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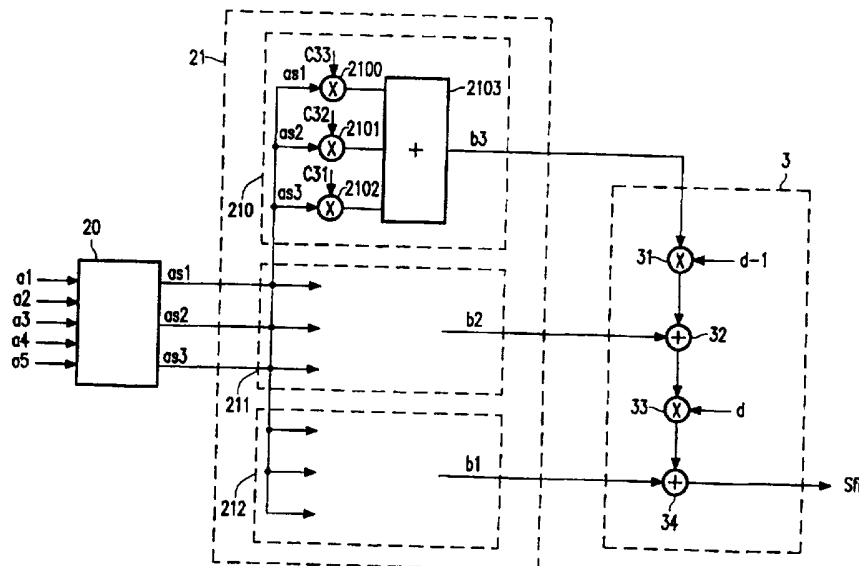
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(54) Title: SPLINE WAVEFORM GENERATION

(57) Abstract

A one-dimensional p -th order spline waveform (C_w) extending along the width or height of a picture device display screen is generated as a chain of sections of p -th order sub-functions (S_{fi}) of a position address (P). If n predetermined values (a_i) are available, $n-p$ p -th order sub-functions (S_{fi}) can be generated each in one of $n-p$ sections (S_i). The invention relates to first selecting $q \geq (p+1)$ selected values (asi) from an array containing the n predetermined values (a_i) and then converting the q selected values (asi) into sub-function coefficients (b_i) determining each of the p -th order sub-functions (S_{fi}). Each of the p -th order sub-functions (S_{fi}) can be written as a linear combination of polynomials of the position address (p) multiplied with associated sub-function coefficients (b_i).

Further, each of the p -th order sub-functions (S_{fi}) can be imagined to be obtained by an addition, in a section (S_i), of portions (pi) of basic functions (F_{bi}) each multiplied by an associated one of the predetermined values (a_i). The basic functions (F_{bi}) are p -th order spline functions. Each of the portions (pi) of the basic functions (F_{bi}) is written as a linear combination of portion coefficients (c_{ij}) corresponding to polynomials of the position address (P). The polynomials range from zero order up to the p -th order. The portion coefficients (c_{ij}) determine the shape of the basic p -th order spline functions (F_{bi}). Each of the sub-function coefficients (b_i) can be calculated from the selected values (asi) by multiplying a matrix comprising the portion coefficients (c_{ij}) with the selected values (asi). The matrix must be a spline matrix to obtain sub-functions (S_{fi}) together composing the spline waveform (C_w). The process of converting the selected values into one of the sub-function coefficients is the same in every section (S_i) since a fixed matrix of portion coefficients (c_{ij}) or multiplication factors is used.



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Spline waveform generation.

The invention relates to a method and a system for generating a one-dimensional spline waveform, the one-dimensional spline waveform being a function of a position on a screen of a display device in one direction, the method comprising the steps of: generating from a position information indicating the position on the screen a position
5 address, the position address indicating a number of a section and a relative position indicating a position within the section for virtually partitioning the screen in sections in the one direction; calculating, in each section, from the relative position and a set of sub-function coefficients a sub-function being a polynomial for obtaining the one-dimensional spline waveform being a chain of consecutive sub-functions in corresponding consecutive
10 sections, and converting, in each section, predetermined values into the sub-function coefficients.

The invention also relates to a method for generating a two-dimensional spline waveform, the two-dimensional spline waveform being dependent on a position in a first and a second direction on a screen of a display device, the display device being scanned
15 in a raster of lines, the first and the second direction being substantially perpendicular.

Such a waveform may be used for correcting deflection errors of a display tube such as convergence errors or east-west distortions. Such a waveform may also be used as a dynamic focusing waveform, or as a waveform influencing the brightness of a displayed picture to compensate for brightness non-uniformity on a display device.

20

It is known that a quadratic spline waveform which extends along the whole width or height of a picture tube screen, and which is a function of a position address, can be generated as a chain of sections of second order sub-functions of the position address. Input coefficients (the predetermined values) are stored in a memory and are referred to as
25 stored values. If n stored values are available, $n-2$ second order sub-functions can be generated each in one of $n-2$ sections. The first second order sub-function is fully determined by 3 of the stored values, and a succeeding second order sub-function in a succeeding section is determined by only one stored value as 2 conditions are already fixed by the demand that the resulting quadratic spline waveform must have a value, and a first derivative which are

continuous in every point, so also at the boundary of the two consecutive sections. This follows from the definition of a p-th order spline function, viz. a function which is, and whose first thru (p-1)-th derivatives are continuous in every point. The quadratic spline waveform is generated as follows:

5 in a first section a first parabola function is calculated at wished positions determined by the position address and by using three of the stored values as parabola coefficients ($f_1(x) = a_0 + a_1 \cdot x + a_2 \cdot x^2$). The stored values are adjustable to obtain a shape of the parabola sections fitting the needed correction on the picture tube screen, in every further section a further parabola is calculated at wished positions determined by the position address
10 using only one stored value not yet used, and by calculating the parabola coefficients out of that one stored value and the two equations determined by the fact that at the border of two succeeding sections the value and the first derivative of the parabola functions in these sections have to be equal. So, two of the parabola coefficients of a succeeding section will depend on coefficients of preceding sections. The calculation of the parabola coefficients
15 from the stored values becomes more and more complex every further section. It is a disadvantage of the known way of generating a quadratic spline waveform that in each section a different program of a computer or different hardware circuits are needed for converting the stored values into parabola coefficients. The most complex calculation in the last section determines the complexity, of the program or the hardware circuits. Further, this
20 complex calculation may need too much time to perform the calculations in real time without storing the sub-function coefficients or intermediate results. A further drawback is that the one extra coefficient used in every section determines the second derivative of the subfunction in this section. The generated quadratic spline waveform will deviate from an intended waveform if this coefficient has been determined slightly wrong. The deviation will
25 influence the generated quadratic spline waveform in all further sections.

It is an object of the invention to calculate a majority of the sub-function coefficients from the predetermined values in a same way in each section.

It is a further object of the invention to convert the predetermined values
30 into the sub-function coefficients without storing the sub-function coefficients for every section.

To this end a first aspect of the invention provides a method for generating a one-dimensional spline waveform as defined in claim 1.

A second aspect of the invention provides a method for generating a two-

dimensional spline waveform as is defined in claim 7.

A third aspect of the invention provides a system for generating a one-dimensional spline waveform as is defined in claim 9.

A fourth aspect of the invention provides a display apparatus comprising a
5 system for generating a one-dimensional spline waveform as is defined in claim 10.

A fifth aspect of the invention provides another method for generating a one-dimensional waveform as is defined in claim 11.

The invention generates a p -th order one-dimensional spline waveform (further referred to as p -th order spline waveform or spline waveform) of the position
10 address. The position address may be a horizontal address representing a horizontal position on the screen of the display device, or a vertical address representing a vertical position on the screen of the display device. The term one-dimensional indicates that the spline waveform depends on only one variable which is either the horizontal or vertical address. The p -th order spline waveform may extend along the whole width or height of the screen and
15 is composed of a chain of sections of p -th order sub-functions of the position address. The position address is partitioned in a section number indicating the number of a section and a relative position indicating the position within a section. If n stored values or predetermined values are available, $n-p$ p -th order sub-functions can be generated each in one of $n-p$ sections. The first p -th order sub-function is fully determined by $p+1$ of the predetermined
20 values. A succeeding p -th order sub-function in a succeeding section is determined by only one predetermined value not yet used as p conditions are already fixed by the demand that the resulting p -th order spline correction waveform must have a value, and a first up to and including $(p-1)$ -th derivative which are continuous in every point, so also at the boundary of two consecutive sections. The invention uses the fact that any p -th order sub-function is fully
25 determined by at least $p+1$ sub-function coefficients. The invention relates to first selecting $q \geq (p+1)$ selected values from an array containing the n predetermined values and then converting the q selected values into sub-function coefficients determining each of the p -th order sub-functions. The conversion is performed such that a p -th order spline waveform is generated. In a first section, a first set of q consecutive selected values which have indices 1
30 to q may be selected from the array of n consecutive predetermined values. In a succeeding second section, a second set of q consecutive predetermined values which have indices 2 to $q+1$ are selected from the n consecutive predetermined values. So, the index of a set of the q selected values is incremented by one in a succeeding section.

It is possible that the selection of the set of q selected values from the n

predetermined values starts with selecting a subset $r < q$ of the n predetermined values which have indices 1 to r , while the $q-r$ selected values which are selected outside the range of n predetermined values (which is the case for indices smaller than 1 or larger than n) get a value zero. These zero values precede the r selected values in the set of q selected values. In
5 the next section $r+1$ selected values correspond to predetermined values which have indices 1 to $r+1$, and only $q-r-1$ selected values will be zero. A same selection outside the array of n predetermined values is possible at the end of the array. In this way it is possible to use an identical conversion of selected values into sub-function coefficients although not a same amount of predetermined values is used in every section. This will become more clear in the
10 description of the Figures.

In the following, the conversion from the selected values into the sub-function values is described.

The invention is based on the insight that it is possible to imagine the p -th
15 order spline waveform extending over the n -p sections to be composed out of a linear addition of basic p -th order spline functions each multiplied by a weighting factor, whereby each weighting factor is one of the n stored values. The basic p -th order spline functions may extend over a few or all sections. A part of the basic p -th order spline function in one section is called a portion or a basic section function.

20 A p -th order sub-function which is the p -th order spline waveform in one of the sections is obtained by an addition of portions of the weighted basic p -th order spline functions in this section. Each of the portions of the basic p -th order spline functions is written as a linear combination of portion coefficients (or multiplication factors) corresponding to polynomials of the position address. The polynomials range from zero order
25 up to the p -th order. The portion coefficients determine the shape of the basic p -th order spline functions, and are determined to obtain a same conversion of stored values into sub-function coefficients in every section for a majority or all of the sub-function coefficients (a few examples are given in the Figures 3 and 6).

The conversion from the stored values into the sub-function coefficients is
30 obtained by calculating the sub-function coefficients out of the added portions of the basic p -th order spline functions, wherein each of the portions is multiplied with an associated one of the stored values. In other words, the addition, in one of the sections, of the portions of the basic p -th order spline functions each multiplied with an associated selected value provides the p -th order sub-function in this section. The p -th order sub-function may be written as

having a zero order polynomial of the position address multiplied with a first sub-function coefficient, added to a first order polynomial multiplied with a second sub-function coefficient, and so on. As a last term a p-th order polynomial of the position address multiplied with a (p+1)th sub-function coefficient is added. Each of the sub-function coefficients is thus a linear combination of the portion coefficients associated with the same polynomial of each of the added portions of the basic p-th order spline functions multiplied by the associated selected values, whereby the portions occurring in a same section are added. Whilst in the above, reference is made to polynomials having a given order also powers of the position address may be used. So, as the sub-function coefficients are determined by linear combinations of the portion coefficients (or multiplication factors) and the selected values, the sub-function coefficients are obtained by multiplying the selected values with a $(p+1)*n$ spline matrix of multiplication factors. The term spline indicates that the multiplication factors are determined to obtain a spline waveform.

As stated earlier, the invention is based on the insight that it is possible to compose the p-th order spline waveform extending over the n-p sections out of a linear addition of basic p-th order spline functions each multiplied by one of the n predetermined values. The fact that the basic functions must be p-th order spline functions causes the succeeding portions of one of the basic functions to have shapes that depend on each other. Thus, portion coefficients of succeeding portions depend on each other. This dependence manifests itself in a specific relation between the multiplication factors of the spline matrix. This relation will become clear from the description of the Figures. Numerous possibilities exists to choose basic functions that are p-th order spline functions. Examples of basic spline functions are shown in Figures 3 and 6.

The spline matrix has to fulfil a further condition to obtain a same conversion in every section for a majority of sub-function coefficients. If the basic p-th order spline functions, as defined above, are copies of each other which each are shifted over one section with respect to each other, the portions which together, in a chain, compose one of the basic p-th order spline functions will repeat in every section as portions of different basic p-th order spline functions. Thus, in every section the same portions of succeeding different basic p-th order spline functions are added, only the weighting factors or stored values differ. This means that the process of converting the stored values into sub-function coefficients is the same in every section: the sub-function coefficients are the same linear combination of different stored values multiplied by chosen portion coefficients. Such a same linear combination gives rise to a fixed matrix of multiplication factors or portion coefficients.

It is advantageous to use a same process in every section for converting the selected stored values into the sub-function coefficients of the p-th order sub-function of the position address to be able to use one algorithm in a suitably programmed computer. If the correction waveform generation is obtained by a circuit which comprises hardware
5 circuits it is advantageous to be able to use the same hardware in every section.

