



(86) Date de dépôt PCT/PCT Filing Date: 1998/11/05

(87) Date publication PCT/PCT Publication Date: 1999/05/27

(45) Date de délivrance/Issue Date: 2004/09/21

(85) Entrée phase nationale/National Entry: 2000/05/17

(86) N° demande PCT/PCT Application No.: EP 1998/007055

(87) N° publication PCT/PCT Publication No.: 1999/026088

(30) Priorité/Priority: 1997/11/17 (97120113.2) EP

(51) Cl.Int.⁶/Int.Cl.⁶ G02B 1/10, C09D 183/04

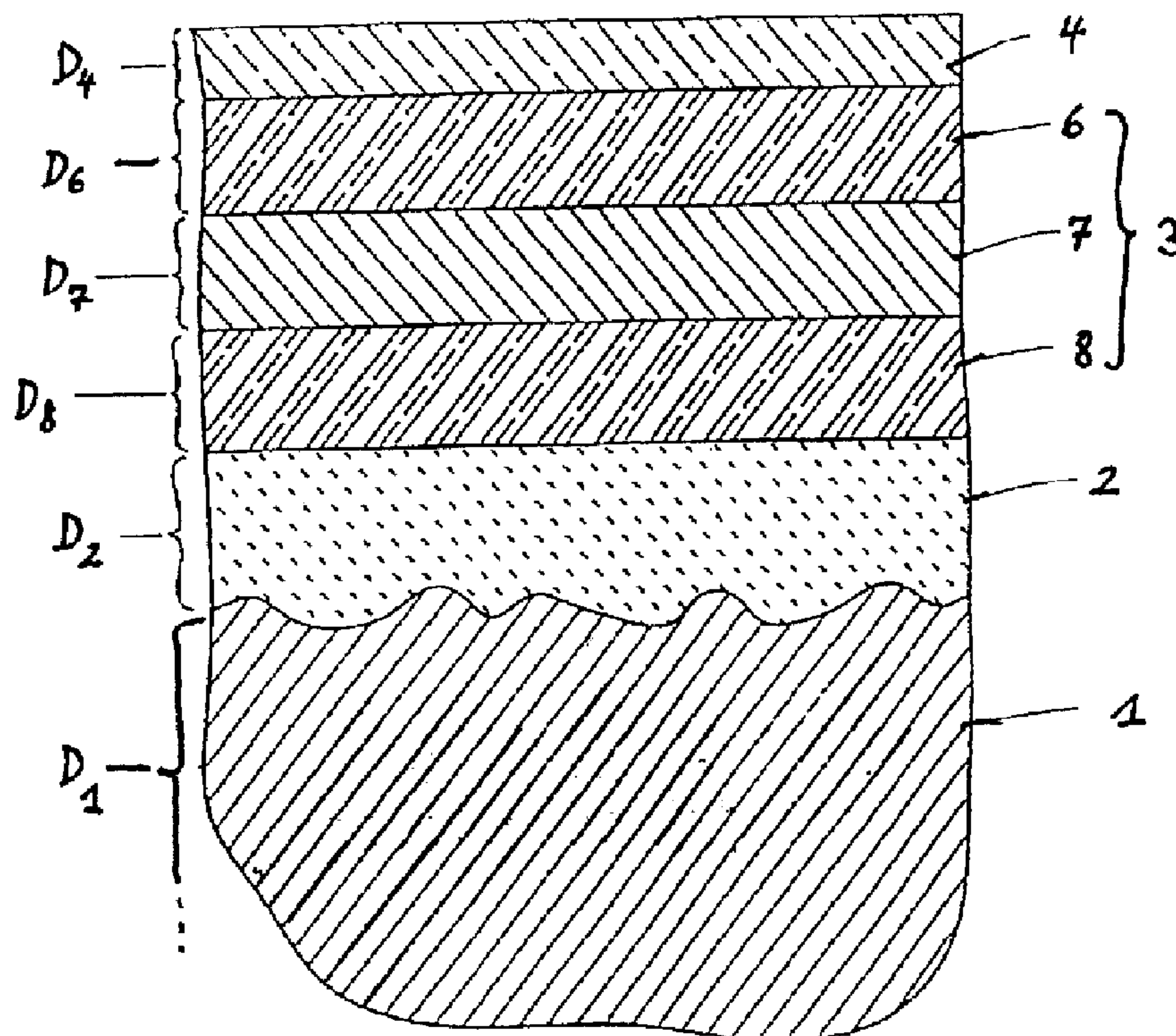
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(54) Titre : **MATERIAU COMPOSITE DESTINE NOTAMMENT A DES REFLECTEURS**

(54) Title: **COMPOSITE MATERIAL, ESPECIALLY FOR REFLECTORS**



(57) **Abrégé/Abstract:**

The present invention relates to a composite material, in particular for reflectors, having a metallic support (1) in strip form, an intermediate layer and having a multilayer optical system (3) which is applied to the intermediate layer (2). A non-metallic protective layer (4), which consists of a low-absorption material and has a thickness (D_4) of from 5 to 20 nm, preferably from 5 to 10 nm, is applied to the multilayer optical system (3).

Composite material, in particular for reflectors

The present invention relates to a composite material, in particular for reflectors, having a metallic support (1) in strip form, an intermediate layer and having a multilayer optical system (3) which is applied to the intermediate layer (2). A non-metallic protective layer (4), which consists of a low-absorption material and has a thickness (D_4) of from 5 to 20 nm, preferably from 5 to 10 nm, is applied to the multilayer optical system (3).

