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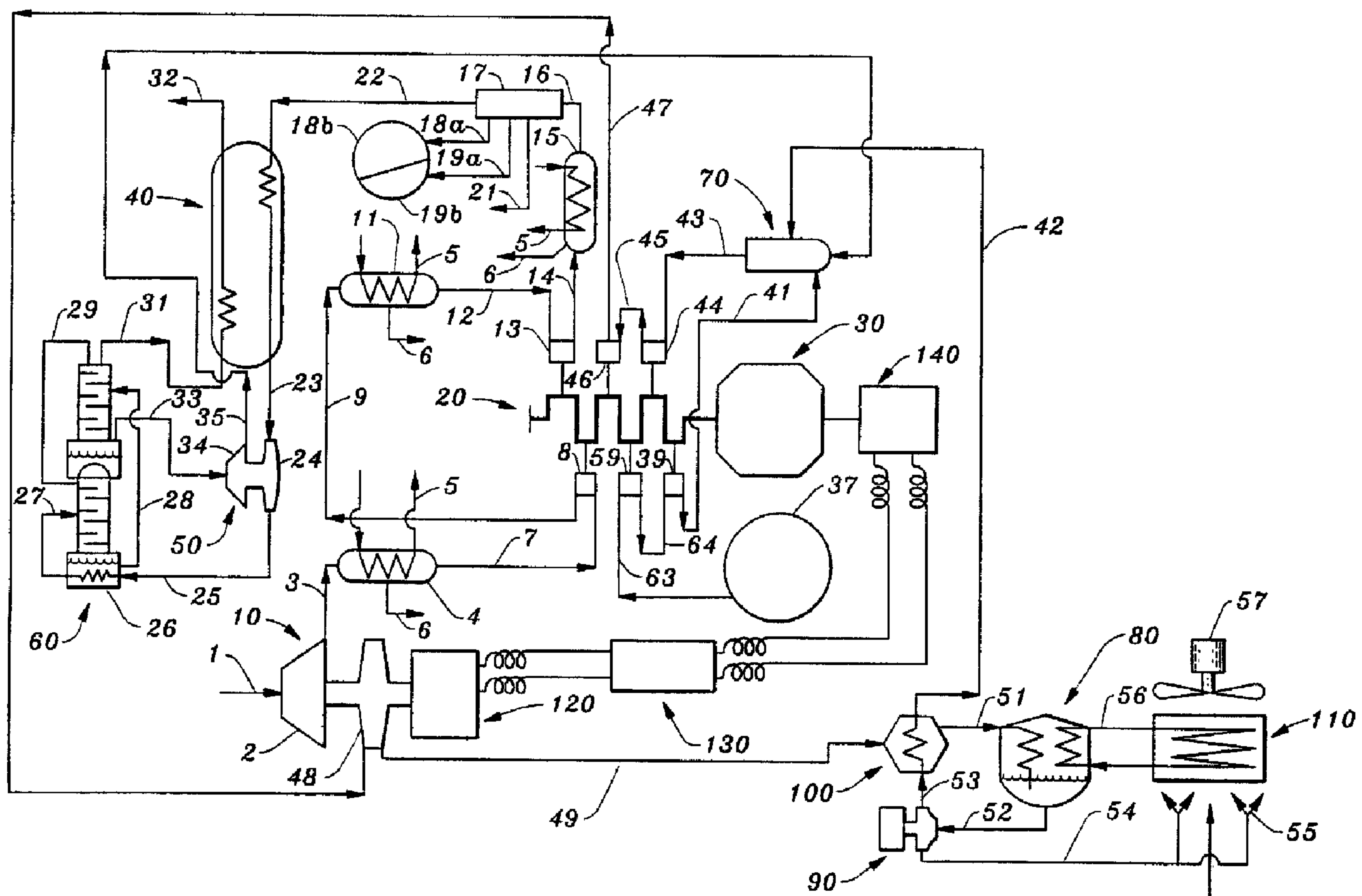
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(57) Abrégé/Abstract:

A low pollution engine (500) is provided for delivering power for vehicles. The engine has an air inlet (510) which collects air from a surrounding environment. A portion of the nitrogen in the air is removed using a technique such as liquefaction, pressure swing

(57) **Abrégé(suite)/Abstract(continued):**

adsorption or membrane based air separation. The remaining air is primarily oxygen, which is then compressed and routed to a combustion chamber. The chamber has an igniter and inputs for the pressurized oxygen and pressurized hydrogen containing fuel, including methane. The combustion products of water and carbon dioxide are expanded through a power generating device, such as a turbine or piston expander (560). The combustion products are then passed through a condenser (580) where the steam is condensed and the carbon dioxide is collected or discharged. A portion of the water is then routed back to the gas generator.

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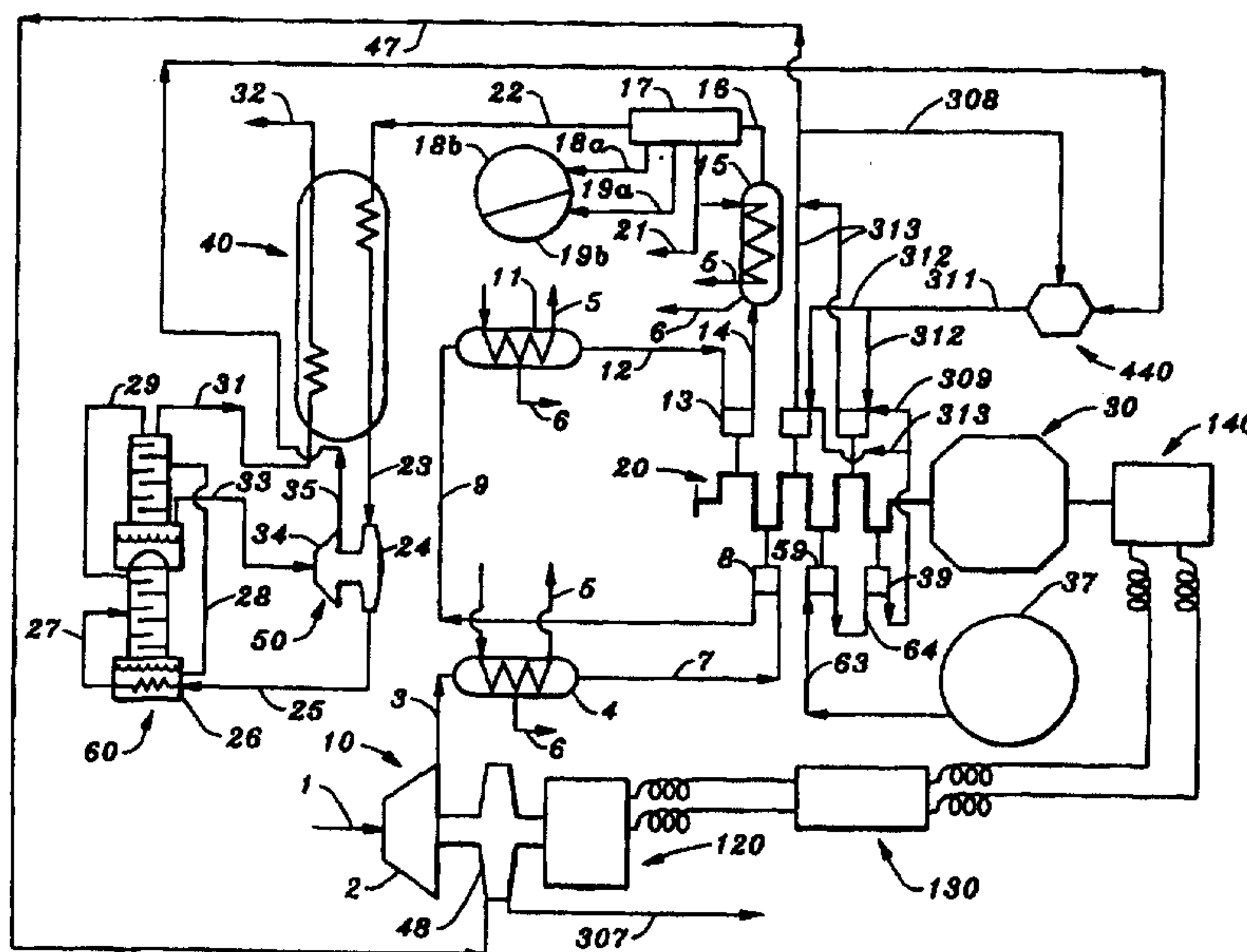
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(54) Title: CLEAN AIR ENGINES FOR TRANSPORTATION AND OTHER POWER APPLICATIONS



(57) Abstract

A low pollution engine (500) is provided for delivering power for vehicles. The engine has an air inlet (510) which collects air from a surrounding environment. A portion of the nitrogen in the air is removed using a technique such as liquefaction, pressure swing adsorption or membrane based air separation. The remaining air is primarily oxygen, which is then compressed and routed to a combustion chamber. The chamber has an igniter and inputs for the pressurized oxygen and pressurized hydrogen containing fuel, including methane. The combustion products of water and carbon dioxide are expanded through a power generating device, such as a turbine or piston expander (560). The combustion products are then passed through a condenser (580) where the steam is condensed and the carbon dioxide is collected or discharged. A portion of the water is then routed back to the gas generator.

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CLEAN AIR ENGINES FOR TRANSPORTATION AND OTHER POWER APPLICATIONS

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Technical Field

10 This invention contains environmentally clean engine designs that emit zero or very low pollutant levels during operation. The CLEAN AIR ENGINE (CLAIRE) invention is directly applicable to both transportation type vehicles including automobiles, trucks, trains, airplanes, ships and to stationary power generation applications. The designs feature hybrid, dual cycle and single cycle engines.

15

Background Art

20 The current art in generating power for transportation purposes basically utilize the internal combustion gas or diesel engine. The current art for electric power generation utilize gas turbines and/or steam turbines. These devices burn hydrocarbon fuels with air which contains (by weight) 23.1% oxygen, 75.6% nitrogen and the remaining 1.3% in other gases. The emissions resulting from the combustion of fuels for internal combustion engines (gasoline or diesel), with air contain the following pollutants that are considered damaging to our air environment. These smog causing pollutants, are: total organic gases (TOG); reactive organic gases (ROG); carbon monoxide (CO);

25 oxides of nitrogen (NO_x); oxides of sulfur (SO_x); and particulate matter (PM). Approximately one half of the total pollutants emitted by all sources of air pollution in California are generated by road vehicles (Emission Inventory 1991, State of California Air Resources Board, prepared January 1994). The major source of this vehicle pollution comes from passenger cars and light to medium

30 duty trucks.

No near term solutions appear in sight to drastically reduce the vast amount of air pollutants emitted by the many millions of automobiles and trucks operating today. Based on the State of California Air Resources Board study, the average discharge per person in California of the air pollutants from mobile vehicles, monitored by this agency during 1991 and reported in 1994, was

35 approximately 1.50 lb/day per person. With a nationwide population of over 250,000,000 people, this data extrapolates to over 180,000 tons of air borne emissions per day being discharged in the USA by mobile vehicles. Also, the number of cars and miles that are being driven continue to increase, further hampering efforts to reduce smog causing pollutants.

Allowable emission thresholds are rapidly tightening by Federal and State mandates. These allowable emission reductions are placing severe demands on the transportation industry and the electric power generating industry to develop new and lower emission power systems.

5 Although considerable effort is being directed at improving the range of electric zero emission vehicles (ZEV) by developing higher energy capacity, lower cost storage batteries, the emission problem is been transferred from the vehicle to the electric power generating plant, which is also being Federally mandated (Clean Air Act Amendments of 1990) to reduce the same air toxic emissions as those specified for automobiles and trucks.

10 The current world wide art of generating power for consumers of electricity depends primarily on fossil fuel burning engines. These engines burn hydrocarbon fuels with air. As described above, combustion of fossil fuels with air usually produce combustion products that contain a number of pollutants. Current United States regulatory requirements prescribe the amounts of the atmospheric pollutants permitted in particular locations. Allowable pollutant thresholds are decreasing over time and thereby putting more and more pressure on industry to find better
15 solutions to reduce these emissions of pollutants in the electric power generating industry and other power generating industries.

Other energy sources being developed to solve the emissions problem, by exploiting non-combustible energy sources include fuel cells and solar cells. Developers are solving many of the technological and economic problems of these alternate sources. However, widespread use of
20 these energy sources for vehicles and for electric power generating facilities do not appear to yet be practical.

Disclosure of Invention

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This invention provides a means for developing a zero or very low pollution vehicle (ZPV) and other transportation power systems (i.e. rail and ship), as well as a zero or low pollution electric power generating facility. The zero or very low pollution is achieved by removing the harmful pollutants from the incoming fuel and oxidizer reactants prior to mixing and burning them in a gas
30 generator or combustion chamber. Sulfur, sulfides and nitrogen are major pollutants that must be removed from the candidate fuels: hydrogen, methane, propane, purified natural gas, and light alcohols such as ethanol and methanol. Since air contains 76% nitrogen by weight, it becomes a major source of pollution that also requires removal prior to combining it with the clean fuel.

Cleansing of the fuel is straightforward and requires no further elaboration. The separation of
35 the oxygen from the nitrogen in the air, however, is accomplished in a variety of ways. For instance, nitrogen can be removed from air by the liquefaction of air and gradual separation of the two major constituents, oxygen and nitrogen, by means of a rectifier (to be described later in more detail). The separation of the gases relies on the two distinct boiling points for oxygen (162°R)

and for nitrogen (139°R) at atmospheric pressure. Air liquefies at an intermediate temperature of (142°R).

Other nitrogen removal techniques include vapor pressure swing adsorption, and membrane based air separation. With vapor pressure swing adsorption, materials are used which are capable of adsorption and desorption of oxygen. With membrane based air separation, an air feed stream under pressure is passed over a membrane. The membrane allows one component of the air to pass more rapidly there through than other components, enriching the amount of different components on opposite sides of the membrane. Such membranes can be of a variety of different materials and use several different physical processes to achieve the desired separation of nitrogen out of the air.

One embodiment of this invention consists of a hybrid power system that combines a Rankine cycle thermal cycle with an auxiliary electric motor for start-up and chill-down requirements. The thermal power cycle of the engine begins by compressing ambient air to high pressures, cooling the air during compression and during the expansion to liquid air temperatures in a rectifier where separation of the oxygen and nitrogen takes place. The cold gaseous nitrogen generated is used to cool the incoming air and then is discharged to the atmosphere at near ambient temperature. Simultaneously, the cold gaseous or liquid oxygen generated by the rectifier is pressurized to gas generator pressure levels and delivered to the gas generator at near ambient temperature. Fuel, gaseous or liquid, from a supply tank is pressurized to the pressure level of the oxygen and also delivered to the gas generator where the two reactants are combined at substantially the stoichiometric mixture ratio to achieve complete combustion and maximum temperature hot gases (6500°R). These hot gases are then diluted with water downstream in a mixing section of the gas generator until the resulting temperature is lowered to acceptable turbine inlet temperatures (2000°R).

The drive gas generated from this mixing process consists of high purity steam, when using oxygen and hydrogen as the fuel, or a combination of high purity steam and carbon dioxide (CO₂), when using oxygen and light hydrocarbon fuels (methane, propane, methanol, etc.). Following the expansion of the hot gas in the turbine, which powers the vehicle or the electric power generating plant, the steam or steam plus CO₂ mixture are cooled in a condenser to near or below atmospheric pressure where the steam condenses into water, thus completing a Rankine cycle. Approximately 75% of the condensed water is recirculated to the gas generator while the remainder is used for cooling and discharged to the atmosphere as warm water vapor. When using light hydrocarbons as the fuel, the gaseous carbon dioxide remaining in the condenser is compressed to slightly above atmospheric pressure and either converted to a solid or liquid state for periodic removal, or the gas can be discharged into the atmosphere when such discharge is considered non-harmful to the local air environment.

Since this thermal cycle requires time to cool the liquefaction equipment to steady state low temperatures, an electric motor, driven by an auxiliary battery, can be used to power the vehicle

and initiate the Rankine cycle until chill-down of the liquefaction equipment is achieved. When chill-down is complete the thermal Rankine engine, connected to an alternator, is used to power the vehicle or stationary power plant and recharge the auxiliary battery.

5 The combination of these two power systems, also referred to as a hybrid vehicle, emit zero or very low pollution in either mode of operation. In addition, the electric motor battery is charged by the zero or very low pollution thermal Rankine cycle engine itself and thus does not require a separate electric power generating plant for recharge. This reduces the power demand from central power stations and also reduces a potential source of toxic air emissions.

10 In place of the electric drive motor and battery, the Rankine cycle engine, with the addition of a few control valves, can also be operated as a minimally polluting open Brayton cycle, burning fuel and incoming air to power the vehicle during the period necessary to allow the Rankine cycle engine liquefaction equipment time to chill-down. This feature is another embodiment of this invention.

15 The zero or very low pollution Rankine cycle engine can also be used in a single cycle thermal mode for vehicles with long duration continuous duty such as heavy trucks, trains, ships and for stationary power generation plants where the chill-down time is not critical to the overall operational cycle.

20 The adaptation of the Otto and Diesel thermal cycles to a low-polluting hybrid engine are also included as embodiments of this invention. By using these thermal cycles, the need for a condenser and recirculating water system are eliminated. Low temperature steam or steam/carbon dioxide gases are recirculated as the working fluid and therefore replace the function of the recirculating water quench of the Rankine cycle embodiments previously discussed.

25 Brief Description of Drawings

Further features and advantages of this invention, which are defined by the appended claims, will become apparent from consideration of the following drawings:

30 Figure 1 is a schematic illustrating an embodiment of this invention and its elements, along with their connectivity. This embodiment constitutes a very low pollution or pollution-free hybrid power system for vehicular and other applications. The fuel reactant is a light hydrocarbon type such as methane propane, purified natural gas, and alcohols (i.e. methanol, ethanol).

35 Figure 2 is a schematic illustrating an embodiment of this invention which is also a very low pollution or pollution-free hybrid power system for vehicular and other applications where the fuel is gaseous hydrogen.

Figure 3 is a schematic illustrating an embodiment of this invention which is a very low pollution or pollution-free power system for vehicular and other applications during cruise and continuous duty. During start-up and a short period thereafter, the engine runs in an open Brayton

cycle mode and thus emits some pollutants.

Figure 4 is a plot of Temperature v. Entropy for the working fluid illustrating the first of two cycles used in the dual mode engine of Fig. 3. This cycle is an open Brayton with inter-cooling between compressor stages (Mode I).

5 Figure 5 is a plot of Temperature v. Entropy for the working fluid illustrating the second cycle used in the dual mode engine of Fig. 3. This cycle is a Rankine with regeneration, (Mode II).