The sub-function coefficients may actually be calculated as claimed in the independent claims 1, 7, 9 and 10. In this case the calculation of a sub-function at positions in a section determined by the position address is performed by multiplying each of the sub-function coefficients with the associated polynomial of the position address and adding the
10 results of the multiplications.

It is also possible to calculate the sub-functions directly from the basic p-th order spline functions which each are multiplied with an associated stored value, as claimed in claim 12. The waveform generation according to the invention needs only a few stored values as the generated correction waveform has an order higher than one.

15 The waveform generated according to the invention may be used directly, for example, to influence the deflection of a picture tube to correct a deflection error which is dependent on a position on the screen in one direction, for example for correcting an east-west error which only depends on the vertical position on the screen. Such a waveform is referred to as a one-dimensional waveform as this waveform depends on only one variable (a
20 horizontal or a vertical position address). Such a one-dimensional waveform may also be used to correct for a non-uniform brightness on a picture tube, for example caused by a varying glass thickness of the picture tube screen. In this case the one-dimensional waveform may be used to obtain a correction voltage influencing the contrast control. In the same way a non uniformity of a brightness of a LCD display due to a non-uniform back-lighting can be
25 corrected. Further would it be possible to generate a one-dimensional waveform which drives a vertical deflection of a picture tube, or which is a correction waveform for obtaining a position dependent scan velocity modulation.

If a deflection error depends on a position on the screen in both directions (horizontal and vertical), as is often the case if a convergence error has to be corrected, in
30 every line a final correction waveform has to be generated which depends on the horizontal and vertical position on the screen. Such a waveform is referred to as a two-dimensional waveform which depends on two variables (the horizontal and vertical position address). It is known to generate such a two dimensional correction waveform according to the expression:

$$W_a(x,y) = a_1.f_1(x,y) + \dots + a_n.f_n(x,y)$$

wherein:

x is a horizontal position on the screen,

y is a vertical position on the screen,

a_i are adjustable stored values, and

5 $f_i(x,y)$ are waveform functions of x and y , for example: x , y , x^2 , $x \cdot y$, $x^2 \cdot y^2$.

Such a known correction waveform generator has to generate complex waveform functions, such as the cross-terms $x^i \cdot y^j$, and is very difficult to adjust to obtain a wished quality of correction.

10 It is a further aspect (see claim 7) of the invention that the two-dimensional correction waveform can be generated, in each line, from calculated coefficients which are derived from a function of the vertical position on the screen, this instead of using the above mentioned adjustable stored values. This function of the vertical position on the screen is the one-dimensional waveform generated according to the first aspect of the
15 invention as described above in relation to claim 1. The final correction waveform becomes simple as the waveform functions only need to depend on the horizontal position, because the calculated coefficients already depend on the vertical position. If a same amount of stored values is used, the quality of the correction according to the invention is improved as the calculated coefficients are generated to be a very smooth (spline) function so that no sharp
20 transitions occur.

An advantageous embodiment of the invention is claimed in claim 2. To obtain optimal freedom in selecting the one dimensional p -th order spline waveform, it should be possible to generate any wished p -th order sub-function in every section. This implies that the basic p -th order spline functions have to be chosen such that the portions
25 added in each segment give rise to a zero order component up to and including the p -th order of the position address. Thus, each of the basic p -th order spline functions is composed out of portions which if they would be added thereby using appropriate weighting factors deliver a zero-th, a first, up to and including a p -th order component of the position address. A sub-function comprises all orders of the position address if all sub-function coefficients are not
30 zero. A consequence of this is that in every row of the spline matrix at least one of the multiplication factors is not zero. Of course the portions of each of the basic p -th order spline functions should be selected such that the composition is a p -th order spline function.

An embodiment of the invention as claimed in claim 3, has the advantage that the conversion from selected values into sub-function coefficients is very simple, as a

minimal number of selected values is used to calculate the sub-function coefficients.

Therefore, each of the basic p -th order spline functions is only non zero during $p+1$ consecutive sections. Thus, in every section only $p+1$ portions of $p+1$ consecutive basic spline functions multiplied with $p+1$ consecutive selected values, respectively, are added.

- 5 The sub-function coefficients of the sub-function obtained in this way are a simple linear combination of only $p+1$ consecutive selected values multiplied with portion coefficients determining the portions of the basic spline function. With $p+1$ portions it is possible to generate any wished p -th order sub-function in every section.

- 10 In a next section, the portions added have the same shape but now are multiplied by $p+1$ consecutive selected values shifted by one with respect to the $p+1$ consecutive selected values in the preceding section. Thus, p consecutive selected values from the preceding section are again used in the succeeding section. This is based, as explained earlier, on the fact that at the border of the two sections the value and all derivatives up to and including the $(p-1)$ th derivative of the sub-functions must be equal to
- 15 obtain a correction waveform which is a p -th order spline function. The above gives rise to a spline matrix which only has $p+1$ rows and $p+1$ columns. The conversion can be performed fast as a simple calculating device is used. It is an advantage if the conversion is fast, because then a more complex high order spline waveform can be generated without a need to calculate and store all $p+1$ sub-function coefficients of each of the $n-p$ p -th order sub-
- 20 functions, before these p -th order sub-functions can be calculated in real time in each section as a function of the stored sub-function coefficients and the position address. It is further advantageous that the conversion is simple to minimise the demands on the calculating device which then becomes cheap.

- 25 An embodiment of the invention as claimed in claim 4, has the advantage that the needed number of stored values is considerably less if quadratic spline functions are used instead of linear functions. On the other hand the implementation of a quadratic spline function is easier than that of a spline having a higher order, such as a cubic spline function, as due to the lower order less multiplications of sub-function coefficients and polynomials of the position address are needed.

- 30 The embodiment of the invention according to claim 5 offers a very simple and inexpensive address generator for generating an address representing the spot position on the screen of the display tube.

It is common practice to generate the position dependent waveform as a function of a variable depending on the time, or depending on a line number. The position

dependent waveform which is generated in this way depends on the amplitude and the frequency of the horizontal or vertical deflection. For example, suppose, the cathode ray tube display arrangement displays a PAL picture which has a vertical amplitude suitable to scan the screen along the whole height. A position dependent waveform depending on time is
5 generated to obtain a certain correction, for example an east-west correction. This waveform has a suitable shape and extends during a vertical scan period over the whole vertical height of the screen. If then the amplitude of the vertical scan is decreased to scan only a part of the height of the screen, the generated position dependent waveform will have the same suitable shape extending during the same vertical scan period but now across only part of the height
10 of the screen. So, the values of the position dependent waveform occur at a wrong position as now the same correction is performed on a smaller part of the screen. At different vertical frequencies (by example: 50Hz PAL, 60Hz NTSC, and 45Hz free running) a different total number of lines appears (as the line frequency does not change significantly) and thus a different position dependent waveform is generated as the lines at different vertical
15 frequencies appear at different positions on the screen. Thus, the position address should be related to the vertical spot position to obtain a position dependent waveform independent of the frequency and amplitude of the vertical deflection. A same reasoning holds for a position waveform depending on the horizontal position on the screen.

The invention provides a position information signal (further referred to as
20 address) generator based on the insight that the spot position on the screen is a linear function in time. The spot position is a linear function in time if the deflection current has a shape for obtaining a linear scan on the picture tube screen. Further, use is made of the fact that a certain deflection current corresponds to a certain position on the picture tube screen. As, in case of a linear scan, the spot position on the screen is a linear function of time, the
25 address generator should generate an address which is a linear function in time. The address generator supplies an address which represents the spot position on the screen if the linear function in time representing the address is coupled to the linear function in time representing the spot position. Thus, the address generator supplies an address which is related to the spot position if two predetermined (wished) addresses occur at two selected levels of the
30 deflection current to which belong two positions on the picture tube screen. The actual value of an address at a certain moment depends on the choice of the predetermined addresses which have to occur at the selected positions on the screen. As the address should be a linear function in time, the address is written as an initial position indication value (further referred to as initial value) added to an incremental value multiplied with the time. The initial value

and the incremental value are determined from two measured moments on which the deflection current reaches the two selected values, respectively, and the values of the above mentioned predetermined addresses.

It is known to obtain a line position indication signal which indicates the vertical spot position on a raster scanned display screen for every line by using an analog to digital converter (further referred to as ADC). The ADC measures a value of the vertical deflection current at a moment a line occurs. The vertical position of the spot and thus of a line on the display screen is determined by the value of the vertical deflection current in this line. So, the ADC supplies a line position indication signal that is a measure of the vertical position of the spot on the screen. If a repetition frequency, or an amplitude of the vertical deflection current changes, still the ADC supplies the actual vertical spot position at the moment a line occurs as the vertical spot position is still determined by the vertical deflection current. The ADC must have a resolution of approximately 13 bits for display systems displaying about 600 lines. A striping would become visible on the screen if a lower resolution would be used. This striping is a brightness modulation caused by different distances between adjacent lines due to inaccuracy in the position of the lines. Such a high resolution ADC is expensive.

An embodiment of an address generator according to the invention as claimed in claim 6 measures the two moments in time at which the two selected levels of the deflection current occur in a simple way by using two comparators, two latches and a counter. Each of the comparators detects whether a corresponding one of the selected levels is reached. The count value of the counter occurring at this moment is stored in a corresponding one of the latches.

These and other aspects will be described and elucidated with reference to the accompanying drawings.

In the drawings:

Figure 1 shows a basic block diagram of a two-dimensional correction waveform generator according to the invention,

Figure 2 shows a basic block diagram of a one-dimensional waveform generator according to the invention,

Figure 3 shows an example of a set of basic functions selected according to the invention,

Figure 4 shows a one-dimensional quadratic spline waveform generated

based on the selected basic functions and predetermined values,

Figure 5 shows a circuit according an embodiment of the invention for calculating sub-functions from the predetermined values,

Figure 6 shows an other example of a set of basic functions selected
5 according the invention,

Figure 7 shows an address generator according to an embodiment of the invention,

Figure 8 shows a waveform of a deflection information being related to a deflection current,

10 Figure 9 shows a waveform representing the address,

Figure 10 shows two graphs representing two vertical deflection currents which have different amplitudes,

Figure 11 shows a picture to elucidate the relation between the vertical deflection current, the vertical position on the screen and the position indication signal with
15 respect to the two vertical deflection currents shown in Figure 10,

Figure 12 shows two graphs representing two vertical deflection currents which have a scan period with a different duration, and

Figure 13 shows a picture to elucidate the relation between the vertical deflection current, the vertical position on the screen and the position indication signal with
20 respect to the vertical deflection currents shown in Figure 12.

Figure 1 shows a basic block diagram of a two-dimensional correction waveform generator according to the invention. The two-dimensional correction waveform generator comprises a position address determining circuit 4 receiving a position information
25 I for supplying a horizontal position address P_h and a vertical address P_v . The position information I is related to a position on a display screen of a display device, for example the position where an electron beam hits a screen of a cathode ray tube CRT under influence of a deflection field. The two-dimensional correction waveform generator further comprises a waveform generator 200 receiving the horizontal position address P_h and calculated
30 coefficients g_i for generating a digital correction waveform W_d in every line. Every one-dimensional waveform generator 100 receives the vertical position information P_v and stored values a_{ij} for generating, in every line, the calculated coefficients g_i depending on the vertical position on the screen. In this way, the digital correction waveform W_d is a linear combination of functions of the horizontal position address P_h each multiplied with a

corresponding calculated coefficient g_i which depends on the vertical position information P_v . The digital correction waveform W_d thus depends on the horizontal and vertical position on the screen.

The digital correction waveform W_d is fed, via a series arrangement of a digital to analog converter 5 and an amplifier 6, as an analog correction waveform W_a to a correction coil L_c for influencing the deflection of the electron beam. The main deflection currents flowing through a horizontal and a vertical deflection coil L_h, L_v are generated from a horizontal and vertical synchronisation information H, V by a deflection circuit 7. A correction current flowing through the correction coil L_c may also be coupled into the main deflection coil L_h or L_v , by example via a injection transformer. Then, the separate correction coil L_c is omitted.

The operation of the waveform generator will be elucidated with an example based on an application in a cathode ray tube (further referred to as CRT) projection television. The invention can also be used in other displays. The projection television comprises three CRT's each emitting one of three primary colours. The CRT's are positioned under an angle to have their respective images overlapping as much as possible for composing a colour picture on a screen. If, without a pre-distorted geometry, each of the CRT's emits a same geometrical figure, these figures will not overlap each other on the screen due to the different angles of the CRT's with respect to the screen. So, the deflection geometry of the CRT's has to be pre-distorted to obtain overlapping or converted pictures on the screen. Two correction waveforms W_a may be generated to correct the geometry in horizontal and vertical direction of the picture generated by the CRT positioned central and representing green. The images on the CRT's representing red and blue have to be pre-distorted by generating appropriate currents through horizontal and vertical convergence coils L_c . Therefore, four two-dimensional correction waveforms W_d have to be generated which are used as reference signals for these currents. For convergence correction of raster scanned CRT's, usually, all the above mentioned correction waveforms W_d are generated in every line and depend on the horizontal and vertical position on the screen and on a number of adjustable predetermined (stored) values a_i .

It was found that the deflection errors occurring in such a projection television can be corrected sufficiently accurate by using seven sets of five stored values a_i . From the seven sets of five stored values a_i is generated a set of seven coefficients g_i in every line. In every line, each of the coefficients g_i out of a set of seven is calculated from every set of five stored values a_i . This calculation is performed by the one-dimensional

waveform generator shown in Figure 2. The one-dimensional waveform generator generates a waveform C_w depending on the vertical position address P_v and a set of five of the stored values a_{ij} , which waveform C_w has in every line a value representing one of the seven coefficients g_i . In this way the seven coefficients g_i are interpolated in every line from the only seven sets of five stored values a_i . The waveform generator 200 calculates, every line from seven coefficients g_i available in this line the digital correction waveform W_d .

