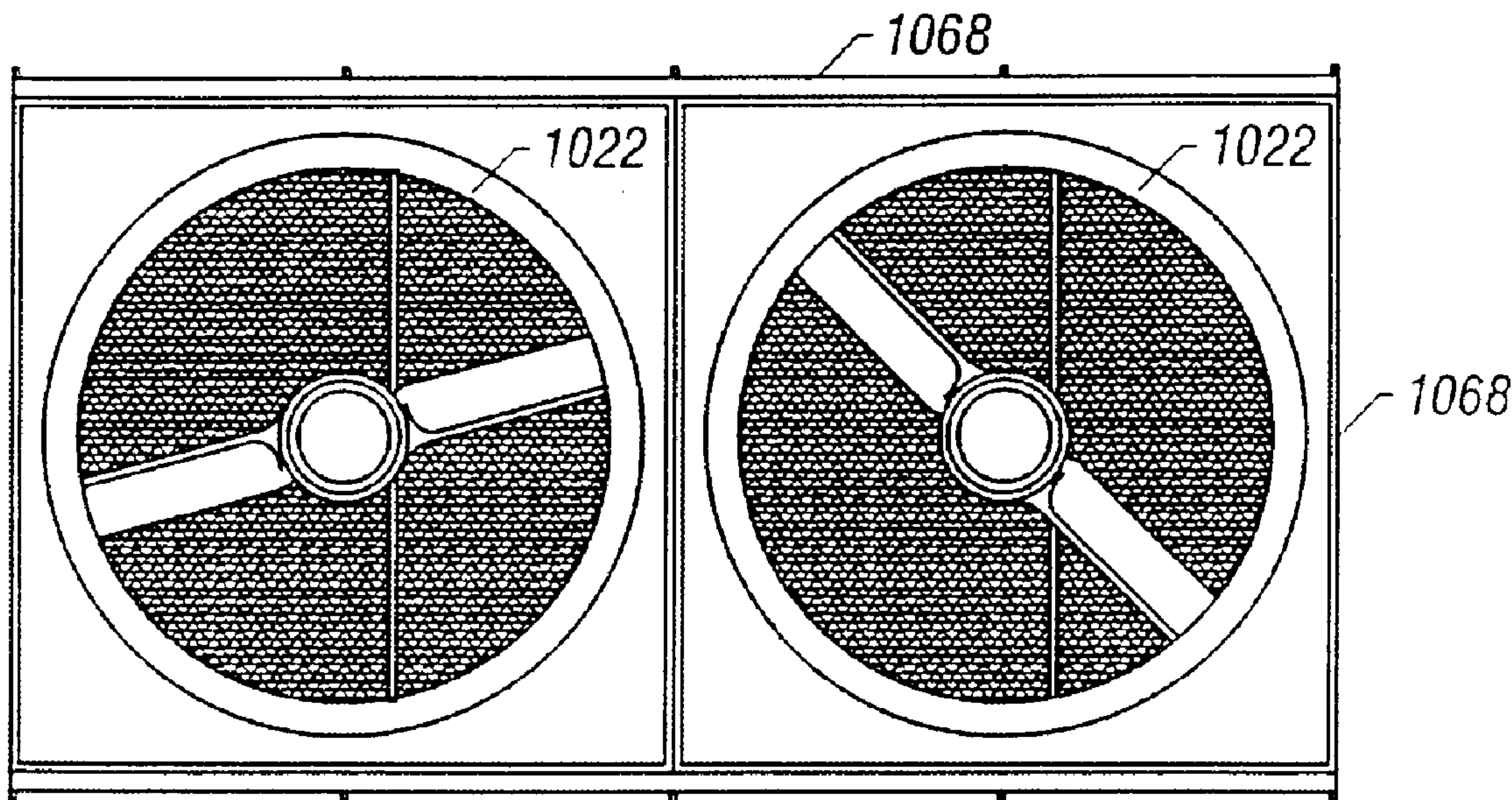




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CONDITIONING



(57) Abrégé/Abstract:

Novel heat exchangers and methods of constructing the heat exchangers for use in indirect evaporative cooling applications. The evaporative apparatus for cooling comprises both a multi-stage indirect evaporative cooling heat exchanger (1074); and a multi-stage sump (1036) where each sump stage, in a one-to-one relationship. Other multi-stage heat exchangers with their associated multistage sumps can be combined, with the cooled air of a first multistage evaporative assembly feeding into the intake end of a second multistage evaporative assembly, and so on. These heat exchangers can be an entire assembly for the pre-cooling and cleaning of the air going to a gas turbine or any other air breathing device, with an air washer stage (1044) in which air is directly cooled by evaporation and where simultaneously the air is also cleaned of dust, dirt and other impurities.

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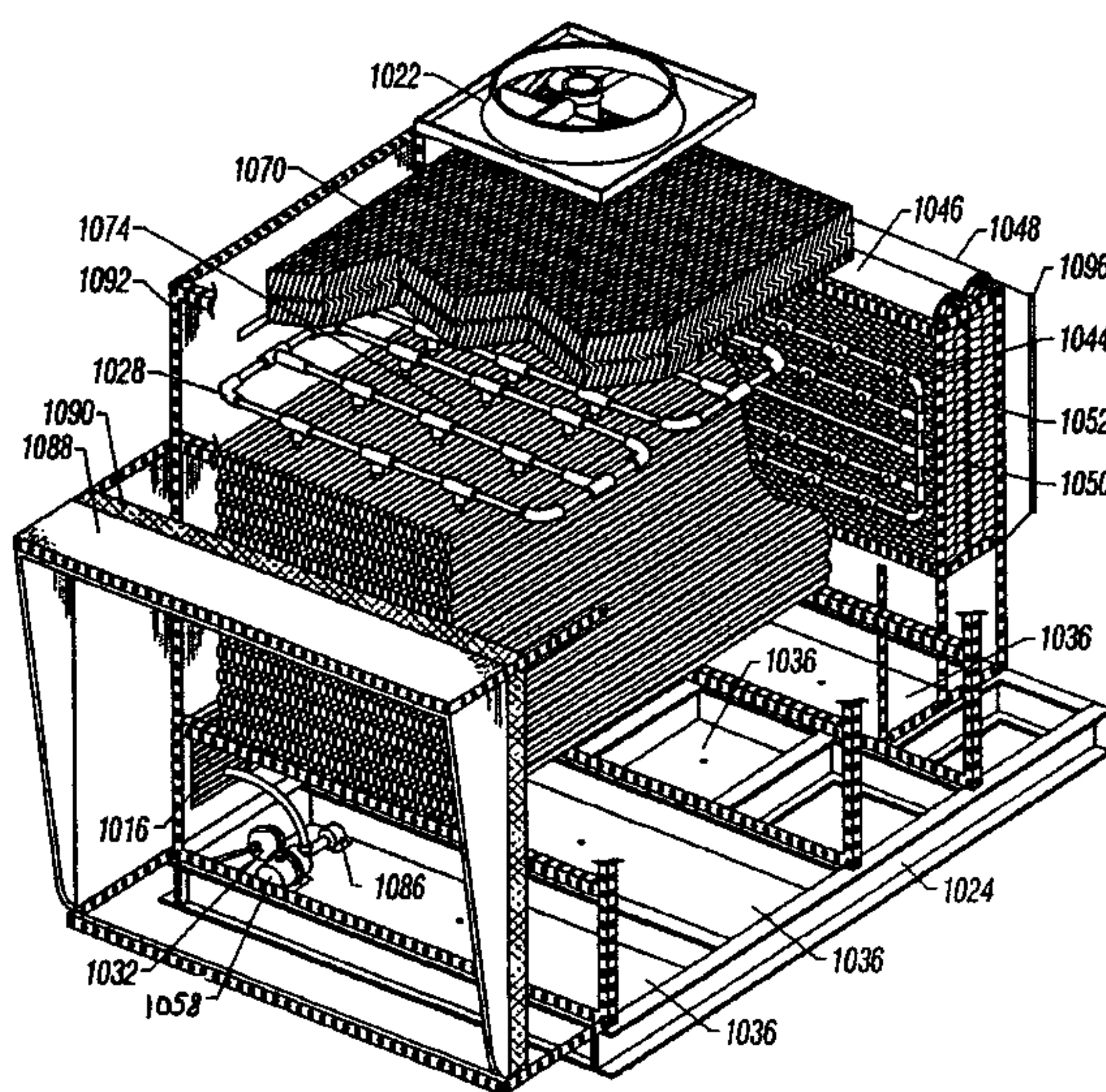
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(54) Title: A HEAT EXCHANGER FOR COOLING AND FOR A PRE-COOLER FOR TURBINE INTAKE AIR CONDITIONING



(57) Abstract: Novel heat exchangers and methods of constructing the heat exchangers for use in indirect evaporative cooling applications. The evaporative apparatus for cooling comprises both a multi-stage indirect evaporative cooling heat exchanger (1074); and a multi-stage sump (1036) where each sump stage, in a one-to-one relationship. Other multi-stage heat exchangers with their associated multistage sumps can be combined, with the cooled air of a first multistage evaporative assembly feeding into the intake end of a second multistage evaporative assembly, and so on. These heat exchangers can be an entire assembly for the pre-cooling and cleaning of the air going to a gas turbine or any other air breathing device, with an air washer stage (1044) in which air is directly cooled by evaporation and where simultaneously the air is also cleaned of dust, dirt and other impurities.

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A HEAT EXCHANGER FOR COOLING AND FOR A PRE-COOLER FOR
TURBINE INTAKE AIR CONDITIONING

5 This application claims the benefit of Provisional Application 60/184,255 filed February 23, 2000.

FIELD OF THE INVENTION

10 The invention relates to a method and apparatus for increasing the density of air being used in a compression process such as air compressors, gas turbines and other processes where the increase of air density is important. This invention also relates to a method and apparatus for reducing the temperature of air. It relates to air-conditioning. It relates to heat exchangers.

15 BACKGROUND

Indirect evaporative cooling invented in the mid-seventies (see, for example, Schlom, et al., United States Patent Number 4,023,949) uses the latent heat of the evaporation of water to remove heat from the air. Direct evaporative coolers on the other hand, also known as swamp coolers, cool the air by passing the air through wet
20 pads by which the evaporative absorption of the latent heat of evaporation by the water directly cools the air. Since the water vapor evaporates directly into the air, the air ends up with a heavy load of moisture. With a third approach, direct refrigeration, the air passes through a heat exchanger where it evaporates a refrigerant such as freon. The latent heat of evaporation of the freon acts on the air through a heat
25 exchanger to cool the air. To recycle the freon additional energy is used to compress and condense the freon vapor back to a liquid, which can then be evaporated all over again. Indirect evaporation evaporates water instead of freon in the heat exchanger. Another difference is that the water vapor is not recaptured and condensed back to the liquid state, as is freon, for example, in the refrigeration case. Therefore the energy
30 use efficiency is increased in the indirect evaporative process because no energy is expended on the condensation of the refrigerant part of a refrigeration process.

Traditionally, gas turbine intake systems depend upon the density of air to increase efficiency. Three methods, historically, to increase gas turbine intake efficiency include steam injection, refrigeration, and direct evaporative cooling. A

less expensive approach to increasing the intake air density by cooling, other than these historical methods, is an indirect evaporative approach. Prior patents in this area include Schlom et al.: US 4,023,949; US 4,107,940; US 4,137,058; US 4,156,351 and US 4,418,527; Fogelman: 5076347; and Kopko: WO9851916A1.

5 Areas in which additional increased efficiency of the indirect evaporative cooling, or the "Everest Cycle" (United States Patent Number 4,023,949), might be improved include (a) better heat exchange process, (b) better water evaporation process, and (c) bringing the "room inlet dry-bulb" as close as possible to the "exhaust air wet-bulb temperature" so as to increase the thermodynamic efficiency of
10 the actual process.

SUMMARY OF THE INVENTION

The present invention comprises novel heat exchangers and methods of constructing the heat exchangers for use in indirect evaporative cooling applications.
15 The heat exchanger is useful for both single and multiple unit (where a plurality of heat exchangers are back-to-back) indirect evaporative processes. The evaporative apparatus for cooling comprises both a multi-stage indirect evaporative cooling heat exchanger; and a multi-stage sump where each sump stage, in a one-to-one relationship with a stage of the multi-stage heat exchanger has sump water at
20 progressively cooler temperatures as one progresses further into the heat exchanger. Because there are separate stages of the heat exchanger and the water sumps, progressive cooling is induced on dry side output air. Other multistage heat exchangers with their associated multistage sumps can be combined, with the cooled air of a first multistage evaporative assembly feeding into the intake end of a second
25 multistage evaporative assembly, and so on.

As a multi-stage process, for n stages, as n approaches infinity, the thermodynamic efficiency may approach a maximum, since the entropy production $dS = \sum dq/T$ may be minimized (S = entropy, dq = heat transferred at temperature T). This is the case where the operational cycle of the multi-stage process is as close to a
30 reversible process as possible. In actual practice most of the thermodynamic efficiency gain may be achieved with four to six stages.

These heat exchangers can be used for comfort cooling, pre-cooling of intake air for gas turbines and for supplying cooling air for other applications such as electrical generators and lubricating oil coolers. As a comfort, or other cooler, the

present invention may be used as either a stand-alone cooling unit or as a pre-cooler for another air conditioning device where it pre-cools the ambient air.

As an application, the indirect-direct evaporative apparatus can be considered as an entire assembly for the pre-cooling and cleaning of the air going to a gas turbine or any other air-breathing device. As such, an additional stage is included, viz., an air washer stage in which air is directly evaporatively cooled and where simultaneously the air is also cleaned of dust, dirt and other impurities.

Accordingly, the present invention provides an evaporative apparatus comprising: (a) a multi-substage direct evaporative cooling stage; (b) one or more air cleaning sub-stages of said multi-sub-stage direct evaporative stage; (c) a first multi-stage indirect evaporative cooling heat exchanger; (d) said first multi-stage indirect evaporative cooling heat exchanger configured to be coupled with a second multi-stage indirect evaporative cooling heat exchanger such that output of said first heat exchanger is fed to input of said second heat exchanger; (e) cool output from said second and said first linked heat exchangers combination is substantially additive of cool outputs of said second and said first linked heat exchangers individually; (f) multi-stage sumps wherein each sump stage, in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures; (g) said separate sumps are thermally insulated from each other to maintain different sump temperatures.

Accordingly, the present invention provides an evaporative apparatus for cooling comprising: (a) a multi-stage indirect evaporative cooling heat exchanger; (b) one or more water-spray direct evaporative cooling stage; (c) a final wetted media stage; wherein air flowing through one or more media of the evaporative apparatus is cleaned; (d) multi-stage sumps wherein each sump stage, in a corresponding relationship to a stage of said multi-stage indirect evaporative cooling heat exchanger, can contain sump water at different temperatures.

The present invention also provides a pre-cooler for cooling intake air of a gas turbine, comprising: (a) a multi-stage indirect evaporative cooling heat exchanger; wherein a first stage (1) is linked with a second stage (2) such that cool output of said first stage is feedable to input of said second stage; wherein cool output from said second and said first linked heat exchangers stages is approximately additive of cool

outputs of said second and said first linked heat exchangers stages individually; (b) a multi-substage direct evaporative cooling stage (1044, 1046, 1048); wherein there are one or more air cleaning sub-stages (1046, 1048) of said multi-substage direct evaporative stage; and (c) multi-stage sumps (1036) wherein each sump stage is in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures, and wherein said separate sumps (1036) are thermally insulated from each other; and wherein (d) at least a last stage of said heat exchanger utilizes a portion (1072) of a dry side (1014) air flow to enter the wet side (1016) evaporative airflow, wherein said air has been sensibly cooled relative to, and is at a lower wet bulb temperature than, the ambient air.

In a further aspect, the present invention provides a method for making an evaporative apparatus comprising the steps of: (a) assembling a first multi-stage indirect evaporative cooling heat exchanger; (b) linking said first multi-stage indirect evaporative cooling heat exchanger with a second multi-stage indirect evaporative cooling heat exchanger; (c) feeding output of said first heat exchanger to input of said second heat exchanger; (d) adding cool output from said second and said first linked heat exchangers combination so as to achieve a cooling substantially additive of cooling of said second and said first linked heat exchangers, individually; (e) containing sump water in multi-stage sumps wherein each sump stage, in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures; (f) insulating said separate sumps thermally from each other; and (g) maintaining different sump temperatures.

BRIEF DESCRIPTION OF THE DRAWINGS

The above and other features and advantages of the invention will be more apparent from the following detailed description wherein:

Figure 1A schematically depicts heat exchanger plates used in this invention, in particular a sinusoidal plate type;

Figure 1B schematically depicts heat exchanger plates used in this invention, in particular a polygonal plate type;

Figure 1C schematically depicts heat exchanger plates used in this invention, in particular, an assembly of two polygonal plates to form an airflow path;

Figure 1D schematically depicts heat exchanger plates used in this invention, in particular, the assembly of 1C with the inclusion of an intermediate plate;

Figure 2A schematically depicts a polygonal plate with deformations to induce air turbulence, i.e., embossed “turbulators” on the heat exchanger plates;

Figure 2B shows a plate assemblage with deformations to induce air turbulence;

Figure 3A shows a plate assemblage with tabs to induce air turbulence;

Figure 3B shows an intermediate plate with tabs to induce air turbulence;

Figure 3C shows a detail of an individual tab;

Figure 3D a detail depicting a section of an intermediate plate, as in Figure 3B, showing an associated airflow, as a consequence of a tab in an intermediate plate;

Figure 4A shows a plate assembly without tabs or deformations;

Figure 4B is an end view of a portion of a heat exchanger, showing dividers;

Figure 5 shows a schematic section of two-stage indirect evaporative cooler showing airflow paths;

Figure 6 shows a schematic section of multistage (“n”-series) indirect evaporative cooler showing airflow paths;

Figure 7 shows a schematic section of cascaded sumps;

Figure 8A shows a schematic top view of an indirect evaporative cooler with first indirect stage on sides;

Figure 8B Schematic side view of an indirect evaporative cooler with first
5 indirect stage on sides;

Figure 9 shows a schematic section of multi-stage indirect evaporative cooler with an air washer operating thermodynamically and psychometrically according to the Schlom Cycle;

Figure 10 shows a schematic section of the air washer;

10 Figure 11 shows a side view of unit described in Figure 5, with the air intake on the left;

Figure 12 shows an isometric section of the unit described in Figure 5;

Figure 13 shows an end view and section of intake of the unit described in Figure
5;

15 Figure 14 shows an end view and section of discharge of the unit described in Figure 5;

Figure 15 shows a side view of unit described in Figure 5, with the intake on right;

Figure 16 shows a top view of the unit described in Figure 5;

20 Figure 17 shows a top view of the multi-stage unit shown in Figure 6;

Figure 18 shows a psychrometric chart depicting various evaporative cycles (direct evaporative cooling, direct evaporative cooling with fogging, multistage indirect evaporative cooling and indirect evaporative cooling with air washer) with comparisons relating to air density;

25 Figure 19 shows plate dividers made with holes;

Figure 20 shows plate dividers made with slats;

Figure 21 shows plate dividers made with reticulated foam;

Figure 22 shows solid plate dividers;

30 Figure 23 shows an isometric section of unit depicted in Figure 9 with item callouts;

Figure 24 shows an isometric section of unit described in Fig. 9 with air flow path depicted;

Figure 25 shows a section of a unit described in Figure 9, as viewed from intake

end;

Figure 26 shows a section of a unit described in Figure 9, as viewed from discharge end;

Figure 27 shows a psychrometric chart depicting the thermodynamic path of an "n"-series arrangement of heat exchangers, for $n = 4$;

Figure 28 shows a section of a unit described in Figure 9, with item callouts.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The following description is of the best mode presently contemplated for carrying out the invention. This description is not to be taken in a limiting sense, but is merely made for the purpose of describing the general principles of the invention. The scope of the invention should be determined with reference to the claims.

The item call-out numbers and description are listed below for reference:

15	<u>Item No.</u>	<u>Description</u>
	1002	Sinusoidal plates.
	1004	Polygonal plates.
	1006	intermediate in assemblage of figure 1 D.
	1008	Deformed portion of plate to induce turbulence.
20	1010	Tabs and /or deformations to induce turbulence.
	1012	Section of intermediate plate with deformations causing airflow to change direction.
	1014	Dry side air path (primary air).
25	1016	Wet side air path (secondary air).
	1018	Dry side air -leaving.
	1020	Wet side air -leaving.
	1022	Wet side fan/s
	1024	Foundation (base).
30	1026	Sump/s.
	1028	Spray manifold.
	1030	Water Inlet.
	1032	Float valve .
	1034	Water line from float valve to first sump.

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- 1036 Sump
- 1038 Water transfer pipe.
- 1040 Overflow /drain pipe.
- 1042 Screens.
- 5 1044 Spray manifold -Air Washer.
- 1046 Cover, Air Washer -primary media.
- 1048 Cover, Air Washer -secondary media.
- 1050 Primary evaporative media.
- 1052 Secondary evaporative media.
- 10 1054 Distribution pump -primary media.
- 1056 Distribution pipe -secondary media.
- 1058 Pump spray manifold -Air Washer
- 1060 Pump/s primary and secondary media.
- 1062 Pipe from pump to spray manifold.
- 15 1064 Pipe from pump/s to media distribution pipes.
- 1066 Access panel
- 1068 Housing.
- 1070 Moisture eliminator
- 1072 Airflow path from primary to secondary air (indirectly cooled air now goes
- 20 to
- the wet side of the next stage).
- 1074 Heat exchanger assembly.
- 1076 'n" series unit and components.
- 1078 Plate separator with holes -end view.
- 25 1079 Plate separator with holes -side view.
- 1080 Plate separator with slats (louvers)-end view.
- 1081 Plate separator with slats (louvers)-side view.
- 1082 Plate separator of reticulated foam -end view.
- 1083 Plate separator of reticulated foam -side view.
- 30 1084 Plate separator, solid -end view.
- 1085 Plate separator, solid -side view.
- 1086 Strainer for pump/s.
- 1088 Intake air hood.
- 1090 Intake air filters.

1092 Framework (structure).

1094 A-B Air flow through heat exchanger to plenum.

1094 B-C Air flow downward in plenum.

1094 C-D Air flow from plenum into sump area.

5 1094 D-E Air flow upward through wet side of heat exchanger to atmosphere.

1096 Air discharge housing.

1098 Plenum (this is where air which has been indirect evaporatively cooled leaves the dry side of the heat exchanger and then enters the wet side of the next stage).

10

The new heat exchanger design utilizes plates or sheets of material in either a or a sinusoidal 1002 shape (Figure 1A) or a polygonal 1004 shape (Figure 1B) in cross section, either one of which closely approximates a repeating wave form. The plates 1004 (Figure 1C) may be arranged in pairs forming channels for air flow; the arrows in 15 Figure 1C indicate the air flow. Optionally, as an enhancement of the heat exchanger, pairs of plates may optionally utilized an intermediate plate 1006 to separate the plate pair and to provide a uniformly shaped channel between them. The purpose of this intermediate plate 1004 (Figure 1D) is to form another heat transfer surface, transferring heat between the center of the airflow and the polygonal walls.

20 The plates may be fabricated from one or more of a number of materials. Any thermally conductive material may be a candidate. Without limiting or restricting the material or materials of which the sheets of material might be fabricated, a number of candidate materials are nevertheless listed. These include steel, galvanized iron, galvanized steel, stainless steel, thermally conductive plastic, thermally conductive 25 ceramic, metal coated with paint, metal coated with varnish, metal coated with plastic, metal coated with ceramic, metal coated with glass, metal coated with diamond-like coating, titanium, thermally conductive composite, aluminum, magnesium, copper or silver.

