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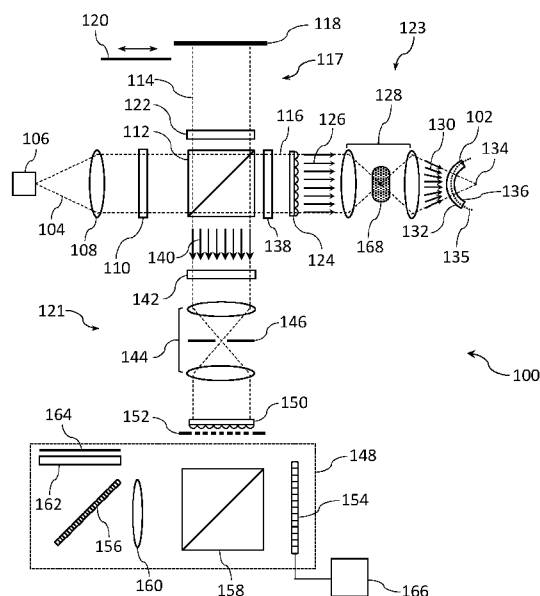


Fig. 1A

(57) Abstract: Apparatus and methods are presented for non-contact in-vivo measurement of one or more properties of a cornea or tear film with spatial resolution. In certain embodiments the cornea/tear film is probed at substantially normal incidence with a converging array of beamlets from a multi-wavelength optical source, and the reflected light analysed interferometrically to generate a time sequence of pachymetry maps. Thickness variations arising from differences between the external and intraocular pressure, e.g. from the ocular pulse or externally applied pressure changes, are measured and analysed to obtain information on a biomechanical response of the cornea. In preferred embodiments the time variation in tear film thickness is measured and subtracted to yield normalised pachymetry data for the biomechanical analysis. In certain embodiments the apparatus is configured to measure the dynamics and profile of the tear film, using either converging or substantially parallel arrays of beamlets.

APPARATUS AND METHOD FOR IN-VIVO MEASUREMENT OF CORNEAL BIOMECHANICAL RESPONSE

Field of the Invention

The invention relates to apparatus and methods for optical metrology, in particular for *in-vivo* measurement of the biomechanical response of the human cornea. However it will be appreciated that the invention is not limited to this particular field of use.

Related Applications

The present application claims priority from Australian Provisional Patent Application No 2018902018 filed on 5 June 2018, the contents of which are incorporated herein by reference.

Background of the Invention

Any discussion of the prior art throughout the specification should in no way be considered as an admission that such prior art is widely known or forms part of the common general knowledge in the field.

Keratoconus is a degenerative condition in which localised thinning and reduced rigidity leads to distortion of the cornea, directly impairing the quality of vision. While the corneal distortions characteristic of more advanced keratoconus are easily detectable by corneal topography or pachymetry, it is preferable to be able to detect the condition at an earlier stage. This would allow for example the screening of people at risk of developing keratoconus so that strategies for managing the condition can be put in place before permanent damage occurs, as well as patient screening prior to refractive surgery. It is thought that early detection of keratoconus, among other corneal diseases, can be effectively achieved by measuring the biomechanical properties of the eye, looking for localised weakening of the cornea. In particular, the focal region of the keratoconic cone is weakened and has different biomechanical properties from other regions of the cornea. This approach may provide discrimination from other perturbations of the cornea that could complicate a diagnosis based purely on geometric features such as corneal elevation and thickness maps.

One technique for measuring the mechanical response of human tissue such as the cornea is optical coherence elastography (OCE), described for example in published US patent application No 2017/0290503 A1 entitled 'Optical coherence elastography to assess biomechanics and detect progression of ocular and other tissues degenerative diseases'. Vibrations in the tissue are excited, e.g. by air puff, ultrasound or mechanical contact, and the

mechanical response measured by optical coherence tomography (OCT). A difficulty with using OCE for corneal measurements is the need to separate the effect of intraocular pressure (IOP) variations from abnormalities in the cornea.

Brillouin microscopy has been proposed as a technique for mapping the mechanical strength across a cornea, at least *ex-vivo*. As described for example in Scarcelli *et al* 'Biomechanical characterization of keratoconus corneas *ex vivo* with Brillouin microscopy', *Investigative Ophthalmology & Visual Science* 55(7), 4490 (2014), Brillouin shift measurements can provide information on the longitudinal modulus of the cornea. However the apparatus is relatively expensive because of the need for a high-resolution spectrometer. Furthermore the technique is time consuming because of the scanning requirement and requires a high on-eye optical intensity, presenting a challenge for *in-vivo* use.

Several types of pachymeter for measuring corneal thickness are known, based for example on ultrasonic techniques such as corneal waveform or optical techniques such as OCT, slit-scanning and Scheimpflug imaging. However these techniques may not have sufficient precision for measuring small spatial or temporal variations in thickness associated with a biomechanical response of the cornea, with repeatability of around $\pm 5 \mu\text{m}$ being reported for many commercially available instruments, see for example McAlinden *et al* 'A comprehensive evaluation of the precision (repeatability and reproducibility) of the Oculus Pentacam HR', *Investigative Ophthalmology & Visual Science* 52(10), 7731 (2011) and Correa-Pérez *et al* 'Precision of high definition spectral-domain optical coherence tomography for measuring central corneal thickness', *Investigative Ophthalmology & Visual Science* 53(4), 1752 (2012). Optical reflectometry techniques for measuring tear film thickness have much higher precision, of order of several nm, but are not well suited for measuring corneal thickness which is some two orders of magnitude greater than tear film thickness, especially when measuring over a large area of the cornea.

Studies of the pressure induced-deformation of the cornea have shown that the eye and cornea experience a creep in shape due to variations of IOP of approximately ± 3 to 6 mm Hg associated with a number of factors including heart rate, posture change, fluid intake, diurnal cycle and certain drugs. These shape changes are measurable with conventional topographical techniques such as Placido disc topography over periods of many seconds or longer. It is also known that IOP fluctuates with ocular pulse, as reported in published US patent application No 2015/0313573 A1 entitled 'Ophthalmic elastography', using a

contacting ultrasound technique applied *ex-vivo* with a simulated pulse. However these pulse-related shape changes are generally about an order of magnitude smaller than those caused by the more gradual IOP variations mentioned previously, and it is difficult to measure corneal thickness non-invasively and *in-vivo* with the level of sensitivity required to assess the underlying biomechanics of the cornea.

The corneal tear film plays an important role in eye health, as well as in vision since it is the first refractive surface encountered by light rays entering the eye, with abnormal tear film breakup implicated in dry eye disease and vision aberrations. As reviewed recently in King-Smith *et al* 'Mechanisms, imaging and structure of tear film breakup', *The Ocular Surface* 16, 4 (2018), the dynamics and causes of tear film breakup have been studied over many years. Tear film thickness and surface shape are both important for determining tear film dynamics, but current imaging techniques are limited to measuring either thickness or surface shape. Spectral domain OCT has been used to measure tear film thickness, see for example dos Santos *et al* 'In vivo tear film thickness measurement and tear film dynamics visualization using spectral domain optical coherence tomography', *Optics Express* 23(16), 21043 (2015), but has not provided information on surface shape. There is a need then for an apparatus that can measure tear film thickness and dynamics over an extended region wherein the shape and position of the eye can be taken into account.

Unless the context clearly requires otherwise, throughout the description and the claims the words 'comprising', 'comprises' and the like are to be construed in an inclusive sense as opposed to an exclusive or exhaustive sense. That is, they are to be construed in the sense of 'including, but not limited to'.

Object of the Invention

It is an object of the present invention to overcome or ameliorate at least one of the limitations of the prior art, or to provide a useful alternative. It is an object of the present invention in a preferred form to provide an apparatus for snapshot *in-vivo* measurement of one or more corneal properties at multiple points across the cornea. It is another object of the present invention in a preferred form to provide an apparatus for *in-vivo* measurement of time variations in corneal thickness or strain. It is another object of the present invention in a preferred form to provide a method for measuring tear film dynamics over an extended region of the cornea.

Summary of the Invention

According to a first aspect of the present invention there is provided an apparatus for measuring one or more properties of a cornea, said apparatus comprising:

a first optical system comprising an optical source and a spatial sampling element for
5 generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a front surface of a cornea; and

a second optical system for:

capturing reflected or scattered light from said front surface and reflected or
scattered light from a second surface or interface of said cornea;

10 measuring relative phase between the reflected or scattered light from said front surface and the reflected or scattered light from said second surface or interface across the portion of said cornea illuminated by said beamlets; and

monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

15 The apparatus is preferably configured such that, in use, the angle of incidence of the beamlets on the front surface is within 3 degrees of normal incidence.

Preferably, the spatial sampling element comprises a lenslet array. In certain embodiments the reflected or scattered light from the front surface and from the second surface or interface is captured with the spatial sampling element. In other embodiments the reflected or
20 scattered light from the front surface and from the second surface or interface is captured with a second spatial sampling element.

Preferably, the apparatus comprises a processor for: producing, from the relative phase measurements, a map of relative phase across the illuminated portion of the cornea; and monitoring the relative phase over time to determine time variations in the map.

25 The apparatus preferably comprises an interferometer for interfering the reflected or scattered light from the front surface and from the second surface or interface with a reference beam, to generate one or more interferograms. Preferably, the processor is configured to utilise the one or more interferograms to track the location of the beamlets on the front surface, for registering two or more maps of relative phase acquired at different times.

30 In preferred embodiments the optical source comprises a multi-wavelength optical source, and the processor is preferably configured to calculate, from the map of relative phase, a

tomographic profile of the cornea. The tomographic profile may comprise one or more of amplitude, phase or optical path length between the front surface and the second surface or interface. Preferably, the second surface or interface comprises the posterior surface of the cornea, such that the optical path length comprises a measure of corneal thickness.

- 5 In preferred embodiments the processor is configured to determine, from time variations in the optical path length, a biomechanical response of the cornea to relative differences between intraocular pressure and an external pressure on the cornea. In certain embodiments the processor is configured to determine a biomechanical response of the cornea to periodic intraocular pressure variations associated with the ocular pulse. In other embodiments the
- 10 apparatus is configured to vary the external pressure on the cornea. In certain embodiments the apparatus is configured to vary the external pressure by applying a source of distributed sound waves, or by varying the ambient pressure at the cornea.

In certain embodiments the processor is configured to determine, from time variations in the optical path length, a biomechanical response of the cornea to a perturbation imposed by one

15 or more of: an air puff source; a source of ultrasound; or a source of acoustic radiation pressure.

In certain embodiments the apparatus is configured to measure time variations in the thickness of a tear film on the cornea. Preferably, the processor is configured to: measure time variations in the thickness of a tear film on the cornea; and subtract the measured time

20 variations in tear film thickness from the optical path length to provide a normalised measurement of corneal optical path length.

According to a second aspect of the present invention there is provided a method for measuring one or more properties of a cornea, said method comprising the steps of:

- generating a converging array of beamlets configured to impinge simultaneously on at
- 25 least a portion of a front surface of a cornea;
- capturing reflected or scattered light from said front surface and reflected or scattered light from a second surface or interface of said cornea;
- measuring relative phase between the reflected or scattered light from said front surface and the reflected or scattered light from said second surface or interface across the
- 30 portion of said cornea illuminated by said beamlets; and
- monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

Preferably, the method further comprises the steps of: producing, from the relative phase measurements, a map of relative phase across the illuminated portion of the cornea; and monitoring the relative phase over time to determine time variations in the map.

Preferably, the method further comprises the steps of: interfering the reflected or scattered
5 light from the front surface and from the second surface or interface with a reference beam to generate one or more interferograms; and utilising the one or more interferograms to track the location of the beamlets on the front surface, for registering two or more maps of relative phase acquired at different times.

In preferred embodiments the beamlets are generated from a multi-wavelength optical source,
10 and the map of relative phase preferably provides a tomographic profile of the cornea. The tomographic profile may comprise one or more of amplitude, phase or optical path length between the front surface and the second surface or interface. Preferably, the method further comprises the step of determining, from time variations in the optical path length, a biomechanical response of the cornea to relative differences between intraocular pressure and
15 an external pressure on the cornea. In certain embodiments a biomechanical response of the cornea to periodic intraocular pressure variations associated with the ocular pulse is determined.

In certain embodiments the method further comprises the steps of: imposing on the cornea a perturbation comprising one or more of an air puff, ultrasound or acoustic radiation pressure;
20 and determining, from time variations in the optical path length, a biomechanical response of the cornea to the perturbation.

In certain embodiments the method further comprises the step of measuring time variations in the thickness of a tear film on the cornea. Preferably, the measured time variations in tear film thickness are subtracted from the optical path length to provide a normalised
25 measurement of corneal optical path length.

According to a third aspect of the present invention there is provided an apparatus for measuring one or more properties of a cornea, said apparatus comprising an optical system for:

generating a converging array of beamlets configured to impinge simultaneously on at
30 least a portion of a first surface or interface of a cornea;

capturing reflected or scattered light from said first surface or interface and reflected or scattered light from a second surface or interface of said cornea;

measuring relative phase between the first and second surfaces or interfaces across the portion of said cornea illuminated by said beamlets; and

5 monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

In certain embodiments the optical system is configured to measure the phases of the first and second surfaces or interfaces relative to a reference beam. In other embodiments the optical system is configured to measure the phases of the first and second surfaces or interfaces
10 relative to a reflection from a tear film on the cornea. The first surface or interface may comprise the air/tear film interface.

Preferably, the apparatus comprises a processor for: producing, from the relative phase measurements, a map of relative phase across the illuminated portion of the cornea; and monitoring the relative phase over time to determine time variations in the map. The optical
15 system preferably comprises a multi-wavelength source for generating the beamlets, and the processor is preferably configured to calculate, from the map of relative phase, a tomographic profile of the cornea.

According to a fourth aspect of the present invention there is provided a method for measuring one or more properties of a cornea, said method comprising the steps of:

20 generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a first surface or interface of a cornea;

capturing reflected or scattered light from said first surface or interface and reflected or scattered light from a second surface or interface of said cornea;

measuring relative phase between said first and second surfaces or interfaces across
25 the portion of said cornea illuminated by said beamlets; and

monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

In certain embodiments the phases of the first and second surfaces or interfaces are measured relative to a reference beam. In other embodiments the phases of the first and second
30 surfaces or interfaces are measured relative to a reflection from a tear film on the cornea. The first surface or interface may comprise the air/tear film interface.

Preferably, the method further comprises the steps of: producing, from the relative phase measurements, a map of relative phase across the illuminated portion of the cornea; and monitoring the relative phase over time to determine time variations in the map. Preferably, the beamlets are generated from a multi-wavelength optical source, and the map of relative phase preferably provides a tomographic profile of the cornea.

According to a fifth aspect of the present invention there is provided an apparatus for investigating a tear film on a cornea, said apparatus comprising:

an illumination system for illuminating a tear film or the anterior surface of a cornea at a plurality of points; and

a capture optical system for capturing return signals comprising hyper-reflective signals from said tear film or scattered light from said anterior surface at said plurality of points, said capture optical system having a capture angle,

wherein said illumination system is configured to, in use:

illuminate a first set of said plurality of points with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently close to normal incidence such that said hyper-reflective signals are within said capture angle, resulting in a set of higher intensity return signals; and illuminate a second set of said plurality of points with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently far from normal incidence such that said hyper-reflective signals are not within said capture angle, resulting in a set of lower intensity return signals;

and wherein said apparatus further comprises a processor for:

processing the higher intensity and lower intensity sets of return signals to obtain optical coherence tomography measurements; and

calculating, from selected optical coherence tomography measurements of the higher intensity and lower intensity sets of return signals, a measure related to the thickness of said tear film.