Figure 2 shows a basic block diagram of a one-dimensional waveform generator according to the invention. The one-dimensional waveform generator generates a p -th order spline waveform C_w of a position address P . This waveform C_w may be used directly to influence the deflection of a picture tube CRT to correct a deflection error which is dependent on a position on the screen in one direction, for example for correcting an east west error which only depends on the vertical position on the screen. The one-dimensional waveform generator may also generate a waveform C_w which represents the calculated coefficients g_i as used in the two-dimensional waveform generator shown in figure 1. The waveform generator 200 of the two-dimensional correction waveform generator also converts coefficients (the calculated coefficients g_i) into a waveform (the digital correction waveform W_d) which depends on only one position address (the horizontal position address P_h) and thus may also be configured as the one-dimensional waveform generator according to the invention.

The one-dimensional waveform generator comprises a position address determining circuit 40 receiving a position information I related to a position where an electron beam hits a screen of a cathode ray tube CRT under influence of a deflection field, for supplying the position address P . The position address P may be a horizontal or a vertical position address. The waveform C_w , which is a p -th order spline function, may be imagined to be a polynomial having terms of the position address P ranging from a power zero up to p . An associated coefficient is multiplied with every power of the position address P . The coefficients must be selected such that a spline waveform is obtained with a suitable shape, for example for correcting a deflection distortion or for obtaining a dynamic focusing voltage or a correction signal to improve brightness uniformity of a displayed picture on the picture tube screen. The p -th order spline waveform C_w also may be imagined to be composed out of a linear combination of polynomials instead of powers of the position address P .

The invention uses the insight that a p -th order spline waveform C_w extending along the whole width or height of the picture tube screen can be generated as a

chain of sections of p -th order sub-functions S_{fi} of the position address P . Figure 4 shows three sub-functions S_{f1}, S_{f2}, S_{f3} in three section S_1, S_2, S_3 . Each of the p -th order sub-functions S_{fi} comprises a linear combination of polynomials with maximum order p . Each polynomial is multiplied by an associated sub-function coefficient b_i . The shape of the p -th order spline waveform C_w is determined by the sub-function coefficients b_i used in each of the sections. Instead of the polynomials also powers of the position address P may be used. The invention is related to a conversion of a limited amount of predetermined values a_i into the sub-function coefficients b_i in each of the sections S_i . In this case the predetermined values a_i are stored in a memory 1. The stored values a_i are determined such that a correction waveform C_w is obtained which has a shape optimally fitting the use of the correction waveform. The predetermined values a_i are stored in the memory 1 via a data input D. The optimal stored values a_i may be determined by an operator looking at a picture displayed on the screen. If n stored values a_i are available, $n-p$ p -th order sub-functions S_{fi} can be generated, each in one of $n-p$ sections.

In every section S_i , a conversion circuit 2 (Figure 2) converts the stored values a_i into the sub-function coefficients b_i . A calculation circuit 3 calculates a sub-function S_{fi} from the sub-function coefficients b_i and the position address P .

For clarity the operation of the one-dimensional waveform generator is elucidated by way of example, for a situation in which five predetermined or stored values a_i are used and in which the generated one-dimensional spline waveform C_w is a quadratic spline waveform, so $n=5$ and $p=2$.

The one-dimensional quadratic spline waveform C_w can be defined as a function composed of a chain of sub-functions S_{fi} being parabola sections. The parabola sections S_{fi} must fulfil two conditions to obtain a quadratic spline waveform C_w : they must be continuous and continuously differentiable with respect to the position address P at boundaries of the sections S_i . So, there are no jumps or sharp bends in the quadratic spline waveform C_w . The number of sections S_i is two less than the number of stored values a_i . In the first section S_1 any parabola section S_{f1} can be generated by using three of the stored values a_i . In every further section S_j only one stored value a_i is needed to define a further parabola section S_{fj} , as two constraints are imposed on the further parabola section S_{fj} at the boundary between this further parabola section S_{fj} and a preceding parabola section S_{fi} . So, three sections S_1, S_2, S_3 are obtained by using five stored values a_1, a_2, a_3, a_4, a_5 . It is assumed that the width of each of the sections is chosen equal. The invention addresses the conversion, in each of the sections S_i , of the five stored values a_i into parabola coefficients

(or sub-function coefficients) b_i . The conversion is the same in every section for the majority or all sub-function coefficients b_i , and does not need to store intermediate results or any other values than the stored values a_i . Further, a fast and simple conversion is realized to be able to calculate the parabola sections S_{fi} in real time.

5 The invention is based on the insight that it is possible to compose the quadratic spline waveform C_w out of a linear addition of basic functions F_{bi} which are quadratic spline functions each multiplied by one of the stored values a_i . In this case, five basic functions F_{bi} are defined, an example of a set of basic functions F_{bi} is shown in Figure 3.

10 The basic functions F_{bi} are composed out of a chain of basic section functions or portions p_i , each portion p_i extending over one section S_i . Figure 3 only shows the portions p_i occurring in the three sections S_1, S_2, S_3 . The portions may be defined by polynomials having terms of the position address P ranging from a power zero up to 2. With every power of the position address P an associated function coefficient c_{ij} is multiplied. The
15 function coefficients c_{ij} are selected such that a basic function F_{bi} is obtained which is a quadratic spline function. The portions p_i of the basic functions F_{bi} may also be defined to be composed out of a linear combination of polynomials instead of powers of the position address P .

Each of the parabola sections S_{fi} (which are the sub-functions which
20 compose together the quadratic spline waveform C_w) may be imagined to be obtained by the addition of portions p_i of the weighted basic functions F_{bi} in a section S_i . The conversion from the stored values a_i into the parabola coefficients b_i can now be imagined as the process calculating the parabola coefficients b_i out of the added portions p_i of the basic functions F_{bi} in a section S_i , wherein each of the portions p_i is multiplied with an associated stored value
25 a_i . In other words, the addition of the portions p_i of the basic functions F_{bi} each multiplied with a stored value a_i provides a parabola function (the parabola section S_{fi}), which may be written as an addition of a zero order component of the position address P multiplied with a first parabola coefficient b_1 , a first order component of the position address P multiplied with a second parabola coefficient b_2 , and a second order component of the position address
30 P multiplied with a third parabola coefficient b_3 . Each of the parabola coefficients b_i is a linear combination of the function coefficients c_{ij} weighted by the stored values a_i associated with the added portions p_i of the basic functions F_{bi} . It is not essential to the invention that the parabola function is written as is described above, the parabola function may, by example, also be written in polynomial terms, by example as an addition of a zero order

component of the position address P, a first order component, and a multiplication of two different first order components (for example: $b_0 + b_1.P + b_2.P(P-1)$).

The basic functions F_{bi} are copies of each other which are shifted over one section S_i (Figure 3). So, the portions p_i which together compose one of the basic functions F_{bi} will repeat in every section S_i as portions p_i of different basic functions F_{bi} . Thus, in every section S_i always the same portions p_i of the different basic functions F_{bi} are added, only the weighting factors or stored values a_i differ. This means that the process of converting the stored values a_i into parabola coefficients (or sub-function coefficients) b_i is the same in every section S_i : the parabola coefficients b_i are the same linear combination of different stored values a_i in every section S_i . Examples of basic functions which are shifted over one segment are shown in Figure 3 and Figure 6.

Figure 3 shows portions of five basic functions F_{b1} up to F_{b5} in the three available segments S_1, S_2, S_3 . A relative address d runs from zero to one in each of the sections S_i . A first portion p_1 of each of the basic functions is defined by (see the portion p_1 of F_{b4} in segment S_2):

$$p_1(d) = d^2 = d + d.(d-1).$$

A second portion p_2 of each of the basic functions is defined by (see the portion p_2 of F_{b3} in segment S_2):

$$p_2(d) = 1 - 2.d.(d-1).$$

A third portion p_3 of each of the basic functions is defined by (see the portion p_3 of F_{b2} in segment S_2):

$$p_3(d) = (d-1)^2 = 1 - d + d.(d-1).$$

The portions p_i defined above should be looked at as an advantageous example. In case of quadratic spline basic functions F_{bi} a more generic expression of a portion p_i would be

$$p_i(d) = c_{1i} + c_{2i}.d + c_{3i}.d.(d-1).$$

So, the portion p_1 is a special choice wherein the function coefficients c_{ij} are defined as $c_{11}=0$, $c_{21}=1$ and $c_{31}=1$. The other function coefficients are $c_{12}=1$, $c_{22}=0$, $c_{32}=-2$, $c_{13}=1$, $c_{23}=-1$, and $c_{33}=1$. In an other generic expression, powers of the relative position address d are used in a linear combination. In an even more generic expression each of the portions is composed out of a linear combination of polynomials of the relative position address d .

The sub-functions S_{fi} , which are parabola sections in this example, are a linear combination of the portions p_i of the basic functions F_{bi} weighted with an associated

stored value a_i . In the first section S1 the sub-function Sf1 can be written as:

$$Sf1(d, a_i) = a_1.p3(d) + a_2.p2(d) + a_3.p1(d)$$

This can be rewritten as:

$$\begin{aligned} Sf1(d, a_i) &= a_3.c11 + a_2.c12 + a_1.c13 + \\ &\quad (a_3.c21 + a_2.c22 + a_1.c23).d + \\ &\quad (a_3.c31 + a_2.c32 + a_1.c33).d.(d-1) \\ &= b_1 + b_2.d + b_3.d.(d-1) \end{aligned}$$

Thus, each of the parabola coefficients b_i is a linear combination of function coefficients c_i weighted by the stored values a_i associated with the added portions p_i of the basic functions

10 F_{bi} in one segment S_i .

This conversion can be written as:

$$\begin{bmatrix} b1 \\ b2 \\ b3 \end{bmatrix} = \begin{bmatrix} c11 & c12 & c13 \\ c21 & c22 & c23 \\ c31 & c32 & c33 \end{bmatrix} \cdot \begin{bmatrix} a3 \\ a2 \\ a1 \end{bmatrix}$$

15 After substitution of the values of the function coefficients c_{ij} as determined earlier, this expression becomes:

$$\begin{bmatrix} b1 \\ b2 \\ b3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 1 \\ 1 & 0 & -1 \\ 1 & -2 & 1 \end{bmatrix} \cdot \begin{bmatrix} a3 \\ a2 \\ a1 \end{bmatrix}$$

20 which corresponds to:

$$Sf1(d, a_i) = a_1 + a_2 + (-a_1 + a_3).d + (a_1 - 2.a_2 + a_3).d.(d-1)$$

So, with the basic functions F_{bi} selected as shown in Figure 3, in the first section S1, the parabola coefficients b_i are calculated as:

$$\begin{aligned} 25 \quad b_1 &= a_1 + a_2 \\ b_2 &= -a_1 + a_3 \\ b_3 &= a_1 - 2.a_2 + a_3 \end{aligned}$$

In the second section S2 the sub-function Sf2 can be written as:

$$Sf2(d, a_i) = a_2.p3(d) + a_3.p2(d) + a_4.p1(d)$$

30 or, written differently:

$$\begin{pmatrix} b1 \\ b2 \\ b3 \end{pmatrix} = \begin{pmatrix} c11c12c13 \\ c21c22c23 \\ c31c32c33 \end{pmatrix} \cdot \begin{pmatrix} a4 \\ a3 \\ a2 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 1 \\ 1 & 0 & -1 \\ 1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} a4 \\ a3 \\ a2 \end{pmatrix}$$

This is the same expression as found in the first section S1, only the stored values a_i have been linearly shifted. So, if the basic functions Fbi are copies of each other which are shifted over one segment a general expression determining the parabola sections Sfi in each section Si is:

$$\begin{aligned} Sfi(d, a_i) = & c11.as3 + c12.as2 + c13.as1 + \\ & (as3.c21 + as2.c22 + as1.c23).d + \\ & (as3.c31 + as2.c32 + as1.c33).d.(d-1) \end{aligned}$$

10 wherein:

d is the relative position address used within each of the segments Si, and $as1, as2, as3$ is a switched subset of the stored values a_i .

The sub-function coefficients b_{ij} in section Sj can be calculated from the selected values as_i according to:

15

$$\begin{pmatrix} b1j \\ b2j \\ b3j \end{pmatrix} = \begin{pmatrix} c11c12c13 \\ c21c22c23 \\ c31c32c33 \end{pmatrix} \cdot \begin{pmatrix} as3 \\ as2 \\ as1 \end{pmatrix} = \begin{pmatrix} 0 & 1 & 1 \\ 1 & 0 & -1 \\ 1 & -2 & 1 \end{pmatrix} \cdot \begin{pmatrix} as3 \\ as2 \\ as1 \end{pmatrix}$$

The in this way generated quadratic spline waveform Cw can be imagined to be composed out of a linear addition of the basic functions Fbi each multiplied by one of the stored values a_i :

20

$$Cw(P) = a1.Fb1(P) + a2.Fb2(P) + a3.Fb3(P) + a4.Fb4(P) + a5.Fb5(P),$$

wherein P is an absolute address, ranging from zero at a start of the first section S1 to a maximum value at an end of the third section S3. A quadratic spline correction waveform Cw obtained if $a1=-1$, $a2=2$, $a3=-2$, $a4=-3$, and $a5=1$ is shown in Figure 4.