30 Since turbulent air flow over a water surface can increase the evaporation rate for a given net air flow rate, increased roughness and vortex generators are used to increase the turbulence of the air flowing over the water film as the water film itself gravitationally flows down toward a sump. Extrapolation of known data of ocean surface roughness related to evaporation rates yields a factor of three or more for the rate of increased evaporation for turbulent air flow compared to a laminar type of air

flow over a smooth ocean.

Another use of this intermediate plate is to provide a support surface for tabs and fins which help enable turbulence in the air flowing over them. The turbulence will improve the heat transfer by changing the laminar flow to turbulent flow.

5 One method of initiating turbulence in the air flow is the use of irregularities (1008, Figure 2A) mechanically or otherwise produced on the surface of the preformed sheets 1002 (Figure 1A), 1004 (Figure 1B) used to produce the "pairs" (Figure 1C). The roughness of these irregularities gives rise to a mixing length of increased turbulent vertical mixing into the airflow. These irregularities can be produced either by
10 embossing the material 1008 (Figure 2A, 2B) or by mechanically attaching tabs, fins 1010 (Figure 3A, 3B, 3C) or "turbulators", to which these tabs, fins, embossments and bumps will be generically referred. The embossments 1008 (Figure 2A) may be applied to the inside of the outer walls of the plate pair channels as shown in Figures 2A and 2B.

15 The tabs 1010 (Figure 3B) are shown formed on an intermediate plate 1006. Figure 3A shows the assembly as in Figure 1D, but with the intermediate plate 1006 having tabs 1010. The turbulators act on the process air flow produce vortex eddies and breakup the laminar flow. Figure 3D shows an air flow condition (arrows) 1012 on a tab 1010 on an intermediate plate 1006.

20 Bumps or tab-like elements can also be added from any material compatible with the basic structure. These may include such materials as sintered metal powder and foamed metal, which, when applied act to increase surface roughness, and may also act to increase the total wetted surface. For many of the tabs or bumps, water flowing gravitationally down a channel may encounter a vertex or edge of a tab, bump
25 or other attached material, and may fall off that object as a droplet, with the potential to provide a greater evaporation rate, as a droplet will expose more surface area. The net effect of introducing methods and devices for producing turbulence is to increase the efficiency of operation of the overall apparatus.

Figure 4A shows an assembly of polygonal plates 1004 and the optional
30 intermediate plate 1006. Figure 4B shows several assemblies as in Figure 4A further assembled into a heat exchanger with polygonal plates 1004, intermediate plate 1006 dividers, and also shows the dry side air path (primary air) 1014 and the wet side air path (secondary air) 1016.

Figure 5 shows a schematic section of the two-stage version of the indirect

evaporative cooler, showing airflow paths. Figure 5 shows the dry side (primary) air path **1014**, the wet side (secondary) air path **1016**, the dry side air leaving **1018** the unit, the wet side air leaving **1020** and the airflow path from the primary to the secondary air **1072**. The two-stage version of the evaporative cooler sits on a base **1024**, which supports sumps **1026** which collects water cascading down the cooler which is sprayed by the spray manifold **1028**. The wet side air **1016**, **1020** is drawn out by the wet side fans **1022**.

Figure 6 shows a schematic section of an n-stage (five stages are shown) indirect evaporative cooler. The incoming dry side (primary) air **1014** enters from the left of Figure 6 and ultimately exits **1018** on the right. The wet side air **1016** enters from the bottom (left) and some exits through the top **1020**, drawn up by the wet side fans **1022**.

However, in the n-stage process, some of the dry side air, at each stage, is redirected into the wet side air, at a next successive stage. Consequently, the already cooled dry side air becomes the wet side air, resulting in a lower temperature wet side air with a lower wet side dew point temperature. The effect, as will be seen, is to efficiently cool the dry side air which exits **1018** to a lower temperature air stream with a higher air density. The coldest dry-side **5002** (Figure 5) is being cooled by the coldest water and the coldest air with the lowest wet bulb temperature.

Another advantageous feature of this embodiment of the heat exchanger is to provide separate, distinct sumps **1036**, **1036**, **1036** (Figure 7) for the water utilized on the "wet side" of the heat exchanger. The separate sumps maintain the coldest water on the leaving side of the heat exchanger. Additionally, these sumps can be arranged in a "cascade" fashion (Figure 7, **1036**, **1036**, **1036**) where the water flows from the coldest sump **1036** on the right to the warmest sump, **1036** on the left.

A float valve **1032** regulates the refilling of the coldest sump **1036** on the right, as required, by the level in the warm-side sump **1036** on the left. When the level in the sump **1036** on the left falls, the float valve **1032** allows water to enter from the water inlet **1030**. The water line **1034** from the float valve to the first sump **1036** on the right, allows the first sump to be refilled according to the level of the last sump (**1036** on the left). Water transfer pipes **1038** and an overflow (and drain) pipe **1040** complete the sump system.

Each separate sump sits at the bottom of separate spray systems **1028** (Figure 5) with separate pumps that supply each separate spray and sump unit. In the

preferred embodiment the first sump **1036** (on the right) would be at the air washer, or, at the last heat exchanger, if a direct evaporative stage were not used. In this embodiment water is supplied to the direct evaporative stage only and then flows down to the lowest sump where any excess water is discharged. Also, at this point
5 sufficient "bleed" **1040** will be employed to maintain a low concentration of dissolved solids in the water to prevent the build-up of dissolved solids on the walls of the heat exchanger. Because the different sumps are sufficiently thermally insulated, and the air progressing through each partition or stage, is tending to be cooler than the previous stage or partition, the temperature of the thermally graded sumps both reflect
10 this increased cooling and contribute to it.

A unique feature of the heat exchanger is that it provides for a portion of the air to be first indirectly evaporatively cooled and then used **1072** (Figure 8A, 8B) for the wet side of the final portion of the heat exchanger. Figure 8A shows a schematic top view of an embodiment of the indirect evaporative cooler with a first indirect
15 stage on the sides. Figure 8B shows a schematic side view of an embodiment of the indirect evaporative cooler with a first indirect stage on the sides.

Advantageously, this process within the heat exchanger itself significantly improves performance. Previous technology utilized separate heat exchangers to achieve this process. The air tends to evaporate the water. The water changes from a
20 liquid to a vapor state, which requires a gain of molecular kinetic energy. This gain of molecular kinetic energy is at the expense of the remaining water, which loses that amount of energy, expressed as the latent heat of evaporation. Thus, the temperature of the unevaporated water and the heat exchange surfaces in contact with it reflect some decrease in their molecular kinetic energy (conservation of energy). The
25 decreased molecular kinetic energy is (expressed as) a decreased temperature. A wet-bulb temperature is that temperature to which a fully aspirated thermometer would fall due to the evaporation from water which is continuously supplied to it by a wetted wick. In order to further cool that wet bulb thermometer, one needs to bring it in contact with matter that is at a lower temperature. Then, sensible heat is transferred
30 from the thermometer to the colder matter. The sensible heat transfer is in the form of the thermometer's higher kinetic energy molecules transferring kinetic energy to the lower kinetic energy matter. This transfer of sensible heat can then lower the thermometer's temperature below the wet bulb temperature, if the temperature of the colder matter is below the thermometer's wet bulb temperature. Air from the dry side

which has been cooled toward the wet bulb temperature of the wet side air has a lower dry bulb temperature.

If one places an imaginary box around the n-stage heat exchanger, one may examine aspects of its efficiency. The wet side air process is evaporating water. The evaporation is a change of phase and takes place isothermally. For an amount of
 5 (latent) energy equal to L released, some amount is absorbed by the dry side air, L-dL. The quantity dL represents energy loss not transferred to the dry air. The amount of entropy transferred in from the ambient temperature wet side air flow is: L/T_{ambient} while the entropy carried out by the dry side air is $(L - dL)/(T_{\text{ambient}} - dT)$ since the
 10 dry side air has been sensibly cooled. The difference is then: heat absorbed at the higher temperature minus the heat rejected at a lower temperature, or,

$$(T_{\text{ambient}}dL - LdT)/(T_{\text{ambient}}(T_{\text{ambient}} - dT)).$$

Where the latent heat loss (dL) is kept as small as feasible, the determining factor is LdT. Since L is a constant, the difference between the temperature at the wet side air
 15 and the dry side air flow (dT) determines the efficiency of the process. The smaller dT, the more efficient the process. In the multistage process, dT is automatically kept small by utilizing some of the cooled dry air flow for the next stage of the wet side cooling.

Figure 9 shows a schematic section of multi-stage indirect evaporative cooler with an air washer operating thermodynamically and psychometrically according to
 20 the Schlom Cycle. The dry air **1014** enters from the left; the wet air **1016** enters from the left bottom. Some of the cooled dry air is used **1072** on the wet side of the next stage. The separate sumps **1026** are fairly thermally isolated from each other. The final, cool dry air **1018** exits on the right to be used, for example, in an electric
 25 generating gas turbine. Screens **1042** are placed in the air stream **1018**. Spray manifolds **1044** provide the washing of the air. There is a cover **1046** for the primary media and a cover for **1048** the secondary media.

Figure 10 shows a schematic section of an air washer operating thermodynamically and psychometrically according to the Schlom Cycle. The air washer is the final stage in this indirect-direct evaporative process. It represents a
 30 direct evaporative mode. In the air washer, the air receives its final cooling and is also thoroughly cleansed of dirt and pollutants of all types. The air washer consists of two sub-stages. The first sub-stage is a spray section **1044** where the air must pass through a deluge of fine spray (not mist) **1044**. The second, final, sub-stage

comprises two media type sub-stages **1046, 1048**. In these two media type substages clean flowing water **1054** (distribution pipe for the primary media), **1056** (distribution pipe for the secondary media) removes any dirt that may have gotten through the previous stages. Also, that clean flowing water **1054, 1056** will re-dissolve any salts
5 that may have been entrained in the evaporation in the previous stages.

In the first air washer sub-stage, the nozzles **1044** (Figure 10) are supplied with clean water, which has been cleansed by use of ten-micron filtration. In this preferred embodiment, this water can be at normal line pressure (50 -70 psi) or can be supplied from the sump by means of a pump at pressures as low as 5 -10 psi. Any workable
10 pressure range may be utilized. Screens **1042** in this air stream are also employed to further breakup the droplets. The spray manifold **1044** directs its water droplet spray into the screens **1042** where they tend to be broken into smaller spray droplets by hitting the screens with the dry air flow (**1018**-arrows shown but not number) entering from the left.

Figure 10 shows a schematic section of the air washer including the pump spray manifold **1058** for the water supply through pipe **1062** to the spray manifold **1044**. A pump **1060** supplies water for the primary **1050** and the secondary **1052** media through the pipes **1064**.
15

The air velocity in this air washer section sub-stage is kept low enough to prevent moisture carryover to the final sub-stage. For a preferred embodiment, this
20 may entail air velocity staying below 500 feet per minute. Excess water from this sub-stage sump **10261** will flow to the sump **10262** of the final stage of the heat exchanger where it will be used on that stage's wet side.

The final media sub-stage consists of media **1050, 1052** such as a cross-fluted design implemented in a cellulose paper, such as Munters "CELDEK" TM, or
25 implemented in glass matting, such as Munters' "GLASDEK" TM, which is supplied with very clean water **1054, 1056**, which has been cleansed with a one-micron filter. Since almost no evaporation occurs in this stage only a very small amount of water is needed, just that amount which is sufficient to maintain wetness throughout this
30 section. Not only will this sub-stage remove any particulate matter which may have gotten past the prior sub-stage, it will also cause any dissolved solids which may have evaporated to again be re-dissolved and then flushed from the system.

A proprietary media may also be used in this stage. It is designed to allow the purified water to very effectively clean the air flowing through it and to not require

frequent replacement. The water in this air washer section sub-stage will be passed through one time only and not used again in this sub-stage. This water will go to the sump **10261** of an indirect evaporative stage where it will be filtered before being used in that stage.

5 This use of this air washer relieves normal intake air filters of a great deal of their work. Before, their role was to remove all potential airborne particulate matter, which could be injurious to the gas turbine. Now they only need remove large particulate matter such as bugs, leaves, feathers and other large items, which could be harmful to the heat exchanger.

10 Advantageously, the air washer sub-stage will provide the cleanliness required by the turbine utilizing potable water only, without any de-ionized water. The use of normal potable water for cleaning the air is a great improvement over current practice, which requires more expensive de-ionized water as the basis of the method of achieving great cleanliness. Advantageously, it should be noted that the
15 addition of water vapor to the cooled air fed to a gas turbine might have a significant impact in reducing emissions of NOx and other pollutants.

 Figure 11 shows a side view of unit described in Figure 5, with the air intake on the right showing wet side fans **1022**, foundation **1024**, housing **1068**, wet side air flow **1016**, pipe from pump to spray manifold **1062** and access panel **1066**.

20 Figure 12 shows an isometric section of the unit described in Figure 5. The wet side air inflow **1016** is shown along with a float valve **1032**, together with a pump for the spray manifold **1058**, an overflow/drain pipe **1040**, a sump **1036**, the foundation **1026**, the heat exchanger assembly **1074**, the spray manifold **1028**, housing **1068**, access panel **1066**, a wet side fan **1022**, and the airflow path from primary to secondary air
25 **1072**.

 Figure 13 shows an end view and section of intake of the unit described in Figure 5. The float valve **1032** may be seen, together with an overflow/drain pipe **1040**, foundation **1024**, housing **1068**, the heat exchanger assembly **1074**, a pipe from the pump to the spray manifold **1062**, a spray manifold **1028**, a wet side fan **1022** and a
30 moisture eliminator **1070**.

 Figure 14 shows an end view and section of discharge of the unit described in Figure 5. The overflow/drain pipe **1040** may be seen, together with the foundation **1024**, housing **1068**, the heat exchanger assembly **1074**, a pipe from the pump to the spray manifold **1062**, a spray manifold **1028**, a wet side fan **1022**, access panel **1066** and a

moisture eliminator **1070**.

Figure 15 shows a side view of unit described in Figure 5, with the intake on left. The foundation **1024**, wet side air flow in **1016**, housing **1068** and wet side fans **1022** are shown.

5 Figure 16 shows a top view of the unit described in Figure 5 with wet side fans **1022** and housing **1068**.

Figure 17 shows a top view of the multi-stage unit shown in Figure 6 with n-series units and components **1076** indicated.

10 Figure 18 shows a psychrometric chart depicting various evaporative cycles (direct evaporative cooling, direct evaporative cooling with fogging, multistage indirect evaporative cooling and indirect evaporative cooling with air washer) with comparisons relating to air density.

Figure 19 shows plate dividers made with holes, including an end-on view **1078**, and cross section **1079**. Figure 20 shows plate dividers made with slats, including an
15 end-on view **1080** and a cross section **1081**. Figure 21 shows plate dividers made with reticulated foam, including an end-on view **1082** and a cross section **1083**. Figure 22 shows solid plate dividers, including an end-on view **1084** and a cross section **1085**.

Figure 23 shows an isometric section of unit depicted in Figure 9. It shows the wet side air inflow **1016** along with a float valve **1032**, a strainer for the pump **1086**,
20 sumps **1036**, the foundation **1024**, the heat exchanger assembly **1074**, the spray manifold **1028**, framework **1092**, intake air hood **1088**, a wet side fan **1022**, intake air filters **1090**, moisture eliminator **1070**, air washer cover for the primary media **1046**, air washer cover for the secondary media **1048**, air discharge housing **1096**, air washer spray manifold **1044**, primary evaporative media **1050**, and the secondary
25 evaporative media **1052**.

Figure 24 shows an isometric section of unit described in Fig. 9 with airflow path depicted **1094**. The airflow **1094** on the path A to B is the airflow entering the heat exchanger and flowing through to the plenum. On the next leg of flow, on path B to C, the flow is downward in the plenum. On the next leg of airflow, the path is C to D, from
30 the plenum to the sump area. On the last leg of airflow shown, the path is from D to E, from the sump area upward through the wet side of the heat exchanger, into the atmosphere.

Figure 25 shows a section of a unit described in Figure 9, as viewed from intake end. It shows the foundation **1024**, a pump for the spray manifold **1058**, a pipe

from the pump to the spray manifold **1062**, sumps **1036**, the heat exchanger assembly **1074**, the spray manifold **1028**, the framework **1092**, wet side fans **1022**, moisture eliminator **1070**, an air washer spray manifold **1044**, primary evaporative media **1050**, and the secondary evaporative media **1052**.

5 Figure 26 shows a section of a unit described in Figure 9, as viewed from discharge end. It shows the foundation **1024**, a pump for the spray manifold **1058**, a pipe from the pump to the spray manifold **1062**, sumps **1036**, the heat exchanger assembly **1074**, the spray manifold **1028**, the framework **1092**, wet side fans **1022**, moisture eliminator **1070**, primary evaporative media **1050**, and the secondary
10 evaporative media **1052**.

Figure 27 shows a psychrometric chart depicting the thermodynamic path of an "n"-series arrangement of heat exchangers, for $n = 4$. In the progressive lowering of the temperature, from point 1 to point 2 to point 3 to point 4, the progressively smaller enthalpy changes are denoted, Δh_1 , Δh_2 , Δh_3 , and Δh_4 , where $\Delta h_1 > \Delta h_2 > \Delta h_3 > \Delta h_4$. This
15 illustrates that the effect of n-stages converges rapidly during the first four to six multi-stages.

Figure 28 shows a section of a unit described in Figure 9. It shows the foundation **1024**, a pump for the spray manifold **1058**, sumps **1036**, the heat exchanger assembly **1074**, the spray manifold **1028**, the framework **1092**, wet side
20 fans **1022**, moisture eliminator **1070**, an air washer spray manifold **1044**, air washer cover **1046** for the primary evaporative media, air washer cover **1048** for the secondary evaporative media and the air discharge housing **1096**. It also shows the wet side air inflow **1016**, the dry side inward airflow **1014**, the dry air outflow **1018**, pumps for the spray media **1060**, intake air hood **1088** and intake air filters **1090**.

25 Advantageously, this invention utilizes more airflow **1016** (Figure 28) on the wet side as compared to the dry side **1014**. This greater airflow on the wet side relative to the dry side creates a much higher thermal efficiency. Air from the wet side, which is not recirculated to the dry side, in circumstances where that is done, or otherwise utilized, is dumped to the atmosphere **1020** (Figure 5). In this
30 invention, there is no need to keep the airflow on the wet side comparable to that on the dry side. Therefore, the relative rate of flow of wet side air to dry side airflow can be chosen to attempt a highest feasible efficiency.

While in the past heat exchangers tended to utilize tubes or a semi-rectangular shape arranged vertically and tended to have header sheets at each end to keep the primary and secondary air flows separated, the new shape can be utilized in either vertical or horizontal applications.

5 When used as a pre-cooler for gas turbines the preferred method is to have the tubes horizontal, in the direction of airflow to the gas turbine intake. In this situation, the length of the plates can be adjusted to provide sound attenuation as "tuned lengths" to damp out specific frequencies. Additionally, the heat exchanger can be made up of two or more sections each of a different length so that several frequencies can be
10 damped out. A further embodiment utilizes a space or plenum between heat exchanger sections, these sections acting as expansion chambers to further dampen the noise, and sound attenuation devices can also be installed in these expansion chambers.

 What is described is a complete, unique, system for cooling and cleaning the air being used by a gas turbine. This cycle is far more efficient than any system now
15 on the market or even contemplated in any theoretical literature. The psychrometric chart (Figure 11) shows graphically how this technology advantageously compares with other technologies and how on a normal warm day in semi-arid regions can provide air at a density almost equal to ISO conditions. From the starting point of nominal ambient conditions of temperature of about 100°F (point A, Figure 18) and a
20 wet bulb temperature of about 70°F (point A, Figure 18) with a relative humidity of about 22% (point A, Figure 18), one can reach a dry bulb temperature for the cooled air of about 65°F (point E, Figure 18). Starting at (point A, Figure 18), one can move along a line of constant moisture or water content to (point E, Figure 18) by indirect evaporative cooling. In the indirect evaporative cooling, moisture is not being taken
25 out of the "dry" side air. Direct evaporative cooling, where the enthalpy, or sensible heat is constant is not added, leads to a wet bulb temperature of about 58°F (point F, Figure 18). In the multi-stage process, under the same approximate conditions, one may achieve about a dry bulb temperature of about 53.5 °F, with a less consumption of energy, because the n-stage process operates more efficiently

30 While the invention herein disclosed has been described by means of specific embodiments and applications thereof, numerous modifications and variations could be made thereto by those skilled in the art without departing from the scope of the invention set forth in the claims.

THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE
PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. An evaporative apparatus comprising:
 - 5 (a) a multi-substage direct evaporative cooling stage;
 - (b) one or more air cleaning sub-stages of said multi-sub-stage direct evaporative stage;
 - (c) a first multi-stage indirect evaporative cooling heat exchanger;
 - (d) said first multi-stage indirect evaporative cooling heat exchanger
 - 10 configured to be coupled with a second multi-stage indirect evaporative cooling heat exchanger such that output of said first heat exchanger is fed to input of said second heat exchanger;
 - (e) cool output from said second and said first linked heat exchangers combination is substantially additive of cool outputs of said second and said first linked
 - 15 heat exchangers individually;
 - (f) multi-stage sumps wherein each sump stage, in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures;
 - (g) said separate sumps are thermally insulated from each other to
 - 20 maintain different sump temperatures.
2. The evaporative apparatus as in claim 1 further comprising:
 - (a) cascaded sumps; wherein makeup water is supplied to a last sump according to a measured level in a first sump;
 - (b) said cascaded sumps connected by a standpipe configured to
 - 25 transfer water between at least two sumps.
3. The evaporative apparatus as in claim 2 further comprising:
 - an external ambient water supply for automatically maintaining designated sump water levels.

4. The evaporative apparatus as in claim 2 further comprising:
a water supply from an air washer stage of said evaporative apparatus for automatically maintaining designated sump water levels.

5. The evaporative apparatus as in claim 1 further comprising:
5 a multistage indirect evaporative cooling heat exchanger; wherein at least a last stage of said heat exchanger utilizes a portion of a dry side air flow to enter the wet side evaporative airflow; wherein said air has been cooled relative to, and is at a lower wet bulb temperature than, the ambient air.

6. The evaporative apparatus as in claim 5 further comprising:
10 a multi-stage indirect evaporative cooling heat exchanger further comprising:

(a) a dry side wherein originally ambient air is cooled without direct contact with evaporating water;

(b) a wet side wherein air is used to directly evaporate water;
15 thereby producing cooling;

(c) a thermally conductive material separating said dry side and said wet side; thereby the cooler side tends to warm and the warmer side tends to cool;

(d) dry side and wet side channels formed by thermally
20 conductive material; wherein the placement of said material forms channels for guiding said dry side air and said wet side air; thereby said wet air containing moisture of some amount and said dry air containing moisture of some other or same amount.

7. The evaporative apparatus as in claim 6 further comprising:
said dry side and wet side channels formed by placing in an opposed
25 sense, polygonal channeled pre-shaped sheets of thermally conductive material together.

8. The evaporative apparatus as in claim 6 further comprising:
said dry side and wet side channels formed by placing in an opposed sense,
sinusoidal-corrugated channeled pre-shaped sheets of thermally conductive material
together.

5 **9.** The evaporative apparatus as in claim 7 or 8 further comprising:
said sheets separated to a required distance by separators inserted between
said sheets.

10. The evaporative apparatus as in claim 7 or claim 8 further comprising:
said sheets fabricated from one or more materials selected from the
10 group consisting of steel, galvanized iron, galvanized steel, stainless steel, thermally
conductive plastic, thermally conductive ceramic, metal coated with paint, metal coated
with varnish, metal coated with plastic, metal coated with ceramic, metal coated with
glass, metal coated with diamond-like coating, titanium, thermally conductive composite,
aluminum, magnesium, copper and silver.