In certain embodiments the processor is configured to calculate the measure related to the thickness of the tear film by: fitting a surface to the optical coherence tomography measurements of the lower intensity set of return signals; and calculating differences between the surface and selected optical coherence tomography measurements of the higher intensity return signals. In other embodiments the processor is configured to calculate the measure related to the thickness of the tear film by: fitting a first surface to the optical coherence tomography measurements of the higher intensity return signals; fitting a second surface to

the optical coherence tomography measurements of the lower intensity return signals; and calculating an offset between the first and second surfaces. The processor is preferably configured to monitor time variations in the measure related to the thickness of the tear film.

In certain embodiments the processor is configured to determine a boundary between the set of higher intensity return signals and the set of lower intensity return signals. The processor may be configured to obtain, from the size or shape of the boundary, or from time variations thereof, information on the thickness, quality or distribution of a lipid layer of the tear film.

Preferably, the illumination system is configured to illuminate the tear film or the anterior surface of the cornea simultaneously at the plurality of points. More preferably, the illumination system is configured to illuminate the tear film or the anterior surface of the cornea with an array of substantially parallel beamlets.

In preferred embodiments the illumination system is configured to illuminate the first set of points with light that impinges on the tear film or the anterior surface at an angle of incidence less than 15 degrees, more preferably less than 8 degrees, and most preferably less than 4 degrees.

In preferred embodiments the illumination system is configured to illuminate the second set of points with light that impinges on the tear film or the anterior surface at an angle of incidence greater than 4 degrees, more preferably greater than 8 degrees, and most preferably greater than 15 degrees.

According to a sixth aspect of the present invention there is provided a method for investigating a tear film on a cornea, said method comprising the steps of:

illuminating said tear film or the anterior surface of said cornea at a plurality of points;

capturing, with a capture optical system having a capture angle, return signals comprising hyper-reflective signals from said tear film or scattered light from said anterior surface at said plurality of points, wherein a first set of said plurality of points is illuminated with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently close to normal incidence such that said hyper-reflective signals are within said capture angle, resulting in a set of higher intensity return signals, and a second set of said plurality of points is illuminated with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently far from normal incidence such that said hyper-

reflective signals are not within said capture angle, resulting in a set of lower intensity return signals;

processing the higher intensity and lower intensity sets of return signals to obtain optical coherence tomography measurements; and

- 5 calculating, from selected optical coherence tomography measurements of the higher intensity and lower intensity sets of return signals, a measure related to the thickness of said tear film.

In certain embodiments the calculating step comprises: fitting a surface to the optical coherence tomography measurements of the lower intensity return signals; and calculating
10 differences between the surface and selected optical coherence tomography measurements of the higher intensity return signals. In other embodiments the calculating step comprises: fitting a first surface to the optical coherence tomography measurements of the higher intensity return signals; fitting a second surface to the optical coherence tomography measurements of the lower intensity return signals; and calculating an offset between the first
15 and second surfaces. Preferably, the method further comprises the step of monitoring time variations in the measure related to the thickness of the tear film.

In certain embodiments the method further comprises the step of determining a boundary between the set of higher intensity return signals and the set of lower intensity return signals. The method may further comprise the step of obtaining, from the size or shape of the
20 boundary, or from time variations thereof, information on the thickness, quality or distribution of a lipid layer of the tear film.

Preferably, the tear film or the anterior surface of the cornea is illuminated simultaneously at the plurality of points. More preferably, the tear film or the anterior surface of the cornea is illuminated with an array of substantially parallel beamlets.

- 25 In preferred embodiments the first set of points is illuminated with light that impinges on the tear film or the anterior surface at an angle of incidence less than 15 degrees, more preferably less than 8 degrees, and most preferably less than 4 degrees.

In preferred embodiments the second set of points is illuminated with light that impinges on the tear film or the anterior surface at an angle of incidence greater than 4 degrees, more
30 preferably greater than 8 degrees, and most preferably greater than 15 degrees.

According to a seventh aspect of the present invention there is provided an article of manufacture comprising a non-transitory computer usable medium having a computer readable program code configured to operate the apparatus according to the first, third or fifth aspects, or to implement the method according to the second, fourth or sixth aspects.

5 **Brief Description of the Drawings**

Preferred embodiments of the invention will now be described, by way of example only, with reference to the accompanying drawings in which:

Figure 1A illustrates in schematic form a spectral domain OCT apparatus for *in-vivo* measurement of one or more properties of a cornea at a plurality of points with phase accuracy, i.e. nm level accuracy, according to an embodiment of the invention;

Figure 1B illustrates in schematic form an alternative configuration of sample arm optics for the OCT apparatus of Figure 1A;

Figure 1C illustrates in schematic form another configuration of sample arm optics for the OCT apparatus of Figure 1A;

Figure 1D illustrates in schematic form an alternative configuration for generating an array of beamlets and collected return signals;

Figure 2 shows in schematic form the structure of a tear film and a human cornea;

Figure 3 illustrates the effect on apparent corneal thickness of changes in eye-to-apparatus axial position;

Figures 4A and 4B show, for six different starting tear film thicknesses from 6 μm to 1 μm , the expected time variation of reflected beamlet power in a number of discrete wavelength bins;

Figures 5A and 5B show, for seven radial positions from the corneal apex, the expected variation of power over six seconds, in a beamlet reflected from a tear film, in a number of discrete wavelength bins;

Figure 6 depicts plots of tear film thickness versus radial position from the corneal apex at a number of different times from zero to six seconds after a blink;

Figure 7 shows an *in-vivo* reflectivity image of a portion of a cornea illuminated with an array of beamlets;

Figure 8 depicts schematically a method for obtaining a measure related to tear film thickness using OCT data calculated across the reflectivity image of Figure 7;

Figure 9 illustrates schematically a model of specular reflection and scattering consistent with the substantially binary intensity distribution seen in Figure 7; and

Figure 10 illustrates schematically the illumination of a plurality of points on a tear film or cornea.

Detailed Description of the Invention

Figure 1A shows in schematic form a spectral domain optical coherence tomography (OCT) apparatus **100** suitable for *in-vivo* measurement of one or more properties of a human cornea **102** at a plurality of points with phase accuracy, i.e. nm level accuracy, according to an embodiment of the present invention. Light **104** from a broadband optical source **106** such as a superluminescent diode with centre wavelength 840 nm and bandwidth 40 nm is collimated by a collimating element **108** such as a lens or a parabolic mirror, linearly polarised by a polariser **110** and then split by a polarisation beam splitting cube (PBS) **112** into reference and sample beams **114**, **116**. The reference arm **117** includes a mirror **118**, a moveable shutter **120** for blocking the reference beam **114** if the apparatus is to be operated without the reference beam, and a quarter wave plate **122** for polarisation transformation so that light reflected from the mirror **118** passes through the PBS **112** and into the detection arm **121**.

The reference arm **117** may also include relay elements as well as dispersion matching components for compensating for the dispersion of optics in the sample arm **123**. The mirror **118** may be moved axially to adjust the path length of the reference arm relative to the sample arm, e.g. to match different eye positions or to obtain information from structures at different depths in the eye. Alternatively or additionally, the entire apparatus **100** may be moved axially with respect to the cornea **102** to adjust the eye to apparatus distance and therefore the path length of the sample arm **123**.

The sample arm comprises a quarter wave plate **138**, a spatial sampling element in the form of a two-dimensional (2-D) lenslet array **124** to generate from the sample beam **116** a 2-D array of sample beamlets **126** which are relayed to the cornea **102** via a lens system **128**. In the illustrated embodiment the lens system is non-telecentric, designed such that the central rays of the relayed beamlets **130** impinge on the anterior surface **132** of the cornea, or more precisely the air/tear film interface as explained below, at or close to normal incidence. The central rays of the converging array of relayed beamlets **130** may for example converge at a point **134** approximately 8 mm beyond a focal surface **135**, i.e. beyond the surface where the beamlet waists lie. In preferred embodiments the lens system **128** is designed such that the focal surface **135** is substantially spherical as shown, with the convergence point **134** of the beamlets **130** approximately at the centre of curvature of this surface. In an alternative embodiment illustrated in Figure 1B the sample arm includes a telecentric or 4F lens system

170 designed to produce an array of relayed beamlets **172** that propagate to the cornea **102** in substantially parallel fashion, in which case the focal surface of the beamlets will be substantially planar. For simplicity of illustration the lenses in the relay lens systems **128** and **170** are depicted as simple single element lenses, although in preferred embodiments they have multiple elements to reduce distortions of the relayed beamlets over the signal bandwidth. In yet another embodiment illustrated in Figure 1C the sample arm includes a lens system **174** comprising a conventional lens **176** and a compound lens **178**. The compound lens comprises a shorter focal length section that directs an inner subset of beamlets **130** onto the cornea **102** at normal or near-normal incidence, and a longer focal length section that directs an outer subset of beamlets **180** onto the anterior sclera **182** or the limbus **184**.

Light scattered or reflected from the anterior or posterior corneal surfaces **132**, **136**, or from other interfaces in the cornea **102** or from deeper eye structures, passes back through the relay lens system **128**, **170** or **174**, then is captured by the lenslet array **124** and reflected by the PBS **112** into the detection arm **121** following polarisation transformation at the quarter wave plate **138**. In general the number of beamlets **126** that can be relayed onto the cornea **102** depends on the design of the 2-D lenslet array **124**, and in certain embodiments there may for example be of order 100 or 1000 beamlets in a square or rectangular pattern with a density of, say, 4 to 100 beamlets per square millimetre at the nominal focal surface **135**, i.e. at the waists of the beamlets **130** or **172**. In use the apparatus will preferably be positioned such that the nominal focal surface **135** is within or very close to the cornea **102**, as shown in Figure 1A. To enhance the relatively weak reflection from the posterior corneal surface **136** it may be further preferred for the nominal focal surface **135** to be close to the posterior corneal surface **136**.

If the reference beam **114** is present it is combined with the reflected sample beamlets **140** at the PBS **112** and the resulting combined beams analysed by a polariser **142** to interfere the light from the sample and reference paths. If the reference beam **114** is blocked by the shutter **120**, an interference signal can arise between light reflected or scattered from two or more surfaces or interfaces in the eye, such as the air/tear film interface and the posterior corneal surface **136**. Whatever the source of the interference signal, the resultant interference pattern, containing information on relative phase between light reflected or scattered from two or more surfaces or interfaces in the eye, is relayed by a system of lenses **144**, and an optional aperture **146** to remove stray light, for spectral analysis in a spectrometer **148** at a

grid of spatial positions determined by a spatial sampling element in the form of a 2-D lenslet array **150**, and a corresponding 2-D aperture array **152**.

The spectrometer **148** is able to analyse a plurality of grid points, beams or beamlets simultaneously, or at least within a single frame of a 2-D sensor array **154**, for snapshot

5 acquisition. After entering the spectrometer **148** the interfered beamlets are redirected by a PBS **158** to a lens **160** that collimates the beamlets for dispersion by a grating **156**, followed by double passage through a quarter wave plate **162** via reflection from a mirror **164** to rotate the polarisation state by 90 degrees. The dispersed spectral components are imaged by the lens **160** onto a 2-D sensor array **154** such as a CMOS camera after passing through the PBS
10 **158**, for extraction or measurement of relative phase between light reflected or scattered from two or more surfaces or interfaces in the eye, in particular from two or more surfaces or interfaces in the cornea or tear film. In preferred embodiments the grating **156** is oriented with respect to the grid of spatial positions determined by the 2-D lenslet array **150** and the corresponding 2-D aperture array **152** such that each of the combined beamlets entering the
15 spectrometer **148** is dispersed onto a separate set of pixels of the 2-D sensor array **154**, as described in published US patent application No US 2016/0345820 A1 entitled 'High resolution 3-D spectral domain optical imaging apparatus and method', the contents of which are incorporated herein by reference. As explained in more detail below, the relative phase between light reflected or scattered from two or more surfaces or interfaces in the cornea or
20 tear film, or more succinctly the relative phase between two or more surfaces or interfaces in the cornea or tear film, can be monitored over time in a series of snapshot measurements at the 2-D sensor array **154** to obtain information on one or more properties of the cornea **102**.

In certain embodiments the sample arm relay system **128**, **170** or **174** also includes a scanning element **168** such as a MEMS mirror for translating the array of relayed beamlets **130** or **172**
25 across the cornea **102** in one or two dimensions, e.g. to create a dense map across a substantial portion of the cornea by 'filling in' the gaps between the beamlets of the beamlet array. This dense map, which is preferably time averaged over many snapshots to average out time-dependent contributions to the measured thickness such as from tear film dynamics and heartbeat-related IOP fluctuations, can be used as a reference or template for correcting
30 eye motion artefacts as described below. For simplicity of illustration the MEMS mirror **168** is shown as being transmissive rather than reflective.

Several variations on the apparatus **100** shown in Figure 1A are possible. For example the splitting and recombining of the sample and reference beams **116**, **114** could be effected with an optical fibre coupler or a non-polarising beam splitter, or the 2-D array of sample beamlets **126** could be generated by a spatial sampling element in the form of an aperture mask, a
5 MEMS mirror array or a diffractive optical element rather than a lenslet array **124**. In yet another variation a spatial sampling element in the form of a 1-D lenslet array or similar could be used to generate a 1-D array of sample beamlets, although in general a 2-D array is preferred for obtaining data across a larger area of the cornea **102** in a single frame. It will be appreciated that, as shown in Figure 1D, an array of sample beamlets **126** could alternatively
10 be formed with a first lenslet array **124** or other spatial sampling element placed before the beamsplitter **112**, and reflected signals captured with a second lenslet array **124-A** or other spatial sampling element located after the beamsplitter **112** in the detection arm **121**. In yet another variation the lenslet array **124** is omitted so that the cornea **102** is illuminated with an unstructured wavefront, although in general for reasons of improved collection efficiency and
15 reduced cross-talk from multiple scattering it is preferable to illuminate the cornea with a plurality of discrete beamlets.

When measuring an eye *in-vivo* the cornea **102** is invariably covered with a tear film, in which case the first reflection will be from the air/tear film interface. As shown schematically in Figure 2 the tear film **200** has multiple layers including a thin outer lipid
20 layer **202** and an aqueous layer **204** that contacts the anterior surface **132** of the cornea **102** via a mucous layer (not shown). It should be noted that the thickness **206** of the tear film is exaggerated relative to the thickness **208** of the cornea. The main reflective surfaces of the corneal structure are summarised in Table 1, with the nominal Fresnel reflections at normal incidence calculated from the relevant refractive indices. In reality the air/tear film
25 reflectivity is dominated by the aqueous layer because the lipid layer is so thin, and is generally a little above 2% at normal incidence with the strength modulated by the structure and thickness of the lipid layer **202**. This is clearly still the most intense reflection, but reflections can also be detected from other surfaces or interfaces including the posterior corneal surface **136** and possibly also from intra-corneal structures such as Bowman's layer
30 **214**. For the purposes of this specification and the appended claims the term 'front surface of the cornea' means either the air/tear film interface **212** or the actual anterior surface **132** of the cornea **102**, depending on whether a tear film **200** is present. The term 'anterior surface

of the cornea' refers specifically to the physical front surface **132** of the cornea, i.e. the tear film/epithelium interface.

