieve to form an iron-containing molecular sieve; and carrying out steam-calcination of the iron-containing molecular sieve powder at a temperature of about 650°C to about 750°C for a period of about 20 minutes to about 2 hours in the presence of water vapor.

10 2. The method of claim 1, wherein adding the iron into the molecular sieve comprises a process selected from the group consisting of ion-exchange, impregnation of an iron salt, and mixing a molecular sieve with iron oxide.

15 3. A method of preparing a catalytic article, the method comprising applying to a substrate a catalytic coating comprising a steam-activated iron-containing molecular sieve powder prepared according to claim 1 or claim 2.

4. The method of claim 3, wherein the coated substrate is adapted to achieve greater than 90% NO_x conversion at 250°C under fast SCR conditions without further steam-treatment.

20 5. A selective catalytic reduction article comprising a substrate having a front upstream end and a rear downstream end defining an axial length and having a catalytic coating thereon, where the catalytic coating comprises:

a first coating layer comprising a steam-activated iron-containing molecular sieve; and

25 a second coating layer comprising a copper-containing molecular sieve.

6. The selective catalytic reduction article of claim 5, wherein the catalytic coating is zoned and comprises:

30 a first, upstream zone comprising the first coating layer comprising the steam-activated iron-containing molecular sieve; and

a second, downstream zone comprising the second coating layer comprising the copper-containing molecular sieve.

35 7. The selective catalytic reduction article of claim 5 or claim 6, wherein the substrate is a porous wall-flow filter or a flow-through monolith.

8. The selective catalytic reduction article of any one of claims 5 to 7, wherein one or both of the following conditions apply:

a weight ratio of the steam-activated iron-containing molecular sieve to the copper-containing molecular sieve is about 1:10 to about 10:1;

5 a weight ratio of iron oxide in the steam-activated iron-containing molecular sieve to copper oxide in the copper-containing molecular sieve is about 1:15 to about 15:1.

9. The selective catalytic reduction article of any one of claims 5 to 7, wherein the steam-activated iron-containing molecular sieve includes iron oxide in an amount of about 1 wt% to about 10 15 wt%, based on the total weight of the iron-containing molecular sieve, and the copper-containing molecular sieve includes copper oxide in an amount of about 1 wt% to about 10 wt%, based on the total weight of the copper-containing molecular sieve.

10. The selective catalytic reduction article of any one of claims 5 to 9, wherein one or both 15 of the following conditions apply:

the copper-containing molecular sieve has a Cu/Al atomic ratio of about 0.05 to about 0.55;

the steam-activated iron-containing molecular sieve has a Fe/Al atomic ratio of about 0.05 to about 2.0.

20 11. The selective catalytic reduction article of any one of claims 5 to 10, wherein the first coating layer extends a distance from the front, upstream end of the substrate towards the rear, downstream end of the substrate and overlays a portion of the second coating layer, which extends from the rear, downstream end of the substrate a distance towards the front, upstream end of the substrate.

25

12. The selective catalytic reduction article of any one of claims 5 to 10, wherein the first coating layer extends from the front, upstream end of the substrate to the rear, downstream end of the substrate and overlays an entirety of the second coating layer, which extends from the rear, downstream end of the substrate to the front, upstream end of the substrate.

30

13. The selective catalytic reduction article of any one of claims 5 to 10, wherein the second coating layer extends a distance from the front, upstream end of the substrate towards the rear, downstream end of the substrate and overlays a portion of the first coating layer, which extends a distance from the rear, downstream end of the substrate towards the front, upstream 35 end of the substrate.

14. The selective catalytic reduction article of any one of claims 5 to 10, wherein the second coating layer extends from the front, upstream end of the substrate to the rear, downstream end of the substrate and overlays an entirety of the first coating layer, which extends from the rear, downstream end of the substrate to the front, upstream end of the substrate.

5

15. The selective catalytic reduction article of any one of claims 5 to 10, wherein the first coating layer and the second coating layer are adjacent and do not overlay each other.

16. The selective catalytic reduction article of any one of claims 5 to 10, wherein the first 10 coating layer and the second coating layer are in direct contact with each other.

17. The selective catalytic reduction article of any one of claims 5 to 16, wherein the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are each 8-ring small pore molecular sieves.