Description

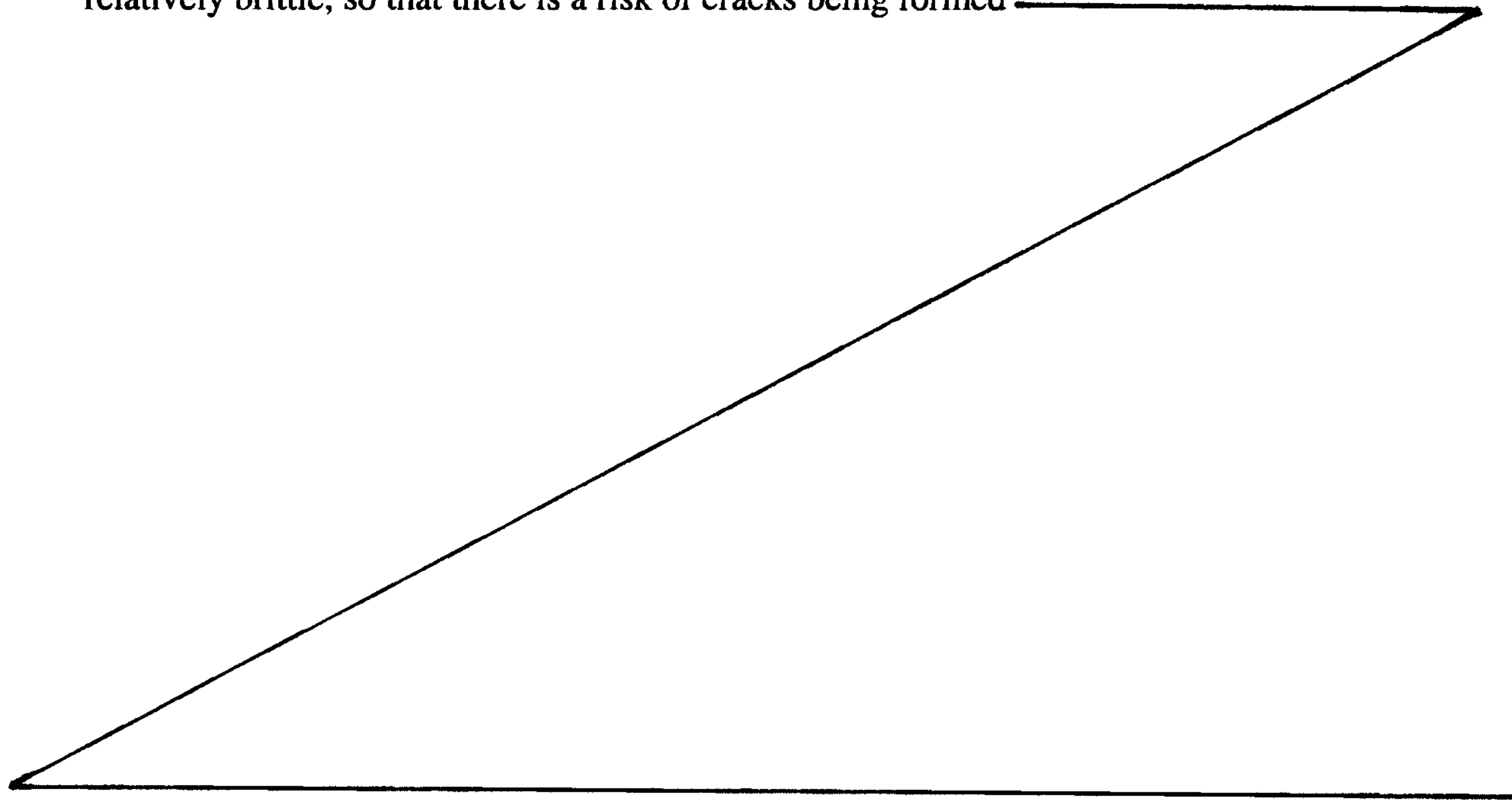
The present invention relates to a composite material, in particular for reflectors, having a
5 metallic support in strip form, an intermediate layer and having a multilayer optical system which is applied to the intermediate layer.

To characterize the reflective properties of a composite material of this nature, the spectral
10 coefficient of the total reflection and that of the diffuse reflection are measured (DIN 5036). Different demands are imposed on the optical properties of reflectors. In many cases, the aim is to have a composite material with a high total reflectivity, i.e.
15 with low reflection losses. If, in addition, a mirror nature, i.e. a low scattering of the light at the reflector surface or a low level of diffuse reflection, is required, the production of such a composite material involves a very high level of outlay in
20 production engineering terms. In some cases, a higher level of diffuse reflection, and in certain circumstances even an absorptive behaviour with regard to the total reflectivity, is also desired. In some special applications, the electromagnetic radiation
25 wavelength which is to be reflected may lie in the UV or in the IR range.