Structure	Nominal refractive index (visible)	Nominal thickness/ μm	Nominal Fresnel reflection at normal incidence
air	1	-	-
lipid tear layer	1.48	0.05	3.75%
aqueous tear layer	1.337	6	0.26%
cornea	1.376	550	0.0207%
aqueous humour	1.336	-	0.0218%

Table 1

Recalling that the interference signal from the cornea **102** contains information on relative

5 phase between light reflected or scattered from two or more surfaces or interfaces in the cornea **102** or tear film **200**, as mentioned previously the relative phase can be monitored over time in a series of measurements to obtain information on one or more properties of the cornea **102**. In preferred embodiments the interferogram detected by the 2-D sensor array **154** is read out in a single frame for subsequent analysis by a processor **166** equipped with

10 suitable computer readable program code, to obtain spatially resolved measurements, i.e. a map, of the cornea **102** across the portion illuminated by the beamlets **130**. By reading out the sensor array **154** in a series of frames or snapshots over time, the processor **166** is able to monitor relative phase over time to determine time variations in a map of relative phase, for obtaining information on one or more properties of the cornea such as thickness or a

15 biomechanical response, e.g. strain. In certain embodiments the processor **166** applies well-known Fourier transform-based OCT techniques to obtain a map of the cornea **102** in the form of a depth-resolved image, also known as a tomogram or tomographic profile. The tomogram may for example comprise one or more of amplitude, phase or optical path length between two or more corneal or tear film surfaces or interfaces, at a grid of points determined

20 by the positions of the relayed beamlets **130** on the cornea **102**. It will be appreciated that the optical path length between two corneal or tear film surfaces or interfaces is approximately equal to the product of the physical distance between those surfaces or interfaces and the effective refractive index, generally with a small offset due to phase changes related to the reflections.

25 In certain embodiments the spectral domain OCT apparatus **100** illustrated in Figure 1A is employed in a snapshot multiprobe interferometric technique for *in-vivo* determination of very small temporal variations, on the nm scale, of corneal thickness at multiple points over

the cornea **102**, and for registering the position of the measurements on the cornea. Spatially resolved information on corneal biomechanical response, such as a measure related to Young's Modulus, can then be obtained from the measured thickness variations, e.g. by a finite element analysis. Although it has been shown to be possible to resolve the tear film

5 **200** over a range of thicknesses with OCT using a sufficiently broad spectrum light source **106**, see dos Santos *et al Optics Express* 23(16), 21043 (2015) for example, the tear film thickness **206** was close to their axial resolution limit of $\sim 1 \mu\text{m}$, which is not ideal for measurements of spatial or temporal thickness variations. Consequently, in preferred

10 embodiments we measure the corneal/aqueous humour interface **136** relative to the air/tear film interface **212**, i.e. the combined tear film + corneal thickness **210**, and track variations in this combined thickness over time in a sequence of frames. In the absence of external pressure changes or perturbations, in general a plot of combined thickness **210** versus time will show a gradual decrease over several seconds between blinks due to tear film flow or evaporation, with superimposed periodic fluctuations on the ~ 1 second timescale due to the

15 corneal strain response to the ocular pulse. These sources of temporal variation are uncorrelated and can be separated for example using standard curve fitting and subtraction techniques.

In a preferred embodiment a number of pachymetry maps, i.e. measurements of tear film + corneal thickness **210** at multiple points across the cornea, are acquired at an appropriate

20 frame rate over several seconds. After accounting for the on-eye positions of the pachymetry maps in the data analysis as described below, the tear film variation is separated from the periodic heartbeat-related fluctuations to provide a map of corneal deformation versus time that can be correlated with the heartbeat. A typical rate of change of tear film thickness of about $1 \mu\text{m}$ over five seconds would correspond to a phase variation of a fringe of

25 approximately 1.7 degrees per frame at a 100 Hz frame rate. As such there is generally no concern with phase wrapping issues, and the precision of the measurement can be maintained by tracking the phase over time. Consequently we can detect spatial variations in corneal elasticity through ultrasensitive *in-vivo* measurements of the periodic corneal biomechanical response to IOP fluctuations induced by the flow of blood synchronous with the heartbeat.

30 In other embodiments the apparatus or method can be used to provide spatially resolved information on a corneal biomechanical response to an external stimulus such as ultrasound, an air puff or acoustic radiation pressure. Such external stimuli are generally localised. Alternatively the apparatus or method can be used to provide spatially resolved information

on a corneal biomechanical response to a distributed stimulus such as changing ambient air pressure or a source of distributed sound waves. The ambient pressure on the cornea may for example be varied via goggles or similar placed over the eye being measured. The apparatus or method may also be applied to monitor changes in biomechanical response over longer
5 time frames, e.g. for detecting long-term corneal degradation or for gauging the effectiveness of clinical crosslinking treatments designed to increase corneal stiffness.

In certain embodiments pachymetry maps are generated with the apparatus **100** operated as a standard Michelson interferometer, with reflections from various interfaces such as the
air/tear film interface **212** and the posterior corneal surface **136** referenced against the

10 reference beam **114**. However in preferred embodiments the apparatus **100** is operated as a common path interferometer with the reference beam **114** blocked, instead using the reflection from a front surface of the cornea, generally the air/tear film interface **212**, as the reference for reflections or scattering from other interfaces or surfaces, preferably including the posterior corneal surface **136**. We note that the phase and intensity of the reflected

15 'reference' light can be influenced by the lipid layer thickness and variations thereof, an effect that can be modelled if necessary. Since the thin lipid layer **202** will tend to influence the intensity of the average tear film reflection at the employed wavelength band, an accurate calibration of reflection intensity versus the slope of the cornea relative to an incident beam for a known reflection is also able to provide information on the lipid layer thickness.

20 Although common path interferometry has slightly inferior signal-to-noise than standard interferometry, it has excellent phase stability as well as low noise during phase measurements, providing high measurement accuracy. Furthermore the common path interferometer measurements are virtually unaffected by axial eye motion since all of the interfaces being measured move together.

25 In preferred embodiments pachymetry maps are generated using an array of converging beamlets **130** as shown in Figure 1A, i.e. with beamlets impinging on a front surface of the cornea **102** at substantially normal incidence. That is, the angle of incidence of the central rays of the beamlets **130** on a front surface of the cornea **102** is preferably within 3 degrees, more preferably within 2 degrees, and most preferably within 1 degree of normal incidence.

30 This is particularly important with the common path interferometry configuration since it provides a consistent specular reflection over a large portion of the cornea against which reflections from other interfaces or surfaces can be referenced. Specular reflections could be captured from beamlets impinging on the cornea at other angles, but this would require

additional optics to capture the reflected beamlets. The preferred combination of common path interferometry and a converging beamlet array at substantially normal incidence enables spatially resolved measurement of phase-resolved corneal thickness with sufficient sensitivity for detecting very small changes in corneal thickness and hence small changes in corneal elasticity.

In alternative embodiments pachymetry maps are generated using an array of substantially parallel beamlets **172** as shown in Figure 1B, although the signal strength from the interfaces of interest is generally strongly attenuated beyond the apex of the cornea because the strong specular reflections are not captured, compromising the accuracy of the phase measurements.

When using conventional OCT an additional difficulty is that the strength of the tear film reflection at the corneal apex is often comparable to the strength of the reference beam **114**, possibly resulting in multiple phantom reflections that can complicate accurate reconstruction of the scattering profile. This is especially true if the signal strength causes saturation of the detector. In conventional OCT it is generally preferred to interfere a weak reflected signal from a sample with a stronger reference signal to provide both phase and depth information from each of the scattering points in an A-scan. As described below, however, probing the eye with an array of substantially parallel beamlets **172** may provide additional information on the tear film, including thickness and quality of the lipid layer.

Although eye motion has minimal effect on phase stability when measuring a pachymetry map of a cornea with the apparatus **100** configured for common path interferometry, it can still affect the measurement accuracy. For example changes in axial position of the eye relative to the apparatus will affect the apparent curvature of the corneal surfaces.

Furthermore because the thickness of a healthy cornea increases gradually from the apex to the periphery, typically varying by $\sim 100\ \mu\text{m}$ over a 4 mm radius, a lateral variation in

beamlet position of about $40\ \mu\text{m}$, e.g. from translation or rotation, would result in a corneal thickness variation of $\sim 1\ \mu\text{m}$. Both these effects must be compensated for to ensure

submicron accuracy of the resultant interferometric corneal pachymetry. In preferred embodiments the location of the tear film surface in a series of pachymetry maps is tracked by introducing a weak reference beam **114** for one or more conventional interferometry

measurements. This enables registration of the pachymetry maps, which in turn allows correction of phase variations related to the eye motion. The frequency with which these conventional interferometry measurements are acquired, relative to the frequency of the common path interferometry measurements, can be chosen according to circumstances such

as degree of eye movement or required measurement accuracy. For adequate registration of the common path pachymetry maps, in most cases it will suffice to acquire the conventional interferometry measurements occasionally, e.g. once every five, ten or twenty pachymetry measurements, optionally with interpolation of corrections across individual pachymetry measurements between successive registration measurements. To avoid saturating the sensor array **154** the intensity of the reference beam **114** in the registration measurements is preferably weaker than the intensity of the captured reflections for each beamlet, e.g. ~1% compared to the ~2% specular reflection from the tear film.

The registration process is explained with reference to the simulated interferometric data plotted in Figure 3, which shows how changes in eye-to-apparatus axial position, caused for example by eye motion, can affect the apparent curvature of various corneal interfaces. In Figure 3 the x-axis represents radial position from the corneal apex in mm, while the y-axis represents optical path length from the location **300** of the front surface, generally the air/tear film interface **212**, in μm . With the apparatus **100** configured for common path interferometry, the location of the posterior corneal surface **136** relative to the front surface is measured as a function of radial position for two different eye-to-apparatus axial positions, resulting in the traces **302-A** and **302-B**. Since the location **300** of the front surface coincides with the x-axis, the traces **302-A** and **302-B** represent a measure of optical path length thickness **304** of the cornea as a function of radial position, as may be measured with a one-dimensional array of beamlets, although as mentioned previously the array of beamlets is preferably two-dimensional. The trace **306** depicts Bowman's layer, another interface that may be measured with the apparatus **100** shown in Figure 1A.

In principle the curvature of a trace such as **302-A** or **302-B** is indicative of the gradual increase in corneal thickness away from the apex, however it will be appreciated from the slight difference in curvature between these two traces **302-A** and **302-B** that variations in eye-to-apparatus axial position will affect corneal thickness measurements. When the apparatus **100** is re-configured for conventional interferometry using the reference beam **114**, the location of the front surface of the cornea is measured for each of the two eye-to-apparatus axial positions, resulting in the traces **308-A** and **308-B**. Importantly, the curvature of these traces **308-A** and **308-B**, which represents the apparent curvature of the front surface of the cornea relative to the planar reference mirror **118**, depends on the optical path length difference between the reference and sample paths, and is therefore sensitive to the eye-to-apparatus axial position. Consequently the difference in curvature between these traces **308-**

A and **308-B** enables a correction to be calculated and applied to the apparent difference in curvature between the traces **302-A** and **302-B**. In Figure 3 the traces **308-A** and **308-B** have been displaced in the y-axis relative to the other traces for convenience of display, but in reality the actual relative positions between the various traces are used in calculating the correction.

Although for simplicity Figure 3 only illustrates the effect on corneal thickness measurements of changes in eye-to-apparatus axial position, the same principle applies to the correction of changes in curvature, shape or slope of the interferometric traces caused by translation or rotation of the eye relative to the apparatus. Once the position of the eye has been registered to the apparatus using the registration frames acquired using conventional interferometry, slight variations in apparent corneal thickness arising from eye motion can be corrected. If necessary, smaller terms in the distortion due to changes in the angles of incidence of the beamlets on a front surface of the cornea can be accounted for using geometry and Snell's law. It can be advantageous for the registration frames, at least, to include data from the anterior sclera **182** or the limbus **184**, using the lens system **174** shown in Figure 1C for example, to assist in accounting for both displacement and rotation as explained in published PCT patent application No WO 2018/136993 A1 entitled 'Optical coherence metrology and tomography with improved registration'.

The above-described registration procedure, based on additional measurements using the reference beam **114**, is not needed if the corneal measurements are acquired using conventional interferometry rather than common path interferometry, although the positional information of the beamlets on the eye still needs to be processed. The above-described registration procedure may also be omitted if the cornea can be registered to itself, e.g. using an existing accurate pachymetry map acquired using the MEMS mirror **168** as described previously, or if eye movement can be tracked with a camera and the MEMS mirror **168** adjusted to lock the position of the beamlets **130** on the eye to stabilise the individual measurements.

A preferred procedure for *in-vivo* measurement of a corneal property such as thickness or biomechanical response using the apparatus **100** can be summarised as follows:

- a) A map of the combined tear film + corneal thickness **210**, i.e. a pachymetry map, represented by the interferometric trace **302-A**, is produced with the reference beam **114** blocked, preferably using an array of converging beamlets **130** as shown in

Figures 1A or 1C although an array of substantially parallel beamlets **172** as shown in Figure 1B may also be used.

- b) A map of the tear film location relative to the apparatus **100**, represented by the interferometric trace **308-A**, is produced with the reference beam **114** unblocked.
- 5 c) For each subsequent pachymetry map measurement or group of measurements **302-B** a new tear film location **308-B** is ascertained.
- d) Based on the apparent change in tear film location, i.e. a comparison of the tear film traces **308-A** and **308-B**, a correction for eye motion can be calculated and applied to the later pachymetry map (or group of maps) **302-B**. Any remaining differences
10 between the pachymetry maps **302-B** and **302-A** can be assigned to actual changes in the cornea **102** or tear film **200**.
- e) By acquiring additional pachymetry maps and correcting them for eye motion, changes in the combined tear film + corneal thickness **210** at a plurality of points across the cornea **102** can be tracked in time. The relative phase between light
15 reflected from the air/tear film interface **212** and the posterior corneal surface **136** can be tracked without concern of phase wrapping if the pachymetry maps are acquired at a sufficiently high frequency, e.g. 100 Hz or more, for phase changes between measurements to be significantly less than π .
- f) The contributions to the time-varying pachymetry data of (i) tear film flow or
20 evaporation and (ii) strain response to heartbeat-related IOP fluctuations or an external stimulus are analysed separately to provide spatially resolved information on both tear film dynamics and corneal biomechanical response. For example a gradual variation in tear film thickness **206** can be subtracted from the pachymetry data to provide a normalised measurement of corneal optical path length, i.e. thickness **208**,
25 and the strain response analysed to provide a measure related to Young's Modulus or some other stiffness or resilience-related parameter at a plurality of points across the cornea **102**.

As the radius of curvature of the cornea varies from the apex towards the periphery, it is possible that the spectral reflection corresponding to a full map of the cornea cannot be
30 captured within the numerical aperture of the lenslet array **124**. A population-based correction to the focal surface **135** could be designed in the relay lenses, e.g. the lens system **128** in Figure 1A. Alternatively the apparatus can be moved axially relative to the eye to optimise the capture of light reflected or scattered from regions of differing radii of curvature.

The above embodiments have been described for the case where the apparatus **100** comprises a multi-wavelength optical source such as a broadband source **106** emitting light over a continuous band of wavelengths. This enables the acquisition of a tomographic profile of the cornea **102**, preferably including a measure of corneal thickness. However information on one or more properties across a cornea can also be obtained by probing the cornea with an array of beamlets generated from a monochromatic source. Monochromatic light will only provide information on relative optical path length variations of the cornea **102** or tear film **200**, either over time or between beamlets, and the return light may need to be monitored regularly to avoid phase wrapping artefacts. However the information on relative optical path length variations thus obtained may still be used in some low cost embodiments to infer a property such as relative strain or variations in tear film thickness **206** at a plurality of points across the cornea.