15 **11.** The evaporative apparatus as in claim 6 further comprising:
portions of said wet side and dry side channels further comprising
(a) air turbulence generation assistants;
(b) moist air turbulence generation assistants;
(c) water film surface increase assistants;
20 (d) water film droplet formation assistants.

12. The evaporative apparatus as in claim 11, wherein the assistants further
comprise:
(a) embossed surface of sheets forming wet side channels;
(b) tabs partially cut and foldably bent from sheets forming wet side
25 channels;
(c) tabs attached to said sheets forming wet side channels;

(d) material attached; wherein said material is in a structurally open form.

13. The evaporative apparatus as in claim **12**, wherein said material attached further comprises:

5 a material selected from the group comprising sintered metal powder and foamed metal.

14. The evaporative apparatus as in claim **1** further comprising:

(a) one or more water-spray direct evaporative cooling stage;

(b) a final wetted media stage; wherein air flowing through one or
10 more media of the evaporative apparatus is cleaned;

15. The evaporative apparatus as in claim **1** further comprising:

(a) a water purifier, comprising:

(b) a water evaporator heated by a hot turbine exhaust, so as to distill water supplied thereto;

15 (c) a condenser disposed in the path of the wet side exhaust of the indirect evaporative heat exchanger for liquefying said distilled water vapor;

(d) means for conveying distilled water vapor from the evaporator to the condenser; and

(e) means for conveying liquefied water from the condenser to said
20 water spray.

16. An evaporative apparatus for cooling comprising:

(a) a multi-stage indirect evaporative cooling heat exchanger;

(b) one or more water-spray direct evaporative cooling stage;

(c) a final wetted media stage; wherein air flowing through one or
25 more media of the evaporative apparatus is cleaned;

(d) multi-stage sumps wherein each sump stage, in a corresponding relationship to a stage of said multi-stage indirect evaporative cooling heat exchanger, can contain sump water at different temperatures.

17. A method for making an evaporative apparatus comprising the steps of:

- 5 (a) assembling a first multi-stage indirect evaporative cooling heat exchanger;
- (b) linking said first multi-stage indirect evaporative cooling heat exchanger with a second multi-stage indirect evaporative cooling heat exchanger;
- (c) feeding output of said first heat exchanger to input of said second
- 10 heat exchanger;
- (d) adding cool output from said second and said first linked heat exchangers combination so as to achieve a cooling substantially additive of cooling of said second and said first linked heat exchangers, individually;
- (e) containing sump water in multi-stage sumps wherein each sump
- 15 stage, in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures;
- (f) insulating said separate sumps thermally from each other; and
- (g) maintaining different sump temperatures.

18. The method for making an evaporative apparatus as in claim **17** further comprising the steps of:

- (a) cascading sumps;
- (b) supplying makeup water to a last sump according to a measured
- level in a first sump;
- (c) connecting said cascaded sumps by a standpipe;
- 25 (d) transferring water between at least two sumps.

19. The method for making an evaporative apparatus as in claim 17 further comprising the step of:

supplying external ambient water for automatically maintaining designated sump water levels.

5 20. The method for making an evaporative apparatus as in claim 17 further comprising the steps of:

supplying water from an air washer stage of said evaporative apparatus for automatically maintaining designated sump water levels.

10 21. The method for making an evaporative apparatus as in claim 17 further comprising the steps of:

(a) utilizing, a portion of a dry side air flow from a at least a last stage of a multistage indirect evaporative cooling heat exchanger to enter the wet side evaporative airflow;

15 (b) cooling said air relative to ambient air, whereby said air is at a lower wet bulb temperature than ambient air.

22. The method for making an evaporative apparatus as in claim 17 further comprising the steps of:

fabricating a multi-stage indirect evaporative cooling heat exchanger further comprising the steps of:

20 (a) utilizing a dry side wherein originally ambient air is cooled without direct contact with evaporating water;

(b) utilizing a wet side wherein air is used to directly evaporate water; thereby producing cooling;

25 (c) utilizing a thermally conductive material separating said dry side and said wet side; thereby the cooler side tends to warm and the warmer side tends to cool;

(d) forming dry side and wet side channels from thermally conductive material;

(e) placing said material;

(f) forming channels for guiding said dry side air and said wet side air; thereby said wet air containing moisture of some amount and said dry air containing moisture of some other or same amount.

5 **23.** The method for making an evaporative apparatus as in claim 17 further comprising the steps of:

(a) forming said dry side and wet side channels

(b) placing in an opposed sense, polygonal channeled pre-shaped sheets of thermally conductive material together.

10 **24.** The method for making an evaporative apparatus as in claim 22 further comprising the steps of:

(a) forming said dry side and wet side channels

(b) placing in an opposed sense, sinusoidal corrugated channeled pre-shaped sheets of thermally conductive material together.

15 **25.** The method for making an evaporative apparatus as in claim 23 or 24 further comprising the step of:

inserting separators between said sheets to set a required distance of separation.

20 **26.** The method for making an evaporative apparatus as in claim 23 or 24 further comprising the step of:

fabricating said sheets from one or more materials selected from the group consisting of steel, galvanized iron, galvanized steel, stainless steel, thermally conductive plastic, thermally conductive ceramic, metal coated with paint, metal coated with varnish, metal coated with plastic, metal coated with ceramic, metal coated with glass, metal
25 coated with diamond-like coating, titanium, thermally conductive composite, aluminum, magnesium, copper and silver.

27. The method for making an evaporative apparatus as in claim **22** further comprising the steps of:

- (a) generating air turbulence with turbulence producing assistants;
- (b) generating moist air turbulence with turbulence producing
5 assistants;
- (c) increasing water film surface with surface increasing assistants;
- (d) forming water film droplets with droplet forming assistants.

28. The method for making an evaporative apparatus as in claim **27**, further comprising the steps of:

- (a) embossing surface of sheets forming wet side channels;
- (b) cutting tabs partially and folding and bending said tabs from sheets
10 forming wet side channels;
- (c) attaching other tabs to said sheets forming wet side channels;
- (d) attaching material; wherein said material is in a structurally open
15 form.

29. The method for making an evaporative apparatus as in claim **28** further comprising the step of:

selecting a material from the group comprising sintered metal powder and foamed metal.

30. The method for making an evaporative apparatus as in claim **27** further comprising the steps of:

- (a) assembling a multi-stage indirect evaporative cooling heat
20 exchanger
- (b) utilizing one or more water-spray direct evaporative cooling
25 stages;
- (c) utilizing a final wetted media stage; wherein air flowing through one or more media of the evaporative apparatus is cleaned;

(d) utilizing a multi-stage sump wherein each sump stage, in a corresponding relationship to a stage of said multi-stage, can contain sump water at different temperatures.

31. The method for making an evaporative apparatus as in claim 17 further comprising the steps of:

assembling a water purifier, further comprising:

(a) heating a water evaporator by the hot turbine exhaust, so as to distill water supplied thereto;

(b) disposing a condenser in the path of the wet side exhaust of the indirect evaporative heat exchanger for a purpose of liquefying;

(c) liquefying said distilled water vapor;

(d) conveying distilled water vapor from the evaporator to the condenser, by a means; and

(e) conveying liquefied water from the condenser to said water spray, by a means.

32. A pre-cooler for cooling intake air of a gas turbine, comprising:

(a) a multi-stage indirect evaporative cooling heat exchanger; wherein a first stage (1) is linked with a second stage (2) such that cool output of said first stage is feedable to input of said second stage; wherein cool output from said second and said first linked heat exchangers stages is approximately additive of cool outputs of said second and said first linked heat exchangers stages individually;

(b) a multi-substage direct evaporative cooling stage (1044, 1046, 1048); wherein there are one or more air cleaning sub-stages (1046, 1048) of said multi-substage direct evaporative stage; and

(c) multi-stage sumps (1036) wherein each sump stage is in a corresponding relationship to a stage of said indirect evaporative cooling heat exchanger, can contain sump water at different temperatures, and wherein said separate sumps (1036) are thermally insulated from each other; and wherein

(d) at least a last stage of said heat exchanger utilizes a portion (1072) of a dry side (1014) air flow to enter the wet side (1016) evaporative airflow, wherein said air has been sensibly cooled relative to, and is at a lower wet bulb temperature than, the ambient air.

5 **33.** The pre-cooler as in claim **32** wherein said heat exchanger is fabricated as two or more sections, wherein each section is of a different length.

34. The pre-cooler as in claim **33** further comprising a plenum between said heat exchanger sections, wherein said plenum(s) sections act as expansion chambers to further dampen the noise.

10 **35.** The pre-cooler as in claim **34** further comprising sound attenuation devices installed in said expansion chambers.

36. The pre-cooler as in claim **32**, comprising wet and dry side channels, parts of said wet and dry side channels further comprising at least one assistant (1008, 1010) selected from the group consisting of air turbulence generation assistants, moist air
15 turbulence generation assistants, water film surface increase assistants and water film droplet formation assistants.

37. The pre-cooler as in claim **32** further comprising dry side and wet side channels formed by placing in an opposed sense, pre-shaped sheets (1002, 1004) of thermally conductive material together, wherein said pre-shaped sheets are selected from
20 the group consisting of polygonal channeled pre-shaped sheets (1004) and sinusoidal-corrugated channeled pre-shaped sheets (1002).

38. The pre-cooler as in claim **37** further comprising horizontal tubes, in the direction of air flow to the gas turbine intake, wherein said length of the sheets (1002, 1004) is adjustable to provide sound attenuation to damp out specific frequencies.

25

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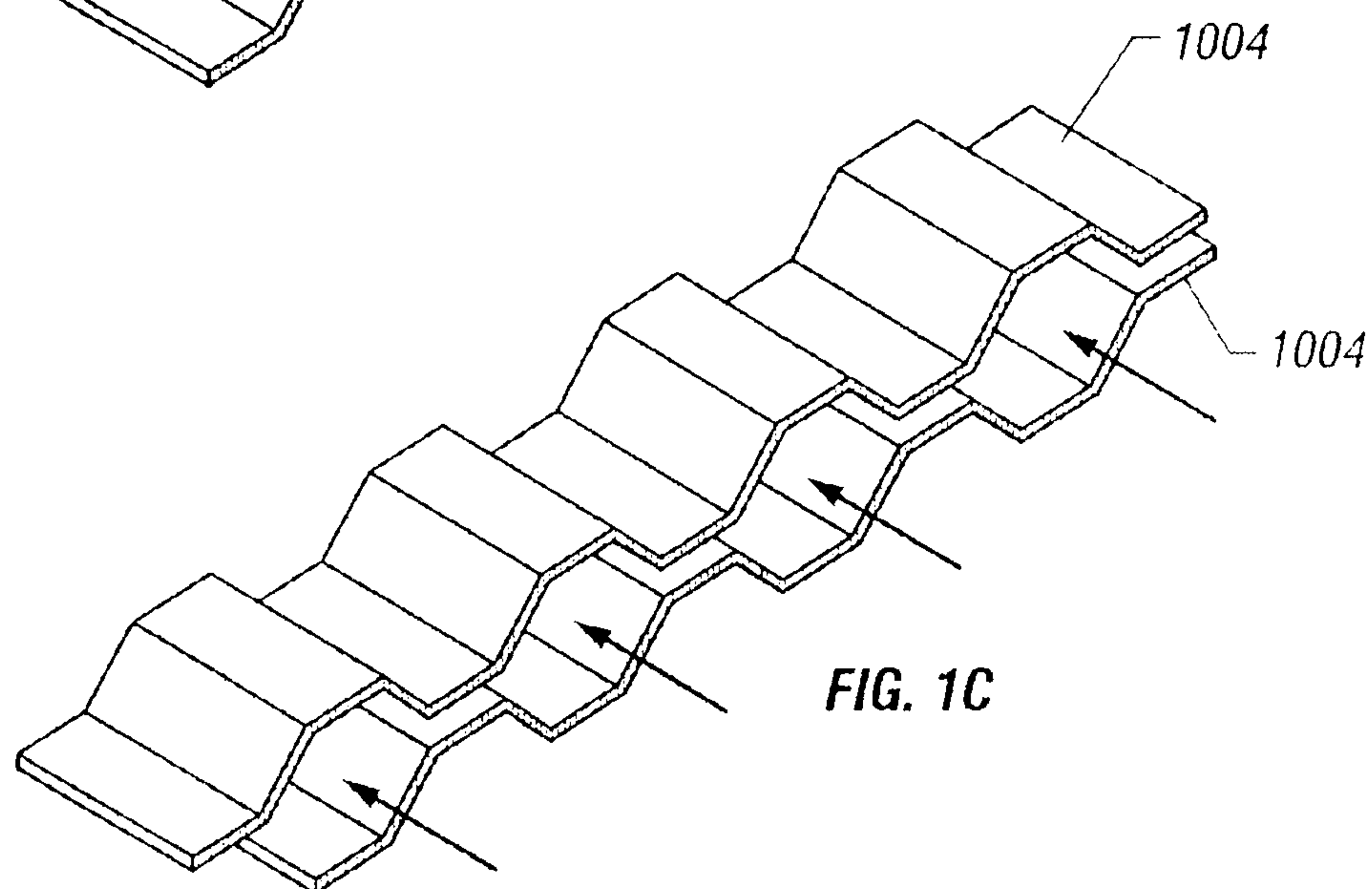
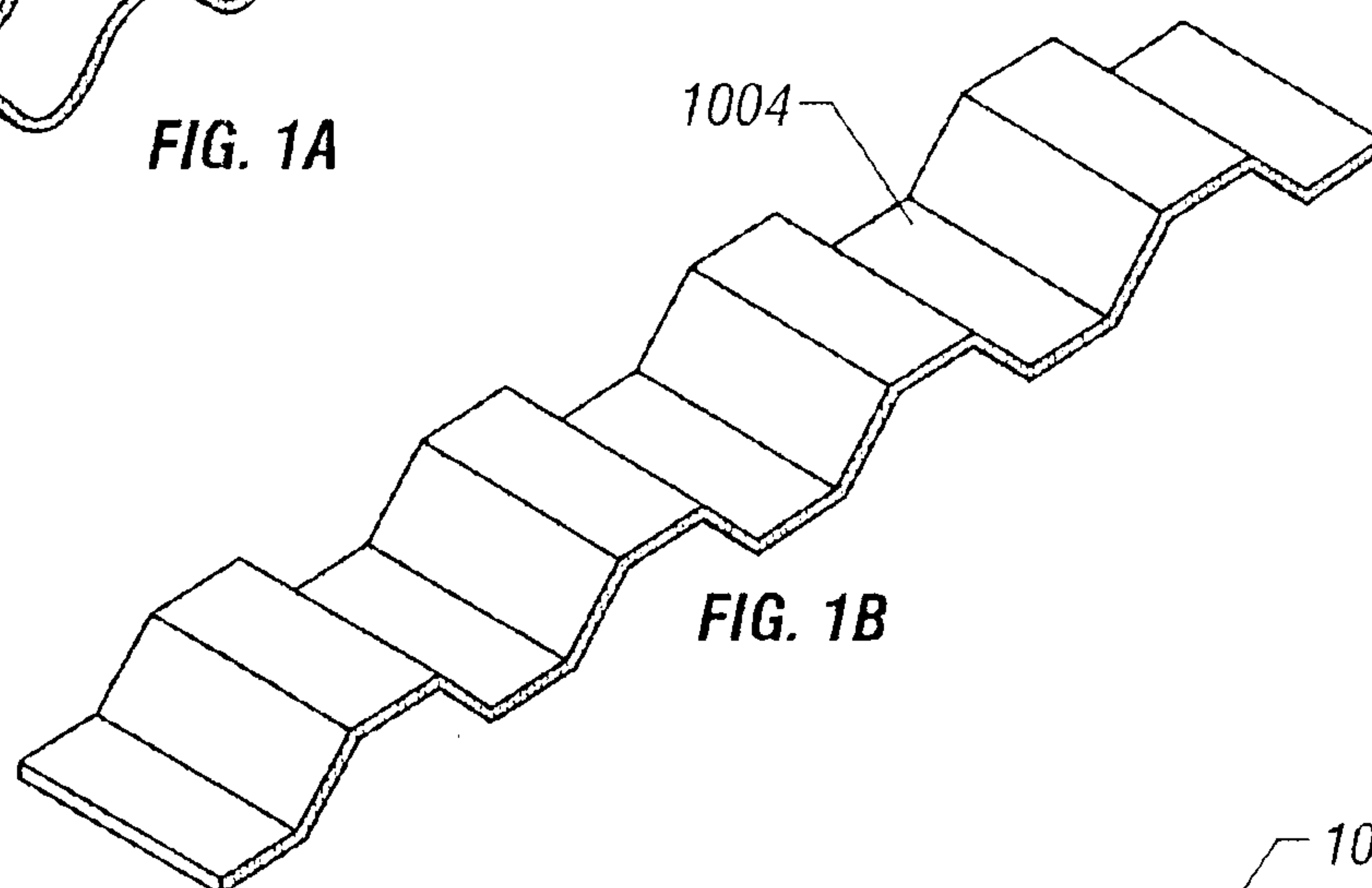
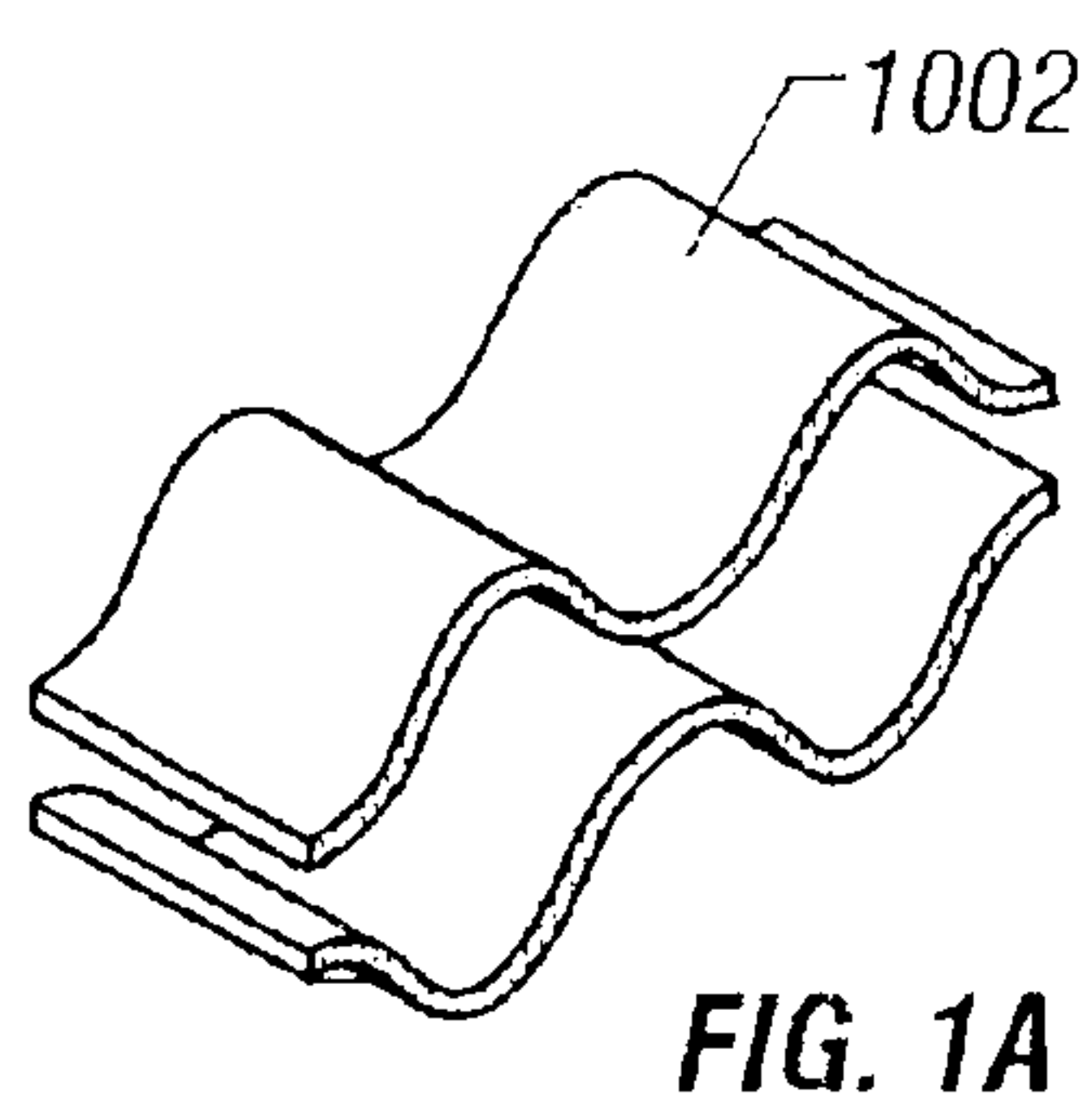
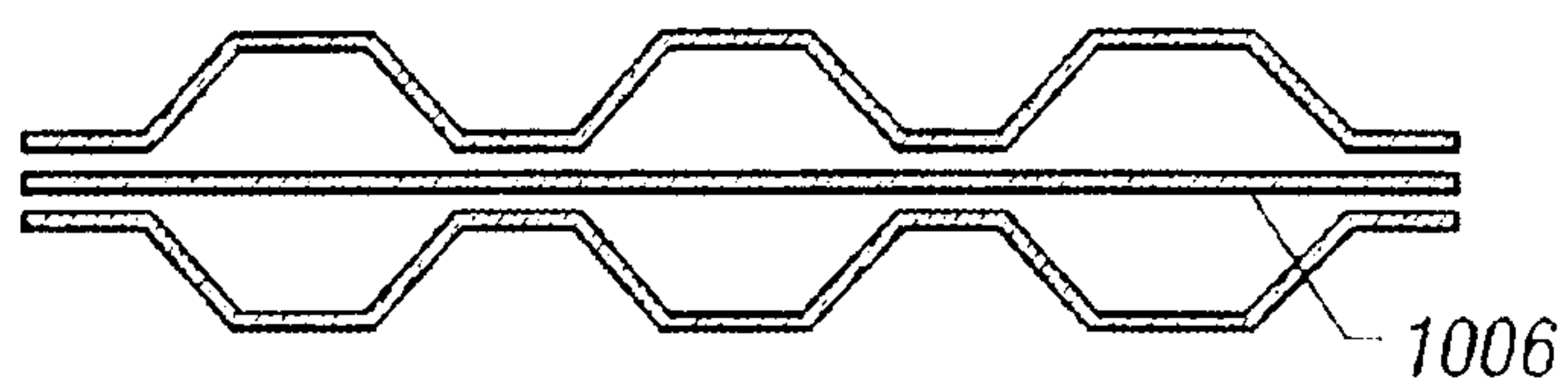


FIG. 1D



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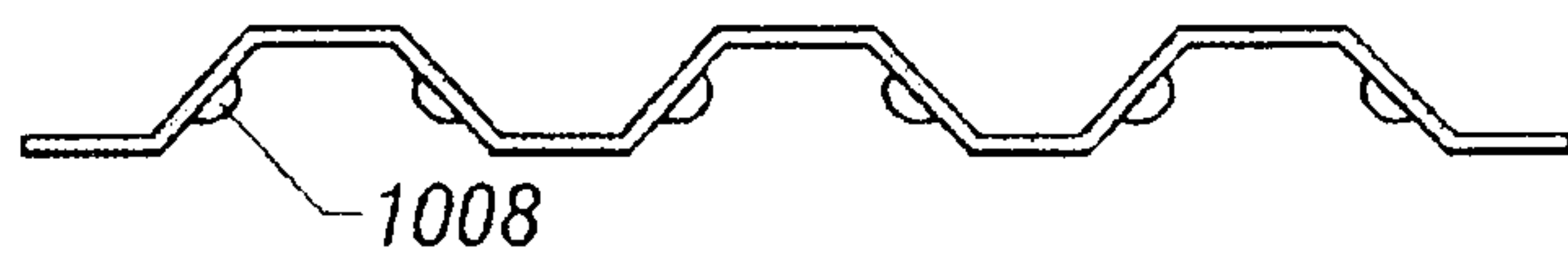