The base material used for reflectors with a high total reflectivity and a low diffuse component, is generally rolled aluminium of a minimum purity of
30 99.8%, for which, since the crude aluminium has a sensitive surface, an intermediate layer has to be applied in order to protect against mechanical and chemical influences and thus maintain its suitability for use. Such a protective intermediate layer is formed
35 in a wet-chemical process which is referred to overall as anodizing and comprises an electrobrightening treatment and an anodic oxidation. By changing the purity and/or the roughness depth, it is possible to influence the level of total reflection, while the

level of diffuse reflection can be influenced by making controlled changes to the rolled structure. In the wavelength range of visible light (380 to 780 nm), the total reflection of composite materials of this nature is from 83% to 87%. Considerable process engineering outlay, primarily a high outlay on rolling technology, as well as a high level of purity of the material used, are required in order to achieve a low level of diffuse reflection, in particular of below 4%, resulting in high costs. Despite these drawbacks, this type of semi-finished product in strip form has become established throughout the world as a standard product for the lighting industry.

Furthermore, it is known, when using less high-grade aluminium support material in strip form, to apply to the support a layer of eloxal which consists of Al_2O_3 in a thickness of approx. 1 to $3\mu\text{m}$ and is then applied to a multiplayer optical system. The reduced-thickness eloxal layer allows the surface to be sufficiently rough and hard and to be free from defects. A highly reflective high-purity aluminium layer is deposited on this eloxal layer. This high-purity aluminium layer is optically dense, about 50 to 80 nm thick and has a total reflection of more than 91% in the visible light range. Yet more layers which increase the reflection can be applied to this reflective layer. For example, a subsequent continuous strip coating is known which has improved optical efficiency of such aluminium strips up to a total light reflectivity of approx. 95%. However, the diffuses light reflectivity of material with a mirror nature is improved only to an insignificant extent. The optically active surface has a good mechanical load-bearing capacity and sufficient chemical resistance for use as a reflector material. However, the intermediate eloxal layer which serves as a smoothing layer is relatively brittle, so that there is a risk of cracks being formed



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in the event of extreme mechanical deformation processes.

A significant drawback of the two known optically active composite materials described above is that they are limited to aluminium as the support material. This entails complex, sometimes environmentally disadvantageous process steps during production, such as wet-chemical brightening, anodizing and, if appropriate, the vacuum coating or the need to use high-purity, specially rolled and therefore expensive starting material.

US-A-5,527,562 has disclosed, as the intermediate layer, a levelling application to an aluminium support which serves as a substrate for a subsequent vacuum coating with an optically reflective layer system. This application is of an organic silicon sol which is applied to suitably pretreated aluminium. The special sol is intended to bring about good levelling of the aluminium-strip surface and high total reflectivities after the coating in vacuo by sputtering of Al, SiO₂, TiO₂. A drawback of this arrangement is that the use of a very specific formulation for the sol layer necessitates a high process engineering outlay.

Furthermore, it is known that curved, rigid reflector bodies (e.g. for headlights) are provided with a levelling coating layer, to which a single-layer reflective application of aluminium is then applied in vacuo, and this in turn is provided with a protective layer. A drawback of this is that the total reflectivity does not exceed that of the aluminium layer, i.e. approx. 90%, and that the resultant surface does not exhibit sufficient mechanical strength. In particular, the surface is so unable to withstand loads imposed by forming operations that under standard industrial conditions further processing would be impossible.

The present invention is based on the object of providing a composite material, in particular for reflectors, of the type described in the introduction,

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with which it is possible, in a less complex and therefore less expensive manner, as required, to achieve any desired total reflectivity, in particular even values of over 95%, and any desired level of
5 diffuse reflection, in particular even values of below 4% (according to DIN 5036) and which has a high mechanical strength and chemical resistance. The composite material should not be limited to a support made from aluminium and should be highly deformable.

10 According to the invention, this is achieved by the fact that a non-metallic protective layer, which consists of a low-absorption material and has a thickness of from 5 to 20 nm, preferably from 5 to 10 nm, is applied to the multilayer optical system.

15 The protective layer may preferably be a sputtered layer, in particular a layer produced by reactive sputtering, a CVD or PECVD layer or a layer which is produced by vaporization, in particular by electron bombardment or from thermal sources. The
20 protective layer may consist predominantly of a material with a low refractive index, such as for example SiO_2 .

The invention opens up entirely new technical and economic possibilities relating to the production
25 of composite reflector materials. In particular, depending on requirements, it is possible, without reducing the mechanical strength of the composite material, to apply an eloxal layer or, in particular, a coating layer with a thickness which is adapted to the
30 roughness of the support, which may characteristically lie within the range from about 2 to 20 μm , for the intermediate layer. The coating material may be a polycondensate produced on the basis of one or more monomers, a polyadduct or a polymer produced in
35 particular by free-radical polymerization. Irrespective of the basis on which the coating-material mixture is produced, it is possible, by suitably selecting the mixture and/or the application process and/or the curing parameters, to set slight or, as far as

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possible, complete levelling of the support surface, resulting in a planar surface with a minimal roughness depth or a desired undulating or rough structure. Thus, with regard to its influence on the reflectivity, the coating material has the same importance as the rolled surfaces of the known aluminium strips.

In this case, the protective layer plays the major role. According to the current state of scientific knowledge in the field of optical physics, each further layer which is applied to a multilayer optical system comprising, for example, a metallic reflective layer and two interference layers positioned above it has a considerable adverse effect on the optical characteristics of the layer system. Surprisingly, according to the invention, it has proven possible - in contrast to this generally recognized scientific knowledge - to significantly increase not only the mechanical load-bearing capacity values (DIN 58165, part 5), but also to increase the reflectivity by approx. 1% point.