In other embodiments of the invention the apparatus **100** of Figure 1A, with the high resolution lens relay **128** providing a specular reflection over a large area of a cornea **102**, is used for determining tear film thickness dynamics, enabling absolute measurements of tear film thickness **206** with submicron accuracy and nm level relative precision significantly superior to those achievable with conventional OCT. With the reference beam **114** preferably blocked with the shutter **120**, in certain embodiments the wavelength-resolved signals read out from the 2-D sensor array **154** by a suitably programmed processor **166** from each beamlet **140** reflected or scattered from the illuminated spots on the cornea **102** are each divided into, say, six or seven 5 nm wide wavelength bins over a number of successive frames. Data is preferably acquired over a period that allows at least one interferometric cycle, which corresponds to a tear film thickness change of greater than $\lambda/(2 * n_{tear})$. For a broadband source **106** of centre wavelength $\lambda = 840$ nm and assuming a tear film refractive index $n_{tear} = 1.337$, this equates to a thickness change of at least 0.31 μm . The corresponding minimum data collection period can be estimated from the typical rate of thickness loss of the pre-corneal tear film **200** between blinks, and will generally be no more than a few seconds.

The processor **166** then calculates the temporal variation of the integrated power for each wavelength bin. Since the signal power within each bin will be relatively high because the return beamlets **140** have been specularly reflected from the cornea **102**, it is possible to exploit the high signal-to-noise ratio and knowledge of the structure of the tear film **200** to achieve more accurate phase measurements. The combined reflected signal from the various tear film layers is the predominant signal that will not average out over the wavelength spread

of the wavelength bins, so will have a variation dependent on the tear film thickness **206** as shown below. Even without numerical analysis, we can clearly identify the variation on a micron scale based on the spread of the time-dependent intensity plots for the wavelength bins. However to measure the profile of the tear film **200** over the cornea **102** we can also
5 use phase information by tracking phase variations between spatial sampling points. In one particular example the 2-D lenslet array **124** and relay optics **128** provide sampling points on a 250 μm spaced square or rectangular grid at the nominal focal surface **135**, i.e. at the waists of the beamlets **130**.

Figures 4A and 4B show, for six starting tear film thicknesses from 6 μm to 1 μm , plots **402**,
10 **404, 406, 408, 410** and **412** of the expected time variation of power in a reflected beamlet in each of six 5 nm wide wavelength bins centred on 0.82, 0.825, 0.83, 0.835, 0.84 and 0.845 μm respectively, for an assumed constant rate of variation of tear film thickness **206**. Each plot is calculated over 35 frames measured at a 10 Hz frame rate, i.e. over 3.5 seconds, with the power variations for each of the six wavelength bins moving through a little over one
15 cycle during the measurement period.

Figures 5A and 5B show, for seven radial positions r from zero to 3.0 mm measured from the corneal apex, plots **502, 504, 506, 508, 510, 512** and **514** of the expected variation of power in a reflected beamlet over six seconds in each of seven 5 nm wide wavelength bins centred on 0.82, 0.825, 0.83, 0.835, 0.84, 0.845 and 0.85 μm respectively. These plots have been
20 generated for a tear film **200** initially 5 μm thick at the apex (post-blink), with a model assuming a weak parabolic shape in tear film thickness **206** across the cornea and a rate of loss that increases with distance from the apex (r). These chosen assumptions are not necessarily realistic, although there is some evidence from fluorescein imaging of tear film dynamics that tear film breakup generally occurs away from the apex, implying either a
25 smaller initial thickness or a higher rate of thickness loss. The main purpose of the assumptions is to show how variations in parameters such as rate of thickness loss can be revealed in this wavelength binning analysis. For example the temporal power variations in each wavelength bin for the $r = 3.0$ mm plot can be seen to cycle more rapidly than in the plot at the apex.

30 Advantageously, with this approach the tear film dynamics at a particular position or region on the cornea **102** can be analysed robustly over time once we have a specular back reflection. For improved phase stability it is preferable for the measurements to be made with

the reference beam **114** blocked, i.e. using common path interferometry, since the tear film thickness **206** is unlikely to be overly sensitive to slight variations in position resulting from eye motion. Alternatively the measurements may be made with a weak reference beam **114** present. The received signals can be normalised for coupling efficiency taking into account the power, relative positions of the beamlet waists and the angle of incidence on the tear film **200**, as well as for the spectral profile of the light **104**. The influence of the lipid layer **202**, which will appear largely as an attenuation term since the bandwidth of its reflectivity profile will generally be much wider than that of the light source **106**, can also be taken into account.

The series of seven plots presented in Figures 5A and 5B have been calculated at radial positions spaced 0.5 mm apart in one axis only across the cornea, although a series of experimental measurements at intervals of 250 μm or less in two dimensions is achievable with the apparatus **100** depending on the design of the lenslet array **124** and the lens relay **128**. Using the assumed continuity of tear film thickness **206** as a function of time and the small variation in tear film thickness over the radial position intervals, pathways of descending contours can be chosen with a phase shift of less than $\pi/2$ between sample points to remove any phase ambiguity, allowing us to obtain an unambiguous tear film profile over time with resolution limited only by the signal-to-noise ratio. Given the strong signals from the specular reflections in each spectral band or wavelength bin, we expect that the time evolution of tear film thickness **206** can be measured *in-vivo* with a precision of several nm. The previously described model, or some other model, can be applied to the data to determine the radial profile of the tear film **200** at different points in time. This is shown in Figure 6, which depicts plots of tear film thickness in μm versus radial position from the corneal apex in mm for $t = 0, 1, 2, 3, 4, 5$ and 6 seconds following a blink, with the plots labelled **602** and **604** depicting the tear film profile at 0 and 6 seconds respectively.

The parameters of the chosen model can also be adapted to provide non-constant tear film dynamics and to identify tear film breakup. The chosen model also can include a factor to account for variation of the lipid layer thickness, which as mentioned previously will generally act to vary the strength of all of the spectral components over time.

The dynamics and profile of the pre-corneal tear film **200** are of interest in providing information regarding the impact of tear film quality and consistency on the refractive properties of the eye. The tear film profile, i.e. shape, is generally not captured in non-

specular topographic OCT images, but is critical in determining refraction at the eye. Therefore the additional information on the tear film profile provided by our analysis can result in improved refraction estimates compared to those obtained purely from corneal topography.

- 5 It is worth noting that the detected return beamlets **140** could be analysed in the processor **166** using conventional OCT techniques, i.e. without the above-described wavelength binning analysis. For example the apparatus **100** may be configured for common path interferometry, with the air/tear film interface **212** providing the common path reference beam and the various layers of the cornea **102**, such as the anterior or posterior surfaces **132**, **136**, providing
10 smaller reflections that can be detected through the fringes. However because the tear film **200** typically has a thickness **206** of only a few microns, and because it can be important to measure tear film thickness down to the sub-micron level during breakup, a very wide spectrum would be required to separate the reflection peaks from the air/tear film interface **212** and the tear film/cornea interface **132**. The required spectral width is well beyond the 40
15 nm bandwidth of the 840 nm light source **106** exemplified in the apparatus **100**. In contrast the wavelength-binning analysis, which just requires a model with *a priori* information on the expected tear film structure and the temporal variation of the phase of light reflected from the tear-film/cornea interface **132**, can provide tear film thickness **206** with sub-micron accuracy using an instrument with a much narrower spectrum, e.g. a 40 nm bandwidth. The same
20 information could also be provided by analysis of the temporal variation of phase and intensity of the Fourier components of the return beamlets **140**, especially the lowest few spectral Fourier components. For simplicity we have described the analysis in terms of a model of the wavelength-dependent fringes where the sensitivity to sub-wavelength shifts can be easily visualised and plotted, but this is not a limitation of the method.
- 25 Because the dynamics of the tear film variation are of the order of seconds and the frame rate of the spectrometer **148** is up to 300 Hz it is possible to increase the sampling density on the cornea by dithering the location of the beamlet array **130** in a pattern that repeats, say, at 5 Hz. For the case of a 250 μm 2-D grid spacing on the cornea **102** we can dither the beamlet array using the MEMS mirror **168** with a peak-to-peak equivalent displacement on the cornea
30 of, say, 300 μm in an axis joining the grid points to provide a series of ‘B scans’ with some oversampling. This allows complete continuity of the phase between spatial points to be achieved while still allowing the tear film dynamics to be captured at 5 Hz. As a potentially useful benefit of this approach, it may be possible to derive a measure of the epithelium

roughness or provide an epithelium profile under the reasonable assumption that the tear film thickness **206** is a smooth function of position before any breakup occurs, so that any microstructure observed in the series of B scans results from the underlying roughness of the tear film/epithelium interface **132**. This information, which gives nm resolved roughness, can be of diagnostic value in refractive surgeries such as photorefractive keratectomy (PRK) where it is important to understand the regrowth of the epithelium and how that can influence the tear film and refraction of the eye.

To recover the topography of the anterior corneal surface **132** the time-averaged decay in tear film thickness is subtracted off the derived phase for each of the wavelength bins, noting that for a tear film thickness of several μm at least some of the wavelength bin plots will generally have components in a sensitive region, i.e. away from a turning point, for most of the frames acquired. A measure of surface roughness or even a nano-topographic profile of the anterior corneal surface **132** can therefore be provided along with the tear film profile as a series of closely spaced B scans. It has been proposed, e.g. in King-Smith *et al* 'Tear film interferometry and corneal surface roughness', *Investigative Ophthalmology & Visual Science* 55(4), 2614 (2014), that variability or roughness of the corneal surface profile limits the ability to achieve a high level of contrast for interferometric spectral measurements, particularly in the visible to NIR. Notably, the use of small focused spots in the present invention, as well as the ability to ensure that the spot size is maintained by accurate positioning of the apparatus **100** relative to the tear film **200**, via standard OCT with the reference beam **114**, should help overcome this limitation. In some implementations it could be advantageous to utilise longer wavelength bands, say around 1550 nm, or have additional longer wavelength bands to enhance the contrast of the received signals.

Apart from providing information on the tear film dynamics, the wavelength binning method provides an alternative to the previously described curve fitting method for subtracting the contribution of the tear film thickness **206** from a pachymetry map, i.e. the combined tear film + corneal thickness **210** at a plurality of points across the cornea **102**. This ensures that the phase variations of the pachymetry map can be normalised at each point in time to account for the thickness of the tear film, thus ensuring nm level precision of corneal thickness **208**, which is important for elastography measurements of the cornea.

As explained previously, for measuring corneal thickness it is preferred to probe the eye using an array of converging beamlets **130** as shown in Figure 1A, i.e. with beamlets

impinging on a front surface of the cornea **102** at substantially normal incidence, to provide a consistent specular reflection over a large portion of the cornea against which reflections from other interfaces or surfaces can be referenced. Unexpectedly, we have found that probing the eye with an array of substantially parallel beamlets **172** as shown in Figure 1B, which provides a large range of incidence angles on the cornea **102**, is useful for studying the tear film **200** and in particular the lipid layer **202**. Figure 7 shows an *in-vivo* reflectivity image **700**, approximately 2 mm in diameter, of a portion of the cornea of an eye obtained by illuminating a plurality of points with a 12x24 array of substantially parallel beamlets and integrating the reflected beamlet power over a depth range. The array of beamlets was generated using light from an (840 ± 15) nm superluminescent diode sampled with a 2-D lenslet array, and extended across an area of approximately 11 mm x 14 mm. The image **700** reveals a substantially binary intensity distribution with a highly reflective central region **702** and a rapid transition to a lower reflectivity outer region **704**. The small dark square just above the higher intensity region **702** is an artefact caused by a defective camera pixel. The shape and size of the higher intensity region **702** varies between individuals and over time for an individual, a variability believed to be due to changes in the thickness, quality or distribution of the lipid layer **202**.

In certain embodiments the reflectivity image **700** is processed to delineate the higher intensity inner region **702** and lower intensity outer region **704**, e.g. using a bimodal segmentation algorithm with a chosen threshold, yielding a boundary **706**. As shown schematically in Figure 8, depth data **804-H**, **804-L** within the higher and lower intensity regions **702**, **704** are calculated using standard optical coherence tomography techniques, e.g. from phase measurements relative to a reference beam **114**, revealing a distinct transition **806** in elevation, typically of 1 to 6 μm , around the boundary **706**. The magnitude of this transition **806**, along with the fact that the substantially binary intensity distribution shown in Figure 7 is not seen in test objects such as model eyes, strongly suggests the effect is related to the tear film. Consequently, differencing measurements between selected depth data **804-H**, **804-L** in the higher and lower intensity regions **702**, **704** will provide a measure related to the thickness of the tear film. We note that elevation accuracies of better than 1 μm can be achieved, despite having an axial imaging resolution of around 10 μm , by finding edges using sub-pixel sampling techniques and fitting surfaces that allow averaging over a sufficiently large number of data points **804-H** or **804-L**.

In certain embodiments, first and second surfaces **800**, **802** are fitted to depth data **804-H**, **804-L** in the higher and lower intensity regions **702**, **704** respectively, allowing us to obtain a measure related to the thickness of the tear film from an offset **808** between the first and second surfaces **800**, **802**. In other embodiments a surface **802** is fitted to depth data **804-L** in the lower intensity region **704**, and differences between that surface **802** and selected depth data **804-H** in the higher intensity region **702** provide a measure related to the thickness of the tear film.

Differences in elevation or offsets between the two surfaces **800**, **802**, or between the surface **802** and selected depth data **804-H**, can be calculated at multiple locations, e.g. over the entire higher reflectivity region **702** or along the boundary **706**, to provide spatially resolved measurements of tear film thickness over the region or boundary, which may be averaged to provide a single tear film thickness measurement. The tear film thickness measurements, averaged or otherwise, can then be used to calculate corrected corneal topography by offsetting the measured points **804-H** in the inner region **702** with the tear film thickness before combining with the measured points **804-L** in the outer region **704** and fitting a surface through the combined points. Advantageously, our edge-finding approach with the substantially binary intensity distribution obviates the previously noted difficulty that standard OCT image segmentation techniques have in separating the air/tear film interface from the tear film/cornea interface, given the typical axial resolution of 5 to 10 μm .

The substantially binary intensity distribution observed in Figure 7 can be explained with reference to Figure 9, which illustrates schematically the interaction of two substantially parallel beamlets **172-1**, **172-2**, represented by their central ray paths, with the lipid **202** and aqueous **204** layers of a tear film **200** and the anterior surface **132** of a cornea **102**. As depicted schematically in Figure 9 the lipid layer **202** is considerably more textured than the aqueous layer **204**. In preferred embodiments the beamlets **172-1**, **172-2** are two of a number of substantially parallel beamlets produced by the combination of a 2-D lenslet array **124** and a telecentric lens relay **170** as shown in Figure 1B. One of the representative beamlets **172-1** impinges on the tear film **200** and cornea **102** at an angle of incidence **900** close to normal incidence, while the other representative beamlet **172-2** impinges on the tear film **200** and cornea **102** at an angle of incidence **902** that is significantly removed from normal incidence. For each beamlet a significant fraction of the light will experience a primarily specular reflection **904** from the tear film **200**, within a cone or range of angles **906** determined largely by the textured nature of the lipid layer **202**. A much smaller fraction of the light in each

beamlet will be scattered at the anterior corneal surface **132**, with this scattering **908** being essentially isotropic. In addition there will be a small amount of isotropic scattering from the lipid layer **202** and a weak specular reflection from the anterior corneal surface **132**. These small components are not shown in Figure 9, as they don't affect the explanation of the substantially binary intensity distribution seen in Figure 7.

Referring to Figures 1A and 1B, it will be appreciated that the 2-D sensor array **154** will only detect return light from the cornea **102** or tear film **200** that is within the capture angle of the optical system used to capture return signals. Whether reflections **904** from beamlets **172** are detected is determined by the curvature of the cornea, i.e. the size of the sample eye, the numerical aperture of the beamlets **172** and the numerical aperture of the capture optical system, which in the illustrated embodiment comprises the lens relay system **170** and the lenslet array **124**. For beamlets such as the representative beamlet **172-1** that impinge on the tear film **200** at an angle of incidence **900** sufficiently close to zero, i.e. close to normal incidence, the detected return signal will be dominated by the specular reflection **904** within the cone of angles **906**, resulting in the bright central region **702** seen in Figure 7. We shall refer henceforth to this brighter captured light from a combination of tear film surface structure and specular reflection as the hyper-reflective signal **910**. On the other hand for beamlets such as the representative beamlet **172-2** that impinge on the tear film **200** at an angle of incidence **902** significantly larger than zero, i.e. far from normal incidence, the hyper-reflective signal **910** will not be captured and the main contribution to the detected return signal will be isotropic scattering **908** from the anterior corneal surface **132**, resulting in the lower intensity outer region **704** seen in Figure 7.

