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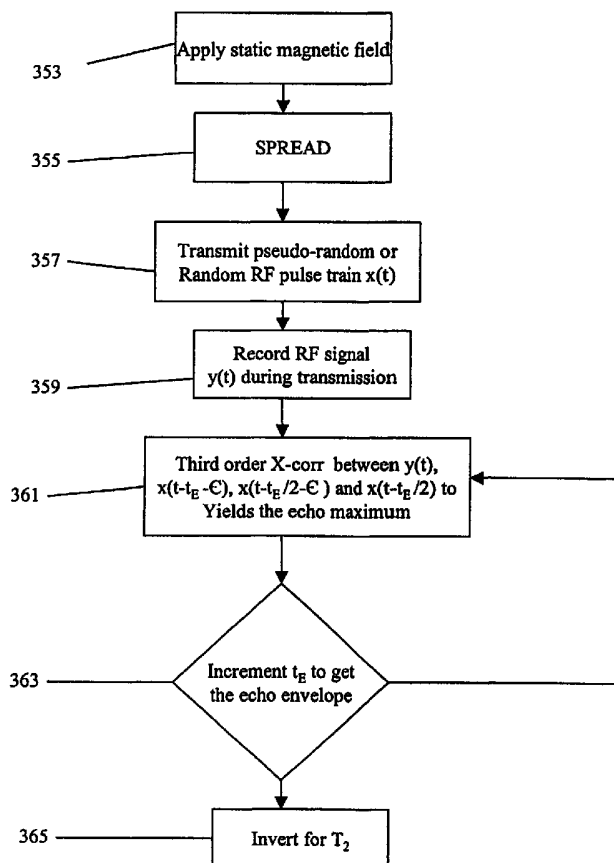
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(54) Title: STOCHASTIC NMR FOR DOWNHOLE USE



(57) Abstract: Stochastic pulsing using random or pseudo-random sequences is used for determination of nuclear spin properties of earth formations. This reduces the power requirements. Processing of the received signals may include linear or nonlinear cross-correlation with the excitation pulse sequence. Inversion of the results of the processing gives the desired nuclear spin property.

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STOCHASTIC NMR FOR DOWNHOLE USE**BACKGROUND OF THE INVENTION****Field of the Invention**

[0001] The invention is related to the field of Nuclear Magnetic Resonance
5 (NMR) methods. In particular, the invention details new methods for creating
excitation pulses using stochastic processes in measurement procedures in
downhole wellbore logging techniques.

Description of the Related Art

10 [0002] NMR is used for well logging and MWD to obtain information on
wellbore structure in the form of the NMR signal amplitude, and T_1 and/or T_2
relaxation times. From these measurements can be determined quantities that
are of importance in oil drilling, such as total porosity, bound and unbound
fluid, permeability, etc. The traditional method for this downhole NMR is
15 pulsed NMR, using hard (strong) RF pulses, which cause spin-flip angles of the
order of 90° and 180° . In a more general sense, this type of NMR is
spectroscopy of the strong nonlinear type, meaning that the response of the
NMR system is not proportional to the strength of the excitation.

20 [0003] NMR methods are based on the well-understood properties of nuclear
spin moments subjected to both a static external magnetic field and an
oscillating external magnetic field. It is known that in the absence of a
magnetic field, nuclear spin vectors will orient themselves in random directions.

In the presence of only a static magnetic field, these individual spins tend to align themselves along the direction of the applied field. This alignment gives rise to an overall magnetization, referred to as the bulk magnetization vector. When the external field is removed, the spins resume their random orientation,
5 and the bulk magnetization vector falls to zero.

[0004] Typical NMR methods determine properties of the material by observing how applied RF magnetic fields affect the spin vectors. In current methods, spins are first aligned via the application of a static external magnetic field. In
10 well logging, this magnetic field is typically provided by a permanent magnet. Once the spins have reached saturation, a single RF magnetic pulse is applied perpendicular to the static field which aligns the spins generally in the plane perpendicular to this applied field in a direction generally perpendicular to both the static and RF fields. This pulse is referred to as a 90E pulse. If only the
15 90E pulse is applied, measurements can be obtained for the rate at which the spins realign along the direction of the static magnetic field. The rate of return along this direction is characterized by a time constant known as the spin-lattice relaxation time, T_1 .

20 [0005] After the application and removal of a 90E magnetic pulse, the spins, as well as realigning along the direction of the constant field, exhibit a precession around the direction of the static field with a frequency known as the Larmor

frequency. The Larmor frequency is given by $\omega_0 = \gamma B_0$, where γ is the gyromagnetic ratio and B_0 is the strength of the applied constant field.

[0006] Typically, the effective static magnetic field is inhomogeneous
5 throughout the formation. As a result according to its local magnetic field, each spin vector tends to precess at slightly different rates. The phase between the vectors, originally nearly zero at the moment the RF magnetic field is removed, diffuses as some vectors spin faster and some spin slower. The diffusion of the phase leads to a reduction of the component of the bulk magnetization in the
10 plane perpendicular to the applied field. This process is known as dephasing. This decay is known as the free induction decay rate and is characterized by its time constant, T_2^* . The dephasing can be recovered partly as long as the underlying cause, the local spatial variation of the magnetic field is static. This is done by using one or more refocusing pulse and leads to the formation of one
15 or more spin echos. The decay of these echos is characterized by its time constant T_2 .

[0007] In prior art, in order to observe the values for these time constants, and in particular of T_2 , the practitioner often applies a sequence of RF magnetic
20 pulses. A sequence of pulses that is used widely in current methods is known as the Carr-Purcell-Meiboom-Gill (CPMG) sequence. In this sequence, the first pulse is a 90° pulse, which aligns the spins generally perpendicular to the applied static magnetic field. Subsequent pulses have twice the duration of the

first pulse, and as a result are able to flip each spin vector a full 180^0 from the direction it had immediately prior to the application of the pulse. A 180^0 pulse is typically applied during a dephasing stage of the spin echos. After the pulse is removed, the order of the spins is reversed, with the slowly precessing spins spatially in front of the faster precessing spins. The phase between the spin vectors, which was previously diffusing, now is converging back to zero. At convergence, the spin vectors are generally aligned in a common direction again, and the bulk magnetization vector reaches a maximum value, creating a magnetic pulse known as a spin echo. The spin echo induces a voltage in a receiver coil, which is measured through the electronic assembly attached to the coil.

[0008] The CPMG sequence can be expressed as

$$TW - 90 - (t - 180 - t - \text{echo})_n \quad (1)$$

where TW is a wait time, 90 is an excitation pulse having a tipping angle of 90^0 , and 180 is a 180^0 refocusing pulse. This gives a sequence of n echo signals. US Patent 6,163,153 to *Reiderman* et al and co-pending US Patent Application Ser. No. 09/551,761 of *Slade* et al, both having the same assignee as the present application, disclose use of a modified CPMG sequence in which the refocusing pulses have tipping angles of less than 180^0 . This can significantly reduce the power requirements. However, power requirements even for tipping angles of 90^0 can still be significant. In addition, CPMG sequences or modified CPMG sequences such as those taught by *Reiderman* and by *Slade* are relatively inefficient in power utilization in that the duty cycle is small, i.e., large amounts

of power are expended in relatively short time intervals and in much of the time (the time between the pulses), no power is used and the apparatus is waiting for the nuclear spin system to respond to the pulses. It would be desirable to have a method of NMR logging that can reduce the power requirements and make
5 more uniform use of power, while still obtaining useful information about formation properties. The present invention satisfies this need.

SUMMARY OF THE INVENTION

[0009] The present invention is method of determining a nuclear magnetic
10 resonance spin relaxation property (parameter of interest) of a region of interest of an earth formation. A magnet on a logging tool conveyed in a borehole in the earth formation is used for producing a static magnetic field in the region of interest and aligning nuclear spins within said region of interest. A primary pulse sequence of small flip angle pulses, random or pseudo-random, is
15 defined. A pulse sequence derived from the primary pulse sequence is used to modulate the radio frequency (RF) output of a transmitting antenna and alter the nuclear spins. A receiving antenna is used for receiving signals indicative of said altered nuclear spins. A processor determines from the received signals the parameter of interest..

20

[0010] The logging tool may be conveyed into the earth formation on a wireline or on a drilling tubular. The logging tool may be a gradient logging tool or it may be one in which the static magnetic field has substantially zero gradient in the region of interest.

[0011] The parameter of interest may be an apparent transverse relaxation time T_2^* , a transverse relaxation time T_2 , or a longitudinal relaxation time T_1 .

Depending upon the parameter of interest, the primary pulse sequence is one of
5 an equal amplitude random phase sequence, a random amplitude equal phase pulse sequence, a random amplitude random phase pulse sequence, and, a maximum length binary sequence.