15

18. The selective catalytic reduction article of claim 17, wherein the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are both independently zeolites having a structure selected from the group consisting of AEI, AFT, AFX, CHA, EAB, ERI, KFI, LEV, SAS, SAT and SAV.

20

19. The selective catalytic reduction article of claim 17, wherein each of the steam-activated iron-containing molecular sieve and the copper-containing molecular sieve are aluminosilicate zeolites having a CHA crystal structure and a silica to alumina ratio (SAR) of about 5 to about 40.

25

20. The selective catalytic reduction article of claims 6-20, wherein the substrate includes an undercoat comprising an AMOx catalyst in the downstream zone.

21. A selective catalytic reduction system comprising:

30 a first selective catalytic reduction article formed of a first substrate including a first catalytic coating layer comprising a steam-activated iron-containing molecular sieve; and

a second selective catalytic reduction article formed of a second substrate including a second catalytic coating layer comprising a copper-containing molecular sieve:

35 wherein the first selective catalytic reduction article and the second selective catalytic reduction article are in fluid communication.

22. The selective catalytic reduction system of claim 21, wherein:

the first substrate of the first selective catalytic reduction article is zoned according to one of the claims of 5-20; and

the second selective catalytic reduction article formed of a second substrate includes a second catalytic coating layer comprising a copper-containing molecular sieve,

5 wherein the first selective catalytic reduction article and the second selective catalytic reduction article are in fluid communication.

23. The selective catalytic reduction system of claims 21-22, wherein the first substrate and the second substrate are each independently selected from the group consisting of a porous 10 wall-flow filter and a flow-through monolith.

24. The selective catalytic reduction system of any one of claims 21-23, wherein the second substrate includes an undercoat comprising an AMOx catalyst.

15 25. An exhaust gas treatment system comprising:

a selective catalytic reduction article or a selective catalytic reduction system according to any one of claims 5 to 24; and

10 a reductant injector in fluid communication with and upstream of the selective catalytic reduction article or the selective catalytic reduction system.

20

26. The exhaust gas treatment system of claim 25, further comprising one or more of a diesel oxidation catalyst, a soot filter, and an ammonia oxidation catalyst.

25 27. The exhaust gas treatment system of claim 25 or claim 26, further comprising an internal combustion engine in fluid communication with and upstream of the selective catalytic reduction article or the selective catalytic reduction system.

30 28. A method for treating an exhaust stream containing NOx, comprising passing the exhaust stream through a selective catalytic reduction article, a selective catalytic reduction system, or an exhaust gas treatment system of any one of claims 5 to 27.

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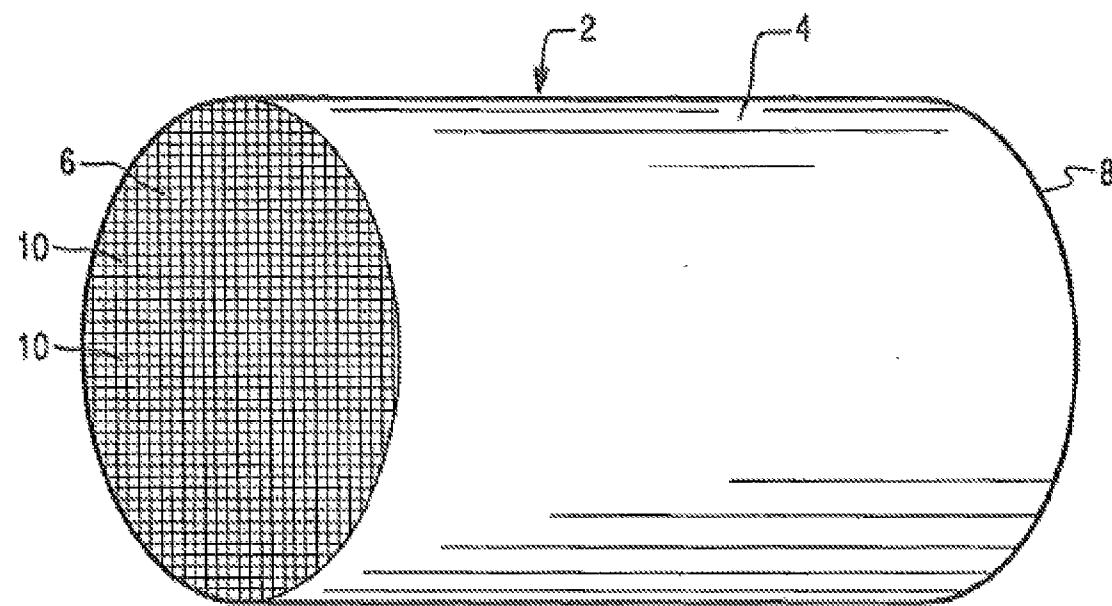