25

In each of the sections Si only three stored values a_i contribute in the parabola coefficients b_i , as the basic functions Fbi used in this example are only non-zero in three consecutive sections Si.

The shape of each of the portions p_i which are associated with a certain stored value a_i can be found as the difference between a first one-dimensional waveform generated with a first set of stored values a_i and a second one-dimensional waveform

30

generated with a second set of stored values a_i wherein only this certain stored value a_i differs with respect to the first set of stored values a_i . The same holds for a chain of portions p_i associated with a certain coefficient.

The known quadratic spline waveform generator calculates the sub-
5 functions S_{fi} by using the expression:

$$S_{fi}(p) = b_{1i} + b_{2i}.p + b_{3i}.p^2$$

wherein, for simplicity, p is introduced to be a relative address running from 0 to 1 in each section S_i .

In a first section S_1 , the sub-function coefficients b_i are chosen to be the first three stored
10 values a_i :

$$b_{11} = a_1, b_{21} = a_2, b_{31} = a_3$$

This substituted in the sub-function expression delivers:

$$S_{f1}(p) = a_1 + a_2.p + a_3.p^2$$

the first derivative is:

$$15 \quad dS_{f1}(p) = a_2 + 2.a_3.p$$

In a second section S_2 , the sub-function S_{f2} and its derivative dS_{f2} are determined by:

$$S_{f2}(p) = b_{12} + b_{22}.p + b_{32}.p^2$$

$$dS_{f2}(p) = b_{22} + 2.b_{32}.p$$

As the total waveform is a quadratic spline function, the sub-function coefficients b_i of the
20 sub-function S_{f2} in the second section S_2 are calculated from the expressions:

$$S_{f2}(0) = b_{12} = S_{f1}(1) = a_1 + a_2 + a_3$$

$$dS_{f2}(0) = b_{22} = dS_{f1}(1) = a_2 + 2.a_3$$

the sub-function coefficient b_i belonging to the p^2 term is chosen to be a new stored value a_i :

$$b_{32} = a_4.$$

25 In a third section S_3 , the sub-function S_{f3} and its derivative dS_{f3} are determined by:

$$S_{f3}(p) = b_{13} + b_{23}.p + b_{33}.p^2$$

$$dS_{f3}(p) = b_{23} + 2.b_{33}.p$$

As the total waveform is a quadratic spline function, the sub-function coefficients b_i of the
sub-function S_{f3} in the third section S_3 are calculated from the expressions:

$$30 \quad S_{f3}(0) = b_{13} = S_{f2}(1) = b_{12} + b_{22} + b_{32} = a_1 + a_2 + a_3 + a_2 + 2.a_3 + a_4$$

$$dS_{f3}(0) = b_{23} = dS_{f2}(1) = b_{22} + 2.b_{32} = a_2 + 2.a_3 + 2.a_4$$

the sub-function coefficient b_i belonging to the p^2 term is chosen to be a new stored value a_i :

$$b_{33} = a_5.$$

The above shows clearly that the conversion process of calculating the

sub-function coefficients b_i from stored values a_i becomes more complex in every further section S_i . This conversion process is thus not the same in every section S_i for a majority or all of the sub-function coefficients b_i . It can also be seen that, in a section S_i , the sub-function coefficient b_i associated to the zero order term of the relative position d depends on sub-function coefficients b_i of all preceding sections S_i .

The parabola sections S_{fi} according to the invention can be calculated in real time from the stored values a_i as the calculation of the parabola coefficients b_i is very simple. Such a simple calculation can be performed fast enough to avoid that first all parabola coefficients b_i have to be calculated and stored before the parabola sections S_{fi} can be calculated in real time.

Figure 6 shows another example of five basic functions $Fb1$ up to $Fb5$ in the three available segments $S1, S2, S3$. A first portion $p1$ of each of the basic functions is defined by (see the portion $p1$ of $Fb3$ in segment $S1$):

$$p1(d) = d^2$$

A second portion $p2$ of each of the basic functions Fb_i is defined by (see the portion $p2$ of $Fb2$ in segment $S1$):

$$p2(d) = 1 + 2 \cdot d - d^2$$

A third portion $p3$ of each of the basic functions is defined by (see the portion $p3$ of $Fb1$ in segment $S1$):

$$p3(d) = 2$$

Wherein the position address d again is a relative address running from zero to one within each of the segments S_i .

In a same way as described above for the basic functions Fb_i shown in Figure 3, the conversion from the stored values a_i into the sub-function coefficients b_i can be calculated to be, in the first segment $S1$:

$$b11 = 2 \cdot a1 + a2$$

$$b21 = 2 \cdot a2$$

$$b31 = -a2 + a3$$

in the second segment $S2$:

$$b12 = 2 \cdot a1 + 2 \cdot a2 + a3$$

$$b22 = 2 \cdot a3$$

$$b32 = -a3 + a4$$

in the third segment S3:

$$b_{13} = 2.a_1 + 2.a_2 + 2.a_3 + a_4$$

$$b_{23} = 2.a_4$$

$$b_{33} = -a_4 + a_5$$

5 wherein the sub-functions S_{fi} are written as:

$$S_{fi}(p) = b_{1i} + b_{2i}.p + b_{3i}.p^2$$

The first sub-function coefficient b_1 is not the same linear combination in every section S_i , as the basic functions F_{bi} are non zero in more than three succeeding sections S_i . The sub-function coefficients b_2 and b_3 are the same in each section, only the
10 associated stored values a_i differ. Again, the sub-function coefficients b_i can be calculated from the stored values a_i in a very simple way.

In this situation, it is possible to use a same conversion in every section S_i by adapting the selection of selected values a_{si} from the stored values a_i as described below. In every section S_i , five selected values a_{si} are selected from the array of five stored values
15 a_i . In the first section S_1 the first two selected values a_{s1}, a_{s2} are selected outside the array of stored values. The selected values a_{si} selected outside the array are chosen to be zero. The next three selected values a_{s3}, a_{s4}, a_{s5} are selected to be the consecutive stored values a_1, a_2, a_3 , respectively. In the second section the indices of the stored values are incremented by one: the four selected values $a_{s2}, a_{s3}, a_{s4}, a_{s5}$ are selected to be a_1, a_2, a_3, a_4 , respectively,
20 and only the first selected value a_{s1} is selected outside the array and thus will be zero. In the third segment all selected values a_{si} are selected within the array and thus are equal to the stored values with a same index. So, if a new array is imagined which comprises the consecutive elements $0, 0, a_1, a_2, a_3, a_4, a_5$, the selection of the selected values a_{si} can be imagined to select five consecutive elements starting in the first section S_1 with the first five
25 elements $(0, 0, a_1, a_2, a_3)$, and succeeding in the second section S_2 with selecting five consecutive elements with indices one higher $(0, a_1, a_2, a_3, a_4)$, and so on. The process of converting, for a sub-function S_{fi} in section S_i , the stored (or predetermined) values a_i into the sub-function coefficients b_i can be described by the next expression:

$$S_{fi}(p) = 2.a_{s1} + 2.a_{s2} + 2.a_{s3} + a_{s4} + 2.a_{s4}.d + (-a_{s4} + a_{s5}).d^2$$

30 and by selecting the selected values a_{si} as described before.

In the first section S_1 is obtained:

$$S_{f1}(p) = 2.0 + 2.0 + 2.a_1 + a_2 + 2.a_2.d + (-a_2 + a_3).d^2$$

In the second section S_2 is obtained:

$$S_{f2}(p) = 2.0 + 2.a_1 + 2.a_2 + a_3 + 2.a_3.d + (-a_3 + a_4).d^2$$

And in the third section S2 is obtained:

$$Sf_3(p) = 2.a_1 + 2.a_2 + 2.a_2 + a_4 + 2.a_4.d + (-a_4 + a_5).d^2$$

In this way, even if basic functions F_{bi} are used which comprise a number of consecutive portions p_i which are non zero, whereby the number is higher than $p+1$ it is possible to use

5 the same program in a computer or the same hardware to convert the predetermined values a_i into the sub-function coefficients b_i .

Figure 5 shows a circuit according to an embodiment of the invention for calculating each of the sub-functions Sf_i from the stored values a_i in each of the sections S_i .

10 This embodiment is based on the example of basic functions F_{bi} as shown in Figure 3.

A selection circuit 20 receives the five stored values a_i for supplying a selection of three stored values a_{si} to a conversion circuit 21. In the first section S1 the selected stored values a_{s1}, a_{s2}, a_{s3} are a_1, a_2, a_3 respectively. In the second section S2 the selected stored values a_{s1}, a_{s2}, a_{s3} are a_2, a_3, a_4 respectively. In the third section S3 the
15 selected stored values a_{s1}, a_{s2}, a_{s3} are a_3, a_4, a_5 respectively.

In this example, the conversion circuit 21 comprises three sub conversion circuits 210, 211, 212 which each convert the three selected stored values a_{si} into one of the three parabola or sub-function coefficients b_i . The first sub conversion circuit 210 comprises a first, second and third multiplier 2100, 2101, 2102 and an adder 2103. The first multiplier
20 2100 receives the first selected stored value a_{s1} and an associated function coefficient c_{33} (which is 1 in the above described example), for generating a first output value which is a multiplication of the selected stored value a_{s1} with the associated function coefficient c_{33} (the function coefficients c_{ij} are determined by the choice of the basic functions F_{bi}). The second multiplier 2101 receives the second selected stored value a_{s2} and an associated
25 function coefficient c_{32} (which is 1 in the above described example), for generating a second output value which is a multiplication of the selected stored value a_{s2} with the associated function coefficient c_{32} . The third multiplier 2102 receives the third selected stored value a_{s3} and an associated function coefficient c_{31} (which is 0 in the above described example), for generating a third output value which is a multiplication of the selected stored value a_{s3} with
30 the associated function coefficient c_{31} . The adder 2103 receives the first, second and third output values to supply the first sub-function coefficient b_3 which is the sum of the first, second and third output values. In a same way, the second and third sub conversion circuits 211, 212 convert the three selected stored values a_{s1}, a_{s2}, a_{s3} into the second and third sub-function coefficients b_2, b_1 . The second and third sub conversion circuits 211, 212 have the

same topology as the first sub conversion circuit 210, only different function coefficients c_{ij} are used. Instead of multipliers 2100,2101,2102 also bit shifters can be used, as the function coefficients c_{ij} are very simple.

The calculation circuit 3 comprises: a first multiplier 31 for multiplying
 5 the first parabola coefficient b_3 with a function of the position address being $d-1$, a first adder 32 for adding a second parabola coefficient b_2 to the result obtained by the first multiplier 31, a second multiplier 33 for multiplying the result of the first addition with the relative position address d , and a second adder 34 for adding a third parabola coefficient b_1 to the result of the second multiplier 33. The second adder 34 supplies the parabola sections
 10 S_{fi} which together compose the quadratic spline waveform C_w . It is possible to use another first order polynomial than the function $d-1$ of the relative position address d to be multiplied with the first parabola coefficient b_3 . It is also possible to use one hardware multiplier instead of the first and the second multiplier 31,34, but then an intermediate result has to be stored. It is further possible to replace a part of or the complete circuit by a suitably
 15 programmed computer.

Although the above used example is limited to the generation of a quadratic spline waveform C_w from five stored values a_i , it is obvious for the man skilled in the art how to generate a higher order spline waveform C_w , or a spline waveform using a different amount of stored values a_i . Still the same conversion circuit can be used in every
 20 section S_i to convert the selected stored values a_{si} into the sub-function coefficients b_i if more stored values a_i are available to generate a spline waveform C_w which has the same order. If a higher order spline waveform C_w is generated, lets assume a p -th order, next adaptations have to be made: a) the calculation circuit 3 has to generate sub-functions S_{fi} having the p -th order, b) the conversion circuit 21 has to generate $p+1$ sub-function
 25 coefficients b_i for determining the p -th order sub-functions S_{fi} , c) each of the sub-function coefficients b_i has to be calculated as a linear combination of function coefficients c_{ij} weighted with selected stored values a_{si} . The number of selected stored values a_{si} depends on the freedom of choice wanted in generating the waveform C_w . This number should be at least $p+1$ if full freedom is wanted (all p -th order sub-functions can have all shapes possible, as
 30 long as the resulting waveform C_w is a p -th order spline function). The function coefficients c_{ij} depend on a choice of the basic functions, as explained above.

Figure 1 shows a cathode ray display apparatus with a position indication signal (or address) generator 4 according to the invention, which will be described below.

Figure 8 and 9 show waveforms elucidating the operation of the address generator 4. Figure 8 shows a waveform of a position information I being related to a deflection current Ih;Iv. The deflection current Ih;Iv may be the vertical Iv or horizontal Ih deflection current.

- 5 The address generator 4 has to supply an address A (uptill now referred as P) which is a linear function in time, as is shown in Figure 9:

$$A(t) = A0 + dA.t$$

wherein A0 is an initial value and dA an incremental value.

- 10 The address A is related to the spot position if two wished addresses A1,A2 occur at two selected levels of the deflection current Ih;Iv. This holds if the deflection current Ih;Iv has a shape for obtaining a substantially linear scan on the screen of the cathode ray tube CRT. Under this condition the spot position on the screen is a substantially linear function of time.

- 15 Two positions on the screen belong to two selected levels of the deflection current Ih;Iv. These two selected levels of the deflection current are represented by two levels I1,I2 of the position information I, see Figure 8. These two levels I1,I2 occur at two moments T1,T2, respectively. The address A is generated to obtain the two wished addresses A1,A2 at the two moments T1,T2, respectively. This will be further elucidated below.