[0012] In different embodiments of the invention, the applied pulse sequence
10 may be a scaled version of the primary pulse sequence or it may comprise a scaled and time shifted version of the primary pulse sequence. In different embodiments of the invention, linear or non-linear cross-correlation may be performed in determining the parameter of interest.

15 **BRIEF DESCRIPTION OF THE DRAWINGS**

[0013] The present invention is best understood by reference to the following figures in which like numerals refer to like elements.

Figure 1 (PRIOR ART) is a schematic illustration of an exemplary drilling system using the present invention.

20 Figures 2A-2C (PRIOR ART) are side elevational views partially in cross section (see Figure 2B) of a drilling assembly including a sensor assembly in accordance with the present invention

Figure 3 is a flow chart illustrating a method for determination of T_2^* from a detection of the free induction decay (FID)

Figure 3a is an example of a Hadamard matrix

Figure 4 is a flow chart illustrating a method for determination of T_2 using a nonlinear cross-correlation.

Figure 5 is a flow chart illustrating a method for determination of T_2 using a
5 linear cross-correlation

Figure 6 is a flow chart illustrating a method for determination of T_2 using multiple echo generation.

Figure 7 is a flow chart illustrating a method for determination of T_1 using saturation

10 **DESCRIPTION OF PREFERRED EMBODIMENT**

[0014] An NMR well logging apparatus which is suitable for use with this invention is described, for example, in United States Patent 6,247,542 to Kruspe et al., the contents of which are fully incorporated herein by reference. The device in *Kruspe* is for exemplary purposes only and the method of the present
15 invention may be used with any NMR well logging apparatus including one conveyed on a wireline. As taught by *Kruspe*, the NMR sensor assembly is slidably coupled to the longitudinal member wherein the sensor assembly includes at least one sensor for obtaining measurements relating to the parameter of interest. When the sensor assembly is held in a non-rotating
20 position, for instance, for obtaining the measurements, the longitudinal member is free to rotate and continue drilling the borehole. The sensor assembly is slidably coupled to the longitudinal member using, for example, at least one guide sleeve slidably coupled to the longitudinal member. The sensor assembly further includes, for example, at least one transmitter. The sensor assembly of

the present invention can include any of a variety of sensors and/or transmitters for determining a plurality of parameters of interest including, for example, nuclear magnetic resonance measurements. The device of *Kruspe* makes it possible, for example, to obtain NMR measurements with the NMR assembly
5 clamped to the borehole while drilling continues.

[0015] Figure 1 (PRIOR ART) shows a schematic diagram of a drilling system 10 with a drillstring 20 carrying a drilling assembly 90 (also referred to as the bottom hole assembly, or "BHA") conveyed in a "wellbore" or "borehole" 26
10 for drilling the wellbore. The drilling system 10 includes a conventional derrick 11 erected on a floor 12 which supports a rotary table 14 that is rotated by a prime mover such as an electric motor (not shown) at a desired rotational speed. The drillstring 20 includes a tubing such as a drill pipe 22 or a coiled-tubing extending downward from the surface into the borehole 26. The drillstring 20 is
15 pushed into the wellbore 26 when a drill pipe 22 is used as the tubing. For coiled-tubing applications, a tubing injector (not shown), however, is used to move the tubing from a source thereof, such as a reel (not shown), to the wellbore 26. The drill bit 50 attached to the end of the drillstring breaks up the geological formations when it is rotated to drill the borehole 26. If a drill pipe
20 22 is used, the drillstring 20 is coupled to a drawworks 30 via a Kelly joint 21, swivel 28, and line 29 through a pulley 23. During drilling operations, the drawworks 30 is operated to control the weight on bit, which is an important parameter that affects the rate of penetration. The operation of the drawworks is well known in the art and is thus not described in detail herein.

[0016] During drilling operations, a suitable drilling fluid 31 from a mud pit (source) 32 is circulated under pressure through a channel in the drillstring 20 by a mud pump 34. The drilling fluid passes from the mud pump 34 into the drillstring 20 via a desurger (not shown), fluid line 38 and Kelly joint 21. The drilling fluid 31 is discharged at the borehole bottom 51 through an opening in the drill bit 50. The drilling fluid 31 circulates uphole through the annular space 27 between the drillstring 20 and the borehole 26 and returns to the mud pit 32 via a return line 35. The drilling fluid acts to lubricate the drill bit 50 and to carry borehole cutting or chips away from the drill bit 50. A sensor S_1 preferably placed in the line 38 provides information about the fluid flow rate. A surface torque sensor S_2 and a sensor S_3 associated with the drillstring 20 respectively provide information about the torque and rotational speed of the drillstring. Additionally, a sensor (not shown) associated with line 29 is used to provide the hook load of the drillstring 20.

15

[0017] In one embodiment of the invention, the drill bit 50 is rotated by only rotating the drill pipe 22. In another embodiment of the invention, a downhole motor 55 (mud motor) is disposed in the drilling assembly 90 to rotate the drill bit 50 and the drill pipe 22 is rotated usually to supplement the rotational power, if required, and to effect changes in the drilling direction.

20

[0018] In the preferred embodiment of Figure 1, the mud motor 55 is coupled to the drill bit 50 via a drive shaft (not shown) disposed in a bearing assembly 57. The mud motor rotates the drill bit 50 when the drilling fluid 31 passes through

the mud motor **55** under pressure. The bearing assembly **57** supports the radial and axial forces of the drill bit. A stabilizer **58** coupled to bearing assembly **57** acts as a centralizer for the lowermost portion of the mud motor assembly.

5 **[0019]** In one embodiment of the invention, a drilling sensor module **59** is placed near the drill bit **50**. The drilling sensor module contains sensors, circuitry and processing software and algorithms relating to the dynamic drilling parameters. Such parameters preferably include bit bounce, stick-slip of the drilling assembly, backward rotation, torque, shocks, borehole and annulus
10 pressure, acceleration measurements and other measurements of the drill bit condition. A suitable telemetry or communications sub **72** using, for example, two-way telemetry, is also provided as illustrated in the drilling assembly **90**. The drilling sensor module processes the sensor information and transmits it to the surface control unit **40** via the telemetry system **72**.

15
[0020] The communication sub **72**, a power unit **78** and an MWD tool **79** are all connected in tandem with the drillstring **20**. Flex subs, for example, are used in connecting the MWD tool **79** in the drilling assembly **90**. Such subs and tools form the bottom hole drilling assembly **90** between the drillstring **20** and the
20 drill bit **50**. The drilling assembly **90** makes various measurements including the pulsed nuclear magnetic resonance measurements while the borehole **26** is being drilled. The communication sub **72** obtains the signals and measurements and transfers the signals, using two-way telemetry, for example, to be processed

on the surface. Alternatively, the signals can be processed using a downhole processor in the drilling assembly 90.

[0021] The surface control unit or processor 40 also receives signals from other
5 downhole sensors and devices and signals from sensors S_1 - S_3 and other sensors
used in the system 10 and processes such signals according to programmed
instructions provided to the surface control unit 40. The surface control unit 40
displays desired drilling parameters and other information on a display/monitor
42 utilized by an operator to control the drilling operations. The surface control
10 unit 40 preferably includes a computer or a microprocessor-based processing
system, memory for storing programs or models and data, a recorder for
recording data, and other peripherals. The control unit 40 is preferably adapted
to activate alarms 44 when certain unsafe or undesirable operating conditions
occur.

15

[0022] A segment 70 of drill pipe 22, illustrated in greater detail in Figures 2,
illustrates the apparatus and method according to the present invention
including a sleeve member, such as a sensor assembly, slidably coupled to a
longitudinal member, such as a section of drill pipe, wherein, when the sleeve
20 member is non-rotating, the longitudinal member is free to rotate. The sleeve
member may be held in a non-rotating position through engagement with the
borehole wall and a decoupling of the sleeve member and the rotating
drillstring. The sleeve member including the sensor assembly illustrated in
Figure 2 describes a nuclear magnetic resonance device according to the present

invention. However, the apparatus and method according to the present invention can be adapted for any MWD device or tool typically used on a rotating drillstring or for wireline logging.

5 [0023] Referring to Figures 2A-2C, the drilling assembly 90 at the end of the drillstring 20 or coiled tubing is illustrated including the segment 70 of drill pipe 22 according to the present invention. The MWD tool 79, including an associated pulsed NMR tool 77 having a sensor assembly 113, and the pulsed power unit 78 are connected in tandem in the drilling assembly 90. The MWD
10 tool 79 may also include a sonic sensor, a density measurement tool, and a porosity measurement tool. As seen in Figure 2B, the NMR tool 77 is rotationally symmetric about a longitudinal axis 128 of the drilling assembly 90.