Figure 6 is a schematic illustrating an embodiment of this invention and its interconnecting elements. This embodiment constitutes a very low pollution or pollution-free hybrid power system for vehicular and other applications similar to that of Fig. 1 but with the addition of two reheaters to the power cycle for improved performance. The fuel reactant for this cycle is a light hydrocarbon.

Figure 7 is a schematic illustrating an embodiment of this invention and its interconnecting elements. This embodiment constitutes a very low pollution or pollution-free hybrid power system similar to that of Fig. 2 but with the addition of two reheaters to the power cycles for improved performance. The fuel reactant for this cycle is hydrogen.

Figure 8 is a plot of Temperature v. Entropy for the working fluid for the power cycle used for the thermal engines shown in Fig. 6 and Fig. 7. This cycle features the Rankine cycle with regeneration and reheat for improved performance.

Figure 9 is a schematic illustrating an embodiment of this invention that features a very low pollution or non-polluting hybrid engine with electric motor drive and a Rankine power cycle utilizing dynamic type turbomachinery. The Rankine power cycle utilizes regeneration and reheaters for increased cycle efficiency and power density.

Figure 10 is a schematic illustrating an embodiment of this invention that features a low-polluting hybrid engine with an electric motor drive and an Otto power cycle reciprocating engine.

25 Figure 11 is a schematic illustrating an embodiment of this invention that features a low-polluting hybrid engine with an electric motor drive and a Diesel power cycle reciprocating engine.

Figure 12 is a schematic illustrating a basic low-polluting engine where a rectifier and air liquefaction devices of previous embodiments are replaced with an air separation plant which separates nitrogen from air by any of a variety of techniques including liquefaction, vapor pressure swing adsorption, membrane based air separation, etc.

Figure 13 is a schematic similar to that which is shown in Fig. 12 but including regeneration in the cycle disclosed therein.

Figure 14 is a schematic similar to that which is disclosed in Figs. 12 and 13 except that a dual cycle arrangement is provided which features a bottoming cycle for enhanced efficiency.

35 Figure 15 is a schematic of a typical pressure swing adsorption plant for use as the air separation plant in one of the engines disclosed in Figs. 12-14.

Figure 16 is a schematic of a membrane flow two stage enrichment of oxygen and nitrogen system for use as part of the air separation plant of the cycles disclosed in Figs. 12-14.

Best Modes for Carrying Out the Invention

According to the first embodiment of the present invention, a zero or very low pollution Rankine cycle thermal engine operating in parallel with a zero emissions electric motor (also referred to as a hybrid engine) is illustrated in Fig. 1. The Rankine engine consists of a dynamic
 5 turbocompressor 10, a reciprocating engine 20, a power transmission 30, a heat exchanger 40, a turboexpander 50, a rectifier 60, a gas generator 70, a condenser 80, a recirculating water feed pump 90, a water heater 100 and a condenser coolant radiator 110. The electric engine consists of an alternator 120, a battery 130 and electric motor 140.

10 Hybrid engine operation begins by starting the electric motor 140 using the battery 130 as the energy source. The electric motor 140 drives the reciprocating engine 20 through the power transmission 30 and thereby initiates the start of the thermal engine that requires a chill-down period for the liquefaction equipment consisting of heat exchanger 40, turboexpander 50 and rectifier 60.

15 Activation of the thermal engine initiates the compression of ambient temperature air from a surrounding environment entering the dynamic compressor 2 through an air inlet duct 1. The compressor 2 raises the air to the design discharge pressure. The air then exits through duct 3 into intercooler 4 where the heat of compression is removed by external cooling means 5 (i.e. air, water, Freon, etc.). Condensed water vapor from the air is tapped-off by drain 6. After the air
 20 exits intercooler 4 through duct 7, at a temperature equal to the compressor inlet, it enters the reciprocating compressor 8 and is raised to the design discharge pressure. The air exits through duct 9 into intercooler 11 and is again cooled to the inlet temperature of the compressor. This compression/cooling cycle is repeated as the air exits intercooler 11 through duct 12 and enters reciprocating compressor 13, then exits through duct 14, enters intercooler 15 and exits through
 25 duct 16, to complete the air pressurization.

The high pressure, ambient temperature air then enters the scrubber 17 where any gases or fluids that could freeze during the subsequent liquefaction are removed. These gases and liquids include carbon dioxide (duct 18a and storage tank 18b), oil (line 19a and storage tank 19b) and water vapor (tap off drain 21). The oil can be from a variety of sources, such as leakage from the
 30 air compression machinery. The dry air then exits through duct 22 and enters heat exchanger 40 where the air is cooled by returning low temperature gaseous nitrogen.

The dry air is now ready to pass through an air treatment device for the separation of nitrogen out of the air and to provide nitrogen free oxygen for combustion as discussed below. The dry air will contain, by weight, 23.1% oxygen, 75.6% nitrogen, 1.285% argon and small traces of
 35 hydrogen, helium, neon, krypton and xenon (total of .0013%). Argon has a liquefaction temperature of 157.5°R, which lies between the nitrogen and oxygen boiling points of 139.9°R and 162.4°R respectively. Therefore argon, which is not removed, will liquefy during the liquefaction process. The remaining traces of gases hydrogen, helium and neon are incondensable

at temperatures above 49°R while krypton and xenon will liquefy; however, the trace amounts of these latter gases is considered insignificant to the following air liquefaction process.

The dry air then exits through duct 23 and enters the turboexpander 24 where the air temperature is further reduced to near liquid air temperature prior to exiting duct 25 and enters the rectifier 60 (a two column type design is shown). Within the rectifier, if not before, the air is cooled to below the oxygen liquefaction temperature. Preferably, a two column type rectifier 60 is utilized such as that described in detail in the work: The Physical Principles of Gas Liquefaction and Low Temperature Rectification, Davies, first (published by Longmans, Green and Co. 1949).

The air exits from the lower rectifier heat exchanger 26 through duct 27 at liquid air temperature and enters the rectifier's lower column plates where the oxygen/nitrogen separation is initiated. Liquid with about 40% oxygen exits through duct 28 and enters the upper rectifier column where a higher percentage oxygen concentration is generated. Liquid nitrogen at 96% purity is recirculated from the lower rectifier column to the upper column by means of duct 29. Gaseous nitrogen at 99% purity (1% argon) exits through duct 31 and enters heat exchanger 40 where cooling of the incoming air is performed prior to discharging through duct 32 to the atmosphere at near ambient temperature and pressure. Gaseous or liquid oxygen at 95% purity (5% argon) exits through duct 33 and enters the turboexpander compressor 34 where the oxygen is pressurized to the design pressure. The high pressure oxygen then exits through duct 35 and enters the gas generator 70.

A light hydrocarbon fuel (methane, propane, purified natural gas and light alcohols such as ethanol and methanol) exits the fuel supply tank 37 through duct 38 and enters the reciprocating engine cylinder 39 where the fuel is raised to the design discharge pressure. The fuel then exits through duct 41 and enters the gas generator 70 to be mixed with the incoming oxygen at the stoichiometric mixture ratio to achieve complete combustion and maximum hot gas temperature (approximately 6500°R). The gas generator includes an ignition device, such as a spark plug, to initiate combustion. While the gas generator 70 is the preferred form of fuel combustion device for this embodiment, other fuel combustion devices could also be used, such as those discussed in the alternative embodiments below. The products of combustion of these reactants result in a high purity steam and carbon dioxide gas and a small amount of gaseous argon (4%).

Following the complete combustion of the high temperature gases, recirculating water is injected into the gas generator 70 through line 42 and dilutes the high temperature gases to a lower temperature drive gas acceptable to the reciprocating engine (approximately 2000°R). This water influx also increases a mass flow rate of combustion products available for expansion and power generation. The drive gas then exits the gas generator 70 through discharge duct 43, enters reciprocating cylinder 44, expands and provides power to the power transmission 30. Other combustion product expansion devices can replace the reciprocating cylinder 44, such as the dynamic turbines discussed in the sixth embodiment below. The gas exits through duct 45, enters the second cylinder 46, expands and also provides power to the power transmission; the gas exits through duct 47 and powers the dynamic turbine 48 which drives the centrifugal compressor 2,

which was driven by the electric motor 140 during start-up, and the alternator 120 to recharge the battery 130.

The gas then exits through duct 49, enters the water heater 100 where residual heat in the gas is transferred to the recirculating water being pumped by pump 90, the water heater gas exits through duct 51, enters the condenser 80 at near or below atmospheric pressure, where condensation of the steam into water and separation of the carbon dioxide takes place. The condensed water exits through line 52, enters the pump 90 where the pressure of the water is raised to the gas generator 70 supply pressure level. A major portion of the pump 90 discharge water exits through line 53, enters the water heater 100 where heat is transferred from the turbine 48 exhaust gas and then exits through line 42 for delivery to the gas generator 70. The remaining water from the discharge of pump 90 exits through duct 54 and is sprayed through nozzles 55 into radiator 110 (evaporative cooling). Coolant for the condenser gases is recirculated through duct 56 to the radiator 110 where heat is rejected to atmospheric air being pumped by fan 57.

The gaseous carbon dioxide, remaining after the condensation of the steam, exits the condenser 80 through duct 58 and enters the reciprocating cylinder 59, (when the condenser pressure is below atmospheric) compressed to slightly above atmospheric pressure and discharged through duct 61. The compressed carbon dioxide can be stored in storage tank 62 and converted to a solid or liquid state for periodic removal; or the gas can be discharged into the atmosphere when such expulsion is permitted.

It should be noted that this hybrid engine generates its own water requirements upon demand and thus eliminates the freezing problem of a steam Rankine cycle in a cold (below freezing) environment. Also, the engine generates its oxidizer requirements on demand and thus eliminates many safety concerns regarding oxygen storage.

A second embodiment of this invention, illustrated in Fig. 2, features a hybrid engine when using hydrogen in place of a hydrocarbon fuel. When using hydrogen as the fuel no carbon dioxide is generated and only high purity steam exits from the gas generator 70. Consequently all systems related to carbon dioxide are deleted, and no other changes are basically required. However, to maintain the same six cylinder engine of Fig. 1, the hydrogen fuel Fig. 2 exits the fuel supply tank 37 through duct 63, enters reciprocating engine cylinder 59, exits through duct 64, enters reciprocating engine cylinder 39, exits through duct 41 and is delivered to the gas generator 70. This permits two stages of compression for the low density hydrogen.

A third embodiment of this invention, illustrated in Fig. 3, features a dual cycle engine where a Brayton cycle is used for start-up and chill-down of the air liquefaction equipment (Mode I) and a Rankine cycle is used for cruise, idle and continuous duty (Mode II). To incorporate this feature, high pressure air is tapped-off from cylinder 13 (air pressurization as previously described for embodiment one) by means of bypass air duct 71 and modulated by valve 72. Also, recirculating water to the gas generator is modulated by means of valve 73 to control the combustion temperature of the fuel and oxygen and the exit temperature of the gaseous mixture being delivered

to power the cycle through duct 43.

The thermodynamic cycles for these two operating Modes are illustrated in Fig. 4 and Fig. 5. The working fluid for power cycle operation in Mode I consists of steam, carbon dioxide and gaseous air. When operating in Mode II the working fluid (as discussed in embodiment one and two) consists of steam and carbon dioxide when using hydrocarbon fuel and steam only when using hydrogen.

An open Brayton cycle, illustrated in Fig. 4, with two stages of intercooling the compressed air, 74a, and 74b, is used to power the engine during Mode I and initiates the chill-down of the liquefaction equipment for subsequent Mode II operation of the Rankine cycle with regeneration 75, illustrated in Fig. 5. Note that this embodiment eliminates the need for an electric motor, battery and alternator.

A fourth embodiment of this invention, illustrated in Fig. 6, includes all the elements of the first embodiment and adds two reheaters 150 and 160 to improve the performance of this engine. While two reheaters 150, 160 are shown, any number of reheaters can be utilized depending on the requirements of each specific application.

The engine operates as described for the first embodiment but with the following changes. Hot gases exiting reciprocating cylinder 44 exit through duct 81, enter the reheater 150 where additional light hydrocarbon fuel and oxygen is injected through ducts 88 and 89 respectively. The heat of combustion of these reactants within the reheater 150 raises the incoming gas temperature to the level of the gas generator 70 output. The reheated gas then exits reheater 150 through duct 82, enters reciprocating cylinder 46, expands and exits through duct 83 and enters reheater 160 where additional oxygen and fuel is injected. The heat of combustion of these reactants within the reheater 160 again raises the incoming gas temperature to the same level as at the gas generator 70 output. The heated gas then exits through duct 84 and enters the dynamic turbine 48, as described previously in the first embodiment. Fuel for the reheater 160 is supplied through duct 86. The oxygen is supplied through duct 87.

A fifth embodiment of this invention, illustrated in Fig. 7, includes all the elements of the second embodiment and adds two reheaters 150 and 160 to improve the performance. This engine operates as described for embodiment four except this engine uses hydrogen fuel. The Rankine cycle of these embodiments using regeneration and reheats is illustrated in Fig. 8. Regeneration is illustrated by 91 and the two reheats are illustrated by 92a and 92b.

A sixth embodiment of this invention; illustrated in Fig. 9, is similar to the fourth embodiment featuring reheaters, illustrated in Fig. 6, except all the machinery consists of dynamic type compressors and turbines. This type of machinery is more suitable for higher power levels (>1000 Shaft Horsepower (SHP)) required for rail, ship or standby power systems.

The Rankine engine consists of dynamic turbocompressors 200, 210, and 220, a power transmission 230, a heat exchanger 240, a turboexpander 250, a rectifier 260, a gas generator 270, a first reheater 280, a second reheater 290, a water heater 300, a condenser 310, a recirculating

pump 320 and a condenser coolant radiator 330. The electric engine consists of an alternator 400, a battery 410 and electric motor 420.

Engine operation begins by starting the electric motor 420 using the battery 410 as the energy source. The electric motor 420 drives the dynamic compressor 201 through power transmission 230, and simultaneously, valve 202 is opened and valve 203 is closed. This initiates the start of the engine in a Brayton cycle mode. As engine speed increases valve 202 is gradually closed and valve 203 is gradually opened to slowly transition into the Rankine cycle mode and permit the liquefaction equipment to chill down. During this transitional period the electric motor 420 is used to maintain scheduled power and speed until steady state Rankine cycle conditions are achieved.

During thermal engine activation air enters turbocompressor 201 through duct 204 and is raised to the design discharge pressure. The air then exits through duct 205 into intercooler 206 where the heat of compression is removed by external cooling means 207 (i.e. air, water, Freon, etc.). Condensed water vapor is tapped-off by drain 208. After the air exits intercooler 206 through duct 209 at a temperature equal to the compressor inlet, it enters compressor 211 and is raised to the design discharge pressure. The air then exits through duct 212 into intercooler 213 and is again cooled to the inlet temperature of the compressor 201. This compression/cooling cycle is repeated as the air exits intercooler 213 through duct 214, enters compressor 215, then exits through duct 216, enters intercooler 217 and exits through duct 218 to complete the air pressurization.

The high pressure ambient temperature air then enters scrubber 219 where gases and fluids that are subject to freezing during the liquefaction process are removed (i.e. carbon dioxide, water vapor and oil). Carbon dioxide exits through duct 221a and is processed and stored in reservoir 221b. Oil is drained through duct 222a and stored in reservoir 222b. Water vapor is drained through duct 223 and discharged overboard.

The dry air then exits through duct 224 and enters the heat exchanger 240 where the air is cooled by returning gaseous nitrogen. It then exits through duct 225 and enters turboexpander 226 where the air temperature is further reduced to near liquid air temperature prior to exiting through duct 227 and enters the rectifier 260. The air exits from the rectifier heat exchanger 228 through duct 229 at liquid air temperature and enters the rectifier's lower column plates where oxygen/nitrogen separation is initiated. Liquid with 40% oxygen exits through duct 231 and enters the upper rectifier column where a higher percentage oxygen concentration is generated. Liquid nitrogen at 96% purity is recirculated from the lower rectifier column to the upper column by means of duct 232. Gaseous nitrogen at 99% purity (1% argon) exits through duct 233 and enters the heat exchanger 240 where cooling the incoming dry air is performed prior to discharging through duct 234 to the atmosphere at near ambient temperature and pressure. Gaseous oxygen or liquid oxygen at 95% purity (5% argon) exits through duct 235 and enters the turboexpander compressor 236 where the oxygen is pressurized to the design pressure. The high pressure oxygen then exits through duct 237 and enters the gas generator 270 through duct 238.

Fuel, i.e. methane, propane, purified natural gas and light alcohols such as methanol and ethanol, exits the fuel supply tank 239 through duct 241 and enters the compressor 242 of turboexpander 250 and is raised to the design discharge pressure. The pressurized fuel then exits through duct 243 and enters the gas generator 270 through duct 244 where it mixes with the
5 incoming oxygen at stoichiometric mixture ratio to achieve complete combustion and maximum hot gas temperature (approximately 6500°R). The products of combustion of these reactants result in a high purity steam, carbon dioxide gas and a small amount of gaseous argon (4%).

Following complete combustion of the high temperature gases, recirculating water is injected into the gas generator through line 245 and dilutes the high temperature gases to a lower
10 temperature drive gas acceptable to the dynamic turbine 247 (approximately 2000°R). The drive gas then exits the gas generator 270 through duct 246 and enters the turbine 247 of turbocompressor 220, where the gas expands and powers the air compressor 215 and the carbon dioxide compressor 273. The gas then exits through duct 248 and enters reheater 280 where the heat extracted due to the turbine 247 work is replenished. This heat is derived from the
15 combustion of added fuel through duct 249 and added oxygen through duct 251 into reheater 280.

The reheated gas then exits through duct 252 and enters turbine 253 of turbocompressor 210 and expands to lower pressure. The power produced by these expanding gases drive the alternator 400 and compressor 211, then exhaust through duct 254 and enter reheater 290. The heat extracted from the gases resulting in the turbine work is replenished with the heat of combustion
20 from added fuel through duct 255 and oxygen through duct 256.

The reheated gas then exits through duct 257, enters turbine 258 of turbocompressor 200 and drives compressor 201 and power transmission 230. The turbine exhaust gas then exits through duct 259 and enters water heater 300 where the residual heat of the turbine 258 exhaust is used to preheat the water that is being recirculated to the gas generator 270. The gas then exits through
25 duct 261, enters the condenser 310 near or below atmospheric pressure, where condensation of the steam into water and separation of the carbon dioxide gas occurs.

The condensed water exits through line 262, enters the pump 263 where the pressure is raised to the supply level of the gas generator 270. A major portion of the discharge water from pump 263 exits through line 264, enters the water heater 300 where heat is absorbed from the turbine
30 exhaust gas and then exists through line 245 for delivery to the gas generator 270. The remaining water from the discharge of pump 263 exits through line 265 and is sprayed through nozzles 266 into radiator 330 for evaporative cooling. Coolant for the condenser gas is recirculated by pump 267 to the radiator 330 through line 268, where heat is rejected to atmospheric air being pumped by fan 269.