FIG. 1

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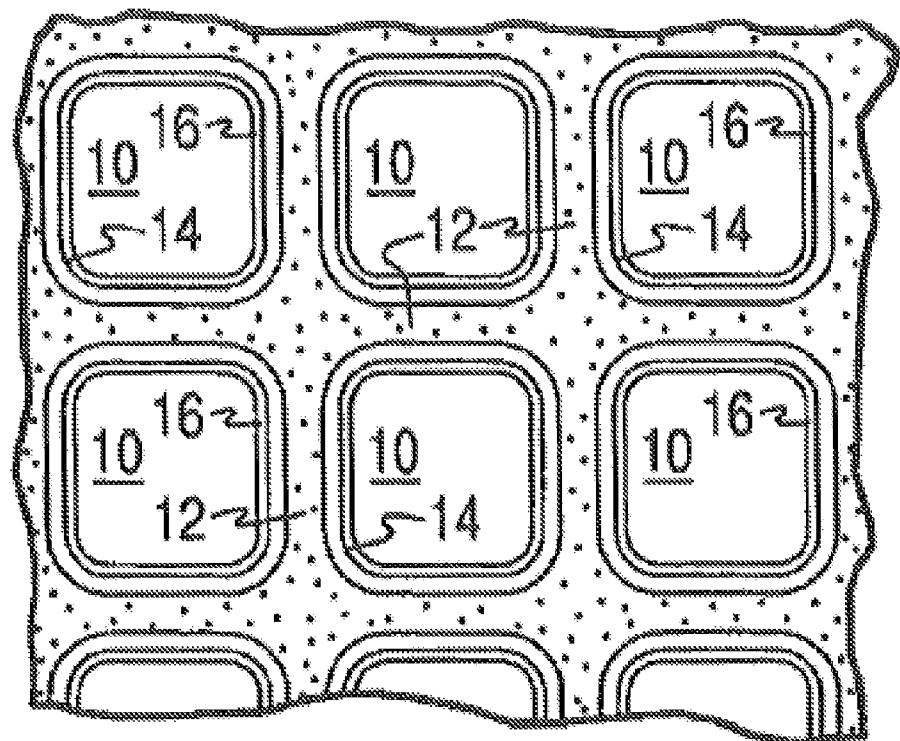


FIG. 2

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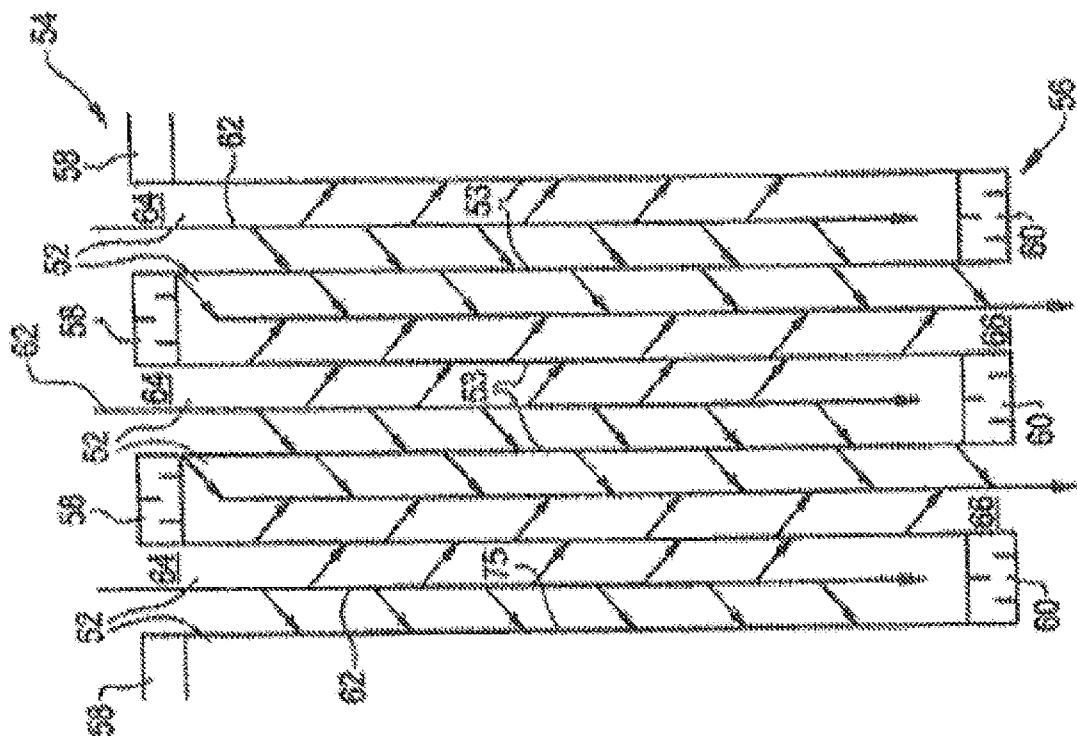


