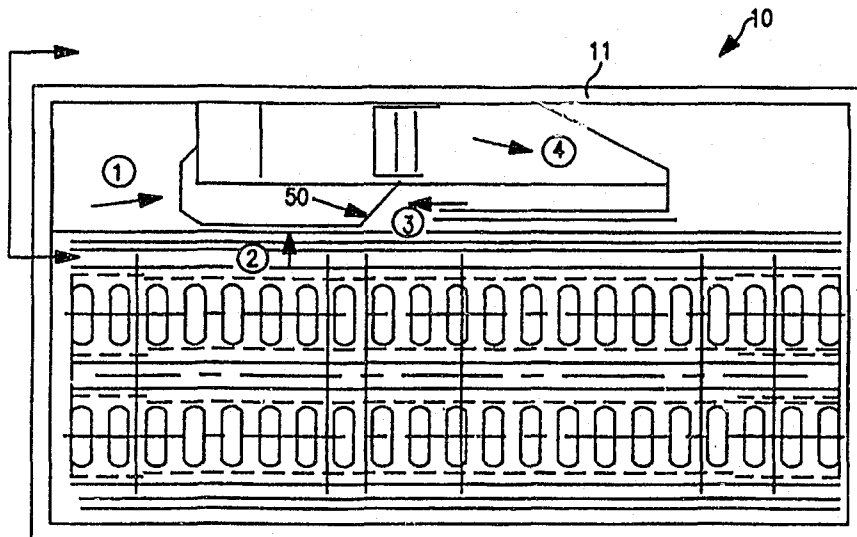




IN

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<p>(21) International Application Number: PCT/US98/08245 (22) International Filing Date: 23 April 1998 (23.04.98) (30) Priority Data: 08/846,993 30 April 1997 (30.04.97) US (71) Applicant: OPLINK COMMUNICATION, INC. [US/US]; Suite 150, 2381 Zanker Road, San Jose, CA 95131 (US). (72) Inventor: BRIA, Michael, P.; 943 South Jackson Street, Green Bay, WI 54301 (US). (74) Agent: BITTMAN, Mitchell, D.; Sequa Corporation, 3 Univer- sity Plaza, Hackensack, NJ 07601 (US).</p>		<p>(81) Designated States: AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GE, GH, GM, GW, HU, ID, IL, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).</p> <p>Published <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i></p>

(54) Title: OPEN BURNER PLENUM FOR A FLOTATION DRYER



(57) Abstract

Air flotation dryer (10) for travelling web (W) includes a housing (11) having a web inlet (12) and a web outlet (13), a plurality of elongated air nozzles arranged transversely to the direction of movement of the web (W) and located on opposite sides. Thereof, the nozzles being secured directly to, supported by and in air-receiving communication with longitudinally extending supply air ducts. A fan communicates with the supply air ducts to supply air to the nozzles. A draw-through style burner fires into the dryer enclosure and the proper amount of air flow to be heated by the burner is regulated such as by a return air screen (50) having a predetermined or variable open area, resulting in a simpler design and a lower pressure drop than in the conventional ducted design where the recirculation air is first collected in a duct and is then heated and sent to the supply fan inlet.

OPEN BURNER PLENUM FOR A FLOTATION DRYERBACKGROUND OF THE INVENTION

The present invention relates to web supporting and drying apparatus. In drying a moving web of material, such as paper, film or other sheet or planar material, it is often desirable that the web be contactless supported during the drying operation, in order to avoid damage to the web itself or to any ink or coating on the web surface or surfaces. A conventional arrangement for contactlessly supporting and drying a moving web includes upper and lower sets of air bars extending along a substantially horizontal stretch of the web. Heated air issuing from the air bars floatingly supports the web in a substantially sinusoidal path and expedites web drying. The air bar array is typically inside a dryer housing which can be maintained at a slightly sub-atmospheric pressure by an exhaust blower that draws off the volatiles emanating from the web as a result of the drying of the ink or coating thereon.

U.S. Patent No. 3,739,491 discloses a high velocity air flotation dryer for drying a running web along the lines of the foregoing. A plurality of spaced air nozzles are positioned on opposite sides of the web. Heated air issuing from the impingement nozzles impinges on the running web to floatingly support and dry the web. The nozzles are in air-receiving communication with an air supply fan through suitable ducting. A burner is located in the ducting downstream from the supply fan outlet for heating the supply air which flows through the air nozzles and impinges on the web. The burner employed is a blow-through type, in that it is located on the outlet or

pressure side of the supply air fan. As a result, in order to supply combustion air to the burner, a fan or blower which has a higher pressure output than the supply air fan is required, which can be expensive.

5 In conventional designs where a draw-through style burner is used, a duct or large plenum collects the return air, and the burner fires into that duct or plenum to heat the air. The duct or plenum is in communication with the inlet of the supply air fan, and supplies the thus heated return air to the fan.
10 Such an arrangement necessarily sends all of the return air past the burner, and is not efficient.

It is therefore an object of the present invention to reduce dryer cost by eliminating ducting otherwise necessary for burner operation. Reduced ductwork also decreases the
15 supply fan pressure requirement which reduces motor size and energy usage.

It is a further object of the present invention to provide a draw-through style burner which fires directly into the dryer enclosure.

20 It is a still further object of the present invention to regulate the amount of air subjected to the burner flame.

SUMMARY OF THE INVENTION

The problems of the prior art have been overcome by the
25 present invention, which provides an air flotation dryer for floatingly drying travelling webs. The dryer includes a housing having a web inlet and a web outlet spaced from the web inlet, and a plurality of elongated air nozzles arranged

transversely to the direction of movement of the web and preferably located on opposite sides of the web, the nozzles being secured directly to, supported by and in air-receiving communication with longitudinally extending supply air ducts.

5 An air supply fan is in communication with the supply air ducts to supply air to the nozzles. Heat is provided to the apparatus with a draw-through style burner, which fires into the dryer enclosure and the proper amount of air flow to be heated by the burner (e.g., flowing past the burner) is
10 regulated such as by a return air screen having a predetermined or variable open area, resulting in a simpler design and a lower pressure drop than in the conventional ducted design where the recirculation air is first collected in a duct and is then heated and sent to the supply fan inlet.