In alternative embodiments the reflectivity image **700** is processed with a segmentation algorithm having two thresholds. Data points with intensity above the higher threshold delineate the region **702** where the return signal is dominated by the lipid layer-influenced hyper-reflective signal **910**, and may be used to fit a surface **800** corresponding to the air/tear film interface. Data points with intensity below the lower threshold delineate the outer region **704** where the return signal is dominated by scattering **908** from the anterior corneal surface **132**, and may be used to fit a surface **802** corresponding to the anterior corneal surface **132**. Data points with intensity between the two thresholds, which typically fall in a narrow band between the regions **702**, **704**, are not used when fitting either surface **800**, **802**. Once the tear film thickness has been determined, however, these intermediate points can be used as

part of the height data by interpolating the offset based on their intensity relative to the two thresholds.

The observed variability in shape and size of the bright central region **702** between individuals, and over time for an individual, is thought to be due to changes in the thickness, quality or distribution of the lipid layer **202**, which will affect the cone of angles **906** of the specular reflection **904** and therefore the hyper-reflective signal **910**. Consequently the shape or size of the bright central region **702**, as well as variations in the shape or size over time, may be a useful indicator of the thickness, quality or distribution of the lipid layer **202**.

Together with the tear film thickness, this may prove useful in distinguishing between different types of dry eye disease, such as aqueous deficient dry eye and evaporative dry eye for example.

In certain embodiments tear film break up or health are assessed via the dynamics of the derived thickness and topology in or of the hyper-reflectivity region **702**. For example machine learning techniques such as Convolutional Neural Networks may be used in combination with large data-sets of both normal and diseased states of the eye to assist in the diagnosis and treatment of ocular conditions, in particular dry eye disease. An association between the intensity distribution seen in Figure 7, including hyper-reflective signals from the tear film, on the one hand, and tear film and lipid layer health on the other hand, is anticipated to yield important correlations or predictive values once sufficiently large databases correlated with existing ocular health metrics have been established.

In certain embodiments, and with reference to Figures 8, 9 and 10, a method for obtaining a measure related to the thickness of a tear film **200** on a cornea **102** is implemented by:

- (i) Illuminating the tear film or the anterior surface of the cornea at a plurality of points **1000**;
- (ii) Capturing, with a capture optical system having a capture angle, return signals comprising hyper-reflective signals **910** from the tear film **200** or scattered light **908** from the anterior surface **132** of the cornea **102** at the plurality of points **1000**, wherein a first set **1002** of the plurality of points is illuminated with light **172-1** that impinges on the tear film or the anterior surface of the cornea at an angle of incidence **900** sufficiently close to normal incidence such that the hyper-reflectivity signals **910** are within the capture angle, resulting in a set of higher intensity return signals, and a second set **1004** of the plurality of points is illuminated with light **172-2** that impinges on the tear film or the anterior surface of the cornea at an angle of

incidence **902** sufficiently far from normal incidence such that the hyper-reflective signals **910** are not within the capture angle, resulting in a set of lower intensity return signals;

(iii) Processing the higher intensity and lower intensity sets of return signals to obtain optical coherence tomography measurements **804-H**, **804-L**; and

- 5 (iv) Calculating, from selected optical coherence tomography measurements of the higher intensity and lower intensity sets of return signals, a measure **808** related to the thickness of the tear film **200**.

The limiting angle of incidence that delineates the first and second sets of points **1002**, **1004**, i.e. the maximum angle of incidence above which the hyper-reflective signals **910** will not be
10 captured, depends on a number of factors. These include the numerical aperture of the illuminating beamlets **172** and the numerical aperture, or capture angle, of the optical system used to capture return signals from the tear film **200** or cornea **102**. A lower numerical aperture in either case results in a smaller limiting angle, or equivalently a smaller high intensity central region **702**. Importantly, the limiting angle or size of the central region **702**
15 depends also on the nature of the tear film **200**, yielding diagnostic value. The limiting angle of incidence is typically between 4 degrees and 8 degrees, but can be up to 15 degrees for some tear films. Therefore the array of beamlets **172** should be generated and directed onto the sample cornea **102** such that at least some of the beamlets **172-1** have an angle of incidence **900** less than 15 degrees, more preferably 8 degrees and most preferably less than 4
20 degrees. Additionally, at least some of the beamlets **172-2** should have an angle of incidence **902** greater than 4 degrees, more preferably greater than 8 degrees, and most preferably greater than 15 degrees.

In the above-described embodiment the reflectivity image **700** of Figure 7 was obtained by illuminating the tear film **200** or cornea **102** at a plurality of points **1000** simultaneously with
25 an array of beamlets **172**. While this is preferred for reasons of acquisition speed and minimisation of eye motion artefacts, it is also possible to illuminate the tear film or cornea at a plurality of points sequentially, e.g. using a scanning beam OCT apparatus, with the subsequent analysis of the reflectivity image **700** or return signals proceeding in an equivalent fashion.

30 Although the invention has been described with reference to specific examples, it will be appreciated by those skilled in the art that the invention may be embodied in many other forms.

The claims defining the invention are as follows:

1. An apparatus for measuring one or more properties of a cornea, said apparatus comprising:

a first optical system comprising an optical source and a spatial sampling element for
5 generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a front surface of a cornea; and

a second optical system for:

capturing reflected or scattered light from said front surface and reflected or
scattered light from a second surface or interface of said cornea;

10 measuring relative phase between the reflected or scattered light from said front surface and the reflected or scattered light from said second surface or interface across the portion of said cornea illuminated by said beamlets; and

monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

15 2. The apparatus according to claim 1, wherein said apparatus is configured such that, in use, the angle of incidence of said beamlets on said front surface is within 3 degrees of normal incidence.

3. The apparatus according to claim 1 or claim 2, wherein said spatial sampling element comprises a lenslet array.

20 4. The apparatus according to any one of claims 1 to 3, wherein the reflected or scattered light from said front surface and from said second surface or interface is captured with said spatial sampling element.

5. The apparatus according to any one of claims 1 to 3, wherein the reflected or scattered light from said front surface and from said second surface or interface is captured with a
25 second spatial sampling element.

6. The apparatus according to any one of claims 1 to 5, wherein said apparatus comprises a processor for:

producing, from the relative phase measurements, a map of relative phase across the illuminated portion of said cornea; and

30 monitoring said relative phase over time to determine time variations in said map.

7. The apparatus according to claim 6, wherein said apparatus comprises an interferometer for interfering the reflected or scattered light from said front surface and from said second surface or interface with a reference beam, to generate one or more interferograms.

5 8. The apparatus according to claim 7, wherein said processor is configured to utilise said one or more interferograms to track the location of said beamlets on said front surface, for registering two or more maps of relative phase acquired at different times.

9. The apparatus according to any one of claims 6 to 8, wherein said optical source comprises a multi-wavelength optical source, and wherein said processor is configured to
10 calculate, from said map of relative phase, a tomographic profile of said cornea.

10. The apparatus according to claim 9, wherein said tomographic profile comprises one or more of amplitude, phase or optical path length between said front surface and said second surface or interface.

11. The apparatus according to claim 10, wherein said second surface or interface
15 comprises the posterior surface of said cornea, such that said optical path length comprises a measure of corneal thickness.

12. The apparatus according to claim 10 or claim 11, wherein said processor is configured to determine, from time variations in said optical path length, a biomechanical response of said cornea to relative differences between intraocular pressure and an external pressure on
20 said cornea.

13. The apparatus according to claim 12, wherein said processor is configured to determine a biomechanical response of said cornea to periodic intraocular pressure variations associated with the ocular pulse.

14. The apparatus according to claim 12 or claim 13, wherein said apparatus is configured
25 to vary said external pressure on said cornea.

15. The apparatus according to claim 14, wherein said apparatus is configured to vary said external pressure by applying a source of distributed sound waves, or by varying the ambient pressure at said cornea.

16. The apparatus according to claim 10 or claim 11, wherein said processor is configured to determine, from time variations in said optical path length, a biomechanical response of said cornea to a perturbation imposed by one or more of: an air puff source; a source of ultrasound; or a source of acoustic radiation pressure.

5 17. The apparatus according to claim 1, wherein said apparatus is configured to measure time variations in the thickness of a tear film on said cornea.

18. The apparatus according to any one of claims 10 to 16, wherein said processor is configured to:

10 measure time variations in the thickness of a tear film on said cornea; and
 subtract the measured time variations in tear film thickness from said optical path length to provide a normalised measurement of corneal optical path length.

19. A method for measuring one or more properties of a cornea, said method comprising the steps of:

15 generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a front surface of a cornea;
 capturing reflected or scattered light from said front surface and reflected or scattered light from a second surface or interface of said cornea;
 measuring relative phase between the reflected or scattered light from said front surface and the reflected or scattered light from said second surface or interface across the
20 portion of said cornea illuminated by said beamlets; and
 monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

20. The method according to claim 19, further comprising the steps of:

25 producing, from the relative phase measurements, a map of relative phase across the illuminated portion of said cornea; and
 monitoring said relative phase over time to determine time variations in said map.

21. The method according to claim 20, further comprising the steps of: interfering the reflected or scattered light from said front surface and from said second surface or interface with a reference beam to generate one or more interferograms; and utilising said one or more
30 interferograms to track the location of said beamlets on said front surface, for registering two or more maps of relative phase acquired at different times.

22. The method according to claim 20 or claim 21, wherein said beamlets are generated from a multi-wavelength optical source, and wherein said map of relative phase provides a tomographic profile of said cornea.

23. The method according to claim 22, wherein said tomographic profile comprises one or more of amplitude, phase or optical path length between said front surface and said second surface or interface.

24. The method according to claim 23, further comprising the step of determining, from time variations in said optical path length, a biomechanical response of said cornea to relative differences between intraocular pressure and an external pressure on said cornea.

25. The method according to claim 24, wherein a biomechanical response of said cornea to periodic intraocular pressure variations associated with the ocular pulse is determined.

26. The method according to claim 23, further comprising the steps of: imposing on said cornea a perturbation comprising one or more of an air puff, ultrasound or acoustic radiation pressure; and determining, from time variations in said optical path length, a biomechanical response of said cornea to said perturbation.

27. The method according to claim 19, further comprising the step of measuring time variations in the thickness of a tear film on said cornea.

28. The method according to any one of claims 23 to 26, further comprising the steps of: measuring time variations in the thickness of a tear film on said cornea; and subtracting the measured time variations in tear film thickness from said optical path length to provide a normalised measurement of corneal optical path length.

29. An apparatus for measuring one or more properties of a cornea, said apparatus comprising an optical system for:

generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a first surface or interface of a cornea;

capturing reflected or scattered light from said first surface or interface and reflected or scattered light from a second surface or interface of said cornea;

measuring relative phase between the first and second surfaces or interfaces across the portion of said cornea illuminated by said beamlets; and

monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

30. The apparatus according to claim 29, wherein said optical system is configured to measure the phases of said first and second surfaces or interfaces relative to a reference beam.

5 31. The apparatus according to claim 29, wherein said optical system is configured to measure the phases of said first and second surfaces or interfaces relative to a reflection from a tear film on said cornea.

32. The apparatus according to claim 31, wherein said first surface or interface comprises the air/tear film interface.

10 33. The apparatus according to any one of claims 29 to 32, wherein said apparatus comprises a processor for:

producing, from the relative phase measurements, a map of relative phase across the illuminated portion of said cornea; and

monitoring said relative phase over time to determine time variations in said map.

15 34. The apparatus according to claim 33, wherein said optical system comprises a multi-wavelength source for generating said beamlets, and wherein said processor is configured to calculate, from said map of relative phase, a tomographic profile of said cornea.

35. A method for measuring one or more properties of a cornea, said method comprising the steps of:

20 generating a converging array of beamlets configured to impinge simultaneously on at least a portion of a first surface or interface of a cornea;

capturing reflected or scattered light from said first surface or interface and reflected or scattered light from a second surface or interface of said cornea;

25 measuring relative phase between said first and second surfaces or interfaces across the portion of said cornea illuminated by said beamlets; and

monitoring said relative phase over time to obtain information on one or more properties of said cornea across the illuminated portion.

36. The method according to claim 35, wherein the phases of said first and second surfaces or interfaces are measured relative to a reference beam.

37. The method according to claim 35, wherein the phases of said first and second surfaces or interfaces are measured relative to a reflection from a tear film on said cornea.

38. The method according to claim 37, wherein said first surface or interface comprises the air/tear film interface.

5 39. The method according to any one of claims 35 to 38, further comprising the steps of:
producing, from the relative phase measurements, a map of relative phase across the illuminated portion of said cornea; and
monitoring said relative phase over time to determine time variations in said map.

40. The method according to claim 39, wherein said beamlets are generated from a multi-
10 wavelength optical source, and wherein said map of relative phase provides a tomographic profile of said cornea.

41. An apparatus for investigating a tear film on a cornea, said apparatus comprising:
an illumination system for illuminating a tear film or the anterior surface of a cornea at a plurality of points; and

15 a capture optical system for capturing return signals comprising hyper-reflective signals from said tear film or scattered light from said anterior surface at said plurality of points, said capture optical system having a capture angle,

wherein said illumination system is configured to, in use:

illuminate a first set of said plurality of points with light that impinges on said tear
20 film or said anterior surface at an angle of incidence sufficiently close to normal incidence such that said hyper-reflective signals are within said capture angle, resulting in a set of higher intensity return signals; and illuminate a second set of said plurality of points with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently far from normal incidence such that said hyper-reflective signals are not within
25 said capture angle, resulting in a set of lower intensity return signals;

and wherein said apparatus further comprises a processor for:

processing the higher intensity and lower intensity sets of return signals to obtain optical coherence tomography measurements; and

30 calculating, from selected optical coherence tomography measurements of the higher intensity and lower intensity sets of return signals, a measure related to the thickness of said tear film.

42. The apparatus according to claim 41, wherein said processor is configured to calculate said measure related to the thickness of said tear film by: fitting a surface to the optical coherence tomography measurements of the lower intensity set of return signals; and calculating differences between said surface and selected optical coherence tomography measurements of the higher intensity return signals.

43. The apparatus according to claim 41, wherein said processor is configured to calculate said measure related to the thickness of said tear film by: fitting a first surface to the optical coherence tomography measurements of the higher intensity return signals; fitting a second surface to the optical coherence tomography measurements of the lower intensity return signals; and calculating an offset between the first and second surfaces.

44. The apparatus according to any one of claims 41 to 43, wherein said processor is configured to monitor time variations in said measure related to the thickness of said tear film.

45. The apparatus according to any one of claims 41 to 44, wherein said processor is configured to determine a boundary between the set of higher intensity return signals and the set of lower intensity return signals.

46. The apparatus according to claim 45, wherein said processor is configured to obtain, from the size or shape of said boundary, or from time variations thereof, information on the thickness, quality or distribution of a lipid layer of said tear film.

47. The apparatus according to any one of claims 41 to 46, wherein said illumination system is configured to illuminate said tear film or said anterior surface of said cornea simultaneously at said plurality of points.

48. The apparatus according to claim 47, wherein said illumination system is configured to illuminate said tear film or said anterior surface of said cornea with an array of substantially parallel beamlets.