- 20 An address generator 4 according to the invention is shown in Figure 7. This address generator 4 comprises a first and a second comparator 40,41 both receiving a position information I which is related to the deflection current and reference levels indicating the two levels I1,I2 for supplying a first and second comparator signal Cs1, Cs2, respectively, to a first and a second latch 42,43. The position information I may, for example, be obtained (not shown) in a known manner from the deflection current Ih;Iv via a current transformer, or a resistor through which the deflection current flows, or, if the deflection current Ih;Iv is generated by a power amplifier in a feedback loop, by a reference waveform to which the deflection current Ih;Iv is compared. Instead of the latches 42,43 any other storage circuit may be used.

- 25 A counter 44 receives a reset signal R occurring during a flyback period, and a clock signal Clk which is summed during the trace period to obtain a count value C which is supplied to a further input of both the first and second latch 42,43. A first calculation unit 45 receives an output value O1 from the first latch 42, and an output value O2 from the second latch 43, to calculate the initial value A0 and the incremental value dA. The first calculation unit 45 receives a start information S indicating that new initial and incremental values A0,dA have to be calculated. The start informations may be related to the

second moment T2 as after this second moment T2 all necessary information for the calculation is available. The start information may also be the reset signal R. A second calculation unit 46 calculates the address A to supply the address A according to the expression:

$$5 \quad A(t) = A0 + dA \cdot t.$$

The second calculation unit 46 receives the reset signal R indicating that the new initial and incremental values A0,dA calculated by the first calculation unit 45 have to be used to calculate the address A in a next field or line. It is possible to combine the first and second calculation units 45,46 in one calculation unit.

- 10 If the address A represents a vertical position of horizontal scanned lines the above expression may be written as:

$$\begin{aligned} i &= \text{line} \\ A(\text{line}) &= A0 + \sum_{i=1} dA \end{aligned}$$

- 15 wherein the address A is calculated to be the initial value A0 to which is added in every line the incremental value dA. In this case, the second calculation unit 46 only needs to perform additions in every line instead of multiplying the incremental value dA with the time t.

The first and second comparator signals Cs1,Cs2 indicate two moments in time T1,T2 (Figure 8) at which two selected levels I1,I2 of the position information I occur

- 20 which correspond to the two selected levels of the deflection current Ih;Iv. A first count value C1 generated by the counter 44 is stored by the first latch 42 at the moment T1 that the first comparator signal Cs1 indicates that the position information I has the first selected value I1. The second latch stores in the same way a second count value C2 at the moment that the second comparator 41 indicates that the position information I has the second wished value I2. The clock signal CLK needs to have a sufficient high repetition rate to be able to obtain sufficiently accurate count values C1 and C2. The first calculating unit 45 calculates the initial value A0 and the incremental value dA from the first and second stored values C1,C2 knowing that these values represent the time moments T1,T2 at which the wished address values A1 and A2 should occur, respectively. The initial value A0 and the
- 25
- 30 incremental value dA are defined by the formulae:

$$\begin{aligned} A0 &= (T1 \cdot A2 - T2 \cdot A1) / (T1 - T2) \\ dA &= (A1 - A2) / (T1 - T2) \end{aligned}$$

These formulae follow from a simple substitution of the measured moments T1,T2 and the wished address values A1,A2 occurring at these moments in the linear function representing

the address A. So, an address generator is realised for calculating with the second calculation unit 46 an address A from the initial value A0 and the incremental value dA in such a way that at the moment the first comparator 40 detects a first selected level of the deflection current, the address A is equal to the first wished address value A1, and that at the moment
5 the second comparator 41 detects a second selected level of the deflection current, the address A is equal to the second wished address value A2. The selected values of the deflection current Ih;Iv have to be selected such that in every display mode (by example a vertical compress mode to display pictures having a 16:9 aspect ration on a picture tube having a 4:3 aspect ratio) the deflection current Ih;Iv covers these values. Preferably, the
10 selected values of the deflection current Ih;Iv are selected as far away as possible from each other to obtain a maximal accuracy. In case the position address A represents the vertical position on the screen, in the way described above, it is possible to obtain an address A which for every horizontal line represents the vertical spot position on the screen, independent on the deflection amplitude or frequency. This will be further elucidated in the
15 description of Figures 10, 11, 12 and 13.

The address A in a certain line may be generated by adding the incremental value dA to the address A of a line preceding the certain line. This addition can be performed with a suitably programmed computer or with the second calculating unit 46 adapted to be a hardware adder. Also the counter 44, the first and second latches 42,43 and
20 the first calculating unit 45 may be replaced by a suitably programmed computer.

An offset value has to be added to the initial value A0 depending on the field if a picture is composed by interlaced fields.

The address generator 4 according to the invention also supplies an address A which is independent on the deflection amplitude or frequency if the deflection
25 current has a shape for obtaining only an approximate linear scan on the screen instead of a substantial linear scan. This is based on the insight that the absolute accuracy is not very important as a small difference between the actual spot position and the address A (a few lines if the address A is the vertical address) still produces an acceptable waveform. This difference causes a fixed error which will be compensated for by adjusting the shape of the
30 waveform. In case the waveform generator is used to generate convergence waveforms, the differential accuracy of a vertical address from field to field is also not very critical, the difference should be below about one eighth of a distance between two consecutive lines to obtain a good interlace. The differential accuracy (in case of a vertical address: from line to line) must be very high, otherwise striping occurs. As the address A is a linear function this

only imposes a condition on the number of bits used to represent the address, this number must be high enough (about 14 bits in the vertical direction) to avoid striping. It is especially this high demand on differential accuracy that makes the known ADC expensive.

5 Figure 10 shows two graphs representing two vertical deflection currents I_{v1}, I_{v2} which have different amplitudes during a scan period with a duration T_s . A first vertical deflection current I_{v1} starts at moment 0 with a start current value I_{s1} , and ends at the moment T_s with an end current value I_{e1} . A second vertical deflection current I_{v2} starts at moment 0 with a start current value $I_{s2} \leq I_{s1}$, and ends at moment T_s with an end current value $I_{e2} \leq I_{e1}$. As an example both vertical deflection currents I_{v1}, I_{v2} are S-corrected sawtooth waveforms which cause an approximately linear vertical scan on the cathode ray tube screen. The first and second vertical deflection current I_{v1}, I_{v2} reach a first predetermined value I_1 at moments T_1 and T_1' respectively. The first and second vertical deflection current I_{v1}, I_{v2} reach a second predetermined value I_2 at moments T_2 and T_2' respectively.

Figure 11 shows a picture to elucidate the relation between the vertical deflection current I_v , the vertical position on the screen and the position indication A with respect to the vertical deflection currents I_{v1}, I_{v2} shown in Figure 10. The dashed line 3 represents a cathode ray tube screen with an aspect ratio of 4:3. The line positioned left from the screen 3 indicates values of the vertical deflection current I_v . At this line are indicated: the start current I_{s1} and end current I_{e1} related to the first vertical deflection current I_{v1} as shown in Figure 4; the start current I_{s2} and end current I_{e2} related to the second vertical deflection current I_{v2} ; and the first and second predetermined vertical deflection current values I_1, I_2 . With a certain value of the vertical deflection current I_v corresponds in a one to one relation a certain vertical position on the screen 3. The first line Sc_1 indicates the scanned part of the screen 3 belonging to the first vertical deflection current I_{v1} . The first line Sc_1 starts at the vertical position Ps_1 corresponding to the start current I_{s1} and ends at the vertical position Pe_1 corresponding to the end current I_{e1} . In this example the first vertical deflection current I_{v1} is chosen to obtain a vertical scan larger than the height of the screen 3. The second line Sc_2 indicates the scanned part of the screen 3 belonging to the second vertical deflection current I_{v2} . The second line Sc_2 starts at the vertical position Ps_2 corresponding to the start current I_{s2} and ends at the vertical position Pe_2 corresponding to the end current I_{e2} . In this example the second vertical deflection current I_{v2} is chosen to

obtain a vertical scan smaller than the height of the screen 3, for example for displaying a display information with an aspect ratio of 16:9.

The predetermined vertical deflection current values I1, I2 correspond to the vertical positions P1 and P2, respectively. The references T1, T1' associated with the vertical position P1 denote the moments at which the first and the second vertical deflection current Iv1, Iv2 reaches the first predetermined value I1, respectively (see also Figure 4). The references T2, T2' denote the moments at which the first and the second vertical deflection current Iv1, Iv2 reaches the second predetermined value I2, respectively.

The line positioned right from the screen 3 indicates values of the vertical spot position indication signal or the vertical address Av according to the invention in relation to the vertical position on the screen 3.

The vertical address Av generated in response to the first vertical deflection current Iv1 follows from the two equations:

$$Av(T1) = A0 + dA \cdot T1 = A1$$

$$Av(T2) = A0 + dA \cdot T2 = A2$$

Due to the first equation it is ensured that at moment T1 at which the vertical current Iv has the first predetermined value I1 a vertical address Av is generated equal to a chosen value A1. Due to the second equation it is ensured that at moment T2 at which the vertical current Iv has the second predetermined value I2 a vertical address Av is generated equal to a chosen value A2.

From this two equations the initial and incremental values A0, dA can be calculated, the calculated values substituted in the linear function representing the vertical address Av gives:

$$Av(t) = (A1 \cdot T2 - A2 \cdot T1) / (T2 - T1) + t \cdot (A2 - A1) / (T2 - T1)$$

wherein $Av(T1) = A1$ and $Av(T2) = A2$.

So, the vertical address Av(t) depends on a choice of the first and second address values A1, A2.

As the first vertical deflection current Iv1 has a shape to obtain a linear vertical scan it is sufficient to lock the vertical address Av on two positions P1, P2 to the screen. All other positions on the screen will then be locked to the vertical address Av as the vertical address Av is a linear function in time. This means that the start value A0=0 corresponds to the vertical position Ps1 and that the end value As corresponds to the vertical position Pe1.

In the following is elucidated that the vertical address Av generated as

described above supplies the same address values at the same vertical positions if the amplitude of the vertical deflection current is changed.

The vertical address A_v generated in response to the second vertical deflection current I_{v2} follows from the two equations:

$$A_v(T1') = A0 + dA.T1' = A1$$

$$A_v(T2') = A0 + dA.T2' = A2$$

Due to the first equation it is ensured that at moment $T1'$ at which the vertical current I_v has the first predetermined value $I1$ a vertical address A_v is generated equal to a chosen value $A1$. Due to the second equation it is ensured that at moment $T2'$ at which the vertical current I_v has the second predetermined value $I2$ a vertical address A_v is generated equal to a chosen value $A2$.

From these two equations the initial and incremental values $A0$, dA can be calculated, the calculated values substituted in the linear function representing the vertical address A_v gives:

$$A_v(t) = (A1.T2' - A2.T1') / (T2' - T1') + t . (A2 - A1) / (T2' - T1')$$

$$\text{wherein } A_v(T1') = A1 \text{ and } A_v(T2') = A2.$$

Thus, the vertical address A_v has the same first address value $A1$ at the first vertical position $P1$ at which the vertical current has the first predetermined value $I1$. And, the vertical address A_v has the same second address value $A2$ at the first vertical position $P2$ at which the vertical current has the second predetermined value $I2$. As also the second vertical deflection current I_{v2} has a shape to obtain a linear vertical scan it is sufficient to lock the vertical address A_v on two positions $P1, P2$ to the screen. All other positions on the screen will than be locked to the vertical address A_v as the vertical address A_v is a linear function in time. So, the vertical address generator 4 generates a vertical address A_v which has the same values at same positions on the screen 3 although the amplitude of the vertical deflection current I_v has been changed.

Figure 12 shows a first and a second vertical deflection current I_{v1}, I_{v2} which have a scan period with a different duration $Ts1, Ts2$, respectively. The first and second deflection current I_{v1}, I_{v2} have the same amplitude. The first deflection current I_{v1} starts at moment 0 with a start current value I_s , and ends at the moment $Ts1$ with an end current value I_e . The second deflection current I_{v2} starts at moment 0 with the same start current value I_s , and ends at the moment $Ts2$ with the same end current value I_e . As an example both vertical deflection currents I_{v1}, I_{v2} are S-corrected sawtooth waveforms which

cause an approximate linear vertical scan on the cathode ray tube screen. The first and second vertical deflection current I_{v1}, I_{v2} reach a first predetermined value I_1 at moments T_1 and T_1' respectively. The first and second vertical deflection current I_{v1}, I_{v2} reach a second predetermined value I_2 at moments T_2 and T_2' respectively.

5

Figure 13 shows a picture to elucidate the relation between the vertical deflection current I_v , the vertical position on the screen and the position indication A with respect to the vertical deflection currents I_{v1}, I_{v2} shown in Figure 12. The dashed line 3 represents a cathode ray tube screen with an aspect ratio of 4:3. The line positioned left from the screen 3 indicates values of the vertical deflection current I_v . At this line are indicated: the start current I_s , the end current I_e , and the first and second predetermined vertical deflection current values I_1, I_2 . With a certain value of the vertical deflection current I_v corresponds in a one to one relation a certain vertical position on the screen 3. The first line Sc_1 indicates the scanned part of the screen 3 belonging to the first vertical deflection current I_{v1} . The second line Sc_2 indicates the scanned part of the screen 3 belonging to the second vertical deflection current I_{v2} . The first and second lines Sc_1, Sc_2 both start at the vertical position P_s corresponding to the start current I_s and both end at the vertical position P_e corresponding to the end current I_e .