35 The gaseous carbon dioxide, remaining from the condensation of steam, exits through duct 271 and enters compressor 273 of turbocompressor 220 and is compressed to slightly above atmospheric pressure (when condenser pressure is below atmospheric) and discharged through duct 274 into storage tank 275. The compressed carbon dioxide can be converted into a liquid or

solid state for periodic removal, or the gas can be discharged into the atmosphere as local environmental laws permit.

The seventh embodiment of this invention, illustrated in Fig. 10, includes the liquefaction system of the previous embodiments but utilizes the intermittent but spontaneous combustion process of the Otto cycle as the thermal power engine. This embodiment eliminates the need for the steam condenser and the recirculating water system.

The Otto cycle steam or steam/CO₂ thermal engine consists of, in addition to the liquefaction system previously described, a premixer 430 where oxygen from duct 35, fuel from duct 41 and recirculating steam or steam/CO₂ from duct 301 are premixed in the approximate ratio of 20%, 5% and 75% by weight respectively. These premixed gases are then directed to the reciprocating pistons 302 through duct 303 and ducts 304 where they are compressed and ignited with a spark ignition system identical to current Otto cycle engines. After the power stroke, the steam or steam/CO₂ gases are discharged to the dynamic turbine 48 through ducts 305, 306 and then into duct 47. Some of the discharge gases are directed back to the premixer 430 through duct 301. The exhaust gases from the dynamic turbine 48 are then discharged to the atmosphere through duct 307.

The eighth embodiment of this invention, illustrated in Fig. 11, is similar to the seventh embodiment, except a Diesel power cycle is used. In this system a premixer 440 mixes the oxygen from duct 35 with steam or steam/CO₂ from duct 308, at an approximate mixture ratio of 23% and 77% by weight respectively, and discharges the gaseous mixture to the reciprocating pistons 309 through duct 311 and ducts 312 where the mixture is compressed to a high pre-ignition temperature. The high pressure fuel, at approximately 5% of the total weight of the gas mixture in the piston cylinder, is injected through ducts 313 and burns at approximately constant pressure. If necessary, an ignition device is located within the combustion cylinder. The hot gases then rapidly expand as the piston moves to the bottom of its power stroke. The steam/CO₂ gases are then discharged into ducts 313 and delivered to the dynamic turbine 48 through duct 47. Some of the discharged gases are diverted to the premixer 440 through the duct 308. The exhaust gases from the dynamic turbine 48 are then discharged into the atmosphere through duct 307.

Figure 12 depicts a basic low-polluting engine 500 which conceptually represents many of the above-described first eight embodiments in a more simplified manner. Rather than identifying specific machinery, Fig. 12 depicts steps in the overall power production cycle. Additionally, the engine 500 of Fig. 12 replaces the rectifier and other liquefaction equipment of embodiments 1-8 with a more generalized air separation plant 530. Details of various different embodiments of this air separation plant 530 are provided in Figs. 15 and 16 and described in detail herein below.

The basic low-polluting engine 500 operates in the following manner. Air from a surrounding environment enters through an air inlet 510 into an air compressor 520. The air compressor 520 elevates the air entering through the air inlet 510 and directs the compressed air to the air separation plant 530. Various different air separation techniques can be utilized by the air separation plant

530 so that enriched nitrogen gases exit the air separation plant 530 through an enriched nitrogen gas outlet 532 and enriched oxygen gases exit the air separation plant 530 through an enriched oxygen gases outlet 534. The enriched nitrogen gases outlet 532 typically returns back into the surrounding environment. The enriched oxygen gases outlet 534 leads to the combustion device 550.

In the combustion device 550, the enriched oxygen gases from the air separation plant 530 are combined with the hydrogen containing fuel from a fuel supply 540 and combustion is initiated within the combustion device 550. A water or carbon dioxide diluent is added into the combustion device to decrease a temperature of the products of combustion within the combustion device 550 and to increase a mass flow rate for a steam or steam and carbon dioxide working fluid exiting the combustion device 550.

This working fluid is then directed into an expander 560, such as a turbine. The turbine is coupled through a power transfer coupling 562 to the air compressor 520 to drive the air compressor 520. Figure 12 shows a rotating shaft as one type of mechanical power transfer coupling 562. Another way to power the air compressor 520 is to generate electricity by means of the power absorber 570 and use part of the generated electricity to drive an electric motor which in turn powers the air compressor 520. The expander 560 also is coupled through a power transfer coupling 564 to a power absorber 570 such as an electric generator or a power transmission for a vehicle. The expander 560 is also coupled through a power transfer coupling 566 to the air separation plant 530 to drive machinery within the air separation plant 530.

The working fluid is then discharged from the expander 560 through a discharge 572. The discharge 572 leads to a condenser 580. The condenser has coolant passing through a coolant flow path 592 which causes water portions of the working fluid entering the condenser 580 to be condensed. A water and carbon dioxide outlet 590 is provided for excess water or water and carbon dioxide mixture from the condenser. A water or water and carbon dioxide diluent path is also provided out of the condenser 580 for returning water or water and carbon dioxide diluent back to the combustion device 550.

As should be readily apparent, the air compressor 520 is generally analogous to the turbocompressor 10 of the first embodiment. The air separation plant 530 is generally analogous to the rectifier 60 of the first embodiment. The fuel supply 540 is generally analogous to the fuel supply tank 37 of the first embodiment. The combustion device 550 is generally analogous to the gas generator 70 of the first embodiment. The expander 560 is generally analogous to the reciprocating cylinders 44, 46 of the reciprocating engine 20 of the first embodiment. The power absorber 570 is generally analogous to the power transmission 30 of the first embodiment and the condenser 580 is generally analogous to the condenser 80 of the first embodiment. Hence, the basic low-polluting engine schematic of Fig. 12 represented by reference numeral 500 merely provides an overall depiction of the power production cycle of this invention. While a specific analogy has been drawn between this basic low-polluting engine 500 and the first embodiment,

shown in Fig. 1, similar analogies can be drawn to the other embodiments of this invention.

With particular reference to Fig. 13, details of a basic low-polluting engine 600 featuring regeneration is provided. The low-polluting engine featuring regeneration 600 depicted in Fig. 13 is identical to the basic low-polluting engine 500 of Fig. 12 except that handling of the working fluid upon discharge from the expander 660 has been altered to feature regeneration. Specifically, the low-polluting engine featuring regeneration 600 includes an air inlet 610, air compressor 620, air separation plant 630, fuel supply 640, combustion device 650, expander 660 and power absorber 670 arranged similarly to the components 510, 520, 530, 540, 550, 560, 570 of the basic low-polluting engine 500 shown in Fig. 12.

In contrast, the low-polluting engine featuring regeneration 600 directs the working fluid through a discharge 672 which leads to a regenerator 674. The working fluid exits the regenerator 674 through a regenerator outlet 676. The regenerator outlet 676 leads to a condenser 680. Within the condenser 680, the working fluid is cooled by action of a coolant flowing along a coolant flow path 682 to be separated into carbon dioxide and water. The carbon dioxide exits the condenser 680 through a carbon dioxide outlet 684 and the water exits the condenser 680 through the water outlet 686. The water outlet 686 leads to a feed water pump 688. Excess water is discharged from the engine 600 at a water excess outlet 690. Other portions of the water are directed along a regenerator water flow path 692 through the regenerator 674 where the water is preheated. The water or steam leaves the regenerator 674 along a water diluent path 694 leading back to the combustion device 650.

The carbon dioxide outlet 684 from the condenser 680 also leads into the regenerator 674 for preheating of the carbon dioxide. The carbon dioxide leaves the regenerator along a regenerator carbon dioxide flow 696 which leads to a carbon dioxide compressor 697. The carbon dioxide compressor 697 in turn leads to a carbon dioxide excess outlet 698 where excess carbon dioxide is removed from the engine 600. If desired, a portion of the carbon dioxide can be directed along a carbon dioxide diluent path 699 back to the combustion device 650 for use as a diluent within the combustion device 650.

With particular reference to Fig. 14, a basic low-polluting engine 700 with bottoming cycle is provided. As with the low-polluting engine featuring regeneration 600 of Fig. 13, portions of the low-polluting engine featuring a bottoming cycle 700 are similar to the basic low-polluting engine 500 of Fig. 12 up until discharge of the working fluid from the expander 560. Hence, the low-polluting engine featuring a bottoming cycle 700 includes an air inlet 710, air compressor 720, air separation plant 730, fuel supply 740, combustion device 750, expander 760 and power absorber 770 having corresponding components in the engine 500 of Fig. 12.

The working fluid is discharged from the expander 760 through a discharge 772 leading to a Heat Recovery Steam Generator (HRSG)/condenser 774. The working fluid is condensed and a water outlet 775 directs water from the condenser 774 and a carbon dioxide outlet 776 directs carbon dioxide from the condenser 774. The carbon dioxide outlet 776 leads to a carbon dioxide

compressor 777, a carbon dioxide excess outlet 778 and carbon dioxide diluent path 779 leading back to the combustion device 750.

5 The water outlet 775 leads to a feed water pump 780 which in turn leads to a water excess outlet 781 and a water regeneration path 782 where the water is regenerated within a bottoming regenerator 787. The water exits the bottoming regenerator 787 along a water diluent path 783 leading back to the combustion device 750.

10 The HRSG/condenser 774 and regenerator 787 are driven by a bottoming cycle including a bottoming cycle boiler 784 which boils water in the bottoming cycle from the discharge working fluid from the discharge 772 and entering the HRSG/condenser 774. The topping cycle also includes a bottoming turbine 786 and a bottoming regenerator 787 which cools steam exiting the steam turbine 786 and heats water entering the water diluent path 783. The bottoming cycle also includes a bottoming condenser 788 cooled by a coolant within a coolant line 789. Hence, the working fluid such as water within the bottoming cycle passes from the condenser 788 to the boiler 784 where the working fluid is heated and turned into a gas. Note that the HRSG/condenser 15 774 and boiler 784 are integrated together but that only heat exchange is allowed, not mixing. The bottoming cycle working fluid then passes through the turbine 786 for production of power which can be directed to the power absorber 770 or other components of the low-polluting engine featuring a bottoming cycle 700. The working fluid then exits the turbine 786 and is cooled in the regenerator 787 before returning to the condenser 788.

20 The air separation plants 530, 630, 730 of Figs. 12-14 can be any of a variety of different apparatuses or systems which are capable of removing at least a portion of the nitrogen from air. For instance, and specifically discussed above with respect to the first through eighth embodiments of Figs. 1-11, the air separation plant 530, 630, 730 can include a rectifier such as the rectifier 60 of Fig. 1 or other liquefaction equipment which separate nitrogen from the air by liquefaction.

25 However, liquefaction processes are not the only processes that can remove at least a portion of nitrogen from air. Several other processes are available to achieve this goal. These processes, which are described in detail below, can be substituted for the cryogenic liquefaction process described in detail hereinabove. One alternative technique available for use in the air separation plant 530, 630, 730 is a pressure swing adsorption plant 800 (Fig. 15). The pressure swing 30 adsorption process, also called vacuum pressure swing adsorption, uses materials which are capable of adsorption and desorption of oxygen or nitrogen such as, for example, synthetic zeolites. The vacuum pressure swing adsorption process can be used to separate oxygen and nitrogen from air.

35 The process typically employs two beds that go through swings in pressure from above atmospheric to below atmospheric pressure. Each bed cycles sequentially from adsorption to desorption and regeneration and back to adsorption. The two beds operate in a staggered arrangement in which one bed is adsorbing while the other bed is regenerating. Thus the beds alternately produce a gaseous product of high oxygen content. With this process, a gaseous

mixture can be produced with a wide range of oxygen purities. As an example, oxygen purities ranging from 90% to 94% are used in many industrial applications and can be successfully produced with commercially available vacuum pressure swing adsorption processes such as those produced by Praxair, Inc. with world headquarters located at 39 Old Ridgebury Road, Danbury,
5 Connecticut 06810-5113.

With particular reference to Fig. 15, a layout of a typical pressure swing adsorption plant 800 is shown. Initially, the air inlet 510 and feed compressor 520 are provided analogous to the air inlet 510 and air compressor 520 of the basic low-polluting engine schematic 500 shown in Fig. 12. Preferably, a filter 515 is interposed between the air inlet and the feed compressor to filter
10 particulates out of the air inlet stream. The compressed air discharged from the feed compressor 520 is directed to a first inlet line 810 passing through a first inlet line valve 815 and into a first enclosure 820.

The first enclosure 820 is provided with an appropriate material capable of adsorption and desorption of oxygen or nitrogen. One material that is used in these applications is zeolite. Two
15 outlets are provided from the first enclosure 820 including a first oxygen outlet 830 coupled to the first enclosure 820 through a first valve 832 and a first nitrogen outlet 835 coupled to the first enclosure 820 through a first nitrogen valve 836. The first nitrogen outlet 835 leads to a nitrogen compressor 837 which raises the gases in the first nitrogen outlet 835 back to atmospheric pressure for discharge through nitrogen discharge 839. In fact, the first nitrogen outlet 835 and first
20 oxygen outlet 830 do not contain pure oxygen or nitrogen but rather merely gases which are enriched in content with oxygen or nitrogen.

The first oxygen outlet 830 leads to a surge tank 870 with a valve 875 beyond the surge tank 870 and leading to an oxygen supply line 880. In parallel with the first enclosure 820, a second enclosure 850 is provided. The second enclosure 850 is similarly loaded with an appropriate
25 material capable of adsorption and desorption of oxygen or nitrogen. A second inlet line 840 leads from the feed compressor 520 through a second inlet line valve 845 and into the second enclosure 850. A second oxygen outlet 860 leads out of the second enclosure 850 and on to the surge tank 870 through a second oxygen outlet valve 862. A second nitrogen outlet 865 also leads out of the second enclosure 850 through a second nitrogen outlet valve 866 and on to the compressor 837. A
30 cycle controller 890 controls the opening and closing of the various valves 815, 832, 836, 845, 862, 866 and 875.

One typical operation sequence of the pressure swing adsorption plant 800 is as follows. Initially, all of the valves are closed except for the first nitrogen valve 836 and the nitrogen compressor 837 is used to reduce pressure in the first enclosure 820 to below atmospheric
35 pressure. The first nitrogen valve 836 is then closed. Next, the first inlet valve 815 is opened. With the first inlet line valve 815 open and all other valves closed, the feed compressor directs air into the first enclosure 820.

As pressure builds up within the first enclosure 820, the material within the first enclosure 820 is caused to adsorb different molecules within the air in a discriminate fashion. For instance, the material can be selected to adsorb nitrogen at elevated pressure. At reduced pressure, the adsorption effect reverses to desorption.

5 In essence, if the material adsorbs nitrogen at pressures elevated above atmospheric pressure and desorbs nitrogen at pressures below atmospheric pressure, the various valves 815, 832, 836 and 875 are sequentially operated so that the first enclosure 820 has an elevated pressure and adsorbs nitrogen before the remaining enriched oxygen air is allowed to freely flow out of the first enclosure 820 along the first oxygen outlet 830. When the oxygen enclosure 820 has a pressure
10 below atmospheric pressure, the material within the first enclosure 820 is desorbing the nitrogen while the first nitrogen outlet valve 836 is open. In this way, when nitrogen is being adsorbed, the remaining air within the first enclosure 820 is enriched in oxygen and is directed to the first oxygen outlet 830 and when the material within the enclosure 820 is desorbing the nitrogen, the nitrogen enriched gases within the first enclosure 820 are allowed to flow into the first nitrogen outlet 835
15 and to the nitrogen discharge 839.

The zeolite material within the enclosure 820 benefits from some residence time to adsorb as much nitrogen (or oxygen) as desired. During this time no oxygen rich or nitrogen rich gases flow to the oxygen supply line 880 or the nitrogen discharge 839. Hence, it is beneficial to use a second enclosure 850 similar to the first enclosure 820 while the valves 815, 832 and 836 are all
20 closed and the zeolite material in the first enclosure 820 is adsorbing nitrogen (or oxygen).

Specifically the valves 845, 862 and 866 are sequentially opened and closed to cause the second enclosure 850 to operate in a manner similar to that outlined with reference to the first enclosure 820 above. When the material within the second enclosure 850 is adsorbing nitrogen (or oxygen) the process is reversed so that the first enclosure 820, having had its zeolite material
25 appropriately desorbed, is brought back on line for repetition of the alternating pattern of use between the first enclosure 820 and the second enclosure 850. As should be apparent, additional enclosures besides the first enclosure 820 and second enclosure 850 could be utilized if the adsorbing material requires more residence time or to increase the overall throughput of oxygen enriched gases from the air. Over time, the material within the first enclosure 820 which adsorbs
30 and desorbs the oxygen or nitrogen tends to lose its effectiveness. The material can be regenerated, if it is in the form of a synthetic zeolite, by application of heat or other regeneration means. Accordingly, when the material within the first enclosure 820 begins to lose its effectiveness, such a heat treatment can be performed or the zeolite material replaced. Should the
35 adsorbing material be configured to adsorb and desorb oxygen rather than nitrogen, the above-described operation of the pressure swing adsorption plant 800 would be adjusted to provide the desired separation of oxygen from nitrogen.

With particular reference to Fig. 16, details of an alternative apparatus and system for use within the air separation plants 530, 630, 730 is provided. In such membrane-based air separation

systems 900 the separation of air into its components is achieved by passing an air feed stream under pressure over a membrane. The pressure gradient across the membrane causes the most permeable component to pass through the membrane more rapidly than other components, thereby creating a product stream that is enriched in this component while the feed stream is depleted in this component.

The transport of the air through a membrane can follow several physical processes. As an example, these processes could be: 1) Knudsen flow separation which is based on molecular weight differences between the gases; 2) Ultramicroporous molecular sieving separation; and 3) Solution-diffusion separation which is based both on solubility and mobility factors. In the case of a solution-diffusion process the air first dissolves in a polymer, then diffuses through its thickness and then evaporates from the other side into the product stream.

Several types of membranes are available for this process, each having specific advantages in particular situations. For example, cellulose acetate membranes exhibit good separation factors for oxygen and nitrogen, but have low flux rates. Thin film composite membranes placed over microporous polysulfone exhibits lower separation factors than cellulose acetate, but have a higher flux at the same pressure differential. Repeating the process in a series configuration can increase the oxygen concentration in the product stream. For example, one industrial membrane, in two passes, may enrich the oxygen content of air to about 50%.

The above described membrane processes operate at a temperature that is near ambient temperature. A higher-than-ambient temperature may arise as a result of a possible temperature rise resulting from pressurization of the air feed stream to create a pressure difference across the membrane.