A further important aspect of the invention is the possibility of using an inexpensive metallic support which may consist of simple industrially rolled aluminium. However, it is also possible, according to the invention, to use other metallic support materials, such as magnesium, copper, titanium, molybdenum, tantalum or steel, such as for example stainless steel, or alloys containing these substances, such as for example brass, thus making it possible, on the one hand, to improve the mechanical properties of the composite material so as to achieve higher strength values, but, on the other hand, also allowing materials which are less expensive than aluminium to be used. The surface roughness of these materials is no longer important, since the surface structure of the composite material according to the invention is determined primarily by the intermediate layer, and the thickness of the intermediate layer can be adapted to the roughness of the support material.

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Advantageously, the entire process of producing the composite material according to the invention can take place in a continuous process: the multilayer optical system and the protective layer can be applied to the intermediate layer using the continuous vacuum strip-coating process, while for the intermediate layer it is possible in particular to use formulations which can be applied using the coil-coating process, dried and, if appropriate, structured. These formulations are in particular stoving enamels with a toughness which can be preset by means of organic or inorganic solvents and which can be cured at temperatures of up to about 250°C and are based on acrylic resins, epoxy resins, phenolic resins, melamin resins, urea resins or polyurethane resins. The curing takes place predominantly as a result of a crosslinking reaction due to activation of the double bonds which are present in the monomers. The enamel layers formed are distinguished by a high scratch resistance, extensibility and insensitivity to corrosive influences.

The coating materials used for the structure-forming layer should predominantly be those which exhibit such flexural adhesion to the support that there is no delamination of the intermediate layer when a support with a material thickness of 0.4 mm is bent around a mandrel with a diameter of 2 mm and an adhesive strip of type Scotch 670 CFM, produced by 3 M, which has been previously stuck on and is also bent around the mandrel is pulled off.

Furthermore, it is advantageous, with regard to a vacuum coating which takes place after the application of the intermediate layer, to use a coating material which has a glass transition temperature of over 100°C and a gas release rate of less than $1 \cdot 10^{-4}$ mbar $1 \text{ s}^{-1} \text{ m}^{-2}$.

Further advantageous embodiments of the invention are given in the subclaims and in the following detailed description. The invention is

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explained in more detail with reference to a plurality of exemplary embodiments which are illustrated in the appended drawing, in which:

5 Fig. 1 shows a diagrammatic sectional illustration through a composite material according to the invention, which is characteristic of the first three exemplary embodiments;

10 Fig. 2 shows a diagrammatic sectional illustration through a composite material according to the invention, which is characteristic of the fourth exemplary embodiment.

15 Throughout the various figures of the drawing, identical parts are always provided with the same reference numerals, so that generally they are also only described once in each case.

20 In all the exemplary embodiments, a composite material according to the invention, in particular for reflectors, comprises a metallic support 1 which is in strip form and in particular is deformable, an intermediate layer 2 which is suitable for less complex adjustment of a surface structure which is the decisive factor in terms of the reflection properties, a multilayer optical system 3 which is applied to the intermediate layer 2, and a non-metallic protective layer 4 which is applied to the multilayer optical system 3 and comprises a low-absorption material. The intermediate layer 2, which is made from a coating material, is applied in a continuous process.

30 The support 1 in strip form may consist of aluminium, magnesium, copper, titanium, molybdenum, tantalum or steel, such as for example stainless steel, or of alloys containing these substances, such as for example brass.

35 In particular, the individual layers may be dimensioned in such a way that the composite material according to the invention is formed as a coil with a width of up to 1600 mm and a thickness of approximately 0.1 to 1.5 mm. In particular, the support 1 may preferably have a thickness D_1 of about 0.1 to 0.7 mm.

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As shown by way of example in the fourth exemplary embodiment (Fig. 2), an adhesion-promoting interface layer 5, which is produced by chromating, phosphating, anodizing, galvanizing or the like, may be applied to the support 1 below the intermediate layer 2. It may also be expedient to pretreat the support 1 by wet-chemical and/or plasma-chemical means prior to the application of the coating material or to anodic oxidation, for cleaning purposes, in particular for degreasing.

An intermediate layer 2 which consists of a coating material is applied to the support 1. The coating material of the intermediate layer 2 may be a polycondensate which is produced on the basis of one or more monomers, a polyadduct or a polymer which is produced in particular by free-radical polymerization. It is particularly advantageous, as mentioned above, if the coating material of the intermediate layer 2 is suitable for a vacuum, i.e. has a glass transition temperature of over 100°C and a gas release rate of less than 10^{-4} mbar $1 \text{ s}^{-1} \text{ m}^{-2}$.

With a view to continuous application of the intermediate layer 2, it is advantageously possible to use coating materials which are based on acrylic resin, epoxy resin, phenolic resin, melamin resin, urea resin or polyurethane resin, can be processed using the coil-coating method, can be cured in particular at temperatures of up to about 250°C and the viscosity of which can be set by means of suitable solvents.

In this case, the coating material may be cured in various ways:

- by multistage curing using UV radiation from lamps or lasers and/or electron beams,
- by curing using UV radiation from lamps or lasers and hot air,
- by curing using UV radiation from lamps or lasers and IR radiation,

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- by curing using UV radiation from lamps or lasers and IR radiation from lasers, if appropriate in combination with hot air.

5 The thickness D_2 of the intermediate layer 2 may advantageously be adapted to the roughness of the support 1, values in the range from about 2 to 20 μm being characteristic.