The vertical address A_v generated in response to the first vertical deflection current I_{v1} follows from the two equations:

$$A_v(T_1) = A_0 + dA \cdot T_1 = A_1$$

$$A_v(T_2) = A_0 + dA \cdot T_2 = A_2$$

Again, the first and second predetermined vertical deflection current values I_1, I_2 occurring at the moments T_1, T_2 , respectively are locked to a first and a second predetermined vertical address value A_1, A_2 , respectively. All other vertical address values are locked to a vertical position, as the vertical address A_v is a linear function of time and the shape of the first vertical deflection current I_{v1} causes a linear vertical scan.

The vertical address A_v generated in response to the second vertical deflection current I_{v2} follows from the two equations:

$$A_v(T_1') = A_0 + dA \cdot T_1' = A_1$$

$$A_v(T_2') = A_0 + dA \cdot T_2' = A_2$$

Now, the first and second predetermined vertical deflection current values I_1, I_2 occurring at the moments T_1', T_2' , respectively are locked to the first and a second predetermined vertical address value A_1, A_2 , respectively. Again, all other vertical address values A_v are locked to

a vertical position, as the vertical address A_v is linear function of time and the shape of the second vertical deflection current I_{v1} causes a linear vertical scan.

The invention can be used to interpolate a vertical or a horizontal
5 correction waveform from a few stored values a_i . The invention can also be used to correct for convergence or other deflection distortions (for example north-south pincushion distortion) occurring in so called transposed scanned picture tubes whereby vertical scanned lines succeed each other in the horizontal direction. Any reference signs in the claims cannot be construed as limiting the claim.

CLAIMS:

1. A method for generating a one-dimensional spline waveform (C_w), the one-dimensional spline waveform (C_w) being a function of a position on a display screen of a display device (CRT) in one direction, the method comprising the steps of:
 - generating (4) from a position information (I) indicating the position on the display screen a position address (P), the position address (P) being partitioned in a section number indicating a number of a section (S_i), and a relative position (d) indicating a position within the section (S_i) for virtually partitioning the display screen in sections (S_i) in the one direction;
 - calculating (3), in each section (S_i), from the relative position (d) and a set of $p+1$ sub-function coefficients ($b_{1i}, \dots, b_{(p+1)i}$) a sub-function (S_{fi}) being a polynomial of degree $p > 1$ for obtaining the one-dimensional spline waveform (C_w) being a chain of $n-p$ consecutive sub-functions ($S_{f1}, \dots, S_{f(n-p)}$) in $n-p$ corresponding consecutive sections ($S(1), \dots, S(n-p)$), an analog representation of the one-dimensional spline waveform (C_w) being continuous and at least $p-1$ times continuous differentiable;
 - selecting, in response to the section number, from an array of n consecutive predetermined values ($a(1), \dots, a(n)$) a selected subset of $q \geq p+1$ consecutive selected values ($a_s(1), \dots, a_s(q)$), the selected subset for the section (S_i) being $a(i+r), a(i+r+1), \dots, a(i+r+q-1)$ with r being selected from a range $p+1-q \leq r \leq 0$, whereby $a(i)=0$ for $i < 1$ and $i > n$; and
 - multiplying in each section (S_i), the selected subset ($a_s(1), \dots, a_s(q)$) with a fixed $(p+1)*q$ spline matrix of multiplication factors (c_{ij}) to produce the set of $p+1$ subfunction coefficients ($b_{1i}, \dots, b_{(p+1)i}$).
2. A method as claimed in claim 1, characterised in that in every row of the spline matrix at least one of the multiplication factors (c_{ij}) is not zero for obtaining sub-functions (S_{fi}) comprising all powers of the relative position (d) from zero up to and including the p -th power.
3. A method as claimed in claim 1, characterised in that $q=p+1$ for obtaining a $(p+1)*(p+1)$ spline matrix and selecting a number of selected values (a_{si}) being equal to a number of sub-function coefficients (b_i).

4. A method as claimed in claim 1, characterised in that $p=2$ for obtaining the waveform (Cw) being a quadratic spline function.

5. A method as claimed in claim 1, characterised in that the step of generating (4) the position address (P) from the position information (I) being related to a

5 deflection current comprises the steps of:

measuring (40,42,44) a first moment in time (T1) at which the position information (I) has a first value (I1),

measuring (41,43,44) a second moment in time (T2) at which the position information (I) has a second value (I2), and

10 calculating (45) the position address (P) as a linear function in time from predetermined position address values (P1,P2) at the first and second moments in time (T1,T2),

whereby the deflection current has a shape for obtaining an approximately linear scan on the screen.

15 6. A method as claimed in claim 5, characterized in that the step of measuring (40,42,43) the first and second moment in time (T1,T2) comprises the steps of:

generating (44) a count value (C) indicative for a period of time,

storing (42) a first count value (O1) in response to detecting (40) that the position information (I) has the first value (I1),

20 storing (43) a second count value (O2) in response to detecting (41) that the position information (I) has the second value (I2), and

calculating (45) the position address (P) as a linear function in time from predetermined position address values (P1,P2) at the first and second moments in time (T1,T2) which are related to the first and second count values (O1,O2).

25 7. A method for generating a two-dimensional spline waveform (Wd), the two-dimensional spline waveform (Wd) being dependent on a position in a first and a second direction on a screen of a display device (CRT), the display device being scanned in a raster of lines, the first and the second direction being substantially perpendicular, the method comprises the steps of:

30 generating (100) m one-dimensional spline waveforms (Cwi) from m sets of predetermined values ($a_{1i}, \dots, a_{ni}$), the one-dimensional spline waveforms (Cwi) being generated according to the method as claimed in claim 1, wherein the position address (P) is a position address (Pv) related to the position on the screen in the first direction, each of the one-dimensional waveforms (Cwi) representing output values (g_i) being the values of the

one-dimensional waveforms (Cw_i) at the positions of the lines in the raster, and
generating (200) from the output values (g_i) and a position address (Ph)
related to the position on the screen in the second direction the two-dimensional spline
waveform (Wd).

5 8. A method as claimed in claim 7, characterized in that the step of
generating (200) the two-dimensional spline waveform (Wd) is performed according to the
method of claim 1, wherein the position address (P) is related to the position on the screen in
the second direction and the predetermined values (a_i) are the output values (g_i).

10 9. A system for generating a one-dimensional spline waveform (Cw_1), the
one-dimensional spline waveform (Cw) being a function of a position on a display screen of
a display device (CRT) in one direction, the system comprising:

means (4) for generating from a position information (I) indicating the
position on the display screen a position address (P), the position address (P) being partitioned
15 in a section number indicating a number (i) of a section (S_i) and a relative position (d)
indicating a position within the section (S_i) for virtually partitioning the display screen in
sections (S_i) in the one direction,

calculating means (3) for calculating, in each section (S_i), from the
relative position (d) and a set of $p+1$ sub-function coefficients ($b_{1i}, \dots, b_{(p+1)i}$) a sub-
20 function (Sf_i) being a polynomial of degree $p > 1$ for obtaining the one-dimensional spline
waveform (Cw) being a chain of $n-p$ consecutive sub-functions ($Sf_1, \dots, Sf_{(n-p)}$) in $n-p$
corresponding consecutive sections ($S(1), \dots, S(n-p)$), an analog representation of the one-
dimensional spline waveform (Cw) being continuous and at least $p-1$ times continuous
differentiable,

25 selecting, in response to the section number, from an array of n
consecutive predetermined values ($a(1), \dots, a(n)$) a selected subset of $q \geq p+1$ consecutive
selected values ($as(1), \dots, as(q)$), the selected subset for the section (S_i) being
 $a(i+r), a(i+r+1), \dots, a(i+r+q-1)$ with r being selected from a range $p+1-q \leq r \leq 0$, whereby
 $a(i)=0$ for $i < 1$ and $i > n$; and

30 multiplying in each section (S_i), the selected subset ($as(1), \dots, as(q)$) with a
fixed $(p+1)*q$ spline matrix of multiplication factors (c_{ij}) to produce the set of $p+1$
subfunction coefficients ($b_{1i}, \dots, b_{(p+1)i}$).

10. A display apparatus comprising:
a display device (CRT) with a display screen for displaying display

information,

an addressing circuit (7) receiving a horizontal and vertical position signal (H,V) for supplying position determining signals to means determining the position on the display screen (Lh,Lv),

5 means for generating a one-dimensional digital waveform (Cw) being represented by discrete values, the one-dimensional digital waveform (Cw) being a function of a position on the display screen in one direction, the means for generating the one-dimensional digital waveform (Cw1) comprising:

means (4) for generating from a position information (I) indicating the position on the display screen a position address (P), the position address (P) being partitioned in a section number indicating a number of a section (Si) and a relative position (d) indicating a position within the section (Si) for virtually partitioning the display screen in sections (Si) in the one direction,

calculating means (3) for calculating, in each section (Si), from the relative position (d) and a set of $p+1$ sub-function coefficients ($b_{1i}, \dots, b_{(p+1)i}$) a sub-function (Sfi) being a polynomial of degree $p > 1$ for obtaining the one-dimensional digital waveform (Cw) being a chain of $n-p$ consecutive sub-functions ($Sf_1, \dots, Sf_{(n-p)}$) in $n-p$ corresponding consecutive sections ($S(1), \dots, S(n-p)$),

selecting, in response to the section number, from an array of n consecutive predetermined values ($a(1), \dots, a(n)$) a selected subset of $q \geq p+1$ consecutive selected values ($as(1), \dots, as(q)$, the selected subset for the section (Si) being $a(i+r), a(i+r+1), \dots, a(i+r+q-1)$ with r being selected from a range $p+1-q \leq r \leq 0$, whereby $a(i)=0$ for $i < 1$ and $i > n$; and

20 multiplying in each section (Si), the selected subset ($as(1), \dots, as(q)$) with a fixed $(p+1)*q$ spline matrix of multiplication factors (c_{ij}) to produce the set of $p+1$ subfunction coefficients ($b_{1i}, \dots, b_{(p+1)i}$),

means (5) for converting (5) the one-dimensional digital waveform (Cw) into an analog one-dimensional spline waveform (Wa), the analog one-dimensional spline waveform (Wa) being continuous and at least $p-1$ times continuous differentiable, and

30 means (Lc;Lh;Lv) receiving the analog one-dimensional spline waveform (Wa) for influencing the position on the display screen.

11. A method for generating a k_i -th order one-dimensional spline waveform (Cw1), the one-dimensional spline waveform (Cw1) being a function of a position on a

display screen of a display device (CRT) in one direction, the method comprising the steps of:

generating (4) from a position information (I) indicating the position in the one direction a position address (P), and

5 generating (2,3) at positions indicated by the position address (P) the waveform (Cw1) from n predetermined input values (ai), the correction waveform (Cw1) being a p-th order spline function composed of n-p consecutive sub-functions (Sfi) in n-p respectively corresponding consecutive sections (Si), wherein p is larger than 1, the correction waveform generating step (2,3) comprising the steps of:

10 generating n basic functions (Fbi) of the position address (P), the basic functions (Fbi) all having a same shape and being shifted over one section (Si) with respect to each other, and each being a ki-th order spline function, the basic functions (Fbi) being composed as a chain of portions (pi) each extending over one section (Si),

15 multiplying each of the basic functions (Fbi) with an associated one of the stored values (ai),

calculating each of the sub-functions (Sfi) by adding, in a same section (Si), the portions (pi) of the basic functions (Fbi) in this section (Si) multiplied with the associated stored values (ai).