Still another membrane separation process uses an electroceramic membrane. Electroceramics are ionic solid solutions that permit movement of ions. To become appreciably mobile, the oxide ion, because of its size and charge, requires a high temperature (about 800°F) to overcome the solid oxide lattice energy. The electroceramic membrane process integrates well with the production of power described in this invention because the power generating process produces waste heat that can be used to generate the required operating temperature of the membrane. For instance, and with reference to Fig. 12, the expander 560 and gas generator 550 can be configured such that the working fluid exiting the expander 560 at the discharge 572 has a temperature at or above 800°F. The working fluid can then be routed to a heat exchanger which heats the electroceramic membranes to 800°F for use in the air development system 530.

The oxygen ions move through the lattice because of a gradient in pressure across the membrane. On the high oxygen partial pressure side of the membrane, oxygen is reduced when it receives four electrons and occupies two vacancies. At the low oxygen partial pressure side, vacancies are created by the reverse reaction. Oxide ions at the low partial pressure side can be removed by liberation of oxygen. The rate of diffusion through the membrane is determined by ion mobility. This mobility is a characteristic of a particular material, and is dependent on the size,

charge and geometry of the cations in the lattice. A possible material for formation of the electroceramic membrane is yttria stabilized zirconia.

With particular reference to Fig. 16, one arrangement for the membrane based air separation system for use in the air separation plants 530, 630, 730 is depicted by reference numeral 900. In this embodiment for the air separation plant, an air inlet 510 and feed compressor 520 are provided similar to the air inlet 510 and feed compressor 520 disclosed in Fig. 12 with regard to the basic low-polluting engine 500. The compressed air is then directed to a junction 910 where return flows from various membrane chambers return for reprocessing and are combined together within the junction 910. A junction outlet 915 provides the only outlet from the junction 910. The junction outlet 915 leads to a first membrane enclosure 920.

The first membrane enclosure 920 is preferably an enclosure which has an inlet and a membrane dividing the enclosure into two regions. Two outlets are provided in the enclosure. One of the outlets is on the same side of the membrane as the inlet and the other outlet is located on a side of the membrane opposite the inlet. If the membrane is of a type which allows oxygen to pass more readily there through than nitrogen, an oxygen rich outlet 924 is located on the downstream side of the membrane and a nitrogen rich outlet 926 is located on a same side of the membrane as the inlet 915. If the membrane allows nitrogen to pass more readily there through, the arrangement of the outlets is reversed.

The junction outlet 915 passes into the first membrane enclosure 920 through the inlet in the first membrane enclosure 920. Because oxygen flows more readily through the membrane within the first membrane enclosure 920, gases flowing through the oxygen rich outlet 924 have an increased percentage of oxygen with respect to standard atmospheric oxygen percentages and the nitrogen rich outlet 926 has a nitrogen content which is greater than that of standard atmospheric conditions.

The oxygen rich outlet 924 leads to a second membrane enclosure 930 where it enters the second membrane enclosure 930 through an oxygen rich inlet 932. The second membrane enclosure 930 is arranged similarly to the first membrane enclosure 920. Hence, a membrane is provided within the second membrane enclosure 930 and two outlets are provided including an oxygen super rich outlet 934 on a side of the membrane opposite the oxygen rich inlet 932 and a second outlet 938 located on a common side of the membrane within the second membrane enclosure 930 as the oxygen rich inlet 932.

The oxygen super rich outlet 934 leads to an oxygen supply 936 for use within one of the engines 500, 600, 700 discussed above. The gases flowing through the second outlet 938 typically have oxygen and nitrogen contents matching that of standard atmospheric conditions but maintaining an elevated pressure. The second outlet 938 returns back to the junction 910 for combining with air exiting the feed compressor 520 and for repassing through the first membrane enclosure 920 as discussed above.

The nitrogen rich outlet 926 exiting the first membrane enclosure 920 is passed to a third membrane enclosure 940 where it enters the third membrane enclosure 940 through a nitrogen rich inlet 942. The third membrane enclosure 940 is similarly arranged to the first membrane enclosure 920 and second membrane enclosure 930 such that a membrane is located within the third
5 membrane enclosure 940 and two outlets are provided from the third membrane enclosure 940. One of the outlets is a nitrogen super rich outlet 944 on a side of the membrane within the third membrane enclosure 940 similar to that of the nitrogen rich inlet 942. The nitrogen super rich outlet 944 can lead to a surrounding atmosphere or be used for processes where a high nitrogen content gas is desirable.

10 A third permeate return 948 provides an outlet from the third membrane enclosure 940 which is on a side of the membrane within the third membrane enclosure 940 opposite the location of the nitrogen rich inlet 942. The third permeate return 948 leads back to the junction 910 for reprocessing of the still pressurized air exiting the third membrane enclosure 940 through the third permeate return 948. This air passing through the third permeate return 948 is typically similar in
15 content to the second permeate return 938 and the air exiting the feed compressor 520.

While many different types of membranes can be utilized within the first membrane enclosure 920, second membrane enclosure 930 and third membrane enclosure 940, the type of membrane would typically not alter the general arrangement of the membrane enclosures 920, 930, 940 and conduits for directing gases between the various permeates 920, 930, 940 and other components
20 of the membrane based air separation plant 900 of Fig. 16.

While various different techniques have been disclosed for separation of nitrogen and oxygen from air, this description is not provided to identify every possible air separation process or apparatus. For example, economic and other consideration may make application of combinations of the above described processes advantageous. Rather, these examples are presented to indicate
25 that several separation processes are available to accomplish the goal of enriching the oxygen content of air supplied to a combustion device and decreasing a corresponding nitrogen content of the air supply to a combustion device. By reducing an amount of nitrogen passing into a combustion device such as these combustion devices 550, 650, 750, an amount of nitrogen oxides produced as products of combustion within the combustion device 550, 650, 750 is reduced and
30 low-pollution combustion based power production results.

Moreover, having thus described the invention it should now be apparent that various different modifications could be resorted to without departing from the scope of the invention as disclosed herein and as identified in the included claims. The above description is provided to disclose the best mode for practicing this invention and to enable one skilled in the art to practice this invention
35 but should not be construed to limit the scope of the invention disclosed herein.

Industrial Applicability

This invention exhibits industrial applicability in that it provides a low or zero pollution combustion based power generation system. Such a system can be used in transportation and stationary power environments. Many countries' governments regulate the amount of pollution which can be generated by power generation system. This invention addresses the need for reduced pollution combustion based power generation systems.

Another object of this invention is to provide a high efficiency combustion based power generation system.

Another object of the present invention is to provide a power generation system which can also produce water as a byproduct. In areas where water is scarce the water byproducts produced by this invention are particularly beneficial.

Another object of the present invention is to provide a combustion based power generation system which includes an air treatment plant for separating nitrogen from the air prior to use of the air to combust a hydrocarbon fuel, such that nitrogen oxides are reduced or eliminated as byproducts of combustion in the power generation system.

Other further objects of this invention, which demonstrate its industrial applicability, will become apparent upon a careful reading of the included description of the invention and review of the drawings included herein, as well as the claims.

CLAIMS

What is claimed is:

1. A hybrid engine consisting of an electric motor drive in parallel with a low-polluting
5 regenerative Rankine cycle engine using as the working fluid the products of complete
combustion of oxygen and a hydrocarbon or simple alcohol, combined with a water quench,
said hybrid engine comprising:
 - an electric motor means connected to a power transmission means, said electric motor
means receives its electric current from a battery means, said battery receives
10 its electric current from an alternator means, said alternator is driven by a
dynamic turbine means;
 - a dynamic compressor means having an inlet adapted to receive air from a supply and
having a discharge, said dynamic compressor including a means to raise the
pressure of said air to a value greater than at said inlet;
 - 15 a first intercooler means including means for receiving said air from said dynamic
compressor discharge and having an output and said intercooler including
means to cool said air;
 - a reciprocating compressor means having an inlet adapted to receive said air from said
first intercooler output and having a discharge, said reciprocating compressor
20 including a means to raise said pressure of the said air to a value greater than at
said inlet;
 - a second intercooler means including means for receiving said air from said
reciprocating compressor discharge and having an output and said second
intercooler means including means to cool said air;
 - 25 a scrubber means, including means for receiving said air from said second intercooler
output and having an output, said scrubber having means to remove carbon
dioxide, water, water vapor and oil form the air;
 - a heat exchanger means having an input adapted to receive said air from said scrubber
output and having an output and said heat exchanger in fluid communication
30 with gaseous nitrogen cooling means;

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a turbo-expander means having an input to receive said air from the heat exchanger output and having an exhaust and said turbo-expander including means to reduce the pressure of said air to a value lower than at said input;

5 a rectifier means having an input adapted to receive said air from said turbo-expander exhaust and having a gaseous nitrogen output and a gaseous oxygen output and said rectifier having a means to separate the gaseous nitrogen and gaseous oxygen from the said air;

said heat exchanger having a gaseous nitrogen inlet adapted to receive said gaseous nitrogen from said rectifier output and having a gaseous nitrogen output;

10 a turbo-expander driven dynamic compressor means adapted to receive said gaseous oxygen from said rectifier output and having a discharge, said turbo-expander driven dynamic compressor including means to raise the pressure of said gaseous oxygen to a value greater than at its inlet;

15 a reciprocating compressor means having an inlet adapted to receive a hydrocarbon type fuel from a supply means and having a discharge and said reciprocating compressor including a means to raise said fuel pressure to a value greater than at said inlet;

20 a high pressure water pump means having an inlet adapted to receive lower pressure water from a supply means and having a discharge and said pump including means to raise the pressure of said water to a value greater than at said inlet;

25 a gas generator means, including inlet means for receiving said oxygen from said turbo-expander driven dynamic compressor discharge, said high pressure fuel from said reciprocating compressor discharge and hot water from a high pressure hot water heater output, means to completely combust said high pressure oxygen with said high pressure fuel to generate a high temperature gas of steam and carbon dioxide, means to quench said high temperature gas with said high pressure water to generate a lower temperature mixture of steam and carbon dioxide gas and having an output;

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a reciprocating turbine means having an input adapted to receive said gas generator output gas, adapted to deliver power to said power transmission connected to said electric motor, and having an exhaust and said reciprocating turbine including a means to lower the pressure of said gas to a value lower than at
5 said input;

a dynamic turbine connected to said dynamic air compressor, including input means to receive said gas from said reciprocating turbine exhaust and have an exhaust, said dynamic turbine including means to lower the gas pressure to a value lower than at said input and said dynamic turbine also connected to said
10 alternator to generate electricity for said electric motor battery;

the said water heater means including inlet means for receiving said gas from the said dynamic turbine exhaust, means for receiving cold water from high pressure supply means, means to transfer the said gas heat to the said water and having a gas output and a high pressure hot water output;

15 a condenser means including input means to receive the water heater output gas, means to receive a coolant from a radiator output, means to transfer heat from said gas to said coolant to condense the steam into water and separate the carbon dioxide gas and output means to discharge the said condensed water, said carbon dioxide gas and said heated coolant;

20 a pump means including and inlet adapted to receive said condenser output water, means to raise said water pressure to a value greater than at said inlet and have a discharge for said water heater cold water inlet and a discharge for radiator evaporative cooling water;

25 the said radiator means including means for receiving said condenser warm coolant output, means to cool the warm coolant with ambient air, means for evaporative cooling the ambient air with spray nozzles using said pump evaporative cooling discharge water, and output means to discharge said coolant and a fan means to circulate said ambient air to absorb heat from said condenser coolant;

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a reciprocating compressor means including inlet means to receive gaseous carbon dioxide from the said condenser output and having a discharge, means to raise the said carbon dioxide pressure to a value greater than at said inlet; and

5 a carbon dioxide conversion and storage means including means for receiving the reciprocating compressor carbon dioxide discharge and means to convert the carbon dioxide into a compact liquid or solid state for periodic removal.

2. A low or no pollution emitting internal combustion engine for vehicle power production or other power uses, comprising in combination:

an air inlet receiving air from a surrounding environment;

10 an air treatment device oriented downstream from said air inlet, said air treatment device including means to separate oxygen from said air and output the oxygen through an oxygen outlet;

a source of fuel, said fuel including hydrogen; and

15 at least one combustion chamber having an ignition device, at least one inlet for receiving fuel and oxygen therein, a piston oriented to oscillate within said chamber, said piston coupled to a power output device, and at least one exhaust for removal of products of combustion within said combustion chamber.

3. The internal combustion engine of claim 2 wherein a premixer is provided upstream of one of said inlets of said combustion chamber, said premixer receiving at least oxygen and
20 steam therein, said steam at least partially created within said combustion chamber as one of said products of combustion and routed to said premixer from said exhaust;

wherein at least one compressor is oriented between said air inlet and said air treatment device, raising a pressure of the air;

25 wherein at least one intercooler is oriented between a first said compressor and said air treatment device, each said intercooler reducing a temperature of the air passing there through;

wherein said air treatment device includes an expander downstream from a last said intercooler, said expander reducing a pressure of the air and a temperature of the air to below

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a condensation point of the oxygen within the air, said air treatment device including said oxygen outlet substantially free of nitrogen;

wherein said air treatment device includes a nitrogen outlet, and wherein said engine includes a heat transfer device including means to transfer heat between nitrogen exiting said air treatment device through said nitrogen outlet and air between said expander and said air inlet;

wherein said expander is coupled to an oxygen compressor interposed between said oxygen outlet of said air treatment device and said combustion device, whereby a pressure of the oxygen is increased; and

wherein a scrubber is provided between said air treatment device and said air inlet to remove gases capable of freezing from the air.

4. The internal combustion engine of claim 2 wherein a premixer is provided upstream of one of said inlets of said combustion chamber, said premixer receiving oxygen from said oxygen outlet of said air treatment device, fuel from said source of fuel and steam created as one of said products of combustion and routed from said combustion chamber exhaust, such that said premixer mixes the fuel, oxygen and steam prior to entry into said combustion chamber through said inlet, whereby an Otto cycle internal combustion engine is provided without nitrogen oxides in its exhaust.

5. The internal combustion engine of claim 2 wherein a premixer is provided upstream of one of said inlets of said combustion chamber, said premixer receiving oxygen from said oxygen outlet of said air treatment device and steam created as one of said products of combustion and routed from said combustion chamber exhaust, such that said premixer mixes the oxygen and steam prior to entry into said combustion chamber through a first said inlet; and

wherein a second inlet is provided for said fuel, said second inlet configured to admit the fuel into said combustion cylinder after compression of said oxygen and steam mixture by said piston, such that said fuel is combusted at substantially constant pressure and a Diesel cycle internal combustion engine is provided without nitrogen oxides in its exhaust.

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6. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion or stationary electric power generation, the engine comprising in combination:

an air inlet;

5 a source of fuel at least partially including hydrogen;

an air treatment device including an inlet coupled to said air inlet, a means to remove nitrogen from the air, so that the air has less nitrogen than at said air inlet, and an oxygen rich outlet;

10 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said outlet of said air treatment device, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

15 wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

20 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein at least one compressor is oriented between said air inlet and said air treatment device, raising a pressure of the air;

25 wherein at least one intercooler is oriented between a first said compressor and said air treatment device, said at least one intercooler reducing a temperature of the air passing there through; and

wherein said air treatment device includes an expander downstream from said at least one intercooler, said expander reducing a pressure of the air and a temperature of the air to below a condensation point of the oxygen within the air, said air treatment device including said oxygen rich outlet.

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7. The engine of claim 6 wherein said air treatment device includes a material capable of adsorption and desorption of an air constituent gas, said material located in contact with air from said air inlet.

8. The engine of claim 7 wherein said material adsorbs nitrogen and desorbs nitrogen based on pressure of the air adjacent the material, wherein at least two separate beds of material are provided with means to sequentially increase and decrease pressure adjacent said beds of material to be above atmospheric pressure and below atmospheric pressure, said beds including means to selectively discharge air enriched with oxygen out of said beds and to said oxygen rich outlet.

9. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion or stationary electric power generation, the engine comprising in combination:

an air inlet;

a source of fuel at least partially including hydrogen;

an air treatment device including an inlet coupled to said air inlet, a means to remove nitrogen from the air, so that the air has less nitrogen than at said air inlet, and an oxygen rich outlet;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said outlet of said air treatment device, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge;

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a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein said air treatment device includes at least one membrane, said membrane
5 having a different permeability for oxygen than for nitrogen, said air treatment device directing air adjacent one side of said membrane and collecting oxygen rich gases and nitrogen rich gases from opposite sides of said membrane, the oxygen rich gases directed to said oxygen rich outlet of said air treatment device.

10 10. The engine of claim 9 wherein two or more membranes are arranged such that air flow through said membranes occurs in series and greater oxygen enrichment and nitrogen enrichment are achieved.

11. The engine of claim 10 wherein a feed compressor is coupled to said air inlet including means to increase pressure of air entering said air treatment device to above
15 atmospheric pressure, said membrane being more permeable to oxygen than to nitrogen, said membrane juxtaposed between an outlet of said feed compressor and an oxygen rich outlet, and a second membrane juxtaposed between said oxygen rich outlet and an oxygen super rich outlet, such that gases on a side of said second membrane opposite said oxygen rich outlet have a greater percentage of oxygen than on said oxygen rich outlet side of said second
20 membrane, said oxygen super rich outlet leading to said oxygen rich outlet of said air treatment device.

12. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion or stationary electric power generation, the engine comprising in combination:

25 an air inlet;
a source of fuel at least partially including hydrogen;

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an air treatment device including an inlet coupled to said air inlet, a means to remove nitrogen from the air, so that the air has less nitrogen than at said air inlet, and an oxygen rich outlet;

5 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said outlet of said air treatment device, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

10 wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge;

15 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein said air treatment device includes an electroceramic membrane juxtaposed between said air inlet and said oxygen rich outlet, said electroceramic membrane including an ionic solid solution which permits movement of oxygen ions there through; and

20 wherein said air treatment device includes means to elevate a temperature of said electroceramic membrane at least partially from heat generated within said fuel combustion device.

13. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion or stationary electric power generation, the engine comprising in combination:

25 an air inlet;

a source of fuel at least partially including hydrogen;

an air treatment device including an inlet coupled to said air inlet, a means to remove nitrogen from the air, so that the air has less nitrogen than at said air inlet, and an oxygen rich outlet;

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a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said outlet of said air treatment device, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein a combustion product expander is coupled to said discharge of said combustor, said expander configured to output power from said engine and an exhaust for the combustion products, wherein said exhaust is coupled to a means to return at least a portion of the combustion products back to said combustion device, such that said engine operates as an at least partially closed cycle; and

wherein said means to return the combustion products back to said combustion device includes means to cool the combustion products while exchanging heat with a separate working fluid upstream from a turbine in a separate closed Rankine cycle engine.

14. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion, the engine comprising in combination:

an air inlet configured to receive air from an environment surrounding said engine;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

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a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, the combustor having a discharge for the combustion products;

a combustion product expander coupled to said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

wherein said engine includes a means to compress the oxygen and the fuel before the oxygen and the fuel enter said combustion device.