FIG. 2A

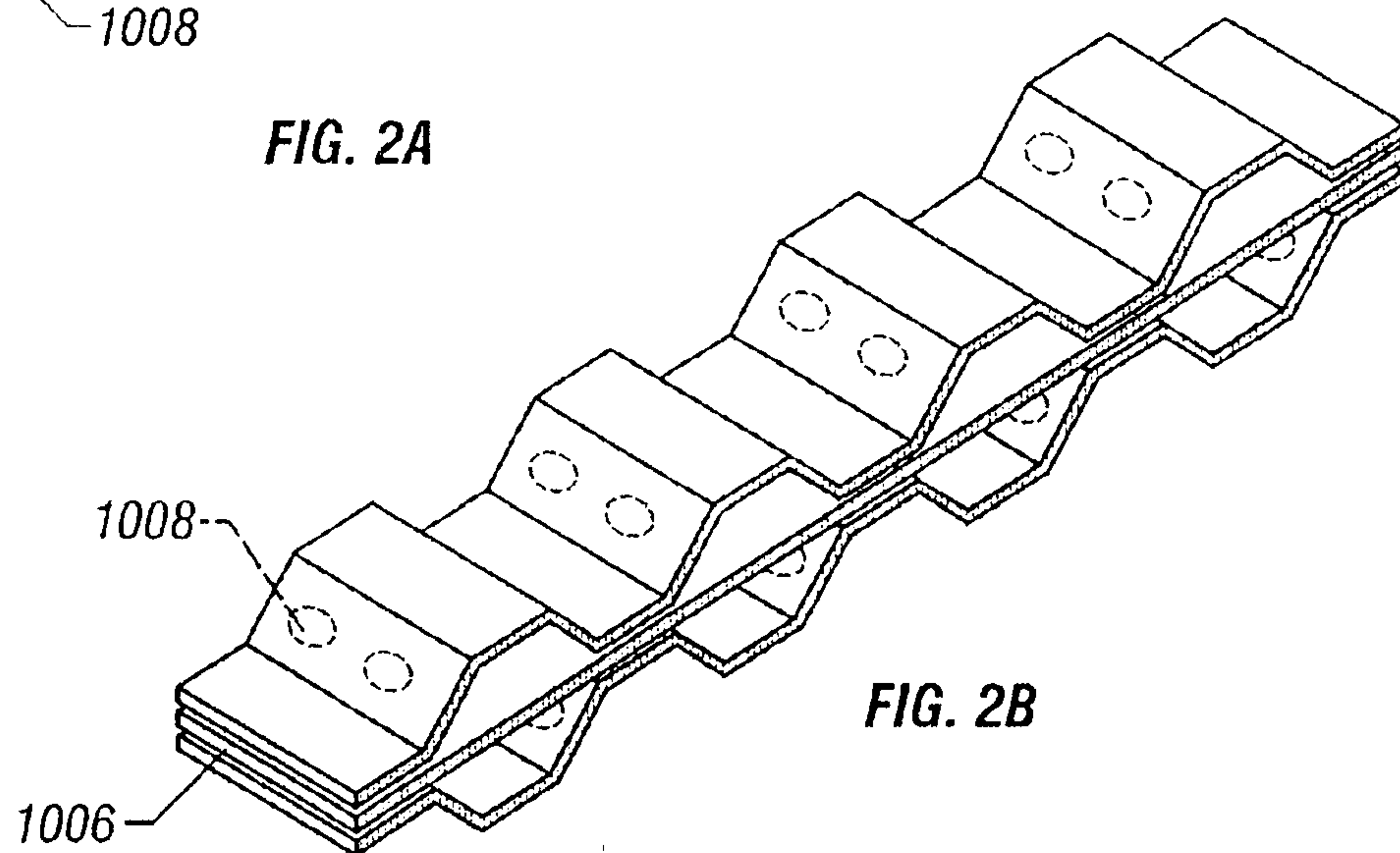


FIG. 2B

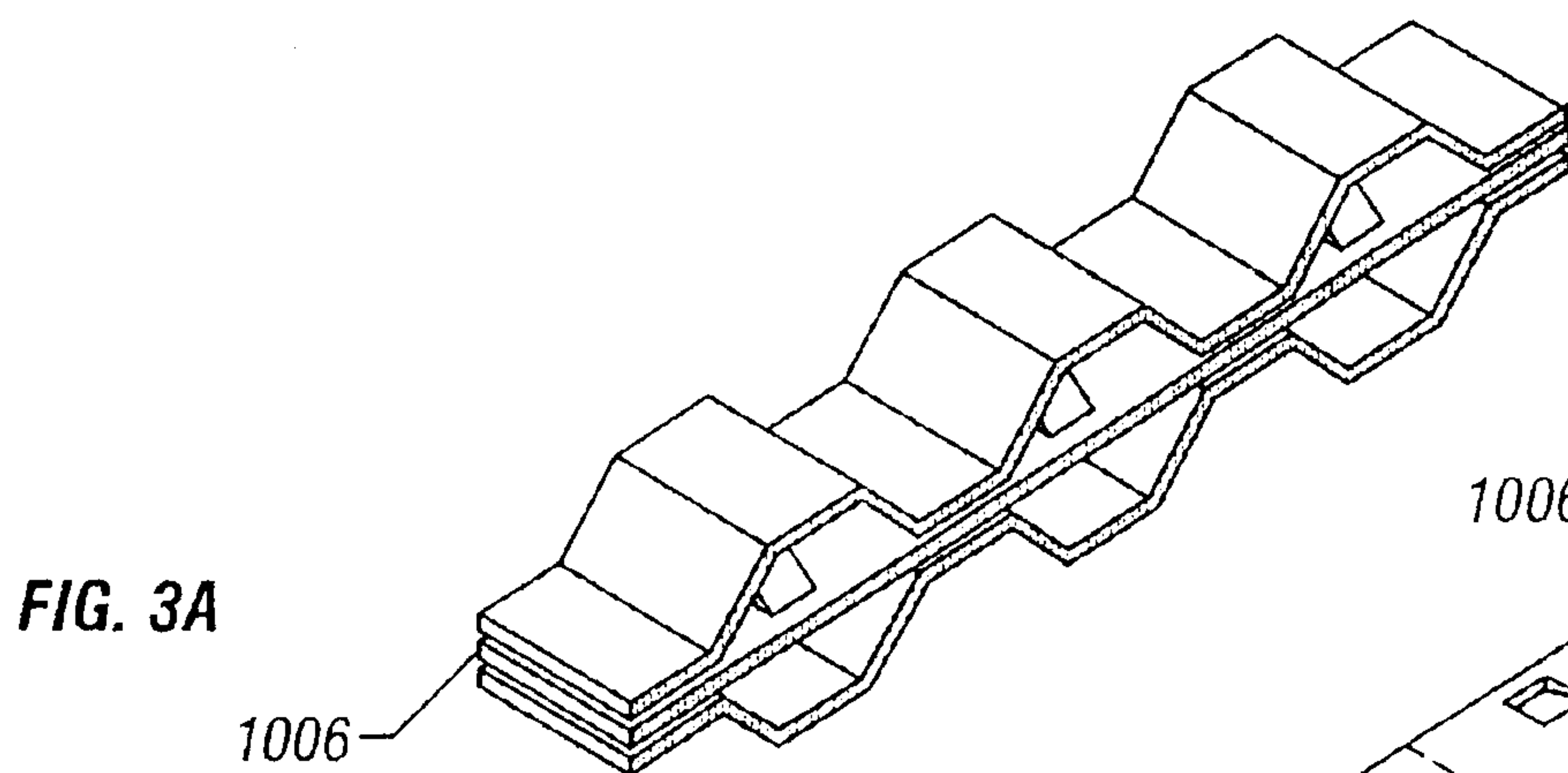


FIG. 3A

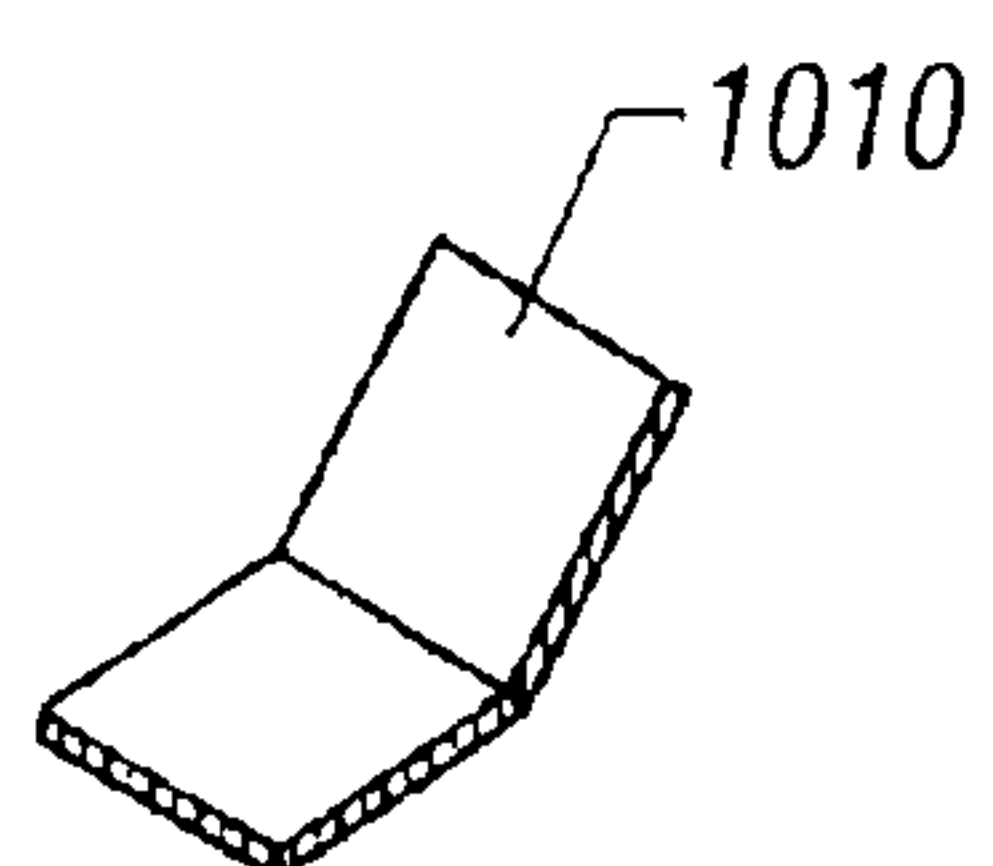


FIG. 3C

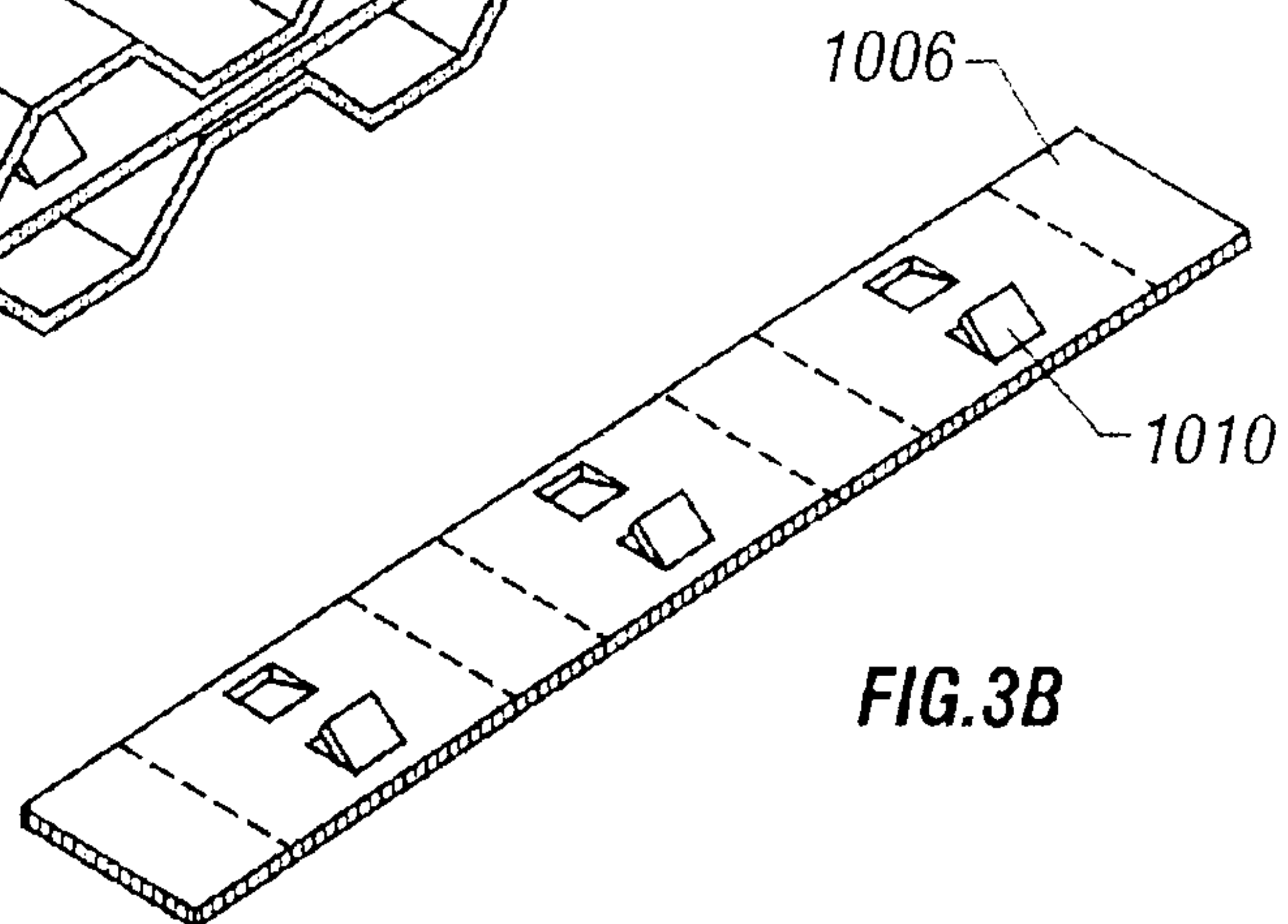
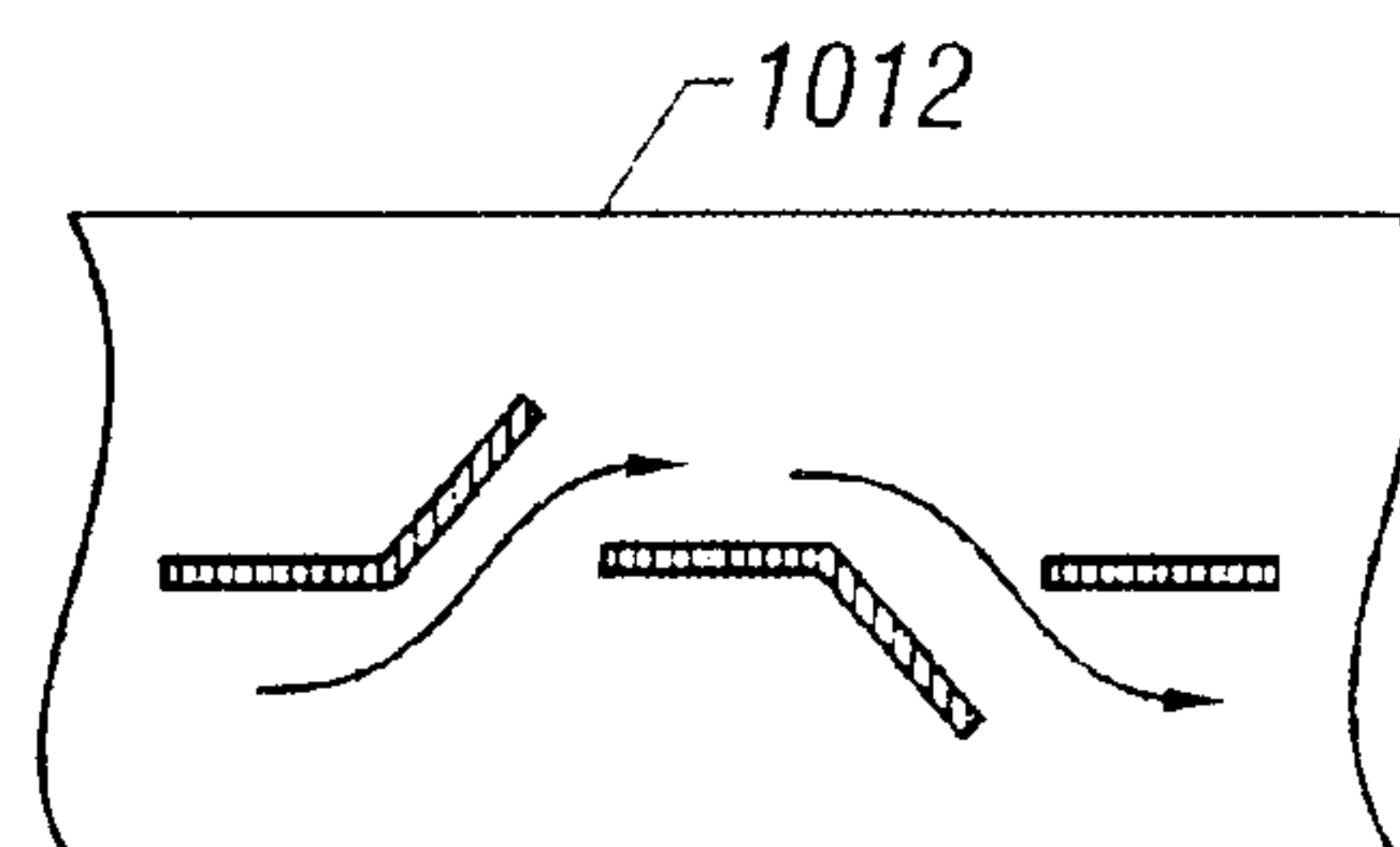


FIG. 3B

FIG. 3D



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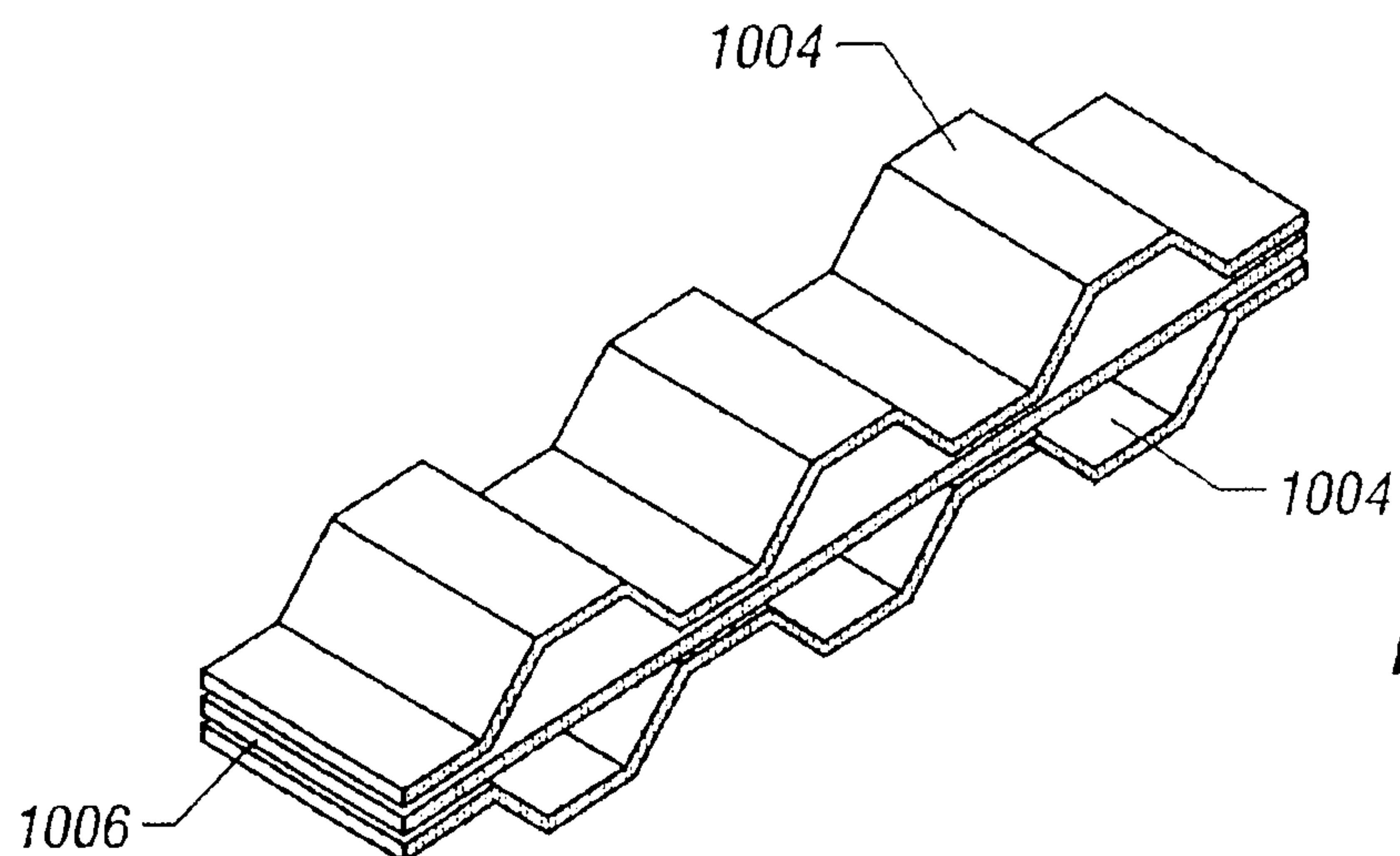