[0024] The longitudinal member is, for example, a drill pipe section 101, which
15 forms the core of the segment 70. Alternatively, the longitudinal member is a shaft in a downhole directional drilling assembly. The drill pipe section 101 is connected to the drillstring 20 by the upper tool joint 103 and the lower tool joint 139, and has a channel or flow pass 105 for the drilling mud to flow downhole. The sensor assembly 113 surrounds the drill pipe section 101 and is
20 slidably coupled to the longitudinal member or the drill pipe section 101. The sensor assembly 113 is coupled to the drill pipe section 101 by at least one of guide sleeves 109 and 111. The guide sleeves 109 and 111 include, for instance, slip rings and bearings 110 and 112, respectively. Alternatively, a single guide sleeve (not shown) including slip rings and bearings, is used, for

example, centrally located between ends of the sensor assembly 113. The guide sleeves 109 and 111 allow the sensor assembly 113 to move freely in the axial direction and to a lesser extent laterally with respect to the drill pipe section 101. The sensor assembly 113 has an outer diameter that is somewhat less than the inner diameter of the borehole 26. For illustrative purposes, Figure 2B shows the space between the sensor assembly 113 and the borehole wall in an exaggerated manner. The NMR sensor assembly includes flow paths 107 and 114 for return flow of the drilling mud from the drilling assembly 90 below wherein the gap between the sensor assembly 113 and the borehole wall are minimized.

[0025] The magnet assembly 115, for providing the static magnetic field, and the RF coil assembly 117 are disposed in the sensor assembly 113. The RF coil assembly 117 includes, for instance, at least one transmitter for transmitting a pulsed RF field into the formation. In the configuration as illustrated in Figure 2B, the RF field is axial and is orthogonal to the static field of the permanent magnet assembly 115 in a region of interest or examination outside the borehole for NMR signal measurements. However, the apparatus of the present invention is not limited to the illustrated sensor assembly 113. Any number of appropriate magnet arrangements and antenna or coil arrangements which provide a static magnetic field and an RF field orthogonal to the static magnetic field direction for creating the region of interest for NMR signal sensitivity can be used according to the present invention. For example, the NMR tool 77 can

employ separate transmitter and receiver RF coils, located, for example, on the sensor assembly 113.

[0026] Typically, the RF coil assembly 117 is pulsed and creates a high
5 frequency electromagnetic RF field orthogonal to the static magnetic field
generated by the magnet assembly 115 and in the region of substantially
uniform field strength creating the region or volume of interest for NMR signal
sensitivity. The sensor assembly 113 detects the NMR signals resulting
therefrom. Rock pores in the earth formations surrounding the wellbore are
10 filled with fluid, typically water or hydrocarbon. The hydrogen nuclei in the
fluid are aligned by the region of homogeneous magnetic field, generated by the
magnet assembly 115. The hydrogen nuclei are then flipped away from the
homogeneous magnetic field by the pulsed RF field produced by RF coil
assembly 117. At the termination of the pulsed RF field from RF coil assembly
15 117, the hydrogen nuclei revolve or precess at high frequency around the
homogeneous magnetic field inducing an NMR signal in the RF coil assembly
117 until the hydrogen nuclei relax to the original direction along the
homogeneous magnetic field. The induced NMR signals are processed
downhole or sent to the surface for processing.

20

[0027] Those versed in the art would recognize that, depending upon the
configuration of the permanent magnet assembly 115, the region of examination
could have one of a number of configurations. In one embodiment, the region
of examination could be substantially toroidal shaped with the axis of the toroid

along the longitudinal axis of the tool. In other configurations, the region of examination could be localized on opposite sides of the borehole or even on just one side of the borehole. It will also be clearly apparent to those skilled in the art that the static magnetic field area can also be obtained if the magnet
5 assembly **115** includes dc-energized electromagnets, or superconducting dc electromagnets. All of these are intended to be within the scope of the present invention.

[0028] The NMR electronics **129** is housed in the NMR sensor assembly **113**.
10 The purpose of the NMR electronics **129** is to control the sensor assembly **113**, record, process and transmit the recorded data, to the telemetry module **72**. This can be done by means of electrical or acoustic telemetry by known devices and will not be discussed. A spring **130** having a cable conduit through the spring **130** allows power and data transmission via the guide sleeve **111** and slip ring
15 through the cable conduit to and from the MWD tool **79**. The MWD tool **79** also transmits data to the sensor assembly **113**, for example, through mud pulse telemetry, and provides power from the power unit **78**.

[0029] The sensor assembly **113** is also provided with at least one clamping
20 pad, clamping piston or ribs **121**. The ribs **121** are capable of outward movement for locking the sensor assembly **113** to the borehole wall during measurement by the sensor assembly **113**. In one embodiment, the ribs **121** are hydraulically activated. In the inactivated position of the ribs **121**, the sensor assembly **113** rests on the lower tool joint **139** and is held up against

gravitational pull by the spring 130 that is fixedly attached to the drill pipe section 101. Continued rotation of the drillstring 20 loosely carries the sensor assembly 113 along. In the activated position, the ribs 121 engage the borehole walls and prevent any further movement of the sensor assembly 113. Further
5 rotation of the drillstring 20 does not affect the position of the sensor assembly 113 that remains in a clamped position against the borehole wall. In the clamped position, the sensor assembly 113 is essentially decoupled from rotational and vertical movement of the drillstring 20, enabling measurements, such as NMR measurements from the NMR sensor assembly 113, to be carried
10 out without interference from tool motion and vibration. By special design of the magnet assembly 115, the region of examination is within the formation and no NMR signal is received from the borehole fluid because no NMR resonance condition exists there.

15 [0030] In another embodiment, at least one sensor of the sensor assembly 113 is located in the at least one clamping pad (not shown) to provide a sensor at the borehole wall when the at least one clamping pad is activated and engaged with the borehole wall. In still another embodiment, at least one transmitter (not shown) is located in the at least one clamping pad to provide a transmitter at the
20 borehole wall when the at least one clamping pad is activated and engaged with the borehole wall.

[0031] In typical operation with prior art pulse sequences, the NMR measurement takes between 0.01 to 1 second, during which time the drill pipe

section 101 advances some distance. Once the NMR measurement has been completed, the ribs 121 are retracted, as a result of which the sensor assembly 113 is no longer coupled to the borehole wall. The sensor assembly 113 then drops down until any further downward motion is stopped by the spring 130. In
5 another embodiment, the ribs 121 are actuated electrically, e.g., by a stepper motor. Other methods, such as those using springs, would be known to those versed in the art.

[0032] In a preferred embodiment of the present invention for use in
10 Measurement-while-drilling, the magnet and antenna configuration disclosed in *Slade* (US Patent 6,215,304, the contents of which are fully incorporated herein by reference) is used. The method of the present invention may also be used in wireline applications: when this is done, a preferred magnet and antenna configuration is disclosed in Beard et al. (US Patent 6,348,792) and in
15 *Reiderman* et al. (US Patent Application Ser. No. 09/605,265, now US Patent *****), the contents of which are fully incorporated herein by reference, may be used. It should be noted that other logging tools could also be used with the method of the present invention.

20 [0033] As an alternative to the pulse sequences the sequences used in prior art (CPMG sequences or modified CPMG sequence) the present invention uses stochastic pulses with relatively small tip angles. This greatly reduces the power requirements. A similar approach has been taken in the field of seismic exploration: early exploration methods relied on high power explosive sources

such as dynamite. In seismic exploration, the impulse response of the earth is indicative of changes in acoustic properties of the earth and recent methods have used swept-frequency sources or stochastic pulsing. See, for example, US Patent 4106585 to *Stafford* and US Patent 5305285 to *Neville*. By cross-
5 correlating the received signals with the outgoing signals, the impulse response of the earth is recovered.

[0034] The present invention utilizes a sequence of small spin-flip angles of the order of 0^0 to 5^0 . The phase of these pulses, the amplitude, or both are varied in
10 a random or pseudo-random fashion. Therefore, the excitation pulse sequence looks stochastic or like noise. For this reason, this kind of excitation in NMR is called stochastic or noise excitation.

[0035] In the simplest form of stochastic NMR, the NMR signals are monitored
15 directly during the stochastic excitation. Joined together, these NMR signals would look like noise (see *Paff et al.*). To recover the impulse response corresponding to the NMR response to a single RF pulse such as the Free Induction Decay (FID) or spin-echo signals, the correlation of the NMR system response with the stochastic excitation must be obtained. The difference with
20 the seismic case is that a linear cross-correlation of the received signal with the excitation sequence does not give the full information due to the complex interaction of nuclear spins with the pulses. As discussed below, there are two types of approaches that can be taken. The first relies on a higher order cross-correlation between the received signals and the excitation pulse sequence. The

second approach uses a linear cross-correlation between the received signals and a transformed sequence derived from the excitation pulse sequences. These are discussed below.