15. The engine of claim 14 wherein said means to compress the oxygen includes at least two compressors, each said compressor including an intercooler there between, at least two of said compressors oriented between said air inlet and said air treatment device, such that the oxygen is compressed along with other constituents of the air entering the air inlet.

16. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion, the engine comprising in combination:

an air inlet configured to receive air from an environment surrounding said engine;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

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a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, the combustor having a discharge for the combustion products;

a combustion product expander coupled to said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein a bypass air duct is provided between said air inlet and said combustion device, said bypass air duct delivering air, including nitrogen, to said combustion device, said bypass air duct including a valve capable of blocking said bypass air duct, whereby air, including nitrogen, can be provided to the combustion device when desired.

17. The engine of claim 14 wherein each of said means to compress is coupled to an electric motor and battery such that said electric motor and battery can drive said means to compress for compression of the oxygen, and wherein said means to compress is also coupled to at least one expander in fluid communication with said combustion products exiting said discharge of said combustion device, such that said expanders can drive said means to compress for compression of the oxygen; and

wherein said electric motors include means to charge said battery when said expanders deliver excess power beyond that necessary to drive said means to compress for compression of the oxygen.

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18. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion, the engine comprising in combination:

an air inlet configured to receive air from an environment surrounding said engine;

a source of fuel at least partially including hydrogen;

5 an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

10 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, the combustor having a discharge for the combustion products;

15 a combustion product expander coupled to said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

20 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein at least one compressor is oriented between said air inlet and said air treatment device, raising a pressure of the air;

25 wherein at least one intercooler is oriented between a first said compressor and said air treatment device, each said intercooler reducing a temperature of the air passing there through; and

wherein said air treatment device includes an expander downstream from a last said intercooler, said expander reducing a pressure of the air and a temperature of the air to below

a condensation point of the oxygen within the air, said air treatment device including said oxygen outlet substantially free of nitrogen.

19. The engine of claim 18 wherein said air treatment device includes a nitrogen outlet, and wherein said engine includes a heat transfer device including means to transfer heat
5 between nitrogen exiting said air treatment device through said nitrogen outlet and air between said expander and said air inlet.

20. The engine of claim 18 wherein said expander is coupled to an oxygen compressor interposed between said oxygen outlet of said air treatment device and said combustion device, whereby a pressure of the oxygen is increased.

10 21. The engine of claim 18 wherein a scrubber is provided between said air treatment device and said air inlet to remove gases capable of freezing from the air.

22. The engine of claim 19 wherein said air treatment device includes a two column rectifier downstream from said expander, said rectifier including said oxygen outlet and said nitrogen outlet.

15 23. The engine of claim 17 wherein at least one of said compressors is oriented between said air inlet and said air treatment device, raising a pressure of the air;

wherein at least one intercooler is oriented between a first said compressor and said air treatment device, each said intercooler reducing a temperature of the air passing there through;

20 wherein said air treatment device includes an expander downstream from a last said intercooler, said expander reducing a pressure of the air and a temperature of the air to below a condensation point of the oxygen within the air, said air treatment device including said oxygen outlet substantially free of nitrogen;

25 wherein said air treatment device includes a nitrogen outlet, and wherein said engine includes a heat transfer device including means to transfer heat between nitrogen exiting said air treatment device through said nitrogen outlet and air between said expander and said air inlet;

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wherein said expander is coupled to an oxygen compressor interposed between said oxygen outlet of said air treatment device and said combustion device, whereby a pressure of the oxygen is increased;

5 wherein a scrubber is provided between said air treatment device and said air inlet to remove gases capable of freezing from the air; and

wherein said air treatment device includes a two column rectifier downstream from said expander, said rectifier including said oxygen outlet and said nitrogen outlet.

24. A low or no pollution emitting combustion engine to provide power for various applications including vehicle propulsion, the engine comprising in combination:

10 an air inlet configured to receive air from an environment surrounding said engine;

a source of fuel at least partially including hydrogen;

15 an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

20 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, the combustor having a discharge for the combustion products;

a combustion product expander coupled to said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products;

25 wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

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wherein at least a portion of said combustion products exiting said exhaust of said combustion product expansion device are routed to a condenser where the gaseous water within said combustion products is condensed to liquid water, said condenser including a first return duct to said water inlet of said combustion device, whereby the H₂O acts as a working
 5 fluid for a Rankine cycle;

wherein said condenser includes a heat transfer fluid therein for removal of heat from the H₂O, said heat transfer fluid in fluid communication with an interior of a radiator oriented in the environment surrounding said engine with air from the surrounding environment passing against an exterior of said radiator and cooling said heat transfer fluid therein; and

10 wherein said condenser includes a second outlet water duct spraying liquid water into the surrounding environment and against said exterior of said radiator for evaporative cooling of said heat transfer fluid within said radiator.

25. A combustion engine providing clean power for various applications and featuring low NO_x production, comprising in combination:

15 a source of air, the air including nitrogen and oxygen;

a source of fuel, the fuel including hydrogen;

an air separator having an inlet coupled to said source of air, and having an outlet, said
 air separator configured to remove at least a portion of the nitrogen from the
 air entering said inlet so that the air exiting said air separator through said
 20 outlet is oxygen enriched;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and air
 from said outlet of said air separator, said combustor combusting the fuel with
 the air to produce elevated pressure and elevated temperature combustion
 products including gaseous water, the combustor having a discharge for the
 25 combustion products;

a combustion products expander coupled to said discharge of said combustor, said
 combustion products expander outputting power from said engine;

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wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

5 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

wherein said fuel combustor can operate in two modes including a first mode where said fuel combustor receives fuel from said source of fuel and oxygen enriched air from said air separator, and a second mode where said fuel combustor receives fuel from said source of
 10 fuel and air from which no nitrogen has been removed, such that said fuel combustor can operate in said second mode with non-oxygen enriched air and can operate in said first mode with oxygen enriched air.

26. A combustion engine providing clean power for various applications and featuring low NO_x production, comprising in combination:

15 a source of air, the air including nitrogen and oxygen;

a source of fuel, the fuel including hydrogen;

an air separator having an inlet coupled to said source of air, and having an outlet, said
 20 air separator configured to remove at least a portion of the nitrogen from the air entering said inlet so that the air exiting said air separator through said outlet is oxygen enriched;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and air from said outlet of said air separator, said combustor combusting the fuel with the air to produce elevated pressure and elevated temperature combustion products including gaseous water, the combustor having a discharge for the
 25 combustion products;

a combustion products expander coupled to said discharge of said combustor, said combustion products expander outputting power from said engine;

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wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

5 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein each of the components comprising said engine are mounted upon a common mobile platform with said combustion product expander coupled to a prime mover of said platform, such that said engine causes said platform to move.

10 27. A variable pollution emitting engine to provide power for various applications, comprising in combination:

an air inlet;

a source of fuel at least partially including hydrogen;

15 an air separator downstream from said air inlet, said air separator configured to remove nitrogen from the air entering the air separator so that the air is primarily oxygen with other non-oxygen constituents at an oxygen enriched air outlet;

20 a fuel combustor, said fuel combustor having at least one entrance for the fuel from said source of fuel and an oxidizer, the oxidizer being air in a first more polluting mode and the oxidizer being the oxygen enriched air from said oxygen enriched air outlet in a second less polluting mode, said fuel combustor combusting the fuel with the oxidizer to produce elevated pressure and elevated temperature combustion products including steam, said combustor having a discharge for said combustion products; and

25 a combustion product expander downstream of said discharge.

28. The engine of claim 27 wherein said fuel combustor includes a water inlet, said water inlet spaced from an inlet for oxidizer to enter said combustor.

29. The engine of claim 27 wherein said source of fuel is a source of hydrocarbon fuel and wherein the combustion products produced within said fuel combustor includes carbon dioxide, the carbon dioxide expanding with the steam of the combustion products within said expansion device.

5 30. The engine of claim 27 wherein said first more polluting mode includes the air entering said entrance of said fuel combustor previously passing through said air inlet and through said air separator before said air separator commences removal of nitrogen from said air separator.

10 31. The engine of claim 27 wherein said first more polluting mode includes the air entering said entrance of said fuel combustor passing through an inlet in communication with a surrounding environment and separate from said air separator.

32. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

15 an air inlet;
a source of fuel at least partially including hydrogen;
an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and
20 an oxygen enriched air outlet;
a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said
25 combustor having a discharge for said combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

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a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

5 wherein said air separator includes means to liquefy at least a portion of the air and means to separate liquid portions of the air from non-liquid portions of the air and means to direct portions of the air which have a greater oxygen content to said oxygen rich outlet.

33. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

10 an air inlet;
a source of fuel at least partially including hydrogen;
an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and
15 an oxygen enriched air outlet;
a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said
20 combustor having a discharge for said combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to
25 said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein at least one compressor is oriented between said air inlet and said air separator, raising a pressure of the air;

wherein at least one intercooler is oriented between a first said compressor and said air separator, said at least one intercooler reducing a temperature of the air passing there through; and

wherein said air separator includes an expander downstream from said at least one intercooler, said expander reducing a pressure of the air and a temperature of the air to below a condensation point of the oxygen within the air, said air separator including said oxygen enriched air outlet.

34. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

an air inlet;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

wherein said air separator includes a material capable of adsorption and desorption of an air constituent gas, said material located in contact with air from said air inlet.

35. The engine of claim 34 wherein said material adsorbs nitrogen and desorbs nitrogen based on pressure of the air adjacent the material, wherein at least two separate beds of material are provided with means to sequentially increase and decrease pressure adjacent said beds of material to be above atmospheric pressure and below atmospheric pressure, said beds including means to selectively discharge air enriched with oxygen out of said beds and to said oxygen enriched air outlet.

36. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

10 an air inlet;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and

15 an oxygen enriched air outlet;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

20 wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

25 wherein said air separator includes at least one membrane, said membrane having a different permeability for oxygen than for nitrogen, said air separator directing air adjacent one side of said membrane and collecting oxygen rich gases and nitrogen rich gases from

opposite sides of said membrane, the oxygen rich gases directed to said oxygen enriched air outlet of said air separator.

37. The engine of claim 36 wherein two or more membranes are arranged such that air flow through said membranes occurs in series and greater oxygen enrichment and nitrogen enrichment are achieved.

38. The engine of claim 37 wherein a feed compressor is coupled to said air inlet including means to increase pressure of air entering said air separator to above atmospheric pressure, said membrane being more permeable to oxygen than to nitrogen, said membrane juxtaposed between an outlet of said feed compressor and said oxygen rich outlet, and a second membrane juxtaposed between said oxygen rich outlet and an oxygen super rich outlet, such that gases on a side of said second membrane opposite said oxygen rich outlet have a greater percentage of oxygen than on said oxygen rich outlet side of said second membrane, said oxygen super rich outlet leading to said oxygen enriched air outlet of said air separator.

39. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

an air inlet;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

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wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

5 a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor; and

wherein said air separator includes an electroceramic membrane juxtaposed between said air inlet and said oxygen enriched outlet, said electroceramic membrane including an ionic solid solution which permits movement of oxygen ions there through.

10 40. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion or stationary electric power generation, the engine comprising in combination:

an air inlet;

a source of fuel at least partially including hydrogen;

15 an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

20 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting said fuel with said oxygen to produce elevated pressure and elevated temperature combustion products including gaseous water, said combustor having a discharge for said combustion products;

25 wherein at least part of a non-H₂O portion of the combustion products is removed from the combustion products after discharge from said combustor, so that the combustion products have a higher percentage of H₂O than the combustion products at said discharge; and

a return line for routing at least a portion of the H₂O rich combustion products back to said combustor through at least one water inlet spaced from said inlet for oxygen into said combustor;

wherein a combustion product expander is coupled to said discharge of said combustor, said expander configured to output power from said engine and an exhaust for the combustion products, wherein said exhaust is coupled to a means to return at least a portion of the combustion products back to said combustion device, such that said engine operates as an
 5 at least partially closed cycle; and

wherein said means to return the combustion products back to said combustion device includes means to cool the combustion products while exchanging heat with a separate working fluid upstream from a turbine in a separate closed Rankine cycle engine.

41. A low or no pollution emitting combustion engine to provide power for various
 10 applications such as vehicle propulsion, the engine comprising in combination:
- an air inlet configured to receive air from an environment surrounding said engine;
 - a source of fuel at least partially including hydrogen;
 - an air separator including an inlet coupled to said air inlet, said air separator
 15 configured to remove nitrogen from the air entering said air inlet so that
 remaining air is primarily oxygen and with other non-oxygen constituents, and
 an oxygen enriched air outlet;
 - a fuel combustor, said fuel combustor receiving fuel from said source of fuel and
 oxygen from said oxygen enriched air outlet of said air separator, said
 combustor combusting the fuel with the oxygen to produce elevated pressure
 20 and elevated temperature combustion products including steam, the combustor
 having a discharge for the combustion products;
 - a combustion products expander downstream from said discharge of said combustor,
 said expander outputting power from said engine and having an exhaust for the
 combustion products; and
 - 25 a reheater located downstream of said combustion product expander, said reheater
 enhancing a temperature of said combustion products exiting said combustion
 product expander, said reheater receiving fuel from a source of fuel at least
 partially including hydrogen and oxygen from said oxygen enriched air outlet
 of said air separator, said reheater also receiving said combustion products of

said fuel combustor, said reheater combusting the fuel with the oxygen in the direct presence of the combustion products of said fuel combustor to produce elevated pressure and temperature reheater combustion products, with said reheater combustion products having a different composition than said combustion products of said fuel combustor, said reheater having a discharge for the reheater combustion products; and

wherein said engine includes a means to compress the oxygen and the fuel before the oxygen and the fuel enter said combustion device.

42. The engine of claim 41 wherein said means to compress the oxygen includes at least two compressors, each said compressor including an intercooler there between, at least two of said compressors oriented between said air inlet and said air treatment device, such that the oxygen is compressed along with other constituents of the air entering the air inlet.

43. A low or no pollution emitting combustion engine to provide power for various applications such as vehicle propulsion, the engine comprising in combination:

an air inlet configured to receive air from an environment surrounding said engine;

a source of fuel at least partially including hydrogen;

an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including steam, the combustor having a discharge for the combustion products;

a combustion products expander downstream from said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products; and

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5 a reheater located downstream of said combustion product expander, said reheater
 enhancing a temperature of said combustion products exiting said combustion
 product expander, said reheater receiving fuel from a source of fuel at least
 partially including hydrogen and oxygen from said oxygen enriched air outlet
 10 of said air separator, said reheater also receiving said combustion products of
 said fuel combustor, said reheater combusting the fuel with the oxygen in the
 direct presence of the combustion products of said fuel combustor to produce
 elevated pressure and temperature reheater combustion products, with said
 reheater combustion products having a different composition than said
 15 combustion products of said fuel combustor, said reheater having a discharge
 for the reheater combustion products; and

wherein a bypass air duct is provided between said air inlet and said combustion
 device, said bypass air duct delivering air, including nitrogen, to said combustion device, said
 bypass air duct including a valve capable of blocking said bypass air duct, whereby air,
 15 including nitrogen, can be provided to the combustion device when desired.

44. The engine of claim 41 wherein each of said means to compress is coupled to an electric
 motor and battery such that said electric motor and battery can drive said means to compress
 for compression of the oxygen, and wherein said means to compress is also coupled to at least
 one expander in fluid communication with said combustion products exiting said discharge of
 20 said combustion device, such that said expanders can drive said means to compress for
 compression of the oxygen; and

wherein said electric motors include means to charge said battery when said expanders
 deliver excess power beyond that necessary to drive said means to compress for compression
 of the oxygen.

25 45. A low or no pollution emitting combustion engine to provide power for various
 applications such as vehicle propulsion, the engine comprising in combination:

an air inlet configured to receive air from an environment surrounding said engine;
 a source of fuel at least partially including hydrogen;

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an air separator including an inlet coupled to said air inlet, said air separator configured to remove nitrogen from the air entering said air inlet so that remaining air is primarily oxygen and with other non-oxygen constituents, and an oxygen enriched air outlet;

5 a fuel combustor, said fuel combustor receiving fuel from said source of fuel and oxygen from said oxygen enriched air outlet of said air separator, said combustor combusting the fuel with the oxygen to produce elevated pressure and elevated temperature combustion products including steam, the combustor having a discharge for the combustion products;

10 a combustion products expander downstream from said discharge of said combustor, said expander outputting power from said engine and having an exhaust for the combustion products; and

a reheater located downstream of said combustion product expander, said reheater enhancing a temperature of said combustion products exiting said combustion
15 product expander, said reheater receiving fuel from a source of fuel at least partially including hydrogen and oxygen from said oxygen enriched air outlet of said air separator, said reheater also receiving said combustion products of said fuel combustor, said reheater combusting the fuel with the oxygen in the direct presence of the combustion products of said fuel combustor to produce
20 elevated pressure and temperature reheater combustion products, with said reheater combustion products having a different composition than said combustion products of said fuel combustor, said reheater having a discharge for the reheater combustion products;

wherein at least one compressor is oriented between said air inlet and said air
25 separator, raising a pressure of the air;

wherein at least one intercooler is oriented between a first said compressor and said air separator, each said intercooler reducing a temperature of the air passing there through; and

wherein said air separator includes an expander downstream from a last said intercooler, said expander reducing a pressure of the air and a temperature of the air to below

a condensation point of the oxygen within the air, said air separator including said oxygen enriched air outlet substantially free of nitrogen.

46. The engine of claim 45 wherein said air separator includes a nitrogen outlet, and wherein said engine includes a heat transfer device including means to transfer heat between
5 nitrogen exiting said air separator through said nitrogen outlet and air between said expander and said air inlet.

47. The engine of claim 45 wherein said expander is coupled to an oxygen compressor interposed between said oxygen enriched air outlet of said air separator and said combustion device, whereby a pressure of the oxygen is increased.

10 48. The engine of claim 45 wherein a scrubber is provided between said air separator and said air inlet to remove gases capable of freezing from the air.

49. The engine of claim 46 wherein said air separator includes a two column rectifier downstream from said expander, said rectifier including said oxygen enriched air outlet and said nitrogen outlet.