FIG. 4A

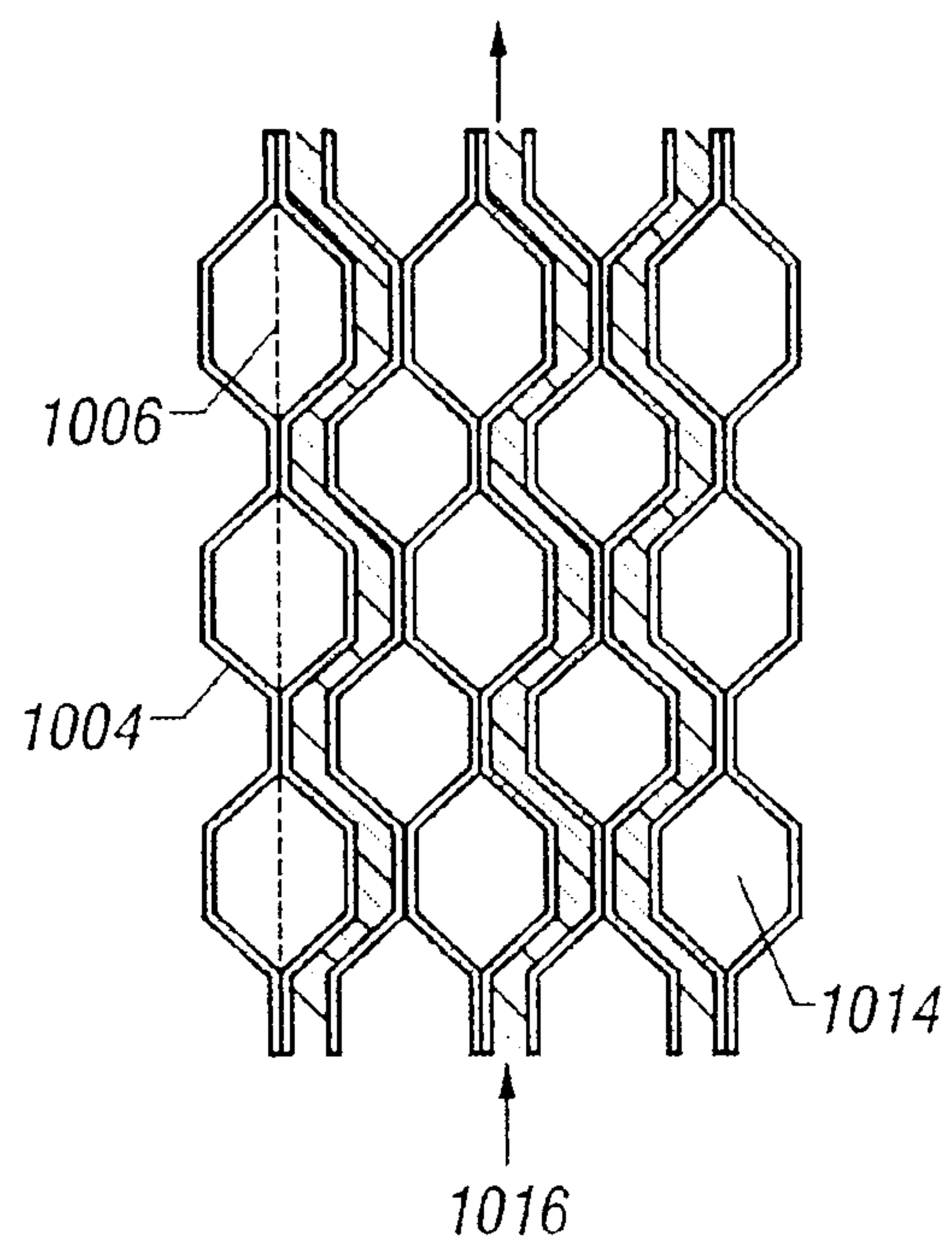


FIG. 4B

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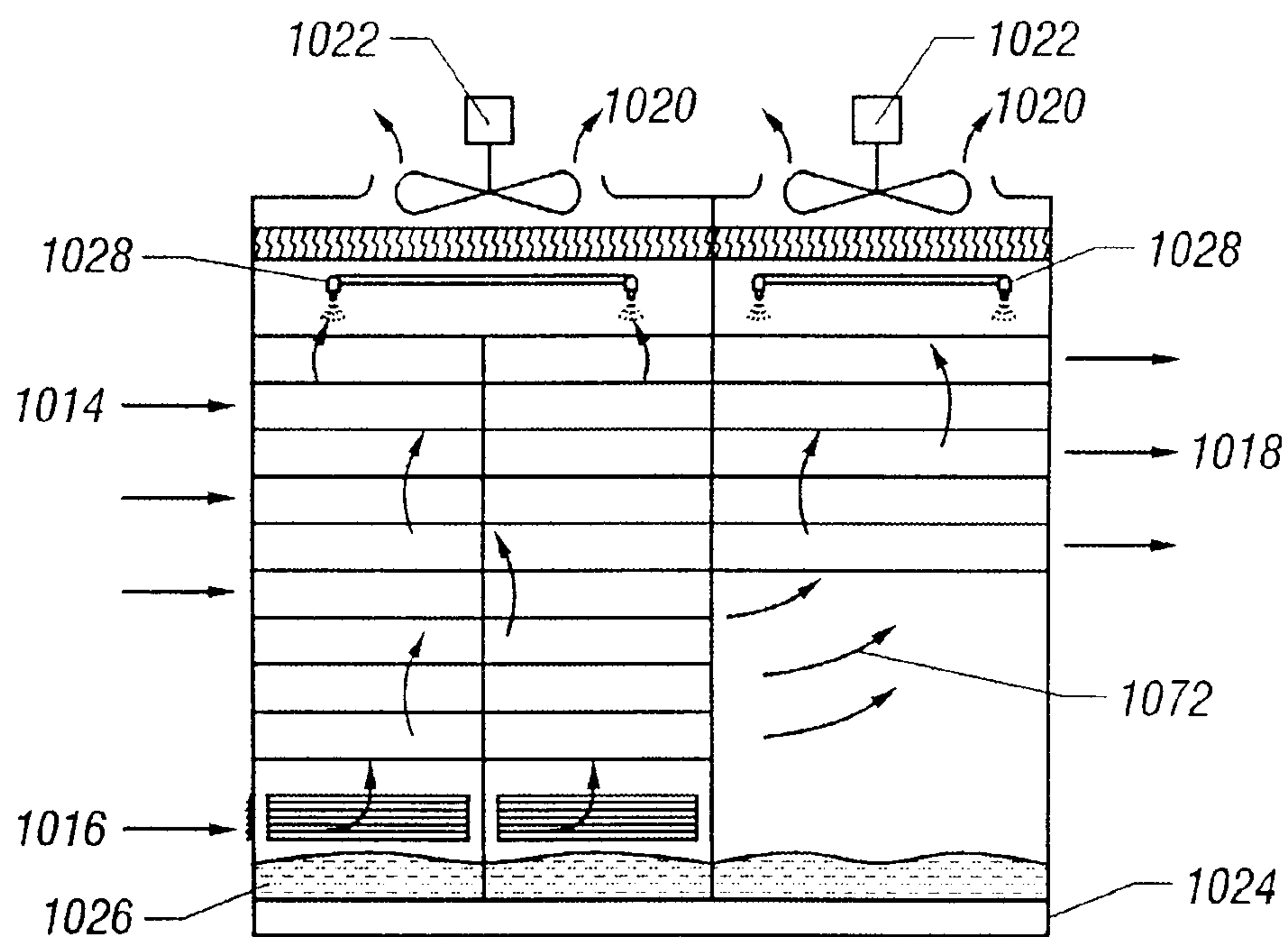


FIG. 5

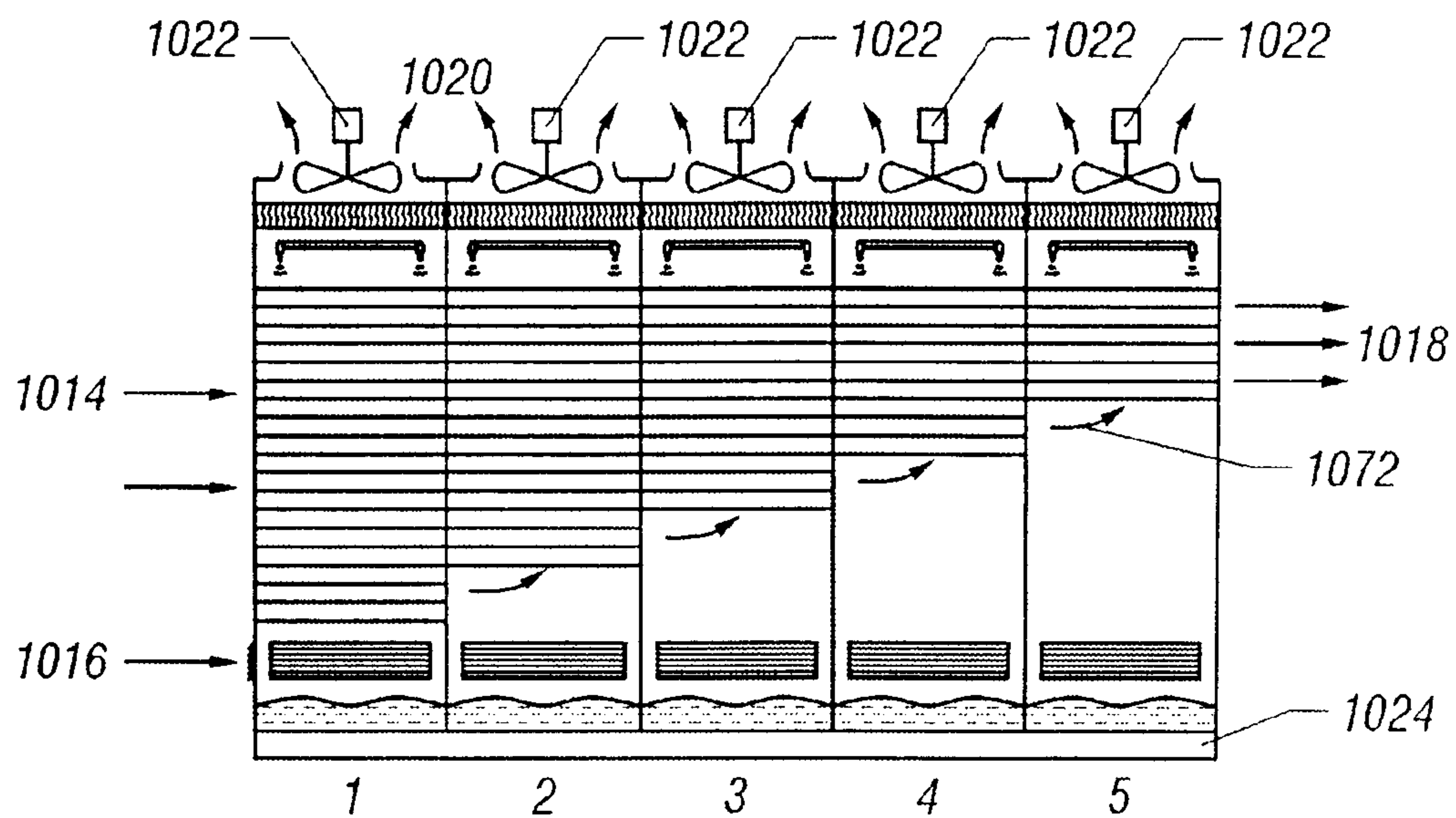


FIG. 6

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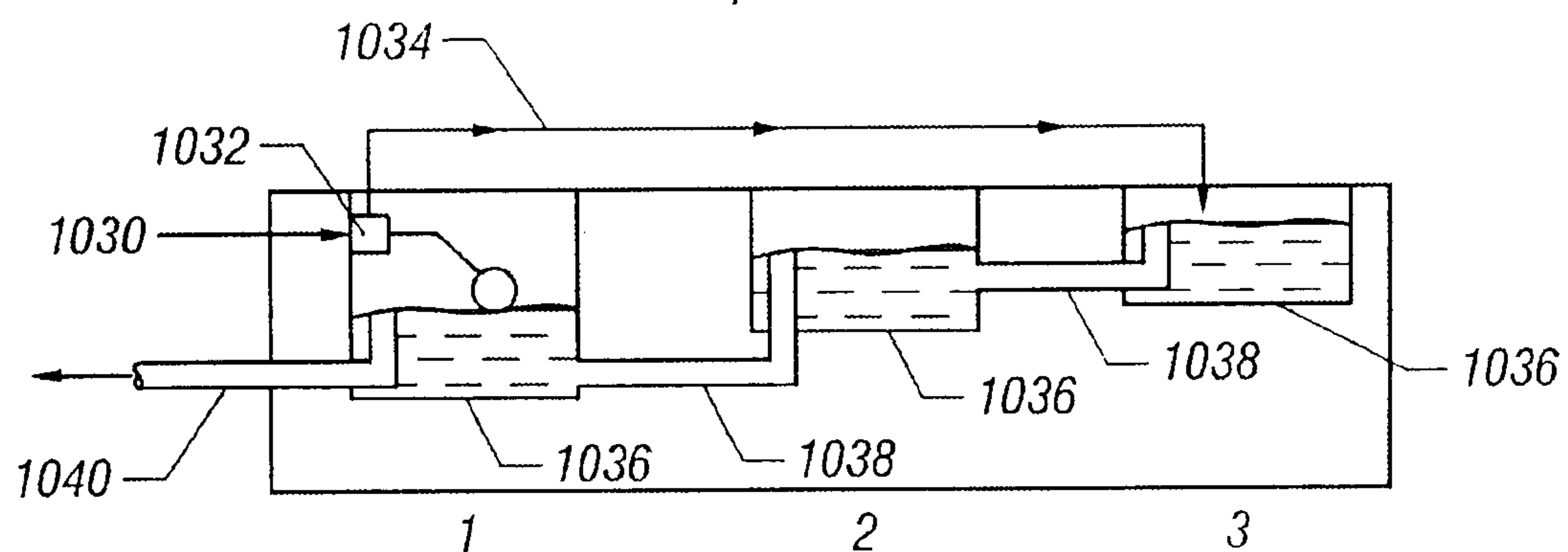


FIG. 7

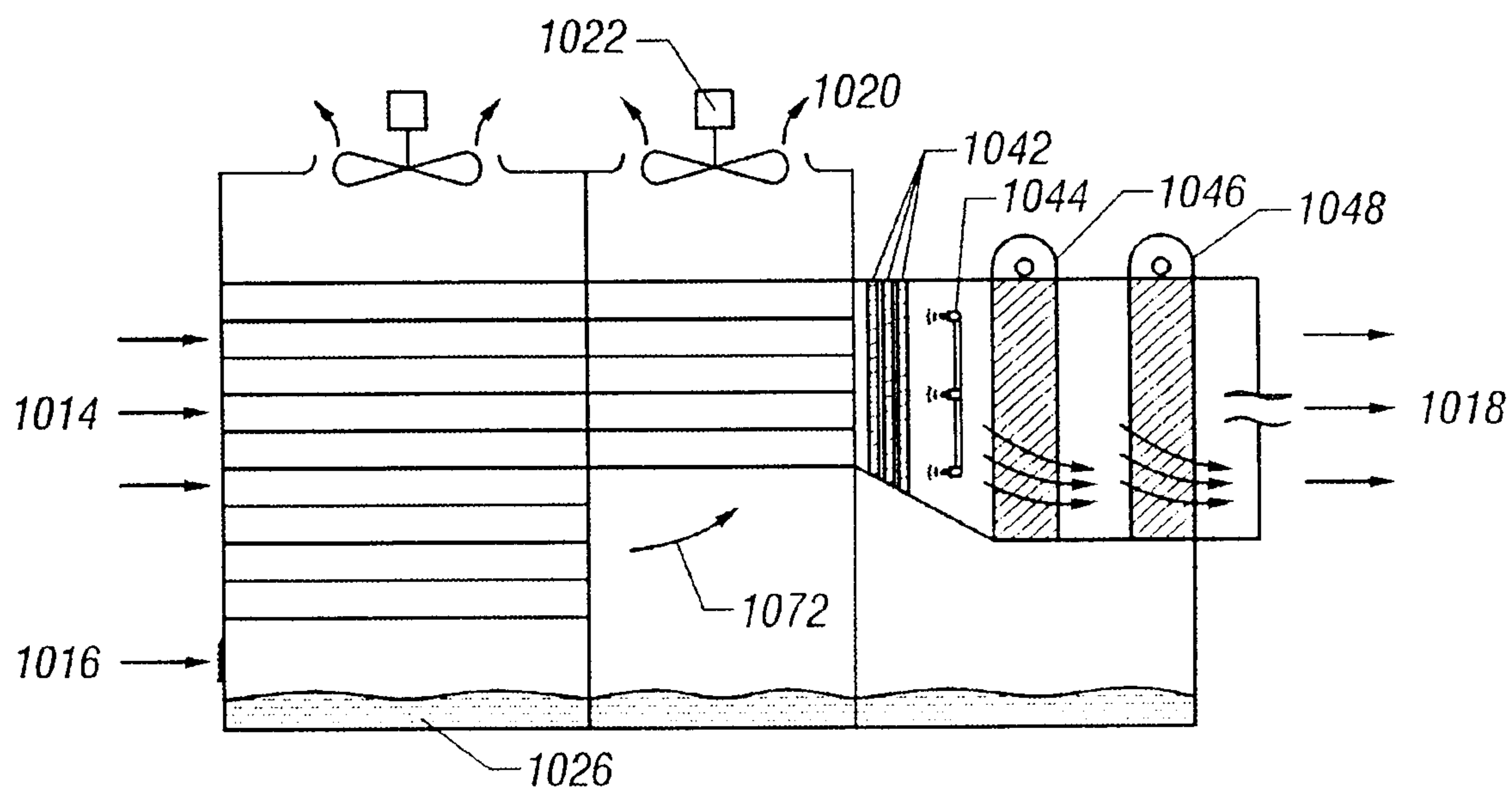


FIG. 9

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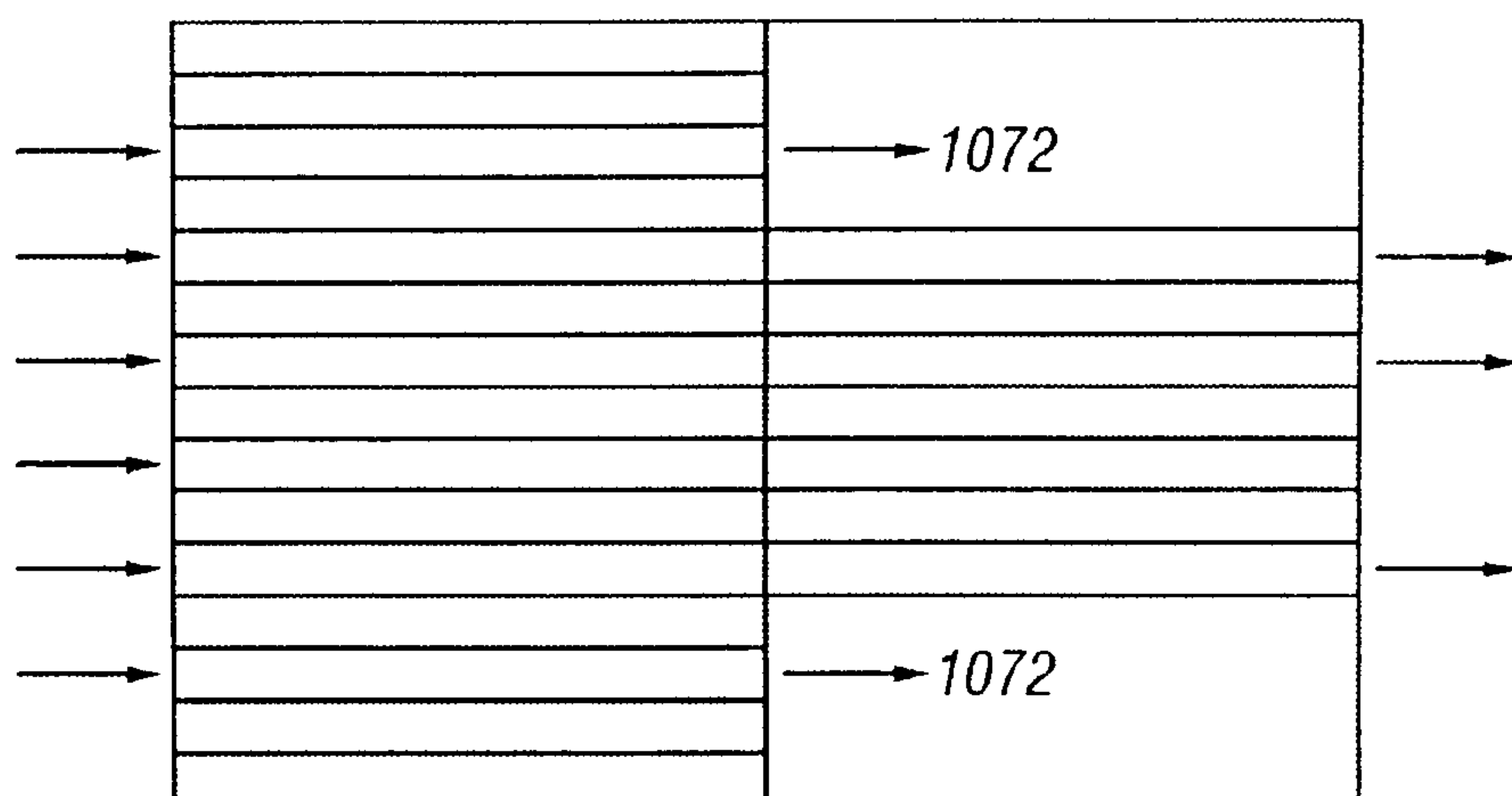