15

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a top view of the flotation dryer in accordance with the present invention;

Figure 2 is a burner plenum/fan inlet flow scheme;

Figure 3 is an illustration showing header air bar
20 temperatures with no fan return air screens;

Figure 4 is an illustration showing header air bar temperatures with all of the return air flowing past the burner.

Figure 5 is an illustration showing header air bar
25 temperatures with a return air screen in accordance with the present invention;

Figure 6 is an illustration showing temperature measurements at the fan inlet screen and fan inlet cone with

no fan return air screen;

Figure 7 is an illustration showing temperature measurements at the fan inlet screen and fan inlet cone with all return air passing by the burner;

5 Figure 8 is an illustration showing temperature measurements at the fan inlet screen and fan inlet cone with a return air screen in accordance with the present invention;

Figure 9 is a front view of the flotation dryer in accordance with the present invention;

10 Figure 10 is an isometric view of the flotation dryer in accordance with the present invention;

Figure 11 is a top view of the flotation dryer in accordance with an alternative embodiment of the present invention;

15 Figure 12 is a front view of the flotation dryer in accordance with an alternative embodiment of the present invention;

Figure 13A is a schematic view of an air flow resistance panel having a single opening in accordance with an alternative
20 embodiment of the present invention;

Figure 13B is a schematic view of an air flow resistance panel having a single adjustable opening in accordance with an alternative embodiment of the present invention;

Figure 13C is a schematic view of an air flow resistance
25 panel having multiple openings in accordance with an alternative embodiment of the present invention; and

Figure 13D is a schematic view of an air flow resistance panel having multiple adjustable openings in accordance with

an alternative embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Turning first to Figures 1, 9 and 10, there is shown
5 generally at 10 a floatation dryer in accordance with the
present invention. The dryer 10 is defined by a housing 11
having a web W inlet 12 and web W outlet 13 spaced from the
inlet 12. The housing 11 can be constructed of any suitable
material, such as steel, and preferably is insulated. A
10 plurality of spaced air nozzles, which can include HI-FLOAT®
air bars commercially available from Grace Tec Systems, are
arranged above and below the path of the web in air receiving
communication with air supply ducts. Heated air emitted from
the air nozzles both floats and dries the running web. Means
15 for heating the air preferably comprises a draw-through style
burner associated with the dryer housing at 100, and in
communication with the supply air fan inlet. A combustion
blower may be used in connection with the burner if necessary,
and if used, need only operate at a lower pressure, typically
20 3-4" wg. No collection duct or plenum for the air returning
to the supply fan is necessary. The burner heats a portion of
the recirculation air prior to its entry into the supply air
fan inlet.

Located in the path of air entering the fan inlet is air
25 flow resistance means for inhibiting or obstructing the flow
of air, preferably a return air screen 50. The air flow
resistance means serves at least two functions. First, it
helps prevent debris from entering the supply air stream.

Second, it regulates the flow of air past the burner so that the optimum amount of air is heated prior to entering the supply fan inlet. The importance of regulating the amount of air heated by the burner is due to the need to keep air temperatures in the dryer below a certain level. This maximum dryer temperature may be due to limits resulting from the type of material of construction and/or limits due to process constraints. A typical process constraint may require that an air stream containing a particular solvent be kept below a set temperature to prevent the solvent from forming undesired by-products in the air stream. Too little air reaching the burner will cause high temperatures in the dryer. Conversely, sending all the air past the burner is not efficient (a ducted system has this arrangement). Such an arrangement requires more space and/or more energy.

The drying process will dictate the amount of heat input and make-up air necessary for the dryer to operate effectively and safely. Based upon this information, the amount of air flowing past the burner can be determined so that the mixed air temperature, make-up and recirculation air streams will be acceptable for the process and dryer materials. The configuration of the air flow resistance means such as a return air screen 50, in particular, the open area of air flow resistance means, is designed based upon these parameters, bearing in mind that too much open area might not provide a durable enough design, and too small an open area would increase system pressure drop and lower dryer efficiency. In all cases, resistance means with particular total and open

areas can be replaced with resistance means of some other total and open areas which will have equal pressure drop if the total area ratio of the two designs is related by the following equation:

5

$$A_1/A_2 = (K_2/K_1)^{1/2}$$

where K_2 and K_1 are loss coefficients of the resistance means and depend on the open area thereof.

10 The burner is exposed to make-up air and only the amount of recirculation air required for the system to operate efficiently and keep air temperatures to some maximum value. Management of air flow is thus effectively accomplished.

Referring again to Figure 1, the flow of air to and from
15 the supply air fan is shown as arrows numbered 1 through 4. Only flow 1 is heated by the burner flame. In the embodiment shown, the open area of the screen 50 which each air flow encounters is set to a value which will allow sufficient flow in path 1 (past the burner) to keep the air temperature in flow
20 1 at some desired value, so that the temperature in the dryer is kept at some desired value. (Path 4 is the total outlet of air from the fan.)

For example, assume for a given process that an average
temperature of 600°F is desired in flow 1 at a nominal burner
25 firing rate to minimize the formation of undesired combustion by-products in the recirculating air stream. For a supply air fan outlet temperature of 500°F, make-up air flow of 1990 scfm, supply air flow of 16,500 acfm, and a return air temperature

of 420°F, it was found that the amount of air flowing past the burner is large relative to the amount of air returning to the fan from the other directions (flow paths 2 and 3). Accordingly, path 1 needs high open area to minimize pressure drop. Typically 50 to 75% open area is suitable. For this application, 56% is the preferred open area. In the other paths, 2 and 3, less flow is needed so that a more restrictive air flow resistance means (e.g., a screen with less open area) is desired to equalize the pressure drop in these paths. Typically, this screen would be 10-50% open area, more preferably 15 to 40% open area. For this application, an open area of 30% is most preferred for this screen. This determination is made by first calculating the flow needed in the stream past the burner, and then calculating the pressure drops through the parallel flow paths. The open area of each screen is adjusted until the parallel flow paths have equal or substantially equal pressure drop for the desired flow rates.