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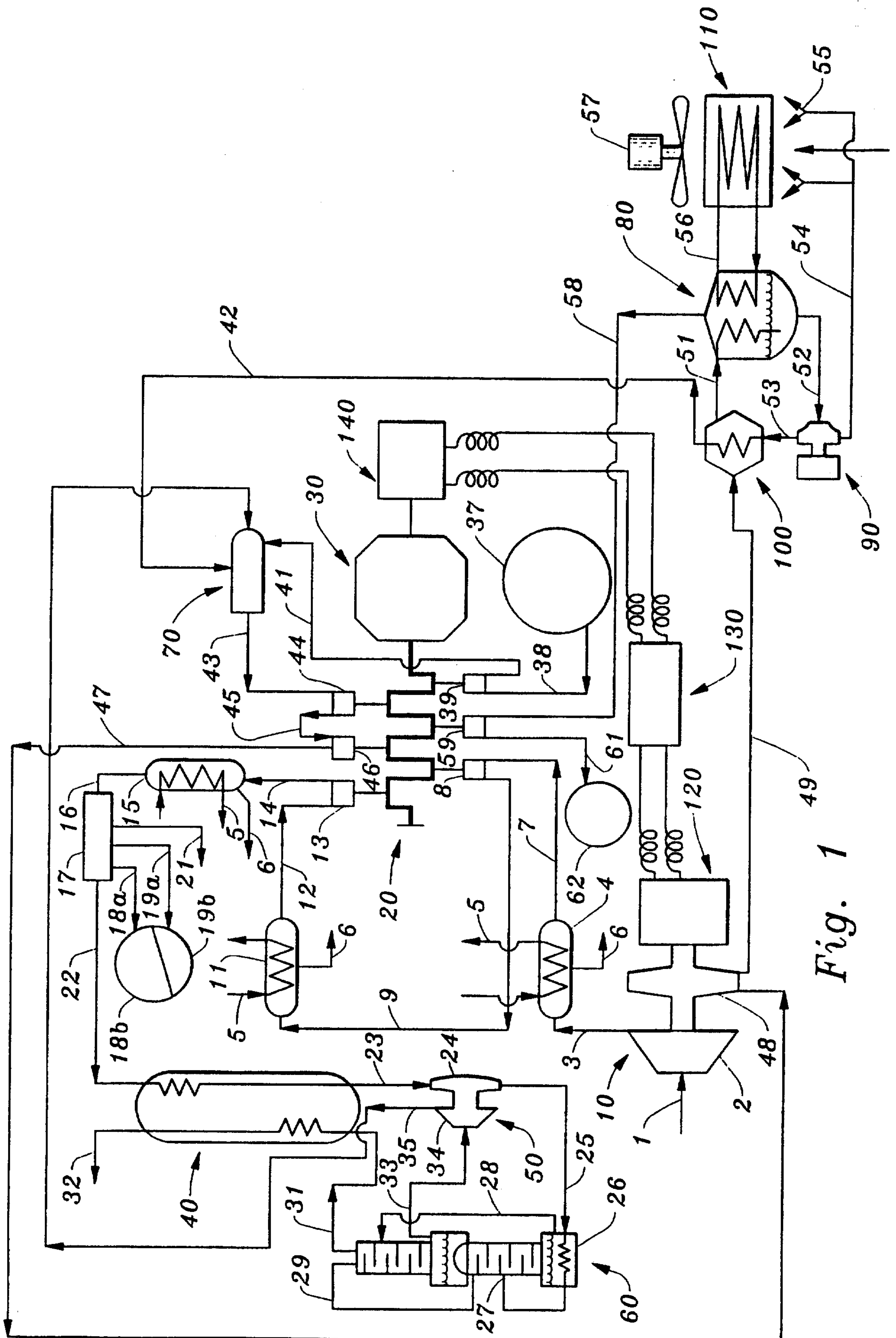


Fig. 1

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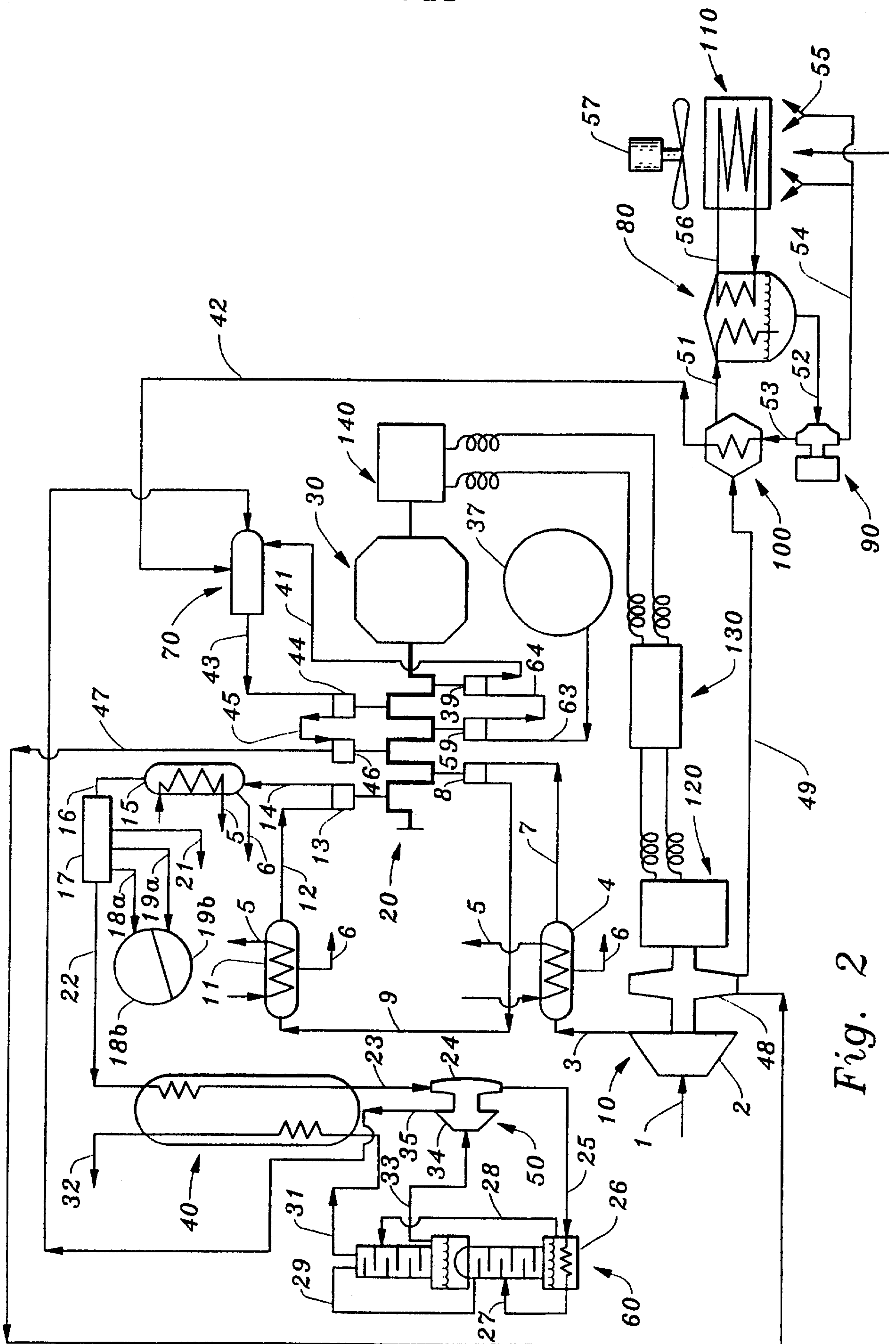


Fig. 2

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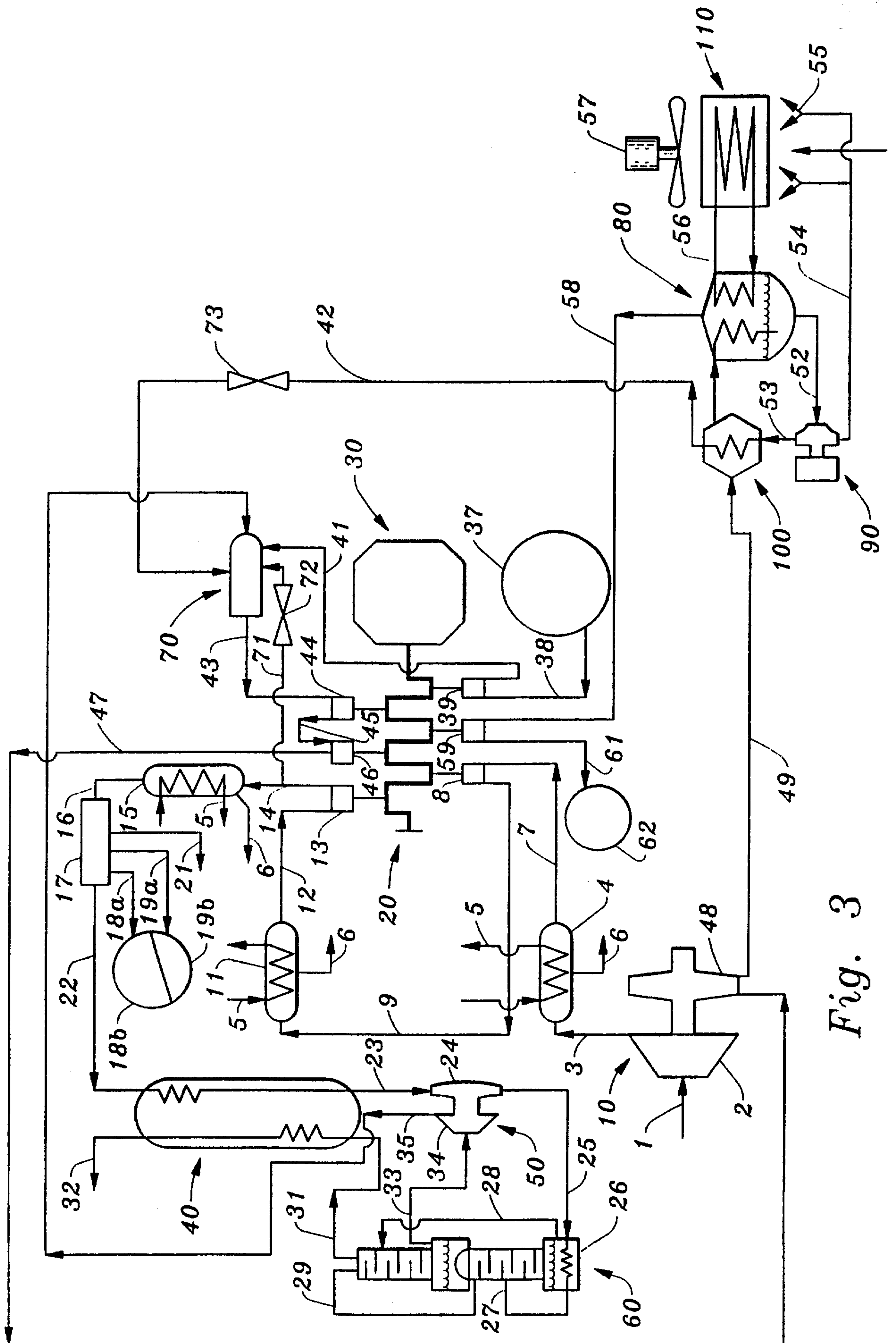


Fig. 3

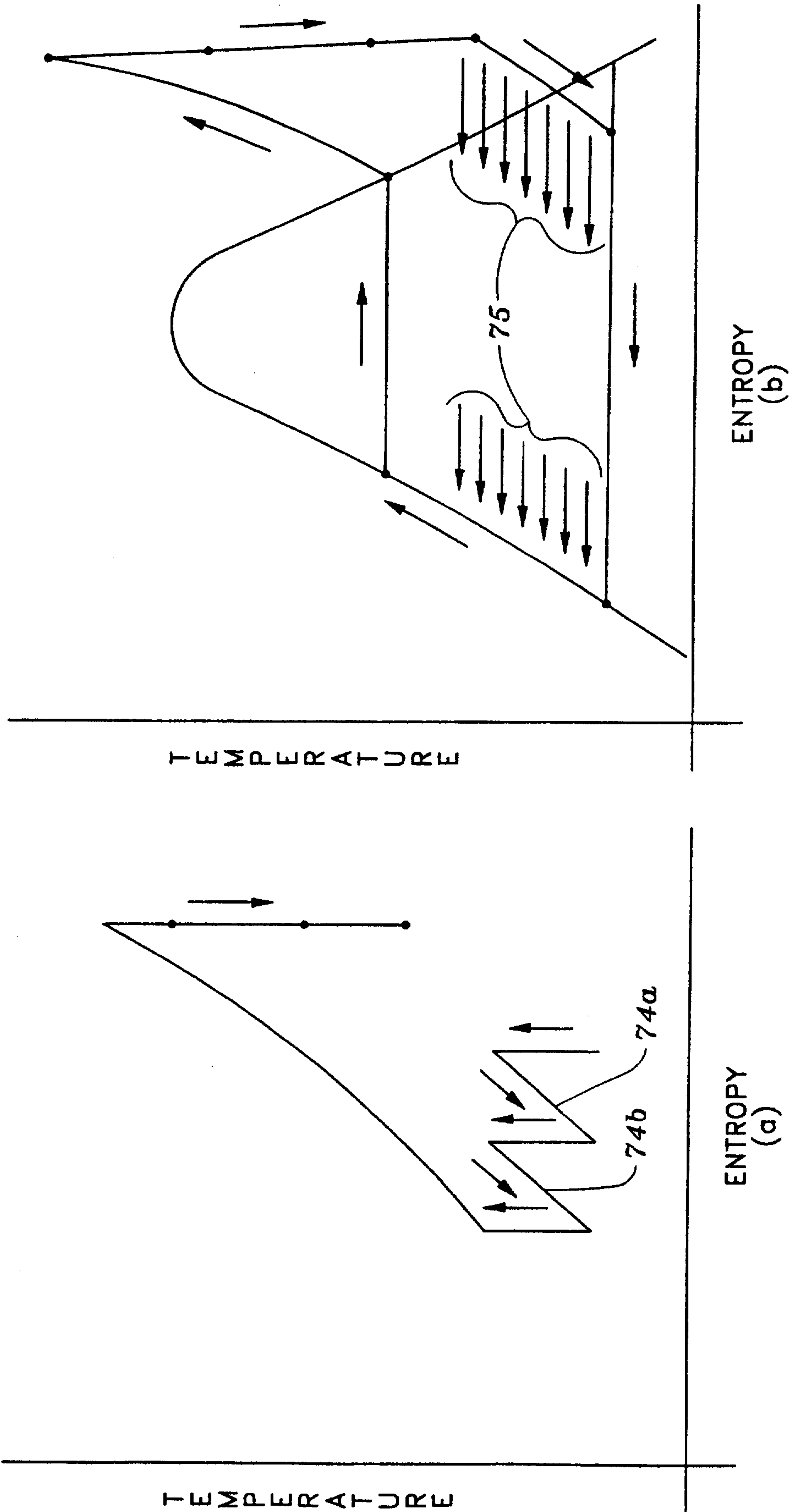


Fig. 5

Fig. 4

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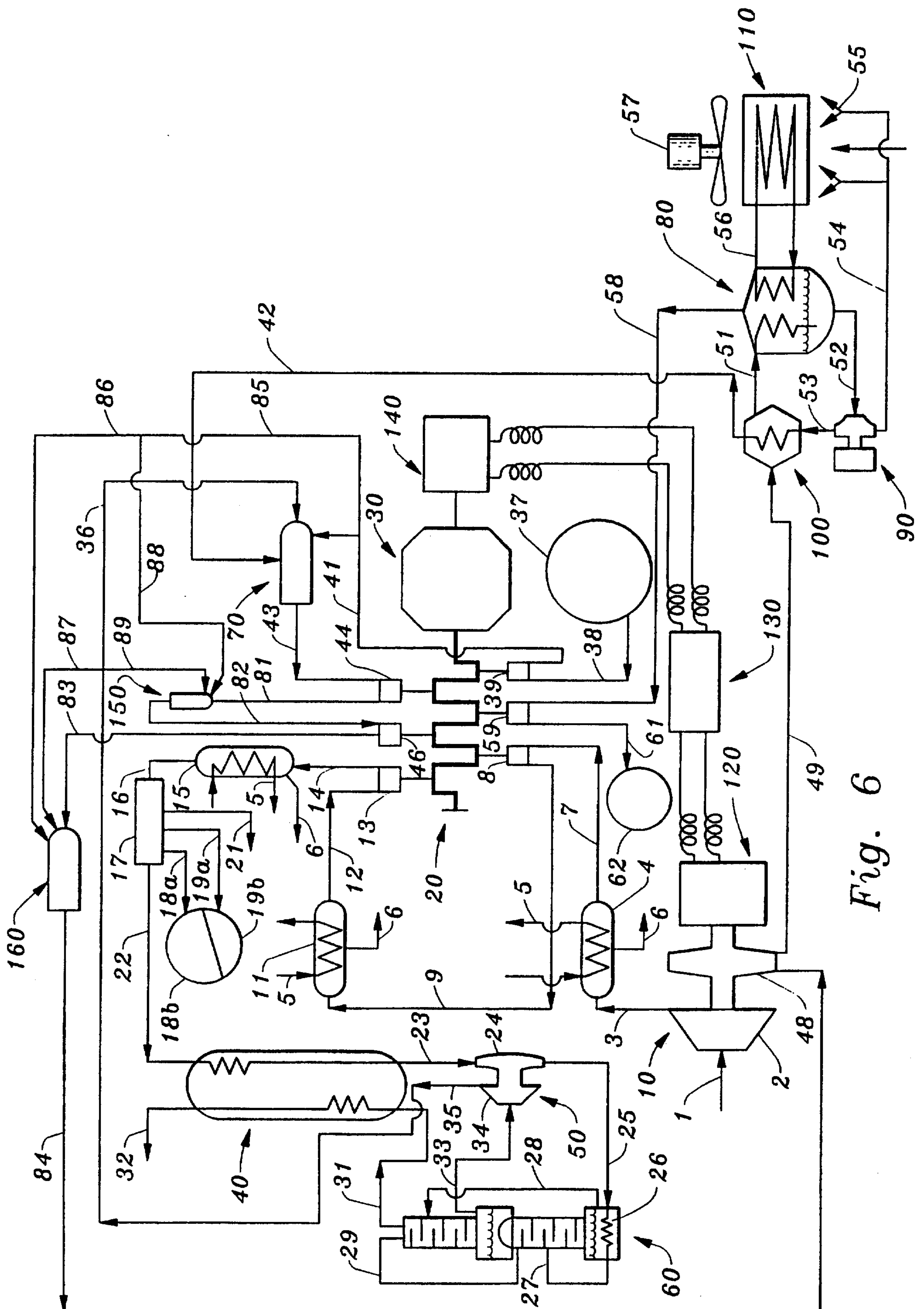