FIG. 8A

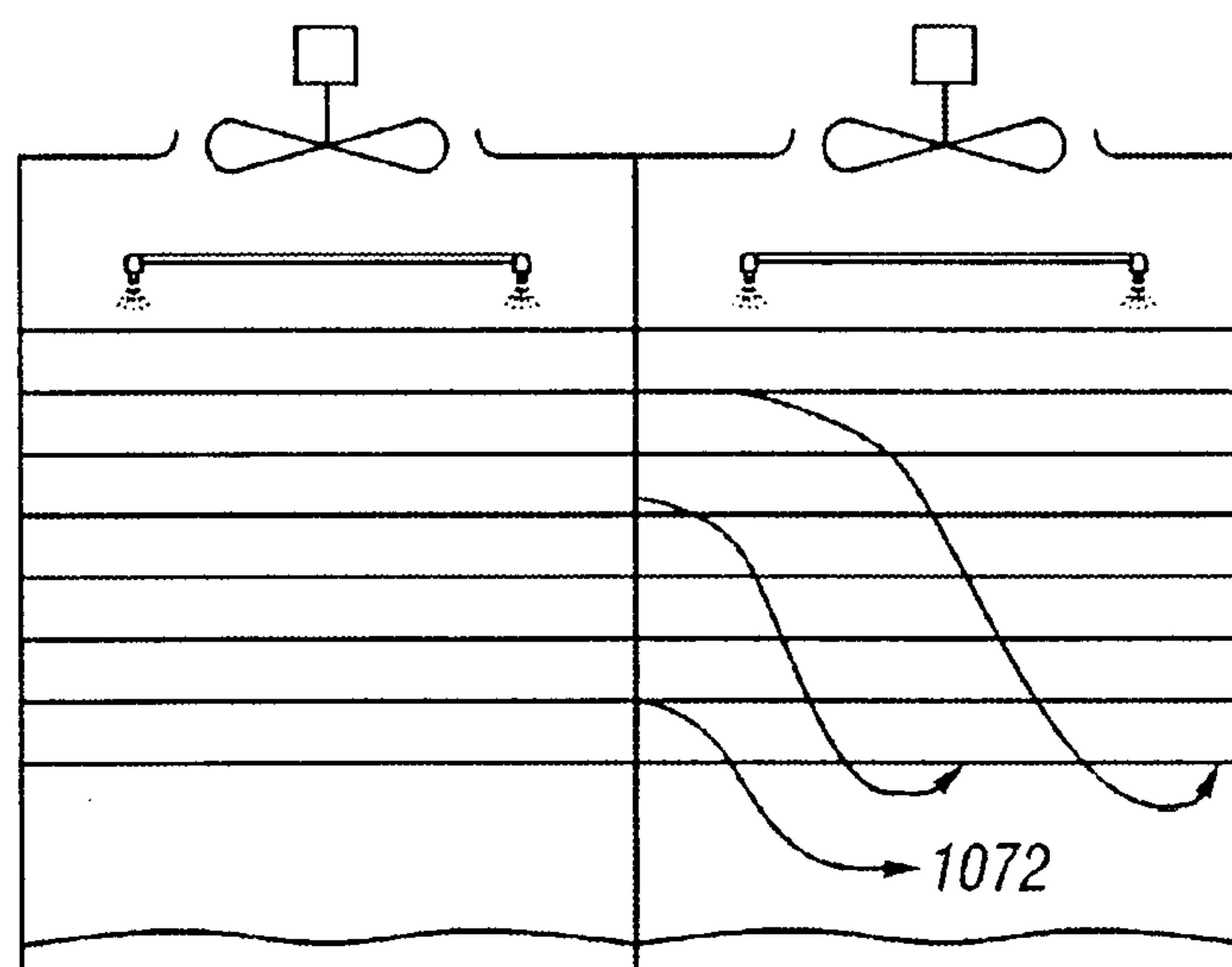


FIG. 8B

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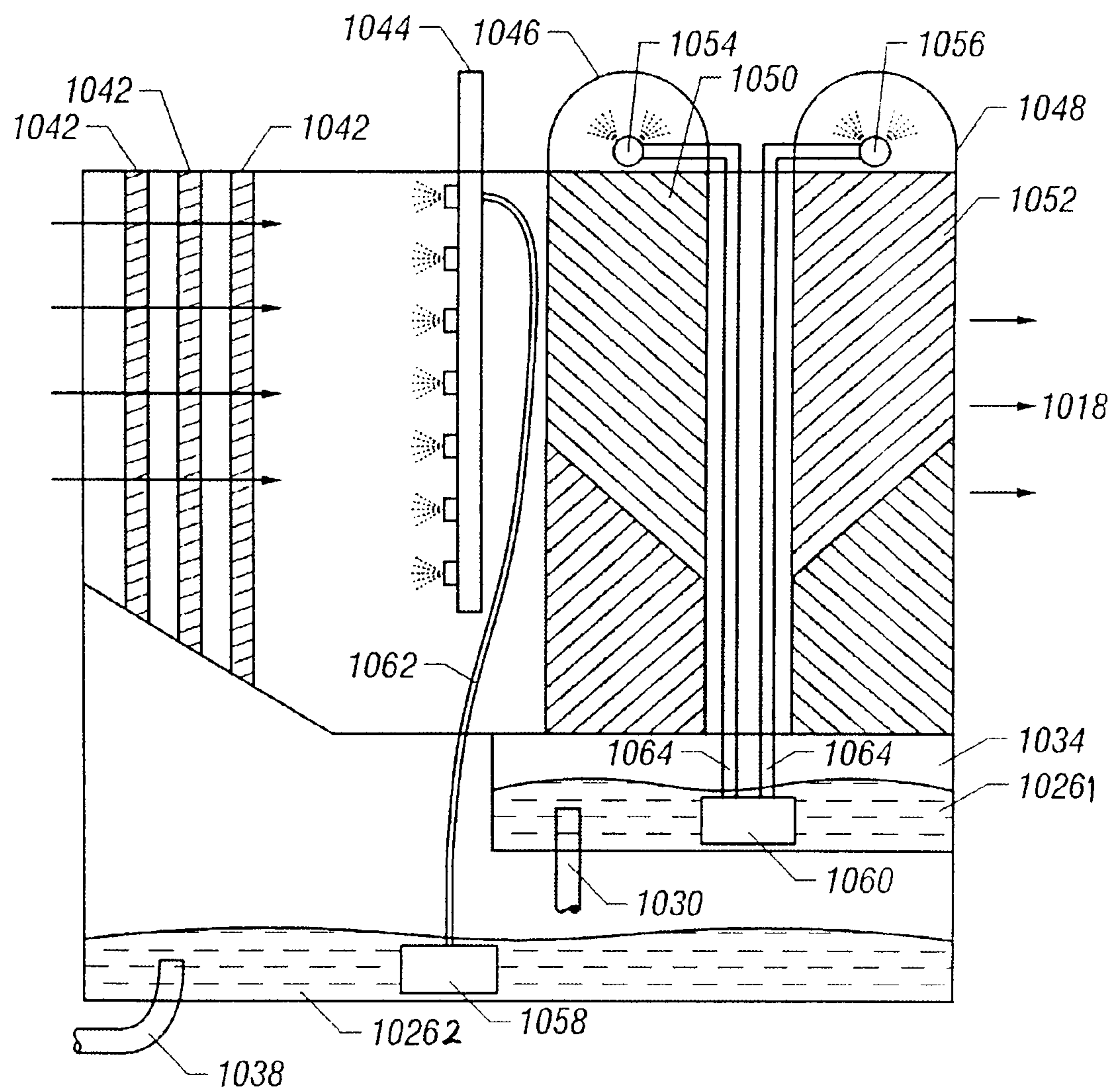


FIG. 10

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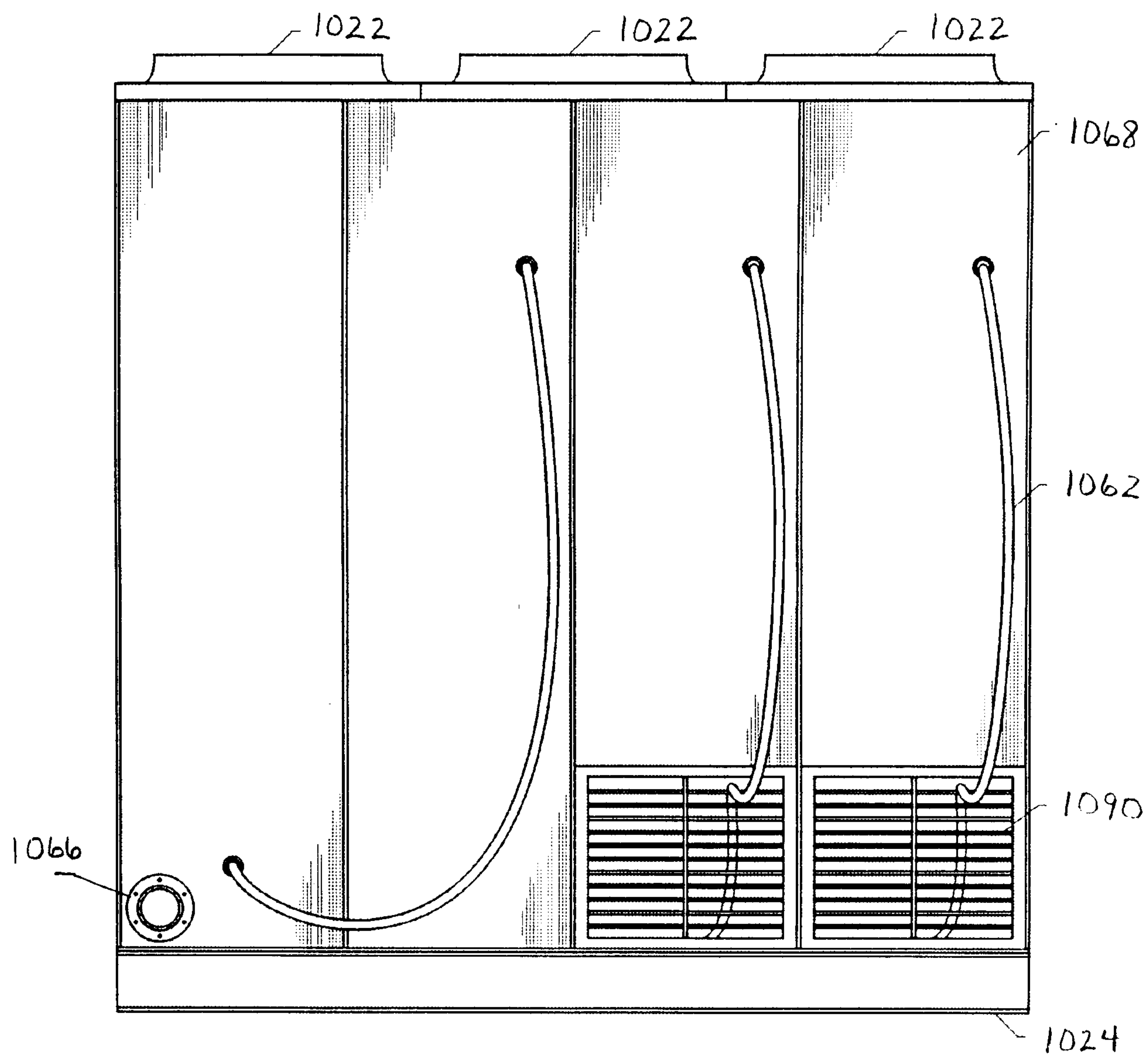


FIG. 11

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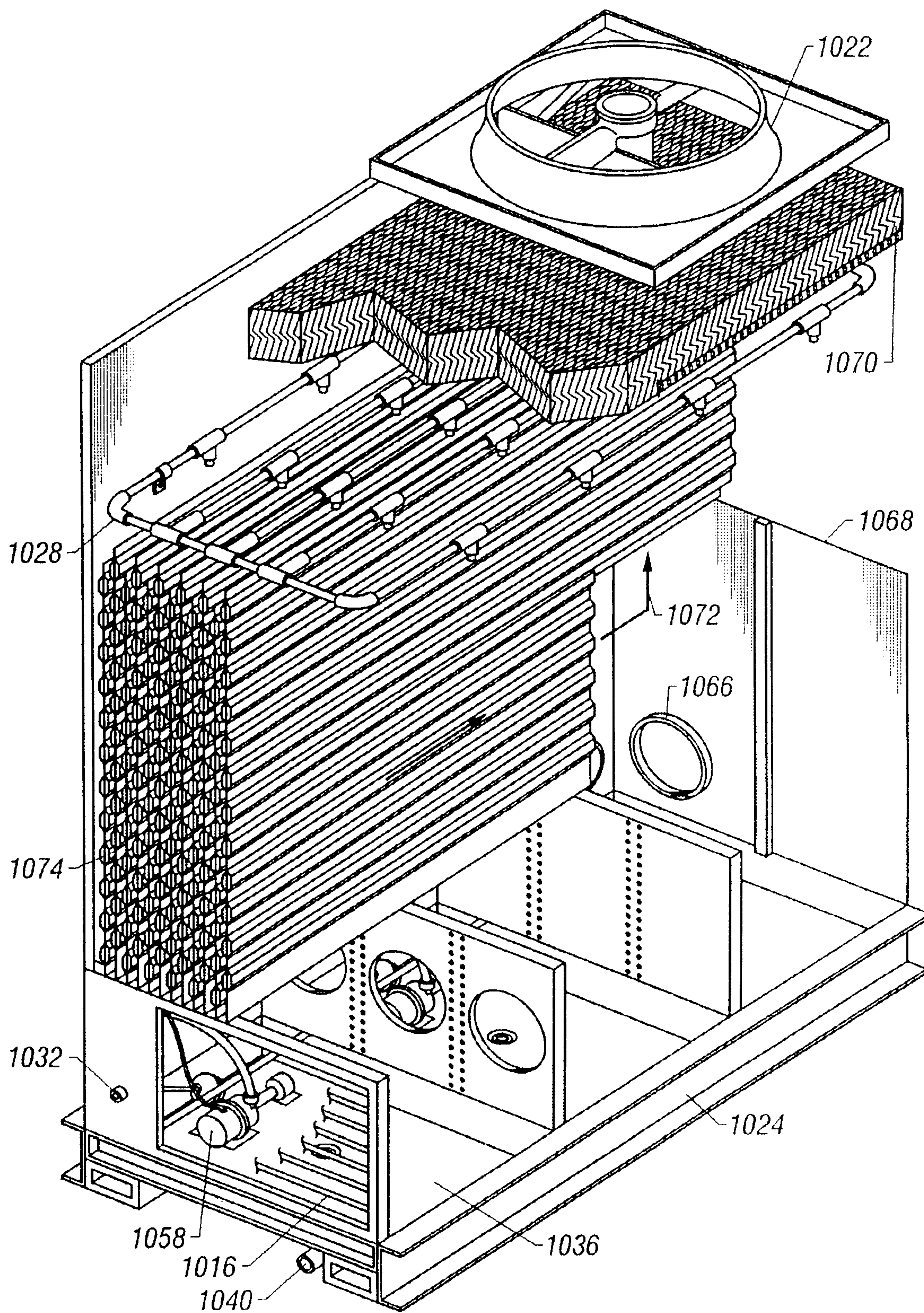


FIG. 12

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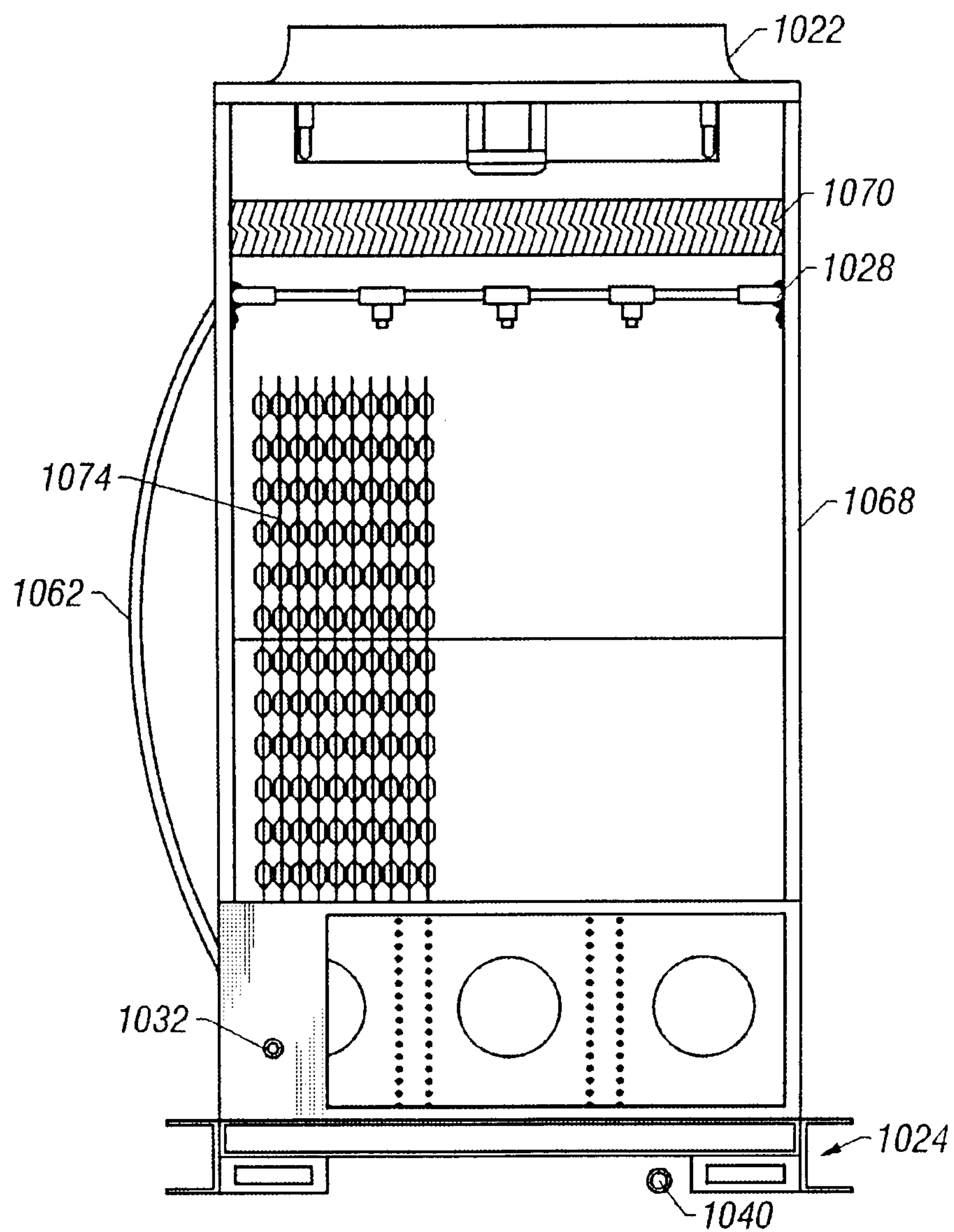


FIG. 13

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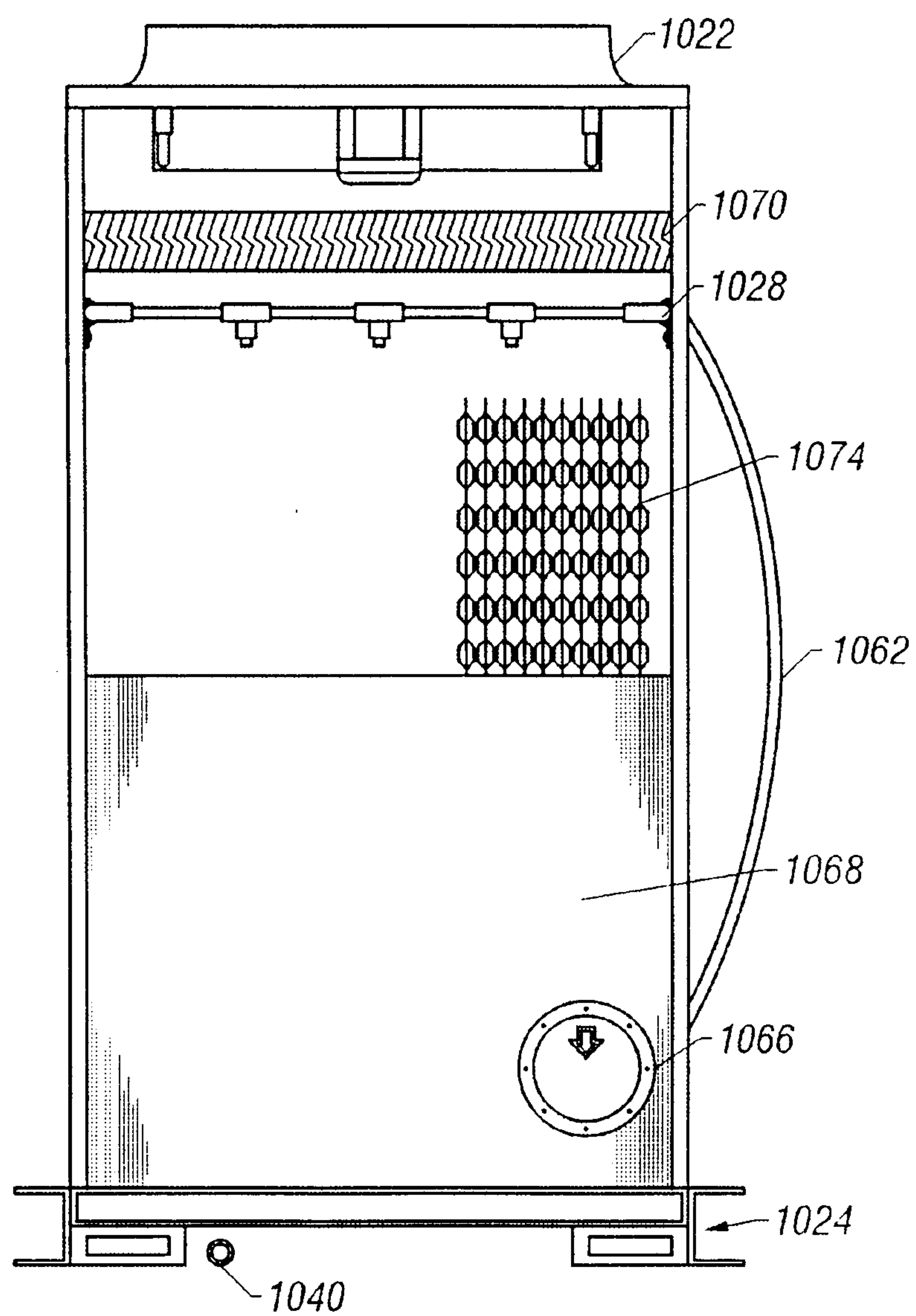


FIG. 14

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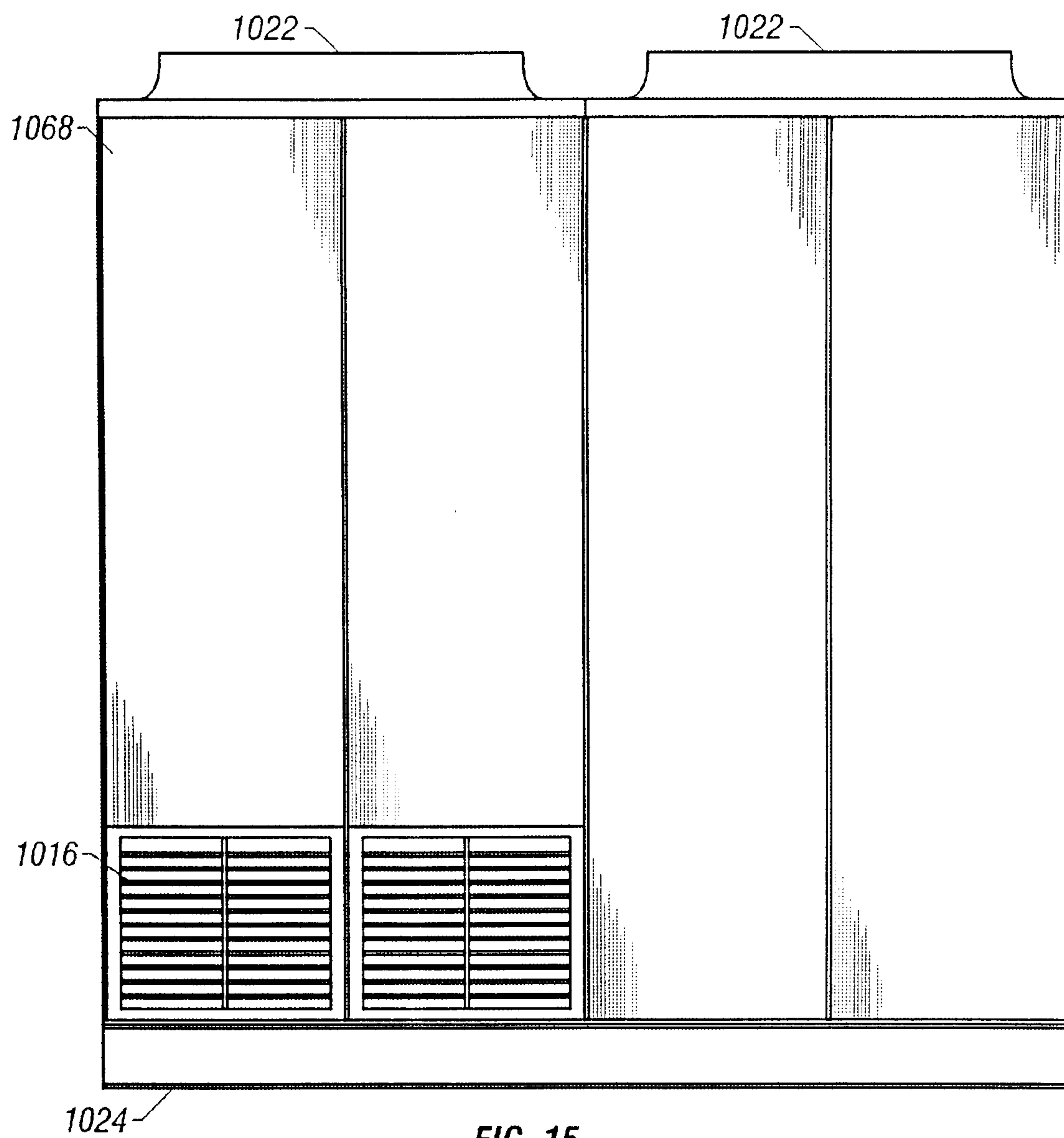