5 [0036]The correlation can be done with analog or digital electronics during measurement or may be numerically after the stochastic NMR signal has been sampled with an analog to digital converter . In logging applications, the latter method would normally be used as analog devices that can withstand the harsh downhole conditions are hard to build.

10

[0037]Nonlinear or higher order cross correlation can be used to generate spin echos, equivalent to Hahn echos. These are needed to get information about T_2 relaxation, which, as stated above, is a source of information for determination of formation properties, and different types of fluids. T_1 relaxation can be
15 measured with a saturation recovery method similar to conventional pulsed NMR. The saturation is effected by any stochastic saturation sequence for example that described in *Nilgens et al.* Then, after an evolution time, the partly relaxed nuclear magnetization is detected by stochastic NMR as described above. This measurement is repeated for a variety of evolution time
20 intervals to sample the whole T_1 saturation recovery curve, which would show the various T_1 components of the formation and can be inverted into a T_1 spectrum in the usual ways.

[0038] The invention is comprised of a method of stochastic excitation of formation molecules in NMR detection. One advantage of the invention is that in comparison to that of conventionally shaped pulses, the pulse train has low peak power. There is also the possibility of creating almost arbitrary frequency profiles as described by *Nilgens et al.*

[0039] Turning now to **Fig. 3**, a flow chart for a method of determination of T_2^* using the detection of free induction decay is shown. As is typical with most methods of making NMR measurements, a static magnetic field is applied 301.

10 A random pulse sequence $x'(t)$ is defined. This could be a random series of white noise pulses having small tip angles or it could be a so-called maximum length binary sequence (mlbs).

[0040] At 302, a process called Saturation Pulses with reduced amplitude distribution ("SPREAD") is used to destroy proton magnetization of such protons that would resonate beyond a certain offset from the selected reference frequency. *Nilgens et al* describe various methods in which this may be done. There are two reasons SPREAD or an equivalent is necessary.

20 [0041] Firstly, the (short) RF pulses, as used in stochastic NMR, excite a relatively wide bandwidth of frequencies. Consequently the FIDs also possess the same wide bandwidth of frequencies. Additionally, if the excitation uses small spin flip angles and causes a linear response, the FIDs are as short as the pulses and, even worse, occur during the pulses, i.e., they are not detectable.

SPREAD ensures that the bandwidth of the FIDs is narrower than the bandwidth of the pulses. This increases the length of the FIDs (increases T2*) and the FIDs can now be seen after the RF pulses.

- 5 [0042] If the bandwidth of the RF pulses is greater than the resonance bandwidth of the sample (sample of limited volume in relatively small gradient), then SPREAD is not needed, but this situation does not occur in downhole NMR as we have always gradients and a sample of large volume. A gradient is always present in multi-frequency logging tools and even for single
10 frequency tools with the opposed magnet configuration, a small gradient remains in the region of examination.

- [0043] Secondly, together with the known distribution of the static magnetic field intensity B_0 , SPREAD can also be used to define a region of NMR
15 sensitivity. This is important to ensure NMR signals are only received from a region far enough from the borehole. This reason for application of SPREAD does not apply to the wireline tools disclosed in *Beard* et al and in *Reiderman* et al '265 application.

- 20 [0044] The applied pulse sequence 303 is given by

$$x(t) = rx'(t) \quad (2)$$

where r is determined as indicated below. The output $y(t)$ of the nuclear spin system is measured 307 and the root-mean-square (RMS) value of $y(t)$ is determined 307. If necessary, the value of r is incremented 309 until an adequate signal level is obtained. The FID $z(t)$ of the system is determined

5 using a linear cross-correlation 311 between $y(t)$ and $x'(t)$. As discussed in *Blümich* (1987), $y(t)$ is cross-correlated with $x'(t-\Phi)$ giving the cross-correlation function $z(\Phi)$ which corresponds to the FID. The FID is then evaluated using prior art methods to give a distribution of T_2^* .

10 [0045] In a preferred embodiment of the invention, the pulse sequence $x'(t)$ is derived from a linear shift register with feedback loops as described by *Ziessow and Blümich* (1974) so that a maximum length binary sequence (mlbs) results. Cyclic shift of such sequences produces the rows of a sequency-ordered Hadamard matrix. A Hadamard matrix is a square matrix containing only 1s

15 and -1s such that when any two columns or rows are placed side by side, half the adjacent cells are the same sign and half the other (excepting from the count an L -shaped "half-frame" bordering the matrix on two sides which is composed entirely of 1s). When viewed as pavements, cells with 1s are colored black and those with -1s are colored white. Therefore, the $n \times n$ Hadamard matrix H_n must

20 have $n(n-1)/2$ white squares (-1s) and $n(n+1)/2$ black squares (1s). An example of a Hadamard matrix is shown in **Fig. 3a**. When the pulse sequence $x'(t)$ is derived from a mlbs, then cross-correlation between $y(t)$ and $x'(t)$ may be equivalently derived as a Hadamard transform of $y(t)$.

- [0046] Turning now to **Fig. 4**, a method of determination of T_2 using a non-linear cross-correlation is shown. The method starts with application of the static magnetic field **353**. Following this, a selective saturation pulse sequence such as SPREAD is applied **355**. A pulse train $x(t)$ is then applied **357**. This pulse train is a random or pseudo random sequence that may be one of (i) equal amplitude, random phase pulses, (ii) random amplitude, equal phase pulses, (iii) random amplitude, random phase pulses, and, (iv) a mlbs. Following the application of the pulse train $x(t)$, the response $y(t)$ is obtained **359**.
- 10 [0047] A third order cross-correlation between $y(t)$, $x(t - t_E/2 - \tau, -\Phi)$, $x(t - t_E/2 - \tau)$ and $x(t - t_E/2)$ is determined **361**, where τ is a short time lag corresponding to a few, for example three, periods of the excitation pulses. Alternatively the echo itself can be derived by cross-correlation of the transverse magnetization response with $x(t - t_E/2 - \tau, -\Phi)$, $x(t - \tau, -\Phi)$ and $x(t - \Phi)$. This produces a spin echo
- 15 at time $\Phi = t_E/2$.
- This simulates a spin echo at a time $\Phi = t_E/2$ for $\tau \ll T_2$. This is discussed in *Paff et al* (1992). Next, the value of t_E is incremented **363** to obtain the echo envelope **361**. After a sufficient range of t_E values has been covered, an inversion of the echo envelope is carried **365** out to obtain a distribution for T_2 .
- 20 [0048] Those versed in the art would recognize that performing the higher order cross-correlation is computationally time consuming. In an alternate embodiment of the invention, only linear cross-correlations are required: this

comes at the expense of an increased acquisition time. However, in applications such as determination of clay-bound water where only the early part of an echo train is needed, the time savings can be considerable. This is discussed next with reference to **Fig. 5**.

5

[0049] As in the methods discussed in **Fig. 4**, the process starts with the application of the static magnetic field **401** and a SPREAD sequence **403**. The pulses that are applied $x(t)$ **405** are derived from a sequence $x'(t)$ as

$$x(t) = r \left[x'(t) + r_E x'(t - t_E / 2) \right] \quad (3)$$

where $x'(t)$ is selected from the group consisting of (i) equal amplitude, random phase pulses, (ii) random amplitude, equal phase pulses, (iii) random amplitude, random phase pulses, and, (iv) mlbs.

15

[0050] The response $y(t)$ is recorded **409** and a linear cross-correlation between $y(t)$ and $x'(t)$ gives a FID sample and an echo at t_E **409**. The process is repeated starting at **403** for additional values of r and r_E to optimize the echo amplitudes.

The additional values of r and r_E are not necessary if their values can be chosen

20

from experience. Once r and r_E have been determined, the value of t_E is incremented **411** until a sufficient number of echos has been obtained. Once a good sequence of signals is obtained, T_2 inversion is carried out **415** using prior art methods.

[0051] Turning now to **Fig. 6**, an alternate embodiment of the invention of **Fig. 5** is discussed wherein the processing requirements are reduced by having multiple echos generated in one step. As before, the static magnetic field is applied **451** and selective saturation is applied **453**. The pulse sequence $x(t)$ that is applied **455** now includes the ability to generate multiple echos. The pulse sequence is given by

$$x(t) = r \left[x'(t) + r_E \sum_{n=1}^{n_{\max}} x' \left(t - (n-1/2)t_E \right) \right] \quad (4)$$

and uses known values of r and r_E . Since the excitation pulse sequence includes a plurality of time shifted versions of the sequence $x'(t)$, multiple echos are generated. As before, $x'(t)$ is selected from the group consisting of (i) equal amplitude, random phase pulses, (ii) random amplitude, equal phase pulses, (iii) random amplitude, random phase pulses, and, (iv) mlbs. A linear cross-correlation between the response $y(t)$ **457** and $xN(t)$ gives the FID and multiple echos **459**. These are then inverted **461** to get the T_2 distribution.