Fig. 6

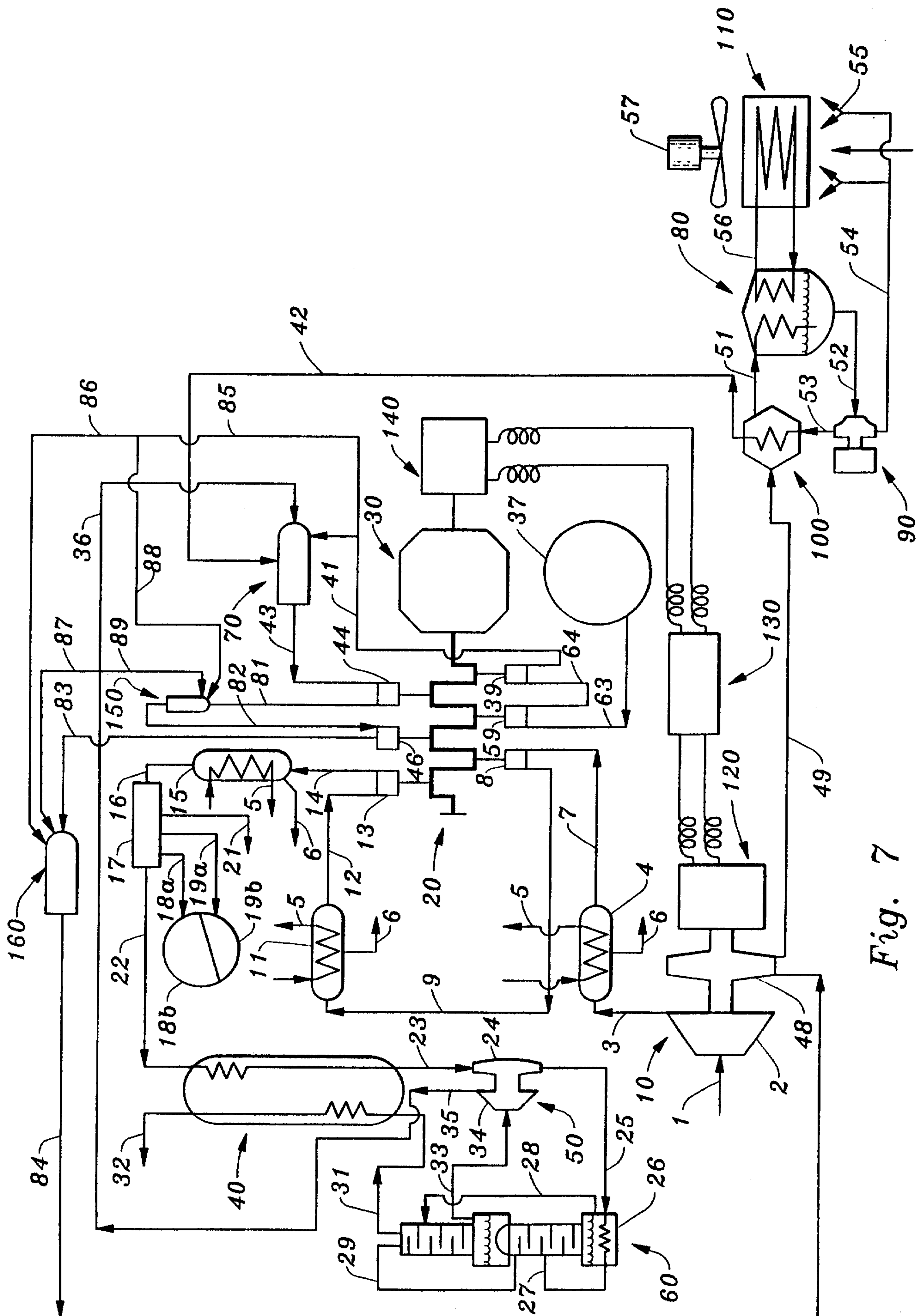


Fig. 7

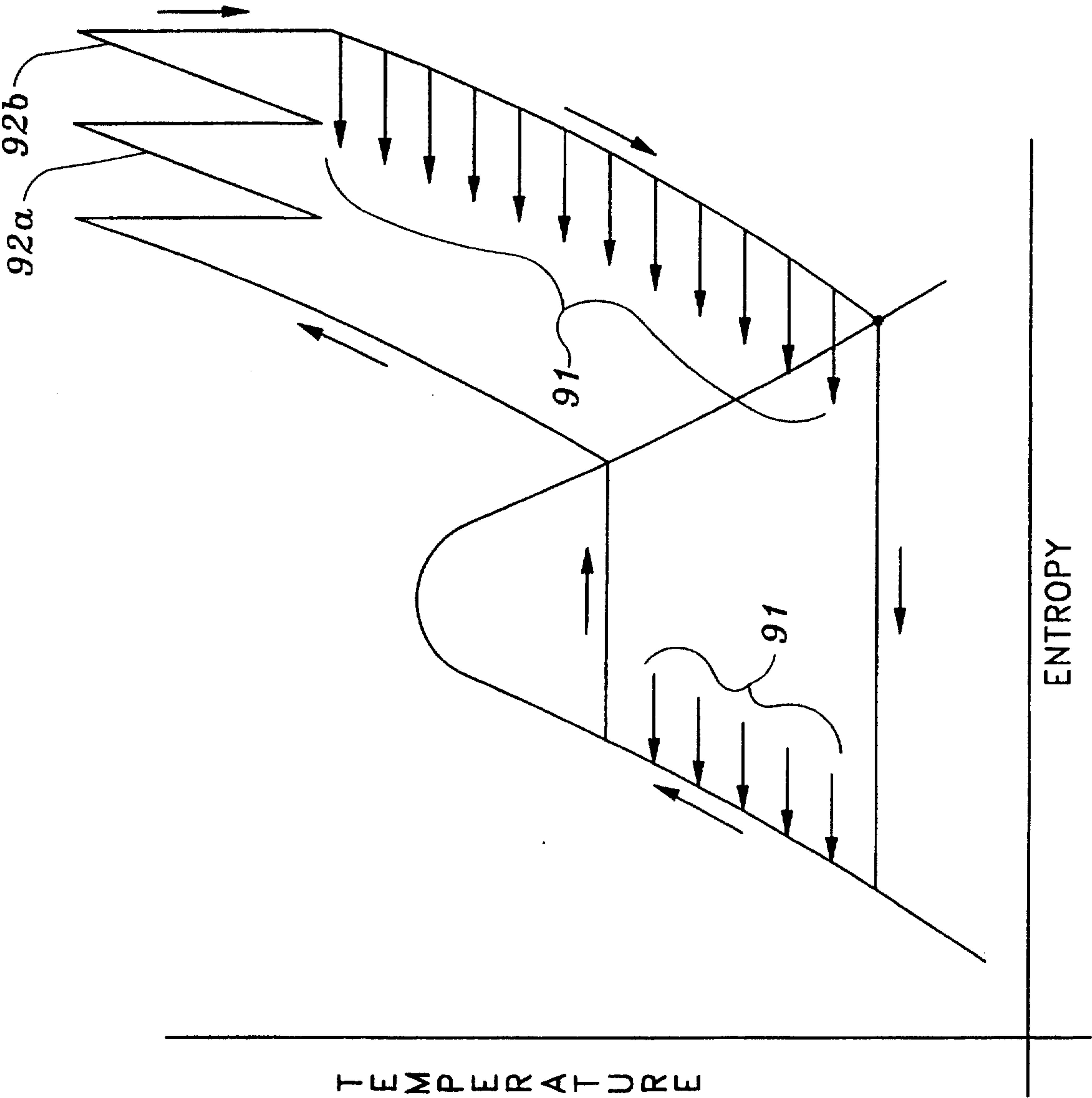


Fig. 8

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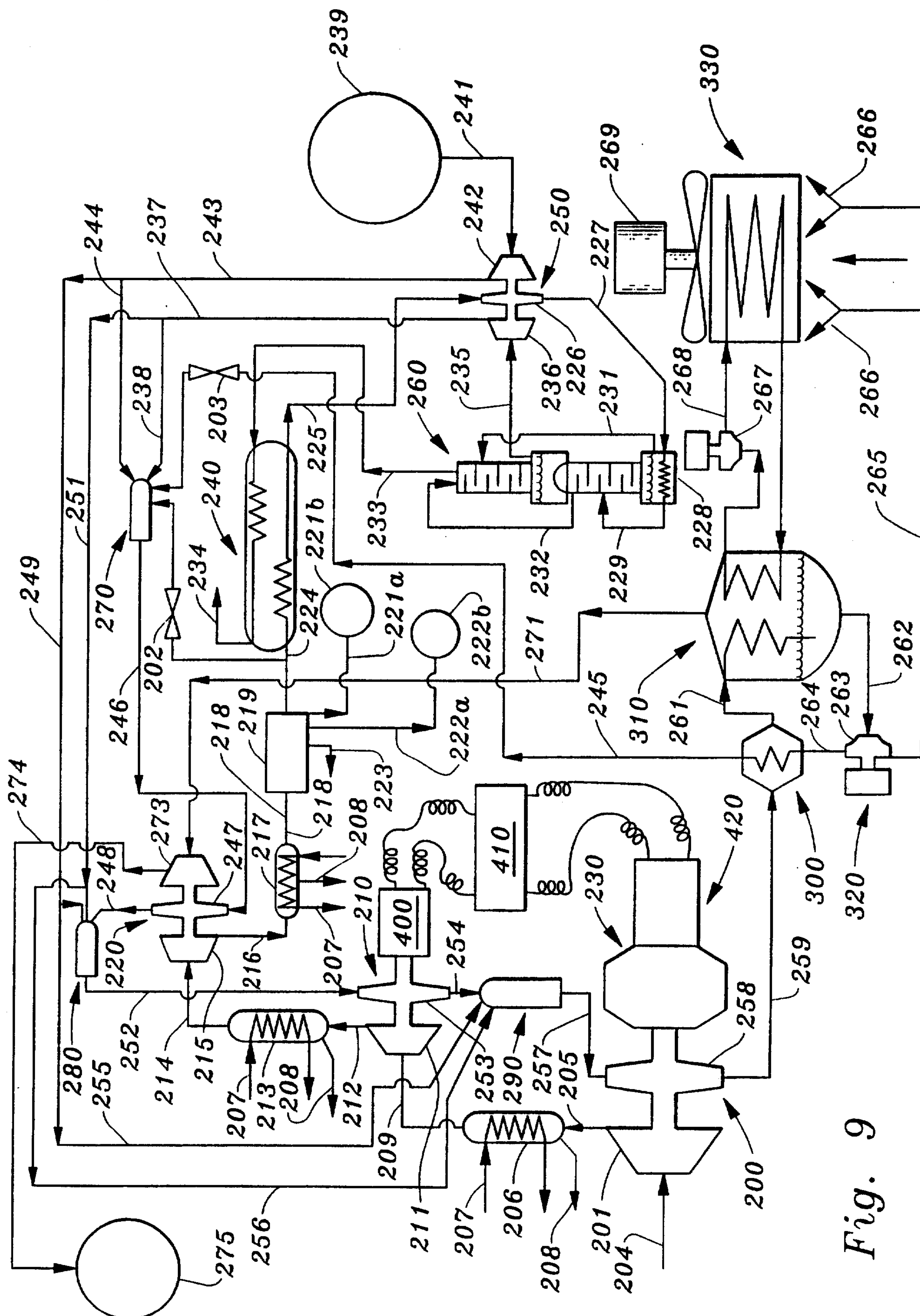
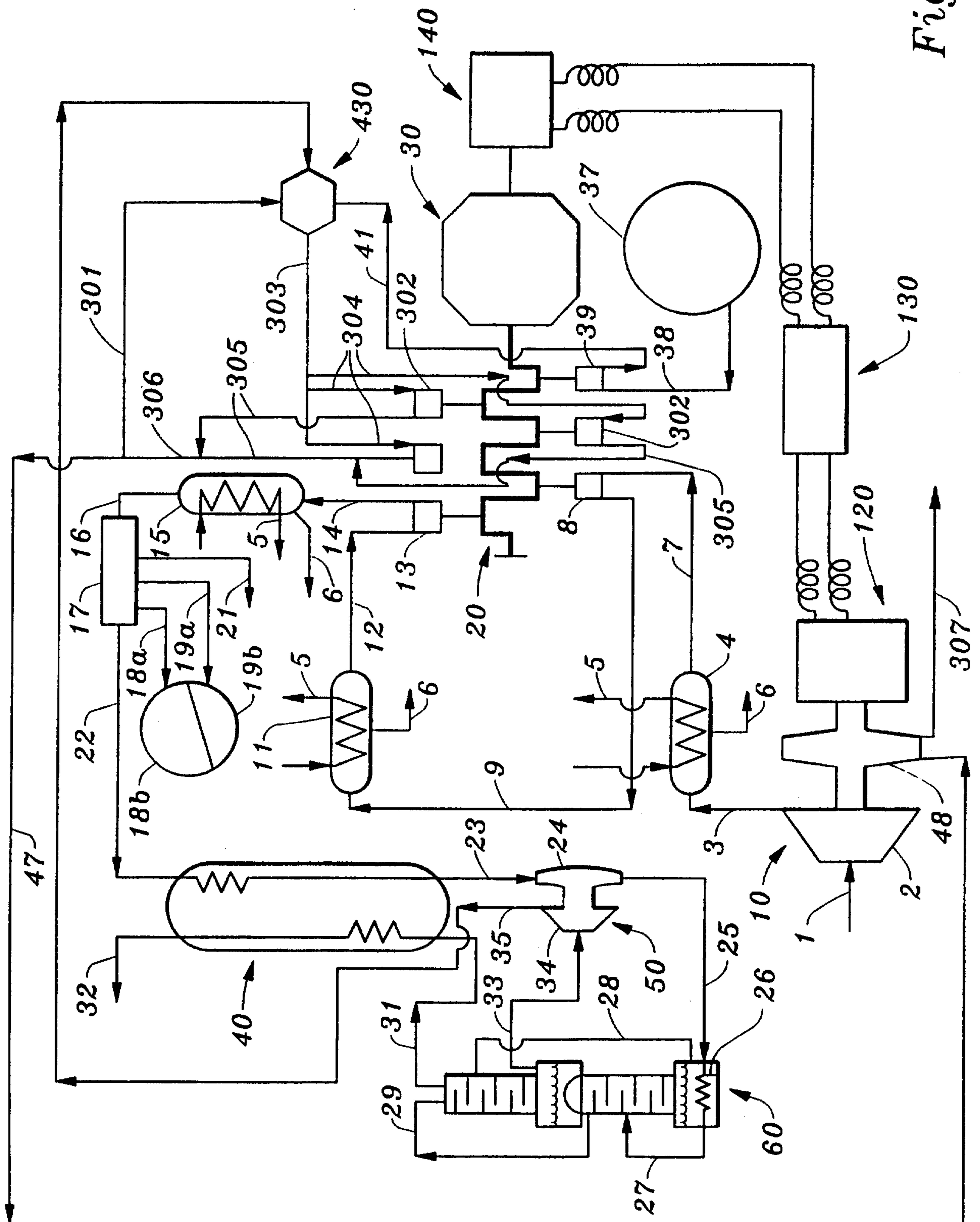


Fig. 9

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Fig. 10



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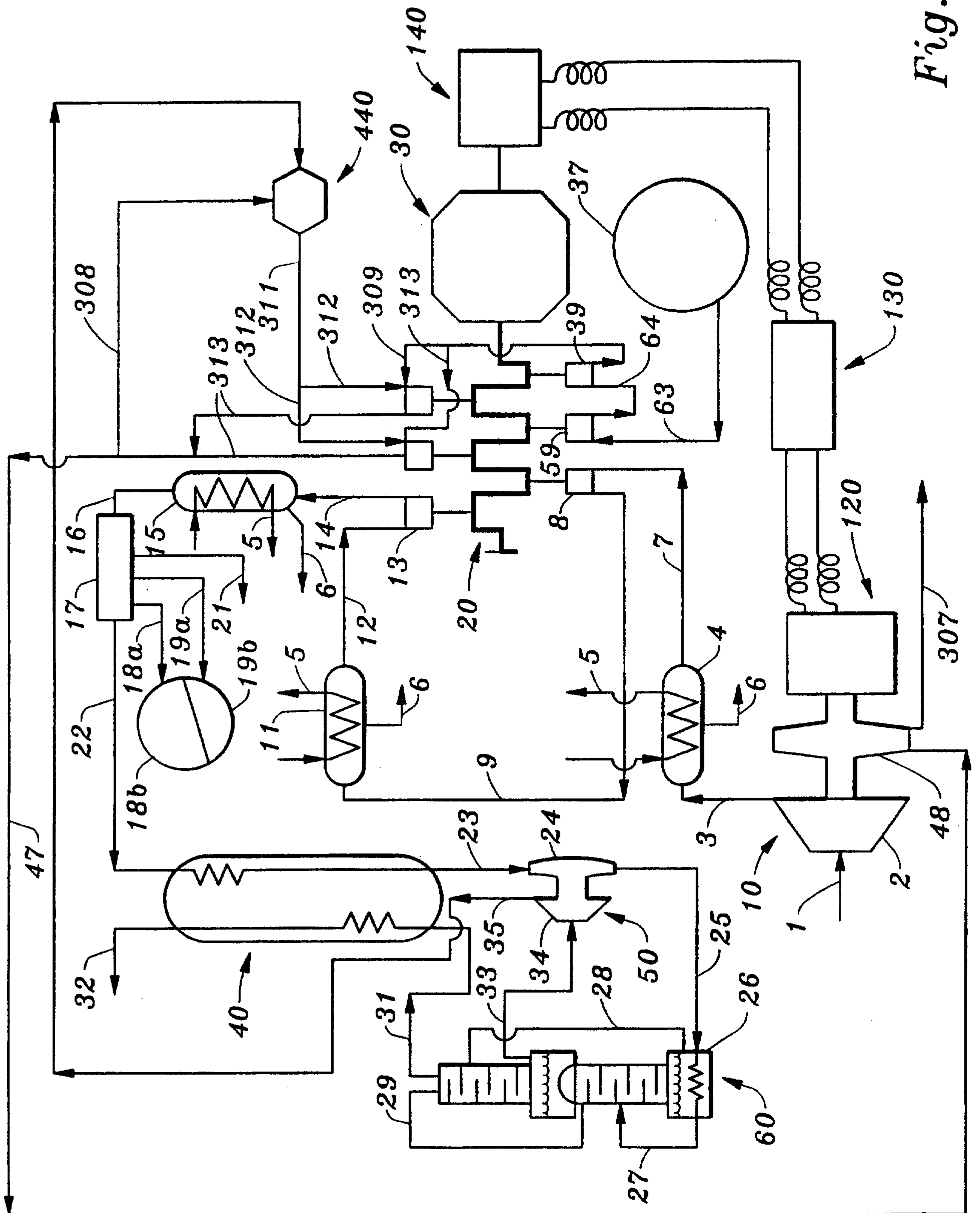