FIG. 3

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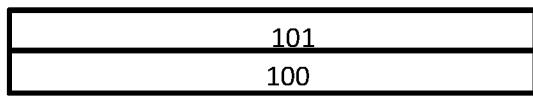


FIG. 4a



FIG. 4f

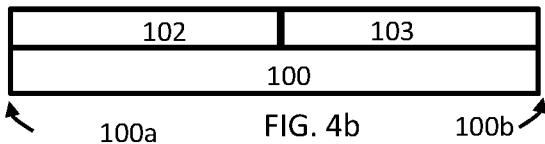


FIG. 4b

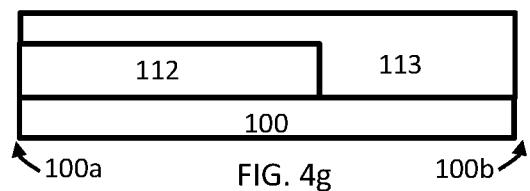


FIG. 4g

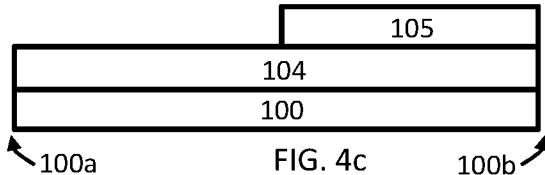


FIG. 4c

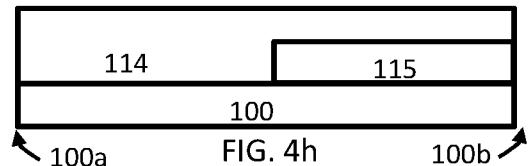


FIG. 4h

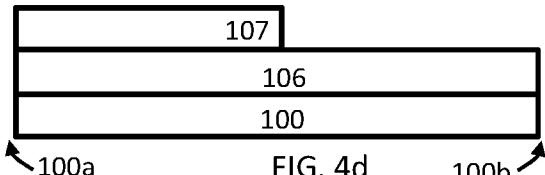


FIG. 4d

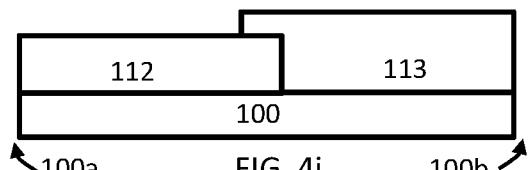


FIG. 4i

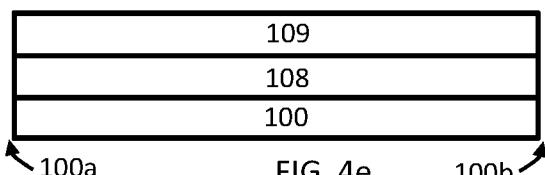


FIG. 4e

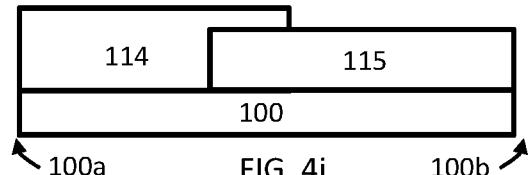


FIG. 4j

INTERNATIONAL SEARCH REPORT

International application No.
PCT/IB2017/054803**A. CLASSIFICATION OF SUBJECT MATTER**