49. The apparatus according to any one of claims 41 to 48, wherein said illumination system is configured to illuminate the first set of points with light that impinges on said tear film or said anterior surface at an angle of incidence less than 15 degrees, more preferably less than 8 degrees, and most preferably less than 4 degrees.

50. The apparatus according to any one of claims 41 to 49, wherein said illumination system is configured to illuminate the second set of points with light that impinges on said tear film or said anterior surface at an angle of incidence greater than 4 degrees, more preferably greater than 8 degrees, and most preferably greater than 15 degrees.

5 51. A method for investigating a tear film on a cornea, said method comprising the steps of:

illuminating said tear film or the anterior surface of said cornea at a plurality of points;

10 capturing, with a capture optical system having a capture angle, return signals comprising hyper-reflective signals from said tear film or scattered light from said anterior surface at said plurality of points, wherein a first set of said plurality of points is illuminated with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently close to normal incidence such that said hyper-reflective signals are within said capture angle, resulting in a set of higher intensity return signals, and a second set of said
15 plurality of points is illuminated with light that impinges on said tear film or said anterior surface at an angle of incidence sufficiently far from normal incidence such that said hyper-reflective signals are not within said capture angle, resulting in a set of lower intensity return signals;

20 processing the higher intensity and lower intensity sets of return signals to obtain optical coherence tomography measurements; and

calculating, from selected optical coherence tomography measurements of the higher intensity and lower intensity sets of return signals, a measure related to the thickness of said tear film.

25 52. The method according to claim 51, wherein the calculating step comprises: fitting a surface to the optical coherence tomography measurements of the lower intensity return signals; and calculating differences between said surface and selected optical coherence tomography measurements of the higher intensity return signals.

30 53. The method according to claim 51, wherein the calculating step comprises: fitting a first surface to the optical coherence tomography measurements of the higher intensity return signals; fitting a second surface to the optical coherence tomography measurements of the lower intensity return signals; and calculating an offset between the first and second surfaces.

54. The method according to any one of claims 51 to 53, wherein said method further comprises the step of monitoring time variations in said measure related to the thickness of said tear film.

55. The method according to any one of claims 51 to 54, wherein said method further
5 comprises the step of determining a boundary between the set of higher intensity return signals and the set of lower intensity return signals.

56. The method according to claim 55, wherein said method further comprises the step of obtaining, from the size or shape of said boundary, or from time variations thereof, information on the thickness, quality or distribution of a lipid layer of said tear film.

10 57. The method according to any one of claims 51 to 56, wherein said tear film or said anterior surface of said cornea is illuminated simultaneously at said plurality of points.

58. The method according to claim 57, wherein said tear film or said anterior surface of said cornea is illuminated with an array of substantially parallel beamlets.

59. The method according to any one of claims 51 to 58, wherein the first set of points is
15 illuminated with light that impinges on said tear film or said anterior surface at an angle of incidence less than 15 degrees, more preferably less than 8 degrees, and most preferably less than 4 degrees.

60. The method according to any one of claims 51 to 59, wherein the second set of points is illuminated with light that impinges on said tear film or said anterior surface at an angle of
20 incidence greater than 4 degrees, more preferably greater than 8 degrees, and most preferably greater than 15 degrees.

61. An article of manufacture comprising a non-transitory computer usable medium having a computer readable program code configured to operate the apparatus according to any one of claims 1 to 18, 29 to 34, or 41 to 50, or to implement the method according to any
25 one of claims 19 to 28, 35 to 40, or 51 to 60.

1/10

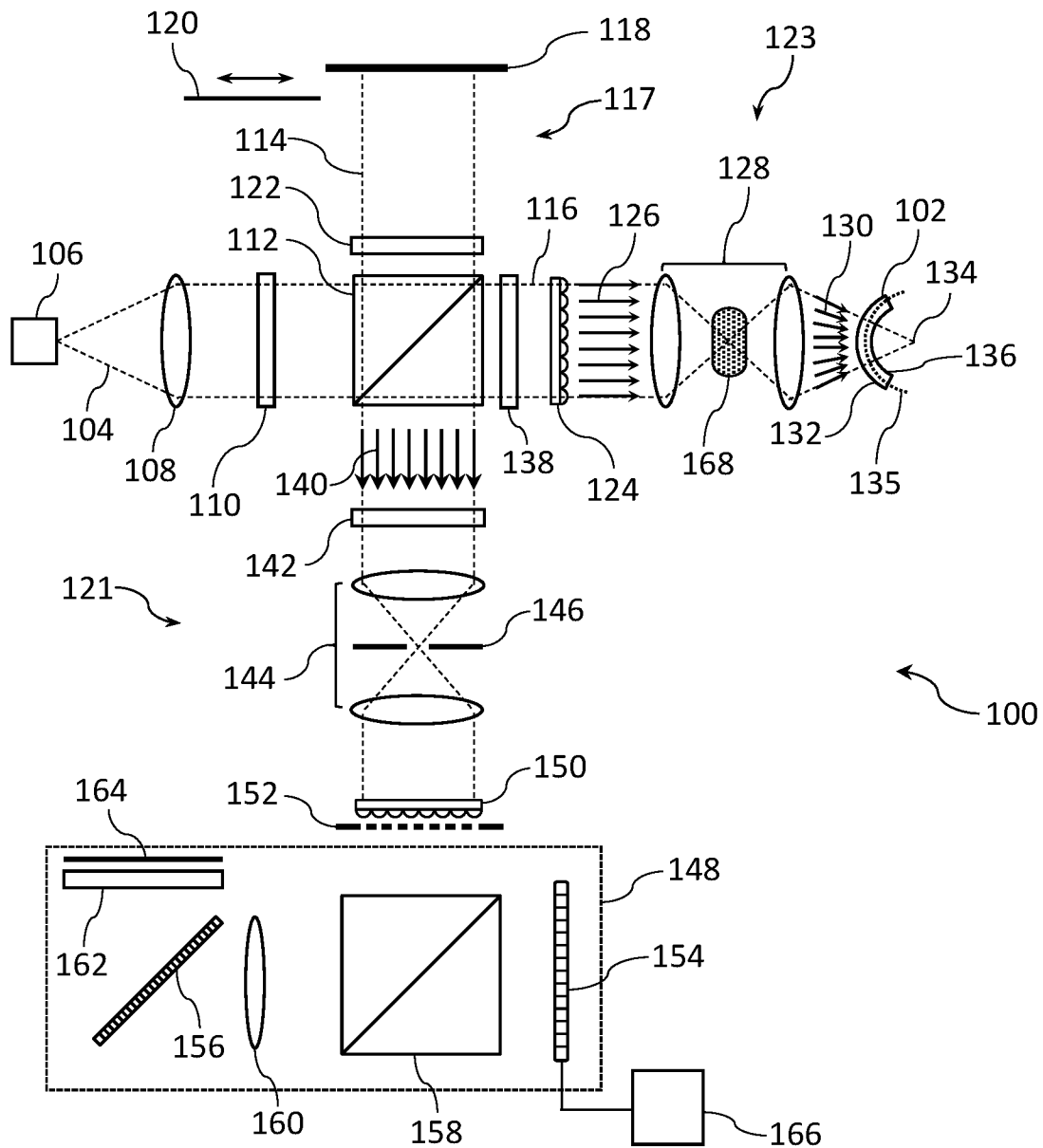


Fig. 1A

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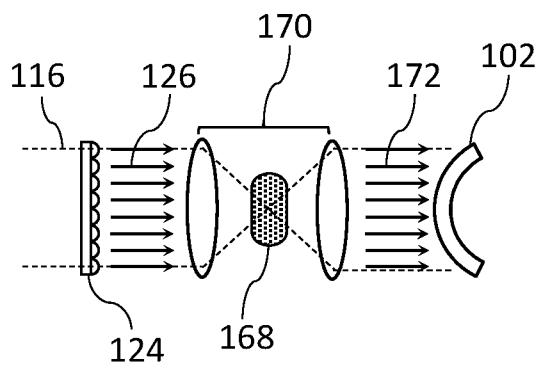


Fig. 1B

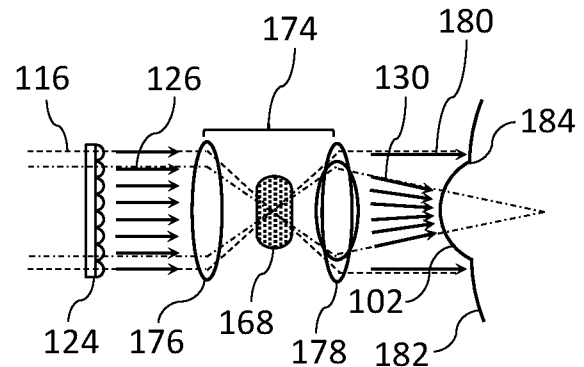


Fig. 1C

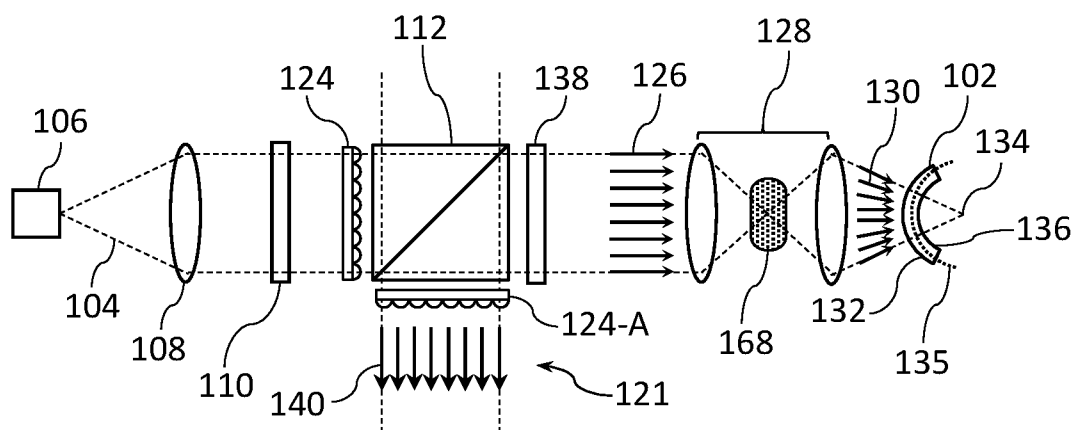


Fig. 1D

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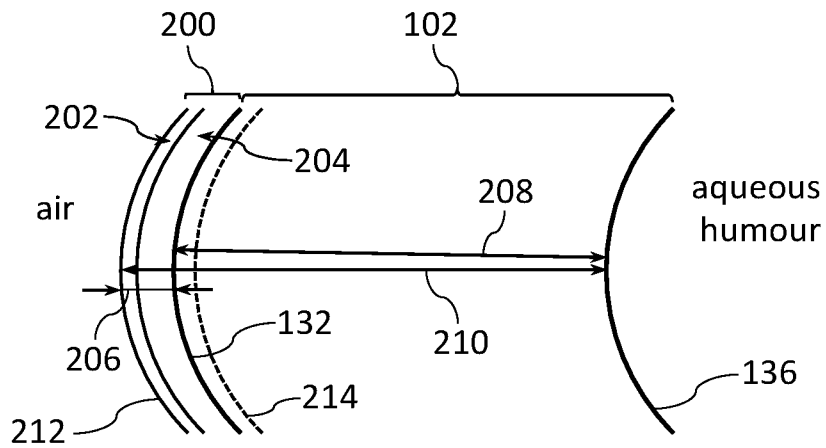


Fig. 2

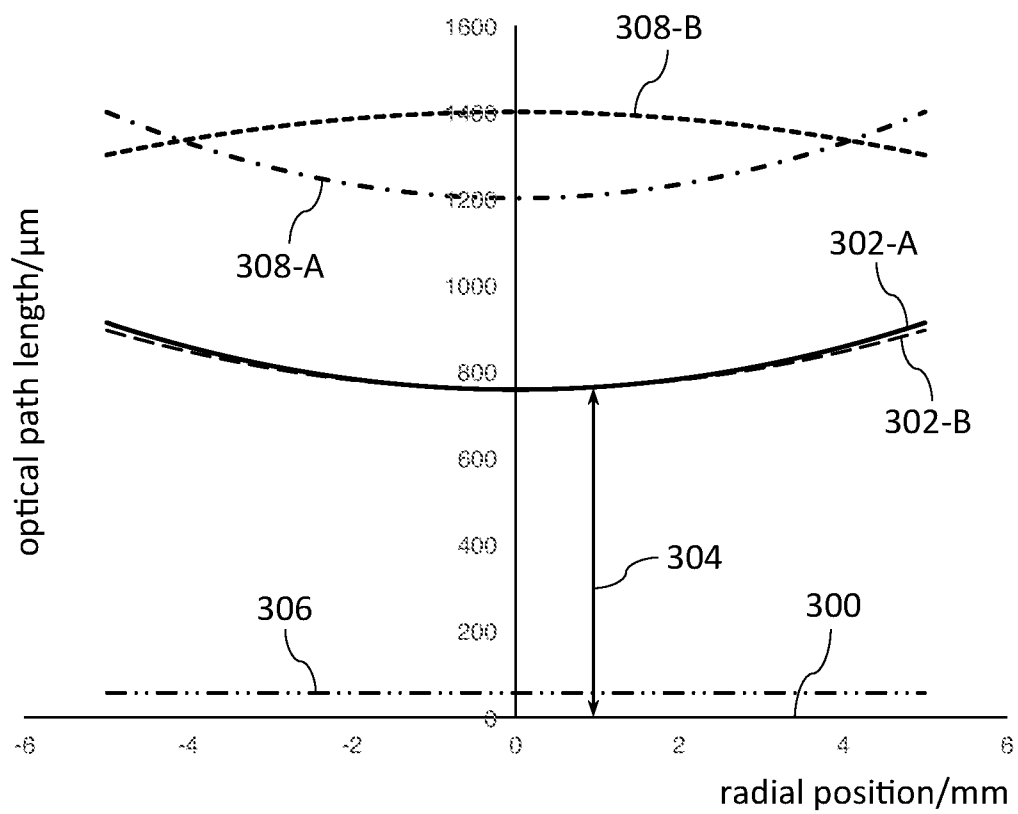


Fig. 3

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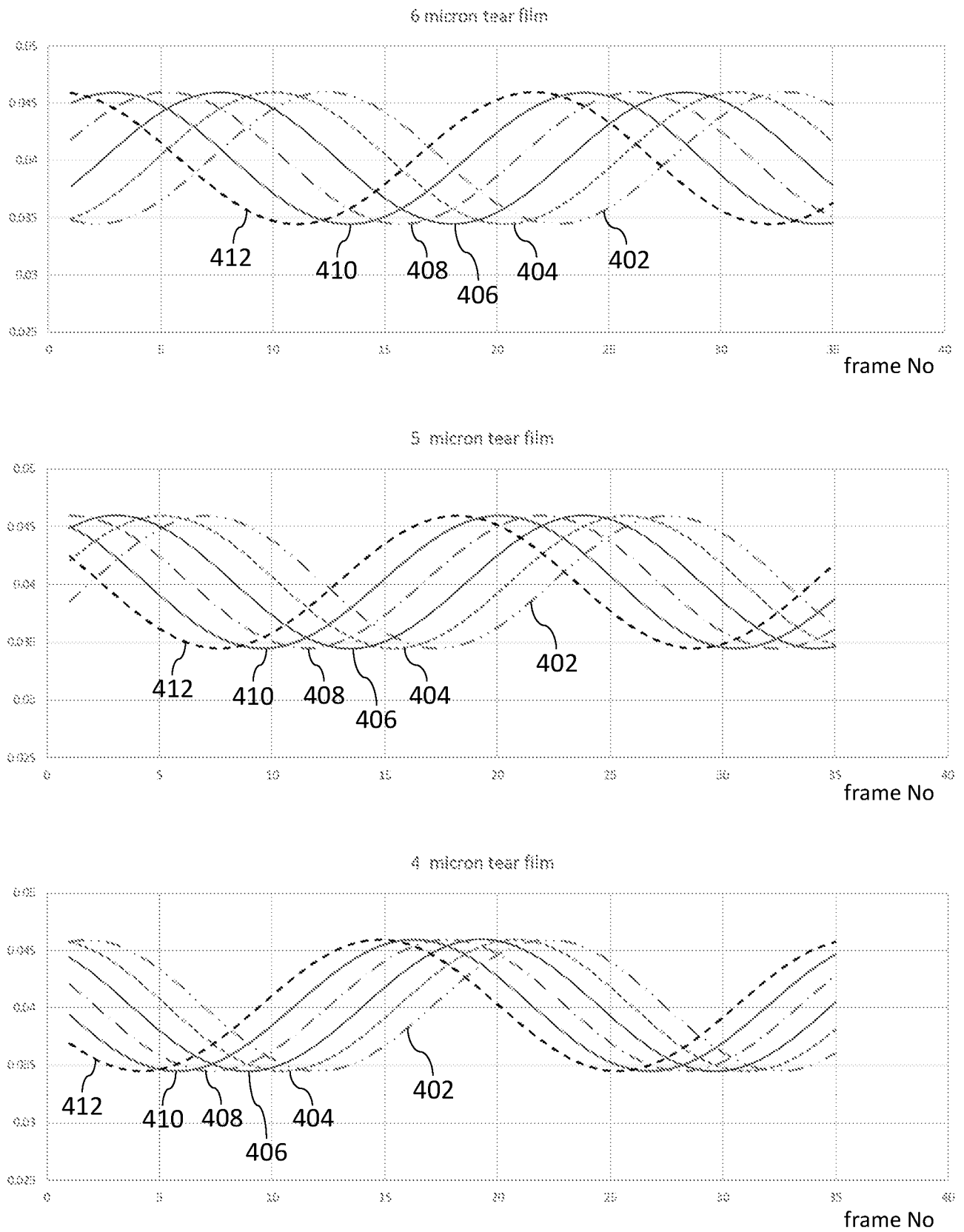