10 On top of the intermediate layer 2 there is the multilayer optical system 3, which in all embodiments of the invention is applied to the intermediate layer 2 using the continuous vacuum strip-coating process. Also in all embodiments, the multilayer optical system 3 comprises three layers, the two upper layers 6, 7 being dielectric layers and the bottom layer 8 being a
15 metallic, in particular aluminium, layer which is applied to the intermediate layer 2. This metallic layer may advantageously be produced by sputtering or by vaporization, in particular by electron bombardment or from thermal sources.

20 The material of the two upper layers 6, 7 of the multilayer optical system 3 may in chemical terms belong to the group consisting of the metal oxides, metal nitrides, metal carbides, metal fluorides or metal sulphides, and the two upper layers 6, 7 should
25 have different refractive indices. The two upper layers 6, 7 of the multilayer optical system 3, like the bottom layer 8, may also be sputtered layers, in particular layers produced by reactive sputtering, or may be produced by vaporization, in particular by
30 electron bombardment or from thermal sources. In addition, CVD or PECVD application processes can be used to form these layers. Application processes of this nature are distinguished by the possibility of achieving low layer-thickness tolerances; specifically,
35 these tolerances do not exceed fluctuations within the range of approximately $\pm 5\%$.

In all the exemplary embodiments, the protective layer 4 which is applied to the multilayer optical system consists of a dielectric material with a

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low refractive index, in particular of SiO_2 . The thickness D_4 of the protective layer 4 is from 5 to 20 nm, preferably from 5 to 10 nm, and it can be applied to the multilayer optical system 3 in a continuous vacuum strip-coating process.

As can be seen from Fig. 1, the intermediate layer 2 is of planar form in the first three exemplary embodiments. The arithmetic roughness average R_a of the layer surface is in this case in the range from about 1 to 100 nm.

The first embodiment relates to a reflector material for visible light, in which in particular a total optical reflectivity determined according to DIN 5036 is at least 95% and a diffuse optical reflectivity is at most 4%. The bottom layer 8 of the multilayer optical system 3 consists of aluminium, and its thickness D_8 is such that the transmission through the layer 8 at the central wavelength of the reflection band is less than 0.5%. This thickness D_8 is approximately 60 nm. The layer 7 above it is an SiO_2 layer with a low refractive index and a thickness D_7 of about 90 nm, while the top layer 6, which is located above it, of the multilayer optical system 3 has a similarly high refractive index, consists of TiO_2 and has a thickness D_6 of about 60 nm. Both layers 6, 7 exhibit low absorption. The respective optical thicknesses D_6 , D_7 of the two upper layers 6, 7 are such that they correspond to about one quarter of the vacuum wavelength of the spectral centre of the desired optical reflection band. This makes the complete layer system 3 virtually colour neutral. The two layers 6, 7, in materials technology terms, are in particular selected in such a manner that the difference between the refractive indices is as high as possible. The thickness D_4 of the protective layer 4 is about 10 nm.

The second embodiment relates to a reflector material for ultraviolet light, in which in particular a total reflectivity determined as set down by DIN 5036 is at least 95% and a diffuse reflectivity is at most

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10%. The composite material differs from the first exemplary embodiment through the materials of high refractive index which are used in the top layer 6 of the multilayer optical system 3. In this case, instead of TiO_2 , it is advantageously possible to use ZrO_2 , HfO_2 with an optimum layer thickness D_6 of about 40 nm, or Al_2O_3 with an optimum layer thickness D_6 of about 45 nm; with ZrO_2 , the short-wave application limit is about 240 nm, with HfO_2 is about 200 nm and with Al_2O_3 is about 200 nm. The SiO_2 layer of low refractive index lying beneath this layer advantageously has a thickness D_7 of about 50 nm, while the bottom, aluminium layer 8 of the multilayer optical system 3 has a thickness D_8 of about 90 nm. The thickness D_4 of the protective layer 4 made from SiO_2 is about 6 nm.