[0052] Turning now to **Fig. 7**, a method of determining T_1 using varying saturation is discussed. A static magnetic field is applied **501** and a pulse sequence $x(t) = r x'(t)$ is defined **503**, where $x'(t)$ is selected from the group consisting of (i) equal amplitude, random phase pulses, (ii) random amplitude, equal phase pulses, (iii) random amplitude, random phase pulses, and, (iv) mlbs. A selective saturation is performed using SPREAD **505**. The pulse sequence

$x(t)$ is applied **507** and the response signal $y(t)$ is obtained **509**. The RMS value of $y(t)$ is obtained **511**. This gives a single point on the saturation curve. The scale factor r is incremented **513** and additional pulse sequences are defined **505** to obtain additional points on the saturation curve. Evaluation of the curve of the RMS value of $y(t)$ as a function of r gives information on T_1 , by comparing the experimental curve with simulated saturating curves. This is discussed in *Blümich* (1987).

[0053] The foregoing description has been limited to specific embodiments of this invention. It will be apparent, however, that variations and modifications may be made to the disclosed embodiments, with the attainment of some or all of the advantages of the invention. It is the object of the appended claims to cover all such variations and modifications as come within the true spirit and scope of the invention.

CLAIMS

- 1 1. A method of determining a parameter of a region of interest of an earth
2 formation comprising:
3 (a) using a magnet on a logging tool conveyed in a borehole in said
4 earth formation for producing a static magnetic field in the
5 region of interest and aligning nuclear spins within said region of
6 interest;
7 (b) modulating a radio frequency (RF) output of a transmitting
8 antenna with an applied pulse sequence derived from a primary
9 pulse sequence of small flip angle pulses and altering said
10 nuclear spins, said primary pulse sequence comprising a random
11 or pseudo-random sequence;
12 (c) using a receiving antenna for receiving signals indicative of said
13 altered nuclear spins;
14 (d) using a processor for determining from said received signals said
15 parameter of interest.
16
- 1 2. The method of claim 1 further comprising conveying said logging tool
2 in said borehole on one of (i) a wireline, and, (ii) a drilling tubular.
3
- 1 3. The method of claim 1 wherein said static magnetic field has a gradient
2 in said region of interest.

1 4. The method of claim 1 wherein said gradient is substantially equal to
2 zero.

3

1 5. The method of claim 1 wherein said parameter of interest comprises an
2 apparent transverse relaxation time T_2^* .

3

1 6. The method of claim 5 further comprising applying a SPREAD
2 sequence prior to applying said applied pulse sequence, said SPREAD sequence
3 substantially eliminating longitudinal magnetization outside a selected portion
4 of said region of interest

5

1 7. The method of claim 5 wherein said primary pulse sequence further
2 comprises a maximum length binary sequence, and wherein using said receiving
3 antenna further comprises receiving said signals during transmission of the
4 applied pulse sequence.

5

1 8. The method of claim 7 wherein determining said parameter of interest
2 further comprises performing a cross-correlation between said received signals
3 and said primary pulse sequence, giving a free induction decay.

4

1 9. The method of claim 7 wherein said applied pulse sequence further
2 comprises a scaled version of the primary sequence.

1 10. The method of claim 8 wherein determining said apparent transverse
2 relaxation time further comprises inverting said free induction decay.

3

1 11. The method of claim 1 wherein said parameter of interest comprises a
2 transverse relaxation time T_2 .

3

1 12. The method of claim 11 further comprising applying a SPREAD
2 sequence prior to applying said applied pulse sequence, said SPREAD sequence
3 substantially eliminating longitudinal magnetization outside a selected portion
4 of said region of interest.

5

1 13. The method of claim 12 wherein said primary pulse sequence is one of
2 (i) an equal amplitude random phase sequence, (ii) a random amplitude equal
3 phase pulse sequence, (iii) a random amplitude random phase pulse sequence,
4 and, (iv) a maximum length binary sequence.

5

1 14. The method of claim 13 wherein using said receiving antenna further
2 comprises receiving said signals during transmission of the applied pulse
3 sequence

4

1 15. The method of claim 14 further comprising determining a third order
2 cross-correlation between the received signal at a time t , the applied pulse signal
3 at a time $t - t_E - \epsilon$, the applied pulse signal at a time $t - t_E/2 - \epsilon$, and the applied

4 pulse signal at a time $t - t_E/2$, wherein determining said third order cross-
5 correlation yields the echo envelope as a function of t_E .

6

1 16. The method of claim 14 further comprising repeating step 14 for at least
2 one additional time and obtaining multiple echos.

3

1 17. The method of claim 16 further comprising inverting said multiple echos
2 and obtaining a distribution of values of T_2 therefrom.

3

1 18. The method of claim 13 wherein the applied pulse sequence $x(t)$ may be
2 derived from the primary pulse sequence $xN(t)$ by a relation of the form

3
$$x(t) = r[xN(t) + r_E xN(t - t_E/2)]$$

4 where r and r_E are scale factors.

5

1 19. The method of claim 18 further comprising determining a linear cross-
2 correlation between the received signal and the applied pulse sequence.

3

1 20. The method of claim 1 wherein said parameter of interest comprises a
2 longitudinal relaxation time T_1 and wherein the applied pulse sequence is a
3 scaled version of said primary pulse sequence.

4

5 21. The method of claim 20 wherein said primary pulse sequence is one of
6 (i) an equal amplitude random phase sequence, (ii) a random amplitude equal

7 phase pulse sequence, (iii) a random amplitude random phase pulse sequence,
8 and, (iv) a maximum length binary sequence
9

1 22. The method of claim 21 wherein determining said longitudinal
2 relaxation time T_1 further comprises evaluating an rms value of said received
3 signals as a function of said scale factor.
4

1 23. An apparatus for determining a parameter of a region of interest of an
2 earth formation comprising:

- 3 (a) a logging tool conveyed in a borehole in said earth formation;
- 4 (b) a magnet on said logging tool for producing a static magnetic
5 field in the region of interest and aligning nuclear spins within
6 said region of interest;
- 7 (c) a random-number generator for generating a random or a
8 pseudo-random primary pulse sequence;
- 9 (d) a transmitting antenna on said logging tool for producing a radio
10 frequency (RF) magnetic field for altering said nuclear spins,
11 said transmitting antenna being modulated by an applied pulse
12 sequence derived from said primary pulse sequence;
- 13 (e) a receiving antenna on said logging tool for receiving signals
14 indicative of said altered nuclear spins; and
- 15 (f) a processor for determining from said received signals said
16 parameter of interest.

1 24. The apparatus of claim 23 wherein said logging tool is conveyed into the
2 borehole on one of (i) a wireline, and, (ii) a drilling tubular.

3

1 25. The apparatus of claim 23 wherein said processor further uses at least
2 one of (i) the primary pulse sequence, and, (ii) the applied pulse sequence for
3 determining the parameter of interest.

4

1 26. The apparatus of claim 23 wherein said parameter of interest is selected
2 from the group consisting of (i) a longitudinal relaxation time T_1 , (ii) a
3 transverse relaxation time T_2 , and, (iii) an apparent transverse relaxation time
4 T_2^* .