Those skilled in the art will recognize that other means for regulating the flow of air to the burner and/or directly to the supply fan inlet could be used. For example, a separate filtering screen and a separate flow control screen or screens could be used, or one or more dampers could be used to control the air flow.

An alternative design is shown in Figures 11 and 12. A supply fan inlet screens 50' is positioned at the supply fan inlet as shown, and acts as a filtering screen. The air flow resistance means comprises panel 50A' having one or more cut-outs or apertures to control air flow in flow paths 2 and 3 as

shown. Various configurations of the cut-outs can be used, as detailed in Figures 13A, 13B, 13C and 13D. For example, Figure 13A depicts a panel 50A' having a single, non-adjustable cut-out 52. Figure 13B shows a panel 50A' having a single cut-out 52 with a damper 53 associated therewith in order to vary the flow resistance. Figure 13C shows a panel 50A' having multiple non-adjustable cut-outs 52 (four shown). This embodiment prevents a concentration of air from occurring. A concentration of air may be deleterious to web handling in the dryer. Figure 13D shows a panel 50A' having multiple cut-outs 52 that are adjustable such as by means of a moveable plate 54 in order to vary the flow resistance.

The cut-out or cut-outs in the panels are preferably 10-50% of the panel areas, most preferably about 30%. The use of such panels to control air flow results in a reduced possibility of the apparatus becoming plugged with debris, thereby resulting in less maintenance. Also, the ease of adjustability of flow resistance with the embodiments such as those shown in Figures 13B and 13D is advantageous. Specifically, for many applications, a fixed screen or panel flow resistance which is calculated for some typical operating condition will be acceptable. However, the advantage of having a variable flow resistance would occur in situations where the process conditions change frequently, perhaps because different solvents are removed for different coatings applied to the web being dried. Different solvents might require varying exhaust and make-up air rates and/or maximum process air temperatures. These might require that more or less air flow be heated by

(e.g., flow past) the burner and that the flow resistance of the other path to the supply fan change. Also, rather than re-design the return air panels for different dryer sizes such as wider webs or longer zone lengths, it may be easier to use one
5 panel design wherein the flow resistance is variable. This design is then adjusted to work acceptably for each dryer size and operating conditions.

Figure 2 illustrates the method used to calculate the appropriate open area of the air flow resistance means for each
10 parallel flow path back to the supply fan in the following examples. The air volume for each path will be that value that causes each path to have equal or substantially equal pressure drop. The schematic illustrates the main source of pressure drop in each path.

15 Slow moving air is accelerated through a small opening of area A_{out} . For the area ratio (A_{in}/A_{out}) normally found in this situation, the loss coefficient K is 0.6. Eventually, all of the parallel air flows must combine at the fan inlet. For combining flows, the loss coefficient K depends on the ratios
20 of the areas of the inlet leg and the outlet (A_{BR}/A_{total}) and the flow ratio of inlet flow to outlet flow (A_{BR}/Q_{total}) .

Normally, the drying process will determine the amount of heat input and make-up air necessary for the dryer to operate effectively and safely. Then the amount of air being heated
25 by the burner (e.g., flowing past the burner) can be determined so that the mixed air temperature, make-up and recirculation air streams, will be acceptable for the process and dryer materials. Next, the remaining recirculation air is assumed

to flow back to the fan by the alternate parallel flow paths. The open area of the screen for each path can now be estimated through an iterative process such that the strength of the screen and filtering characteristics of the screen are
5 adequate, and the pressure drop is acceptable (small open areas would increase system pressure drop and lower dryer efficiency). When all of the flow paths have equal or substantially equal pressure drop for the assumed flow rates, the design is complete.

10

COMPARATIVE EXAMPLE 1

For purposes of comparison, header supply air temperatures were measured in a dryer having no return air screen or other means to regulate air flow, and the location of measurement and
15 results are shown in Figure 3. This illustrates that the non-uniformity of air flow and temperature at the fan inlet due to the absence of the air screen leads to poor uniformity in supply air temperature to the air bars.

Temperature was also measured at the fan inlet cone, at
20 eight 45° intervals from the 12 o'clock position. Variations in temperature ranged from 332°F to 604°F, as shown in Figure 6. Similarly, screen temperatures were measured at positions two inches left and right of the centerline and four inches vertically starting five inches from the top edge of the screen
25 in flow path 1 of Figure 1, and the results are shown in Figure 6. The screen temperatures were non-uniform and exceeded 1400°F at some locations, which is undesirable.

COMPARATIVE EXAMPLE 2

Additional temperature measurements were carried out as in Comparative Example 1, except that the condition of 0% open area in the flow paths other than the path past the burner was maintained. Figure 4 illustrates the non-uniformity of supply air temperature to the air bars, and Figure 7 sets forth the results of screen temperature and fan inlet cone temperature measurements. From these results, it is seen that inlet air temperatures to the fan are much lower and more uniform. However, the average air bar pressure (Figure 4) was only 2.0" wg, dropping from 3.1" wg. This results in an inefficient design, as the fan rpm would need to increase along with fan power to obtain the same air bar performance.

15

EXAMPLE 1

Air screens designed as detailed above were installed in a dryer, and the same header air bar temperature, screen temperature and fan inlet cone temperature measurements were made as in the comparative examples. The results are shown in Figures 4 and 8. The header air temperatures are uniform and the average air bar pressure is nearly equal to the pressure measured with no screens, 3.0" versus 3.1" wg. In Figure 8, temperatures at the fan inlet cone only vary by 52°F, and fan inlet screen temperatures are also uniform.

25

What is claimed is:

1. An air flotation dryer for drying a running web in a web path, comprising:

5 a dryer housing having a web inlet and a web outlet spaced from said web inlet;

a plurality of air bars positioned in said dryer housing to floatingly support and dry said running web;

10 a supply air fan having a fan inlet and a fan outlet, said fan outlet being in communication with said plurality of air bars via headers for supplying heated air to said air bars;

a burner associated with said dryer housing for heating a portion of air entering said fan inlet; and

15 air flow resistance means between said burner and said fan inlet for regulating the amount of air which is heated by said burner.