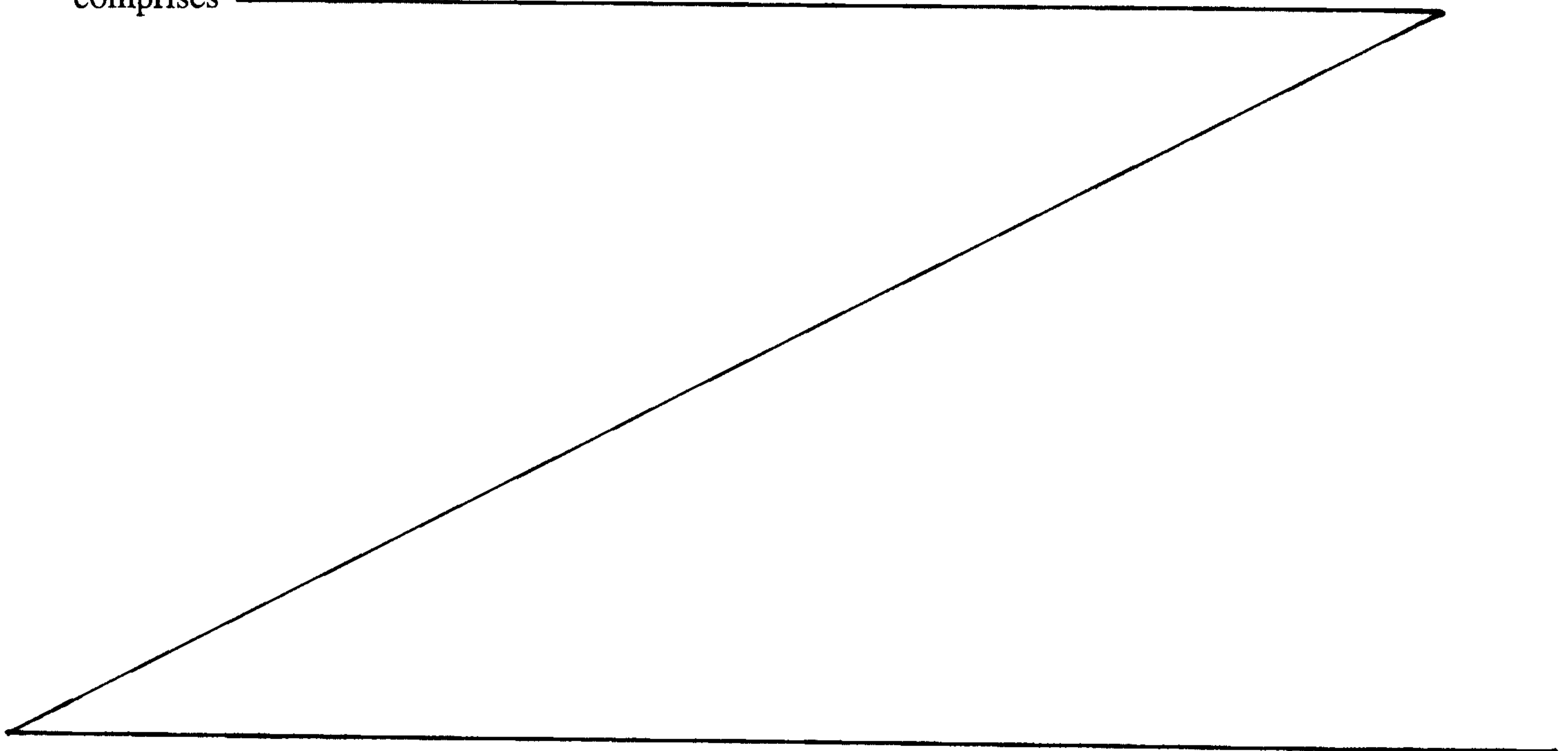
According to a third embodiment of the invention, a composite material according to the invention, as illustrated in Fig. 1, may also be provided with a multilayer optical system 3 which is such that a high absorbance determined in accordance with DIN 5036 is achieved. The lower metallic layer 8 on the coating-material surface, with a high absorbance, as well as the reflection-reducing dielectric layers 6, 7 lying above it, can be applied using the continuous vacuum strip-coating process. In this case, the layers 6, 7, 8 may be selected in such a way that they bring about a high total absorbance. A mechanical load-bearing capacity, determined in accordance with DIN 58196, of the surface of the composite material is - as with the first two embodiments and the fourth embodiment - better than H 50 - 1.

In the fourth exemplary embodiment of the invention, which is illustrated in Fig. 2, the intermediate layer 2 has an undulating or rough surface. The arithmetic roughness average R_a of the layer surface is in this case in the range from about 0.1 to 5 μm . This structure may be formed directly by the curing process or by a mechanical treatment which

takes place during or after curing of the coating material, if appropriate with the introduction of additional energy. In this case, the energy may be introduced by the above-described options for curing the coating material, such as single- or multistage, optionally combined curing using UV radiation, electron beams, hot air and/or IR radiation. A composite material according to the invention which is constructed in this way has a diffuse optical reflectivity, determined in accordance with DIN 5036, which lies in the range from 4 to about 95%.

The possibility of using a coating material or an eloxal layer to produce the intermediate layer 2 imparts a high corrosion resistance to the support 1, the coating material at the same time allowing a high surface hardness and scratch resistance, at least corresponding to the surface properties of an eloxal layer, to be achieved. An intermediate layer 2 which consists of coating material furthermore has a high flexibility, so that considerable mechanical deformations can be carried out on the composite material according to the invention without any cracks, in particular microcracks, being formed. Thus, in all four exemplary embodiments described, the coating materials used exhibited a flexural adhesion to the support 1 which was such that, in the mandrel flex test and with a material thickness of the support 1 of 0.4 mm and bending around a mandrel with a diameter of 2 mm, there was no delamination of the intermediate layer 2 when an adhesive strip of type Scotch™ 670 CFM, produced by 3 M, which was previously stuck on and was also bent around the mandrel, was pulled off. The coating according to the invention can be washed and withstands, without problems, the stresses imposed by further processing in illumination engineering, in particular during the shaping processes which have to be carried out.

The present invention is not limited to the exemplary embodiments illustrated, but rather comprises



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all means and measures which have the same effect in the context of the invention. By way of example, the protective layer 4 according to the invention does not have to consist of SiO_2 . Other suitable materials are those from the same chemical substance groups as those which can also be used for the upper two layers 6, 7 of the multilayer optical system 3. Furthermore, it is pointed out in particular that the intermediate layer 2 according to the invention does not absolutely have to be transparent, but rather may also, for example, be coloured, since the spectral properties of the reflected light are independent of this intermediate layer. A commercially available, standard industrial coating material can be used. A further advantage of the composite material according to the invention is that its edges are protected against corrosion.