FIG. 15

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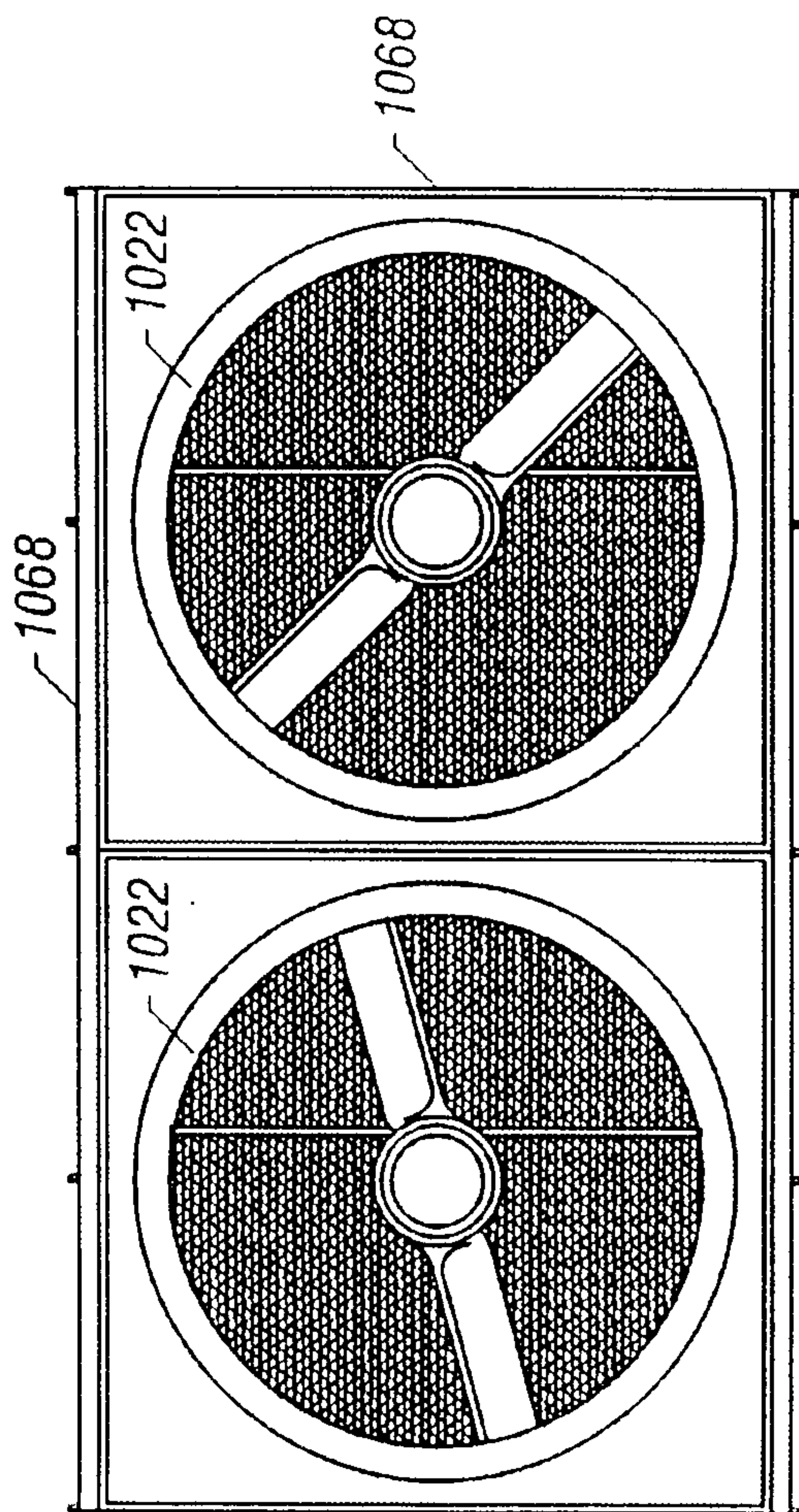


FIG. 16

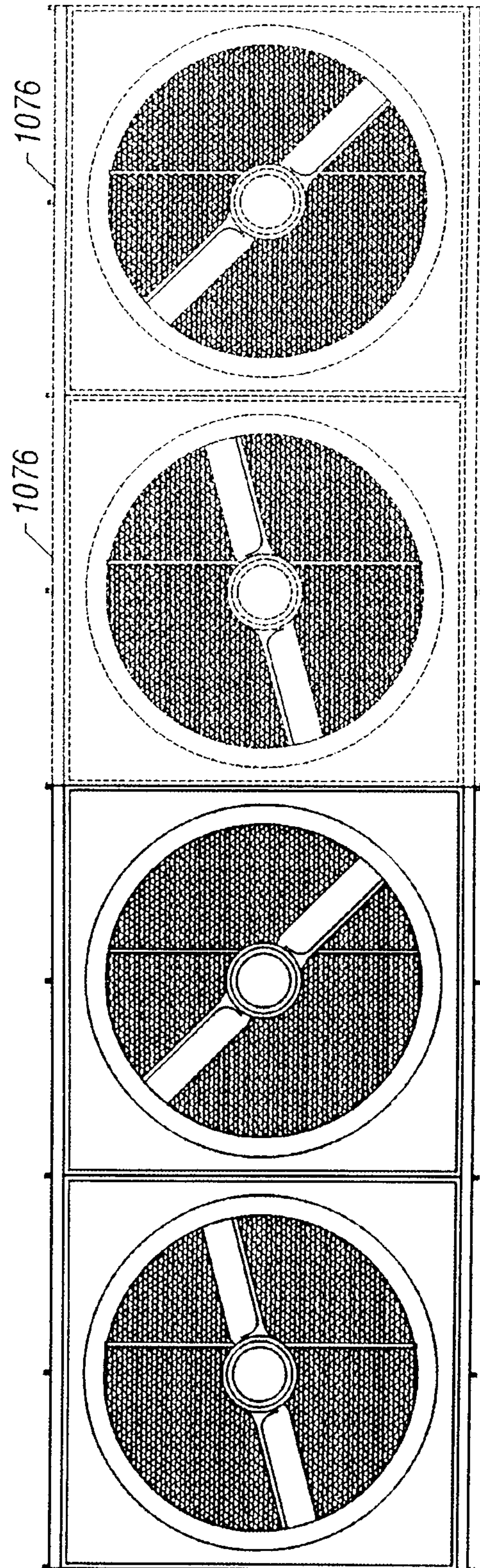
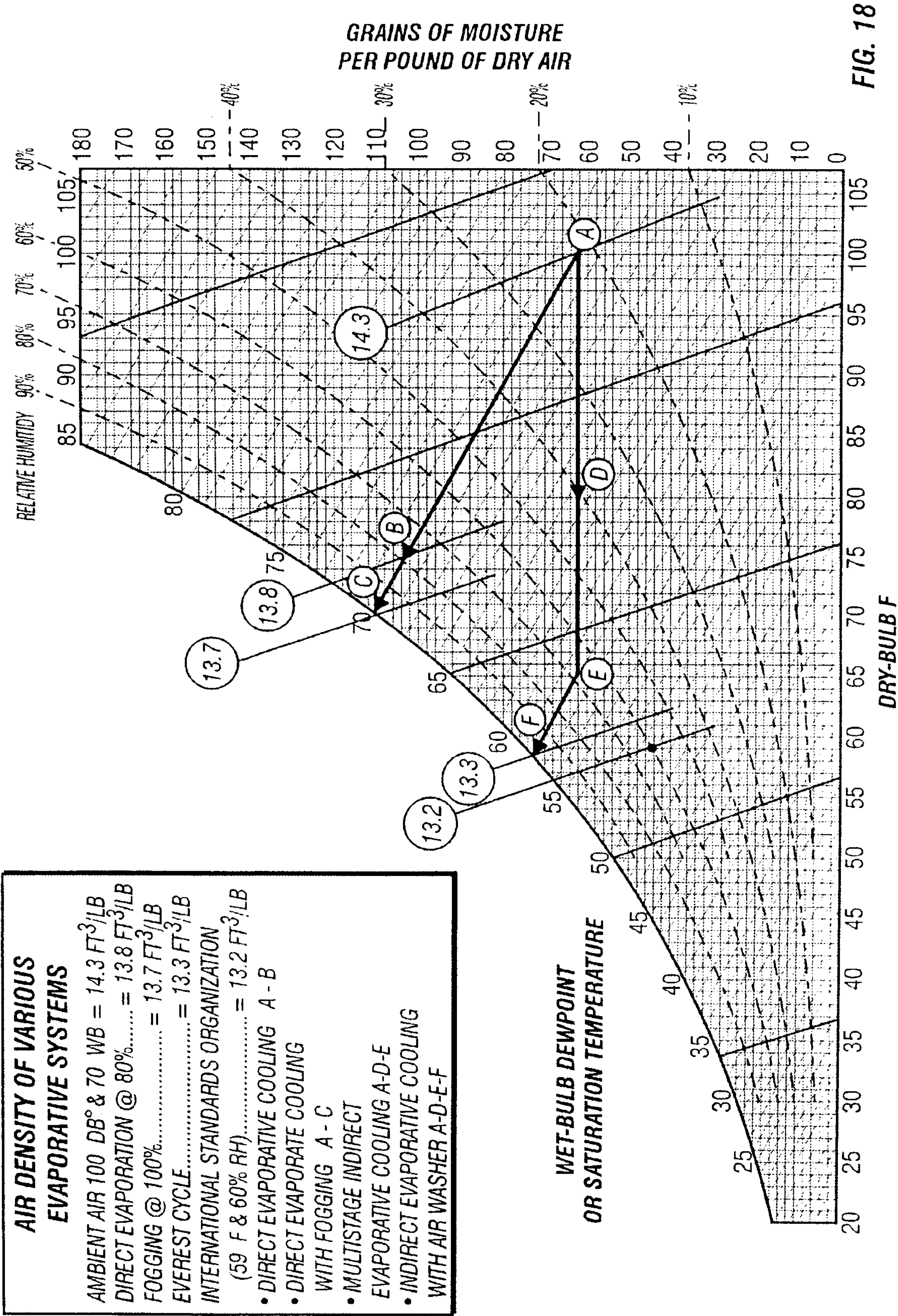


FIG. 17

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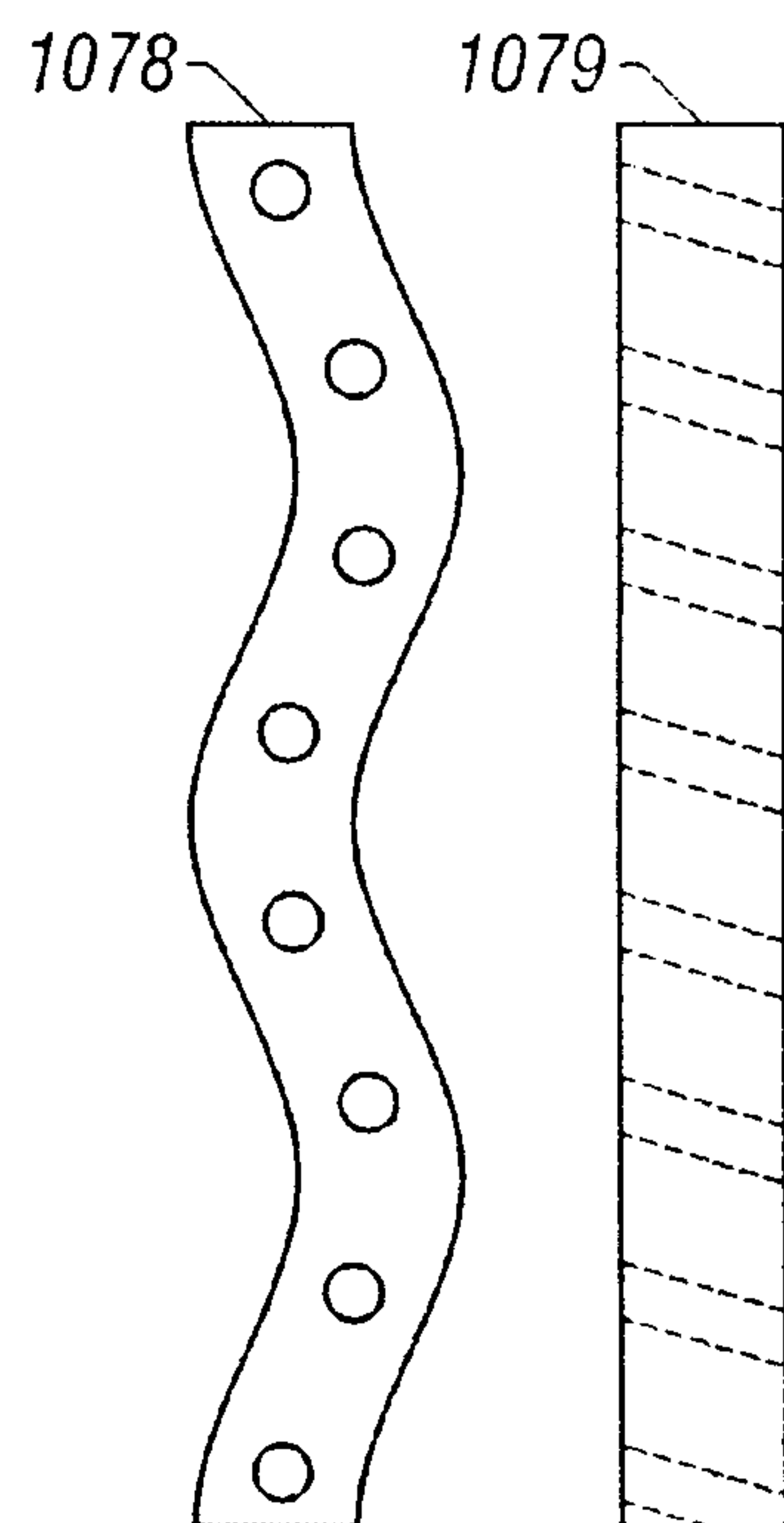