2. The dryer of claim 1, wherein said air flow resistance means comprises a return air screen having a predetermined open area.

20 3. The dryer of claim 1, wherein said air flow resistance means comprises a solid panel having one or more openings therein.

4. The dryer of claim 3, wherein the size of said one or more openings in said panel is adjustable.

25 5. The dryer of claim 1, wherein said burner fires directly into said dryer housing.

6. The dryer of claim 2, wherein said burner fires directly into said dryer housing.

7. The dryer of claim 1, wherein air flow to said supply

air fan comprises air from: (1) a first air flow path flowing past said burner comprising a first portion of recirculation air; and (2) a second air flow path comprising a second portion of recirculation air, and wherein said air flow resistance
5 means is positioned in said first air flow path.

8. The dryer of claim 1, wherein air flow to said supply air fan comprises air from: (1) a first air flow path flowing past said burner comprising a first portion of recirculation air; and (2) a second air flow path comprising a second portion
10 of recirculation air, and wherein said air flow resistance means is positioned in said second air flow path.

9. The dryer of claim 1, wherein air flow to said supply air fan comprises air from: (1) a first air flow path flowing past said burner comprising a first portion of recirculation
15 air; and (2) a second air flow path comprising a second portion of recirculation air, and wherein said air flow resistance means is positioned in said first and second air flow paths.

10. The dryer of claim 7, wherein said second air flow path comprises air flowing across said headers and air flow
20 parallel to said headers.

11. The dryer of claim 8, wherein said second air flow path comprises air flowing across said headers and air flow parallel to said headers.

12. The dryer of claim 1, wherein said burner is a draw-
25 through burner.

13. The dryer of claim 2, wherein said burner is a draw-through burner.

14. The dryer of claim 2, wherein said return air screen

has about 10-50% open area.

15. An air flotation dryer for drying a running web in a web path, comprising:

a dryer housing having a web inlet and a web outlet spaced
5 from said web inlet;

a plurality of air bars positioned in said dryer housing in communication with ducting;

a supply air fan having an fan inlet and a fan outlet, said fan outlet being in communication with said plurality of
10 air bars via said ducting for supplying heated air to said air bars to floatingly support and dry said running web;

a burner associated with said dryer housing for heating a portion of air entering said fan inlet;

a first air flow path to said fan flowing past said burner
15 consisting essentially of make-up air and a first portion of air recirculating from said air bars;

a second air flow path to said fan consisting essentially of a second portion air recirculating from said air bars, said second portion of air flowing into said fan inlet without
20 passing past said burner; and

air flow resistance means between said burner and said fan inlet for regulating the amount of recirculation air in said first portion of air recirculating from said air bars.

16. The dryer of claim 15, wherein said air flow
25 resistance means comprises a return air screen in at least said first air flow path, said return air screen having a predetermined open area.

17. The dryer of claim 16, wherein said return air screen

has about 10-50% open area.

18. The dryer of claim 15, wherein said air flow resistance means comprises a solid panel having one or more openings therein.

5 19. The dryer of claim 18, wherein the size of said one or more openings in said panel is adjustable.

20. The dryer of claim 18, wherein 10-50% of the area of said panel is open.

21. A method of controlling the amount of air heated by
10 a burner in an air flotation dryer having a dryer housing having a web inlet and a web outlet spaced from said web inlet; a plurality of air bars positioned in said dryer housing to floatingly support and dry said running web; a supply air fan having a fan inlet and a fan outlet, said fan outlet being in
15 communication with said plurality of air bars via headers for supplying heated air to said air bars; and a burner associated with said dryer housing for heating a portion of air entering said fan inlet; said method comprising:

causing a predetermined portion of air to be heated by
20 said burner prior to entering said supply fan inlet.

22. The method of claim 21, wherein air flow resistance means is positioned in said dryer housing to cause said predetermined portion of air to be heated.

23. The method of claim 22, wherein said air flow
25 resistance means comprises a screen having a predetermined open area.