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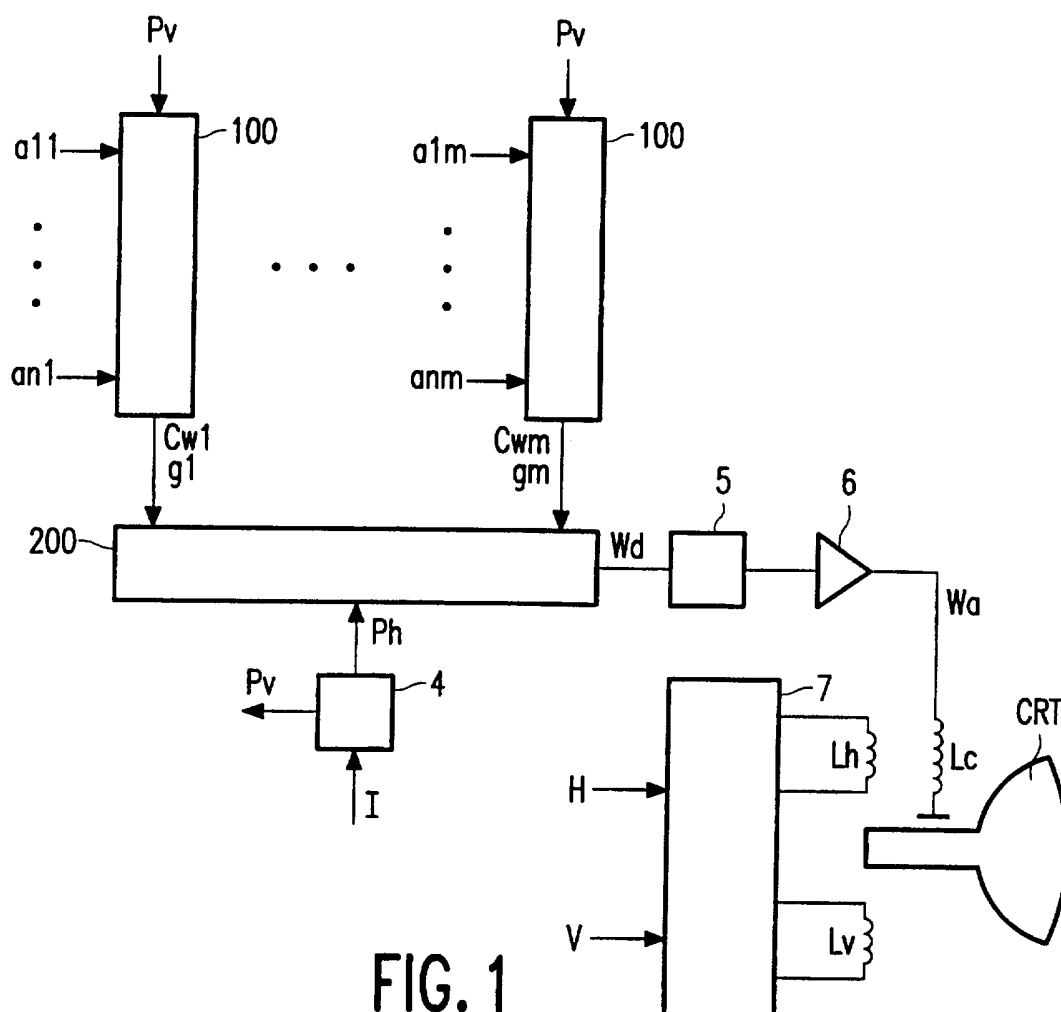


FIG. 1

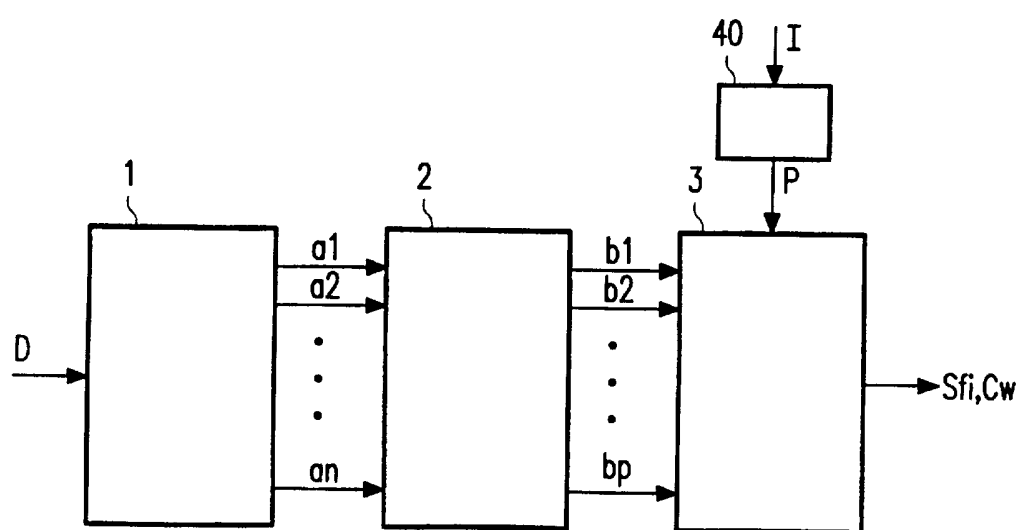


FIG. 2

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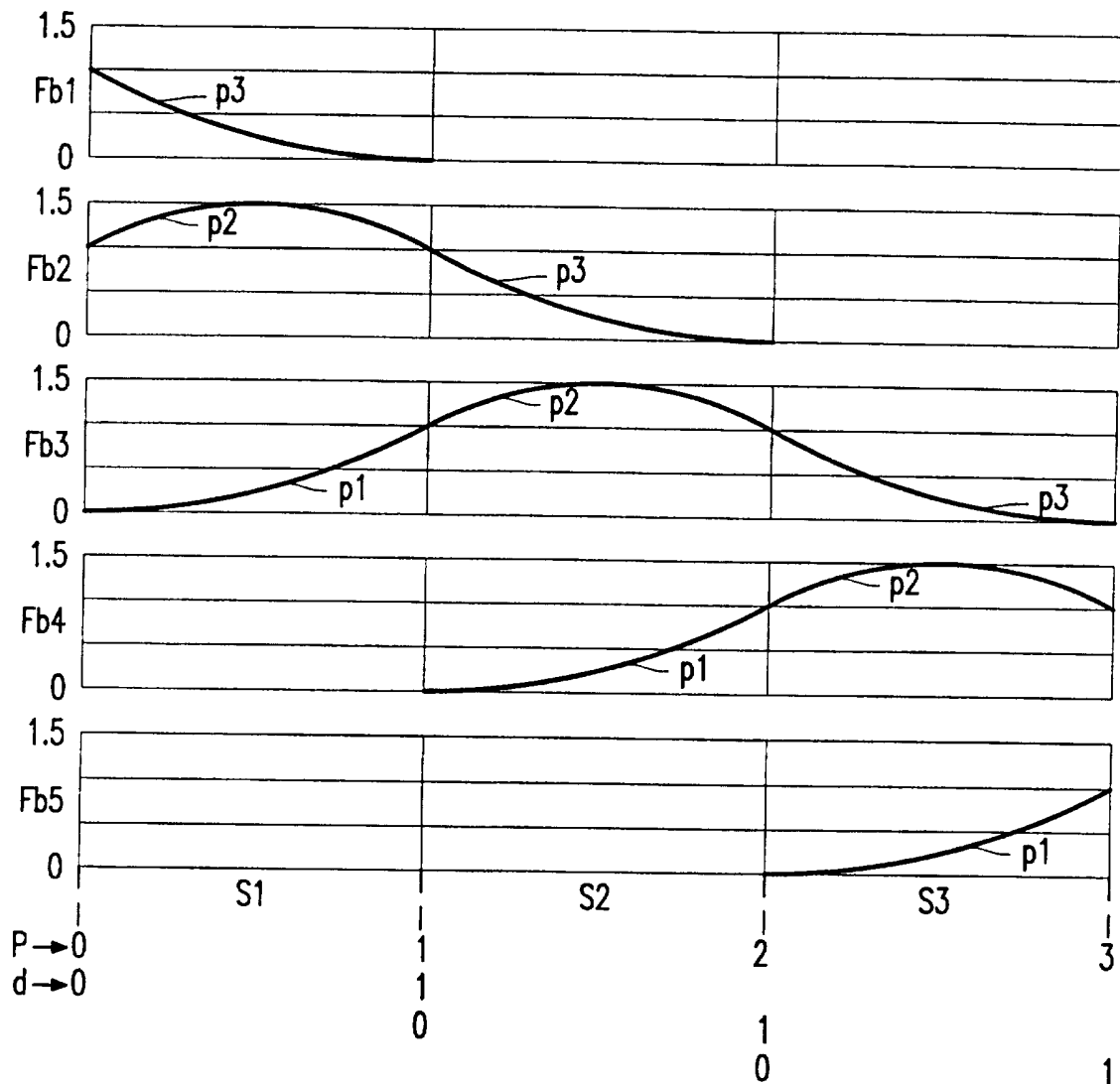


FIG. 3

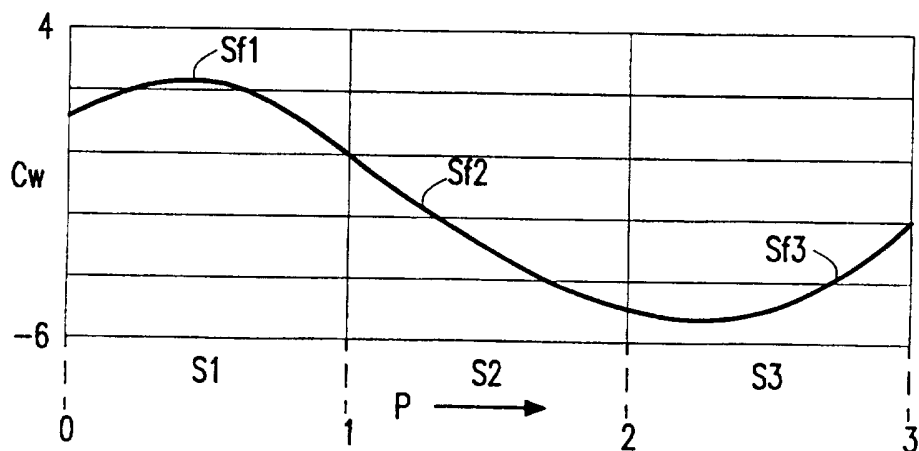


FIG. 4

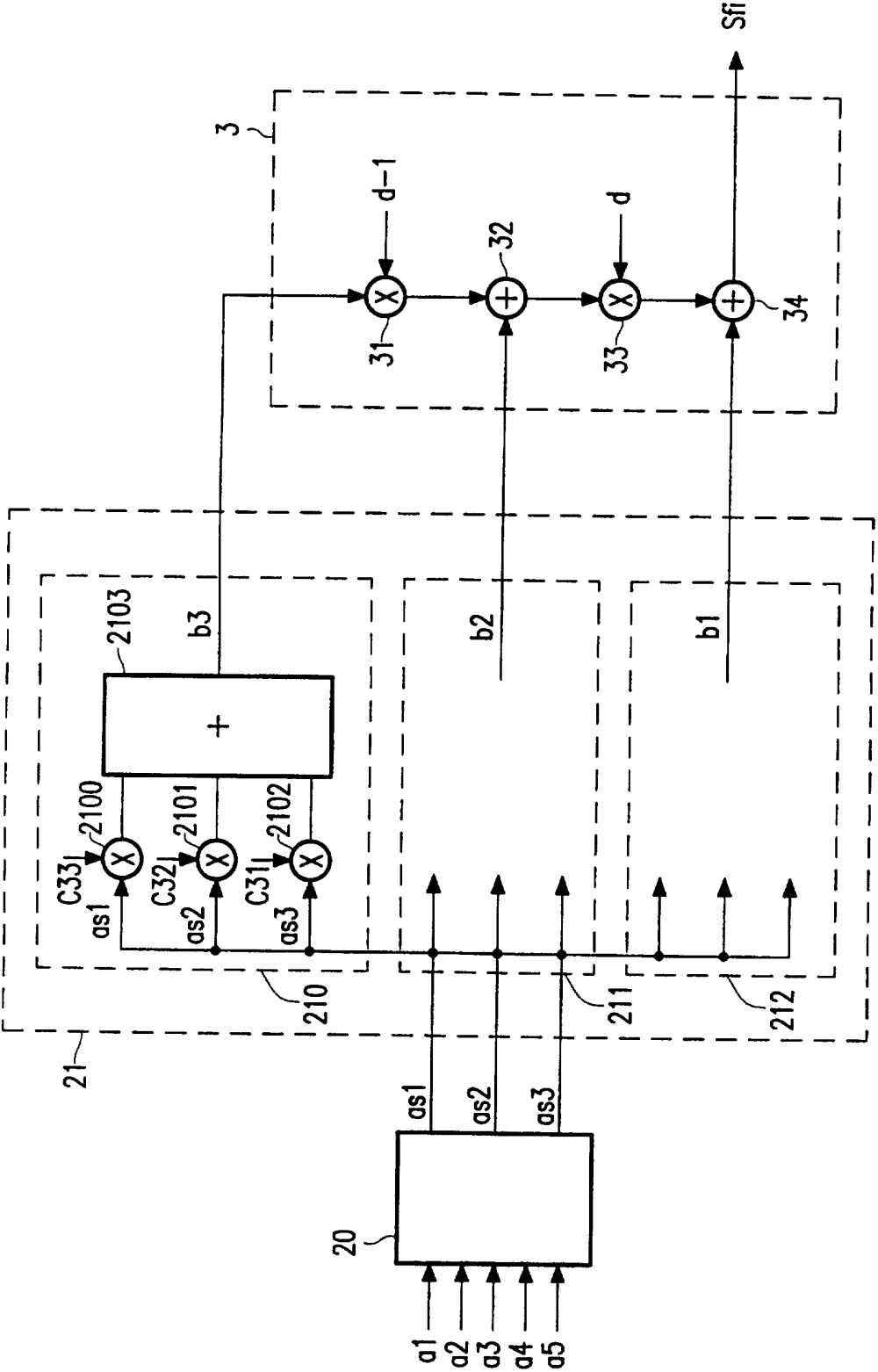


FIG. 5

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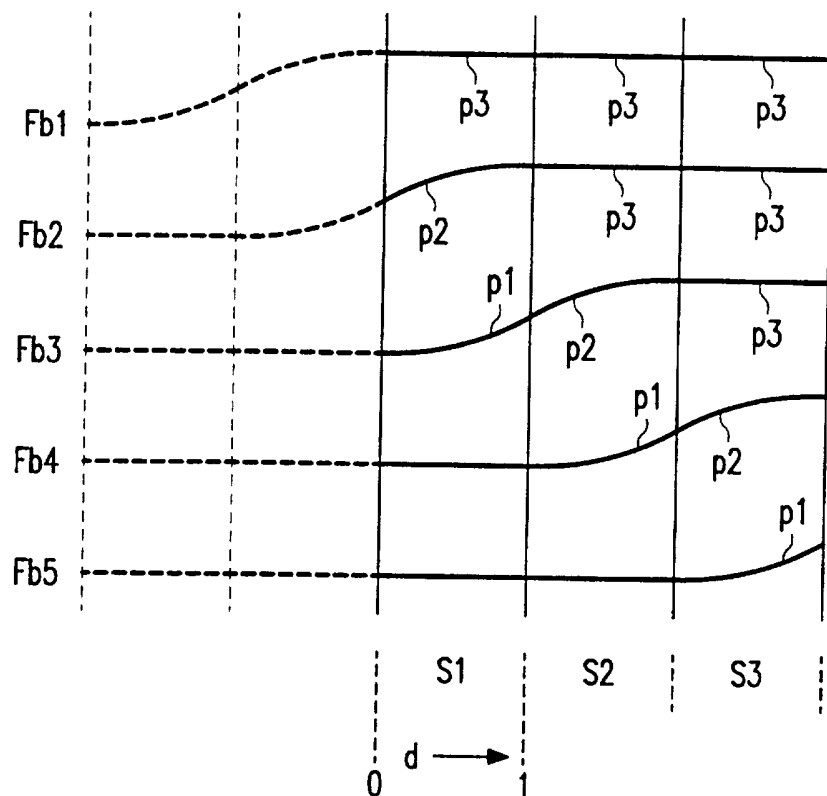