C01B 39/02(2006.01)i, B01J 37/02(2006.01)i, B01J 29/072(2006.01)i, B01J 29/70(2006.01)i, B01J 35/04(2006.01)i, F01N 3/20(2006.01)i

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

C01B 39/02; B01J 29/072; B01D 53/94; C01B 39/06; B01J 29/70; F02B 37/00; B01J 29/68; C01B 39/44; B01J 37/02; B01J 35/04; F01N 3/20

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
Korean utility models and applications for utility models

Japanese utility models and applications for utility models

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
eKOMPASS(KIPO internal) & Keywords: iron, molecular sieve, steam, calcination, SCR, catalyst, copper, NOx conversion

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2004-0120873 A1 (TRAN, PASCALINE H. et al.) 24 June 2004 See paragraph [0009]; examples 1-3 and 7; tables 1 and 2.	1-4
Y		5-7, 21
Y	US 2016-0038878 A1 (JOHNSON MATTHEY PUBLIC LIMITED COMPANY) 11 February 2016 See paragraphs [0006], [0008] and [0038]; claims 1 and 8; figures 1 and 6.	5-7, 21
X	US 2015-0246346 A1 (JOHNSON MATTHEY PUBLIC LIMITED COMPANY) 03 September 2015 See paragraph [0030]; example 1; claims 1 and 17.	1-4
X	US 2015-0246345 A1 (JOHNSON MATTHEY PUBLIC LIMITED COMPANY) 03 September 2015 See abstract; paragraph [0046]; example 1; claims 1-44.	1-4
Y	WO 2016-070090 A1 (BASF CORPORATION) 06 May 2016 See page 3, lines 5-10; claim 1; figure 1.	5-7, 21

 Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier application or patent but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

20 November 2017 (20.11.2017)

Date of mailing of the international search report

20 November 2017 (20.11.2017)

Name and mailing address of the ISA/KR

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INTERNATIONAL SEARCH REPORT

International application No.
PCT/IB2017/054803

Box No. II Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. Claims Nos.: because they relate to subject matter not required to be searched by this Authority, namely:

2. Claims Nos.: 18,19,26 because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
Claims 18, 19 and 26 are not clear because they refer to claim 17 or 25 respectively, which does not comply with PCT Rule 6.4(a).

3. Claims Nos.: 8-17,20,22-25,27,28 because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.

2. As all searchable claims could be searched without effort justifying an additional fees, this Authority did not invite payment of any additional fees.

3. As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:

4. No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.

The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.

No protest accompanied the payment of additional search fees.

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/IB2017/054803

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2004-0120873 A1	24/06/2004	AU 3943002 A CA 2428139 A1 EP 1345691 A2 EP 1495804 A1 JP 2004-536756 A KR 10-2003-0059250 A US 2003-0108467 A1 US 6689709 B1 US 7118722 B2 US 7332148 B2 WO 02-41991 A2	03/06/2002 30/05/2002 24/09/2003 12/01/2005 09/12/2004 07/07/2003 12/06/2003 10/02/2004 10/10/2006 19/02/2008 30/05/2002
US 2016-0038878 A1	11/02/2016	CN 106714940 A DE 102015112465 A1 EP 3177386 A1 GB 2533448 A GB 2533448 B KR 10-2017-0038927 A US 9597636 B2 WO 2016-020806 A1	24/05/2017 11/02/2016 14/06/2017 22/06/2016 28/06/2017 07/04/2017 21/03/2017 11/02/2016
US 2015-0246346 A1	03/09/2015	CN 106029228 A DE 112015001052 T5 EP 3110550 A1 GB 2543165 A JP 2017-510437 A KR 10-2016-0129030 A WO 2015-128663 A1	12/10/2016 08/12/2016 04/01/2017 12/04/2017 13/04/2017 08/11/2016 03/09/2015
US 2015-0246345 A1	03/09/2015	CN 106029227 A DE 112015001008 T5 EP 3110548 A1 GB 2543166 A JP 2017-512630 A KR 10-2016-0127108 A WO 2015-128668 A1	12/10/2016 20/04/2017 04/01/2017 12/04/2017 25/05/2017 02/11/2016 03/09/2015
WO 2016-070090 A1	06/05/2016	CA 2965962 A1 CN 107107044 A EP 3229956 A1 KR 10-2017-0076751 A MX 2017005510 A	06/05/2016 29/08/2017 18/10/2017 04/07/2017 24/07/2017