FIG. 19

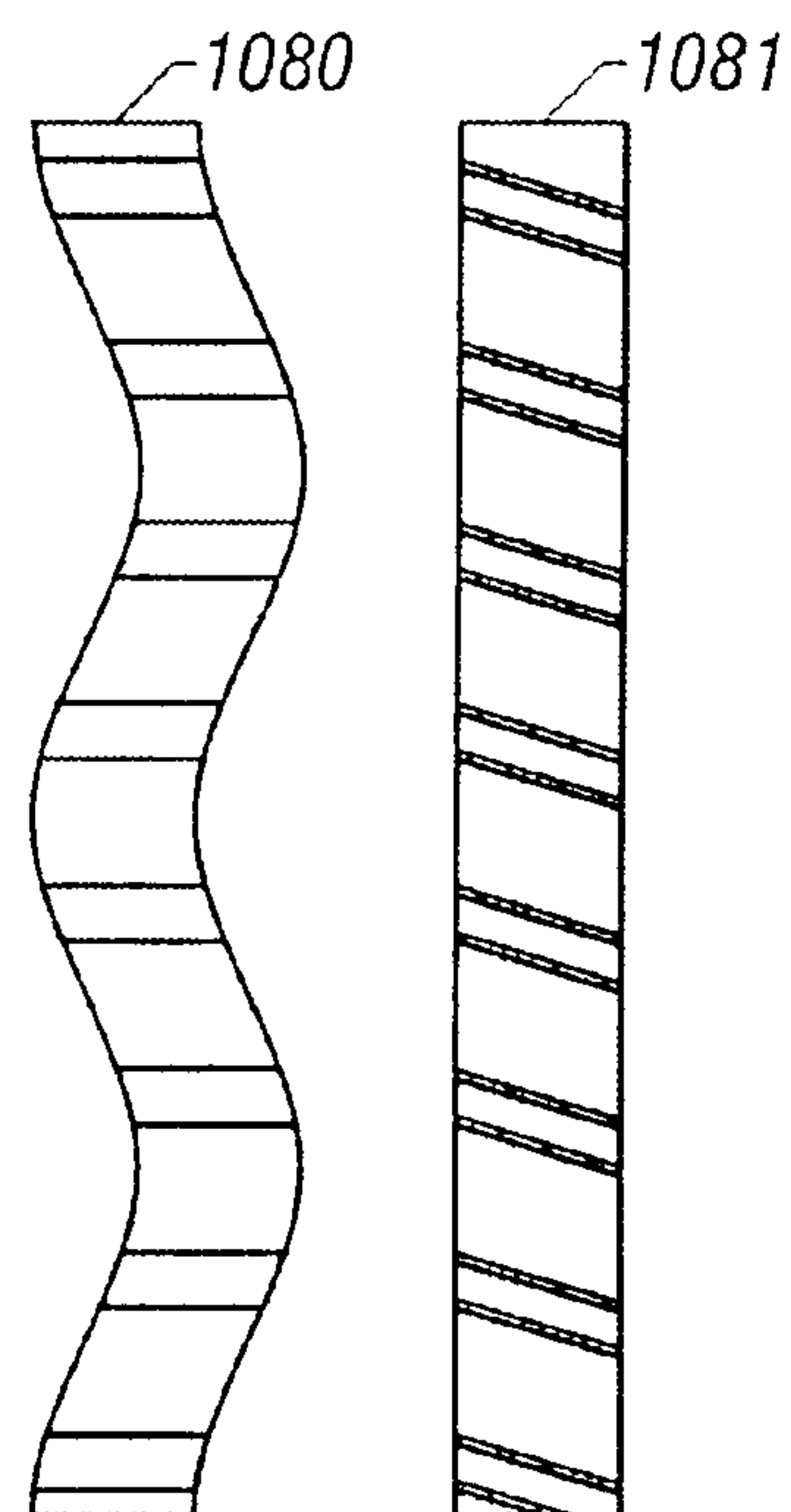


FIG. 20

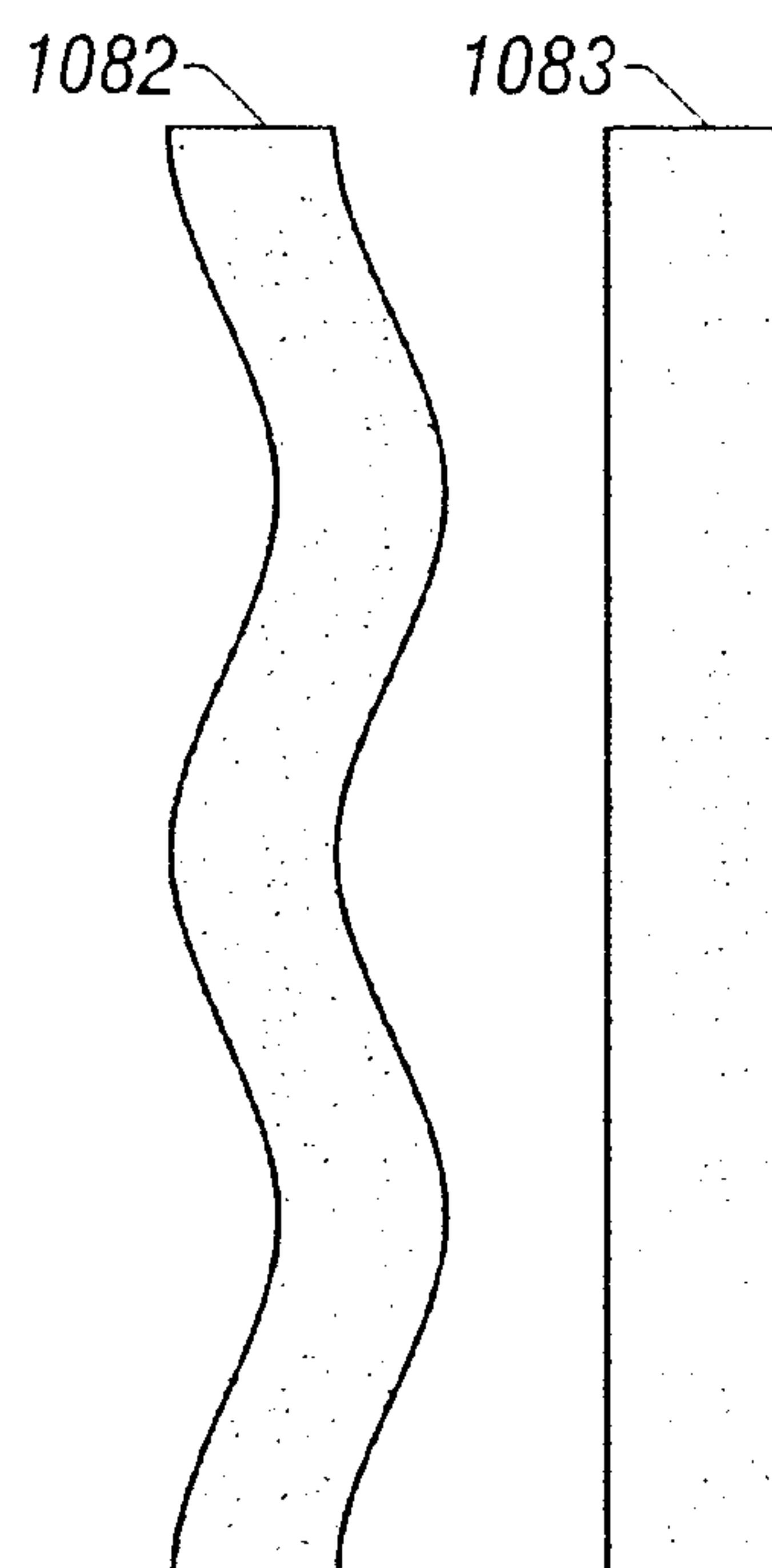


FIG. 21

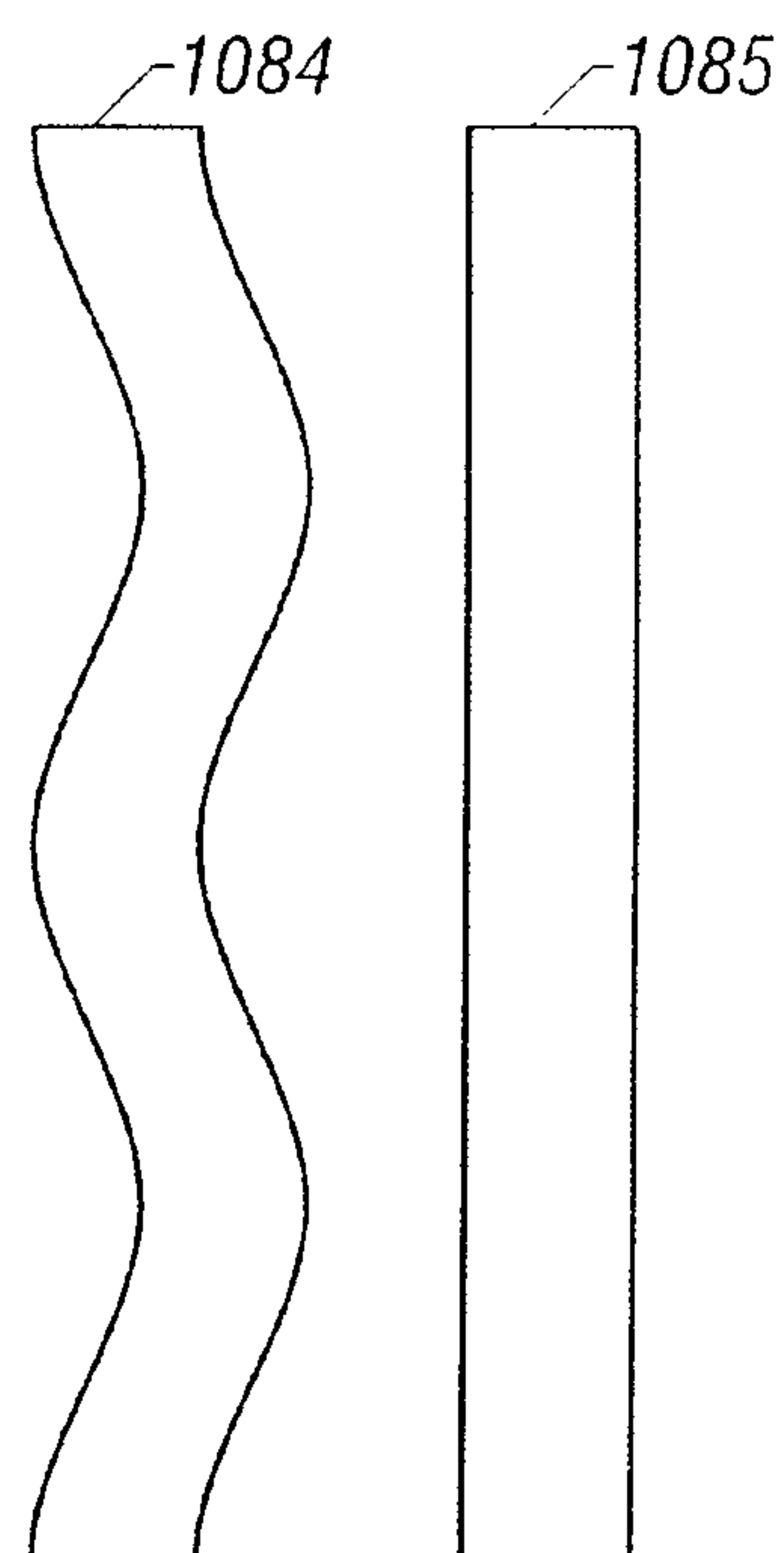


FIG. 22

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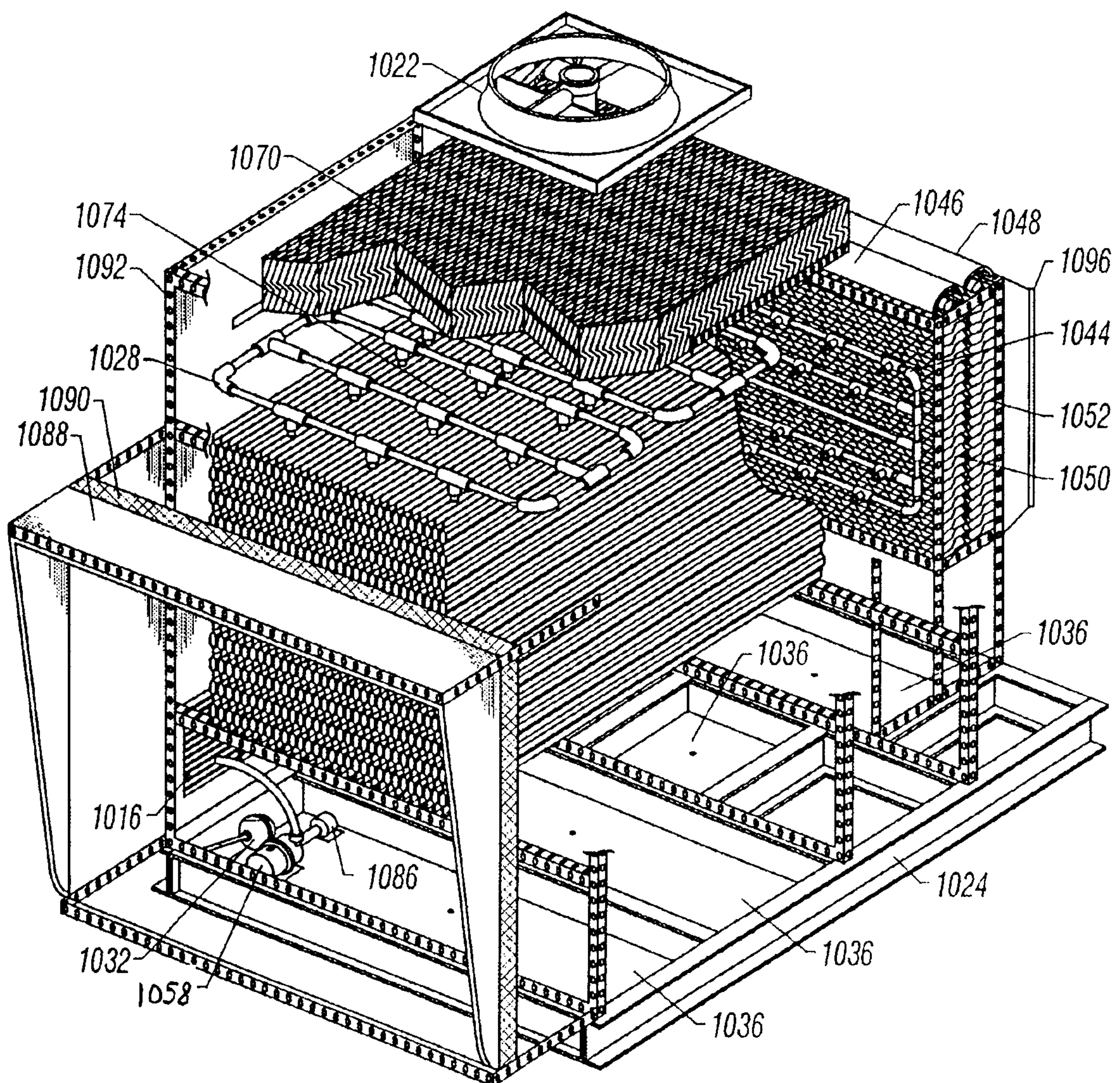


FIG. 23

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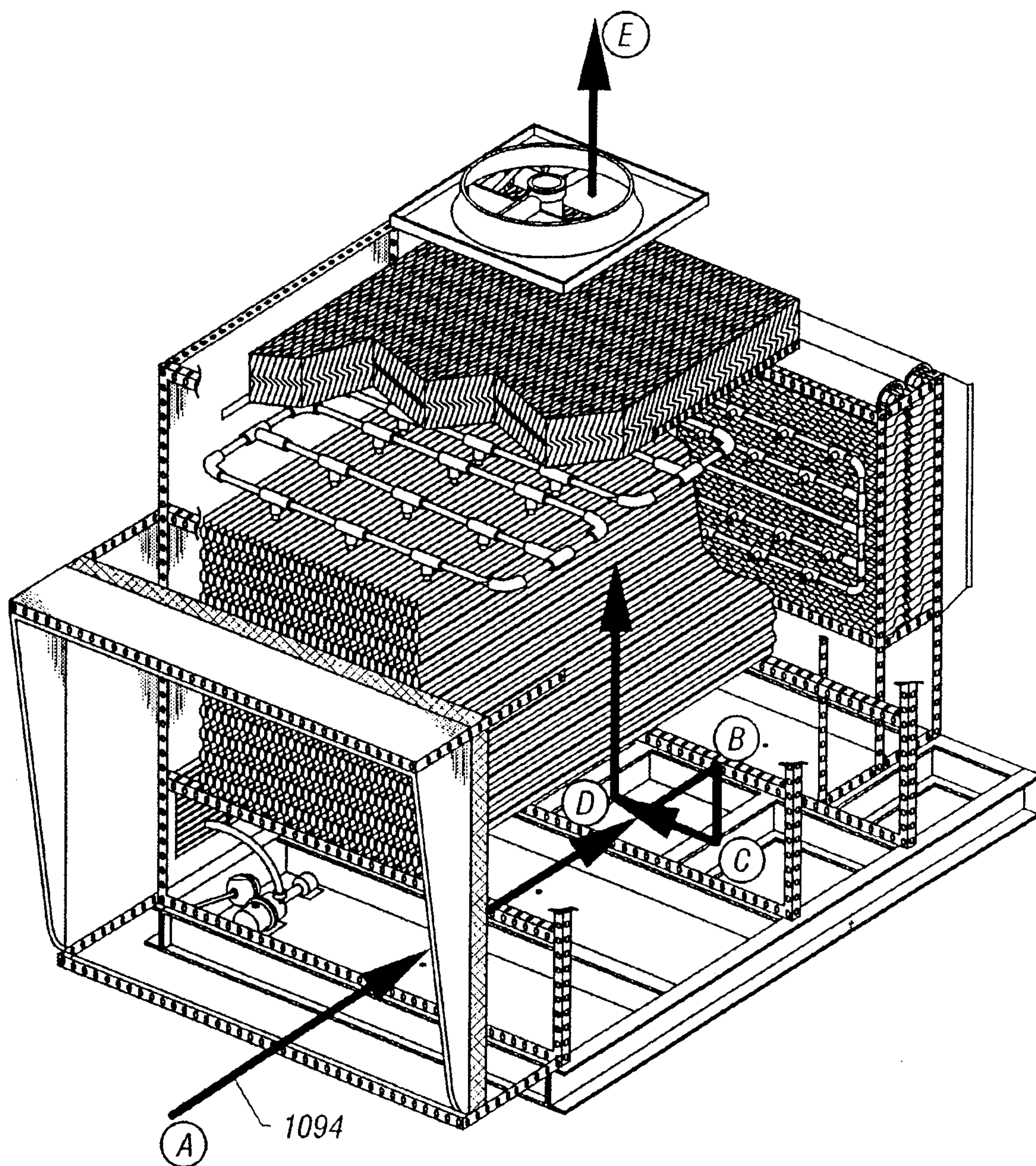


FIG. 24

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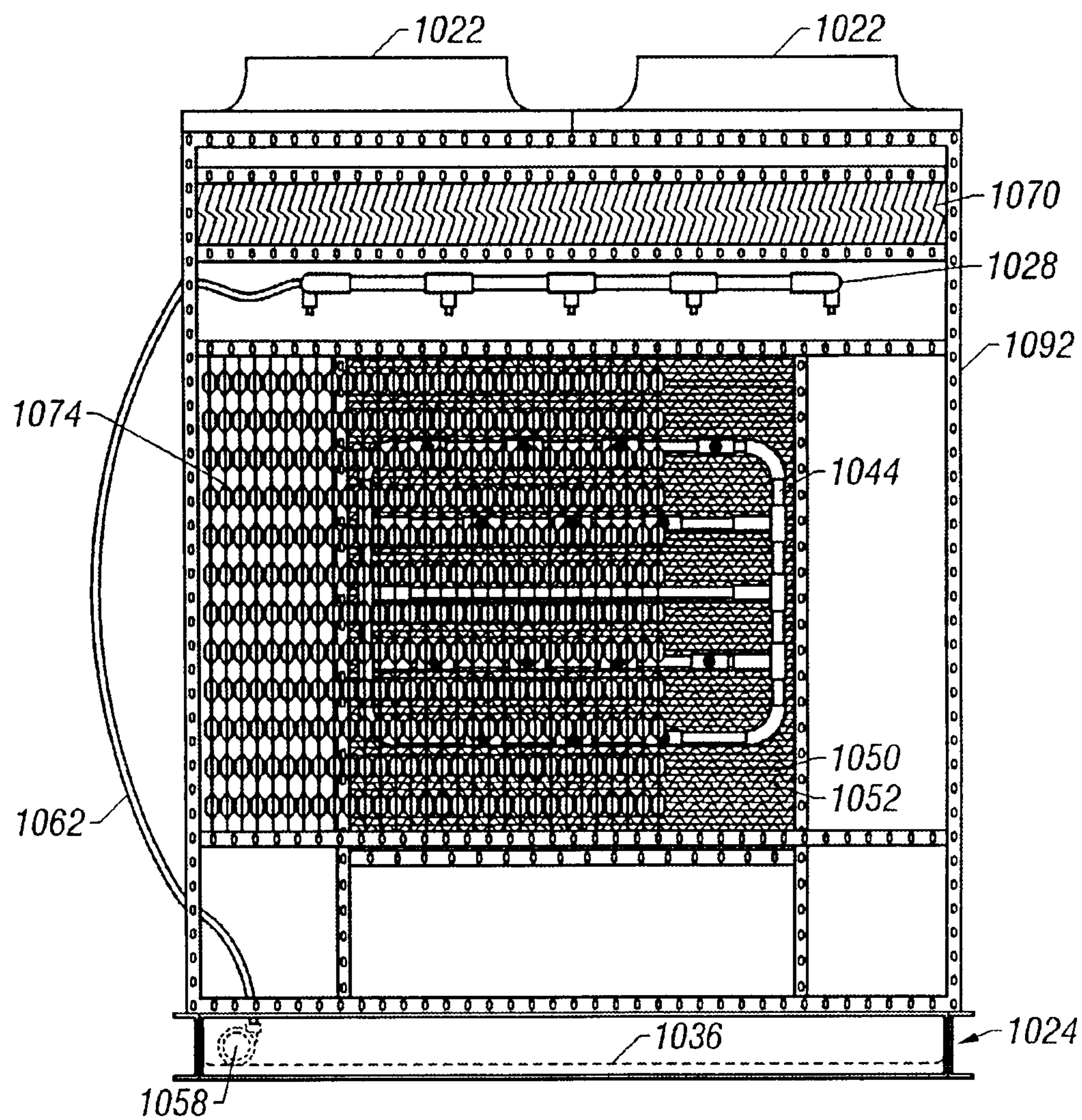


FIG. 25

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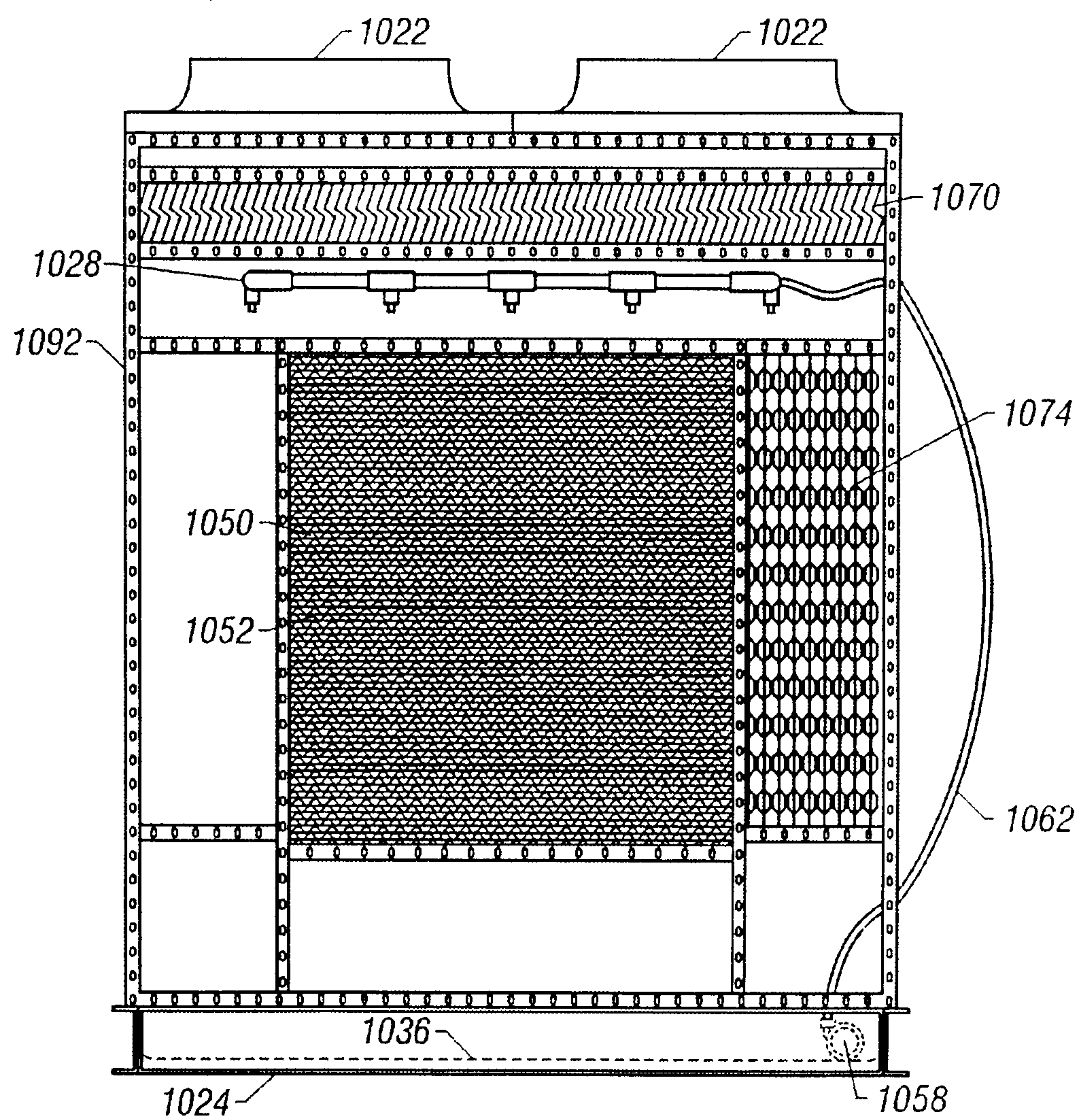
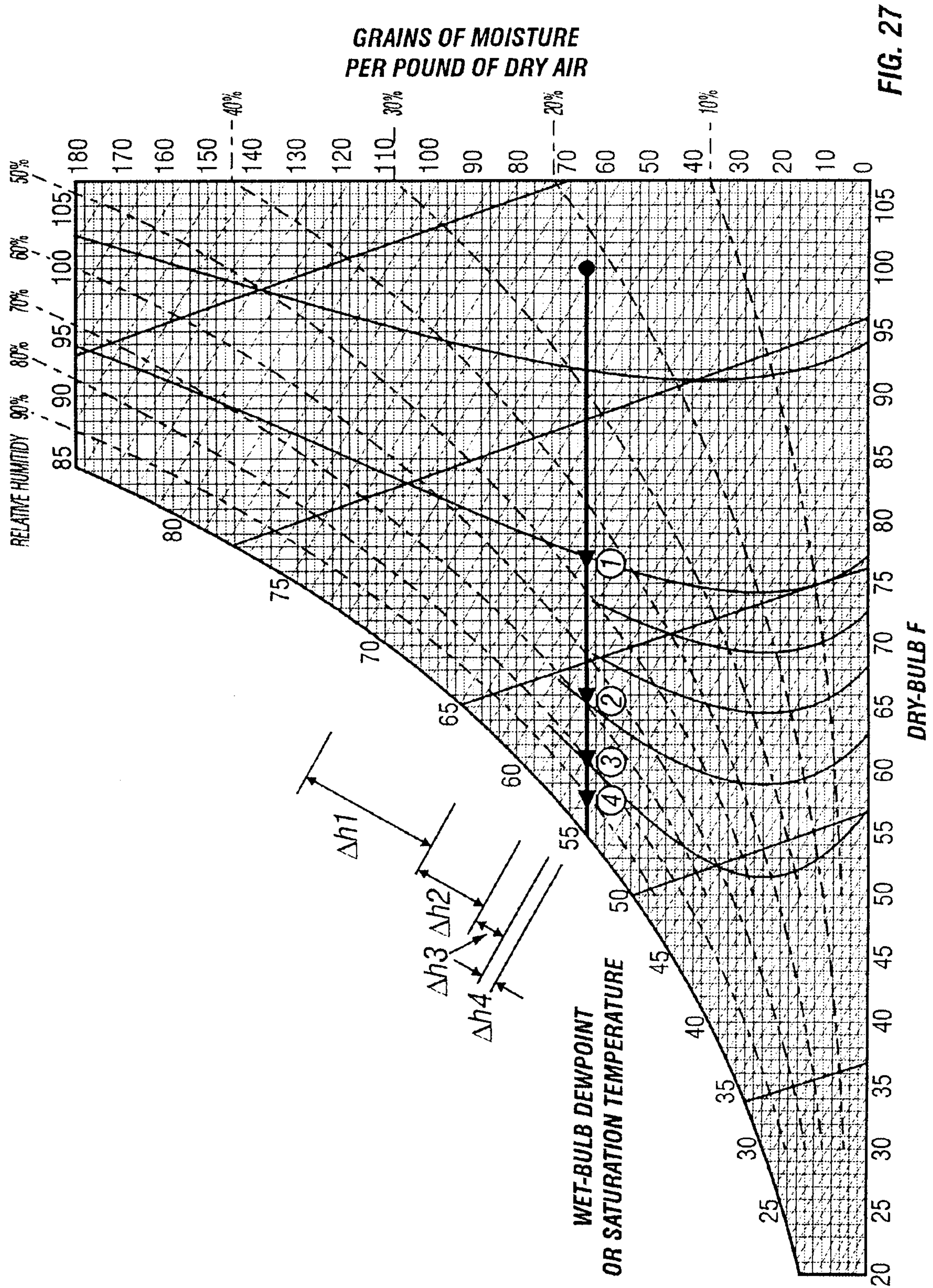


FIG. 26

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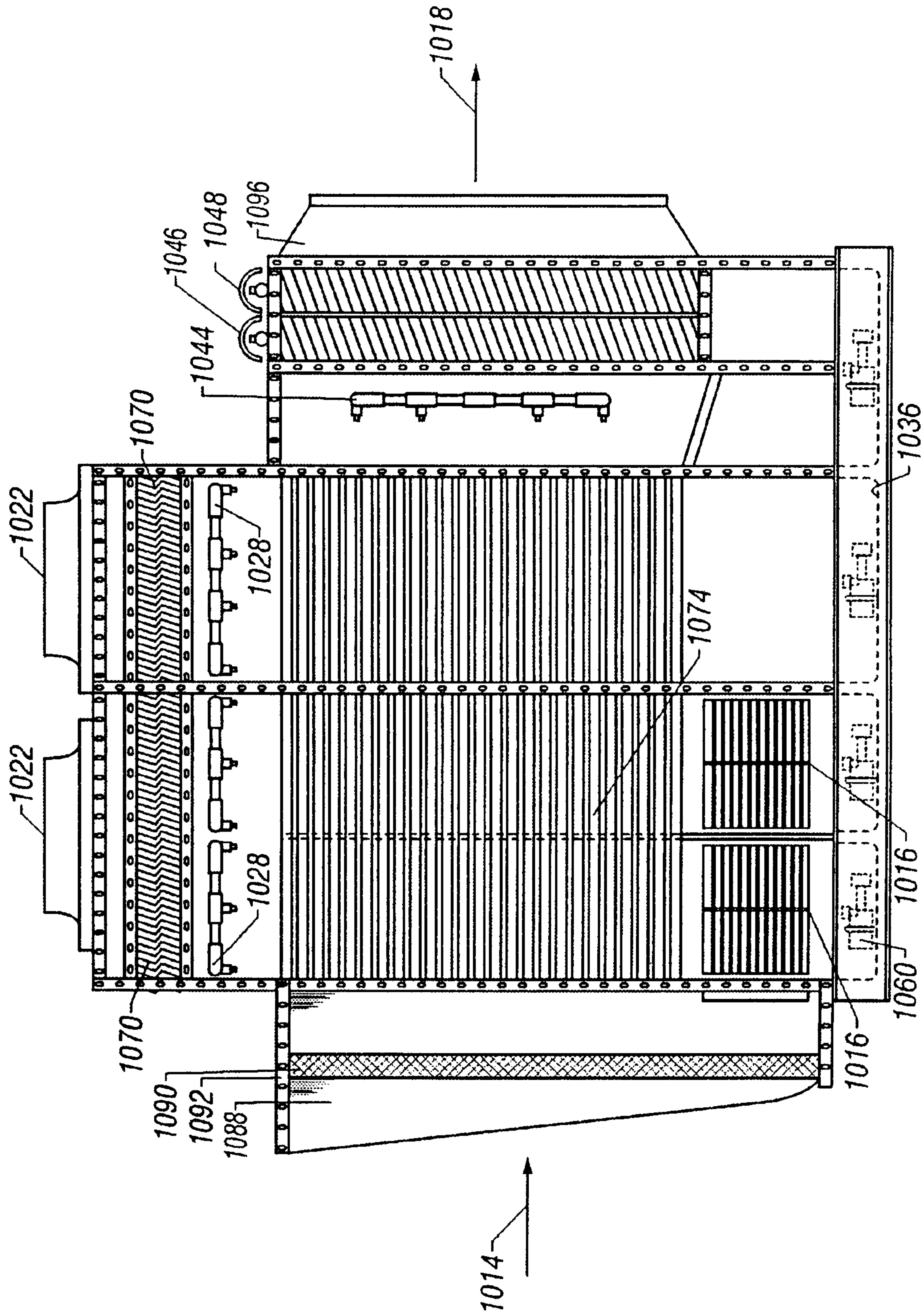


FIG. 28