Furthermore, the invention is not limited to the combination of features defined in Claim 1, but rather may also be defined by any other desired combination of specific features of all the individual features disclosed overall. This means that in principle virtually any individual feature of Claim 1 can be omitted or replaced by at least one individual feature disclosed at some other point in the application. To this extent, Claim 1 is merely to be understood as an initial attempt at formulating an invention.

List of reference symbols

1	Support
2	Intermediate layer
3	Multilayer optical system
4	Protective layer
5	Interface layer
6	Upper layer of 3
7	Middle layer of 3
8	Bottom layer of 3
D_1	Thickness of 1
D_2	Thickness of 2
D_4	Thickness of 4
D_6	Thickness of 6
D_7	Thickness of 7
D_8	Thickness of 8
R_a	Arithmetic roughness average

THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. Composite material suitable for reflectors, having a metallic support in strip form, an intermediate layer and having a multilayer optical system which is applied to the intermediate layer, characterized in that a non-metallic protective layer, which consists of a low-absorption material which is such that it permits a total optical reflectivity determined according to DIN 5036 of at least 95% and which has a thickness of from 5 to 20 nm, is applied to the multilayer optical system and that the thickness of the intermediate layer is in the range from about 2 to 20 μm and the intermediate layer comprises a coating material which is a polycondensate produced on the basis of one or more monomers, a polyadduct or a polymer.
2. Composite material as claimed in claim 1 wherein said polycondensate is produced by free-radical polymerization.
3. Composite material according to Claim 1 or Claim 2 characterized in that the coating material is processed using a coil-coating method.
4. Composite material according to Claim 1, 2 or 3, characterized in that the coating material is a stoving enamel with a pre-settable toughness which is based on a material selected from the group consisting of acrylic resin, epoxy resin, phenolic resin, melamin resin, urea resin and polyurethane resin and can be cured at temperatures of up to about 250°C.
5. Composite material according to Claim 1, 2, 3 or 4, characterized in that the coating material of the intermediate layer is selected according to the support which is pretreated by wet-chemical a plasmachemical means for cleaning purposes, and is hardened by curing using an energy source whereby the double bonds which are present in the monomers are crosslinked.

6. Composite material according to claim 1, 2, 3, 4 or 5 wherein the coating material exhibits a flexural adhesion to the support which satisfies at least one of the following provisions a) no delamination of the intermediate layer in a mandrel flex test with a material thickness of the support of 0.4 mm and bending around a mandrel with a diameter of 2 mm, when an adhesive strip of type Scotch 670 CFM, produced by 3 M, which has previously been stuck on and is also bent around the mandrel, is pulled off, and b) a mechanical load-bearing capacity of the surface, determined according to DIN 58196, is better than H 50 – 1.
7. Composite material as claimed in claim 5 or 6 wherein said energy source is selected from the group consisting of UV radiation, IR radiation, electron beam, and hot air.
8. Composite material according to one of Claims 1 to 7, characterized in that the coating material is suitable for a vacuum having a glass transition temperature of over 100°C and a gas release rate of less than 10^{-4} mbar $1\text{ s}^{-1}\text{ m}^{-2}$.
9. Composite material according to one of Claims 1 to 8, characterized in that the support is of a material selected from the group consisting of aluminium, magnesium, copper, titanium, molybdenum, tantalum, steel, brass and any alloys of these materials.
10. Composite material according to one of Claims 1 to 9, characterized in that an interface layer is applied to the support below the intermediate layer and said interface layer is produced by a process selected from the group consisting of chromating, phosphating, anodizing and galvanizing.
11. Composite material according to one of Claims 1 to 10, characterized by being in the form of a coil with a width of up to 1600mm.

12. Composite material as claimed in claim 11 wherein said coil has a thickness in the range of 0.1 to 1.5 mm.
13. Composite material according to one of Claims 1 to 12, characterized in that the multilayer optical system comprises three layers, the two upper layers being dielectric layers and the bottom layer being a metallic layer which has been applied to the intermediate layer.
14. Composite material according to claim 13 wherein said bottom layer is an aluminum layer which has been applied to the intermediate layer.
15. Composite material according to Claim 13 or 14, characterized in that the metallic layer of the multilayer optical system is a sputtered layer.
16. Composite material according to claim 13, 14 or 15 wherein the metallic layer is produced by a process selected from the group consisting of vaporization, electronic bombardment and a process using thermal sources.
17. Composite material according to Claim 13, 14, 15 or 16, characterized in that the material of the two upper layers of the multilayer optical system in chemical terms belongs to the group consisting of the metal oxides, metal nitrides, metal carbides, metal fluorides and metal sulphides, and the two upper layers have different refractive indices.
18. Composite material according to one of Claims 13 to 17, characterized in that the top layer of the multilayer optical system consists of a material with a high refractive index and the layer beneath it consists of a material with a low refractive index.
19. Composite material according to claim 18 wherein said top layer of the multilayer optical system is of a material selected from the group consisting of