24. The method of claim 22, wherein said air flow resistance means has a variable open area.

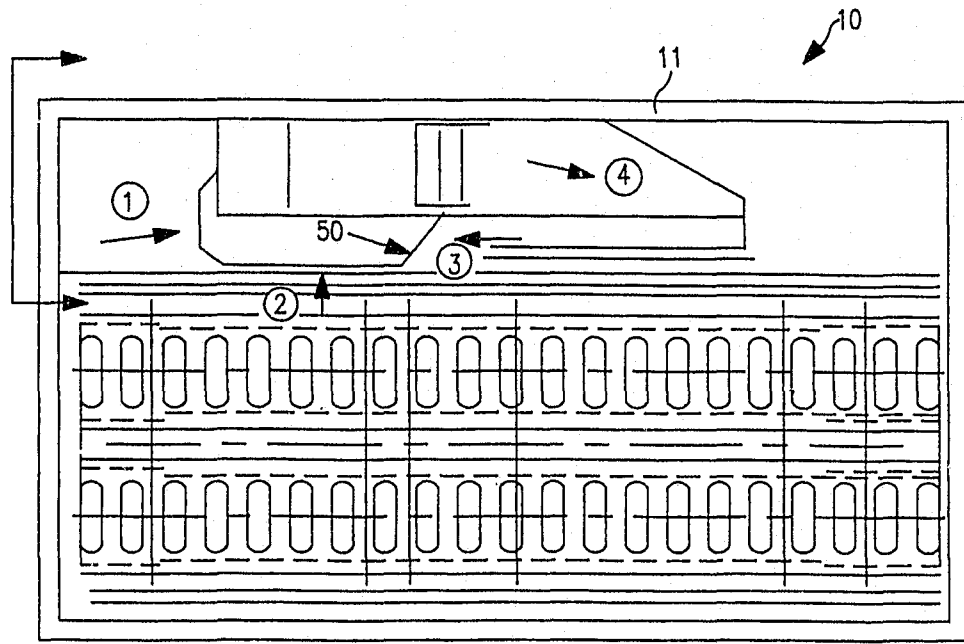


FIG. 1

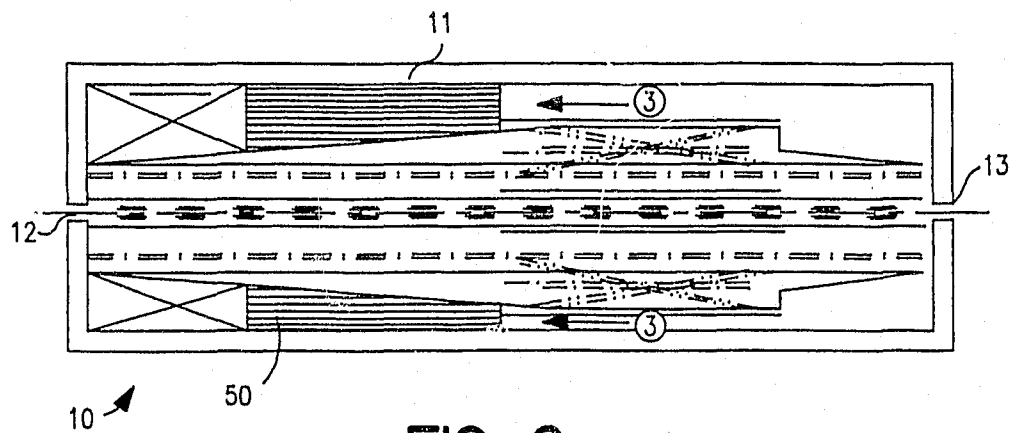


FIG. 9

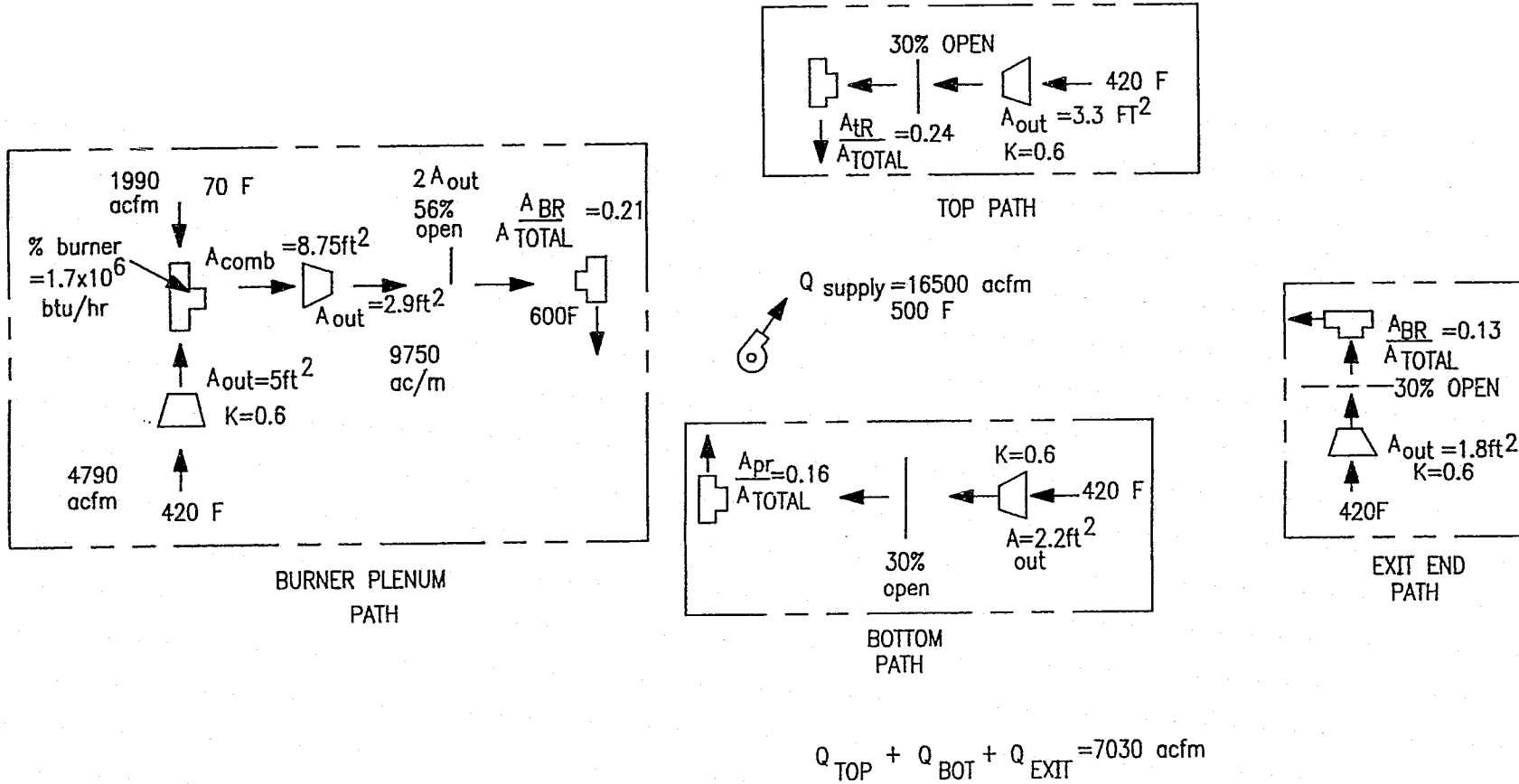


FIG. 2

HEADER AIR TEMPERATURES WITH MAXON OVENPAK BURNER AND NO FAN RETURN AIR SCREENS
STEADY-STATE CONDITIOND, 400 F AIR TEMPERATURE SETPOINT