5

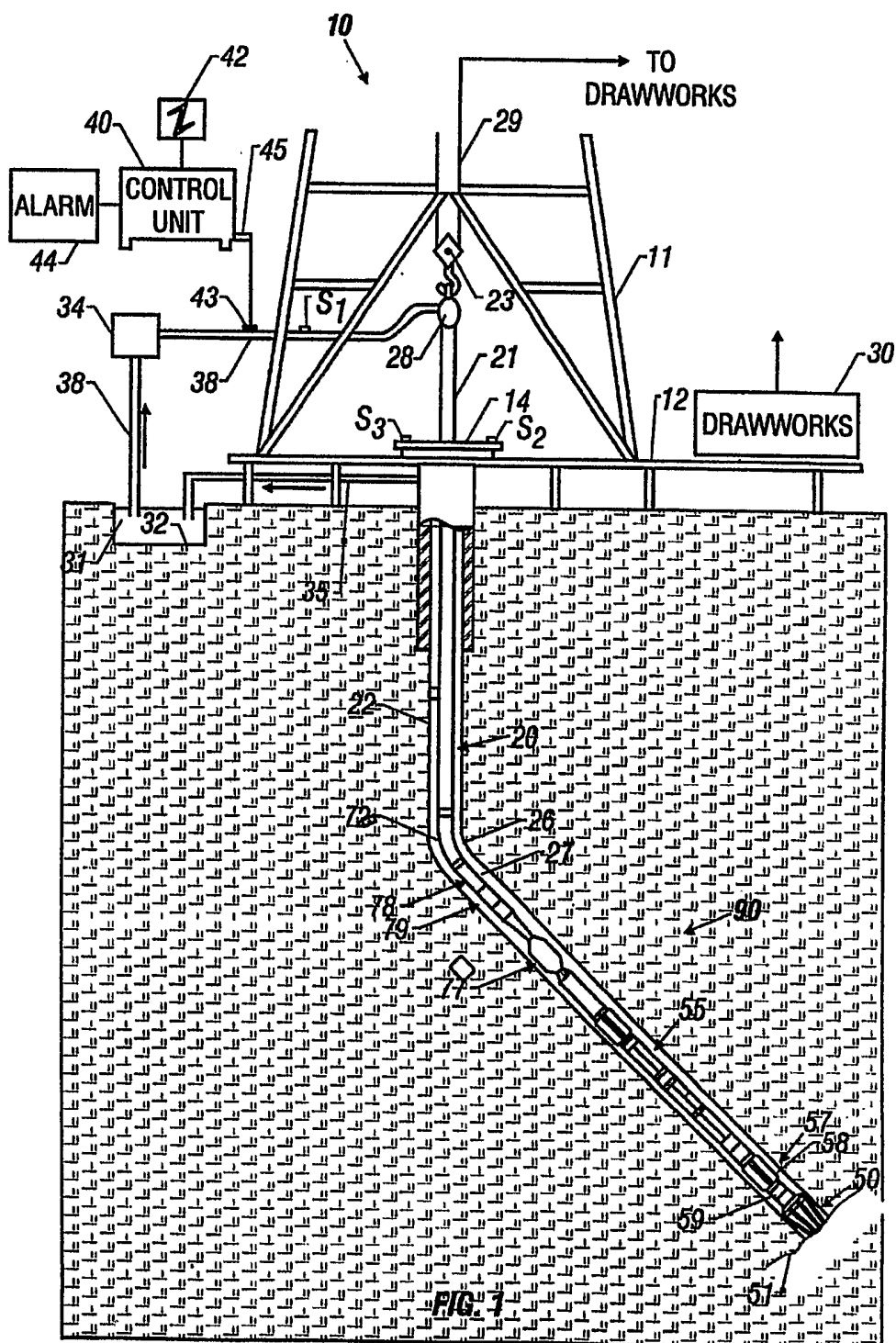
1 27. The apparatus of claim 23 wherein said transmitting antenna and said
2 receiving antenna are the same.

3

1 28. The apparatus of claim 23 wherein said processor is located at one of (i)
2 the logging tool, and, (ii) a surface location.

3

29. The apparatus of claim 23 wherein said processor further performs one
of (i) a linear cross-correlation, and, (ii) a nonlinear cross correlation, for
determining said parameter of interest.