FIG. 6

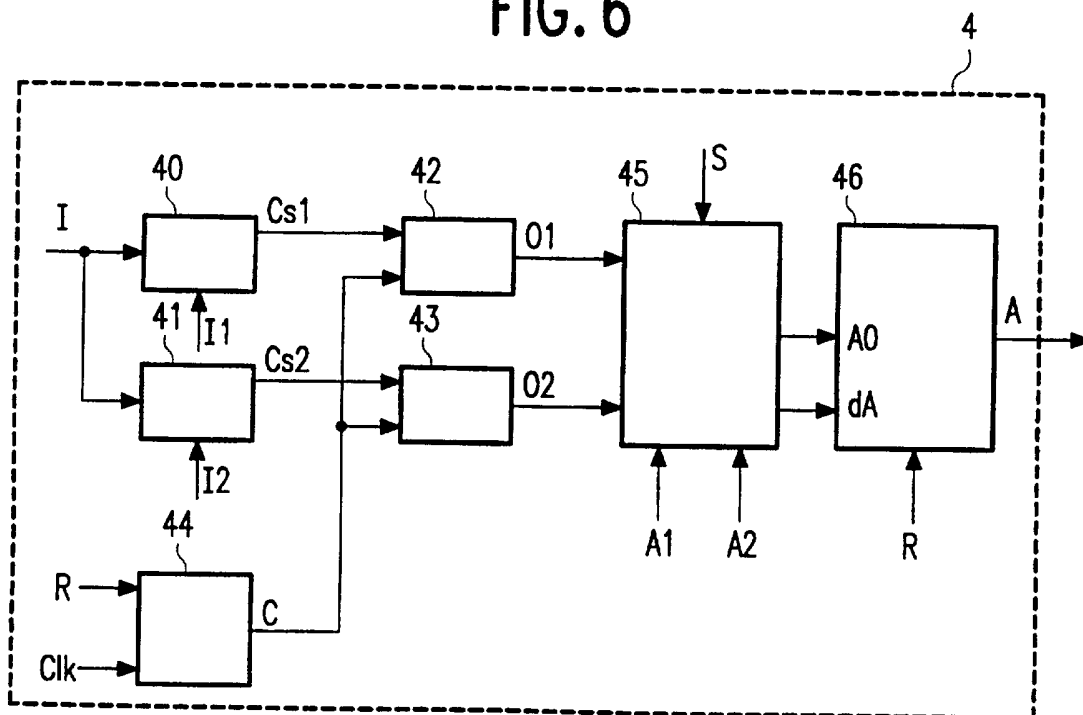


FIG. 7

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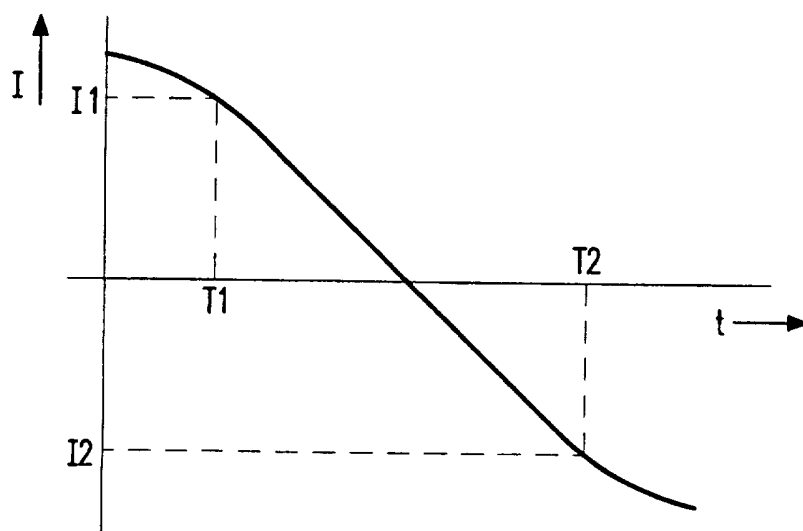


FIG. 8

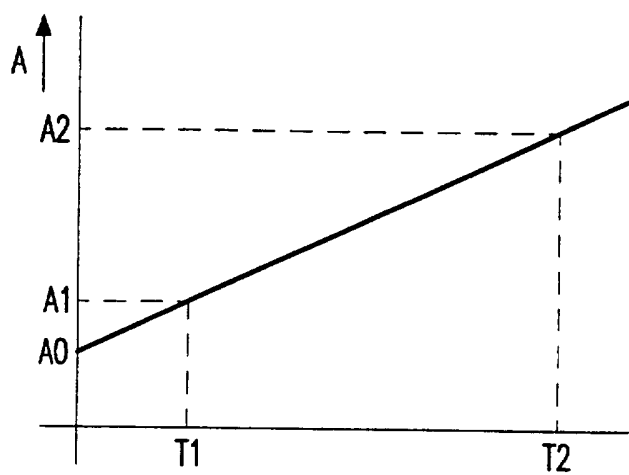


FIG. 9

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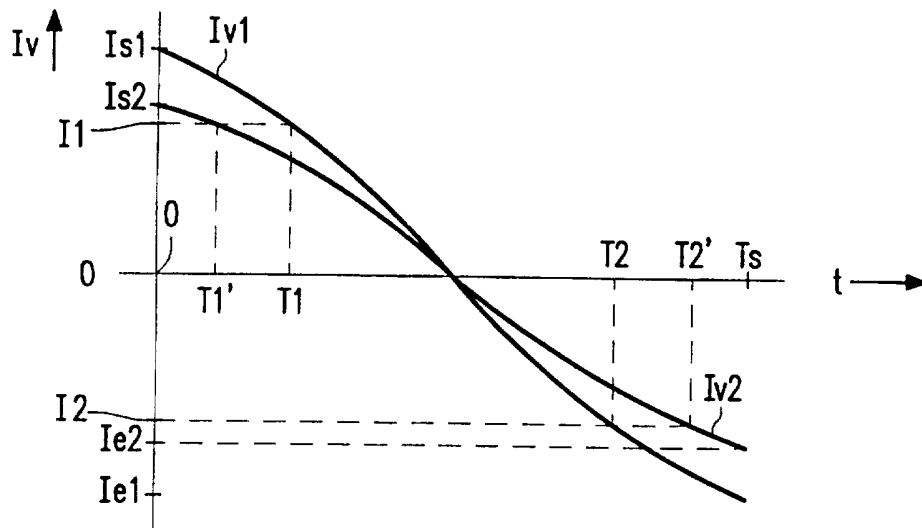


FIG. 10

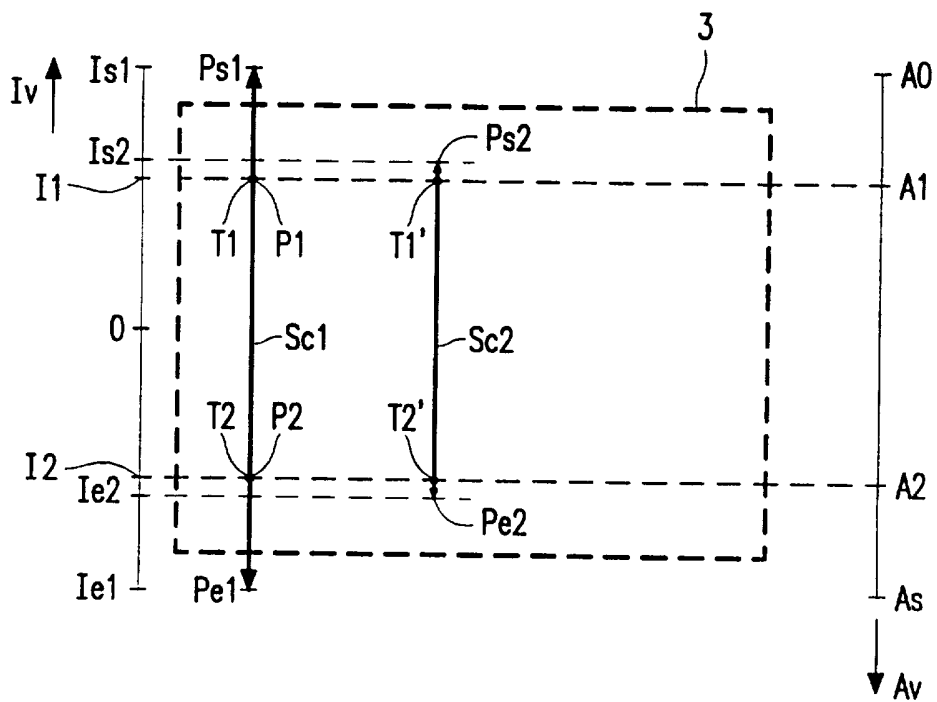


FIG. 11

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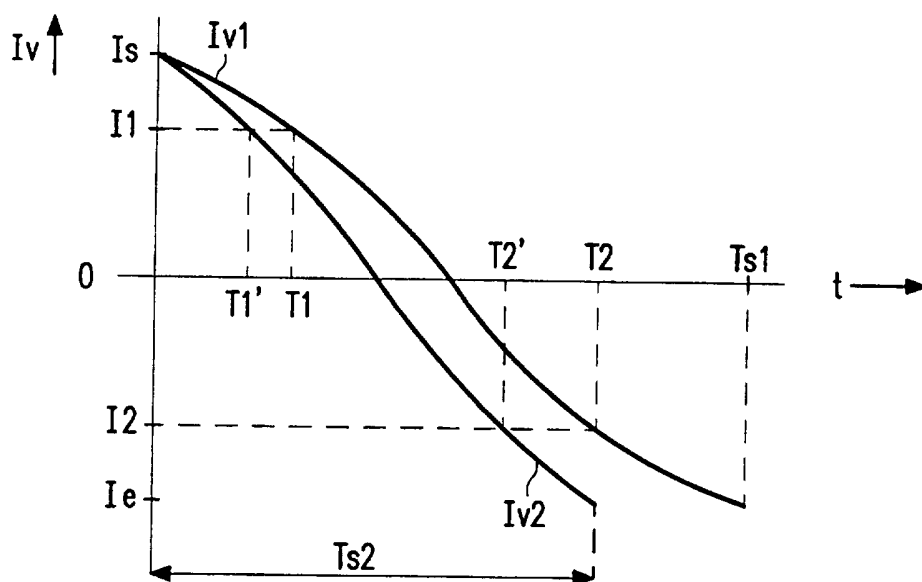


FIG. 12

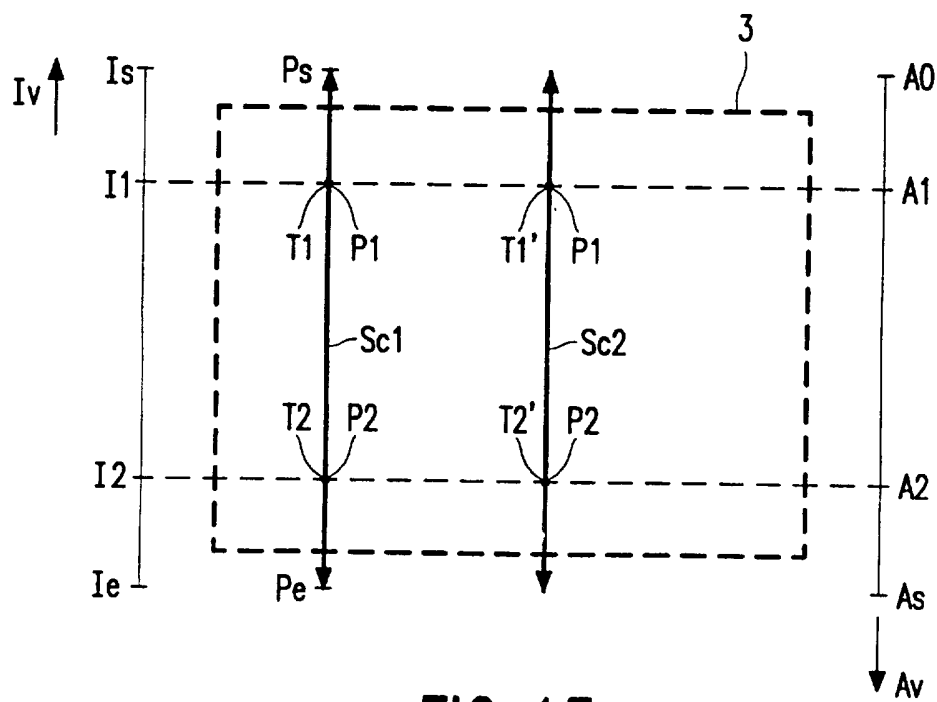


FIG. 13