Fig. 4A

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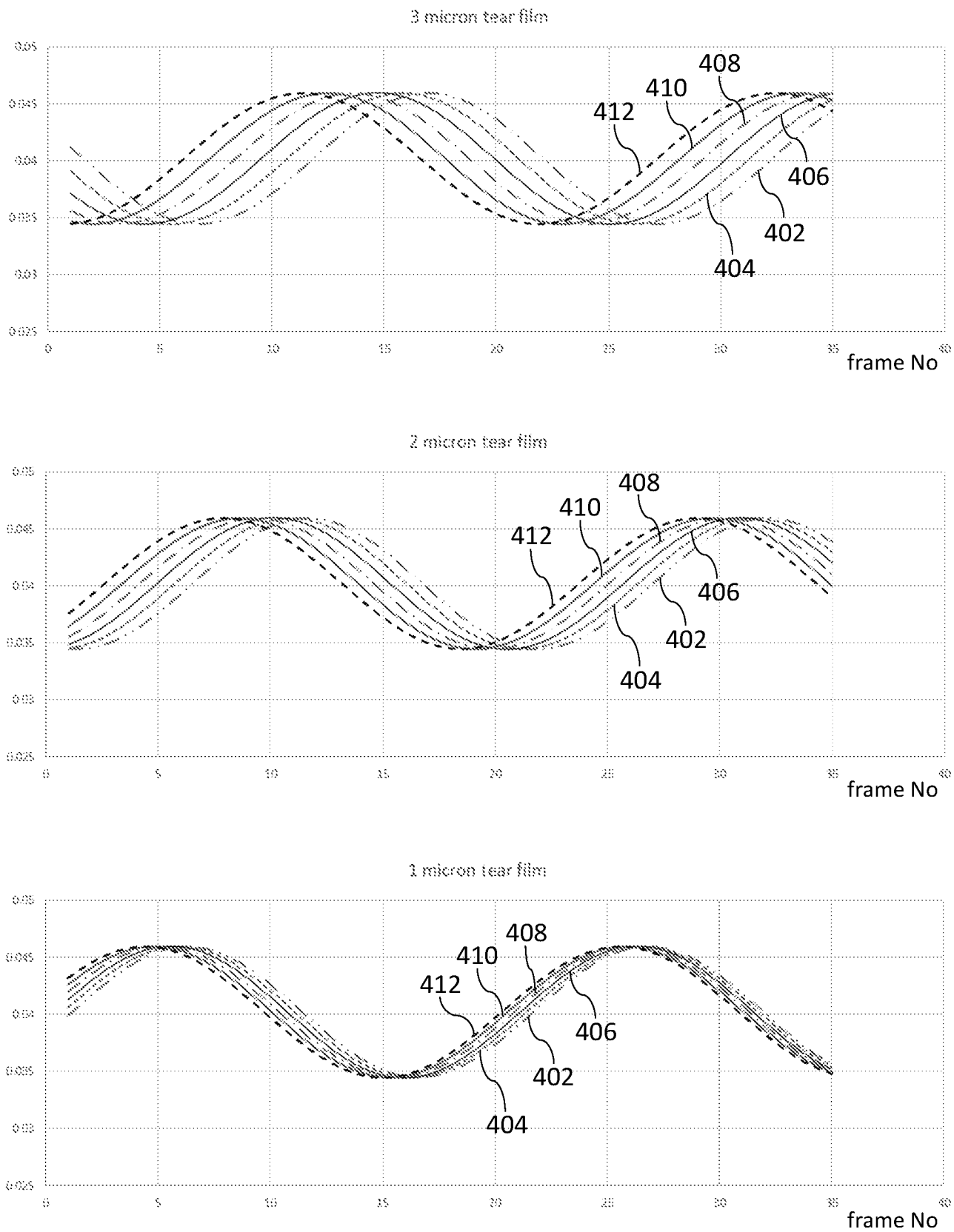


Fig. 4B

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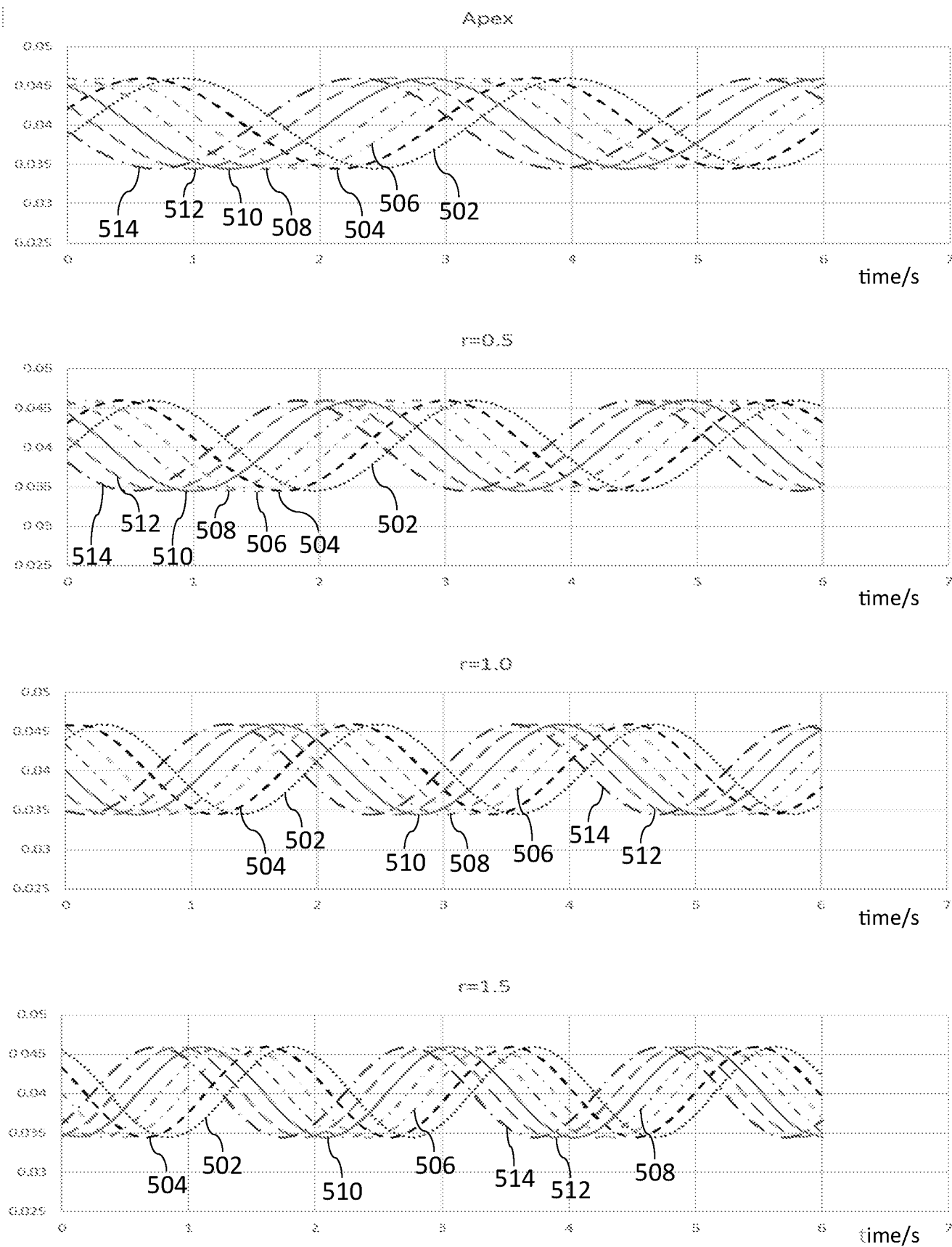


Fig. 5A

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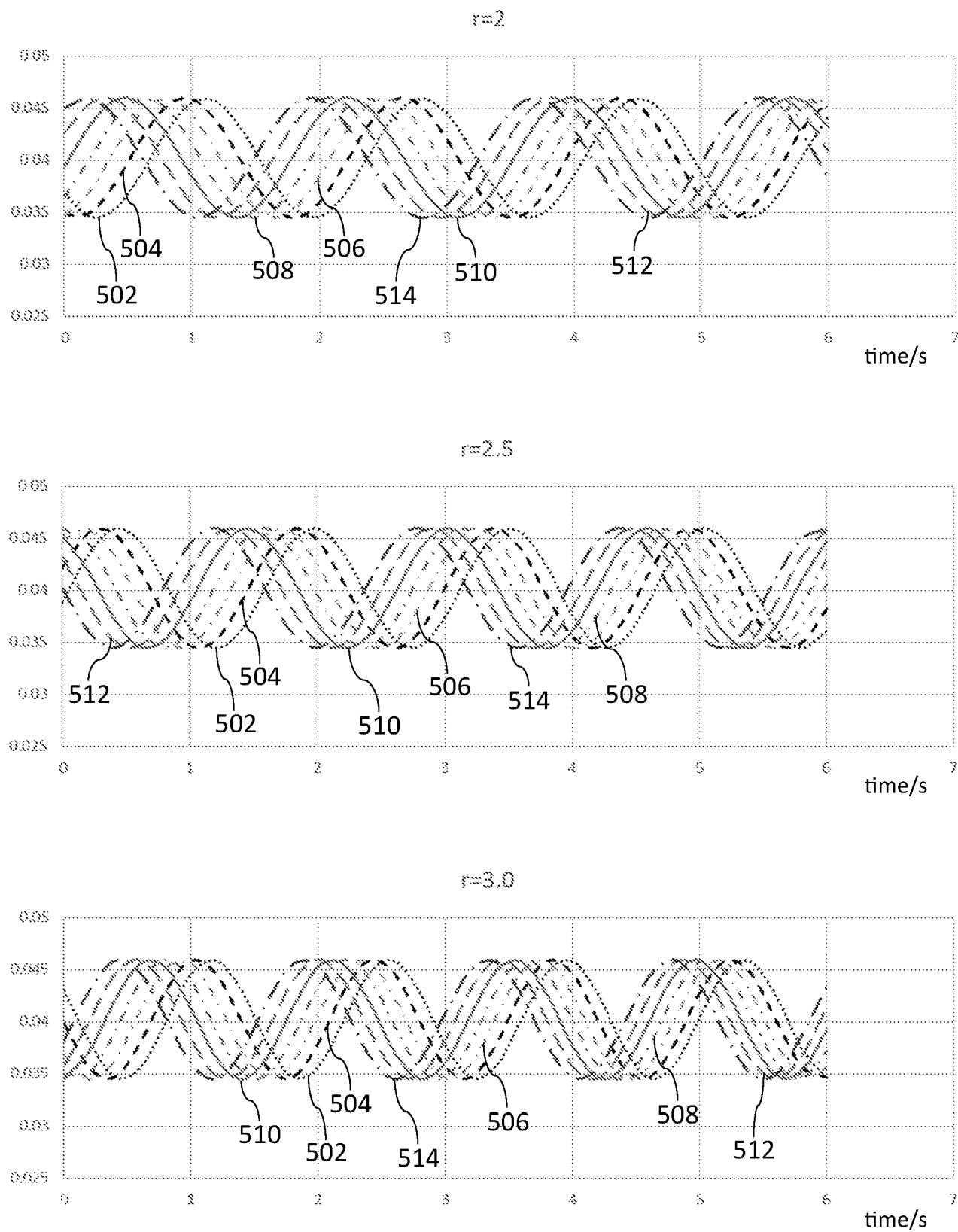


Fig. 5B

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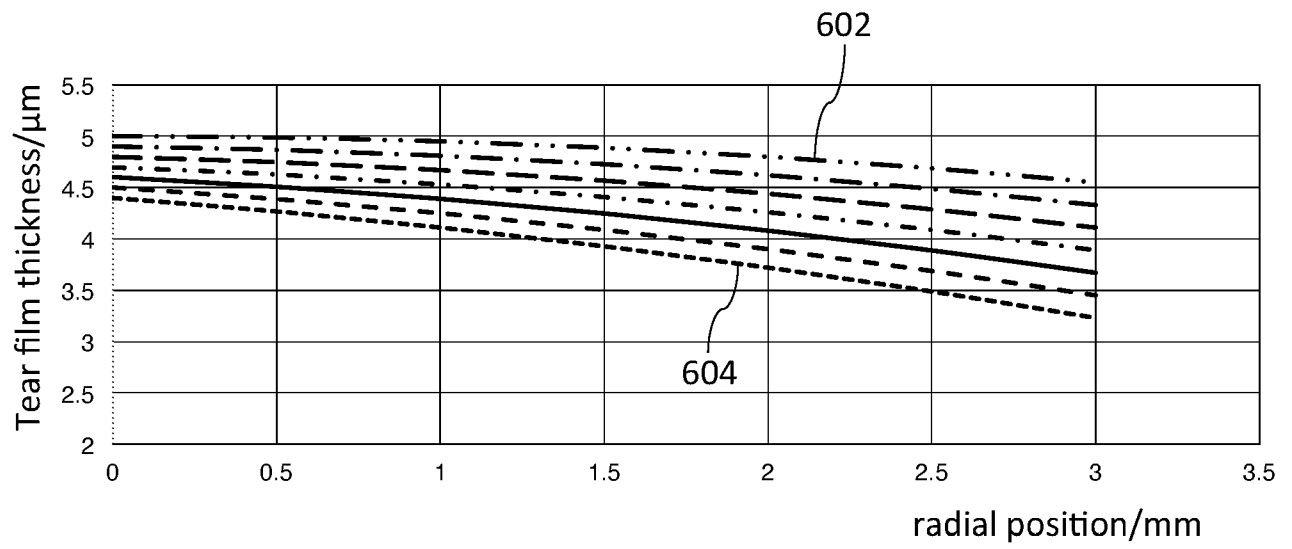