PRIOR ART

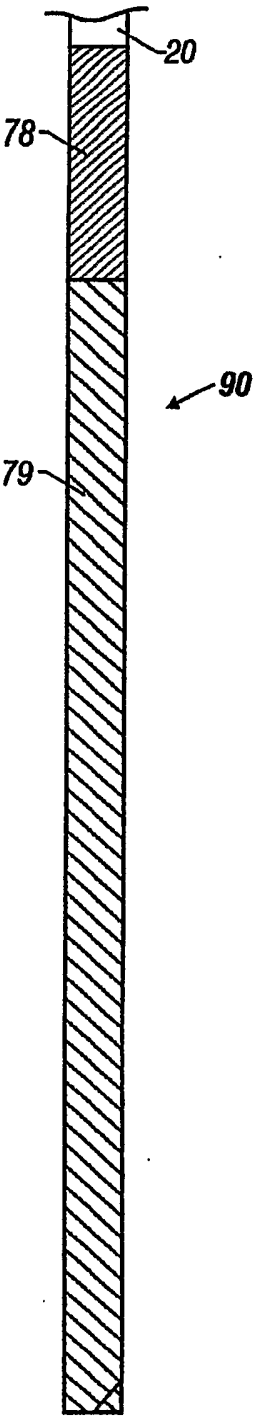


FIG. 2A

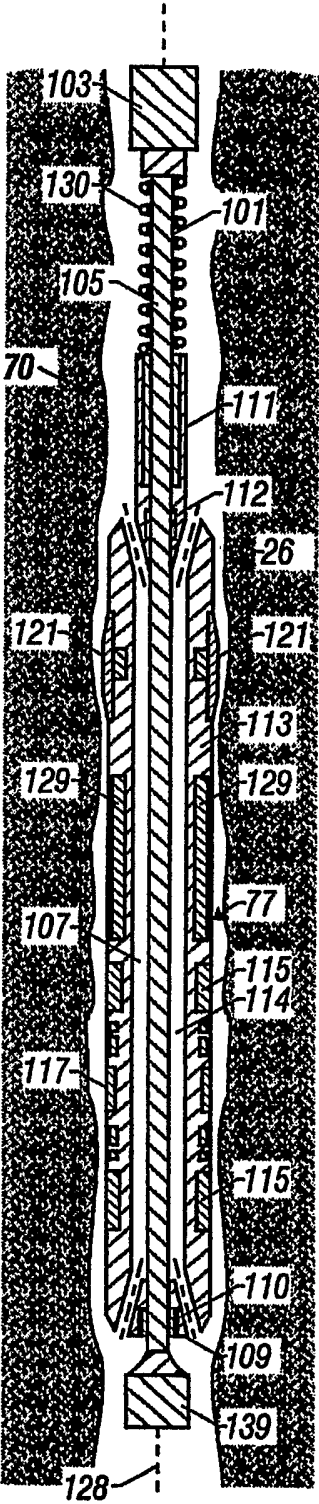


FIG. 2B

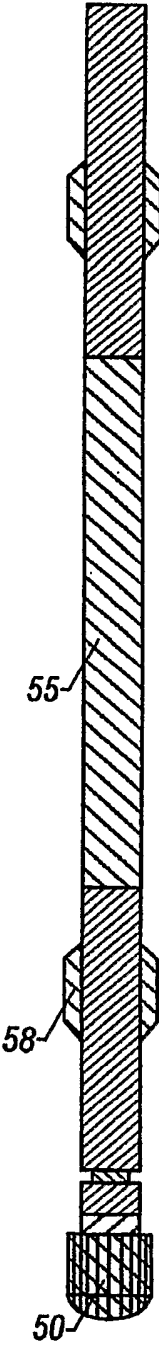


FIG. 2C

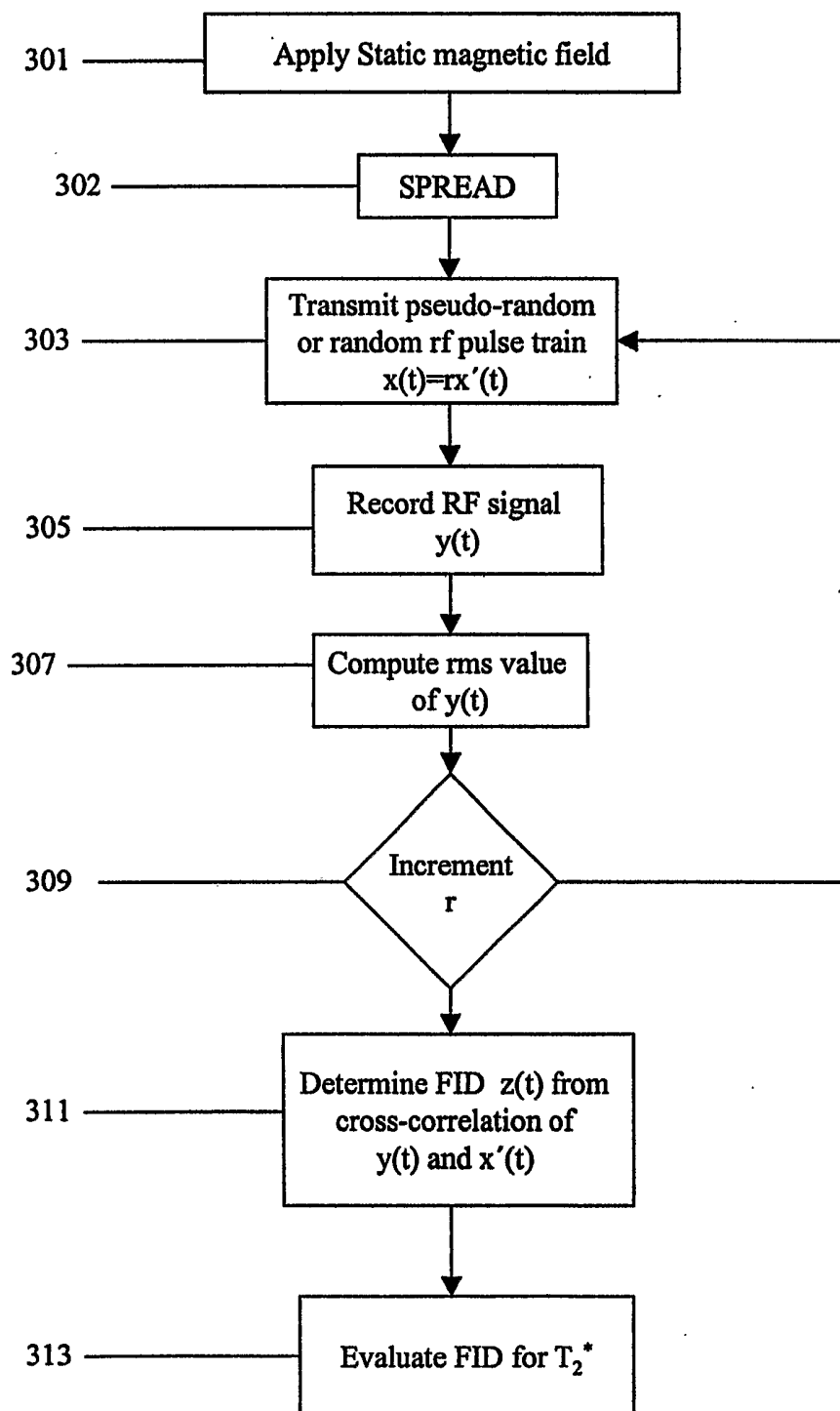


Figure 3

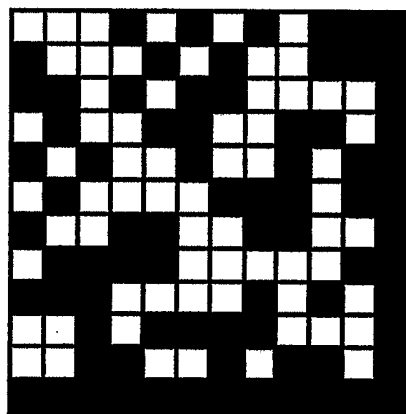


Figure 3a

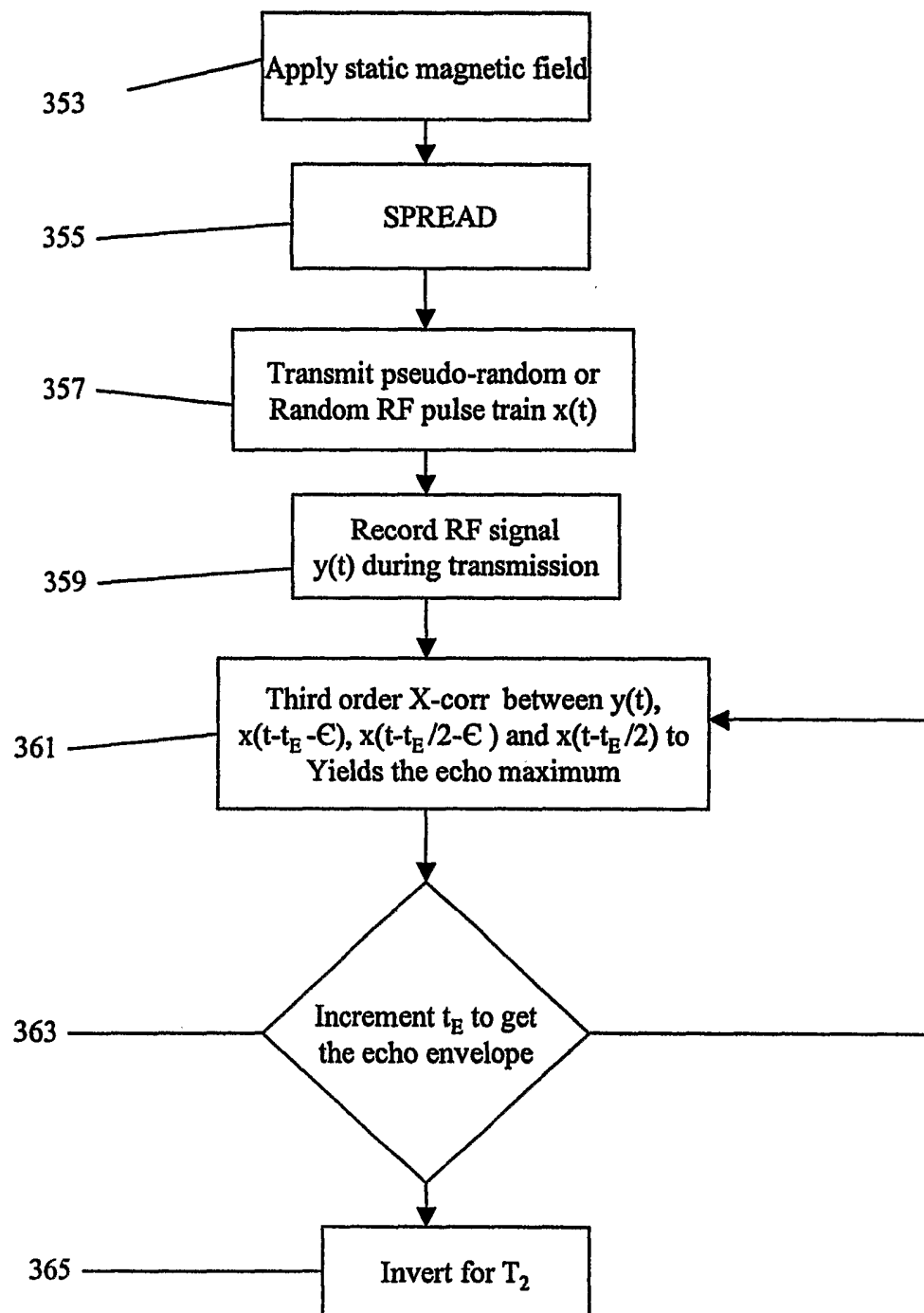


Figure 4

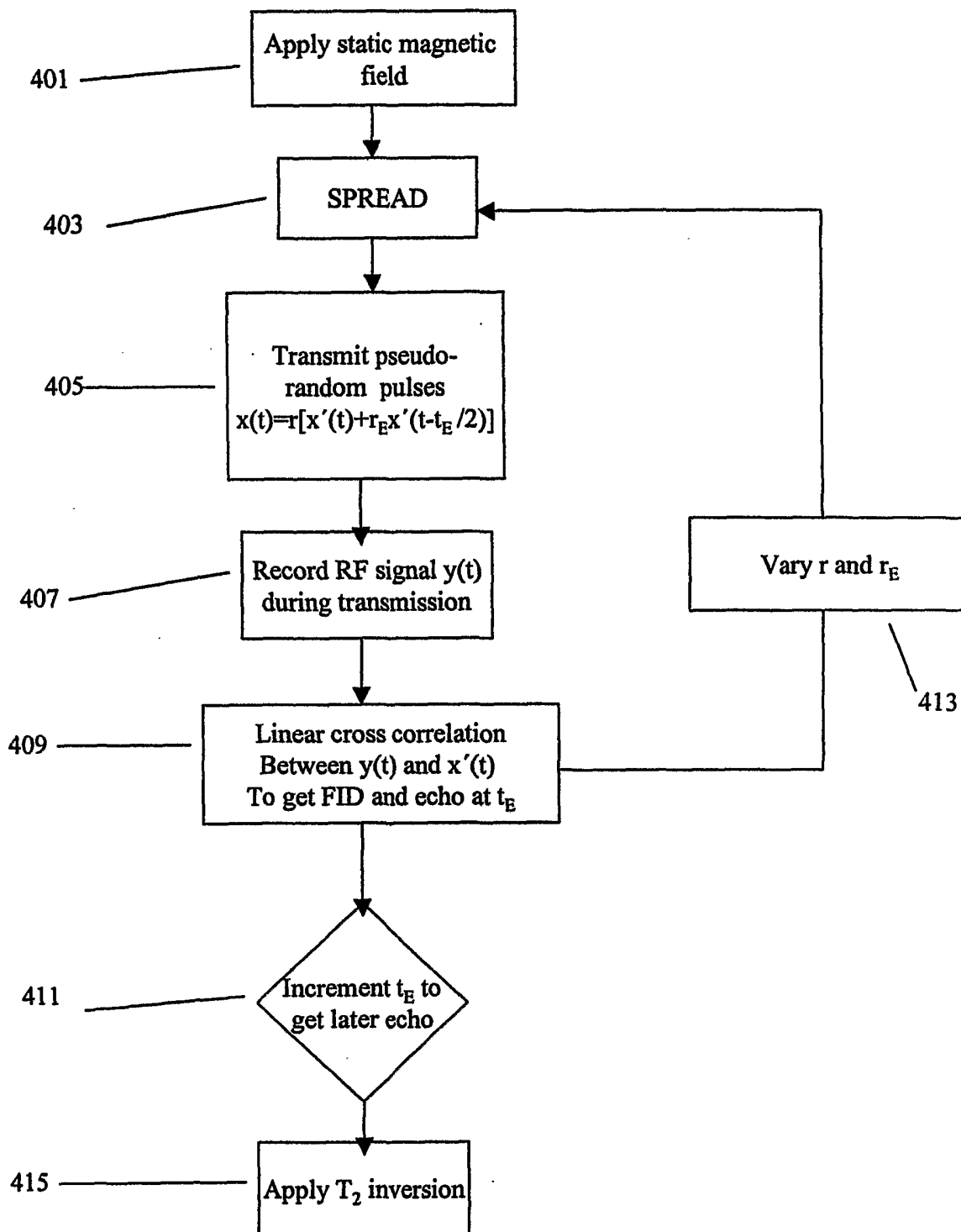


Figure 5

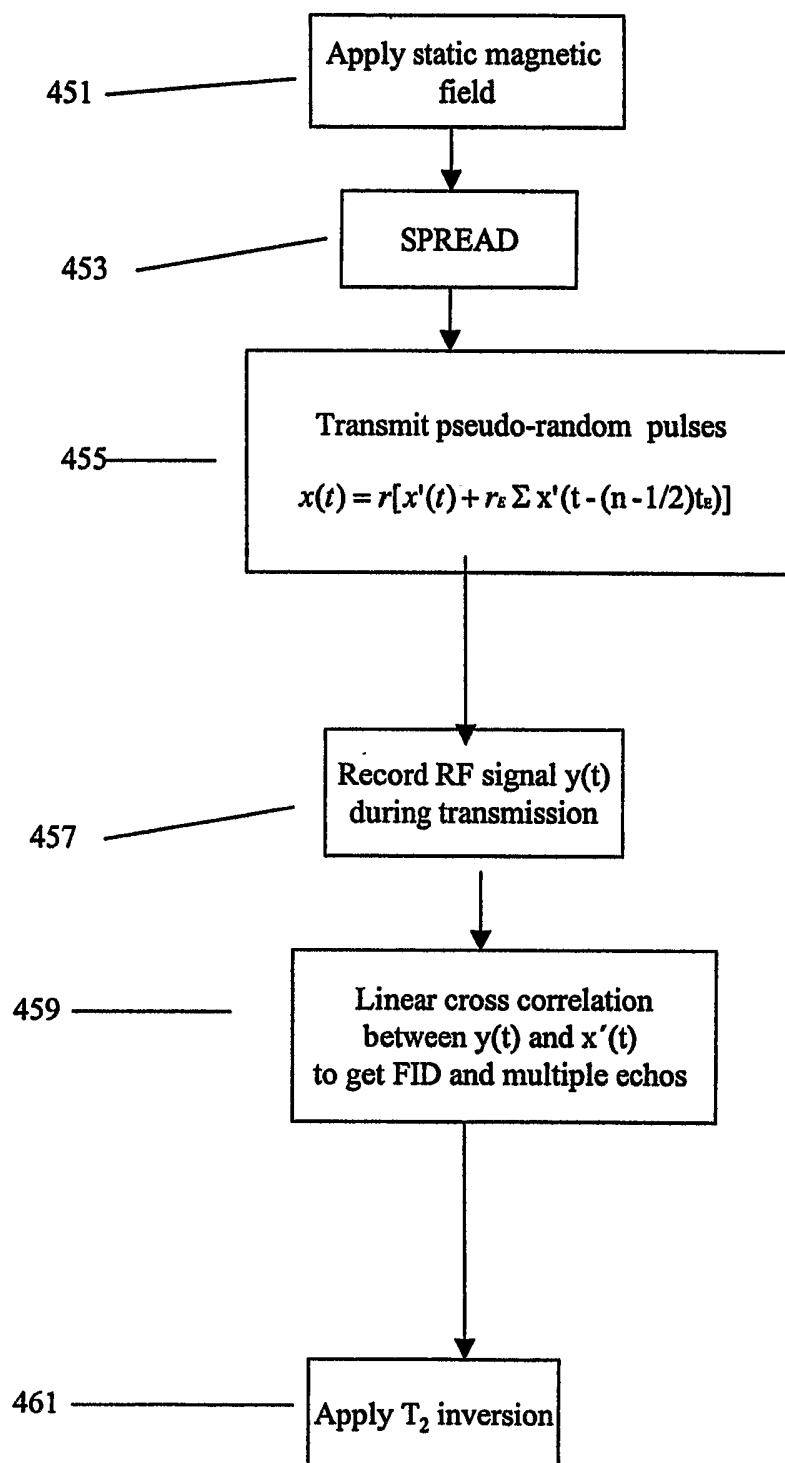


Figure 6

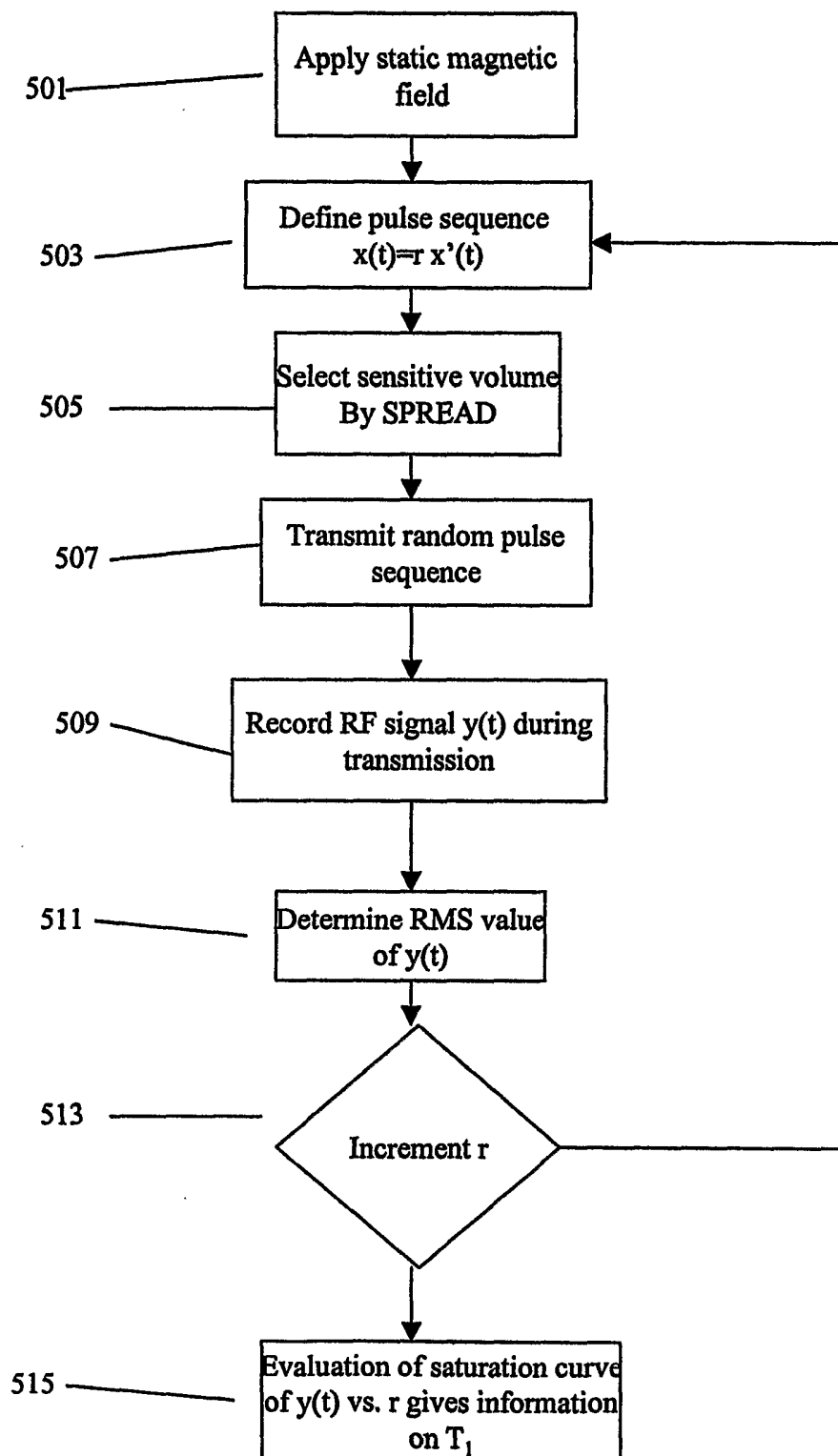


Figure 7

INTERNATIONAL SEARCH REPORT

Internatio Application No

PCT/US 03/25964

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G01V3/32

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G01V

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, INSPEC, COMPENDEX, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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Y		4, 6, 7, 10, 12-14
A	----- -/--	5

☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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Date of the actual completion of the international search

9 December 2003

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

Internatio Application No
PCT/US 03/25964

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
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A		2
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