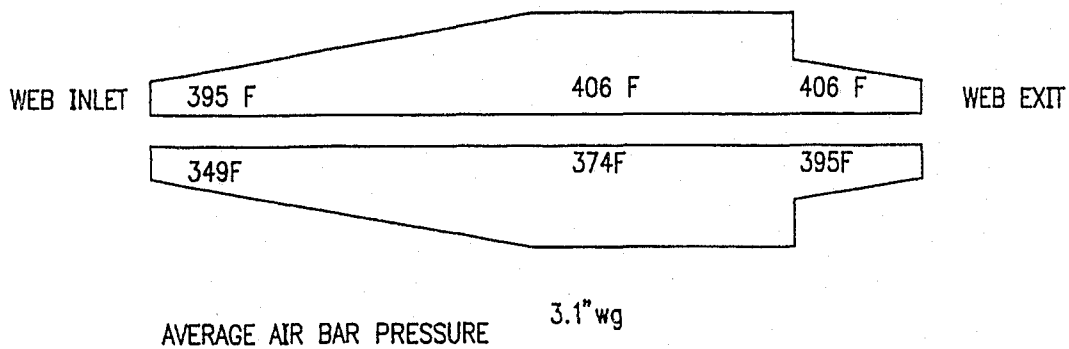
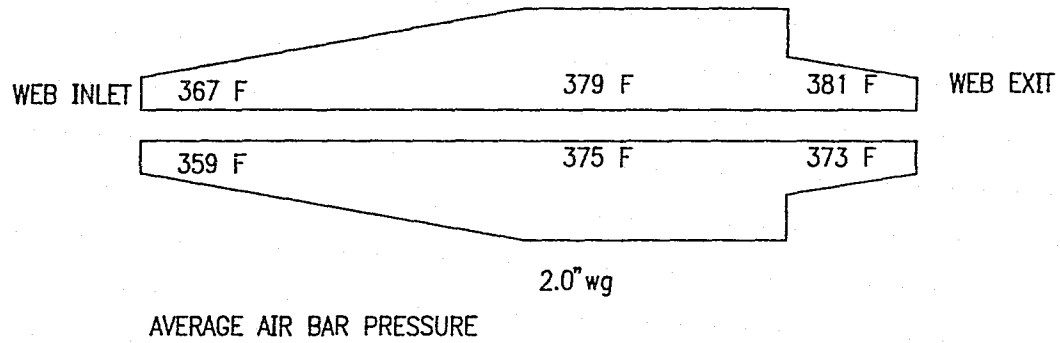


FIG. 3

HEADER AIR BAR TEMPERATURES WITH MAXON OVENPAK BURNER AND ALL RETURN AIR PAST BURNER

STEADY-STATE CONDITIONS, 400 F AIR TEMPERATURE SETPOINT

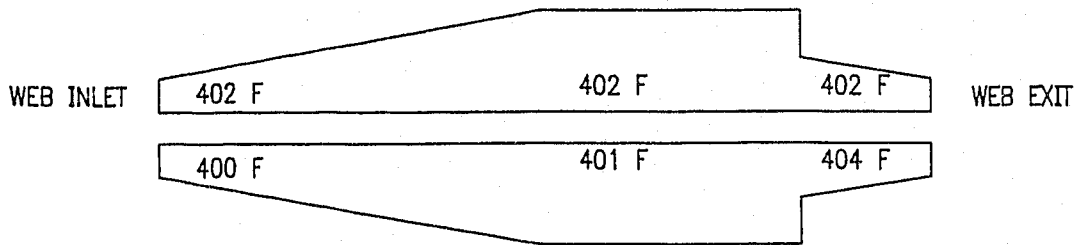


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FIG. 4

SUBSTITUTE SHEET (RULE 28)

HEADER AIR BAR TEMPERATURES WITH MAXON OVENPAK BURNER
AND INITIAL FAN RETURN AIR SCREEN DESIGN
STEADY-STATE CONDITIONS, 400 F AIR TEMPERATURE SETPOINT

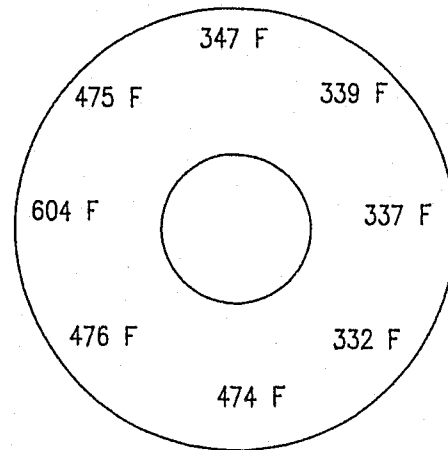


AVERAGE AIR BAR PRESSURE: 3.0" wg

FIG. 5

TEMPERATURE MEASUREMENTS FOR MAXON OVENPAK
BURNER WITH NO FAN RETURN AIR SCREENS

771 F	588 F
1093 F	1240 F
1114 F	1393 F
1044 F	1384 F
1056 F	1475 F
1447 F	1387 F
1027 F	992 F
412 F	431 F
316 F	401 F



FAN INLET CONE
TEMPERATURES

FAN INLET SCREEN
TEMPERATURES

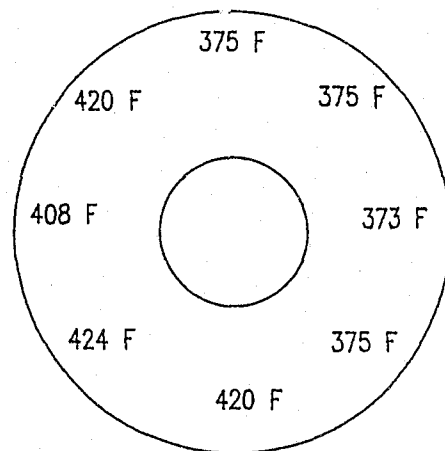
NOTE: STEADY STATE CONDITIONS, 400 F
AIR TEMPERATURE SETPOINT.