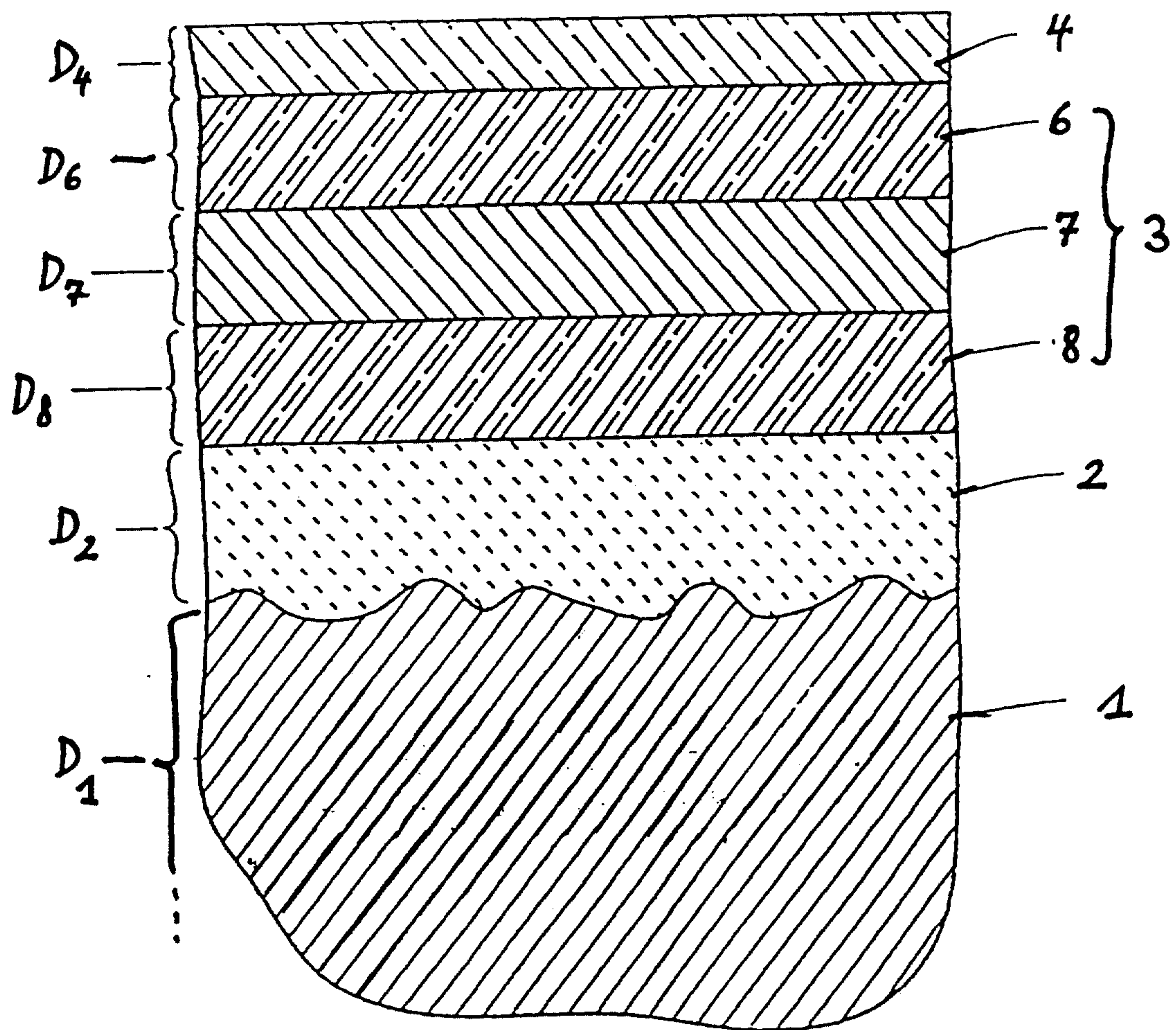
TiO₂, ZrO₂, HfO₂ and Al₂O₃.

20. Composite material according to one of Claims 13 to 18, characterized in that the two upper layers of the multilayer optical system are sputtered layers.
21. Composite material as claimed in claim 13 to 18 wherein said two upper layers are selected from the group consisting of CVD layers, PECVD layers and layers produced by vaporization.
22. Composite material according to one of Claims 13 to 20, characterized in that the two upper layers of the multilayer optical system exhibit low absorption which is such that they permit a total optical reflectivity determined according to DIN 5036 of at least 95%.
23. Composite material according to one of Claims 1 to 22, characterized in that the intermediate layer has an arithmetic roughness average in the range from 1 to 100 nm and a diffuse optical reflectivity determined according to DIN 5036 of at most 4%.
24. Composite material according to one of Claims 1 to 22, characterized in that the intermediate layer has a rough surface with arithmetic roughness average in the range from 0.1 to 5 µm which is such that a diffuse optical reflectivity determined according to DIN 5036 lies in the range from 4 to 95%.
25. Composite material according to Claim 24, characterized in that the rough surface of the intermediate layer is formed during the operation of curing the coating material.
26. Composite material according to Claim 24 or 25, characterized in that the rough surface of the intermediate layer is formed by a mechanical treatment which takes place during curing of the coating material.

27. Composite material according to Claim 26, characterized in that the rough surface of the intermediate layer is formed by a mechanical treatment which takes place after curing of the coating material.
28. Composite material according to one of Claims 1 to 27, characterized in that the protective layer consists of a dielectric material with a low refractive index.
29. Composite material according to one of Claims 1 to 27, characterized in that the protective layer is SiO₂.
30. Composite material according to one of Claims 1 to 29, characterized in that the protective layer is a layer selected from the group consisting of a sputtered layer, a CVD layer, PECVD layer and a layer which is produced by vaporization.

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FIG. 1



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FIG. 2