Fig. 6

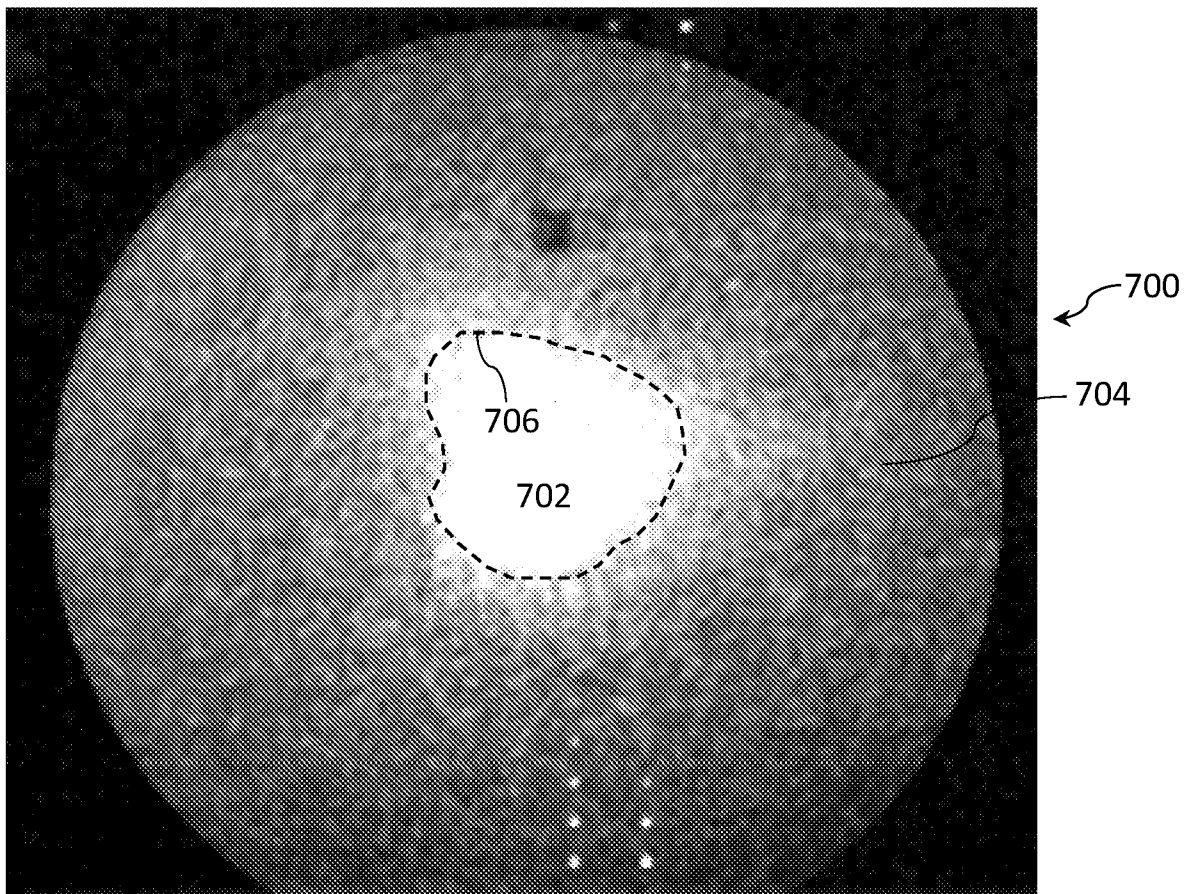


Fig. 7

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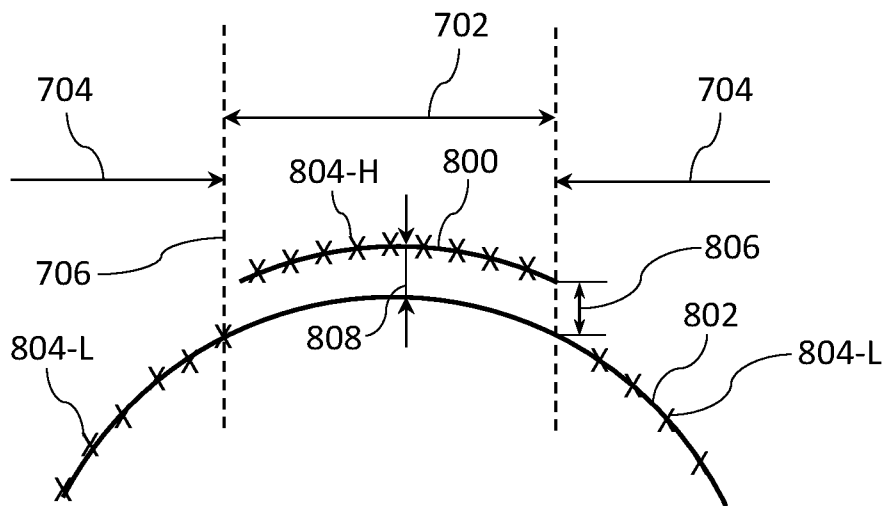


Fig. 8

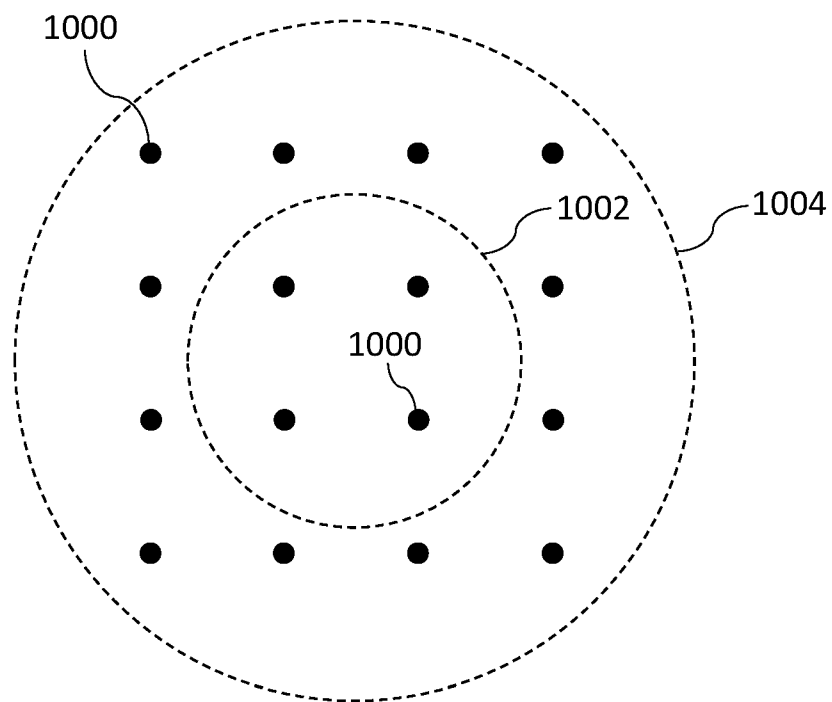


Fig. 10

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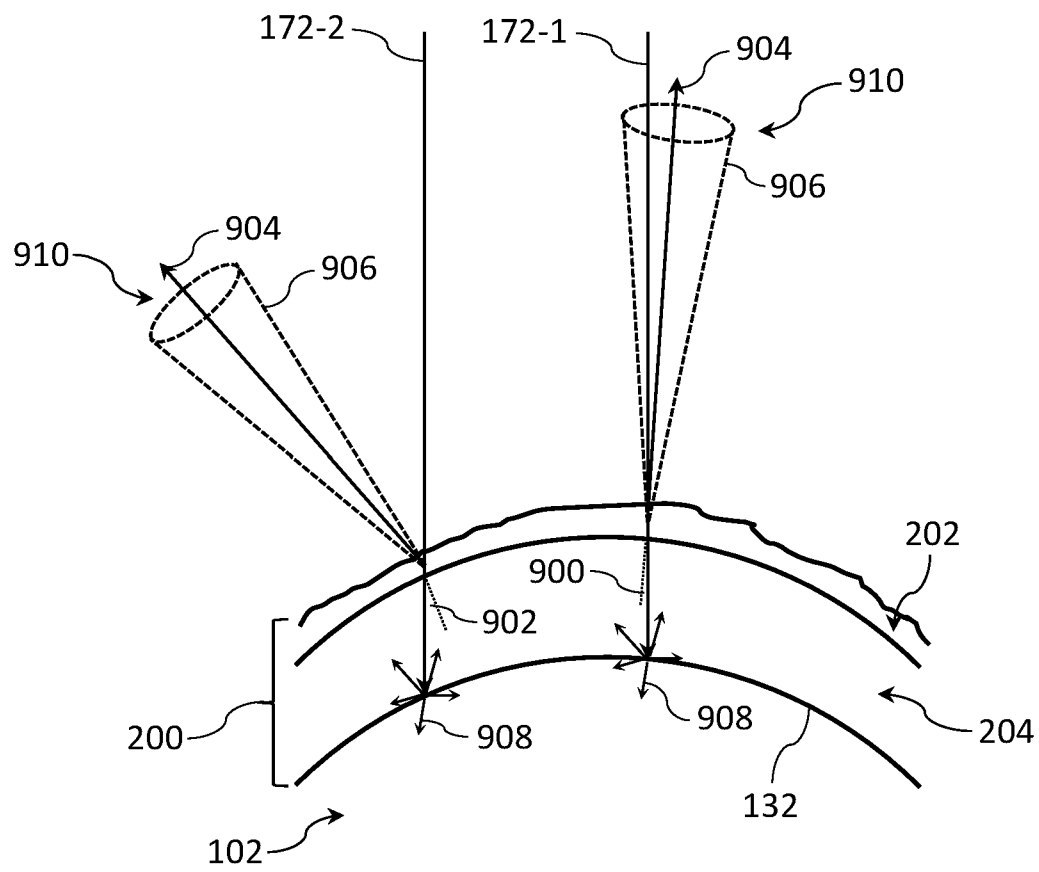


Fig. 9

INTERNATIONAL SEARCH REPORT

 International application No.
PCT/AU2019/050571

A. CLASSIFICATION OF SUBJECT MATTER

A61B 3/10 (2006.01)

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

PATENW: IPC/CPC symbols: A61B3/10/C/CC/IC/LOW, A61B3/1005/C/CC, A61B3/107/C/CC/IC/LOW, A61B3/101/C/CC/IC/LOW;
 PATENW keywords: cornea, phase, interfere, reflect, scatter, monitor, time, array, converge, pachymetry and like terms. Espacenet keywords: cornea, phase, pachymetry. Google Patent Keywords: phase, interference, cornea, scatter, reflect, time. Applicant(s)/Inventor(s) name searched in internal databases provided by IP Australia and Espacenet.

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
	Documents are listed in the continuation of Box C	



Further documents are listed in the continuation of Box C



See patent family annex

* Special categories of cited documents:	
"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"D" document cited by the applicant in the international application	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier application or patent but published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 26 September 2019	Date of mailing of the international search report 26 September 2019
Name and mailing address of the ISA/AU AUSTRALIAN PATENT OFFICE PO BOX 200, WODEN ACT 2606, AUSTRALIA Email address: pct@ipaustalia.gov.au	Authorised officer Harish Ramachandran AUSTRALIAN PATENT OFFICE (ISO 9001 Quality Certified Service) Telephone No. +61262832396

Box No. II Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:
the subject matter listed in Rule 39 on which, under Article 17(2)(a)(i), an international search is not required to be carried out, including
2. ☐ Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a)

Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

See Supplemental Box for Details

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying additional fees, this Authority did not invite payment of additional fees.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☒ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:
1-40, 61

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.
- ☐ The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.
- ☐ No protest accompanied the payment of additional search fees.

INTERNATIONAL SEARCH REPORT		International application No.
C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		PCT/AU2019/050571
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2018/0146851 A1 (CYLITE PTY LTD) 31 May 2018 whole document, especially abstract and paragraphs [0090]-[0091], fig. 10	1-40, 61
A	US 2017/0189233 A1 (OPTIMEDICA CORPORATION) 06 July 2017 whole document	1-40, 61
A	WO 2012/110051 A1 (WAVELIGHT GMBH) 23 August 2012 whole document, especially abstract, figs. 3-4, 6-8	1-40, 61

Form PCT/ISA/210 (fifth sheet) (July 2019)

Supplemental Box**Continuation of: Box III**

This International Application does not comply with the requirements of unity of invention because it does not relate to one invention or to a group of inventions so linked as to form a single general inventive concept.

This Authority has found that there are different inventions based on the following features that separate the claims into distinct groups:

- Claims 1-40, 61 (in part) are directed to an apparatus/method for measuring one or more properties of a cornea. The feature of measuring relative phase between the reflected or scattered light from the front surface and the reflected or scattered light from the second surface across the portion of the cornea and monitoring the relative phase over time to obtain information on one or more properties of the cornea is specific to this group of claims.
- Claims 41-60, 61 (in part) are directed to an apparatus/method for investigating a tear film on a cornea. The feature of capturing, with a capture optical system having a capture angle, return signals comprising hyper-reflective signals from the tear film, resulting in a set of higher intensity return signals within the capture angle and a set of lower intensity return signals outside the capture angle, processing the higher intensity and lower intensity return signals to obtain optical coherence tomography measurements, and calculating from the optical coherence tomography measurements a measure related to the thickness of the tear film is specific to this group of claims.

PCT Rule 13.2, first sentence, states that unity of invention is only fulfilled when there is a technical relationship among the claimed inventions involving one or more of the same or corresponding special technical features. PCT Rule 13.2, second sentence, defines a special technical feature as a feature which makes a contribution over the prior art.

When there is no special technical feature common to all the claimed inventions there is no unity of invention.

In the above groups of claims, the identified features may have the potential to make a contribution over the prior art but are not common to all the claimed inventions and therefore cannot provide the required technical relationship. Therefore there is no special technical feature common to all the claimed inventions and the requirements for unity of invention are consequently not satisfied *a priori*.

INTERNATIONAL SEARCH REPORT		International application No.	
Information on patent family members		PCT/AU2019/050571	
This Annex lists known patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.			
Patent Document/s Cited in Search Report		Patent Family Member/s	
Publication Number	Publication Date	Publication Number	Publication Date
US 2018/0146851 A1	31 May 2018	US 2018146851 A1	31 May 2018
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		EP 3011288 A1	27 Apr 2016
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		CA 2916057 A1	16 Apr 2015

Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.

Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.

INTERNATIONAL SEARCH REPORT		International application No.	
Information on patent family members		PCT/AU2019/050571	
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INTERNATIONAL SEARCH REPORT		International application No.	
Information on patent family members		PCT/AU2019/050571	
This Annex lists known patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.			
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INTERNATIONAL SEARCH REPORT		International application No.	
Information on patent family members		PCT/AU2019/050571	
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Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.			

INTERNATIONAL SEARCH REPORT		International application No.	
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Patent Document/s Cited in Search Report		Patent Family Member/s	
Publication Number	Publication Date	Publication Number	Publication Date
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Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.			

INTERNATIONAL SEARCH REPORT		International application No.	
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Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.			
Form PCT/ISA/210 (Family Annex)(July 2019)			

INTERNATIONAL SEARCH REPORT Information on patent family members		International application No. PCT/AU2019/050571	
This Annex lists known patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.			
Patent Document/s Cited in Search Report		Patent Family Member/s	
Publication Number	Publication Date	Publication Number	Publication Date
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		MX 2013009422 A	24 Jan 2014
		MX 356121 B	14 May 2018
		RU 2013140352 A	27 Mar 2015
		US 2013321822 A1	05 Dec 2013
End of Annex			
Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001. Form PCT/ISA/210 (Family Annex)(July 2019)			