FIG. 6

TEMPERATURE MEASUREMENTS FOR MAXON OVENPAK
BURNER WITH ALL RETURN AIR PAST BURNER

366 F	357 F
499 F	500 F
----	506 F
460 F	458 F
413 F	431 F
----	453 F
395 F	413 F
380 F	405 F
369 F	371 F

FAN INLET SCREEN
TEMPERATURES



FAN INLET CONE
TEMPERATURES

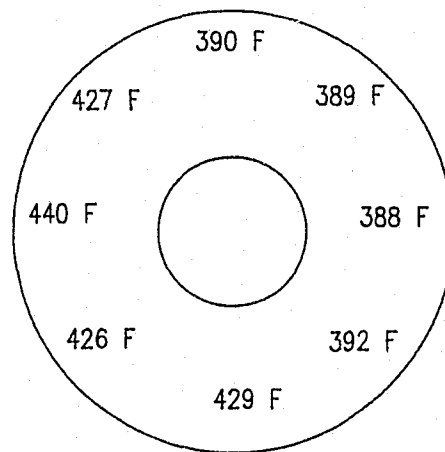
NOTE: STEADY STATE CONDITIONS, 400 F
AIR TEMPERATURE SETPOINT.

FIG. 7

TEMPERATURE MEASUREMENTS FOR MAXON OVENPAK
BUMPER WITH INITIAL FAN RETURN AIR SCREEN DESIGN

420 F	374 F
675 F	560 F
686 F	744 F
580 F	686 F
529 F	597 F
471 F	382 F
401 F	312 F
307 F	324 F
333 F	375 F

FAN INLET SCREEN
TEMPERATURES



FAN INLET CONE
TEMPERATURES

NOTE: STEADY STATE CONDITIONS, 400 F
AIR TEMPERATURE SETPOINT.