Fig. 11

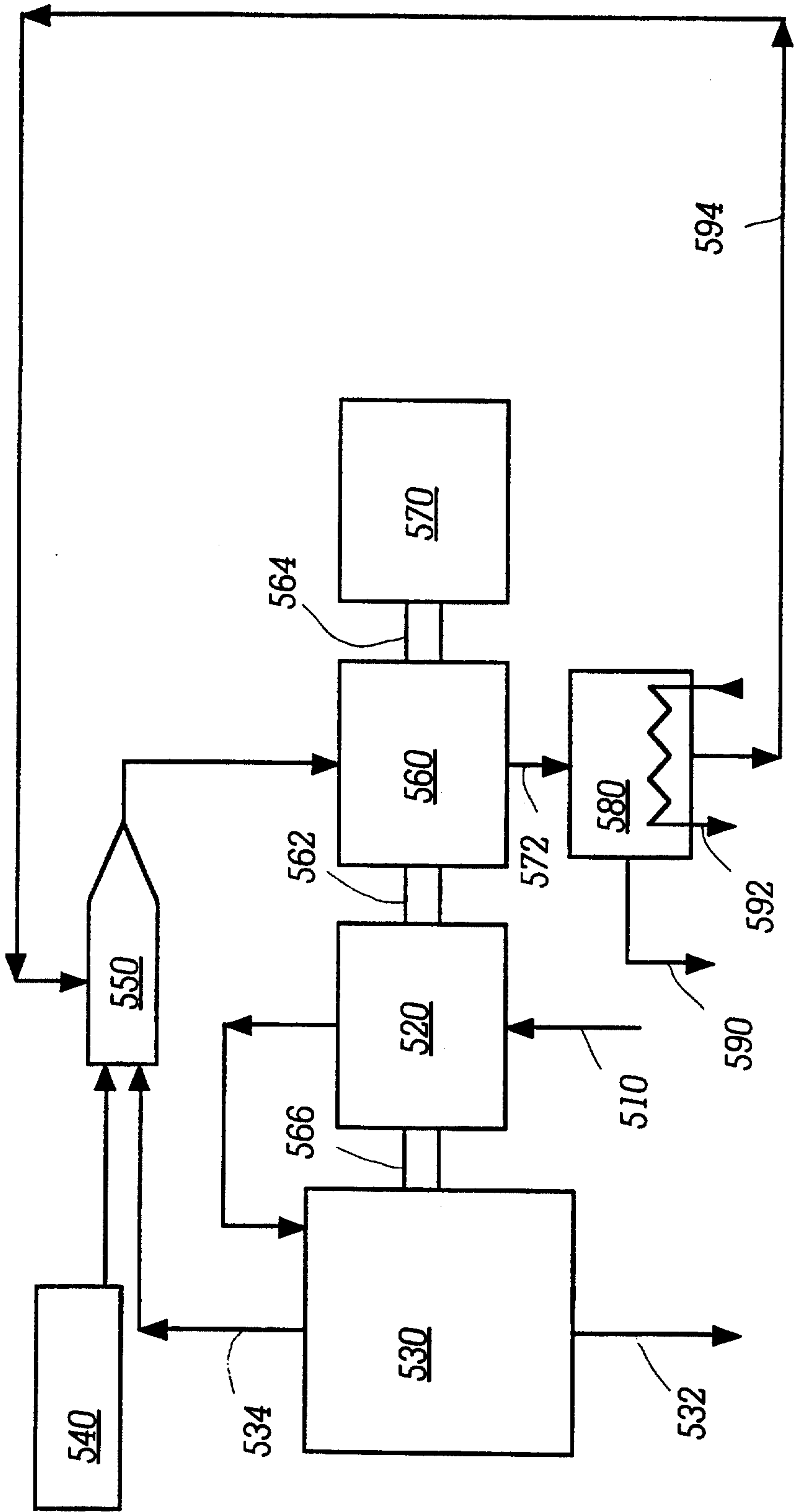


Fig. 12

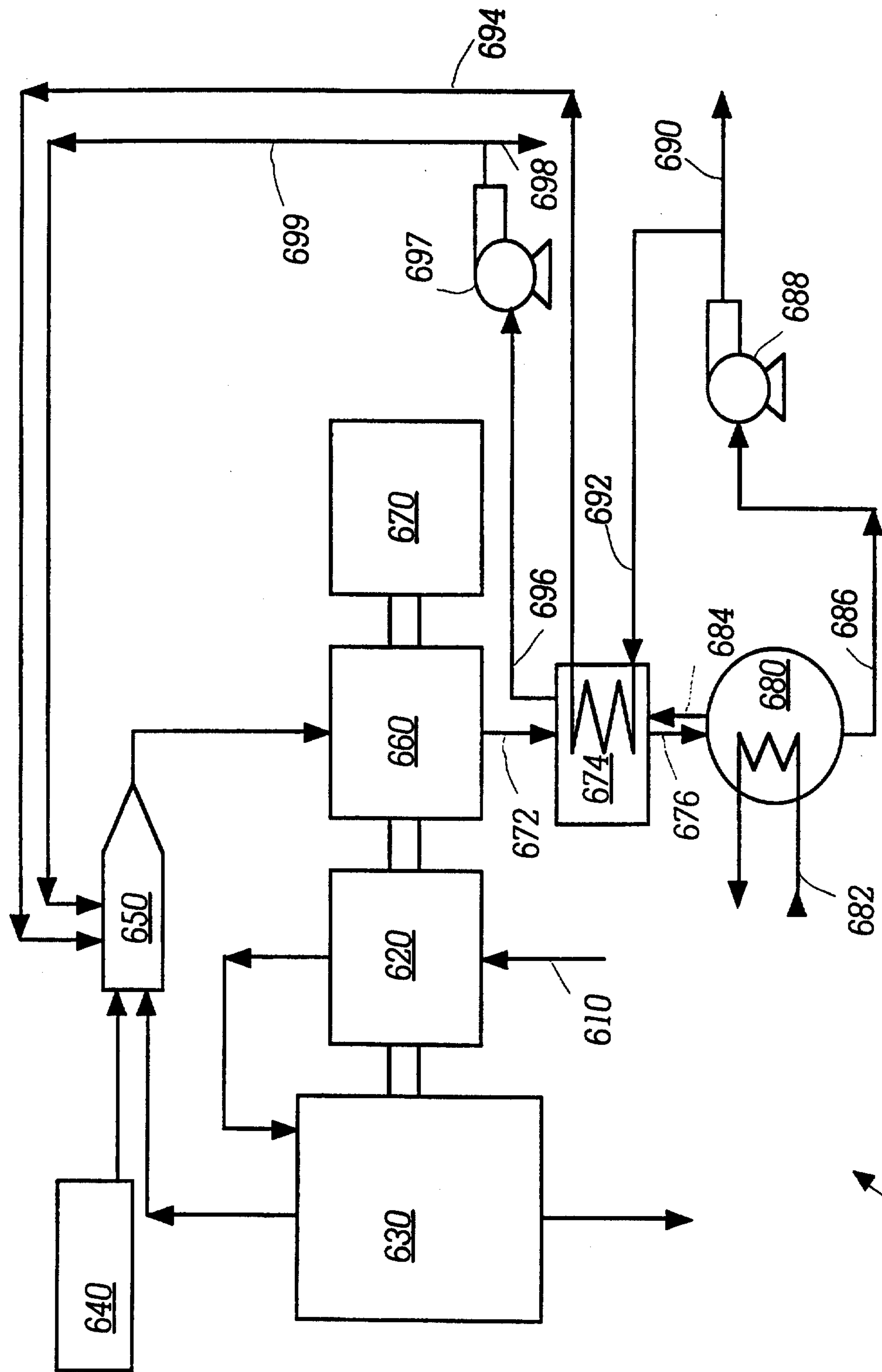


Fig. 13

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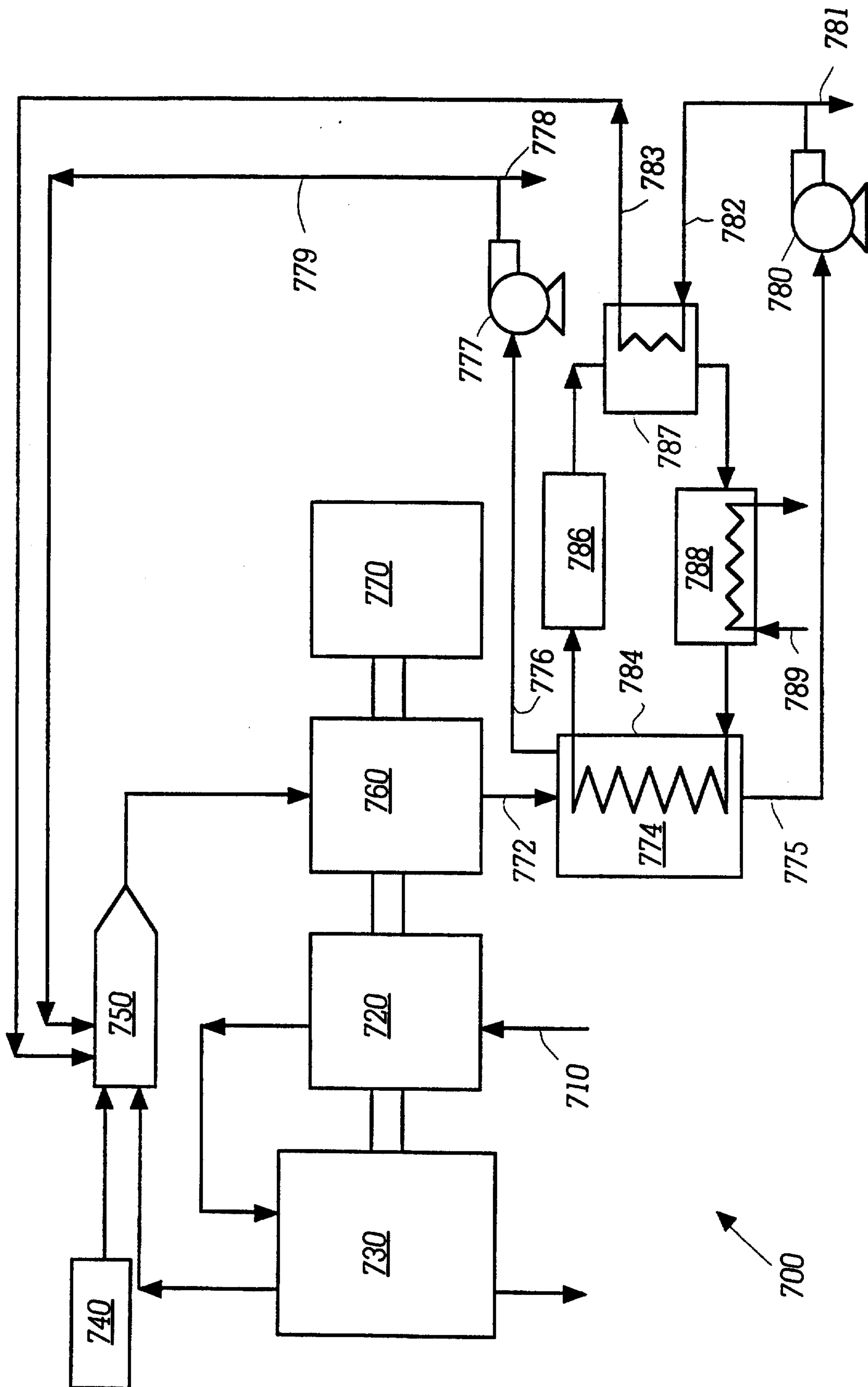


Fig. 14

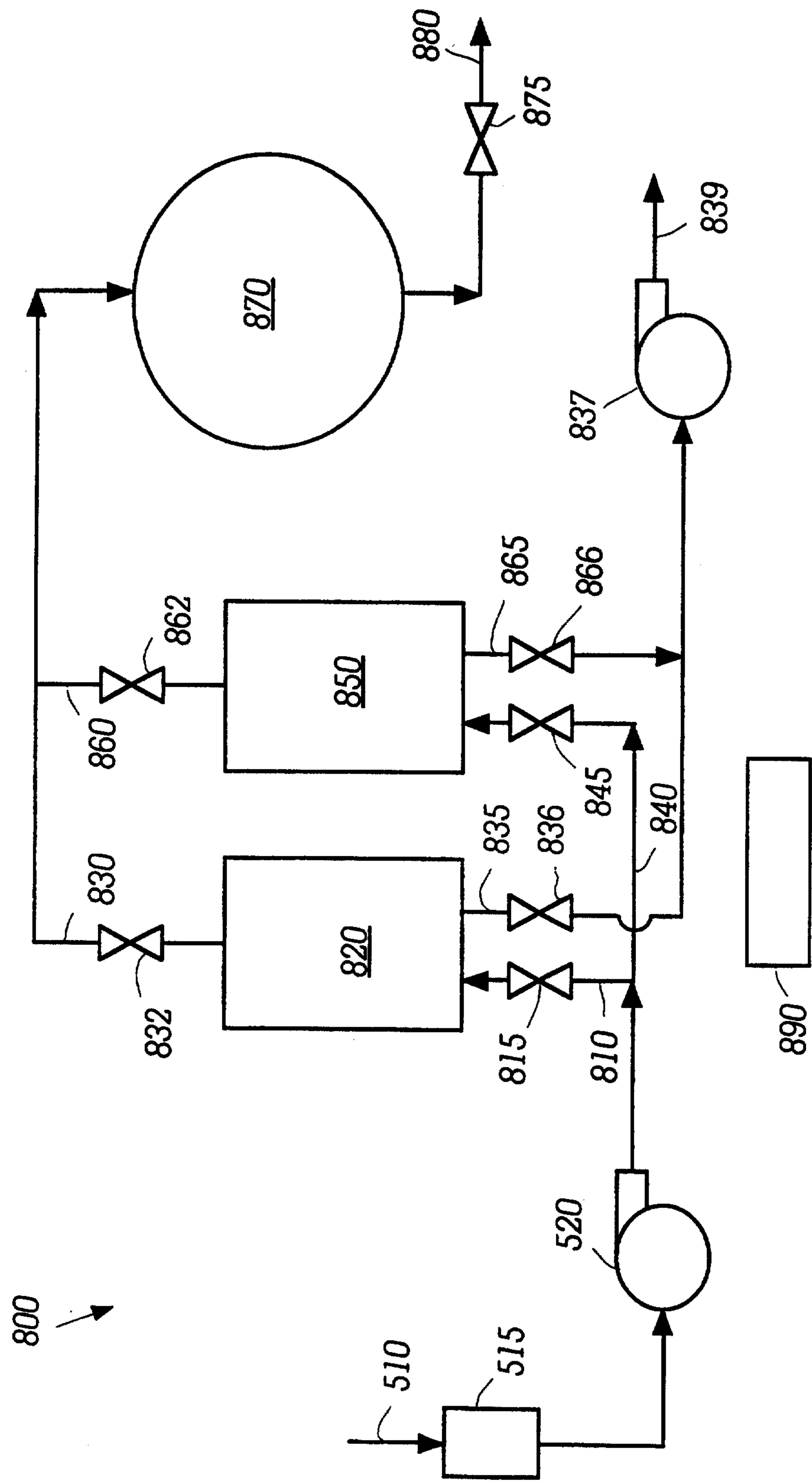


Fig. 15

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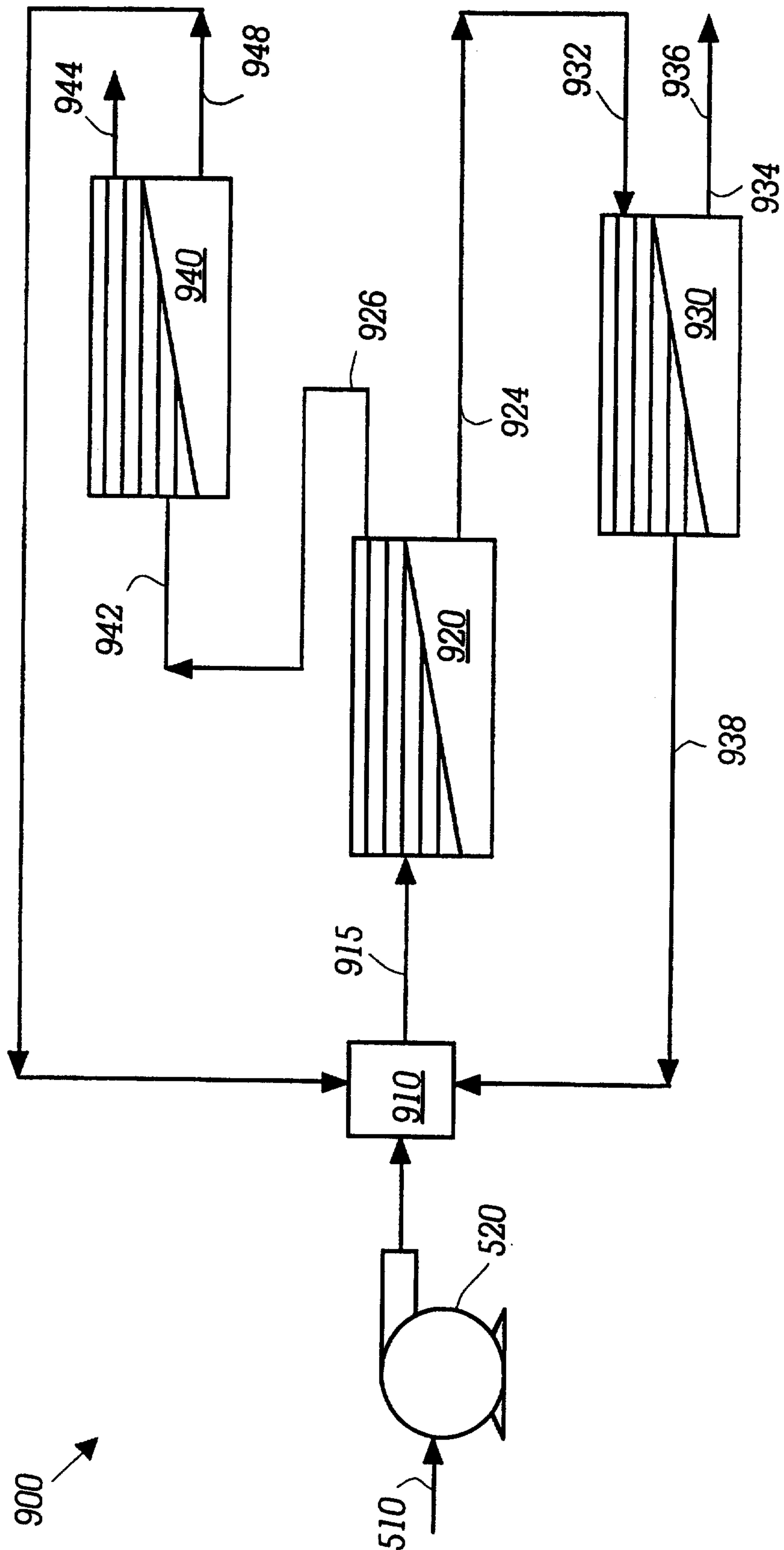


Fig. 16