FIG. 8

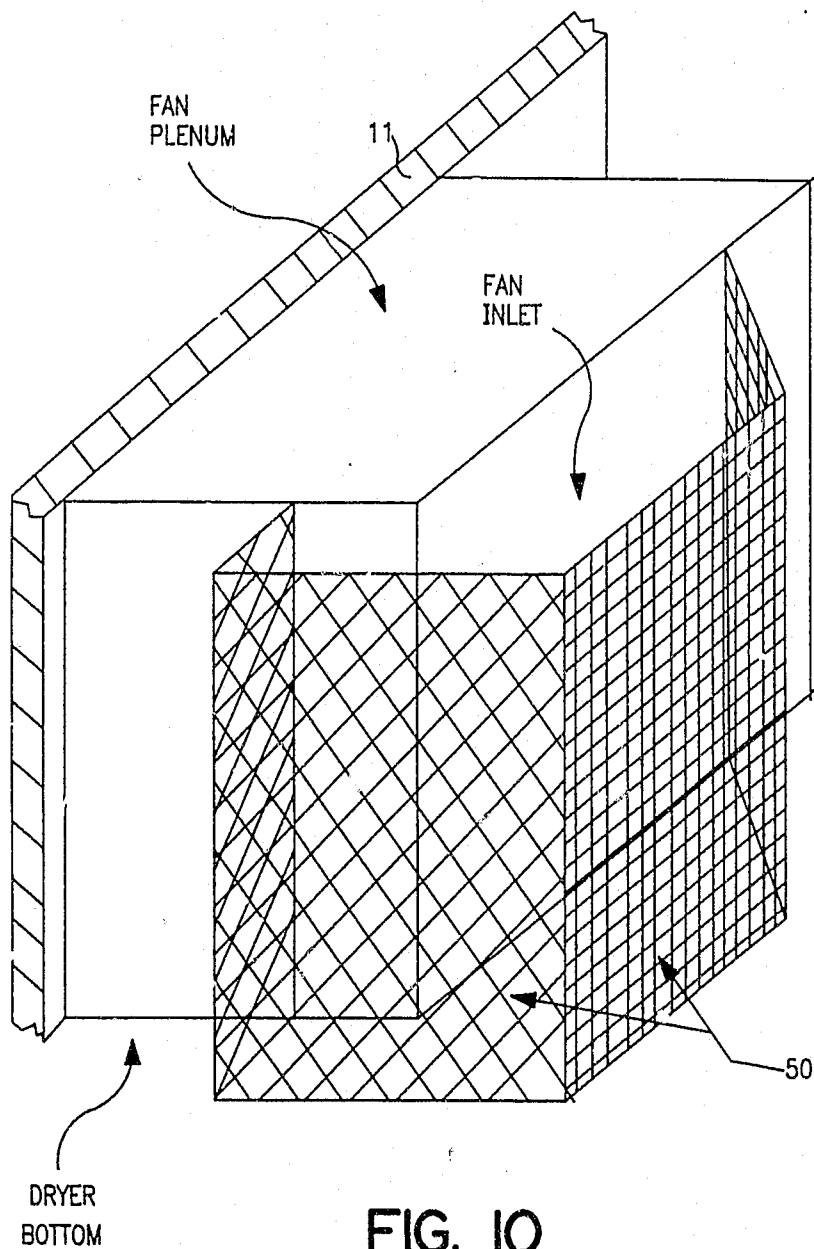


FIG. 10

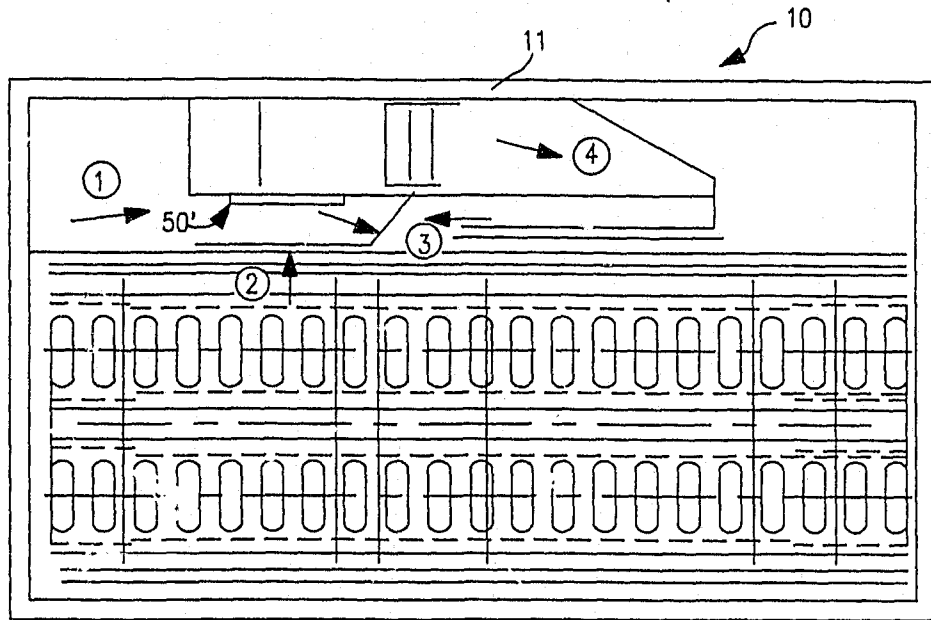


FIG. 11

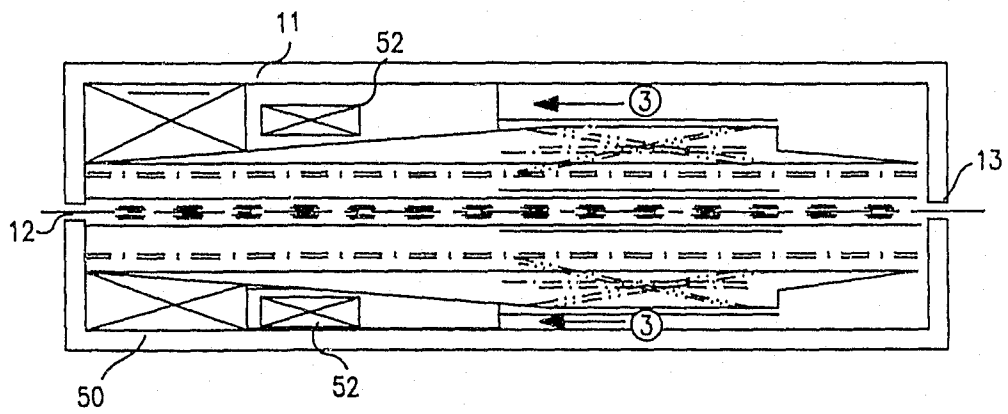


FIG. 12

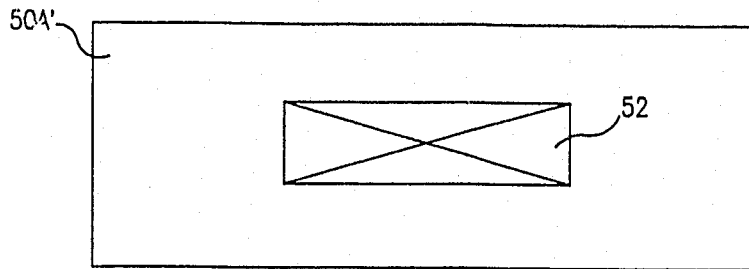


FIG. 13A

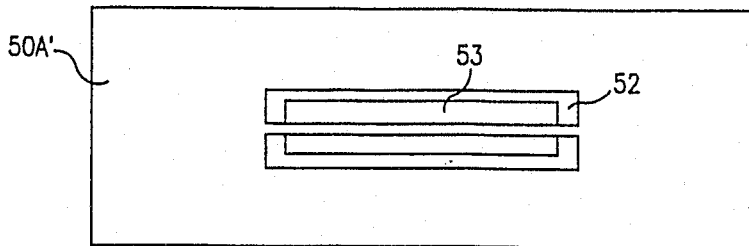


FIG. 13B

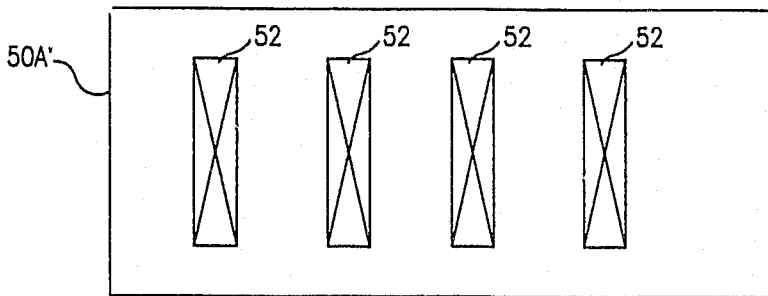


FIG. 13C

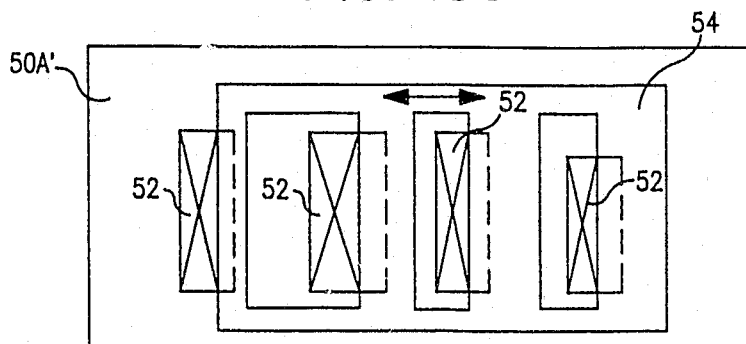


FIG. 13D

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US98/08245

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :F26B 9/00
US CL :34/629,643

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 34/629,643

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
NONEElectronic data base consulted during the international search (name of data base and, where practicable, search terms used)
NONE

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 3,308,555 A (KRUGER) 14 MARCH 1967, SEE THE ENTIRE DOCUMENT.	1-24
A	US 3,739,491 A (CREAPO ET AL) 19 JUNE 1973, SEE THE ENTIRE DOCUMENT.	1-24
A	US 5,608,973 A (KARLSTEDT ET AL) 11 MARCH 1997, SEE THE ENTIRE DOCUMENT.	1-24

 Further documents are listed in the continuation of Box C.
 See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be of particular relevance	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*G* document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 16 JULY 1998	Date of mailing of the international search report OCT 13 1998
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230	Authorized officer <i>R. Caposela</i> RONALD C. CAPOSSELA Telephone No. (703) 308-0688